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## Title

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## ELECTRON-CLOUD BUILD-UP SIMULATIONS IN THE PROPOSED PS2: STATUS REPORT\*

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#### Abstract

A replacement for the PS storage ring is being considered, in the context of the future LHC accelerator complex upgrade, that would likely place the new machine (the PS2) in a regime where the electron-cloud (EC) effect might be significant. We report here our current estimate of the EC density  $n_e$  in the bending magnets and the field-free regions at injection and extraction beam energy, for both proposed bunch spacings,  $t_b = 25$  and 50 ns. The primary model parameters exercised are the peak secondary emission yield (SEY)  $\delta_{\text{max}}$ , the electron-wall impact energy at which the SEY peaks,  $E_{\text{max}}$ , and the chamber radius *a* in the field-free regions of the bunch intensity  $N_b$ , and we provide a tentative explanation for the non-monotonic behavior of  $n_e$  as a function of  $N_b$ .

#### **INTRODUCTION**

In the results presented here we employed the EC buildup simulation codes ECLOUD [1] and POSINST [2], which have been well benchmarked against each other [3]. In each case analyzed, we estimated the electron-cloud density by time-averaging over two beam batches. For the 25-ns spacing option, a batch is defined as a train of 168 full consecutive buckets followed by 12 empty buckets. For the 50-ns spacing option, a batch is defined by a sequence of 84 bunches filling every other bucket, followed by 12 empty buckets. Other parameters are summarized in Table 1. For the sake of simplicity at this stage of the simulation process, we assumed the same bunch sizes in the field-free region and in the dipole bending magnet.

### DEPENDENCE ON $\delta_{\max}$

The primary variable that determines the build-up of  $n_e$ is  $\delta_{\max}$ . We have assumed a model for the secondary electron emission spectrum that approximately represents stainless steel [2]. By varying  $\delta_{\max}$ , we conclude that there is a rather clear threshold for significant EC density  $n_e$ when  $\delta_{\max}$  exceeds ~ 1.3 for the 50 ns option, as seen in Figs. 1 (here  $n_e$  represents the temporal and spatial average of the electron density in the section being simulated). For the 25 ns option, threshold is lower,  $\delta_{\max} \sim 1.2$ . Table 1: Selected PS2 Parameters used in Simulations.

Ring and beam	
Ring circumference $C = 1346.4 \text{ m}$	
RF frequency $f_{\rm RF} = 40 \text{ MHz}$	
Harmonic number $h = 180$	
Bunch spacing $t_b = 25 \text{ or } 50 \text{ ns}$	
Bunch intensity (nom.)	
at $t_b = 25 \text{ ns}$ $4.2 \times 10^{11}$	
at $t_b = 50 \text{ ns}$ $5.9 \times 10^{11}$	
Inj./extr. beam kinetic energy 4/50 GeV	
Transv. RMS bunch sizes	
at inj. $(\sigma_x, \sigma_y) = (6.3, 5.9) \text{ mm}$	
at extr $(\sigma_x, \sigma_y) = (1.95, 1.83) \text{ mm}$	
RMS bunch length at inj./extr. $\sigma_z = 1.0/0.33$ m	
Pipe cross section	
dipole elliptical, $(a, b) = (6, 3.5)$ cm	
field-free round, $a = 4 - 6$ cm	
Dipole bending field at extr. $B = 1.7 \text{ T}$	
Secondary e <sup>-</sup> parameters	
Peak SEY $\delta_{\max} = 1.0 - 1.8$	
Electron energy at $\delta_{\text{max}}$ $E_{\text{max}} = 292.6 \text{ eV}$	
SEY at 0 energy $\delta(0) = 0.2438 \times \delta_{\max}$	
Simulation parameters	
Bunch profile 3D gaussian	
Full bunch length $L_b = 5\sigma_z$	
Max. no. of macroelectrons 20000	
Integration time step $3 \times 10^{-11}$ s	
Space-charge grid size $64 \times 64$	

#### DEPENDENCE ON $N_b$

The dependence of  $n_e$  on  $N_b$  is shown in Figs. 2. One sees a non-monotonic dependence on  $N_b$ , particularly at extraction energy, by virtue of which  $n_e$  peaks at a value of  $N_b$  that is significantly lower than nominal. For the bending magnets at extraction energy, the explanation of this nonmonotonic dependence is almost certainly the following: As  $N_b$  increases from low values, the average electron-wall impact energy  $\langle E_0 \rangle$  rises roughly proportionally to  $N_b$  and crosses the value  $E_{\rm max} \simeq 300$  eV, at which point the SEY is highest, when  $N_b \simeq (1-3) \times 10^{11}$ . As  $N_b$  increases beyond this value,  $\langle E_0 \rangle$  exceeds  $E_{\text{max}}$ , hence the effective SEY decreases, hence so does  $n_e$ . This non-monotonicity is particularly clear at extraction energy because  $\sigma_z$  is short enough that the beam impulsively imparts energy to the electrons. At injection energy,  $\sigma_z$  is large enough that the beam-electron force is not impulsive due to the phase averaging of the electrons temporarily trapped by the beam

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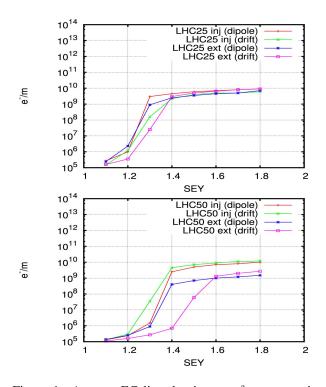


Figure 1: Average EC line density vs.  $\delta_{\text{max}}$ , assuming nominal values for  $N_b$ , for  $t_b = 25$  (top) and 50 ns (bottom). The line density is proportional to  $n_e$ , with  $10^{10}$ e<sup>-</sup>/m corresponding to  $n_e = 1.55 \times 10^{12}$  m<sup>-3</sup>.

potential, hence the proportionality  $\langle E_0 \rangle \propto N_b$  is spoiled, hence  $\langle E_0 \rangle$  remains below  $E_{\max}$  up to significantly higher values of  $N_b$ . This explanation is probably valid for fieldfree regions as well (see the discussion below).

#### SUMMARY OF PRESENT RESULTS

#### Average EC density

Table 2 summarizes our estimates of the ecloud density for most cases explored, assuming  $\delta_{\text{max}} = 1.3$ , a value that is generally believed to correspond to conditioned stainless steel, and assuming that the vacuum chamber in the fieldfree region has a radius a = 6 cm. Roughly speaking, the average  $n_e$  is in the range (a few)×10<sup>10</sup>–(a few)×10<sup>12</sup> m<sup>-3</sup>, while the local density within the 1 $\sigma$  beam ellipse is in the range (a few)×10<sup>11</sup>–(a few)×10<sup>12</sup> m<sup>-3</sup>. In general, the 50-ns option is clearly favored over the 25-ns option: roughly speaking, the former leads to lower values of  $n_e$ by factors of ~ 3 relative to the latter.

#### Dependence on chamber radius in drift regions

We examined the dependence of  $n_e$  on the pipe radius ain the range a = 4 - 6 cm. Results at extraction energy are shown in Fig. 3. We conclude that the dependence is weak at nominal values of  $N_b$ , but may be significant at lower bunch intensities. For the 50-ns option, however, the results unambiguosly favor a lower value of a. The no-

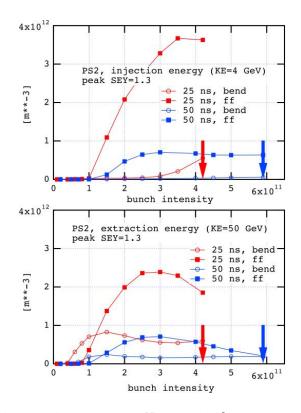


Figure 2: Simulated  $n_e$  vs.  $N_b$ , assuming  $\delta_{\text{max}} = 1.3$ . The arrows indicate the nominal design values of  $N_b$  for 25 ns (red) and 50 ns (blue) bunch spacing.

ticeable non-monotonicity of  $n_e(a)$  is related to the abovementioned non-monotonicity of  $n_e(N_b)$ .

#### DISCUSSION

We explored the numerical stability of our results against basic computational parameters. We conclude that the value of the integration time step size  $\Delta t = 3 \times 10^{-11}$ s is sufficiently small for stable results (the results become unstable when  $\Delta t$  is somewhere in the range  $(10 - 50) \times 10^{-11}$  s). Spot-checks showed that space-charge grid sizes  $16 \times 16$ ,  $32 \times 32$  and  $64 \times 64$  did not yield significant differences; we intend to revisit this somewhat puzzling result.

All results above are for a tri-gaussian bunch profile. We spot-checked the sensitivity of  $n_e$  against the transverse and longitudinal bunch profile by considering parabolic transverse bunch shape and flat longitudinal profile. The conclusion is that these bunch shapes lead to slightly lower (~ 5 - 10%) values of  $n_e$  compared with the gaussian shape, in all cases considered.

In order to check the above-mentioned explanation for the non-monotonicity of  $n_e(N_b)$ , we varied  $E_{\text{max}}$  while holding all other variables fixed. Results are shown in Fig. 4. As expected, the peak of  $n_e(N_b)$  shifts monotonically with  $N_b$ . More detailed analysis (not shown here) also show that  $\langle E_0 \rangle$  is a fairly linear function of  $N_b$ , and furthermore that the value of  $N_b$  where  $n_e$  peaks is a linear function of the value of  $N_b$  at which  $\langle E_0 \rangle = E_{\text{max}}$ .

Table 2: Estimated  $n_e$  (in m<sup>-3</sup>), Assuming  $\delta_{max} = 1.3$ .

	Injection energy		Extraction energy	
	Bending magnet	Field free region	Bending magnet	Field free region
Overall:				
$t_b = 25 \text{ ns}, N_b = 4.2 \times 10^{11}$	$\sim 6 \times 10^{11}$	$\sim 4 \times 10^{12}$	$\sim 6 \times 10^{11}$	$\sim 2 \times 10^{12}$
$t_b = 50 \text{ ns}, N_b = 5.9 \times 10^{11}$	$\sim 5\times 10^{10}$	$\sim 6\times 10^{10}$	$\sim 2 \times 10^{11}$	$\sim 2\times 10^{11}$
Within the $1\sigma$ beam ellipse:				
$t_b = 25 \text{ ns}, N_b = 4.2 \times 10^{11}$	$\sim 5  imes 10^{12}$	$\sim 8  imes 10^{12}$	$\sim 5  imes 10^{12}$	$\sim 6  imes 10^{12}$
$t_b = 50 \text{ ns}, N_b = 5.9 \times 10^{11}$	$\sim 5\times 10^{11}$	$\sim 2\times 10^{12}$	$\sim 3 \times 10^{12}$	$\sim 6\times 10^{11}$

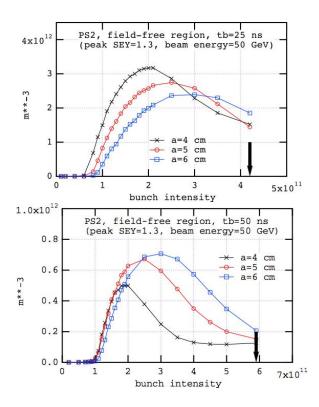


Figure 3: Average  $n_e$  vs.  $N_b$  in a field-free region at extraction energy, assuming  $\delta_{\max} = 1.3$ , for 3 values of the chamber radius a.

These results strengthen our tentative explanation, at least for extraction energy in a dipole bending magnet. For other cases, the results are less conclusive. In any case, the sensitivity of  $n_e$  on  $E_{\text{max}}$  is weak at nominal values of  $N_b$ , but may be significant at lower values of  $N_b$ .

The non-monotonicity of  $n_e(N_b)$  has been noticed in earlier simulations for the SPS and the FNAL Main Injector upgrade [4], but not yet verified experimentally. We intend to further explore this phenomenon in the near future, via simulations and experiments at the SPS.

We have not yet methodically explored the sensitivity of our results to the details of the secondary electron emission spectrum. The above results assume a spectrum with a substantial rediffused component, which tends to yield higher

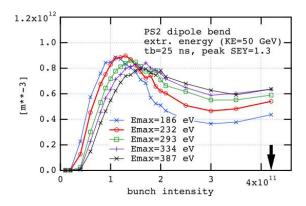


Figure 4: Average  $n_e$  vs.  $N_b$  in a dipole bending magnet at extraction energy for various values of  $E_{\text{max}}$ , assuming  $\delta_{\text{max}} = 1.3$  and  $t_b = 25$  ns in all cases.

values of  $n_e$  than a low-rediffused-component spectrum.

Simulations of the effect of the EC on the beam show a threshold value  $n_e \sim 0.5 \times 10^{12} \text{ m}^{-3}$  for significant instability and/or emittance growth [5]. This value lies in the mid-range of our estimates for  $n_e$ . Therefore, while more detailed investigations remain to be carried out, we feel confident to conclude that smooth, reliable, operation of the PS2 will almost certainly require mitigation of the EC, likely via low-emission coatings.

#### ACKNOWLEDGMENTS

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