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March 1980

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#### Radon in Energy-Efficient Residences

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#### ABSTRACT

Radon concentrations were measured in seventeen houses incorporating energy-saving features, most of which included specific measures to achieve low infiltration rates. Ventilation rates in these houses ranged from 0.04 to 1.05 air changes per hour; corresponding radon concentrations were found to range from 0.6 to  $22 \text{ nCi/m}^3$ . In general, radon concentration tended to increase with decreasing ventilation rate. In one house, a mechanical ventilation system with an air-to-air heat exchanger was installed, and radon concentrations were measured at selected ventilation rates. The correlation between increasing ventilation and decreasing radon concentration was confirmed, and it appears that mechanical ventilation with air-to-air heat exchangers can maintain air quality as well as energy efficiency in many houses where air quality problems exist.

Keywords: energy conservation, heat recovery, indoor air quality, infiltration, mechanical ventilation, radon, residential buildings

Radon and its decay products have always been present as part of the earth's natural radiation burden. Radon emanates from soil, rock, and earth-derived building materials, and can gain entry to buildings through cracks and openings in the structure or around the foundation. Buildings serve to contain any contaminants that enter or are generated within the building itself and, for this reason, these pollutants typically reach higher concentrations indoors than outdoors. Limited surveys in ordinary houses have found mean concentrations of indoor radon ranging from 0.2 to 1.3  $nCi/m^{3^{1}}$  -- five to ten times the outdoor background levels. Prolonged exposure to high concentrations of the radioactive decay products of radon is known to pose a health risk; it is possible that the concentrations in existing houses in the United States may cause thousands of cases of lung cancer each year.<sup>2</sup> Unless special care is taken, indoor concentrations of radon and radon daughters could be further increased by energy-conserving measures that reduce ventilation rates.

Infiltration -- the uncontrolled leakage of air through cracks and gaps in the building envelope -- is the dominant mechanism for ventilating houses during seasons when doors and windows are normally kept closed. In conventional U.S. houses, infiltration rates range from 0.5 to 1.5 air changes per hour (ach)<sup>3</sup>, but construction techniques have been developed and are now being used to achieve infiltration rates as low as 0.1 ach. Reducing infiltration is a cost-effective way to reduce home heating requirements, and a trend toward construction of lowinfiltration houses is rapidly developing in response to the rising cost of energy.

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This building trend, while supporting national efforts to conserve energy, may lead to increased human exposure to radon and radon daughters as well as to other indoor-generated contaminants, such as carbon monoxide, nitrogen oxides and particulates from combustion appliances and tobacco smoke; formaldehyde from urea formaldehyde foam insulation, particleboard and plywood; and other organic contaminants from various chemicals used indoors. Because reducing infiltration clearly affects indoor air quality and poses potential health risks to occupants, it is important that the impact of making houses more energyefficient be studied carefully so that appropriate preventive and/or contaminant control measures can be developed and incorporated into building construction practices.

The concentration of radon-222 in a given house depends on the outdoor levels, the indoor radon sources, and the ventilation rate in the house. Radon source strengths vary significantly from house to house and, in any given house, may vary with time. A steady-state radon concentration is achieved in a house when both the radon source strength and the ventilation rate are held constant for a time long enough for several air changes to have occurred. Based on these assumptions, the steady-state radon activity is represented by the following equation:

$$I = \frac{\sigma + I_o \lambda_v}{\lambda + \lambda_v}$$

(1)

where

I = indoor radon concentration  $(nCi/m^3)$ 

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 $I_{o} = outdoor radon concentration (nCi/m<sup>3</sup>)$ 

 $\sigma = radon \text{ source strength (nCi/m<sup>3</sup>/hr)}$ 

 $\lambda$  = the radioactive decay constant of radon (0.0076/hr)

### $\lambda_{\rm v}$ = ventilation rate (hr<sup>-1</sup>)

Under typical conditions, I >> I<sub>0</sub> and  $\lambda_v$  >>  $\lambda$ , so that equation (1) reduces to

 $\mathbf{I} = \frac{\sigma}{\lambda_{\mathbf{v}}}$ 

(2)

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Thus, under steady-state conditions, indoor radon concentration is inversely proportional to ventilation rate. Because both radon source strength and infiltration rate can also vary significantly with changes in weather conditions, it is not always accurate to assume that they remain constant during a buildup to steady-state conditions, especially when the ventilation rate is very low and the time required to achieve steady state is correspondingly long. This fact contributes to the uncertainty in our results.

In this study, we measured radon concentrations and infiltration rates in seventeen houses in the U.S. and Canada. Three of the houses selected are research or demonstration energy-efficient houses and four are privately owned residences built to assure very low infiltration rates. Eight houses of passive solar design and one conventionally heated house were studied because of the possible significance of rockbed heat storage as an additional radon source.<sup>4</sup> Some of the passive

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solar houses did not have low infiltration rates but most incorporated such energy-conserving measures as weatherstripping and caulking, along with typical passive solar design features. One house was an underground structure having a potential for high radon influx because of its large surface contact with soil.

Sampling was performed under conditions designed to permit the radon concentration to achieve, as nearly as possible, the steady-state levels that would exist if infiltration were the only air-exchange mechanism. To approximate this correspondence, we had the occupants close windows and doors the night before sampling. Grab samples of air were collected in Tedlar<sup>5</sup> bags and returned to our laboratory for analysis with a zinc sulfide scintillation counting system using 100 ml scintillation cells.<sup>6</sup> This method allows accurate measurement of radon in concentrations as low as  $1 \text{ nCi/m}^3$  with counting times of several hours. We also modified Jonassen's method<sup>7</sup> of concentrating air samples so that a three-liter sample could be counted, thus reducing statistical uncertainty to 10% for radon concentrations as low as  $0.2 \text{ nCi/m}^3$  with 30-minute counting periods.

Infiltration was measured by a tracer gas technique.<sup>8</sup> A volume of gas (either ethane or sulfur hexafluoride) was injected into the house and dispersed by means of fans to achieve a homogeneous concentration of about 100 ppm. An infrared analyzer and a chart recorder were used to detect and record the dilution of the gas with time. From the dilution rate, we determined the infiltration rate of the house. The infiltration rate and radon concentrations measured in each house are given in Table 1 and plotted in Figure 1a.

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As the plot reveals, radon concentrations tend to be higher in houses having very low infiltration rates. The figure also demonstrates that radon concentrations in these energy-efficient houses exceed the indoor levels in conventional houses (on the order of  $1 \text{ nCi/m}^3$ ) and, in some cases, reach very high levels -- exceeding  $10 \text{ nCi/m}^3$ . The scatter in the plot reflects variations in radon source strength ( $\sigma$ ); the variations could result from temporal fluctuations in the radon source, from differences in the nature of the sources from house to house, or from differences in design and construction among the houses. There are no obvious design features which account for the differences in source magnitude among these houses. If  $\sigma$  were constant and identical for each house and only the ventilation rate differed, the plot of log(I) versus log ( $\lambda_{v}$ ) would result in a straight line, following equation (2).

To reduce radon-daughter exposure in such tightly constructed houses, three basic measures can be adopted: the first is to reduce the indoor radon source by blocking routes of radon entry into the interior For example, cracks and openings in basement floors and walls space. can be sealed to prevent radon-bearing soil gas from leaking into the This technique has proved effective in houses located in structure. some communities in Canada.<sup>9</sup> The second measure is to remove radon daughters, along with particulates, from the air by means of filtering devices or electrostatic precipitators. The effectiveness of these devices in reducing-radon-daughter concentrations has yet to be evaluated. A third method is to install a mechanical ventilation system to increase air exchange and thereby reduce the concentrations of radon and radon daughters as well as those of all other indoor-generated contaminants. A potentially cost-effective means of maintaining adequate ventilation

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without losing the energy benefits gained by tight construction is to equip the mechanical ventilation system with an air-to-air heat exchanger.<sup>10</sup>

The effectiveness of such a system for controlling radon levels in a tightly constructed building was studied in detail at one energy-efficient house.<sup>11</sup> In the initial survey we measured a radon concentration of 22 nCi/m<sup>3</sup> under steady-state infiltration conditions of about 0.1 ach. During a later study, a heat exchanger was installed and operated for several days at each of four different ventilation rates. Continuous radon measurements were made at these four rates. The radon measurements were also repeated under natural infiltration conditions with the heat exchanger off. The average steady-state radon concentrations measured under these five ventilation conditions, plotted as a function of ventilation rate in Figure 1b, are well fitted by a straight line corresponding to a constant radon source of 2.5 nCi/m<sup>3</sup>/hr. These data demonstrate that increasing ventilation is an effective means of reducing high radon concentrations in tight houses.

These preliminary findings confirm that reduced ventilation rates lead to increased radon concentrations in residential buildings. Where radon source strengths are naturally low, the increased exposure due to reduction in ventilation may be very small, but in houses having high radon source strengths, energy-conserving measures that lower overall infiltration may pose a serious health risk to occupants.

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12) We thank J. Woods and R. Rasmussen of the Energy Research Institute at Iowa State University and R. Dumont of the National Research Council, Division of Building Research (Canada), who measured air infiltration rates at the houses tested in Iowa and Saskatchewan, respectively; R. Kammerud of LBL, who made arrangements for measuring passive solar houses; and P.A. Hillis of LBL, who assisted in analyzing air samples. The work described in this report was funded by the Office of Buildings and Community Systems, Assistant Secretary for Conservation and Solar Energy of the U.S. Department of Energy under contract No. W-7405-ENG-48.

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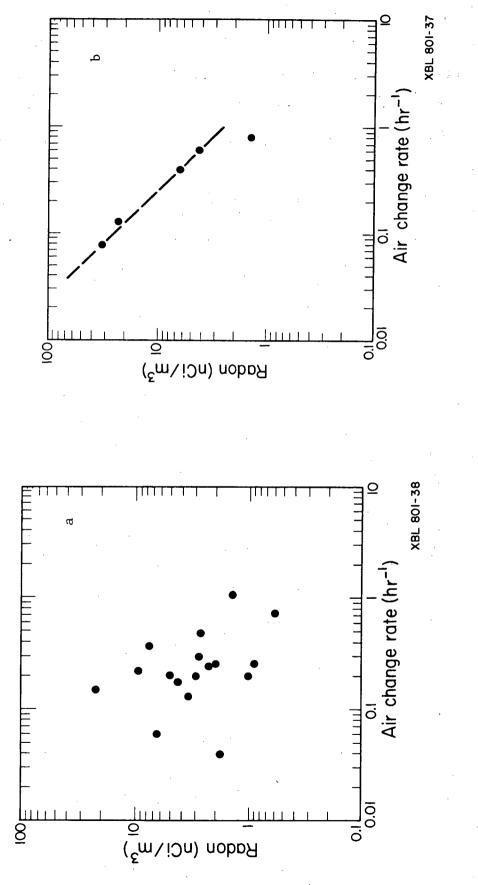


Fig. 1. Radon concentration vs. ventilation rate in (a) seventeen energy-efficient houses where infiltration was the only ventilation mechanism and (b) a single house with a mechanical ventilation system where ventilation rate was varied.

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| Table l. | Radon | Concentration | and | Infiltration | Rates | in | Various | House | Types |
|----------|-------|---------------|-----|--------------|-------|----|---------|-------|-------|
|----------|-------|---------------|-----|--------------|-------|----|---------|-------|-------|

| House Location      | House Type                      | Radon<br>Concentration<br>(nCi/m <sup>3</sup> ) | Infiltration<br>Rate (ach) |  |
|---------------------|---------------------------------|---|----------------------------|--|
| Minnesota           | Infiltration reduction measures | 1.8   | 0.04                       |  |
| Minnesota           | Infiltration reduction measures | 6.5   | 0.06                       |  |
| Texas               | Underground                     | 3+5   | 0.13                       |  |
| Maryland            | Energy research house           | 22  | 0.15                       |  |
| Illinois            | Infiltration reduction measures | 4.3   | 0.18                       |  |
| Iowa                | Energy research house           | 1.0   | 0.20*                      |  |
| Saskatchewan,       | Infiltration reduction measures | 3.0   | 0.20                       |  |
| Canada              |                                 |   |                            |  |
| California          | Energy Research House           | 5.0   | 0.20                       |  |
| New Mexico          | Passive Solar                   | 9.3   | 0.22                       |  |
| New Mexico          | Passive Solar                   | 2.3   | 0.24                       |  |
| New Mexico          | Passive Solar                   | 2.0   | 0.26                       |  |
| New Mexico          | Passive Solar                   | 0.9   | 0.26                       |  |
| New Mexico          | Conventional heating            | 2.8   | 0.30                       |  |
| New M <b>exi</b> co | Passive Solar                   | . 7.6   | 0•37                       |  |
| New Mexico          | Passive Solar                   | 2.7   | 0.48                       |  |
| New Mexico          | Passive Solar                   | 0.6   | 0.73                       |  |
| New Mexico          | Passive Solar                   | 1.4   | 1.05                       |  |

\*Infiltration rate measured by researchers at Iowa State University.

†Infiltration rate measured by researchers at the National Research Council, Division of Building Research (Canada).

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