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EARTH SCIENCES DIVISION

MASTER

PROGRAM ROCMAS: INTRODUCTION AND USER'S GUIDE

J. Noorishad and M.S. Ayatollahi

September 1980



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PROGRAM ROCMAS: INTRODUCTION AND USER'S GUIDE

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TABLE OF CONTENTS

	<u>Page</u>
INTRODUCTION	1
I. GOVERNING EQUATIONS	1
Pressure-Strain Equation	2
Stress-Strain Relation	2
Load Balance	3
II. NUMERICAL METHOD	4
Solution Scheme	6
III. COMPUTER CODE	7
Documentation and Availability	7
Spatial Grid	7
Material Properties	7
Fluid Properties	8
Initial Conditions	8
Boundary Conditions	8
Time Stepping and Solution Control	8
Output	8
IV. VALIDATION	9
V. APPLICATION	11
VI. SUMMARY	17
VII. REFERENCES	13
VIII. USER'S GUIDE	16
APPENDIX I. SAMPLE PROBLEM WITH SAMPLE INPUT OUTPUT	27
Sample Problem	29
Sample Input Data Preparation for Coupled Problems	33
Sample Output for Uncoupled Problem	37
I. General parameters and material properties	37
II. Displacement and pressure results	38
III. Stress and flow results	39
APPENDIX II. LISTING OF FORTRAN IV SOURCE PROGRAM	41

INTRODUCTION

ROCMAS (ROCK MASS) is a finite-element program for coupled flow and stress in deformable, saturated, fractured rock medium. The two-dimensional code combines the capability of isothermal transient pressure analysis and stress-strain analysis in formations with discrete fractures and porous blocks. Coupling of the pressure field and the mechanical deformation is founded on the extension of Biot's consolidation theory for porous elastic medium to nonlinear fracture behavior. The current version of the model is described by Noorishad [18]. Summary of early developments and related information are in Ayatollahi [1]. The early version of this code is known as PORFRC.

I. GOVERNING EQUATIONS

In this model, the fluid movement and the solid deformation are coupled. Each point in space, either inside a discrete fracture or within a rock block, has a pressure variable P and a solid displacement vector \bar{u} . The pressure field determines the fluid flow. The coupling between P and \bar{u} can be described in the following loop. As the pressure changes, the effective stress acting on the rock solid changes accordingly and affects the displacement or strain of the solid. The displacement of solid changes the flow path of fluid and results in changes in the pressure field. The last coupling step is especially important for fractures. The fracture flow is very sensitive to the aperture $2b$. The fracture-specific permeability $k^f = (2b)^2/12$ for parallel-plate laminar flow is used in this model.

Pressure-Strain Equation

The mathematical form of the coupling between the fluid flow and solid displacement can be written down as a set of three equations for the pressure-strain, strain-stress, and stress-load balance relations. The first fluid flow equation is

$$\frac{1}{M^i} \frac{\partial P}{\partial t} - \alpha^i \frac{\partial \epsilon}{\partial t} = \nabla \cdot \frac{k^i}{\mu} \nabla P$$

where α^i and M^i ($i =$ fractures or rock medium blocks) are material properties (Biot constants) representing the responses of fluid mass content to changes in pressure and changes in volumetric strain ϵ . Depending on the boundary conditions, the derivative $\partial \epsilon / \partial t$ in some cases can be approximated in terms of the pressure derivative $\partial P / \partial t$. The fluid flow equation will be reduced to a simple transient pressure equation with the storage coefficient in front of $\partial P / \partial t$ determined by the porosity and compressibilities of fluid and void structures.

Stress-Strain Relation

In more general cases, the volumetric strain $\epsilon = \epsilon_{xx} + \epsilon_{zz}$ depends on the effective stress field. The pressure counteracts normal to the fluid-solid interfaces. The effective stress-strain relation can be formally written in the form of Hook's Law [2-5]:

$$\tau = \alpha^i P \bar{I} = \bar{C}^i : \epsilon$$

For isotropic elastic porous rock medium, the components of the tensor \bar{C}^i can

be expressed in terms of two elastic constants, e.g., Young's modulus and Poisson's ratio. For anisotropic, inelastic deformable fractures, the stress-strain-strain relation is very nonlinear. In this model, a nonlinear normal stress-normal displacement relation and a nonlinear shear stress-shear displacement relation are used [12]. The normal and shear stiffness (change of stress per unit change of displacement) as functions of stresses characterize the fracture behavior. The displacement \bar{u} is simply related to the strain $\bar{\epsilon}$ by the component definition:

$$\epsilon_{i,j} = 0.5 \left(\frac{\partial u_i}{\partial x_j} + \frac{\partial u_j}{\partial x_i} \right)$$

Load Balance

The third equation for the unknowns P , $\bar{\tau}$ and $\bar{\epsilon}$ is Newton's first law of static equilibrium applied to an infinitesimal volume element of the fluid-filled medium

$$\nabla \cdot \bar{\tau} + \rho_s \bar{f} = 0$$

where ρ_s is the bulk mass density and \bar{f} is the body force. One body force or volumetric force is the gravity. Both the gravity effects on the fluid and rock can be taken into account. Gravitational drainage of fluid can be modeled.

II. NUMERICAL METHOD

Having established the governing and constitutive relations for fractures and solids from structural and fluid flow analysis points of view, the media under consideration could be thought to be composed of two materials with known behaviors. Analysis of such media for coupled stress and fluid flow behavior is made feasible by application of a numerical method. The method starts with adoption of a variational principle [8,9]. The variational form, written for general initial and boundary conditions, includes all the terms of the static-structural analysis variational and those of the transient fluid flow analysis in porous media. A coupling term links the two functions [1,18]. A finite-element discretization is used to discretize the space domain. The two-dimensional space is decomposed into finite element quadrilateral domains with four-corner nodes[22]. Each node has the values of three variables: the pressure P and the two components of solid displacement \bar{u} . Isoparametric bilinear polynomial basis functions are used to interpolate from the nodal values to the space within an element representing the porous rock medium. For a fracture, it is assumed that the aperture is small and fluid flow is along the fracture surfaces. The pressure difference between adjacent nodes across the aperture is negligible and a one-dimensional element can be used for interpolating between two end point pressures [21]. For the fracture displacements, it is convenient to take the same spatial (global) coordinates for each pair of points across the small aperture for the four-corner element. However, the relative movements of the surfaces in the direction vertical to the fracture plane and along the fracture are important for

the structure analysis. The fracture element in terms of these relative displacements is used [12].

Taking variation of the discretized variational principle with respect to u and p results in the following matrix equations:

$$[K] \{\bar{u}\} + [C] \{p\} = \{F\}$$

$$[C]^T \{\bar{u}\} + ([E] + I * [H]) \{p\} = I * \{Q\}$$

where the matrix $[K]$ contains the coefficients of the stiffness of stress displacement of both inelastic fractures and elastic medium, $[C]$ the Biot coupling coefficients, $[E]$ fluid storage coefficients, $[H]$ fluid hydraulic conductivities, and $\{Q\}$ the fluid boundary fluxes. The column vector $\{\bar{u}\}$ contains the $2N$ nodal values of \bar{u} for the m porous nodes and $N - m$ fracture nodes, $\{p\}$ the N values of p , and $\{F\}$ the body force and boundary loads.

Time Discretization: The notation $I*$ in the matrix equation represents the time integration from 0 to t . To step from t to $t+\Delta t$, this model uses a predictor-corrector scheme. The solution is first predicted at $t+\Delta t$ with

2 * 3 * 1

$$I * p_{\hat{t}} = A(t+\Delta t) = \int_0^{t+\Delta t} P(\tau) d\tau = A(t) + \frac{1}{2} \Delta t (P_t + P_{t+\Delta t})$$

and then it is corrected by linear interpolation

$$I * p_t = A(t + \Delta t) = A(t) + \frac{1}{2} \Delta t (P_t + P_{t+\Delta t})$$

the unknown at $t+\Delta t$ is given by

$$P_{t+\Delta t} = P_t + \frac{1}{\theta} (P_{t+\theta\Delta t} + P_t)$$

It is noted that $\theta = 1$ is the central differencing Crank-Nicholson scheme. The coefficient $\theta > 1$ is used to damp out the numerical oscillation while slightly slowing down the convergence rate [20].

Solution Scheme

The nonlinear behavior of fracture stress-displacement is dealt with by the stiffness perturbation technique [12] during each time step. The stiffness matrix depends on the displacement when the displacement are out of the linear range. Iterations proceed until the stiffness matrix stabilizes within convergent criteria.

Within one iteration the matrix equation of $\{u\}$ and $\{P\}$ is solved by a direct procedure. The matrix is decomposed into lower and upper triangular matrices by the Gaussian LU decomposition method [2]. This reduces the matrix equation into two triangular systems which can be solved by backward and forward substitution procedures.

III. COMPUTER CODE

Documentation and Availability

The code is written in FORTRAN IV and presently being used on the CDC 7600 at LBL. Set-up of the data follows the organization of other finite-element programs at the University of California, Berkeley. Familiar options of two-dimensional finite-element (2-D FE) stress and strain analysis codes and two-dimensional finite-element (2-D FE) fluid flow codes are included in this code.

Spatial Grid

The two-dimensional grid consists of four-corner quadrilateral elements for the porous rock medium and two-node elements for the discrete fractures. The fractures can extend from one boundary to another, intersect each other, or can be isolated in the porous rock medium. An axisymmetric grid is also used.

Material Properties

The constant permeability of the porous rock medium and the initial aperture of the fracture are input parameters. For coupled calculations, the pressure- and stress-induced changes in displacement will be used to update the aperture and the fracture permeability.

The parameters α^i in the fluid flow equation for the porous rock medium and fracture can be estimated in general from the porosity and the compressibility of fluid as $1/(\alpha C_f)$. The coupling constants α^i are dimensionless.

$\alpha^i = 0$ decouples the pressure calculations from the stress-strain analysis.

For material with highly incompressible solid grains, $\alpha \approx 1$.

The mechanical properties required are Young's modulus and Poisson's ratio for the elastic porous rock medium and the initial normal stiffness, tangential stiffness, cohesion, and angle of friction for the fracture.

Fluid Properties

The fluid density and viscosity are input parameters.

Initial Conditions

Distribution of stresses, pressure and displacement can be specified at initial or program restarting time.

Boundary Conditions

Pressure and flux boundary conditions can be specified for the fluid flow. Static load and displacement boundary conditions can be specified for the stress-strain analysis.

Time Stepping and Solution Control

The time step can be increased logarithmically. A convergent criterion is specified on the stiffness difference in the iteration-perturbation procedure to handle the nonlinear fracture behavior.

Output

At the end of each time step, the pressure, displacement and the flow flux and the stress components on the elements can be printed. Graphic output of the mesh with the plot of the principal components of stress, and displacement are generated in the program.

IV. VALIDATION

The code is developed from an early iterative finite element program with steady state flow and static force-displacement analysis in jointed formation with impermeable rock [17]. Most of the efforts to validate this code are on the transient fluid flow behavior in fractures embedded in porous rock medium. Validation of the capability to handle coupling between transient fluid flow and stress-strain analysis is limited due to absence of both the analytic solutions and other numerical results. The documented tests [1] on the transient fluid flow in porous media and in fractures will be listed below.

1. Continuous Finite-Radius Well Source: The early time transient pressure responses of an axisymmetric flow to a producing well are compared with the analytic solution of Mueller and Witherspoon [15].
2. Finite Axisymmetric Aquifer: The late time pressure responses with no flow as well as constant outer boundaries are compared with the analytic solutions of Muskat [16].
3. Vertical Fractures: The pressure responses for a single vertical fracture and two perpendicular vertical fractures intersecting a well at the center of a rectangular porous medium are compared with the analytic solutions of Raghavan [19]. Geometry, mesh, input data, and the results for the latter problem are given at the end.
4. Vertical Fracture Near a Well: The pressure responses for an observation well in a system with a fracture not intersecting, but aligned with a producing

and an observation well, are compared with the analytic solution of Heber-Cinco et al. [13].

5. Horizontal Fracture: The pressure responses for a horizontal fracture located at the center of an aquifer and intersecting a well in an axisymmetric region are compared with the analytic solution of Gringarten and Ramey [11].

V. APPLICATION

The importance of the coupling between the fluid flow and the mechanical deformation in fractures has been analyzed by the iterative steady state version of this code. The flow through a jointed dam foundation has been simulated [17]. It is noted that a deformable fracture system has lower flow through the foundation and higher uplift pressure than a rigid network of fractures. The code has also been used in the analyses of laboratory experiments of large rock samples with tension fractures and of field tests in shallow fractured formations [7]. It is well known that high pressure at a wellbore can open up the fractures and will result in a high injection rate while low pressure at a wellbore during withdrawal can close the fracture and decrease the hydraulic conductivity of flow.

This recently developed transient code is well suited for a thorough study of the mentioned effects due to the fact that it can provide additional insight to the very important transient processes of the coupling phenomena.

VI. SUMMARY

This model is for the study of coupled fluid flow and stress in deformable fractured rock masses. The effective mass theory of Biot is used to relate the pressure changes with the displacements of the rock matrix. The deformation of the fracture surfaces in turn affects the fracture flow through the sensitive dependence of permeability on aperture.

The code combines techniques of fluid flow modeling and stress-strain analysis. The two-dimensional finite-element code incorporates the flow element of Wilson and Witherspoon [21] for the fracture flow, the joint element of Goodman et al. [12] for the representation of mechanical behavior, and a predictor-corrector scheme to damp out numerical oscillation.

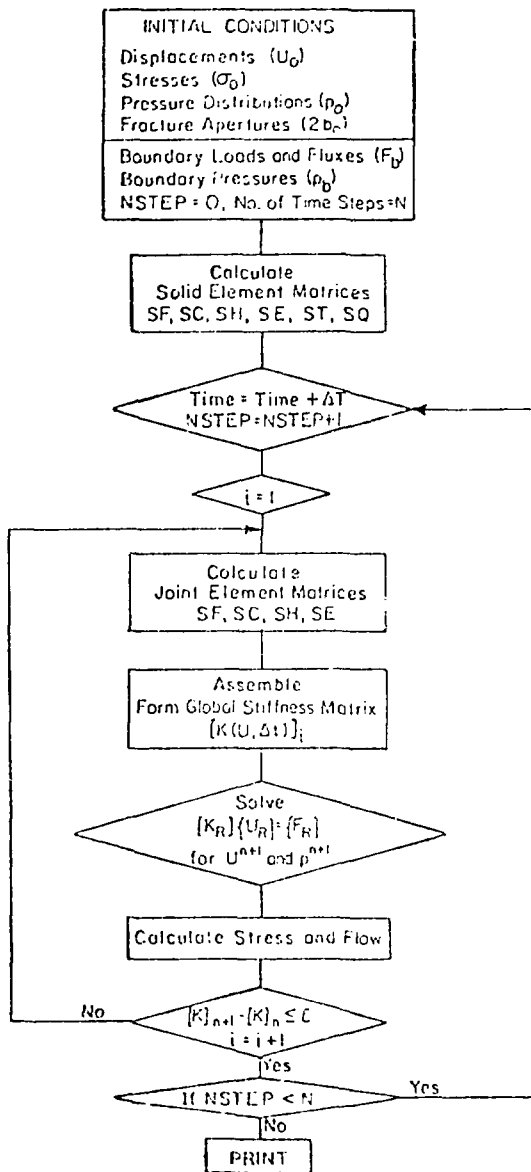
The model is based on general theory which is of fundamental interest and practical importance. The code has the capability of handling a range of complex problems in fluid flow, induced rock mass deformation and soil consolidation [8]. Further developments to couple the fluid flow with heat transfer, or to incorporate dynamic stress analysis, can increase the range of applicability. More extensive application of the code is called for.

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Flow chart for stress and flow analysis of fractured porous media.



VIII. USER'S GUIDE

The program "ROCMAS" is written in FORTRAN IV and uses both large core and small core memory of the CDC 7600. The large core is used for storage of

- (i) nodal points, their coordinates in two directions, their proper code used to describe boundary conditions, initial loads or displacements,
- and (ii) elements, their material type properties, the correspondence between structural nodes and flow nodes, and between structural elements and flow elements, flow boundary codes, and any other properties that are unique for each node or each element.

The large core is also used to store large matrices and vectors needed for the solution of the final system of equations and the equation identifiers for the three degrees of freedom at each nodal point.

The small core memory furnishes storage of the COMMON blocks as well as DIMENSION statements.

Since "ROCMAS" is not written to use a dynamic storage option, it is necessary to keep in mind the maximum size of the arrays for which large core storage is provided. For the time being, the following limits should be kept in mind:

Maximum number of nodal points = 300

Maximum number of structural elements (joints and solids) = 300

Maximum number of joint elements = 50

Maximum number of different materials = 12

The input data* should be prepared in the groups of cards described below:

<u>Group</u>	<u>Column</u>	<u>Format</u>	<u>Word</u>	<u>Explanation</u>
I-1	1-5	A5	"TITLE"	Title card to start with computation
I-2	1-72	8A9	HED	Any desired titling, or blank cards
I-3	1-72	8A9	HED	two cards.
I-4	1-5	I5	NUMNP	Total no. of nodal points in the mesh
	6-10	I5	NUMEL	Total no. of elements in the mesh
	11-15	I5	NUMMAT	Total no. of different materials
	16-20	I5	NSHELL	Highest no. of solid material
	21-25	I5	NPC	No. of boundary pressure cards
	26-30	I5	NJMP	No. of joints with modified aperture
	31-35	I5	IRAND	Random aperture generator if = 1, otherwise equal to zero
	36-40	I5	NIT	Total no. of time step iterations
	41-45	I5	IPLOT	Plot output requested, if equal to 1; otherwise equal to zero
	46-50	I5	IPUNCH	Punch requested for final joint element properties if = 1, otherwise = 0
	51-55	F5.0	TTOTAL	Total estimated on time (decimal seconds)
	56-65	F10.0	CONLIM	Joint stiffness convergence constant
	66-70	I5	NAXI	Axisymmetric problem if 1, two-dimensional problem if 0

* An example of input data preparation is given at the end.

<u>Group</u>	<u>Column</u>	<u>Format</u>	<u>Word</u>	<u>Explanation</u>
I-5	1-10	F10.3	AAM	Mean aperture lognormal distribution
	11-20	F10.3	THETA	Time integration factor
	21-30	F10.3	AAS	Standard deviation lognormal distribution
	31-40	F10.3	ACELX	x-direction acceleration
	41-50	F10.3	ACELY	y-direction acceleration
I-6	1-10	F10.3	XNHP	Maximum net head pressure (optional)
	11-20	F10.3	SPWT	Fluid specific gravity
	21-35	E15.5	VISC	Fluid viscosity
	36-40	I5	IPRINT	No. of time step printouts required
	41-45	I5	NDTN	Variable time step counter if > 1
	46-55	E10.5	DT	Initial time increment
	56-65	E10.5	SYSDIM	System dimension, if P_D , t_D calculated*
66-75	E10.5	TOTALQ	Total flow, if P_D , t_D calculated*	
II-1	1-8	A10	"MATERIAL"	Title card for material specifications
II-2	1-5	A10	"INCOMPRESS"	For incompressible fluid **
			"COMPRESS"	for compressible fluid

*Note that P_D , t_D calculation uses properties of first solid, therefore, it is meaningful only for a special class of problems.

**Only used for uncoupled steady state fluid flow problems. Minor modification of the solution algorithm is required for steady state coupled problems, i.e. when $\alpha \neq 0$ and incompressible fluid assumption is used.

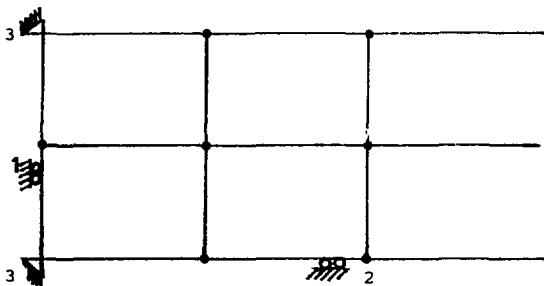
<u>Group</u>	<u>Column</u>	<u>Format</u>	<u>Word</u>	<u>Explanation</u>
II-3	<u>Properties of solid materials</u>			
	1-5	I5	MTYPE	Material type, NSHELL > MTYPE > 1
	6-14	E9.4	RO	Mass density
	15-23	E9.4	E(1,MTYPE)	Permeability
	24-32	E9.4	E(2,MTYPE)	Compression modulus
	33-41	E9.4	E(3,MTYPE)	Poisson's ratio
	42-50	E9.4	E(4,MTYPE)	Biot's constant α (pressure displacement coupling coefficient)
	51-59	E9.4	E(5,MTYPE)	Biot's constant M (reciprocal of specific storage in case of flow analysis alone)
	One card per material type should be punched. Maximum number of solid material cards is equal to NSHELL.			
II-4	<u>Fracture material properties</u>			
	1-5	I5	MTYPE	Material type
	6-14	E9.4	BLANK	
	15-23	E9.4	E(1,MTYPE)	Normal stiffness
	24-32	E9.4	E(2,MTYPE)	Tangential stiffness
	33-41	E9.4	E(3,MTYPE)	Cohesion
	42-50	E9.4	E(4,MTYPE)	Friction angle
	51-59	E9.4	E(5,MTYPE)	Maximum closure
	60-68	E9.4	E(6,MTYPE)	Biot's constant, α
	69-77	E9.4	E(7,MTYPE)	Biot's constant, M

<u>Group</u>	<u>Column</u>	<u>Format</u>	<u>Word</u>	<u>Explanation</u>
III	<u>Output Information</u>			
	1-6	A10	"OUTPUT"	Title card for output specifications
	1-80	40I2	NPP(I)	Number of perturbations in time step I
	1-80	40I2	IPAT(J)	Output scheme for each time step
	Output schemes: (1) IPAT=0 No prints, no plots requested			
			(2) IPAT=1	Print requested
			(3) IPAT=2	Print and plot requested
IV	<u>Plot Information</u>			
	If IPLOT=0 skip this group.			
	1-10	E10.4	XLENGTH	x-dimension of plot (inches)
	11-20	E10.4	YLENGTH	y-dimension of plot (inches)
	21-30	E10.4	PSCL	Factor for plotting stresses in the solids
	31-40	E10.4	CONJT	Multiple for PSCL to plot stresses in joints

<u>Group</u>	<u>Column</u>	<u>Format</u>	<u>Word</u>	<u>Explanation</u>
V	<u>Nodes</u>			
V-1	1-5	A5	"NODES"	Title card for nodal points
V-2	1-5	I5	N	Nodal point number
	6-10	I5	NXP	Increment to reach next nodal point
	11-20	E10.3	R(N)	x-coordinate (R-if axisymmetric) of N
	21-30	E10.3	Z(N)	y-coordinate (z-if axisymmetric) of N
	31-40	E10.3	CD	Displacement code of N
	41-50	E10.3	CDI	Displacement code to be used for preceding node
	51-60	E10.3	DU	Load or displacement at N in x-direction
	61-70	E10.3	DV	Load or displacement at N in y-direction

Note: If CD or CDI are equal to:

- 0 DU and DV are specified loads
- 1 DU is specified displacement, DV is specified load
- 2 DU is specified load, DV is specified displacement
- 3 DU and DV are specified displacements (Fig. 7)



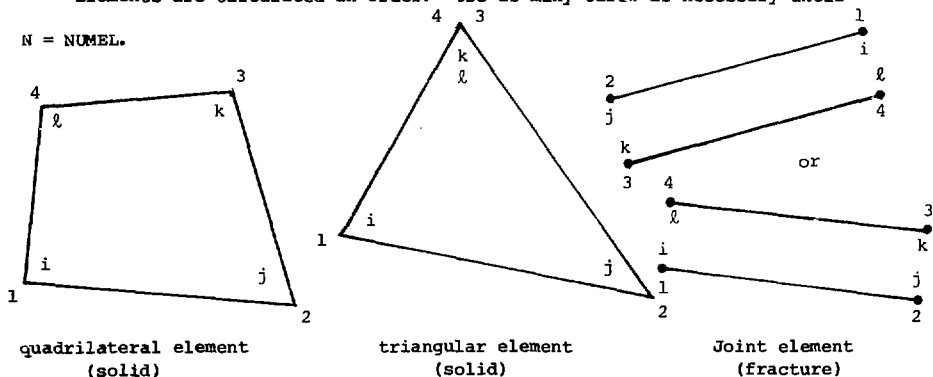
Sketch: Application of load or displacement boundary codes.

Nodal point cards need not be in order, except when generating a set where the last node in the row should come after the first. The last nodal point of the system should appear on the last card.

<u>Group</u>	<u>Column</u>	<u>Format</u>	<u>Word</u>	<u>Explanation</u>
VI	<u>Elements</u>			
VI-1	1-7	A7	"ELEMENT"	Title card for elements
VI-2	1-5	I5	M	Element number
	6-10	I5	IX(M,1)	Nodal points 1 to 4 defining the element must be counterclockwise for solids and lengthwise for joints (Fig. 8)
	11-15	I5	IX(M,2)	
	16-20	I5	IX(M,3)	
	21-25	I5	IX(M,4)	
	26-30	I5	IX(M,5)	Material type
	31-35	I5	IXD(1)	Increments used to change IX(M,1) to reach next generated element
	36-40	I5	IXD(2)	
	41-45	I5	IXD(3)	
	46-50	I5	IXD(4)	
	51-55	I5	JXD	Increment used to alternate material type

Elements are calculated in order. Use as many cards as necessary until

$N = \text{NUMEL.}$



Sketch: Element nodal point numbering.

<u>Group</u>	<u>Column</u>	<u>Format</u>	<u>Word</u>	<u>Explanation</u>
--------------	---------------	---------------	-------------	--------------------

VII Boundary distribution load

If NPC = 0, skip this group.

VII-1	1-8	A8	"PRESSURE"	Title card for boundary pressures
VII-2	1-5	I5	I1	Nodal point number
	6-10	I5	I2	Nodal point number
	11-20	F10.3	PS1	Pressure at I1
	21-30	F10.3	PS2	Pressure at I2

VIII Flow conditions

This group must not appear before Group VII.

VIII-1	1-4	A4	"FLOW"	Title card for flow at the boundary
VIII-2	1-5	I5	N	Nodal point number. If joint use smaller nodal point across the joint.
	6-10	I5	NL	IB(N) = nonzero, if constant PHIO(N)
	11-20	F10.3	PH	PHIO(N) = pressure or head if SPWT = 0
	21-30	F10.3	QQ	Q(N) = flowrate at N

If IB(N) = 0 and Q(N) = 0.0, omit this card.

Cards are needed only if IB(N) ≠ 0 or if Q(N) ≠ 0.0.

<u>Group</u>	<u>Column</u>	<u>Format</u>	<u>Word</u>	<u>Explanation</u>
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IX Residual stresses

Skip this group if no initial stress is given.

IX-1	1-8	A8	"RESIDUAL"	Title card for initial stresses
IX-2	1-10	I10	N	Element number
	11-20	E10.3	RESID(N,1)	Stress in x-direction
	21-30	E10.3	RESID(N,2)	Stress in y-direction
	31-40	E10.3	RESID(N,3)	Stress in z-direction
	41-50	E10.3	RESID(N,4)	Shear stress in xy plane

Note that compressive stresses are negative. Repeat as many cards as needed to define NUMEL. The program will calculate stresses for intermediate elements by assigning the preceding values.

X	1-4	A4	"DONE"	Title card
---	-----	----	--------	------------

This card marks the end of the data for generating the mesh physical information for this particular problem.

<u>Group</u>	<u>Column</u>	<u>Format</u>	<u>Word</u>	<u>Explanation</u>
XI	<u>Joint properties modification</u>			
	Use only if NJMP > 0.			
XI	1-5	I5	I	Joint element to be modified
	6-15	F10.3	COEG	Coefficient to modify the aperture
	16-30	F15.5	COEM1	Coefficient to modify normal stiffness
	31-45	F15.5	COEM2	Coefficient to modify tangential stiffness
	46-60	F15.5	COEM3	Coefficient to modify cohesion
	61-75	F15.5	COEM4	Coefficient to modify friction angle
XII	1-5		"BLANK"	If the flow or pressure source is a step function (kept constant in time). Use another title card if the source is an initial pulse.
xIII	1-10	I10	NSTEP	Number of time steps with a constant time increment DT
	11-30	E20.5	DT	Constant time increment for NSTEP
XIV	Use as many cards as needed to reach NDTN in Group I. For steady state problems* use one card, NSTEP = 1 and DT > zero.			
XIV	1-3	E13	"END"	Final card in the data deck.

* Reminder: For steady state fluid flow problems, put E(6.MTYPE) equal to zero and use "INCOMPRESS" card.

APPENDIX I
SAMPLE PROBLEM
WITH SAMPLE INPUT OUTPUT

SAMPLE PROBLEM

As an example for data preparation, the problem of fluid flow to a well intersecting a vertical fracture is solved. Although the data is originally set up for coupled stress-flow analysis, the problem is first solved in uncoupled state for the purpose of comparison with the existing solution [Raghavan et al., (17)]. To achieve a conventional fluid flow analysis, one has to assign a zero value to the coupling coefficient α and a value equivalent to $1/S_g$ (inverse specific storage) to M . Later, allowing for the deformability of the medium, a coupled analysis is performed. As it is shown in Table 1, in this case $\alpha \neq 0$ (a value equal to 1.0 is assumed) and $M = 1/\rho C_f$. Figures 1 through 4 present the results of the modeling and following plates exhibit the setup of the data. PSP system equivalent units are used in the tabulation of the data set.

TABLE 1. Material properties used for the analysis of fluid flow in fractured rock mass.

Material type	Properties	Value
fluid	γ_f , specific weight	$9.8 \times 10^3 \text{ N/m}^3$
	C_f^{-1} , incompressibility	1.95 GPa
	η , viscosity	$2.8 \times 10^{-4} \text{ N-sec/m}^2$
porous rock	E , Young's modulus	2.45 GPa
	ν , Poisson's ratio	0.25
	γ_r , specific weight	$2.45 \times 10^4 \text{ N/m}^3$
	n , porosity	2.15
	k , permeability	10^{-5} m/s
	M , Biot's storage constant	coupled 1.47 GPa uncoupled* 14.0 GPa
	α , Biot's coupling constant	coupled 1.0 uncoupled 0.0
	fractures	K_N , initial normal stiffness
	K_S , initial tangential stiffness	0.50 GPa/m
	C_0 , cohesion	0.0
	ϕ , friction angle	$30^\circ.0$
	$2b$, initial aperture	$1 \times 10^{-3} - 1 \times 10^{-14} \text{ m}$
	n , porosity	0.15
	M , Biot's storage constant	coupled 1.47 GPa uncoupled* 14.0 GPa
	α , Biot's storage constant	coupled 1.0 uncoupled 0.0

* In this case M is the reciprocal of the specific coefficient of storage of the porous medium.

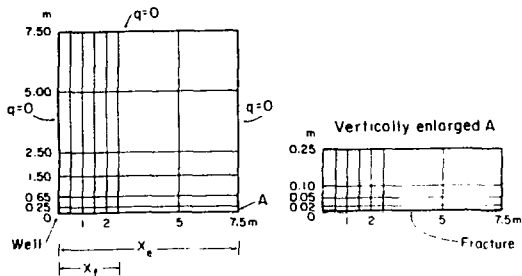


FIG. 1.--TWO-DIMENSIONAL FINITE ELEMENT MESH. (XBL 806-7222)

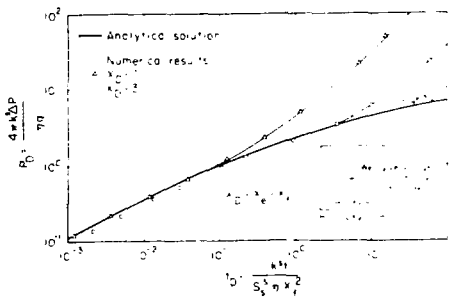


FIG. 2.-- P_D VERSUS t_d FOR A SINGLE FRACTURE INTERSECTING A WELL AT THE CENTER OF A RECTANGULAR POROUS MEDIUM. ANALYTICAL SOLUTION AFTER RAGHAVAN ET AL. (1976). (XBL 806-2703)

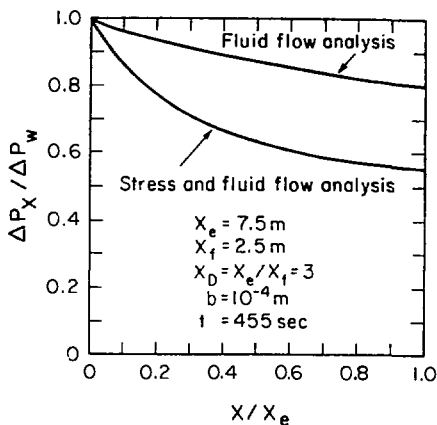


FIG. 3.--PRESSURE DROP ALONG SOFT FRACTURE OF 0.1 mm APERTURE IN FLUID FLOW ANALYSIS AND STRESS-FLUID FLOW ANALYSIS. (XBL 806-2705)

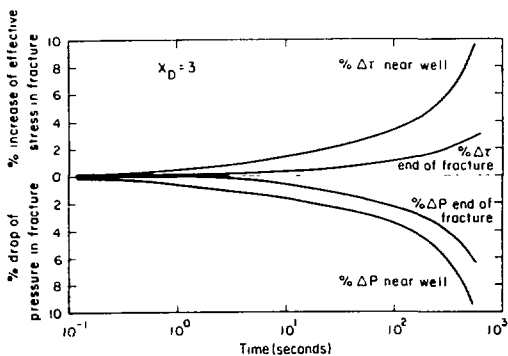


FIG. 4.--THE VARIATION OF PRESSURE AND EFFECTIVE STRESS ALONG THE NEAR AND FAR ENDS OF THE FRACTURE. (XBL 806-2706)

I. General parameters and material properties

PLANF STRAIN-FLOW ANALYSIS OF JUNCTION STRUCTURE

SIMULATION PUMPING OF CONFINED AQUIFER WITH SINGLE VERTICAL FRACTURE

INTERSECTING THE WELL---PLAIN STRAIN PROBLEM

NUMNP-NUMBER OF NODAL POINTS-----	88
NUMEL-NUMBER OF ELEMENTS-----	70
NUMMAT-NUMBER OF DIFFERENT MATERIALS-----	3
NSHELL-NUMBER OF SOLID MATERIALS-----	1
NPC-NUMBER OF BOUNDARY PRESSURE CARDS-----	16
NJNP-NUMBER OF JOINTS WITH MODIFIED APERTURES-----	-0
IRAND-RANDON APERTURE GENERATOR IF 1-----	-0
NIT-NUMBER OF TIME STEPS-----	35
IPLOT- PLOT INFORMATION REQUIRED IF 1-----	-0
IPUNCH-PUNCH IF 1-----	1
TTOTAL-ESTIMATED TOTAL CP TIME(DECIMAL SECONDS)-----	50
AAK-MEAN-APERTURE LOGNORMAL DISTRIBUTION-----	0.
AAS-STANDARD DEVIATION-LOGNORMAL DISTRIBUTION-----	0.
ACELX-X ACCELERATION (FEET/SECOND)-----	0.
ACELY-Y ACCELERATION (FEET/SECOND)-----	0.
XNHP-MAXIMUM NET HEAD PRESSURE (PSF)-----	0.
SPWT-FLUID SPECIFIC WEIGHT-----	-0.
NDTN-VARIABLE TIME-STEP COUNTER,IF G.T. 1-----	10
IPRT,NO. OF CYCLES FOR DISPL. PRINT-----	0
DT-INICIAL TIME INCREMENT-----	1.00000E-03
CONLM JCINT STIFF,CONVERG.CONSTANT-----	6250
MAXI-AXISYM. PROBLEM IF= 1-----	-0
THETA- TIME INTEGRATION CONSTANT-----	2.000
VISC-FLUID VISCOSITY (PSF)-----	5.85000E-06
SYSDIM-SYSTEM DIMENSION REQUIRED IF PD,TD WANTED	3.14160E+00
TOTALQ-TOTAL FLOW REQUIRED IF PD,TD WANTED-----	4.30000E-05

SIMULATION PUMPING OF CONFINED AQUIFER WITH SINGLE VERTICAL FRACTURE
INTERSECTING THE WELL---PLAIN STRAIN PROBLEM

MATERIAL NO. = 1

MASS DENSITY-----	4.85
PERMEABILITY-----	3.1000E-13
ELASTIC MODULUS-----	5.1600E+07
POISSONS RATIO-----	2.5000E-01
BIGTS CONSTANT(ALPHA)-----	0.
BIGTS CONSTANT(M)-----	2.0700E+07

MATERIAL NO. = 2

KN-----	1.0000E+08
KI-----	1.0000E+08
C-----	0.
PHI-----	2.0000E+01
MAX. CLOSURE-----	-3.2800E-04
BIGTS CONSTANT (ALPHA)-----	0.
BIGTS CONSTANT (M)-----	4.1100E+07

MATERIAL NO. = 3

KN-----	7.5000E+11
KI-----	7.5000E+11
C-----	0.
PHI-----	3.0000E+01
MAX. CLOSURE-----	-3.2800E-09
BIGTS CONSTANT(ALPHA)-----	-0.
BIGTS CONSTANT (M)-----	4.1100E+07

II. Displacement and Pressure Results

DISPL. AND PRESSURES AT TIME 5.5555E+01

MODAL PT	DISPL IN X-DIREC	DISPL IN Y-DIREC	PRESSURE	DIMENSIONLESS TIME	EQUATIONLESS PRESSURE, PB
1	-7.7687E-10	-4.10125E-16	2.89331E+04	0.	4.1111E+00
2	-7.86172E-10	-8.20235E-16	2.91475E+04	3.35826E+01	3.30045E+00
3	-1.24544E-15	-8.20250E-16	2.92903E+04	8.39566E+00	2.74195E+00
4	-1.65013E-15	-8.20250E-16	2.93971E+04	3.7314CE+00	2.33413E+00
5	-2.1223E-15	-8.20250E-16	2.94774E+04	2.09892E+00	7.02331E+00
6	-7.1893E-15	-2.44075E-15	2.95341E+04	1.34331E+00	1.80358E+00
7	-2.1012E-15	-4.10125E-16	2.95826E+04	3.35826E+01	3.22075E+00
8	-2.1919E-15	-2.05028E-15	2.96486E+04	1.49256E-01	1.58802E-01
9	-1.44350E-17	-7.46621E-16	2.89381E+04	1.49256E-01	4.11110E+00
10	-7.81726E-16	-8.52995E-16	2.91475E+04	3.35826E+01	3.30045E+00
11	-1.2462E-15	-8.80239E-16	2.92903E+04	8.39566E+00	2.74195E+00
12	-1.64542E-15	-8.80746E-16	2.93971E+04	3.7314CE+00	2.33413E+00
13	-2.1223E-15	-1.06843E-15	2.94774E+04	2.09892E+00	7.02331E+00
14	-2.18933E-15	-2.44074E-15	2.95341E+04	1.34331E+00	1.80358E+00
15	-2.11620E-15	-4.10125E-16	2.95826E+04	3.35826E+01	3.22075E+00
16	-1.45979E-15	-2.05008E-15	2.96486E+04	1.49256E-01	1.58802E-01
17	-4.10125E-17	-7.71954E-16	2.89598E+04	1.49256E-01	4.02723E+00
18	-7.73185E-16	-8.49702E-16	2.91527E+04	3.35826E+01	3.28258E+00
19	-1.24705E-15	-8.82404E-16	2.92946E+04	8.39566E+00	2.73108E+00
20	-1.65341E-15	-8.82912E-16	2.94000E+04	3.7314CE+00	2.32275E+00
21	-2.08180E-15	-1.09420E-15	2.94799E+04	2.09892E+00	2.01363E+00
22	-2.16582E-15	-2.45320E-15	2.95376E+04	1.34331E+00	1.79017E+00
23	-2.01123E-15	-4.08977E-15	2.95953E+04	3.35826E-01	1.7023E-01
24	-6.247E-17	-7.0909E-15	2.96529E+04	1.49256E-01	1.60323E-01
25	-5.5620E-17	-8.10911E-16	2.89902E+04	1.49256E-01	3.50961E+00
26	-1.49195E-16	-8.45846E-16	2.91611E+04	3.35826E+01	3.24753E+00
27	-1.24660E-15	-8.86204E-16	2.93009E+04	8.39566E+00	2.70660E+00
28	-1.65465E-15	-8.86607E-16	2.94045E+04	3.73140E+00	2.2544E+00
29	-2.02731E-15	-1.13101E-15	2.94837E+04	2.09892E+00	1.95884E+00
30	-2.13161E-15	-2.44264E-15	2.95427E+04	1.34331E+00	1.77040E+00
31	-2.00145E-15	-4.07407E-15	2.96145E+04	3.35826E+01	3.3111E-01
32	-1.50354E-16	-2.11880E-15	2.96498E+04	1.49256E-01	1.94250E-01
33	-1.64350E-16	-8.75846E-16	2.90360E+04	1.49256E-01	2.1723E+00
34	-7.63737E-16	-8.34322E-16	2.91766E+04	3.35826E+01	3.18740E+00
35	-1.24877E-15	-8.91453E-16	2.93114E+04	8.39566E+00	2.66611E+00
36	-1.64757E-15	-9.01493E-16	2.94122E+04	3.73140E+00	2.27584E+00
37	-1.54922E-15	-1.18720E-15	2.94902E+04	2.09892E+00	1.97357E+00
38	-2.07745E-15	-2.42446E-15	2.95510E+04	1.34331E+00	1.73034E+00
39	-1.68608E-15	-4.05101E-15	2.96123E+04	3.35826E-01	1.9042E-01
40	-2.9054E-16	-2.17504E-15	2.96925E+04	1.49256E-01	1.90184E+01
41	-4.1655E-16	-8.0388E-15	2.91648E+04	1.49256E-01	2.30045E+00
42	-8.25649E-16	-6.66925E-16	2.92290E+04	3.35826E+01	2.98517E+00
43	-1.25179E-15	-9.07378E-16	2.93432E+04	8.39566E+00	2.54255E+00
44	-1.6F50CE-15	-9.58559E-16	2.94360E+04	3.73140F+00	2.18354E+00
45	-1.78829E-15	-1.32779E-15	2.95107E+04	2.09892E+00	1.89425E+00
46	-1.93776E-15	-2.37784E-15	2.95744E+04	1.34331E+00	1.64784E+00
47	-1.95953E-15	-3.98859E-15	2.96072E+04	3.35826E-01	1.55256E-01
48	-6.8153E-16	-2.30999E-15	2.95934E+04	1.49256E-01	1.80020E+00
49	-1.0251E-15	-1.31117E-15	2.93202E+04	1.49256E-01	2.4521CE+00
50	-1.2564CE-15	-1.04206E-15	2.93516E+04	3.35826F+01	2.2139E+00
51	-1.30936E-15	-9.96649E-16	2.94213E+04	8.39566E+00	2.2401E+00
52	-1.50630E-15	-1.12731E-15	2.94945E+04	3.73140E+00	1.95695E+00
53	-1.62114E-15	-1.54992E-15	2.95608E+04	2.09892E+00	1.70055E+00
54	-1.73975E-15	-2.30788E-15	2.96278E+04	1.34331F+00	1.46023E+00
55	-1.53514E-15	-3.84036E-15	2.96009E+04	3.35826E-01	3.83778E-01
56	-1.29194E-15	-2.36201E-15	2.96568E+04	1.49256F+01	1.67382E-01
57	-1.5347E-15	-1.89149E-15	2.95754E+04	1.49256E+01	1.6441E+00
58	-1.6761E-15	-1.59045E-15	2.95835E+04	3.35826F+01	1.61247E+00
59	-1.73E-15	-2.39405E-15	2.96070E+04	3.39566E+00	2.5725E+00
60	-1.77226E-15	-1.52532E-15	2.96424E+04	3.73140F+00	1.38444E+00
61	-1.74045E-15	-1.84909E-15	2.96829E+04	2.09892F+00	1.22757F+00
62	-1.7746CE-15	-2.26638E-15	2.97251E+04	1.34331F+00	1.06417F+00
63	-2.05371E-15	-3.49802E-15	2.99048E+04	3.35426F+01	3.68620E-01
64	-2.03974E-15	-2.99237E-15	2.99534E+04	1.49256F+01	1.5759E-01
65	-2.03877E-15	-2.28741E-15	2.97358E+04	1.49274E-01	1.00722E+00
66	-2.70455E-15	-1.45743E-15	2.97435E+04	3.35826F+01	5.57809E-01
67	-2.5491E-15	-3.07361E-15	2.97541E+04	8.39566E+00	6.8433E-01
68	-2.94249E-15	-1.91478E-15	2.97755E+04	3.73140E+00	8.88637E-01
69	-2.25181E-15	-2.09642E-15	2.97910E+04	2.09892E+00	6.0225E-01
70	-2.22718F-15	-3.34244E-15	2.98139E+04	1.34331E+00	7.20597E-01
71	-2.2491E-15	-3.27953E-15	2.99221E+04	3.35826E+01	2.01710E-01
72	-2.3126E-15	-3.24284E-15	2.99622E+04	1.49256E-01	1.46319E-01
73	-4.10125E-15	-2.48164E-15	2.99272E+04	1.49256E-01	2.81684E-01
74	-3.8240E-15	-2.51128E-15	2.99278E+04	3.35826E+01	2.7961E-01
75	-3.09E-15	-2.43919E-15	2.99292E+04	8.39566E+00	2.9230E+00
76	-3.31144E-15	-2.70325E-15	2.99321E+04	3.73140E+00	2.4303CE-01
77	-3.1137F-15	-2.77332E-15	2.99356E+04	2.09892E+00	2.49205E-01
78	-2.95923E-15	-2.83441E-15	2.99359E+04	1.34331E+00	2.2495E-01
79	-2.62CE3E-15	-3.23597E-15	2.99650E+04	3.35826E-01	1.2547CE-01
80	-2.60775E-15	-3.59276E-15	2.99770E+04	1.49256E-01	4.80561E-02
81	-2.05662E-15	-2.2955E-15	2.99682E+04	1.49256E-01	1.23196E-01
82	-2.5838E-15	-2.6484E-15	2.9940E+04	3.35826E+01	1.27455E-01
83	-2.5889E-15	-2.94571E-15	2.99645E+04	8.39566E+00	1.2025E+00
84	-2.47553E-15	-3.10342E-15	2.99698E+04	3.73140E+00	1.1485E-01
85	-2.5404E-15	-3.18551E-15	2.99710E+04	2.09892E+00	1.2331E-01
86	-2.56279E-15	-3.22943E-15	2.99724E+04	1.34331E+00	1.64838E-01
87	-2.44684E-15	-3.46551E-15	2.99807E+04	3.35826E-01	7.48482E-02
88	-2.3924E-15	-3.95748E-15	2.99840E+04	1.49256E-01	5.08802E-02

APPENDIX II

LISTING OF FORTRAN IV SOURCE PROGRAM

```

PROGRAM ROCMAS(INPUT=201,OUTPUT,PUNCH=201,PLOT,TAPE8,TAPE9, STRFLC
1 TAPE99=PLCT,TAPE90,TAPE1) STRFLC
C STRFLC
C ***** STRFLC
C PROGRAM ROCMAS STRFLC
C ***** STRFLC
C PLANE-STRAIN AND AXISYMMETRIC QUASI-STATIC STRESS-FLUID FLOW STRFLC
C ANALYSIS OF FRACTURED ROCK MASS. A DIRECT EQUATION SOLVER IS USED STRFLC
C TO SOLVE THE COUPLED EQUATIONS.A STIFFNESS PERTUREATION SCHEME STRFLC
C FORCES STRESSES AND DEFORMATIONS TO FOLLOW THE PROPER NON-LINEAR STRFLC
C CONSTITUTIVE LAW OF THE FRACTURE MATERIALS. STRFLC
C THIS CODE WAS BASICALLY DEVELOPED BY M.S. AYATOLLAHI IN 1978. STRFLC
C LATER,IN 1979,IT WAS CORRECTED,REVISED AND EXTENDED,FOR GENERAL STRFLC
C APPLICATION. BY J.NOORISHAD. STRFLC
C ***** STRFLC
C IN SPITE OF THE POUNDING WEIGHT),FOOT,SECOND HEACINGS,ANY CONSISTENT STRFLC
C SYSTEM OF UNITS COULD BE USED. STRFLC
C ***** STRFLC
C CODE(I)- STRUCTURAL NODAL POINT CODE THAT INDICATES WHAT BOUNDARY STRFLC
C CONDITION( LOAD OR DISPLACEMENT) IS ASSIGNED AT POINT I STRFLC
C (I,J,MTYPE)- MATERIAL MODULI (ROCK OR JOINT ) STRFLC
C EPSK- AVERAGE DEFORMATION OF A JOINT STRFLC
C IBIN(I)- FLOW MESH NODAL POINT CODE,IF #0 ASSIGNED VALUE OF HEAD STRFLC
C OR PRESSURE REMAINS CONSTANT AT POINT N STRFLC
C INDEX- PRINT PLCT CODE STRFLC
C IPAT- PRINT AND PLOT CODE-NO PRINT,NO PLOT IF 0,PRINT IF 1,PRINT, STRFLC
C PLOT IF 2 STRFLC
C IPER- TOTAL PERTURBATION INDEX STRFLC
C IX(I,M), I=1,5- THE FIRST FOUR REPRESENT NODAL POINTS AROUND ELEM STRFLC
C N IN STRUCTURAL MESH AND THE LAST INDICATES MTYPE STRFLC
C KN(I)- NORMAL STIFFNESS OF JOINT I CALCULATED INITIALLY FROM E(I,2) STRFLC
C KS(I)- TANGENTIAL STIFFNESS OF JOINT I CALCULATED FROM E(I,3) STRFLC
C NP-TIME STEP INDEX STRFLC
C MTYPE- NUMBER ASSIGNED TO EACH MATERIAL (STARTING WITH 1 ) STRFLC
C NIT-NUMBER OF TIME STEPS STRFLC
C MNN- PERTURBATION INDEX STRFLC
C NP- DUMMY FOR NPP STRFLC
C MPP(J)- NUMBER OF PERTURBATIONS IN TIME STEP NUMBER J STRFLC
C QIN)- FLOW RATE AT FLOW NODAL POINT N STRFLC
C PHID(N)-PRESCRIBED HEAD OR PRESSURE AT FLOW POINT N WHERE I9(N)#0 STRFLC
C R(I)- X COORDINATE OF STRUCTURAL NODAL POINT I STRFLC
C RESID(N,I), I=1,4 X, Y, Z, AND XY COMPONENTS OF RESIDUAL STRESS STRFLC
C RO(MTYPE)- SPECIFIC MASS OF ROCK MATERIAL STRFLC
C XLNGTH - X LENGTH OF MESH PLOT STRFLC
C YLNGTH - Y LENGTH OF MESH PLOT STRFLC
C DISPL - SCALE FACTOR FOR DISPLACEMENT PLOTS STRFLC
C PSF - SCALE FOR STRESS PLCT STRFLC
C SPWT-FLUID SPECIFIC WEIGHT STRFLC
C TFL- TIME NEEDED FOR FLOW CALCULATION STRFLC
C TIT- TIME SPENT FOR ONE PERTURBATION STRFLC
C TL- TIME LEFT STRFLC
C TST- TIME REQUIRED FOR REAC AND PRINT OF INPUT DATA STRFLC
C UR(I),UZ(I)-R AND Z COMPONENTS OF DISPLACEMENT OR LOAD AT POINT I STRFLC
C V- RELATIVE DISPLACEMENT OF OPPOSING NODAL POINTS IN A JOINT STRFLC
C VISC-FLUID VISCOSITY STRFLC
C MNI)- APERTURE OF FLOW ELEMENT N CALCULATED IN EACH ITERATION STRFLC
C M(I)- INITIAL APERTURE OF JOINT I IN STRUTURAL MESH STRFLC
C Z(I)- Z OR Y COORDINATE OF STRUCTURAL NODAL POINT I STRFLC
C ***** STRFLC
C NOTE----- VECTORS DISP(150),DRG(2N)-IMP(50,4),IEL(50,2),SIGN(50), STRFLC
C AND SIG(150) ARE NOT USED IN THIS VERSION . STRFLC
C STRFLC

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LARGE A(125000),IO(900)
LARGE IX(301,5),RESID(301,4),R(300),Z(300),WR(300),UZ(300) STRFLF
* ,CODE(300),IDEST(300),R,RN(50),R,KS(50),MT(50),IOUT(301),Q(300), LARGE.
*QP(50),M(50),VEL(50),FR(50),RE(50),GN(900),DISPZ(300,2),TEMP(300),LARGE.
*PHI0(300),IB(300),IDEQ(3,300),KCODE(3,300),TEL(50,2),IMP(50,4) LARGE.
* ,TL0A0(900),SIGN(50),SIGT(50),00@900) STRFLF
COMMON/BLANK/S(0,0),P(10),NSTRS(4),VOL,RRR(5),ZZZ(5),LEAD,RADN, BLANK.
1 RR(4),ZZ(4),IFAT(50),ACELX,ACELY,MRES,RC(12), BLANK.
2 MTYPE,XI,XCEI,YCEN,XTR(10),FAC,H(6),PD(4,12),00(2,4), BLANK.
3 PRS,PZS,PRT,PT,EG BLANK.
COMMON/GE/MSHELL,IPUNCH,E(7,12),INDEX,NP,MNH,NCORE,MUMNP,ICORR, GEN.2
1 MUEL,M02,MED(16),DISPL,NJELT,IPER,MUMMAT,PSF,PSFJ,XSCL,SPMT,GEN.3
3VISC,YSCCL,DSCCL,FSCCL,PJCL,NP(4),CONLIN,MAXI,NG,MEANG,LNGTH,NEQ,NJMPGEN.4
* ,MFL0N,MUMNP2,MUMNP,LN(12),NF2 GEN.5
COMMON/APTR,IRANG,NJUMP,AAS,AAN
COMMON/CCPOOL/XMIN,XMAX,YMIN,YMAX,CCXMIN,CCKMAX,CCYMIN,CCYMAX
COMMON/CCFACT/FACTOR
C
DIMENSION NPP(50),MUF(50) STRFLF
DIMENSION IXD(4),IXP(4),LST(0) STRFLF
LOGICAL FLAG STRFLF
DATA TITLE/5HTITLE/,ZMAT/8MMATERIAL/,ZOUT/6MOUTPUT/,FLOW/4HFLOW/, STRFLF
1 ZMODE/5HMODES/,ELEMEN/7HELEMENT/,PRESS/8HPRESSURE/, STRFLF
2 INCON/10HINCPRESS/,RESIX/8HRESIDUAL/,RESTAR/7HRESTART/, STRFLF
3 DONE/4HDONE/,BLANK/5HBLANK/,IXD/4*1/,END/3HEND/ STRFLF
C
FACTOR = 100. STRFLF
LOAD = 0 STRFLF
1 FORMAT (1H10A9/1H 0A9) STRFLF
STRFLF
5 READ 6, WORD STRFLF
6 FORMAT (ZA10) STRFLF
IF (WORD .EQ. TITLE) GO TO 1000 STRFLF
IF (WORD .EQ. ZMAT) GO TO 2000 STRFLF
IF (WORD .EQ. ZOUT) GO TO 3000 STRFLF
IF (WORD .EQ. ZMODE) GO TO 4000 STRFLF
IF (WORD .EQ. ELEMEN) GO TO 5000 STRFLF
IF (WORD .EQ. PRESS) GO TO 6000 STRFLF
IF (WORD .EQ. FLOW) GO TO 6500 STRFLF
IF (WORD .EQ. RESIX) GO TO 8000 STRFLF
IF (WORD .EQ. RESTAR) GO TO 9000 STRFLF
IF (WORD .EQ. DONE) GO TO 9999 STRFLF
IF (WORD .EQ. END) GO TO 300 STRFLF
STRFLF
C
UNIDENTIFIED CARD STRFLF
PRINT 10, WORD STRFLF
10 FORMAT (10HUNIDENTIFIED CARD A10/4H PROGRAM WILL SEARCH FOR NEXT STRFLF
1 TITLE CARD) STRFLF
C
SCAN DECK FOR NEXT CASE IF ANY STRFLF
15 READ 6, WORD STRFLF
IF (WORD .EQ. TITLE) GO TO 1000 STRFLF
IF (WORD .EQ. END) GO TO 300 STRFLF
GO TO 15 STRFLF
STRFLF
1000 READ 20, MED, MUMNP, MUEL, MSHELL, MPC, NJMP, IRANG, STRFLF
1 NIT, IPLCT, IPUNCH, ITOTAL, CONLIN, MAXI, AAN, THETA, STRFLF
2 AAS,ACELX,ACELY,XNHP,SPMT,VISC,IPRT,NOTN,DT,SYSZIN,TOTAL STRFLF
20 FORMAT (0A9/0A9/10I5,F5.0,F10.0,I5/5F10.3/2F10.3,E15.5, STRFLF
12I5,3E10.5) STRFLF
REWIND 0 STRFLF

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      GO TO 5
C                                     STRFLC
C MATERIAL PROPERTIES
C                                     STRFLC
2000 PRINT 1, MFD
      READ 2, ICOMP
      FORMAT (A10)
      IF (ICOMP.EQ. INCOF) PRINT 3
      3 FORMAT( ' FLUID IS IMCOMPRESSIBLE *')
      DO 2035 M=1, MUMHAT
      READ 2010, MTYPE, RG(MTYPE), (E(J, MTYPE), J=1, 7)
2010 FORMAT (I5, 8E9.4)
      PRINT 2015, MTYPE
2015 FORMAT ( /15M MATERIAL NO. =I3)
      IF (MTYPE.LE. NSHELL) GO TO 2019
      PRINT 2030, (E(J, MTYPE), J=1, 7)
      GO TO 2035
2019 PRINT 2020, RO(MTYPE), (E(J, MTYPE), J=1, 5)
2035 CONTINUE
      2020 FORMAT (22H MASS DENSITY-----F8.2/22H PERMEABILITY-----
*E14.4/23H ELASTIC MODULUS -----E14.4/22H POISSONS RATIO-----E
*E14.4/23H BIOTS CONSTANT (ALPHA) E14.4/23H BIOTS CONSTANT(N)-----E
*E14.4)
2030 FORMAT (10H KW-----E25.4/10H KY-----E25.4/10H C-----E25.4/
110H PHI-----E25.4/20H MAX. CLOSURE-----E15.4/
* 23H BIOTS CONSTANT (ALPHA) E14.4/22H BIOTS CONSTANT( N ) E14.4)
      GO TO 5
C
C INFORMATION FOR OUTPUT
C                                     STRFLC
3000 READ 3010, (NPP(I), I=1, NIT)
3010 FORMAT (40I2)
      ITOT = 0
      DO 3012 I=1, NIT
3012 ITOT = ITOT + NPP(I)
      READ 3015, (IPAT(J), J=1, ITOT)
3015 FORMAT (40I2)

      PRINT 1, MFD
      K1 = 1
      DO 3025 I=1, NIT
      K2 = K1 + NPP(I) - 1
      PRINT 3020, NPP(I), I, (IPAT(J), J=K1, K2)
3020 FORMAT ( / / I6, * PERTURBATIONS IN TIME STEP NUMBER * I3, 10X, * OUTPUT
*SCHEME * 20I3)
      STRFLC
3025 K1 = K2 + 1
      IF (XPLST.EQ. 0) GO TO 3035
      READ 3030, XLNGTH, YLNGTH, PSCL, CONJT
      STRFLC
3030 FORMAT (4E10.4)
      STRFLC
3035 GO TO 5
C
C ESTABLISH NOJAL POINT PROPERTIES
C                                     STRFLC
4000 DO 4010 M=1, MUMHAT
4010 R(N) = BLANK
      N = 0
      NXP = 0
4015 NP = N
      IF (N.GE. MUMHAT) GO TO 4035
      NX = NXP
      READ 4020, N, NXP, DR, DZ, CD, COI, DU, DV
      STRFLC
4020 FORMAT (2I9, 6E10.3)
      IF (N.LE. 0. DR.N.GT. MUMHAT) GO TO 4035
      STRFLC
      CODE IN) = CD
      STRFLC
      R(N) = DR
      STRFLC

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      Z(N) = DZ                                STRFLC
      UR(N) = DU                                STRFLC
      UZ(N) = DV                                STRFLC
      IF(MX.EQ.0) GO TO 4015                     STRFLC
      IF((N-NP)*MX.GE.0) GO TO 4025              STRFLC
      MX = - MX                                  STRFLC
      PRINT 4021, NP,N                          STRFLC
4021 FORMAT(* INCREMENT FOR GENERATION BETWEEN NODES* I5* AND*I5* IS  STRFLC
      1F INCORRECT SIGN ** SIGN CHANGED*)      STRFLC
                                                STRFLC
4025 LX = (IABS(N-NP) + IABS(NX) - 1)/IABS(NX)  STRFLC
      DR = (R(N)-R(NP))/LX                       STRFLC
      DZ = (Z(N)-Z(NP))/LX                       STRFLC
4030 NP = NP + NX                               STRFLC
      IF(MX.GT.0.AND.NP.GE.N) GO TO 4015        STRFLC
      IF(MX.LT.0.AND.NP.LE.N) GO TO 4015        STRFLC
      R(NP) = R(NP-MX) + DR                      STRFLC
      Z(NP) = Z(NP-MX) + DZ                      STRFLC
      CODE(NP) = CDI                             STRFLC
      UR(NP) = 0.                                STRFLC
      UZ(NP) = 0.                                STRFLC
      GO TO 4030                                 STRFLC
C
      PRINT NODAL POINTS                        STRFLC
4035 PRINT 1, HED                               STRFLC
      PRINT 4040                                 STRFLC
4040 FORMAT(110H)NODAL POINT          TYPE X-ORDINATE Y-ORDINATE X-10 STRFLC
      1AD OR DISPLACEMENT Y LOAD OR DISPLACEMENT X-CODE T-CODE ) STRFLC
      DO 4055 N=1,MJHNP                      STRFLC
      IF(R(N).EQ.BLANK) PRINT 4045          STRFLC
4045 FCNAT(* NO INPUT FOR THIS NODE * )    STRFLC
      IF(CODE(N).EQ.0.0) GO TO 4022          STRFLC
      IF(CODE(N).NE.3.0) GO TO 4023          STRFLC
      ID(2*N)=1                               STRFLC
      ID(2*N-1)=1                             STRFLC
      GO TO 4022                               STRFLC
4023 IF(CODE(N).NE.2.0) GO TO 4024          STRFLC
      ID(2*N)=1                               STRFLC
      GO TO 4022                               STRFLC
4024 IF(CODE(N).EQ.1) ID(2*N-1)=1          STRFLC
4022 CONTINUE                                 STRFLC
      IF(R(N).NE.BLANK) PRINT 4050,N,CODE(N),R(N),Z(N),UR(N),UZ(N), STRFLC
      , ID(2*N-1),ID(2*N)                   STRFLC
4050 FORMAT(I12,F12.3,2E12.3,2E24.7,2I10)  STRFLC
      IF(CODE(N).LT.1.0) CODE(N) = CODE(N) / 57.29577951 STRFLC
4055 CONTINUE                                 STRFLC
      GO TO 5                                  STRFLC
C
      NODAL POINTS, BAND WIDTH, CHECK CORE CAPACITY, JOINTS AND FLOW STRFLC
5000 PRINT 1, HED                               STRFLC
      PRINT 5010                                 STRFLC
5010 FORMAT(69H)ELEMENT NO.      I      J      K      L      MATERIAL  JO STRFLC
      IINT NO      WIDTH)           STRFLC
      N = 1                                     STRFLC
      MBAND = 0                                 STRFLC
      JX = 0                                    STRFLC
5015 OO 5020 I=1,4                   STRFLC
5020 IXP(I) = IXD(I)                   STRFLC
      JX = JXD                               STRFLC
      READ 5025, M, (IX(M,I), I=1,5), IXD, JXD STRFLC
5025 FORMAT(11I5)                       STRFLC

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5102 IF (IDEST(J) .EQ. 0) IDEST(J)=K
      IF (IDEST(J) .LT. K) IDEST(J)=IDEST(J)
      IF (IDEST(J) .LE. K) GO TO 5106
      KK=IDEST(J)
      DO 5104 II=1, NUMNP
      IF (IDEST(II) .EQ. KK) IDEST(II)=K
5104 CONTINUE
5106 IF (L .EQ. 2) GO TO 5100
      I=IX (N, 2)
      J=IX (N, 3)
      K = MIND(I, J)
      L=2
      GO TO 5095
5108 CONTINUE
      DO 5110 N=1, NUMEL
      MTYPE=IX (N, 5)
      IF (MTYPE .EQ. NSHELL) GO TO 5110
      PERM=E (1, MTYPE)
      IF (ABS (PERM) .LT. E-12) GO TO 5110
      DO 5111 K=1, 4
      I=IX (N, K)
5111 IF (IDEST(I) .EQ. 0) IDEST(I)=I
5110 CONTINUE
      DO 5105 N=1, NUMNP
      I=IDEST (N)
      IF (I .EQ. 0) GO TO 5105
      IDEST(I)=IDEST (I)
5103 IF (I .NE. N) GO TO 5105
      NUHFNPN=NUHFNPN+1
      IDEST(N)=NUHFNPN
5105 CONTINUE
5113 PRINT 5112, MBAND, NJELT, NUFNPN
5112 FORMAT (35H0ST. STIFFNESS PATRUX BAND WIDTH =I5/20H NUMBER OF JIONSTRFLC.
      ST ELEMENTS =I5/2EH NUMBER OF FLOW NODES =I5) STRFLC.
      GO TO 5 STRFLC.
C PRESSURE CARDS IF ANY STRFLC.
6000 PRINT 1, MED STRFLC.
      PRINT 6010 STRFLC.
6010 FORMAT (/29H0PRESSURE BOUNDARY COMDITIONS/ 42H I J PRESSSTRFLC.
      1URE-I PRESSURE=J ) STRFLC.
      DO 6040 L=1, NPC STRFLC.
      READ 6015, I1, I2, PS1, PS2 STRFLC.
6015 FORMAT (2I5, 2F10.3) STRFLC.
      PRINT 6020, I1, I2, PS1, PS2 STRFLC.
6020 FORMAT (2I5, 2F10.3) STRFLC.
      DR = R(I2) - R(I1) STRFLC.
      DZ = Z(I1) - Z(I2) STRFLC.
      CC = CODE (I1) STRFLC.
      IF (CC .EQ. 3) GO TO 6030 STRFLC.
      PI = (Z.*PS1 + PS2)/6. STRFLC.
      IF (NAXI .NE. 0) STRFLC.
      1 PI = (R(I1)*(3.0*PS1+PS2) + R(I2)*(PS1+PS2)) / 12.0 STRFLC.
      SINA = 0. STRFLC.
      COSA = 1. STRFLC.
      IF (CC .GE. 0.8) GO TO 6025 STRFLC.
      SINA = SIN(CCA) STRFLC.

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        COSA = COS(CC)
6825 IF (CC .EQ. 1.0 .OR. CC .EQ. 1.0) UZ(I1) = UZ(I1) + DR*PI
      IF (CC .NE. 1.0) UR(I1) = UR(I1) + DZ*PI*COSA + DR*PI*SINA
6830 CC = CODE(I2)
      IF (CC .EQ. 3.0) GO TO 6840
      PI = (2.*PS2 + PS1)/6.
      IF (MAXI .NE. 0)
1      PI = (R(I2)*(3.0*PS2+PS1) + R(I1)*(PS1+PS2)) / 12.0
      SINA = 8.
      COSA = 1.0
      IF (CC .GE. 9.0) GO TO 6035
      SINA = SIN(CC)
      COSA = COS(CC)
6035 IF (CC .NE. 1.0) UR(I2) = UR(I2) + DZ*PI*COSA + DR*PI*SINA
      IF (CC .EQ. 1.0 .OR. CC .EQ. 0.0) UZ(I2) = UZ(I2) + DR*PI
6040 CONTINUE
      GO TO 5
C
C***** FLOW NODE PROPERTIES ***
6500 CONTINUE
      DO 6501 I=1,NUMFNP
      IO(I)=0
      PHIO(I)=0.0
6501 O(I)=0.0

      IF (NUMFNP .GT. 0) GO TO 7110
      PRINT 7105
7105 FORMAT (37H FLOW CARDS MUST FOLLOW ELEMENT CARDS)
      LBA0 = 1

7110 MBFLCW = 0

      DO 7120 M=1,NUMEL
      MTYPE=IX(M,5)
      IF(MTYPE.LE.NSHELL) GO TO 7121
      I=IX(M,1)
      J=IX(M,2)
      K=IABS(IDEST(I)-IDEST(J))
      IF(K.GT.MBFLOW) MBFLOW=K
      GO TO 7120
7121 DO 7122 I=1,3
      II=IX(M,I)
      I1=I+1
      DO 7122 L=I1,4
      LL=IX(M,L)
      K=IABS(IDEST(LL)-IDEST(II))
      IF(K.GT.MBFLOW) MBFLOW=K
7122 CONTINUE
7120 CONTINUE
      MBFLOW=MBFLOW+1
C
      PRINT 7125
7125 FORMAT(110H0FLOW NODAL PCINTS CODE X-ORDINATE Y-ORDINATE NST
1     LET HEAD(PSF) FLOW RATE(CFS) CORRESPONDING NODAL POINTS)
      NX = 1
7130 READ 7135, N, NL, PH, QF
7135 FORMAT (2I5,2F10,3)
      IF (N .GT. NUMNP .OR. N .LE. 0) GO TO 7170
      IF (N .GT. NK) GO TO 7145

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7140 L = IDEST(N)                               STRFLC
      IB(L) = NL                                 STRFLC
      PHIO(L) = PH                               STRFLC
      Q(L)=QF                                    STRFLC
      GO TO 7150                                  STRFLC

7145 L1 = IDEST(NX)                               STRFLC
      IF (L1 .LE. L) GO TO 7165                 STRFLC
      L = L1                                     STRFLC

7150 DO 7151 J=1,0                               STRFLC
7151 LST(J) = 0                                   STRFLC
      J1 = 0                                      STRFLC
      DO 7155 J=NX,NUMNP                         STRFLC
      IF (IDEST(J) .NE. L) GO TO 7155          STRFLC
      J1 = J1 + 1                                 STRFLC
      LST(J1) = J                                 STRFLC
7155 CONTINUE                                    STRFLC
      PRINT 7160, L, IB(L),R(NX),Z(NX),PHIO(L),Q(L), (LST(J),J=1,J1) STRFLC
7160 FORMAT (2I12,2F12.2,2E19.6,4X,8I4)       STRFLC
      IF (J1.LE.1) GO TO 7162                   STRFLC
      JMIN=LST(1)                                 STRFLC
      DO 7161 J=2,J1                              STRFLC
7161 JMIN=MIN0(JMIN,LST(J))                   STRFLC
      KEQ=KEQ-J1+1                                STRFLC
      JNUM=IDEQ(3,JMIN)                          STRFLC
      DO 100 J=1,J1                                STRFLC
      K=LST(J)                                    STRFLC
100 IDEQ(3,K)=JNUM                               STRFLC
      JMIN=JMIN+1                                 STRFLC
      J1=0                                        STRFLC
      DO 101 K=JMIN,NUMNP                         STRFLC
      DO 101 J=1,3                                 STRFLC
      IF (IDEQ(J,K).EQ.JNUM) J1=J1+1           STRFLC
101 IF (IDEQ(J,K).GT.JNUM) IDEQ(J,K)=IDEQ(J,K)-J1 STRFLC
7162 IF (L.EQ.NUMNP) GO TO 7170                 STRFLC
7165 NX = NX + 1                                 STRFLC
      IF (NX - N) 7145, 7140, 7130             STRFLC
7170 PRINT 7175, NBFLLM                          STRFLC
7175 FORMAT(/ * F. CONDUCTIVITY MATRIX BAND WIDTH = * I5) STRFLC

      DO 41 I=1,NUMNP                             STRFLC
      K=IDEST(I)                                   STRFLC
      KOE(1,I)=IO(2*I-1)                          STRFLC
      KOE(2,I)=IO(2*I)                            STRFLC
41 KOE(3,I)=IB(K)                                STRFLC

C ***** COMPUTE BANDWIDTH OF THE STRUCTURE ***** STRFLC

      NBRAND=1                                     STRFLC
      DO 111 N=1,NUMEL                             STRFLC
      DO 111 I=1,4                                  STRFLC
      IN=IX(N,I)                                    STRFLC
      DO 111 II=1,3                                 STRFLC
      IA=IDEQ(II,IN)                               STRFLC
      DO 111 J=1,4                                  STRFLC
      JN=IX(N,J)                                    STRFLC
      DO 111 JJ=1,3                                 STRFLC
111 NBRAND=MAX0(NBRAND, IABS(IA-IDEQ(JJ,JN)))    STRFLC
      NBRAND=NBRAND+1                              STRFLC
      PRINT 102,NBRAND,KEQ                        STRFLC

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102 FORMAT(25H GLOBAL SYSTEM BANDWIDTH, I5/24H TOTAL SYSTEM EQUATIONS)STRFLC
1, I5) STRFLC
PRINT 51 STRFLC
51 FORMAT(10H NODE ,10H IDEQ(1,N),10H IDEQ(2,N),10H IDEQ(3,N) ,10H)STRFLC
* ID(1,N) ,10H ID(2,N) ,10H ID(3,N) ) STRFLC
DO 53 N=1,MUMNP STRFLC
53 PRINT 52 ,N,(IDEQ(I,N),I=1,3),(KODE(J,N),J=1,3) STRFLC
52 FORMAT(I5,8I10) STRFLC
GO TO 5 STRFLC
C STRFLC
C INITIAL STRESSES IF ANY STRFLC
0000 PRINT 1, MEO STRFLC
PRINT 0010 STRFLC
0010 FORMAT (37H0 I N I ' I A L S T R E S S E S /56H#ELEMENT X-STRFLC
1STRESS Y-STRESS Z-STRESS XY-STRESS) STRFLC
NRES = 1 STRFLC
L = 1 STRFLC
0015 READ 0020, N, (RESID(N,I), I=1,4) STRFLC
0020 FORMAT (I10,4E10.3) STRFLC
IF (N - L) 0040, 0035, 0025 STRFLC
0025 DO 0030 I=1,4 STRFLC
0030 RESID(L,I)=RESID(L-1,I) STRFLC
0035 PRINT 0037, L, (RESID(L,I), I=1,4) STRFLC
0037 FORMAT ( I5,3X,4F12.3) STRFLC
IF (L .EQ. MUMEL) GO TO 0050 STRFLC
L = L + 1 STRFLC
IF (N - L) 0015, 0035, 0025 STRFLC
0040 PRINT 0045, N STRFLC
0045 FCNAT(* RESIDUAL STRESS INPUT ERROR, N=*I4) STRFLC
LBAD = 1 STRFLC
GO TO 0015 STRFLC
0050 GO TO 5 STRFLC
C STRFLC
C RESTART PARAMETERS IF NEEDED STRFLC
9000 IF (NJELT .GT. 0) GO TO 9015 STRFLC
PRINT 9010 STRFLC
9010 FORMAT (40H RESTART CARDS MUST FOLLOW ELEMENT CARDS) STRFLC
GO TO 15 STRFLC
9015 READ 9005, (KN(I),KS(I),MT(I),N(I), I=1,NJELT) STRFLC
9005 FORMAT( 4E20.6 ) STRFLC
GO TO 5 STRFLC
C STRFLC
C ALL INPUT NOW IN --IF CORRECT PROCEED WITH SOLUTION STRFLC
9999 IF (LBAD .NE. 0) GO TO 15 STRFLC
C STRFLC
C PLOT MESH STRFLC
IF (IPLOT .EQ. 0) GO TO 124 STRFLC
C STRFLC
C PREPARE CONSTANTS FOR PLOTTING STRFLC
CCYMIN = (10.5 - YLNTH) / 2.0 STRFLC
CCYMAX = CCYMIN + YLNTH STRFLC
CCXMIN = 0.0 STRFLC
CCXMAX = XLNTH STRFLC
XMIN=R(1) STRFLC
YMIN=Z(1) STRFLC
XMAX=XMIN STRFLC
YMAX=YMIN STRFLC
DO 112 I=2,MUMNP STRFLC
IF (R(I) .GT. XMAX) XMAX = R(I) STRFLC
IF (R(I) .LT. XMIN) XMIN = R(I) STRFLC
STRFLC

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IF (Z(I) .GT. YMAX) YMAX = Z(I)
IF (Z(I) .LT. YMIN) YMIN = Z(I)
112 CONTINUE
XCOM = XLNGTH / (YMAX-XMIN)
YCOM = YLNGTH / (YMAX-YMIN)
DISPL = 0.02 * (XMAX - XMIN)

XSCL = (XPAX - XMIN) / XLNGTH
YSCL = (YMAX - YMIN) / YLNGTH
DSCL = DISPL / XLNGTH
PSF=XSCL/PSCL*0.5
PSFJ = PSF / CONJT
PJCL=PSCL*CONJT

CALL CCBGA
WRITE (98, 115) MED
115 FORMAT (BA9/BA9)
CALL CCLTF (-1.2,0.5, 1, 2)
CALL CCLBL (1,1)
DO 119 N=1,NUMEL
NI=IX(N,1)
NJ=IX(N,2)
NK=IX(N,3)
NL=IX(N,4)
XTR(1) = R(NI)
XTR(2) = R(NJ)
XTR(3) = R(NK)
XTR(4) = R(NL)
XTR(5) = XTR(1)
XTR(6) = Z(NI)
XTR(7) = Z(NJ)
XTR(8) = Z(NK)
XTR(9) = Z(NL)
IF (IX(N,5) .GT. NSHELL) GO TO 117
XTR(10) = XTR(6)
CALL CCPLT (XTR 1), XTR(6), 5, 4HJOIN)
117 CONTINUE
COR = 3.
XCEN = XTR(1) + XTR(2) + XTR(3)
YCEN = XTR(6) + XTR(7) + XTR(8)
IF (NK .EQ. NL) GO TO 118
COR = 4.
XCEN = XCEN + XTR(4)
YCEN = YCEN + XTR(9)
118 XCEN=XCEN/COR*XCEN+.05
YCEN=YCEN/COR*YCEN+.1
119 CONTINUE
WRITE (98,121) XSCL, YSCL
121 FORNAT (15H 1 IN CN X AXIS/4H =E12.4,3H FT/15H 1 IN OM Y AXIS/
14H =E12.4,3H FT)
DO 123 I=1,NUMMAT
WRITE (99, 2815) I
IF (I .LE. NSHELL) GO TO 122
WRITE (99,2830) (E(J,I),J=1,7)
GO TO 123
122 WRITE(98,2828) RO(I),(E1J,I),J=1,6)
123 CONTINUE
XP = CCXMAX + 0.5
CALL CCLTF (XP, 18.5, 0, 2)
CALL CCNEXT
C***** INITIALIZE*****
DO 4 I=1,NJELT

```

```

SIGN(I)=8.0
4 SIGY(I)=0.8
NF2=NUMFNP+NUMFNP
124 READ 6,WORD
NF2=NUMFNP+NUMFNP
IF(WORD.EC.BLANK) NF2=NUMFNP
MEQ=KEQ
MN=HBAND*AEQ
MN9=HBFLOW*NF2
N2=1
N2=MN+1
N3=N2+MN9
N4=N3+NEQ
N5=N4+NEQ
N6=N5+NEQ
N7=N6+NF2
N8=N7+NF2
N9=N8+NUMFNP
I1=1
I2=2*NF2+I1
I3=NEQ+I2
DO 135 I=M3,M9
A(I)=0.0
135 CONTINUE

C **** INITIAL MODAL LOADS ****
DO 750 I=1,NUMNP
K1=IDEQ(1,I)
K2=IDEQ(2,I)
K3=IDEQ(3,I)
J=IDEST(I)
A(M3+K3-1)=PHIO(J)
TEMP(I)=PHIO(J)
A(M4+K1-1)=A(M4+K1-1)+UR(I)
A(M4+K2-1)=A(M4+K2-1)+UZ(I)
DBO(K1)=0.0
DBO(K2)=0.0
750 CONTINUE
DO 505 K=1,NEQ
TLOAD(K)=0.0
505 CONTINUE
CONTINUE

C
C CALCULATION OF APERTURES
IF(INJELT.GT.0) CALL APERTUR

C
125 TIT=0.0
TFL=0.0
TL=0.0
PP=0
TIME=0.0
IPER=0
NSTEP=0
DRT=1.-1./THETA
DTH=DT/2.
TOTN=THETA*CTH
HTOT=DTH-10TH

CALL SECND(ITST)
SOLVE NON-LINEAR STRUCTURE BY SUCCESSIVE APPROXIMATIONS
C
C

```

```

C
170 MP = MP + 1
NCC=0
IP=NFP(MP)
READ 1005,MSTEP,DT
STRFLC
STRFLC
STRFLC
STRFLC
STRFLC
C
174 CONTINUE
TIME=TIME+DT
STRFLC
STRFLC
175 DO 195 MNN=1,IP
FLAG = ,FALSE.
STRFLC
STRFLC
IPER=IPER+1
STRFLC
INDEX = IPAT(IPER)
STRFLC
C
185 CONTINUE
STRFLC
STRFLC
C PD,TD CALCULATED, IF SYSDIM AND TOTALQ IS SUPPLIED
STRFLC
STRFLC
QQ=TOTALQ
IF(QQ.NE.0.) GO TO 185
STRFLC
RD=1.0
STRFLC
TOT=1.0
STRFLC
GO TO 187
STRFLC
186 CONTINUE
STRFLC
RD= SYSDIM*E(1,1)/(VISC*QQ)
STRFLC
TOT=E(1,1)*TIME*E(5,1)/VISC
STRFLC
187 CONTINUE
STRFLC
C
IF(FLAG) GO TO 190
STRFLC
CALL STIFF(THETA*CT/2.,A(N2),A(N2),A(N3),A(N4),A(N5),NEQ,MUFPNP,
STRFLC
,MN,MN9,MBAND,MBFLOW,TIME)
STRFLC
C
SOLVE FOR DISPLACEMENTS
STRFLC
STRFLC
C
CALL SOLVES(THETA,DT,TIME,A(N2),A(N2),A(N3),A(N4),A(N5),A(N6),
STRFLC
,*KODE,ID(1),ID(12),NUMMP,NEQ,NUMEL,NSHELL,MBAND,MBFLOW,
STRFLC
,*MURFNP,ICCMR,IDEST,INDEX,IPER,MNN,IDEQ,PHIO,Q,IP,QN,A(M7),MN9,
STRFLC
,S TLOAD)
STRFLC
321 CONTINUE
STRFLC
IF(THETA.EQ.1.0) GO TO 323
STRFLC
I=0
STRFLC
DO 325 K=1,NEQ
STRFLC
A(M3+I)=A(M3+I)/THETA+DRT*A(M5+I)
STRFLC
STRFLC
325 I=I+1
STRFLC
323 CONTINUE
STRFLC
IF(INDEX.NE.0) PRINT 324,MP
STRFLC
324 FORMAT('0ISPL AND PRESS. AT THE END OF TIME STEP NO. ',I5)
STRFLC
IF(INDEX.EQ.0) GO TO 192
STRFLC
PRINT 2008,TIME
STRFLC
2008 FORMAT(1H1, 30H DISPL. AND PRESSURES AT TIME , E15.4// 6X,
STRFLC
, 10H NODAL PT ,20H0ISPL IN X-DIREC ,20H0ISPL IN Y-DIREC
STRFLC
, 14H PRESSURE 22H DIMENSIONLESS TIME,TO,2EH DIMENSIONLESS PRSTRFLC
*ESSURE,PD//)
STRFLC
CALL PRINT(MUMNP,IDEQ,MNXI,R,RC,TOT,A(M3),TEMP)
STRFLC
326 FORMAT(I10,SE20.5)
STRFLC
192 CONTINUE
STRFLC
190 CALL STRFLD(A(M3),A(N4),A(N5),TIME,IP,FLAG,NCC,DT)
STRFLC
IF(FLAG) GO TO 191
STRFLC
IF(INDEX.NE.0) GO TO 193
STRFLC
C.....NOT NEEDED IF UNCOUPLED FLOW PROBLEM IS SOLVED.....
STRFLC
IF( E(4,1).EQ.0.0 ) GO TO 193
STRFLC
PRINT 324,MP
STRFLC
PRINT 2008,TIME
STRFLC

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```

MAT=IABS(IX(I,5))
WT(J)=E(5,MAT)
15 CONTINUE
GO TO 35
C
10 PRINT 16
16 FORMAT (* APERATURES ARE RANDOMLY GENERATED*)
DO 20 K=1,NJELT
J = ICUTIK)
MAT=IABS( IX(J,5) )
APR=0.0
DO 25 I=1,12
YFL=RNRF(0)
25 APR=APR+YFL
VTH=(APR-E.0)*AAS+AAM
WT(K) = -EXP(VTH)
20 CONTINUE
35 IF( NJMP.EQ.0 ) GO TO 40
C
DO 50 JI=1,NJMP
READ 100,I,COEG,COEM1,COEM2,COEM3,COEM4
100 FORMAT (I5,F10.3,4F15.5)
PRINT 200 ,I,COEG,COEM1,COEM2,COEM3,COEM4
200 FORMAT (I714,7X,6MC0EG = ,F10.3,10X,7MC0EM1= ,F10.3,10X,7MC0EM2= ,F10.3,10X,7MC0EM3= ,F10.3,10X,7MC0EM4= ,F10.3)
DO 220 J = 1,NJELT
IF (IOUT(J) .EQ. I) GO TO 230
220 CONTINUE
230 WT(J) = COEG * WT(J)
MAT=IABS( IX(I,5) )
E(1,MAT)=COEM1*E(1,MAT)
E(2,MAT)=COEM2*E(2,MAT)
E(3,MAT)=COEM3*E(3,MAT)
E(4,MAT)=COEM4*E(4,MAT)
50 CONTINUE
C
40 CONTINUE
RETURN
END
SUBROUTINE STIFF(OT,A1,A2,2,BO,PO,NQ,NAP,MN,MN9,MT,MF,TIME)
C
LARGE A(125000),IO(900)
LARGE IX(301,5),RESID(301,4),R(300),Z(300),JR(300),UZ(300)
* ,COE(300),IDEST(300),R,KN(50),R,KS(50),WT(50),ICUT(301),Q(300),
*QP(50),W(50),VEL(50),FR(50),RE(50),QN(900),DISPI(300,2),TEMP(300),
* PHIQ(300),IB(300),IOEQ(3,300),KODE(3,300),IEL(50,2),JMP(50,4)
* ,TLOAD(900),SIGN(50),SIGT(90),DBO(600)
COMMON/BLANK/S(6,8),P(10),RSTRS(4),VCL,RRR(5),ZZZ(5),LBA0,RADN,
1 RR(4),Z(4),IPAT(50),ACELK,ACELY,NRES,RO(12),
2 MTYPE,XI,XCFN,CEN,XTR(10),FAC,H(6),PD(6,12),QQ(2,4),
3 PRS,FZS,PRT,FZT,EG
COMMON/GEN/MSHELL,IPUNCH,E(7,12),INDEX,MP,N4N,NCORE,NJMP,ICMPR,
1 NUPEL,N02,MED(16),DISFL,NJELT,IPER,NUMMAT,FSF,PSFJ,KSC,L,SFWT,
3 VISC,YSC,L,DSCL,FSCL,PJCL,NP(4),COM,IP,MAXI,NB,MEAND,LANGTH,MEQ,NJMP
* ,NBFLOW,NUPNF2,NUMFNP,LM(12),MF2
COMMON/EP/ST(4,8),SO(2,4),AJ(8,2),DD(2,2),QJ(4),HR(6),MZ(5)
* ,EJ(2,2)
LARGE A1(NQ,1),A2(NMP,1),B(1),BO(1),PO(1)
DIMENSION PP(2),RP(2),TL(8)
COMMON/STF/SF(8,0),SC(8,4),SH(4,4),SE(4,4)

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C                                     STRFLC
C         REMIND 8                               STRFLC
C         REMIND 9                               STRFLC
C         ISH=4                                 STRFLC
C         JSH=2                                 STRFLC
C         LBAD= 0                               STPFLE
C                                     STRFLC
C         DC 702 K=1,NEQ                        STRFLC
C         DD 702 L=1,MBAND                      STRFLC
702 A1(K,L)=0.0                                STRFLC
C         DD 701 KK=1,MNP                      STRFLC
C         DD 701 LL=1,MBFLCW                   STRFLC
C         IF(INF2.GT,NUMFNPI) A2(KK,MBFLOW+LL)=0.0
701 A2(KK,LL)=0.0                             STRFLC
C                                     STRFLC
C         MJ = 0                               STRFLC
C                                     STRFLC
C         DO 300 N=1,MJMEL                     STRFLC
C         DD 200 I=1,4                          STRFLC
C         NP(I)=IX(N,I)                        STRFLC
200 CONTINUE                                  STRFLC
C         MTYPE=IX(N,5)                         STRFLC
C         IF(MTYPE.LE,MSHELL) GO TO 92         STRFLC
C         MJ=MJ+1                               STRFLC
C                                     STRFLC
C         JOINT MATERIAL PROPERTY ASSIGNMENT    STRFLC
C                                     STRFLC
C         KN AND KS ARE MODIFIED AFTER EACH PERTURBATION, THEREFORE,
C         AFTER FIRST PERTURBATION OF FIRST TIME STEP CALCULATED STIFFNESSES
C         ARE USED                             STRFLC
C                                     STRFLC
C         WHEN RESTARTED STIFFNESS VALUES THAT ARE RESULTS OF PRECEEDING
C         RUNS ARE READ IN DIRECTLY            STRFLC
C                                     STRFLC
C         IF(INP.GT.1) GO TO 61                 STRFLC
C         IF(MNH.GT.1) GO TO 61                 STRFLC
C         IF (IPUNCH .GE. 2) GO TO 61          STRFLC
C         KN(INJ) = E(1,MTYPE)                  STRFLC
C         KS(INJ) = E(2,MTYPE)                  STRFLC
61 CONTINUE                                  STRFLC
C                                     STRFLC
C         ***** JOINT ELEMENTS *****      STRFLC
C         CALL JTST IF (B,BO,PO,MJ,N)          STRFLC
C         IF (VOL.LI.0.0) IX(N,5)=-IX(N,5)    STRFLC
C         CALL ASMBLE (DT,A1,A2,N,S,AJ,OD,EJ,IDEOQ,NEQ,NF2,IOEST,JSH)
C         GO TO 300                             STRFLC
C                                     STRFLC
C         ***** SOLID ELEMENTS *****      STRFLC
C                                     STRFLC
C         92 CONTINUE                          STRFLC
C         IF (IPER.GT.1.AND,SPMT.EQ.0.0) GO TO 94
C         IF(MNH.GT.1) GO TO 94                STRFLC
C         CALL ELSTIF (B,BO,PO,N)              STRFLC
C         CALL ASMBLE (DT,A1,A2,N,SF,SC,SH,SE,IDEOQ,NQ,NF2,IOEST,ISH)
C         GO TO 300                             STRFLC
C         94 READ (8) SF,SC,SP,SE,NP           STRFLC
C         93 CALL ASMBLE (DT,A1,A2,N,SF,SC,SH,SE,IDEOQ,NQ,NF2,IOEST,ISH)
300 CONTINUE                                  STRFLC
C         IF(MNH.GT.1) GO TO 500               STRFLC

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DO 301 I=1, NUMNP
J=IDEST(I)
K=IDEO(3,I)
IF( KODE(3,I).LE.0 ) GO TO 350
TLOADIK=PO(K)*1.0E+20
QN(J)=TLOAD(K)
GO TO 301
350 QN(NUMNP+J)=TLOAD(K)+Q(J)
301 CONTINUE
500 RETURN
END
SUBROUTINE JTSTIF(B,B0,PD,H,N)
C
LARGE A(125000),ID(900)
LARGE IX(301,5),RESID(3(1,4),R(300),Z(300),UR(300),UZ(300))
* ,CDE(300),IDEST(300),R,KN(50),R,KS(50),WT(50),ICUT(301),O(300),
LARGE
*QP(50),M(50),VEL(50),FR(50),RE(50),QN(900),DISPI(300,2),TEMP(300),LARGE
*PHIO(300),IB(300),IDEQ(3,300),KODE(3,300),IEL(50,2),IMP(50,4)
LARGE
* ,TLOAD(900),SIGM(50),SIGT(50),DBO(600)
STRFLF
COMMON/BLANK/S(0,0),P(10),RSTRS(4),VOL,RRR(5),ZZZ(5),LBD,RADN,
BLANK
1 RR(4),ZZ(4),IPAT(50),ACELX,ACELY,NRES,RO(12),
BLANK
2 NTYPE,XI,XCE,YCEN,XTR(10),FAC,M(6),PD(4,12),QQ(2,4),
BLANK
3 PRS,PZS,PRT,PZT,EG
BLANK
COMMON/GEN/NSHELL,IPUNCH,E(7,12),INDEX,MP,NYN,NCORE,MUMNP,ICOMPR,
GEN.2
1 NUNEL,NJ2,MED(16),DISPL,NJELT,IMR,NUMMAT,FSF,PSFJ,KSCS,SPMT,GEN.3
3VISC,YSCS,DSCL,FSCL,PJCL,NP(4),CONLIM,MAXI,NB,MEAND,LMGTH,MEQ,NJPP,GEN.4
* ,MBFLOW,MUMNF2,MUMFNP,L(12),NF2
GEN.5
COMMON/EN/ST(4,8),SQ(2,4),AJ(8,2),DD(2,2),QU(4),HR(6),HZ(6)
EM.2
* ,EJ(2,2)
EM.3
C
LARGE B(1),BO(1),PO(1)
STRFLF
DIMENSION AS(4,4),TR(2,2),PPP(8),SS(4,4),TTF(6),SSS(6),V(4)
STRFLF
DIMENSION AT(6,2),CJ(8,2),DUM(24),PP(8)
STRFLF
DIMENSION EPRO(8),CPRO(8)
STRFLF
DATA AT/1.,-1.,1.,-1.,1.,-1.,1.,1./
STRFLF
DATA AS/2.,1.,-1.,-2.,1.,2.,-2.,-1.,-1.,-2.,2.,1.,-2.,-1.,1.,2./
STRFLF
DATA SS/-0.5,0.,0.,0.,0.5,0.,0.5,0.,-0.5,0.,0.,-0.5,0.5,0.5,0.,
STRFLF
1 0.5,0.,0.,-0.5/
STRFLF
C
DATA INCON/10HINC(PRESS/
STRFLF
II=IX(IN,1)
STRFLF
JJ=IX(N,2)
STRFLF
RM = -1.0
STRFLF
IF (NAXI.NE. 0) RM = -(R(JJ) + R(II)) / 2.0
STRFLF
DR=R(JJ)-R(II)
STRFLF
DZ=Z(JJ)-Z(II)
STRFLF
VOL = SQRT(DR*DR + DZ*DZ)
STRFLF
IF (VOL .EQ. 0.0) GO TO 470
STRFLF
STRFLF
C** MATERIAL PROPERTIES
STRFLF
50 COMS=KS(M)*VOL/6.0
STRFLF
COMN=KN(M)*VOL/6.0
STRFLF
C
STRFLF
INITIALIZE
STRFLF
DO 100 I=1,8
STRFLF
P(II)=0.0
STRFLF
EPRO(II)=0.0
STRFLF
CPRO(II)=0.0
STRFLF
DO 100 JJ=1,8
STRFLF
100 S(II,JJ) = 0.0
STRFLF
DO 99 I=1,4
STRFLF
EJ(II)=0.0
STRFLF

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```

99 DD(II)=0.0
99 DD 98 I=1,16
99 AJ(I)=0.0
C      DEVELOP RESIDUAL STRESS CONTRIBUTIONS TO THE LOAD VECTOR
C
C *****
C THE FOLLOWING SIGN CONVENTION IS ADOPTED. THE NORMAL STRESS IS POSITIVE
C WHEN DIRECTED OUTWARD FROM THE ELEMENT ON THE FACE (II, JJ). THE SHEAR STRESS
C IS POSITIVE WHEN DIRECTED FROM II TO JJ AND KK TO LL INSIDE THE ELEMENT
C
      TR(1,1)=DR/VOL
      TR(1,2)=DZ/VOL
      IF (IPER.GT.1) GO TO 171
      SC = TR(1,1) * TR(1,2)
      S2 = TR(1,2) ** 2
      C2 = TR(1,1) ** 2
111 RSTRS(1)=RESID(N,1)*S2+RESID(N,2)*C2+2.*RESID(N,4)*SC
      RSTRS(2)=(RESID(N,2)-RESID(N,1))*SC+RESID(N,4)*(S2-C2)
      TFORMY=RSTRS(1)*VOL*RM
      TFORMX=RSTRS(2)*VOL*RM
      RATLO=0.0
      IF (MAXI.EQ.0) GO TO 112
      II=IX(N,1)
      RATLO=(-1./RM)*[R(II)/2.+VOL/3.0]-0.5
112 PPP(1)=TFCRY*(0.5-RATLO)
      PPP(2)=TFCRX*(0.5-RATLO)
      PPP(3)=TFCRY*(0.5+RATLO)
      PPP(4)=TFORMX*(0.5+RATLO)
      PPP(5)=-PPP(3)
      PPP(6)=-PPP(4)
      PPP(7)=-PPP(1)
      PPP(8)=-PPP(2)
171 CONTINUE

      DO 200 II=1,4
      IN = II + II
      IS = IN - 1
      DO 200 JJ=1,4
      JN = JJ + JJ
      JS = JN - 1
      TDUM=AS(II, JJ)
      IF (MAXI.NE.0) TDUM=-TDUM*RH+SS(II, JJ)*DR
      S(IS, JS)=COM*TDUM
200 S(IN, JN)=COM*TDUM

C      ROTATE TO GLOBAL COORDINATES
      TR(2,1) = -TR(1,2)
      TR(2,2) = TR(1,1)
      IF (TR(1,1).EQ.1.) GO TO 450

      DO 400 NN=1,4
      JJ = NN + NN
      DO 410 II=1,8
      TDUM=S(II, JJ-1)*TR(1,1)+S(II, JJ)*TR(2,1)
      S(II, JJ) = S(II, JJ-1)*TR(1,2) + S(II, JJ) *TR(2,2)
410 S(II, JJ-1)=TDUM
      DO 420 II=1,8
      TDUM=S(JJ-1, II)*TR(1,1)+S(JJ, II)*TR(2,1)
      S(JJ, II) = S(JJ-1, II)*TR(1,2) + S(JJ, II)*TR(2,2)
420 S(JJ-1, II)=TDUM
400 CONTINUE

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```

I1=IX(N,1)                                STRFLC
I2=IX(N,2)                                STRFLC
K1=IDEQ(3,I1)                              STRFLC
K2=IDEQ(3,I2)                              STRFLC
TLOAD(K1)=TLOAD(K1)+GY                     STRFLC
TLOAD(K2)=TLOAD(K2)-GY                     STRFLC
60 CONTINUE                                 STRFLC
C                                           STRFLC
IF(IPER.GT.1) GO TO 640                     STRFLC
DO 600 I=1,2                                STRFLC
DO 600 J=1,2                                STRFLC
K=IX(N,J)                                  STRFLC
L=IDEST(K)                                  STRFLC
EPRO(I)=EPRO(I)+EJ(I,J)*PHZO(L)           STRFLC
600 CONTINUE                                 STRFLC
DO 610 I=1,8                                STRFLC
DO 610 J=1,2                                STRFLC
K=IX(N,J)                                  STRFLC
L=IDEST(K)                                  STRFLC
CPRO(I)=CPRO(I)+AJ(I,J)*PHIO(L)           STRFLC
610 CONTINUE                                 STRFLC
DO 620 J=1,2                                STRFLC
K=IX(N,J)                                  STRFLC
K3=IDEQ(3,K)                                STRFLC
BO(K3)=BO(K3)-EPRO(J)                     STRFLC
620 CONTINUE                                 STRFLC
DO 630 J=1,4                                STRFLC
K=IX(N,J)                                  STRFLC
K1=IDEQ(1,K)                                STRFLC
K2=IDEQ(2,K)                                STRFLC
BO(K1)=BO(K1)+CPRC(IJ+J-1)                STRFLC
BO(K2)=BO(K2)+CPRC(IJ+J)                  STRFLC
630 CONTINUE                                 STRFLC
640 CONTINUE                                 STRFLC
RETURN                                       STRFLC
470 PRINT 471,N                             STRFLC
471 FORMAT(17H BAD JOINT ,N=I3/)           STRFLC
LBAD=LBAD+1                                 STRFLC
RETURN                                       STRFLC
END                                          STRFLC
SUBROUTINE FORMB(S1,T1,IP)                  STRFLC
COMMON/BLANK/S(4,8),P(18),RSTRS(4),VOL,RRR(5),ZZZ(5),LBAD,RADN, BLANK,
1 MR(4),ZZ(4),IPAT(58),ACEIX,ACELY,MRES,RO(12), BLANK,
2 HTYPE,XI,XCE,XVCEN,XTR(18),FAC,M(6),PD(4,12),QQ(2,4), BLANK,
3 PRS,FZS,PRT,PZT,EG BLANK,
COMMON/EM/ST(4,8),SQ(2,4),AJ(8,2),DD(2,2),QU(4),HR(6),HZ(6) EM,2
,EJ(2,2) EM,3
DIMENSION HS(6),HT(6),II(6),JJ(6) STRFLC
DATA II/1,3,5,7,9,10/,JJ/2,4,6,8,11,12/ STRFLC
C                                           STRFLC
DO 50 I=1,48                                STRFLC
50 PD(I)=0.0 STRFLC
SM=1.0-S1 STRFLC
SP=1.0+S1 STRFLC
TM=1.0-T1 STRFLC
TP=1.0+T1 STRFLC
C                                           STRFLC
H(1)=SM*TP/4.0 STRFLC
H(2)=SP*TP/4.0 STRFLC
H(3)=SM*TP/4.0 STRFLC
H(4)=SM*TP/4.0 STRFLC
H(5)=(1.0-S1)*S1 STRFLC

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C      H(6)=(1.0-T1*T1)
C      HS(1)=-TH/4.
C      HS(2)=-HS(1)
C      HS(3)=TP/4.
C      HS(4)=-HS(3)
C      HS(5)=-2.*S1
C      HS(6)=0.0
C      HT(1)=-SH/4.
C      HT(2)=-SP/4.
C      HT(3)=-HT(2)
C      HT(4)=-HT(1)
C      HT(5)=0.0
C      HT(6)=-2.*T1
C      PZT=HT(1)*ZZ(1)+HT(2)*ZZ(2)+HT(3)*ZZ(3)+HT(4)*ZZ(4)
C      PZS=HS(1)*ZZ(1)+HS(2)*ZZ(2)+HS(3)*ZZ(3)+HS(4)*ZZ(4)
C      PRS=HS(1)*RR(1)+HS(2)*RR(2)+HS(3)*RR(3)+HS(4)*RR(4)
C      PRT=HT(1)*RR(1)+HT(2)*RR(2)+HT(3)*RR(3)+HT(4)*RR(4)
C      XJ=PRS*PZT-PRT*PZS
C      PSR=PZT/XJ
C      PTR=-PZS/XJ
C      PSZ=-PRT/XJ
C      PTZ=PRS/XJ
C      DO 100 I=1,6
C      HR(I)=PSR*HS(I)+PTR*HT(I)
100  HZ(I)=PSZ*HS(I)+PTZ*HT(I)
C      IF (IP.NE.0) GO TO 150
C      R=1
C      GO TO 170
150  R=H(1)*RR(1)+H(2)*RR(2)+H(3)*RR(3)+H(4)*RR(4)
C      FCRM STRAIN DISPLACEMENT MATRIX
C
170  DO 200 K=1,6
C      I=II(K)
C      J=JJ(K)
C      PD(1,I)=HR(K)
C      PD(2,J)=HZ(K)
C      IF (IP) 180,190,100
180  PD(3,I)=H(K)/R
190  PD(4,I)=HZ(K)
200  PD(4,J)=HR(K)
C      DO 300 K=1,4
C      QQ(1,K)=HR(K)
300  QQ(2,K)=HZ(K)
C
C      FAC=XJ*R
C      RETURN
C      END
C      SUBROUTINE ELSTIF(B,BO,PO,N)
C
C      LARGE A(1,25000),IO(900)
C      LARGE IX(301,5),RESIO(301,4),R(300),Z(300),UR(300),UZ(300)
C      * ,CODE(300),IDEST(300),R,KM(50),R,KS(50),HT(50),ICUT(301),Q(300),LARGE,
C      *QP(50),M(50),VEL(50),FR(50),RE(50),QH(900),JISPI(300,2),TEMP(300),LARGE,
C      *PHIQ(300),IB(300),IDEQ(3,300),CODE(3,300),IEL(50,2),IMP(50,4)
C      * ,TLOAD(900),SIGN(50),SIGT(50),DBO(600)
C      COMMON/BLANK/S(8,0),P(10),RSTRS(4),VGL,RRR(5),ZZ(5),LBD,RADN,
C      BLANK,2

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1          RR(4),ZZ(4),IPAT(50),ACELX,ACELY,MRES,RC(12),   BLANK.
2      MTYPE,XI,XCE1,YCEN,XTR(10),FAC,H(6),PD(4,12),QQ(2,4),   BLANK.
3      PRS,PZS,PRT,PZT,EG   BLANK.
COMMON/GEN/MSHELL,IPUNCH,E(7,12),INDEX,MP,MN,NCGRE,NUMMP,ICOMPR, GEN.2
1      NUML,NO2,HED(16),DISPL,NJELT,IPER,NUMMAT,PSF,PSFJ,XSCL,SPWT,GEN.3
3      VISC,YACL,DACL,FSCL,PJCL,MP(4),COML,IN,MAXI,NB,MBAND,LNPTH,NEQ,NJMP,GEN.4
*      ,MDFLOW,NUMFZ,MUFAP,LN(12),NFZ   GEN.5
COMMON/EM/ST(4,8),SQ(2,4),AJ(8,2),DD(2,2),QU(4),HR(6),HZ(6)
*      ,EJ(2,2)   EM.2
C          STRFLC
LARGE B(1),BO(1),PO(1)   STRFLC
DIMENSION DX(4),EE(1),EMU(1),EN(1),EM(1),OUM(2,4),   STRFLC
*      PR(10),TTT(6),SSS(6),QB(4),D(4,4)   STRFLC
COMMON/STF/SF(8,8),SC(8,4),SH(4,4),SE(4,4)   STRFLC
DIMENSION EPRO(10),CPRO(10)   STRFLC
DATA INCOMP/10HINCOMPRESS/,SSS/-.57735027,.,57735027,0.0,.,.7745967,
.0.0,.,7745967/,TTT/1.0,1.0,0.0,0.0,55555556,.,00000009,.,55555556/
C          STRFLC
DO 6 I=1,10   STRFLC
EPRO(I)=0.0   STRFLC
CPRO(I)=0.0   STRFLC
PR(I)=0.0   STRFLC
6 P(I)=0.0   STRFLC
DO 2 J=1,16   STRFLC
SE(J)=0.0   STRFLC
2 SH(J)=0.0   STRFLC
DO 3 JJ=1,32   STRFLC
ST(JJ)=0.0   STRFLC
3 SC(JJ)=0.0   STRFLC
DO 1 I=1,4   STRFLC
1 DX(I)=0.0   STRFLC
5 CONTINUE   STRFLC
DO 70 I=1,4   STRFLC
M=IX(N,I)   STRFLC
RR(I)=R(IN)   STRFLC
ZZ(I)=Z(IN)   STRFLC
70 CONTINUE   STRFLC
K=IX(N,5)   STRFLC
FACT=E(2,K)/((1.-2.*E(3,K))^(1.+E(3,K)))   STRFLC
C1=(1.-E(3,K))*FACT   STRFLC
C2=E(3,K)*FACT   STRFLC
C3=(.5-E(3,K))*FACT   STRFLC
EEN=E(4,K)   STRFLC
PERM=E(1,K)/VISC   STRFLC
IF (MAXI.EC.8) D7=0.0   STRFLC
IF (ICOMPR.EQ.INC(M)) EEN=1.0   STRFLC
DO 85 I=1,64   STRFLC
85 SF(I)=0.0   STRFLC
C          STRFLC
C          FORM STRAIN AND FLOW MATRICES AT THE CENTER OF THE ELEMENT
C          STRFLC
DO 520 I=1,3   STRFLC
D(I,4)=0.0   STRFLC
D(4,I)=0.0   STRFLC
DO 510 J=1,3   STRFLC
510 D(I,J)=C2   STRFLC
520 D(I,I)=C1   STRFLC
D(4,4)=C3   STRFLC
CALL FORMB(0.0,0.0,0.0,MAXI)   STRFLC
DO 540 I=1,8   STRFLC
540 SQ(I)=PERM*QQ(I)   STRFLC
DO 533 I=1,4   STRFLC

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170 SH(I,J)=H1*FACK+SH(I,J)
500 CONTINUE
C
C ***** FORM GLOBAL MODAL LOAD VECTOR *****
C
      IF(MAN.GT.1) GO TO 503
      DO 501 J=1,4
      K=IX(N,J)
      K1=IDEQ(1,K)
      K2=IDEQ(2,K)
      TLOAD(K1)=TLOAD(K1)-P(J+J-1)
      TLOAD(K2)=TLOAD(K2)-P(J+J)
      IF(IPER.GT.1) GO TO 501
      BO(K1)=BO(K1)-PR(J+J-1)
      BO(K2)=BO(K2)-PR(J+J)
501 CONTINUE
      IF(SPWT.EC.0) GO TO 503
      DO 502 I=1,4
      J=IX(N,I)
      K=IDEQ(3,J)
      TLOAD(K)=TLOAD(K)-DX(I)
502 CONTINUE
503 CONTINUE
      DO 505 I=1,8
      DO 505 J=1,4
505 SF(J,I)=SF(I,J)
C
      IF(IPER.GT.1) GO TO 830
      DO 800 I=1,4
      DO 800 J=1,4
      K=IX(N,J)
      L=IDEST(K)
      EPRO(I)=EPRO(I)+SE(I,J)*PHI(L)
800 CONTINUE
      DO 810 I=1,8
      DO 810 J=1,4
      K=IX(N,J)
      L=IDEST(K)
      CPRO(I)=CPRO(I)+SC(I,J)*PHI(L)
810 CONTINUE
      DO 820 J=1,4
      K=IX(N,J)
      K1=IDEQ(1,K)
      K2=IDEQ(2,K)
      K3=IDEQ(3,K)
      BO(K1)=BO(K1)+CPRC(J+J-1)
      BO(K2)=BO(K2)+CPRC(J+J)
      BO(K3)=BO(K3)-EPRC(J)
820 CONTINUE
830 CONTINUE
615 CONTINUE
      WRITE (9) ST,SQ,NP
      WRITE (8) SF,SC,SH,SE,NP
C
700 RETURN
C
C
      END
SUBROUTINE ASMBLE (DT,A1,A2,N,SF,SC,SH,SE,IDEQ,NQ,NMP,IDEST,NH)
C
COMMON/BLANK/S(8,8),P(18),RSTRS(4),VCL,RRR(5),ZZZ(5),LBAO,RADN,
1      RR(4),ZZ(4),IPAT(58),ACELX,ACELY,NRES,RO(12),
      BLANK,2

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2      MTYPE,XI,XCE,X,YCEN,XTR(10),FAC,H(6),PD(4,12),QQ(2,4),      BLANK.
3      PRS,FZS,PRT,PZT,EG      BLANK.
COMMON/GEN/NSHELL,IPUNCH,E(7,12),INDEX,MP,NMN,MCDFE,NUMMP,ICCMFR,  GEN,2
1      NUMEL,ND2,MED(16),DISPL,NJELT,IPER,NUMHAT,PSF,PSFJ,XSCL,SPHT,  GEN,3
3VISC,YISCL,DISCL,PSCL,PJCL,NP(4),CONL,IM,NAXI,NB,MBAND,LENGTH,MEO,NJMPGEN,4
*      ,MBFLOW,NUMMF2,NUMFNP,LM(12),MF2      GEN,5
*      COMMON/EH/ST(4,8),SQ(2,4),AJ(3,2),DD(2,2),QJ(4),HR(6),HZ(6)  GEN,2
*      ,EJ(2,2)      EM,3
C      LARGE A1(AQ,1),A2(MNP,1),IDEST(1),IDEQ(3,1)      STRFLC
C      DIMENSION SF(8,1),SC(8,1),SH(INH,1),SE(NM,1)      STRFLC
      L=1      STRFLC
      DD 703 I=1,4      STRFLC
      J=NP(I)      STRFLC
      DD 704 K=1,2      STRFLC
      LH(L)=IDEG(K,J)      STRFLC
704 L=L+1      STRFLC
703 LH(I+8)=IDEQ(3,J)      STRFLC
      IJ=12      STRFLC
      IF(MTYPE.GT.NSHELL) IJ=10      STRFLC
      DD 701 I=1,8      STRFLC
      II=LH(I)      STRFLC
      DD 702 J=1,8      STRFLC
      JJ=LH(J)-II+1      STRFLC
702 IF(JJ.GT.0) A1(II,JJ)=A1(II,JJ)+SF(I,J)      STRFLC
      DD 701 J=9,IJ      STRFLC
      JJ=LH(J)-II+1      STRFLC
701 IF(JJ.GT.0) A1(II,JJ)=A1(II,JJ)+SC(I,J-8)      STRFLC
      DD 705 I=9,IJ      STRFLC
      II=LH(I)      STRFLC
      L=1      STRFLC
      DD 706 K=1,4      STRFLC
      K2=L+L      STRFLC
      K1=K2-1      STRFLC
      KK=LH(K1)-II+1      STRFLC
      LL=LH(K2)-II+1      STRFLC
      IF(KK.GT.0) A1(II,KK)=A1(II,KK)+SC(K1,I-8)      STRFLC
      IF(LL.GT.0) A1(II,LL)=A1(II,LL)+SC(K2,I-8)      STRFLC
706 L=L+1      STRFLC
      DD 705 J=9,IJ      STRFLC
      JJ=LH(J)-II+1      STRFLC
705 IF(JJ.GT.0) A1(II,JJ)=A1(II,JJ)-SH(I-8,J-8)*DT-SE(I-8,J-8)      STRFLC
      IJ=4      STRFLC
      IF(MTYPE.EY.NSHELL) IJ=2      STRFLC
      DD 720 I=1,IJ      STRFLC
      II=NP(I)      STRFLC
      LL=IDEST(II)      STRFLC
      DD 708 J=I,IJ      STRFLC
      J1=NP(J)      STRFLC
      KK=IDEST(J1)      STRFLC
      LLF=FINB(LL,KK)      STRFLC
      MBF=IABS(LL-KK)+1      STRFLC
      A2(LLF,MBF)=A2(LLF,MBF)+SH(I,J)      STRFLC
      IF(MNP.GT.NUMFNP) A2(LLF,MBFLOW+MBF)=A2(LLF,MBFLOW+MBF)-SE(II,J)      STRFLC
708 CONTINUE      STRFLC
1000 RETURN      STRFLC
      ENC      STRFLC
SUBROUTINE SOLVES(THETA,DT,TIME,A1,A2,B,BO,PO,H1,IO,MOH,MB,NUMMP,  STRFLC
*NEQ,MEL,NSH,MBAND,MBFLOW,NUMFNP,ICONPR,IOEST,INDEX,IPER,NMN,IDEO,  STRFLC
*PHIC,Q,IP,QA,QAFZ,TL)      STRFLC

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DO 200 I=IL,IM,MEQ                                STRFLC
L=L+1                                              STRFLC
J=L                                                STRFLC
IB=IB+1                                           STRFLC
C=A1(I)/A1(N)                                     STRFLC
IF (C.EQ.0.0) GO TO 200                          STRFLC
DO 180 K=I,IM,NEQ                                 STRFLC
A1(J)=A1(J)-C*A1(K)                              STRFLC
100 J=J+NEQ                                        STRFLC
A1(I)=C                                            STRFLC
JB=IB                                             STRFLC
200 CONTINUE                                       STRFLC
MB(N)=JB                                          STRFLC
300 CONTINUE                                       STRFLC
MB(MEQ)=8                                         STRFLC
RETURN                                             STRFLC
END                                                STRFLC
SUBROUTINE MULTPLY(A2,B,M1,QQ,MB,NEQ,NUMFNP)      STRFLC.
C                                                  STRFLC.
LARGE A2(NUMFNP,1),MB(1),M1(1),QQ(1)           STRFLC.
C DIMENSION B(1)                                STRFLC.
MM=NUMFNP-1                                      STRFLC.
DO 300 N1=1,NUMFNP                              STRFLC.
BB=A2(N1)*M1(N1)                                STRFLC.
L=N1                                             STRFLC.
IL=N1+NUMFNP                                    STRFLC.
IH=MB(N1)                                       STRFLC.
IF (IH)120,120,50                               STRFLC.
50 DO 180 I=IL,IH,NUMFNP                       STRFLC.
L=L+1                                           STRFLC.
BB=BB+A2(I)*M1(L)                              STRFLC.
100 CONTINUE                                    STRFLC.
120 L=N1                                        STRFLC.
IL=N1+MM                                        STRFLC.
IH=MB(N1+NUMFNP)                               STRFLC.
IF (IH)250,250,150                             STRFLC.
150 DO 200 I=IL,IH,MM                          STRFLC.
L=L-1                                           STRFLC.
BB=BB+A2(I)*M1(L)                              STRFLC.
200 CONTINUE                                    STRFLC.
250 B(N1)=BB+B(N1)                              STRFLC.
QQ(N1)=B(N1)                                    STRFLC.
300 CONTINUE                                    STRFLC.
RETURN                                          STRFLC.
END                                             STRFLC.
SUBROUTINE BACKS(IN,MM,A1,B,MB)                STRFLC.
C                                                  STRFLC.
LARGE A1(1),B(1),MB(1)                         STRFLC.
C MMP=MM-1                                       STRFLC.
M=0                                             STRFLC.
270 N=N+1                                       STRFLC.
C=B(N)                                          STRFLC.
IF (A1(N).NE.0.0) B(N)=B(N)/A1(N)             STRFLC.
IF (N.EQ.MM) GO TO 300                         STRFLC.
IL=N+1                                         STRFLC.
IH=N+MB(N)                                     STRFLC.
M=M+1                                          STRFLC.
DO 285 I=IL,IH                                STRFLC.
M=M+MM                                         STRFLC.
285 B(I)=B(I)-A1(N)*C                          STRFLC.

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      GO TO 270
C
300 IL=N
      N=N-1
      IF(N.EQ.0) RETURN
      IH = N+MB(N)
      M=N
      C=B(N)
      DO 400 I=IL,IH
      M=M*MH
400 C=C-A1(M)*B(I)
      B(N)=C
      GO TO 300
C
      ENB
      SUBROUTINE STRFLC(B,BO,PO,TIME,IP,FLAG,NCC,JT)
C
      LARGE A(125000),ID(900)
      LARGE IX(301,5),RESID(301,4),R(300),Z(300),UR(300),UZ(300)
      * ,CODE(300),IDEST(300),R,KM(50),R,KS(50),MT(50),IGUT(301),Q(300),
      *QP(50),N(50),VEL(50),FR(50),RE(50),QNI(900),JISPI(300,2),TEMP(300),LARGE,
      * PHIO(300),IB(300),IDEQ(3,300),KCODE(3,300),IEL(50,2),IMP(50,4)
      * ,TLOAD(900),SIGM(50),SIGT(50),DBO(600)
      COMMON/BLANK/S(8,8),P(10),RSTRS(4),VOL,RRR(5),ZZZ(5),LBA0,RADN,
1      RRR(4),ZZ(4),IFAT(50),ACELX,ACELY,MRES,RO(12),
2      MTYPE,XI,XCEA,YCEN,XTR(10),FAC,H(6),PO(4,12),QQ(2,4),
3      PRS,PZS,PRT,PZT,EG
      COMMON/GEN/NSHELL,IPUNCH,E(7,12),INDEX,MP,NNM,NCODE,MUMMP,ICOMP,
1      NUMEL,ND2,HE0(16),DISPL,KJELT,IPER,MUMHAT,PSF,PSFJ,KSCS,SPW,GEN,3
3      VIS,YSCS,DSCL,FSCL,PJCL,AP(4),COM,IP,MAXI,NB,HEA0,LNHT,MEQ,KJMP,GEN,4
      * ,MBFLOW,NUMAP2,MUMFNP,LM(12),MFZ
      COMMON/CCFOOL/XMIA,XMAX,YMIN,YMAX,CCXMIN,CCXMAX,CCYMIN,CCYMAX
      COMMON/EN/ST(4,8),SO(2,4),AJ(8,2),DD(2,2),QU(4),MR(6),HZ(6)
      * ,EJ(2,2)
      LARGE B(1),BO(1),PO(1)
      DIMENSION SIG(7),TP(6),QR(4)
      LOGICAL FLAG
C
C      COMPUTE ELEMENT STRESSES
C
1  MPRINT=0
      REMIND 9
      QPODR=0.0
      MJ= 0
      PI=4.0*ATAN(1.0)
      RADN=180.0/PI
      RAD2=0.5*RADN
      P12=2.0*ATAN(1.0)
      IF(INDEX.NE.0) PRINT 2001,TIME,MP,IPER
      IF (IPER .EQ. 1) XMI = -1.0E15
C
      IF (INDEX .LT. 2) GO TO 10
      IF (XMIN .LT. XMI) GO TO 7
      XCON = (XMAX-XMIN) * 0.125 / (CCXMAX-CCXMIN)
      YCON = (YMAX-YMIN) * 0.125 / (CCYMAX-CCYMIN)
      XPC = 0.05
      YPC = 0.05
      XMI = XMIA
      XMA = XMA
      YMI = YMIN
      YMA = YMAX
      DEL = XPC * (XMA - XMIN)

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XMIN = XMIN - DEL
XMAX = XMAX + DEL
DEL = YPC * (YMA - YMIN)
YMIN = YMIN - DEL
YMAX = YMAX + DEL
DEL = XPC * (CCXMAX - CCXMIN)
CCXMIN = CCXMIN - DEL
CCXMAX = CCXMAX + DEL
DEL = YPC * (CCYMAX - CCYMIN)
CCYMIN = CCYMIN - DEL
CCYMAX = CCYMAX + DEL
7 WRITE (98, 5) HED, MP, IPER
5 FORMAT (8A9/8A9/17H ITERATION NUMBER14,20H PERTUREATION NUMBER14)
CALL CCLT F (-1.8, 0.5, 1, 2)
CALL CCL3L (1,1)
CALL CCPLCT (XMI, YMI, 1, 6HNOJOIN, 8, 1)
CALL CCPLCT (XMIN, YMIN, 1, 6HNOJOIN, 1, 1)
CALL CCPLCT (XMA, YMA, 1, 6HNOJOIN, 8, 1)
CALL CCPLCT (XMAX, YMAX, 1, 6HNOJOIN, 1, 1)
CALL CCPLCT (XMI, YMA, 1, 6HNOJOIN, 9, 1)
CALL CCPLCT (XMIN, YMAX, 1, 6HNOJOIN, 1, 1)
CALL CCPLCT (XMA, YMA, 1, 6HNOJOIN, 9, 1)
CALL CCPLCT (XMAX, YMAX, 1, 6HNOJOIN, 1, 1)
C
10 DO 300 N=1,NUMEL
IF (INDEX ,ED, 0) GO TO 15
MPRINT = MPRINT - 1
IF (MPRINT .GT. 0) GO TO 15
MPRINT = 50
C
15 IX(N,5)=IABS(IX(N,5))
MTYPE = IX(N,5)
C
IF (INDEX ,NE, 2) GO TO 110
DO 16 I=1,4
J=IX(N,I)
K1=IDEQ(1,J)
K2=IDEQ(2,J)
XTR(1)=R(J)+8(K1)*DISPL
II=I+5
16 XTR(II)=Z(J)+8(K2)*DISPL
XTR(5)=XTR(1)
XTR(10)=XTR(6)
COR = 3
XCEN = XTR(1) + XTR(2) + XTR(3)
YCEN = XTR(8) + XTR(6) + XTR(7)
IF (N3 .EQ. N4) GO TO 20
COR = 4
XCEN = XCEN + XTR(4)
YCEN = YCEN + XTR(9)
20 XCEN = XCEN / COR
YCEN = YCEN / COR
IF (MTYPE .GT. NSHELL) GO TO 290
C
PLOT GRID INCLUDING DISPLACEMENTS
CALL CCPLCT (XTR(1), XTR(6), 5, 4HJOIN)
KOR = COR
DO 50 NC = 1,KOR

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      N1=IX(N,NC)                                STRFLC
      NI=IDEQ(1,N1)                               STRFLC
      IF (B(N1) .EQ. 0.0) GO TO 30                STRFLC
      XC = XCON                                    STRFLC
      IF (XTR(NC) .GT. XCEN) XC = -XCON          STRFLC
      YC = YCON                                    STRFLC
      IF (XTR(NC+5) .GT. YCEN) YC = -YCON       STRFLC
      XC = XTR(NC) + XC                          STRFLC
      YC = XTR(NC+5) + YC                       STRFLC
      NS=0                                         STRFLC
      IF(B(N1).GT.0.0) NS=0                      STRFLC
      CALL CCPL0T(XC, YC, 1, 6HNOJCIN, NS, 1)    STRFLC
30 CONTINUE                                       STRFLC
C
118 IF(MTYPE.GT.NSHELL) GO TO 290               STRFLC
      READ (9) ST,SO,MP                          STRFLC
      DO 31 I=1,4                                 STRFLC
      SIG(I)=RESID(N,I)                          STRFLC
31 QU(I)=0.0                                     STRFLC
      POAVE=0.0                                   STRFLC
      PAVE=0.0                                    STRFLC
      DO 50 I=1,4                                 STRFLC
      MI=MP(I)                                    STRFLC
      L=IDEQ(1,MI)-1                             STRFLC
      M=2*I-1                                    STRFLC
      MM=M+1                                     STRFLC
      DO 40 K=M,MM                               STRFLC
      L=L+1                                       STRFLC
      DO 40 J=1,4                                 STRFLC
40 SIG(J)=SIG(J)+ST(J,K)*B(L)                  STRFLC
      L=IDEQ(3,MI)                               STRFLC
      POAVE=POAVE+TEMP(NI)/4.0                  STRFLC
      PAVE=PAVE+B(L)/4.0                       STRFLC
      DO 45 K=1,2                                 STRFLC
45 QU(K)=QU(K)+SQ(K,I)*B(L)                   STRFLC
50 CONTINUE                                     STRFLC
      PDIFF=E(4,MTYPE)*(PAVE-POAVE)            STRFLC
      DO 55 I=1,3                                 STRFLC
55 SIG(I)=SIG(I)+PDIFF                          STRFLC
      GEFF=SPWT*(1,MTYPE)/VISC                  STRFLC
      QU(1)=-QU(1)                               STRFLC
      QU(2)=-QU(2)+GEFF                         STRFLC
      CC=(SIG(1)+SIG(2))/2.0                    STRFLC
      BB=(SIG(1)-SIG(2))/2.0                    STRFLC
      CR=SQRT(BB**2+SIG(4)**2)                  STRFLC
      SIG(5)=CC+CR                               STRFLC
      SIG(6)=CC-CR                               STRFLC
      IF (SIG(4).GT.10E-15.OR.BB.GT.10E-15) GO TO 80 STRFLC
      EPS=8.78539816                             STRFLC
      SIG(7)=100.0                               STRFLC
      GO TO 90                                    STRFLC
80 SIG(7)=RAD2*ATAN2(SIG(4),BB)                STRFLC
      EPS=ATAN2(SIG(4),BB)/2.0                  STRFLC
90 AA=ABS(QU(1))                                STRFLC
      IF (AA.GT.10E-30) GO TO 100               STRFLC
      ANG=PI2                                    STRFLC
      GO TO 280                                   STRFLC
100 BB=ABS(QU(2)/QU(1))                        STRFLC
      ANG=SQRT(BB)                               STRFLC
      ANG=ATAN(ANG)                              STRFLC
280 QU(3)=QU(1)*COS(ANG)**2+QU(2)*SIN(ANG)**2 STRFLC

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      QU(I)=ANG*PADN                                STRFLC
      IF(INDEX.EQ.8) GO TO 271                       STRFLC
      PRINT 270,N,(SIG(I),I=1,7),(QU(J),J=1,4)       STRFLC
270  FORMAT (I8,12E10.2)                            STRFLC
2801  FCRMAT(1H1/* STRESSES AND FLOWS AT TIME *F10.3//* STRFLC
      1 ITERATION NUMBER *I4,* PERTURBATION NUMBER *I4,/* STRFLC
      2* ELEMENT*,4X,*SIGR*,6X,*SIGZ*,5X,*SIGT*,6X,*SIGRZ*,5X,*SIGMAX*, STRFLC
      35X,*SIGMIN*,4X,*ANGLE*,5X,*FLWR *,6X,*FLWZ *,5X,*FLWMAX*,4X,*ANGLE*STRFLC
      4*/*IF JOINT*,4X,*SIGN*,6X,*SIGS*,5X,*NDISP*,6X,*TDISP*,5X,*NSTIF*,STRFLC
      55X,*TSTIF*,4X,*STRNGTH*,5X,*MIOTH*,5X,*FRFLO*,3X,* RE*) STRFLC
C
C 271  CONTINUE                                     STRFLC
      PLOT STRESSES                                 STRFLC
      IF (INDEX.LT. 2) GO TO 220                   STRFLC
      CC = COS(EPS)                                 STRFLC
      SS = SIN(EPS)                                 STRFLC
      XL = SIG(5) * CC * PSF                         STRFLC
      XTR(1) = XCEM - XL                             STRFLC
      XTR(2) = XCEM + XL                             STRFLC
      XL = SIG(5) * SS * PSF                         STRFLC
      XTR(5) = YCEM - XL                             STRFLC
      XTR(6) = YCEM + XL                             STRFLC
      CALL CCPLCT (XTR(1), XTR(5), 2, 4HJOIN)        STRFLC
      IF(SIG(5).GE.0.0) GO TO 210                   STRFLC
      XTR(1) = XTR(1) - 0.02 * SS                   STRFLC
      XTR(2) = XTR(2) - 0.02 * SS                   STRFLC
      XTR(5) = XTR(5) + 0.02 * CC                   STRFLC
      XTR(6) = XTR(6) + 0.02 * CC                   STRFLC
      CALL CCPLCT (XTR(1), XTR(5), 2, 4HJOIN)        STRFLC
210  XL = SIG(6) * SS * PSF                         STRFLC
      XTR(1) = XCEM + XL                             STRFLC
      XTR(2) = XCEM - XL                             STRFLC
      XL = SIG(6) * CC * PSF                         STRFLC
      XTR(5) = YCEM - XL                             STRFLC
      XTR(6) = YCEM + XL                             STRFLC
      CALL CCPLCT (XTR(1), XTR(5), 2, 4HJOIN)        STRFLC
      IF(SIG(6).GE.0.0) GO TO 220                   STRFLC
      XTR(1) = XTR(1) - 0.02 * SS                   STRFLC
      XTR(2) = XTR(2) - 0.02 * SS                   STRFLC
      XTR(5) = XTR(5) - 0.02 * CC                   STRFLC
      XTR(6) = XTR(6) - 0.02 * CC                   STRFLC
      CALL CCPLCT (XTR(1), XTR(5), 2, 4HJOIN)        STRFLC
C
C 220  GO TO 300                                    STRFLC
290  CALL JTSTR(B,80,PO,M.,N,FLAG,IP)              STRFLC
300  CONTINUE                                       STRFLC
C
      IF(FLAG.OR.MN.EQ.IP) GO TO 302                STRFLC
      PRINT 304, IPER                                STRFLC
304  FORMAT (52HOPPROBLEM CONVERGED IN THIS ITERATION AT PERTURBATION(I4)STRFLC
302  IF (INDEX.NE.2) GO TO 330                       STRFLC
      WRITE (98,305) XSCI, YSCI, OSCL, PSCI, #JCL   STRFLC
305  FORMAT (15H 1 IN CN X-AXIS/4H =E12.4,3H FT/15H 1 IN ON Y-AXIS/ STRFLC
      14H =E12.4,3H FT/18H 1 IN DISPLACEMENT/4H =E12.4,3H FT/5H 1 IN/STRFLC
      24H =E12.4,11H PSF STRESS/5H 1 IN/4H =E12.4,14H PSF JT STRESS) STRFLC
      DD 320 I=1,NUMHAT                               STRFLC
      IF(I.GT.NSHELL) WRITE (98,315) I, (E(J,I),J=1,5) STRFLC

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IF(I.LE.NSHELL) WRITE(90,308) I,RO(I), (E(K,I),K=1,6) STRFLC
308 FORMAT(/9M MATERIALI3/20H MASS DENSITY =F0.3/16H PERMEABILITY STRFLC
.Y =E14.3/21H ELASTIC MODULUS =E14.3/21H PCISSGN RATIO =F9,STRFLC
.3/23HBIOTS CONSTANT ALPHA =F10.3/19HBIOTS CONSTANT M =E14.3/22H STRFLC
.THERMAL EXPAN.COEF. =E14.3) STRFLC
STRFLC
315 FORMAT(/9M MATERIALI3/20H KN =E12.3/20H KS STRFLC
1 =E12.3/20H C =E12.3/20H PHI =STRFLC
2E12.3/20H MAX CLOSURE =E12.3) STRFLC
320 CONTINUE STRFLC
STRFLC
XP = CCXMAX + 0.5 STRFLC
CALL CCLTR (XP, 10.5, 0, 2) STRFLC
CALL CCNEXT STRFLC
330 RETURN STRFLC
C STRFLC
END STRFLC
SUBROUTINE JTSTR(B,BO,PO,H,N,FLAG,IP) STRFLC
C STRFLC
LARGE A(125000),ID(900) STRFLC
LARGE IX(301,5),RESID(301,4),R(300),Z(300),UR(300),UZ(300) STRFLC
* ,CODE(300),IDEST(300),R,KN(50),R,KS(50),MT(50),IGUT(301),Q(300), LARGE
* QP(50),M(50),VEL(50),FR(50),RE(50),QN(900),DISPI(300,2),FEMP(300), LARGE
* PHIO(300),IB(300),IDEG(13,300),KODE(3,300),IEL(50,2),IMP(50,4) LARGE
* ,TLOAD(900),SIGN(50),SIGT(50),D90(600) STRFLC
COMMON/BLANK/S(8,8),P(10),RSTRS(4),VGL,RRR(5),ZZZ(5),LBD,PADN, BLANK
1 RR(4),ZZ(4),IPAT(50),ACELX,ACELY,NRES,RC(12), BLANK
2 MTYPE,XI,XCE,YCEN,XTR(10),FAC,M(6),PD(4,12),QQ(2,4), BLANK
3 PRS,FZS,PRT,FZT,EG BLANK
COMMON/GEN/NSHELL,IPURC,E(7,12),INDEX,MP,MNH,NCORE,NUMNP,ICCMFR, GEN.2
1 NUMEL,ND2,ME0(16),DISPL,NJELT,IPER,NUMMA1,FSF,PSFJ,XSCL,SPWT,GEN.3
3VISC,YSCL,DSCL,FSCL,PJCL,NF(4),CDMLN,NAXI,NB,MBAND,LENGTH,ME0,NJMP,GEN.4
* ,MBFLOW,NUMNF2,NMFAP,LM(12),NF2 GEN.5
COMMON/CCFOCL/XPIN,XMAX,YMIN,YMAX,CCXMIN,CCXMAX,CCYMIN,CCYMAX CCP00L
COMMON/EN/ST(4,8),SQ(2,4),AJ(8,2),DD(2,2),QU(4),HR(16),HZ(6) EH.2
* ,EJ(2,2) EH.3
COMMON/CCFACT/FACTOR STRFLC
C STRFLC
LARGE B(1),BD(1),PO(1) STRFLC
DIMENSION PPP(8),V(4),U(4) STRFLC
LOGICAL FLAG STRFLC
REAL L STRFLC
C *****ESTABLISH DISPLACEMENTS ALONG AND NORMAL TO JOINT STRFLC
C STRFLC
M = M + 1 STRFLC
CAYN = KN(M) STRFLC
CAYS = KS(M) STRFLC
EM1 = E(1,MTYPE) STRFLC
EM2 = E(2,MTYPE) STRFLC
EM3 = E(3,MTYPE) STRFLC
EM4 = E(4,MTYPE) STRFLC
FT=0.0 STRFLC
STREN=0.0 STRFLC
POAVE=0.0 STRFLC
STRFLC
I=IX(N,1) STRFLC
J= IX(N,2) STRFLC
DR=R(J)-R(I) STRFLC
DZ=Z(J)-Z(I) STRFLC
RR1 = 0.5 * (R(J) + R(I)) STRFLC
ZZ1 = 0.5 * (Z(J) + Z(I)) STRFLC

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L=SQRT(DR*DR+DZ*DZ)
DR=DR/L
DZ=DZ/L
DO 100 II=1,4
  K=IX(N,II)
  K1=IDEO(1,K)
  K2=IDEO(2,K)
  POAVE=POAVE+TEMP(K)/4.0
  V(II)=-B(K1)*DZ+B(K2)*DR
100 U(II)=B(K1)*DR+B(K2)*DZ
C
C ***** COMPUTE EFFECTIVE STRAIN
C EPSN POSITIVE MEANS JCENT IS OPEN
C EFST POSITIVE MEANS (KK,LL) MOVES ALONG U+ MORE THAN (II,JJ)
C
  EPST=0.5*(U(4)-U(1)+U(3)-U(2))
  EPST=-EPST
  IF(ABS(EPST) .LE. 1.0E-13) EPST = 0.0
  EPSN=0.5*(V(4)-V(1)+V(3)-V(2))
  IF(ABS(EPSN) .LE. 1.0E-15) EPSN = 0.0
C
C COMPUTE NORMAL AND SHEAR FORCE PER UNIT LENGTH AND CALCULATE STRENGTH
C INITIAL STRESSES ARE ALWAYS COMPRESSIVE (NEGATIVE)
C
  C2=DR**2
  S2=DZ**2
  SC=DR*DZ
  FMRES = RESID(N,1)*S2 + RESID(N,2)*C2 + RESID(N,4)*2.*SC
  FMRES = FMRES + POAVE
  FTRES = (RESID(N,2)-RESID(N,1))*SC + RESID(N,4)*(S2-C2)
  ETHICK = MT(M)
  FN = CAYN * EPSN + FMRES

  IF (INDEX .NE. 2) GO TO 200
  IF (ABS(XTR(7))-XTR(6)) .LE. 0.01 * (YMAX - YMIN))
1    XCEN = 0.4*XTR(1) + 0.6*XTR(2)
  IF (ABS(XTR(2))-XTR(1)) .LE. 0.01*(XMAX-XMIN))
1    YCEN = 0.4*XTR(6) + 0.6*XTR(7)
  XL = FN * DZ * PSFJ
  XTR(1) = XCEN - XL
  XTR(2) = XCEN + XL
  KL = FN * DR * PSFJ
  XTR(5) = YCEN + XL
  XTR(6) = YCEN - XL
  CALL CCFLOT (XTR(1), XTR(5), 2, 4*HJOIN)
  IF(FM.GE.0.0) GO TO 200
  XTR(1) = XTR(1) - 0.02 * DR
  XTR(2) = XTR(2) + 0.02 * DR
  XTR(5) = XTR(5) + 0.02 * DZ
  XTR(6) = XTR(6) - 0.02 * DZ
  CALL CCFLOT (XTR(1), XTR(5), 2, 4*HJOIN)
200 CONTINUE
C
  IF(FMRES.GT.0.) GC TO 220
C
  FMRES .LE. 0
  IF (ETHICK .EQ. 0.) GO TO 215
  IF (EPSN .LE. 0.0) GO TO 205
C
  ETHICK .NE. 0 AND EPSN .GT. 0
  CAYN = -FMRES / EPSN
  IF (CAYN .EQ. 0.0) CAYN = 1.0E-8

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      IF (CAYN .GT. EM1) CAYN = EM1
      GO TO 230
STRFLC
STRFLC
STRFLC
C      FMRES .LE. 0 AND WT .NE. 0 AND EPSM .LE. 0
205 CAYN = (FN - FMRES) / ETHICK
      IF (CAYN .LT. EM1) CAYN = EM1
      GO TO 230
STRFLC
STRFLC
STRFLC
C      ETHICK = 0, FMRES .LE. 0 .OR. FMRES .GT. 0 AND EPSM .LT. 0
215 CAYN = CAYN * 1.0E10
      CAYS = CAYS * 1.0E10
      GO TO 260
STRFLC
STRFLC
STRFLC
C      FMRES .GT. 0
220 IF (EPSM .LT. 0.0 .AND. ETHICK .EQ. 0.0) GO TO 215
      IF (EPSM .EQ. 0.0) GO TO 230
      CAYN = -FMRES / EPSM
      IF (EPSM .LT. 0.0) CAYN = CAYN + EM1
STRFLC
STRFLC
STRFLC
C      CALCULATION OF KS
230 FT = CAYS * EPST + FTRES
      AFN = ABS(FN)
      EPSNLM = ABS(FMRES) / EM1
      IF (EPSM .GT. EPSALM .OR. FN .GT. 0.0) AFN = 0.0
      STREM = EM3 + AFN * TAN (EM4/57.29577951)
STRFLC
STRFLC
STRFLC
      IF (EPST .EQ. 0.0 ) GO TO 260
      IF (EM3 .EQ. 0.0 .AND. EM4 .EQ. 0.0) GO TO 260
      IF (EPST .LT. 0.0) STREM = - STREM
      CAYS = (-FTRES + STREM) / EPST
      IF (CAYS .EQ. 0.0) CAYS = 9.0E-9
STRFLC
STRFLC
STRFLC
      IF (CAYS .GT. EM2) CAYS = EM2
      ABS(FTRES) .LE. ABS(STREM)
      IF (ABS(FTRES) .GT. ABS(STREM)) GO TO 235
      GO TO 260
STRFLC
STRFLC
STRFLC
C      ABS(FTRES) .GT. ABS(STREM)
235 IF (FTRES * EPST .GE. 0.0) GO TO 260
STRFLC
STRFLC
STRFLC
C      FTRES AND EPST HAVE OPPOSITE SIGNS
      EPSLIM = 2.0 * STREM / EM2
      IF (ABS(EPST) .GT. EPSLIM) GO TO 260
STRFLC
STRFLC
STRFLC
C      ABS(EPST) .LE. EPSLIM
      CAYS = 1-FTRES - STREM / EPST + EM2
STRFLC
STRFLC
STRFLC
260 IF (ABS(CAYN-KN(M)) .GT. CONLIM .OR. ABS(CAYS-KS(M)) .GT. CONLIM)
1 FLAG = .TRUE.
      KN(M)=CAYN
      KS(M) = CAYS
STRFLC
STRFLC
STRFLC
C      ***** CALCULATE FLOW IN FRACTURES *****
C
C      IF (INDEX.EQ.0) GO TO 500
115 NB=NT(M)
      IF (EPSM.GE.NB) GO TO 150
      PRINT 140,M
140 FORMAT('DISPLACEMENT GREATER THAN ALLOWED IN JOINT ELEMENT NO.*I5)
STRFLC
STRFLC
STRFLC
150 W(HI)=ABS(ABS(NB)+EPSM)
      CON=1.0/(12.0*VISC)
STRFLC
STRFLC
STRFLC

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