

Lawrence Berkeley Laboratory

UNIVERSITY OF CALIFORNIA

Materials & Molecular Research Division

Submitted to the Journal of the Electrochemical Society

RECEIVED

LAWRENCE
BERKFLEY LABORATORY

PEG FORMATION BY SHORT CIRCUIT DIFFUSION IN Al $_2$ 0 $_3$ SCALES CONTAINING OXIDE DISPERSIONS

JAN 20 1982

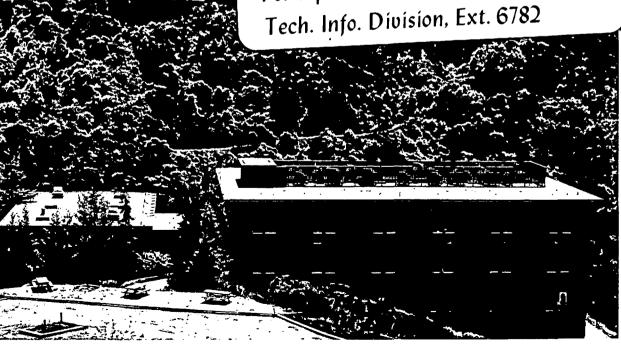
LIBRARY AND DOCUMENTS SECTION

H. Hindam and D.P. Whittle

November 1981

TWO-WEEK LOAN COPY

This is a Library Circulating Copy which may be borrowed for two weeks. For a personal retention copy, call Tach Info. Division, Ext. 6782



Prepared for the U.S. Department of Energy under Contract W-7405-ENG-48

DISCLAIMER

This document was prepared as an account of work sponsored by the United States Government. While this document is believed to contain correct information, neither the United States Government nor any agency thereof, nor the Regents of the University of California, nor any of their employees, makes any warranty, express or implied, or assumes any legal responsibility for the accuracy, completeness, or usefulness of any information, apparatus, product, or process disclosed, or represents that its use would not infringe privately owned rights. Reference herein to any specific commercial product, process, or service by its trade name, trademark, manufacturer, or otherwise, does not necessarily constitute or imply its endorsement, recommendation, or favoring by the United States Government or any agency thereof, or the Regents of the University of California. The views and opinions of authors expressed herein do not necessarily state or reflect those of the United States Government or any agency thereof or the Regents of the University of California.

PEG FORMATION BY SHORT CIRCUIT DIFFUSION IN Al₂O₃ SCALES CONTAINING OXIDE DISPERSIONS

H. Hindam and D. P. Whittle*

Lawrence Berkeley Laboratory, University of California Berkeley, California 94720

*Electrochemical Society Active Member.

This work was supported by the Director, Office of Energy Research, Office of Basic Energy Sciences, Materials Sciences Division of the U.S. Department of Energy under Contract No. W-7405-ENG-48.

It is well established that the addition of active elements (Y., Ce, Hf, Th, etc.) or dispersoids of the respective oxide phases improves the oxidation behavior of Cr_2O_3 and Al_2O_3 forming alloys and coatings. The beneficial effects include: enhancement of selective oxidation leading tocurtailment of the transient stage and rapid development of a protective scale, alteration of its growth rate and improvement in the adhesion of the scale to substrate. The latter effect. which represents significant practical importance for alloy protection, is the most dramatic and has received considerable attention. A recent review(1) has summarized the various observations and interpretations of this phenomenon. Whilst there is no general consensus view on the mechanism of scale adhesion, the formation of inwardly growing oxide pegs, which mechanically key the scale to substrate is recognized as a pertinent factor.

The purpose of this communication is to present recent observations and advance a mechanism for peg formation. A detailed model accounting for the development of such a tortuous alloy/scale interface and its implications on scale adhesion are the subject of a comprehensive future publication (2).

Alloy specimens with nominal compositions (wt.%) Fe-10Al and Fe-10Al-lHf were oxidized in air at 1200°C for a period of two weeks. The $\alpha\text{-Al}_20_3$ scale formed on the Hf-free alloy spalled readily upon cooling revealing a relatively planar alloy/scale interface exhibiting oxide free cavities(2). The structure of the tenaciously adherent scale formed on the Hf-containing alloy is shown in Figure (1). The upper micrograph is a deep-etched

Keywords: Alloy, Oxidation, Diffusion.

section while the lower one was obtained using conventional sample preparation procedures. The scale consists of $\alpha\text{-Al}_2\text{O}_3$ containing dispersed HfO $_2$ particles (light phase). Unreacted Fe particles are also embeded in the scale (arrows). Unlike the Hf-free alloy, the alloy/scale interface is highly irregular due to the development of a profusion of inwardly growing pegs. It is evident that the growth of these protrusions is closely related to the distribution of the HfO₂ precipitates incorporated in the scale. Although, the continuity of the HfO₂ particles cannot be adequately revealed in a two dimensional section, it can be seen occasionally that a well developed peg consists of a HfO₂ stringer completely enveloped by the Al₂O₃ scale.

In attempting to interpret peg formation, it was implicitly suggested (3) that $\mathrm{Al}_2\,\mathrm{O}_3$ grows inward in the alloy encapsulating the internal HfO₂ particles via preferential oxygen diffusion along the supposedly incoherent interfaces between the precipitates and alloy matrix. However, there is no evidence that HfO₂ is precipitated internally in the alloy ahead of the scale. Furthermore, recent measurements indicate that the relative contribution of boundary diffusion to the growth of α -Al₂O₃ internal precipitates in dilute Ni-Al alloys diminishes rapidly as temperature is increased in the range of $800-1100^{\circ}$ C(4) and becomes negligible at 1200°C(5), the temperature at which peg formation is predominant. Nevertheless, other interfaces such as between well oriented two phase Co-Cr-Al-Y alloy coating prepared by electron beam physical vapor deposition (PVD) might be effective for oxygen transport(6).

In the light of the present observations, the following growth model is proposed. The incorporation of HfO₂ as well as unreacted Fe particles in the scale is consistent with the Al₂O₃ growth on Hf-containing alloys being controlled by inward oxygen diffusion, most probably along grain boundaries and other structural imperfections. Since the diffusivity of oxygen in HfO₂ is expected to be several orders of magnitude greater than in Al₂O₃*, the HfO₂ precipitates within the scale act as short circuit diffusion paths for oxygen transport leading to preferential localized scale thickening in the neighborhood of these particles.

Figure (2) demonstrates that the scale thickness measured parallel to the local growth direction at random positions, as shown in the inset, increases linearly with increasing thickness of the HfO_2 precipitates. The scatter in the data is due, as mentioned earlier, to the difficulty in measuring the true length of the HfO_2 stringers. A least squares fit to the data gives a linear correlation factor of 0.88 and the gradient of the best fit line is 0.98 $\mu m/\mu m$, consistent with the very large difference in oxygen diffusivities in the oxides.

Once the concept of peg formation being caused by localized variations in the scale growth rate is accepted, a number of other important conclusions are evident. The distribution of the internal oxide particles, which are eventually incorporated into the scale, is important, as implied in earlier hypotheses (1,3,10). If the particles are too uniformly distributed, then localized variations in scale thickness tend to be smoothed out and the oxide protrusions will not penetrate very far into the alloy. A simple calculation shows that with 1% active element in the alloy produces approximately 2 vol. % oxide in the scale. If this

is uniformly distributed as, for example, 2 μm diameter spherical particles, then these would be 8 μm apart. This would be a poor distribution, since the resulting pegs would only penetrate about 20% thicker than the total scale thickness. The factors governing the microstructure and distribution of HfO_2 in the scale need to be examined.

The advanced model implies that differences in transport rates through the oxide of the active element and the host scale should be critical. Accordingly, the following generalizations can be made. Al $_2$ O $_3$ grows very slowly and almost any addition might be expected to locally increase its growth rate. This is not the case for Cr $_2$ O $_3$ scales, which may well explain why active element additions to Cr $_2$ O $_3$ forming alloys do not generally lead to appreciable oxide peg development although some improvement in adhesion is usually observed.

Acknowledgement

This work was supported by the Director, Office of Energy Research, Office of Basic Energy Sciences, Materials Science Division of the U.S. Department of Energy under Contract No. W-7405-ENG-48.

References

- D. P. Whittle and J. Stringer, Phil. Trans. Roy. Soc., London <u>A27</u>, 309 (1980).
- H. Hindam and D. P. Whittle, to be published.
- I. M. Allam, D. P. Whittle and J. Stringer, Oxid. Met. <u>12</u>, 35 (1978); ibid <u>13</u>, 381 (1979).
- D. P. Whittle, Y. Shida, G.C. Wood, F. H. Stott and D. B. Bastow, submitted to Phil. Mag. (1981).
- H. Hindam and D. P. Whittle, paper presented at the 34th Pac. Coast Regional Meeting of the American Ceram. Soc., Newport Beach, CA., October 1981.

^{*}The diffusivity of oxygen in pure Hf0 $_2$ has not yet been measured. However, it is expected to be within the range of that of oxygen-deficient oxides: $\sim 10^{-9}$ cm 2 /sec. in Nb $_2$ O $_5$ (7) and 10^{-7} cm 2 /sec. in Er $_2$ O $_3$ (8) at 1200°C. Do in polycrystalline α -Al $_2$ O $_3$ (9) is $\sim 10^{-15}$ cm 2 /sec.

- D. P. Whittle, D. H. Boone and I. M. Allam, Thin Sol. Films <u>73</u>, 359 (1980).
- 7. W. K. Chen and R. A. Jackson, J. Chem. Phys. <u>47</u>, 1144 (1967).
- 8. C. D. Wirkus, M. F. Berard and D. R. Wilder, J. Amer. Cer. Soc. <u>50</u>, 113 (1967).
- 9. Y. Oishi and W. D. Kingery, J. Chem. Phys. <u>33</u>, 480 (1960).
- 10. J. K. Tien and F. S. Pettit, Met. Trans., 3, 1587 (1972); C. S. Giggins, B. H. Kear, F. S. Pettit and J. K. Tien, Met. Trans. 5, 1685 (1974).

Figure 1. Section through Al₂O₃ scale formed on Fe-10 Al-1Hf formed at 1200°C showing pegs at alloy/scale interface and HfO₂ particles incorporated into the scale.

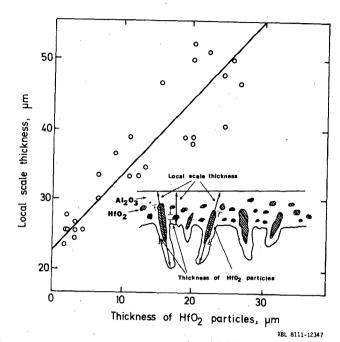
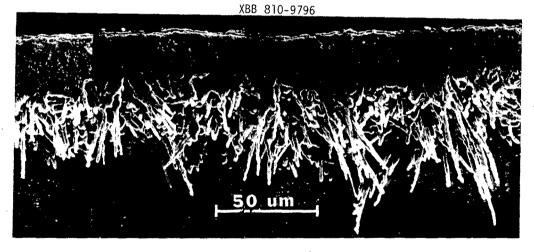


Figure 2. Local scale thickness as a function of thickness of HfO₂ particles.





This report was done with support from the Department of Energy. Any conclusions or opinions expressed in this report represent solely those of the author(s) and not necessarily those of The Regents of the University of California, the Lawrence Berkeley Laboratory or the Department of Energy.

Reference to a company or product name does not imply approval or recommendation of the product by the University of California or the U.S. Department of Energy to the exclusion of others that may be suitable.

TECHNICAL INFORMATION DEPARTMENT LAWRENCE BERKELEY LABORATORY UNIVERSITY OF CALIFORNIA BERKELEY, CALIFORNIA 94720