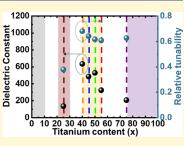


Exploring the Morphotropic Phase Boundary in Epitaxial $PbHf_{1-x}Ti_xO_3$ Thin Films

Megha Acharya, Handong Ling, Djamila Lou, Maya Ramesh, Brendan Hanrahan, Gabriel Velarde, Mark Asta, Kristin Persson, and Lane W. Martin*



a potential morphotropic phase boundary (MPB) akin to that in the PbZr_{1-x}Ti_xO₃ system. End members, PbHfO₃ and PbTiO₃, were found to possess orthorhombic (*Pbam*) and tetragonal (*P4mm*) crystal structures and antiferroelectric and ferroelectric (~87 μ C/cm²) behavior, respectively. PbHf_{0.75}Ti_{0.25}O₃ and PbHf_{0.25}Ti_{0.75}O₃ solid solutions were both found to be ferroelectric with rhombohedral (*R3c*, ~22 μ C/cm²) and tetragonal (*P4mm*, ~46 μ C/ cm²) structures, respectively. For intermediate PbHf_{1-x}Ti_xO₃ compositions (e.g., x = 0.4, 0.45, 0.5, and 0.55), a structural transition was observed from rhombohedral (hafnium-rich) to tetragonal (titanium-rich) phases. These intermediate compositions also exhibited mixedphase structures including *R3c*, monoclinic (*Cm*), and *P4mm* symmetries and, in all cases, were



ferroelectric with remanent $(5-22 \ \mu C/cm^2)$ and saturation $(18.5-36 \ \mu C/cm^2)$ polarization and coercive field $(24-34.5 \ kV/cm)$ values increasing with *x*. While the dielectric constant was the largest for PbHf_{0.6}Ti_{0.4}O₃, the MPB is thought to be near x = 0.5 after separation of the intrinsic and extrinsic contributions to the dielectric response. Furthermore, piezoelectric displacement–voltage hysteresis loops were obtained for all chemistries revealing displacement values as good as PbZr_{0.52}Ti_{0.48}O₃ films in the same geometry. Thereby, the PbHf_{1-x}Ti_xO₃ system is a viable alternative to the PbZr_{1-x}Ti_xO₃ system offering comparable performance.

INTRODUCTION

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Some of the best performing piezoelectrics are ferroelectric materials that exhibit large magnitudes of spontaneous polarization where the motion of domain walls can enhance the electromechanical response. Among the various families of piezoelectric ferroelectrics, PbZr_{1-x}Ti_xO₃ has been used extensively as both sintered ceramics and thin films for a multitude of applications including sensors, ultrasonic transducers, voltage-tunable capacitors, resonators, surface acoustic wave devices (e.g., filters, phase shifters, phase delay lines), electro-optic modulators, microelectromechanical system (MEMS)-based devices, and so on.¹⁻⁵ The PbZr_{1-x}Ti_xO₃ system is of particular interest because it exhibits a nearly temperature-independent phase boundary (at x = 0.48) called a morphotropic phase boundary (MPB) about which the material possesses outstanding dielectric and electromechanical properties.⁶⁻⁸ The mechanism for enhancement of the piezoelectric response at the MPB is thought to be related to the ease of rotation of the polar axis from rhombohedral to tetragonal phases facilitated by the presence of an intermediate monoclinic phase whose polar axis is expected to be contained along a direction in between that of the rhombohedral and tetragonal phases.^{9–12}

Thin films of $PbZr_{1-x}Ti_xO_3$ can, however, suffer from deleterious effects including polarization fatigue (degradation with read-write cycles) and retention (degradation with time), imprint, and low breakdown strength and switching

speed.^{13–17} Additionally, the integration of epitaxially grown PbZr_{1-x}Ti_xO₃ thin films on non-oxide semiconductor substrates for MEMS or CMOS processes can be challenging. 1,3,5,18,19 Epitaxial growth of $\bar{Pb}Zr_{1-x}Ti_xO_3$ films on silicon requires high temperatures and oxidizing environments that increase the risk of forming interfacial phases.^{19,20} In turn, identifying silicon-compatible functional oxides with dielectric, piezoelectric, and ferroelectric properties comparable to that of PbZr_{1-x}Ti_xO₃ has become increasingly important as these materials are being considered for a range of next-generation devices. While zirconium and hafnium are chemically similar,²¹⁻²³ zirconium exhibits higher reactivity with silicon²⁴ as compared to hafnium. The energetics of the reactions involved were further confirmed using the Interfaces Reaction application^{25,26} in the Materials Project²⁷ platform by comparing the reaction-energy values for the interfacial reactions of PbHfO3 and PbZrO3 with SiO2 as a function of mixing ratios (Figure S1a,b). Such effects have also been seen in recent experiments where, for example, a study on $Hf_{1-r}Zr_rO_2$ films grown on silicon used the zirconium for in

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situ scavenging of the interfacial SiO₂.²⁸ At the same time, the discovery of ferroelectricity in HfO₂-based materials²⁹ has driven a resurgence in efforts to integrate HfO₂-based ferroelectrics directly on silicon.^{30–32} Experimental trials with atomic layer deposition on silicon using hafnia-based precursors have been as successful as that with the zirconia-based precursors.³³

In the current work, we build from these lessons and explore the MPB in the PbHf_{1-x}Ti_xO₃ (0 < x < 1) system which is analogous to $PbZr_{1-x}Ti_xO_3$.^{34,35} Previous studies on PbHf_{1-x}Ti_xO₃ bulk ceramics and polycrystalline films report the presence of an MPB near PbHf_{0.5}O₃.^{33,36–45} Additionally, a few reports have suggested an improvement in fatigue and imprint behavior in certain compositions of polycrystalline $PbHf_{1-x}Ti_xO_3$ thin films as compared to that in $PbZr_{1-x}Ti_xO_3$. This, combined with the higher compatibility of the growth process, further motivates the need to more extensively study PbHf_{1-x}Ti_xO₃ as epitaxial thin films and probe the composition-driven evolution in the crystal structure and dielectric, piezoelectric, and ferroelectric properties. In this spirit, here, highly crystalline, fully relaxed, and epitaxial PbHf_{1-x}Ti_xO₃ (x = 0, 0.25, 0.4, 0.45, 0.5, 0.55, 0.75, and 1) thin films are synthesized on $SrRuO_3/SrTiO_3(001)$ substrates. Using X-ray diffraction, the crystal structure and lattice parameters of the films are examined. Similar to the $PbZr_{1-r}Ti_rO_3$ system, a structural phase transition is observed as the ratio of Ti^{4+} (ionic radius of 0.61 Å) to Hf^{4+} (ionic radius of 0.76 Å) is varied wherein the $PbHf_{1-r}Ti_rO_3$ system goes from an orthorhombic (*Pbam*) phase for $PbHfO_3^{46}$ to a rhombohedral (R3c) phase for PbHf_{0.75}Ti_{0.25}O₃ to a mixedphase regime (i.e., a mixture of rhombohedral R3c, monoclinic *Cm*, and tetragonal *P*4*mm* phases) in the range x = 0.4-0.55, before finally transitioning to a purely tetragonal (P4mm) phase for PbHf_{0.25}Ti_{0.75}O₃ and PbTiO₃. Subsequent study of ferroelectric polarization-electric field hysteresis loops reveals a transition from antiferroelectric behavior for the x = 0heterostructures to ferroelectric behavior in the composition range x = 0.25 - 1. The remanent and saturation polarization and the coercive-field values increase with increasing titanium content owing to the larger magnitude of polar displacement (again consistent with the $PbZr_{1-x}Ti_xO_3$ system). Furthermore, composition-dependent dielectric constant (ε_r) measurements indicate an enhancement in the dielectric response in the composition range x = 0.4 - 0.55 that is attributed to the coexistence of the rhombohedral, monoclinic, and tetragonal phases and the ease of polarization rotation therein. Fielddependent studies of ε_r are used to estimate the intrinsic and extrinsic contributions to response, and the maximum intrinsic response is found for PbHf_{0.5}Ti_{0.5}O₃ heterostructures (the likely location of the MPB) while the maximum extrinsic response was found for PbHf_{0.6}Ti_{0.4}O₃ heterostructures (pointing to the presence of a comparatively mobile-domain configuration). The piezoelectric response of heterostructures of all compositions was measured using piezoresponse force microscopy (PFM) and laser Doppler vibrometry and compared to that of films of $PbZr_{0.52}Ti_{0.48}O_3$ of the same thickness and geometry. The piezoresponse of the $PbHf_{1-x}Ti_xO_3$ films, especially near the MPB, was found to be comparable to that of PbZr_{0.52}Ti_{0.48}O₃, further reinforcing the similarity between the two material systems as well as the potential for the use of this system in applications calling for low-loss, high-performance piezoelectric thin films.^{47,48}

EXPERIMENTAL SECTION

Growth of Thin-Film Heterostructures. 50-200 nm-thick $PbHf_{1-x}Ti_xO_3$ (x = 0, 0.25, 0.4, 0.45, 0.5, 0.55, 0.75, and 1) thinfilm heterostructures were synthesized on (001)-oriented SrTiO₃ substrates using pulsed-laser deposition. 35-45 nm-thick SrRuO3 layers were used as the conducting oxide for both the top and bottom electrodes. Pulsed-laser deposition was performed by ablating ceramic targets using a KrF excimer laser (248 nm, LPX 300, Coherent), in an on-axis geometry with the target-to-substrate distance of 55 mm. Multiple growth conditions and target chemistries were explored for synthesizing the parent compositions (i.e., PbHfO₃ and PbTiO₃). The best results were obtained for PbHfO₃ (PbTiO₃) heterostructures grown on SrTiO₃(001) substrates at a laser fluence of 1.93 J/cm², a laser repetition rate of 10 Hz (5 Hz), a heater temperature of 600 °C (650 °C), and a dynamic oxygen pressure of 10 mTorr (100 mTorr) and using ceramic targets with composition PbHfO₃ (Pb_{1.1}TiO₃). The $PbHf_{1-x}Ti_xO_3$ solid solutions (x = 0.25, 0.4, 0.45, 0.5, 0.55, and 0.75) were synthesized using two different routes. The first case involved synthesis using alternate ablation from the two parent targets (i.e., PbHfO₃ and PbTiO₃) with sub-unit-cell-level mixing using a programmable target rotator (Neocera, LLC) synced with the excimer laser. In this approach, by alternating pulses from the different targets in the right proportions, any composition can be obtained. In the other case, individual targets with compositions $PbHf_{1-x}Ti_xO_3$ (x = 0.4, 0.45, 0.5, and 0.55) were used for synthesizing the heterostructures. For thin-film heterostructures with compositions PbHf_{0.75}Ti_{0.25}O₃ and PbHf_{0.25}Ti_{0.75}O₃, the best results were obtained with the first route (i.e., with alternate ablation from two parent targets), while for compositions $PbHf_{1-x}Ti_xO_3$ (x = 0.4, 0.45, 0.5, 0.55) the best results were obtained with the second route (i.e., ablation from a single target). For all growths, the heterostructures were cooled from the growth temperature to room temperature at 10 °C/min. in a static oxygen pressure of ~760 Torr.

Structural Characterization Using X-ray Diffraction. X-ray diffraction studies were performed to determine the crystal structure of the synthesized PbHf_{1-x}Ti_xO₃ (x = 0, 0.25, 0.4, 0.45, 0.5, 0.55, 0.75, and 1) thin-film heterostructures with a high-resolution X-ray diffractometer (Panalytical, X'Pert³ MRD) using 1/2° and 1/16° slits for the incident optics and a 0.275 mm slit for the diffracted-beam optics for the PIXcel3D-Medipix3 detector. The structural properties of the thin films in the out-of-plane direction (perpendicular to the plane of the substrate) were probed using $\theta - 2\theta$ line scans. The crystalline quality of the films in the plane of the substrate was assessed using X-ray rocking curves about the 002nc-diffraction condition of all heterostructures. Furthermore, (a)symmetric azimuthal scans were carried out about the PbHf_{1-x}Ti_xO₃ 118_R- and 006_{R} (for PbHf_{0.75}Ti_{0.25}O₃ heterostructures), $20\overline{2}_{M}$ (for PbHf_{0.5}Ti_{0.5}O₃ heterostructures), and 112_{T} and 101_{T} (for PbHf_{0.25}Ti_{0.75}O₃ heterostructures) diffraction conditions while varying the azimuthal angle (φ) at a fixed 2θ and sample-stage tilt (χ) value. Additionally, in order to determine the crystal structure and the lattice parameters of the heterostructures with composition $PbHf_{1-x}Ti_xO_3$ (x = 0, 0.25, 0.4, 0.45, 0.5, 0.55, 0.75, and 1), X-ray diffraction reciprocal space mapping (RSM) studies were performed about the 362₀- and 084_{O} -diffraction conditions (PbHfO₃), 103_{pc} - and 202_{pc} -diffraction conditions [PbHf_{1-x}Ti_xO₃ (x = 0.25, 0.4, 0.45, 0.5, 0.55, 0.75, and 1)] of the films and SrTiO₃ 103-diffraction condition of the SrTiO₃ substrate, as appropriate.

Electrical and Dielectric Characterization. All electrical measurements were conducted in a dark and noise-isolated enclosure with the drive electrical bias applied through the top electrode. The electrical properties for heterostructures of all compositions [PbHf_{1-x}Ti_xO₃ (x = 0, 0.25, 0.4, 0.45, 0.5, 0.55, 0.75, and 1)] were studied for 50–200 nm-thick films grown on SrTiO₃(001) substrates. While all the synthesized heterostructures could be characterized successfully, the temperature-dependent dielectric characterization was found to be challenging for the PbHf_{1-x}Ti_xO₃ films less than 200 nm thick owing to a high dielectric loss factor (>0.1). We point out that this is generally common in thin films and was variable across the

compositions studied. To provide directly comparable results, in turn, we focused on results obtained for 200 nm-thick $PbHf_{1-x}Ti_xO_3$ heterostructures. Furthermore, 45- and 35-nm-thick films of a conducting oxide, SrRuO₃, were used as the top and bottom electrodes, respectively. A relatively thicker film was used for the top electrode as compared to that for the bottom electrode to counteract for any potential degradation in the quality of the top electrode, having been synthesized at a slightly lower temperature (650 °C) as compared to the bottom electrode (700 °C). The thicker top electrode also allows it to be more robust to repeated contacting for measurements using micropositioner-based probes."

The measurements were performed with circular-capacitor (diameter 25 μ m) structures patterned on the top electrode using photolithography, followed by wet chemical etching of SrRuO3 via a 0.1 M NaIO₄ solution. The polarization values were measured as a function of electric field (-650 to 650 kV/cm) at room temperature using a Precision Multiferroic Tester (Radiant Technologies, Inc.). Prior to any dielectric measurements, all the capacitors were switched 50–60 times and poled with a bias of a magnitude -1 V with a dwell time of 1 s. Dielectric and loss tangent measurements were performed as a function of frequency (1-100 kHz), temperature (25-550 °C), DC electric field (-250 to 250 kV/cm), and up to a maximum AC field strength value of 50 kV/cm using an E4990A Impedance Analyzer (Keysight Technologies). For the frequency-dependent DC bias measurements, an AC signal with an excitation amplitude of 10 mV (which translates to a field of 0.5 kV/cm) was applied with the frequency being varied between 1 and 100 kHz for a fixed applied background DC bias. The applied background DC bias was varied from 0 to -250 kV/cm with a step size of 5 kV/cm. For the Rayleigh measurements (AC excitation-dependent studies), an AC signal was applied, and its excitation amplitude was varied from 0 to 50 kV/cm at a fixed frequency of 10 kHz while maintaining zero background bias

Electromechanical Characterization with PFM. The localized piezoelectric displacement hysteresis loops were measured as a function of an applied voltage via switching spectroscopy-based PFM using an MFP-3D (Asylum Research). The applied voltage was in the form of a sine wave (AC excitation signal) which is carried by a square wave (DC bias) which steps up or down in magnitude as a function of time (in the form of a triangular-square pulse). Between each voltage step, the DC bias offset is set to zero while the AC excitation is still active, to determine the bias-induced change in displacement. This displacement was measured as a function of applied DC bias continuously while cycling the pulse 5-10 times (each cycle has a duration of 5 s).

Electromechanical Characterization with Laser Doppler Vibrometry. For the macroscopic electromechanical surface displacement studies, the heterostructures were electrically stimulated with an AC-excitation field (-350 to 350 kV/cm) at a frequency of 10 kHz using a ferroelectric tester (Precision Multiferroic Tester, Radiant Technologies, Inc.) while a 2 μ m-sized HeNe laser ($\lambda = 633$ nm) spot was focused on the surface of the 50 μ m-diameter top electrode. Upon applying electrical field, the capacitor structure will be displaced vertically along the path of the laser owing to the macroscopic electromechanical response of the heterostructures. The magnitude of the response was monitored using a laser vibrometer (PolyTech GmbH) with a sensitivity of 5 nm/V. Based on the electrical feedback received from the vibrometer, the surface piezoelectric displacement values were determined as a function of electric field using the ferroelectric tester.

First-Principles Density Functional Perturbation Theory (**DFPT**) **Calculations.** Piezoelectric tensors and force constants are calculated for PbHf_{1-x}Ti_xO₃ compositions of $2 \times 2 \times 1$ supercells of the perovskite structure comprising 20 atoms. The calculations were performed for certain selected PbHf_{1-x}Ti_xO₃ compositions with x = 0, 0.25, 0.5, 0.75, and 1, where the titanium content was increased from x = 0 to 1 for two different parent compounds, that is, the rhombohedral and the tetragonal crystal structure. The composition PbHf_{0.5}Ti_{0.5}O₃ was found to exhibit two distinct cation orderings for the supercell in consideration. The piezoelectric and dielectric tensors

of these systems are calculated using DFPT, $^{49-52}$ utilizing the Vienna ab initio simulation package^{\$3,54} within the PBE generalized gradient approximation (GGA+U).⁵⁵ An energy cut-off for the plane waves is set at 1000 eV with a *k*-point density of approximately 2000 per reciprocal atom (pra) for the DFPT calculations.⁵⁶ The resulting piezoelectric and dielectric values reported are the maximum modulus of the total tensors.

RESULTS AND DISCUSSION

50–200 nm-thick PbHf_{1-x}Ti_xO₃ (x = 0, 0.25, 0.4, 0.45, 0.5, 0.55, 0.75, and 1) thin-film heterostructures were grown on 45 nm SrRuO₃/SrTiO₃(001) substrates using pulsed-laser deposition as noted in the Experimental Section. Following growth, X-ray diffraction was used to study the structure and epitaxy of the films as noted in the Experimental Section. Before discussing the results, it is useful to explore what is known about the crystal structures of this system. The end member PbHfO₃ is known to be antiferroelectric and to exhibit an orthorhombic crystal structure (*Pbam; Figure 1a*).⁴⁶ Three

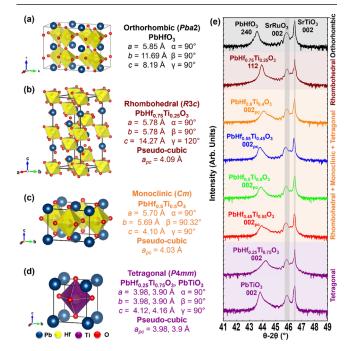


Figure 1. Crystal structure and lattice parameters for (a) the orthorhombic (*Pba2*) antiferroelectric phase of PbHfO₃, (b) the rhombohedral (*R3c*) ferroelectric phase of PbHf_{0.75}Ti_{0.25}O₃, (c) the monoclinic (*Cm*) ferroelectric phase of PbHf_{0.25}Ti_{0.5}O₃, and (d) the tetragonal (*P4mm*) ferroelectric phase of PbHf_{0.25}Ti_{0.75}O₃ and PbTiO₃. (e) X-ray-diffraction measurements (θ -2 θ line scan) for 200-nm-thick, (240_O)-oriented PbHfO₃, 112_R-oriented PbHf_{0.75}Ti_{0.25}O₃, and 002_{pc}-oriented PbHf_{1-x}Ti_xO₃ (with x = 0.4, 0.45, 0.5, 0.55, 0.75, and 1) heterostructures grown on 40 nm SrRuO₃/SrTiO₃(001) substrates.

types of crystal structures have been reported for bulk-ceramic versions of $PbH_{f_{-x}}Ti_xO_3$: (1) rhombohedral (*R3c*; Figure 1b) for $x \le 0.5$, (2) monoclinic (*Cm*; Figure 1c) for $PbHf_{0.5}Ti_{0.5}O_3$, and (3) tetragonal (*P4mm*; Figure 1d) for $x \ge 0.6$.^{42,43,57} Looking now at the films produced herein, in all cases, the films were found to be single crystalline and phase-pure (Figure 1e). End-member PbHfO₃ heterostructures were fully (240₀)-oriented (where the subscript 'O' refers to orthorhombic indices) and end-member PbTiO₃ heterostructures were fully (001)-oriented and exhibited a tetragonal crystal

structure. Using θ -2 θ line scans (Figure 1e) and RSM studies about the 084₀- and 362₀- (for PbHfO₃ heterostructures; Figure S2) and 103- and 202-diffraction conditions (for PbTiO₃ heterostructures; Figure S3), the crystal structure and lattice parameters were extracted (Table S1).

Exact attribution of the crystal structure for single-crystalline thin films is somewhat challenging because of the limited number of diffraction conditions accessible through laboratorybased diffractometers. From prior studies on bulk ceramics, the $PbHf_{0.75}Ti_{0.25}O_3$ and $PbHf_{0.25}Ti_{0.75}O_3$ heterostructures were expected to exhibit rhombohedral (R3c) and tetragonal (P4mm) structures, respectively. To evaluate if this was the case here, azimuthal scans about the R3c $118_{\rm R}$ - ($2\theta = 54.57^{\circ}$, sample-stage tilt (χ) = 35.33, where the subscript 'R' stands for lattice indexing corresponding to rhombohedral structure) and P4mm 112- $(2\theta = 55.25^{\circ}, \text{ sample-stage tilt } (\chi) = 36.22)$ diffraction conditions were completed. From this, the presence (absence) of rhombohedral (tetragonal) and tetragonal (rhombohedral) phases in the PbHf_{0.25}Ti_{0.75}O₃ and PbHf_{0.75}Ti_{0.25}O₃ heterostructures, respectively, was confirmed (Figure S4). In prior studies on $PbHf_{0.5}Ti_{0.5}O_3$ ceramics, the crystal structure was found to be predominantly monoclinic (Cm); however, being close to the phase boundary, it also contained a minor phase with rhombohedral (R3c) symmetry.^{42,57} Using the same azimuthal-scan methodology, but now looking for the monoclinic $Cm \ 20\overline{2}_{M}$ -diffraction condition (2 θ = 54.94°, sample-stage tilt (χ) = 35.86, where the subscript 'M' stands for lattice indexing corresponding to monoclinic structure) along with that for the rhombohedral and tetragonal phases (noted above), we explored the compositions near the 'potential' phase boundary (i.e., x = 0.4-0.55 heterostructures; Figure S5). As expected, the compositions demonstrated nonzero peak intensity for all three diffraction conditions indicating a complex mixture of phases with R3c, Cm, and P4mm symmetry. To further understand the nature of the structure for these mixed-phase compositions, the peak profile corresponding to the 003_{pc}-diffraction condition for these heterostructures was fit using Voigt functions to estimate the volume fraction of the three phases (i.e., R3c, Cm, and P4mm; Figure S6). The mixed-phase heterostructures (i.e., x = 0.4– 0.55) exhibited different volume fractions of R3c (23.5-32.4%), Cm (27.5-61.3%), and P4mm (9.5-49%) phases. Akin to the end-member films, the lattice parameters corresponding to the rhombohedral (PbHf_{0.75}Ti_{0.25}O₃), mixed-phase (x = 0.4-0.55), and tetragonal (PbHf_{0.25}Ti_{0.75}O₃) heterostructures were determined (Figures S7 and S8) and summarized (Table S1). All heterostructures were found to be fully relaxed, consistent with the large lattice mismatch between the $PbHf_{1-x}Ti_xO_3$ films and the substrate. For the compositions with mixed-phase and tetragonal structures, the c/a ratio (tetragonality) was found to increase with increasing titanium content, which can be interpreted as an increasing volume fraction of the tetragonal phase.⁴⁴ Knowing the crystal structure and the lattice parameters, the epitaxial relationship of the synthesized heterostructures to the substrate was also determined using off-axis azimuthal scans as noted in the Experimental Section. While the rhombohedral (PbHf_{0.75}Ti_{0.25}O₃) end member was found to exhibit two rotational variants (I and II) with the corresponding epitaxy as $P b H f_{0.75} T i_{0.25} O_3 [100_R] || S r T i O_3 [100] and$ $PbHf_{0.75}Ti_{0.25}O_3[100_R]||SrTiO_3[010]$ (Figure S9), the (predominantly) monoclinic mixed-phase heterostructures (i.e., x =0.4-0.55) were found to be single-variant with the epitaxy as

PbHf_{1-x}Ti_xO₃ (x = 0.4-0.55)[110_M]llSrTiO₃[100] (Figure S10). The tetragonal (PbHf_{0.25}Ti_{0.75}O₃) end member, on the other hand, was found to be single-variant and to exhibit relatively simplistic epitaxy such that PbHf_{0.25}Ti_{0.75}O₃[100]ll SrTiO₃[100] (Figure S11).

The structure, as expected, varies dramatically with chemistry and, considering that the polarization depends strongly on structure, the ferroelectric properties should also vary. Capacitor structures were fabricated as noted in the Experimental Section and ferroelectric hysteresis loops were measured as a function of electric field (at a frequency of 10 kHz) for all heterostructures as noted in the Experimental Section (Figure 2). Starting with the PbHfO₃ heterostructures,

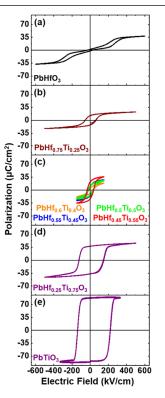


Figure 2. Polarization-electric field hysteresis loops at a frequency of 10 kHz for capacitors 25 μ m in diameter for (a) the orthorhombic (*Pba2*) antiferroelectric phase of PbHfO₃, (b) the rhombohedral (*R3c*) ferroelectric phase of PbHf_{0.75}Ti_{0.25}O₃, (c) the mixed-phase ferroelectric PbHf_{1-x}Ti_xO₃ x = 0.4, 0.45, 0.5, and 0.55 compositions, and tetragonal (*P4mm*) ferroelectric phases of (d) PbHf_{0.25}Ti_{0.75}O₃ and (e) PbTiO₃.

which are known to be robustly antiferroelectric, a characteristic double-hysteresis loop was observed indicating an electric field-induced phase transition from a nonpolar (*Pbam*) to a polar, ferroelectric (*Pba2*) phase with a maximum polarization of ~53 μ C/cm² at 1600 kV/cm (Figures 2a and S12). As even a relatively small amount of titanium is incorporated, as in the PbHf_{0.75}Ti_{0.25}O₃ heterostructures, ferroelectric behavior (with remanent and saturation polarization of ~12.5 and ~22 μ C/ cm², respectively, and a coercive field ~60 kV/cm) is observed, consistent with the crystal structure changing from orthorhombic to rhombohedral symmetry. Upon further increasing the titanium content (as in the *x* = 0.4–0.55 heterostructures), ferroelectric behavior is retained and the remanent (~5, ~11, ~12, and ~22 μ C/cm², respectively) and saturation (~18.5, ~28, ~27, and ~36 μ C/cm², respectively) polarization and the

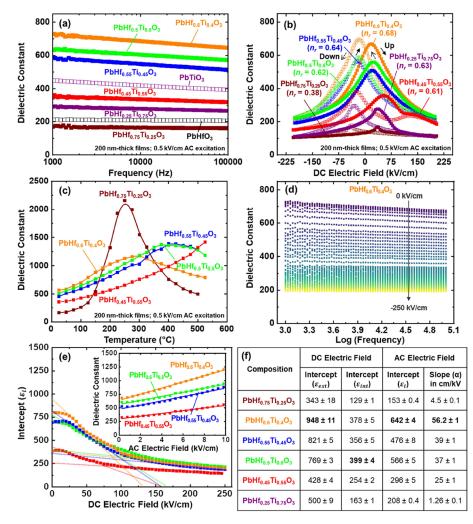


Figure 3. Dielectric constant measurements for PbHf_{1-x}Ti_xO₃ heterostructures with x = 0, 0.25, 0.4, 0.45, 0.5, 0.55, 0.75, and 1 (a) as a function of frequency from 1 to 1000 kHz and (b) as a function of background DC field at frequency 10 kHz with two different voltage sweep directions (marked by solid and hollow squares for up and down, respectively). (c) Dielectric constant measurements of PbHf_{1-x}Ti_xO₃ heterostructures with <math>x = 0, 0.25, 0.4, 0.45, 0.5, 0.75, and 1 (a) as a function of temperature (25–525 °C) at 10 kHz. (d) Dielectric constant as a function of frequency measured with increasing background DC field for a PbHf_{0.6}Ti_{0.4}O₃ heterostructure. (e) Plot of zero-field dielectric constant (ε_i) as a function of background DC field. The inset shows dielectric constant (ε_r) as a function of AC excitation for PbHf_{1-x}Ti_xO₃ heterostructures with x = 0.4-0.55. (f) Summary of the fitting parameters for the DC and AC-field dependent measurements.

coercive field (~24, ~27, ~30, and ~34.5 kV/cm, respectively) were all found to gradually increase with x. This is consistent with a systematic increase in the polar displacement (tetragonality) with increasing titanium content. Increasing the titanium content further, as in the PbHf_{0.25}Ti_{0.75}O₃ heterostructures, results in a tetragonal structure and further increases in the remanent (38 μ C/cm²) and saturation (46 μ C/cm²) polarization as well as the coercive field (130 kV/cm). Finally, for the PbTiO₃ heterostructures (with the highest tetragonality), the remanent and saturation polarization (87 μ C/cm²) and the coercive field (179 kV/cm) were found to be the highest across the $PbHf_{1-x}Ti_xO_3$ system. All told, an increase in polar displacement (polarization) with increasing titanium content was accompanied by an increase in the coercive field (because the magnitude of spontaneous polarization for a ferroelectric is directly proportional to the intrinsic coercive field).^{58,59} On a mesoscopic scale, a higher energy associated with the nucleation and motion of 180° domains walls in tetragonal phases during switching can further increase the coercive field

values.⁶⁰ Thereby, in parallel to a structural phase transition from the rhombohedral to tetragonal phase with increasing titanium content (x = 0.25 to 1), a simultaneous increase in remanent and saturation polarization and coercive field values was observed, likely to be due to the increasing volume fraction of tetragonal phase.

Having studied the structural and ferroelectric properties of single- and mixed-phase (anti)ferroelectric compositions for PbHf_{1-x}Ti_xO₃, we now focus on the primary realm of interest: the properties of the mixed-phase compositions (x = 0.4-0.55) in the vicinity of the expected MPB. We begin by measuring the frequency-dependent ε_r as noted in the Experimental Section as a function of composition (Figure 3a). All heterostructures exhibit minimal frequency dependence of response (across the frequencies studied), and the ε_r increases moving from both end-member compositions and is a maximum for the PbHf_{0.6}Ti_{0.4}O₃ heterostructures. The ε_r was also probed as a function of DC-background bias (Figure 3b) to explore dielectric tunability (n_r).^{61,62} As expected, the highest tunability was observed in the vicinity of the MPB

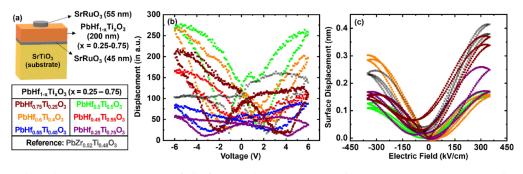


Figure 4. Electromechanical response measurements of $PbH_{1-x}Ti_xO_3$ heterostructures with x = 0.25, 0.4, 0.45, 0.5, 0.55, and 0.75. (a) Schematic of the capacitor geometry and key of samples (colors are consistent throughout the figure). (b) Using switching spectroscopy in PFM at a frequency of 0.2 Hz, piezoelectric displacement–voltage butterfly loops were acquired. (c) Macroscopic surface displacement butterfly loops were acquired from 50 μ m-diameter capacitors using laser vibrometry. Note that while accurate electric field values can be provided for the studies completed on macroscopic capacitors (c), the added voltage drop at the scanning probe tip-capacitor interface render field values incomparable; hence we report voltages in (b).

compositions with the highest value (68% for a field of 200 kV/cm found for the PbHf_{0.6}Ti_{0.4}O₃ heterostructures, further confirming the observation that materials with high ε_r typically have higher tunability.^{11,63,64} Next, ε_r was measured for all compositions as a function of temperature from 25 to 550 $^\circ \mathrm{C}$ as noted in the Experimental Section.⁶⁵⁻⁶⁷ With increasing titanium content, the peak in ε_r (and therefore the Curie temperature, T_c) appears to shift to higher temperatures, making the measurements more unreliable due to the higher loss tangent values at the highest temperatures probed herein. Here, data for heterostructures of composition x = 0, 0.25, 0.4,0.45, 0.5, and 0.55 for which the loss tangent for most of the measured temperature range was <0.15 are shown (Figures 3c and S13). All the synthesized heterostructures exhibit a peak corresponding to the ferroelectric-to-paraelectric phase transition in their dielectric constant vs temperature curves. Such observations are consistent with the studies on the composition-dependent evolution of $T_{\rm C}$ in ${\rm PbZr}_{1-x}{\rm Ti}_x{\rm O}_3^9$ as well as $PbHf_{1-x}Ti_xO_3^{44}$ ceramics.

Past studies on PbHf_{1-x}Ti_xO₃ ceramics found PbHf_{0.5}Ti_{0.5}O₃ 33840414468as the composition corresponding to the MPB.^{33,38,40,41} The presence of complex domain structures, however, can greatly influence the dielectric behavior of the mixed-phase, thin-film compositions (x = 0.4-0.55). Thus, two measurements were performed, as noted in the Experimental Section, to help better identify the location of the MPB in the films: frequency-dependent ε_r measurements with increasing DC-background bias^{48,69–71} and Rayleigh studies as a function of increasing AC field.^{72,73} Such studies allow for the quantification of the intrinsic/extrinsic and reversible/irreversible contributions to the dielectric response. For the first measurement, the background-DC electric field studies involved fitting the frequency-dependence (from 1 to 100 kHz) of ε_r at each value of electric field (0 to -250 kV/cm) to the equation $\varepsilon_{\rm r} = \varepsilon_{\rm i} - \alpha \log f$ and extracting the fielddependent intercept (ε_i) and the slope (α). As an example, we present the electric field-dependent dielectric response for one composition (x = 0.4; Figure 3d), but the datasets for the other compositions near the MPB (x = 0.4-0.55) are also provided (Figure S14). Furthermore, ε_i is plotted as a function of the applied background-DC bias for the compositions near the MPB (Figure 3e). Such plots typically show two regimes based on the contribution to the overall dielectric response. The lowfield regime arises from a mixture of intrinsic (fundamental response of the polarization within a domain to applied field)

and extrinsic (response due to movement of domain walls) contributions while the high-field regime provides a way to probe the intrinsic contribution (because the domain walls are pinned by the high field and are static). The intercepts, in turn, quantify the intrinsic and the extrinsic contribution to the overall dielectric response, and the slope can be considered as a form of tunability which measures how effectively the applied DC electric field can suppress the extrinsic response. For the second measurement type (i.e., Rayleigh studies), the dielectric response was recorded as a function of applied AC-excitation field at a frequency of 10 kHz with zero background-DC bias. The linear (low-field) regime of the plots was fitted to the Rayleigh law $\varepsilon_r = \varepsilon'_i + \alpha' E_i$, where *E* is the magnitude of the AC electric field and the fitting parameters ε'_i and α' are the reversible and irreversible domain-wall contributions to the overall dielectric response, respectively (inset, Figure 3e). To compare the mixed-phase compositions with the single-phase ferroelectric compositions, similar measurements were performed for PbHf_{0.75}Ti_{0.25}O₃ and PbHf_{0.25}Ti_{0.75}O₃ heterostructures (Figure S15a,b). The intercept for the linear fits in the low-field (ε_{ext}) and the high-field (ε_{int}) regimes for DC fielddependent studies and the reversible (ε'_i) and irreversible (α') domain-wall contributions obtained from the linear Rayleigh fits for AC field-dependent studies have been summarized for all heterostructures (Figure 3f).

There were several observations from the DC and AC fielddependent dielectric studies worth highlighting. Overall, as expected, the mixed-phase compositions (i.e., x = 0.4-0.55) exhibit a higher ε_r as compared to the single-phase compositions (i.e., PbHfO₃, PbHf_{0.75}Ti_{0.25}O₃, PbHf_{0.25}Ti_{0.75}O₃, and PbTiO₃). As seen in the structural characterization, the presence of a dominant monoclinic phase in the mixed-phase compositions can be the reason for enhanced dielectric response owing to the ease of polarization rotation (similar to what is observed in the $PbZr_{1-x}Ti_xO_3$ system).^{10,12} Delving deeper into the $PbHf_{1-x}Ti_xO_3$ compositions with the DC fielddependent studies, first, in the low-field regime, the mixedphase compositions (x = 0.4-0.55) exhibited a considerably higher ε_{ext} (428-948) as compared to the PbHf_{0.75}Ti_{0.25}O₃(343) and PbHf_{0.25}Ti_{0.75}O₃(500) heterostructures. Within the mixed-phase compositions, $\varepsilon_{\mathrm{ext}}$ was the highest for the PbHf_{0.6}Ti_{0.4}O₃ heterostructures (948) indicating a relatively higher contribution of domain walls in the same. On the other hand, $\varepsilon_{\rm int}$ was the highest for the PbHf_{0.5}Ti_{0.5}O₃ heterostructures. This suggests that the MPB is

likely close to PbHf_{0.5}Ti_{0.5}O₃ instead of PbHf_{0.6}Ti_{0.4}O₃, despite the latter showing a higher overall ε_r . Similar conclusions can be drawn from the Rayleigh studies, where the reversible (ε_i) and irreversible (α') domain-wall contributions are the highest for the PbHf_{0.6}Ti_{0.4}O₃ heterostructures. Such observations can be connected back to the ferroelectric measurements where the coercive field values for the PbHf_{1-r}Ti_rO₃ heterostructures were found to increase with increasing titanium content (likely related to the increasing tetragonal phase fraction), owing to the higher energy associated with the movement of 180° domains walls in tetragonal phases during switching.⁶⁰ Among the mixed-phase compositions, the PbHf_{0.6}Ti_{0.4}O₃ heterostructures should possess the lowest fraction of tetragonal phase, being closer to the rhombohedral (hafnium-rich) side of the phase diagram. Thereby, the relative ease in polarization rotation caused by the presence of non-180° domain-wall motion therein could be the reason for the higher extrinsic response in the $PbHf_{0.6}Ti_{0.4}O_3$ heterostructures (as compared to that in $PbHf_{0.5}Ti_{0.5}O_3$).

The enhanced dielectric response in the mixed-phase $PbHf_{1-x}Ti_xO_3$ compositions (x = 0.4-0.55) reinforces the idea that it is possible to realize the MPB phenomenon in a silicon-compatible system with properties similar to those observed in the archetypal $PbZr_{1-x}Ti_xO_3$. Thereby, after the structural, ferroelectric, and dielectric measurements, the electromechanical properties for the synthesized capacitor heterostructures were characterized using switching spectroscopy-based PFM as noted in the Experimental Section. Note that quantitative extraction of piezoelectric coefficients using such PFM approaches is challenging,⁷⁴⁻⁷⁶ thus, we provide only qualitative and relative measures herein. The displacement-voltage hysteresis loops and the corresponding change in phase for 200 nm-thick PbHf_{1-x}Ti_xO₃ films (Figures 4a and S16) were measured, with PbHf_{0.5}Ti_{0.5}O₃ and PbHf_{0.6}Ti_{0.4}O₃ demonstrating the highest piezoelectric displacement values (Figure 4b). Though in theory, a relatively higher magnitude of enhancement in piezoelectric displacement (and coefficient, d_{33}) values would be expected for the mixed-phase compositions (x = 0.4-0.55), the same was not exactly seen in practice. This is not surprising for PFM-based measurements because some of the past studies with $PbZr_{1-x}Ti_xO_3$ films have shown similar results, where no actual compositiondependent change in the measured d_{33} values was detected for films $\leq 1 \ \mu m$ thick.^{77,78} To further explore this point (and acknowledging the potential limitations of such PFM-based studies), we probed the same heterostructures using laser Doppler vibrometry as noted in the Experimental Section (Figure S17a), which allows us to directly measure the macroscopic electromechanical surface displacement of the capacitors (Figures 4c and S17b). These studies reveal that the displacement values for all heterostructures are similar in magnitude without any significant composition-dependent enhancement and are similar to that of PbZr_{0.52}Ti_{0.48}O₃.

It seems important to delve a bit deeper into the reasoning for such behavior. Similar to the dielectric response, the piezoelectric response too can have both intrinsic and extrinsic contributions, especially near the MPB. Unlike the dielectric response of thin films, however, observing any compositiondependent enhancement in piezoelectric response can be challenging^{78,79} due to the mechanical clamping imposed by the underlying substrate suppressing the voltage-dependent piezoelectric displacement in the thin-film heterostructures. The substrate-induced clamping in such cases suppresses both

the intrinsic (value expected for the material in a monodomain state) and the extrinsic (value inclusive of the movement of ferroelastic domain walls in the absence of any clamping) contributions to the piezoelectric response. $^{69-72}$ Furthermore, the thickness of the film can be a governing factor in determining the severity of substrate-induced clamping. For films with thickness $\geq 1 \ \mu m$, restrictions on domain-wall motion were found to be severely reduced, thus leading to a more accurate estimate of the piezoelectric properties.^{71,77,80,81} Due to these limitations, we turned to ab initio methods as noted in the Experimental Section to further understand the evolution of the properties near the MPB. As expected from the past studies on $PbHf_{1-x}Ti_xO_3$,^{41,45} the calculated modulus values for both piezoelectric and dielectric response were found to exhibit a maximum near the mixed-phase compositions (Figure S18), further reinforcing the presence of a phase boundary therein. Thus, despite the lack of a quantitative analysis using PFM-based characterization, it is worth noting that all the heterostructures exhibited displacement values on par with that of (if not slightly better than) a reference PbZr_{0.52}Ti_{0.48}O₃ heterostructure (corresponding to the MPB) synthesized using identical growth parameters to the $PbHf_{1-x}Ti_xO_3$ heterostructures on a $SrRuO_3/SrTiO_3(001)$ substrate (Figure S19a-f); further pointing to the similarity between the two material systems as thin-film heterostructures and making $PbHf_{1-x}Ti_xO_{3}$, a promising material system for future studies concerning piezoelectric applications. As discussed earlier, despite the chemical similarity of zirconium and hafnium, zirconium is expected to be relatively more reactive with silicon than hafnium. Thus, having demonstrated the utility of the $PbHf_{1-x}Ti_xO_3$ system as a potential alternative to the $PbZr_{1-x}Ti_xO_3$ system, we also touch on potential material-design concepts based on these materials. As a single layer, $PbZr_{1-x-y}Hf_yTi_xO_3$ on silicon could be used instead of undoped $PbZr_{1-x}Ti_xO_3$ facilitating the scavenging of interfacial SiO₂ by reaction with zirconium while retaining the polar functionalities in the heterostructure with the presence of unreacted hafnium in $PbHf_{1-x}Ti_xO_3$.¹¹ Another example can be compositionally graded¹²⁻¹⁴ PbZr_{1-x-y}Hf_yTi_xO₃ heterostructures for integration on silicon exhibiting piezoelectric loops with large voltage offsets which can exhibit a large piezoelectric response with a low dielectric constant near zero bias for MEMS applications.

CONCLUSIONS

The $PbZr_{1-x}Ti_xO_3$ system has been studied extensively because of its exceptional dielectric, piezoelectric, and ferroelectric properties. An isotypic material system which is relatively unexplored is the PbHf_{1-x}Ti_xO₃ system, which offers an added benefit that it can be (relatively) more compatible with integration on silicon wafers and existing CMOS fabrication processes. Here, we synthesized 50-200 nm-thick $PbHf_{1-x}Ti_xO_3$ (x = 0, 0.25, 0.4, 0.45, 0.5, 0.55, 0.75, and 1) thin-film heterostructures on SrRuO₃/SrTiO₃(001) substrates. In turn, the structural, ferroelectric, dielectric, and electromechanical properties of the PbHf_{1-x}Ti_xO₃ thin films across the phase diagram were explored. Similar to the $PbZr_{1-x}Ti_xO_3$ system, a composition-driven structural phase transition from rhombohedral to tetragonal phases was observed with a mixedphase [rhombohedral (R3c) + monoclinic (Cm) + tetragonal (P4mm)] structure in the composition range x = 0.4-0.55. The ferroelectric properties across the phase diagram reflected the changing crystal structure in terms of polarization and

coercive-field values both of which were found to increase with increasing titanium content. Furthermore, ε_r was enhanced in the mixed-phase compositions near the MPB with the maximum value being observed for PbHf_{0.6}Ti_{0.4}O₃ heterostructures. Additional electric-field-dependent dielectric measurements, however, revealed that the PbHf_{0.5}Ti_{0.5}O₃ heterostructures are likely closer to the true MPB based on its highest intrinsic contribution to the dielectric response (similar to the observations in bulk $PbHf_{1-x}Ti_xO_3$ ceramics). The presence of ferroelectric domain walls which are relatively more mobile in PbHf_{0.6}Ti_{0.4}O₃ heterostructures (as compared to that in $PbHf_{0.5}Ti_{0.5}O_3$) is expected to be the primary source of an enhanced extrinsic contribution leading to an enhanced overall dielectric response. Furthermore, displacement-voltage hysteresis loops and surface displacement-electric field loops were obtained using switching spectroscopy in PFM and laser vibrometry, respectively, for all the synthesized heterostructures. While the substrate-induced quenching of domain wall motion in thin films limited the extrinsic contribution to the piezoelectric response for the mixed-phase compositions, the measured displacement values were found to be at par with that of a reference PbZr_{0.52}Ti_{0.48}O₃ composition, further confirming the similarity between $PbHf_{1-x}Ti_xO_3$ and $PbZr_{1-r}Ti_rO_3$ systems in terms of functionalities.

ASSOCIATED CONTENT

③ Supporting Information

The Supporting Information is available free of charge at https://pubs.acs.org/doi/10.1021/acs.chemmater.2c02295.

Reactivity of PbHfO₃ and PbZrO₃ with SiO₂; X-ray diffraction studies - lattice parameters for PbHfO₃; Xray diffraction studies – lattice parameters for PbTiO₃; crystal structure of $PbHf_{0.75}Ti_{0.25}O_3$ and $PbHf_{0.25}Ti_{0.75}O_3$; crystal structure of $PbHf_{1-x}Ti_xO_3$ for x = 0.4, 0.45, 0.5, and 0.55; X-ray diffraction studies – lattice parameters for $PbHf_{1-x}Ti_xO_3$ (0.25 < x < 0.75); epitaxy of (00*l*)-oriented PbHf_{1-x}Ti_xO₃ (x = 0.25, 0.4,0.45, 0.5, 0.55, and 0.25) films; temperature-dependent dielectric constant measurements; DC electric fielddependent dielectric constant measurements; DC/AC electric field-dependent dielectric constant measurements; PFM electromechanical studies; laser vibrometer-based electromechanical surface displacement measurements; first-principles density functional perturbation theory calculations; and characterization of reference PbZr_{0.52}Ti_{0.48}O₃ thin-film heterostructures (PDF)

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Author Contributions

M.Ac. and L.W.M. conceived of the work. M.Ac., H.L., D.L. M.R., G.V., M.As. K.P., and L.W.M. developed and implemented the methodology and experiments. M.Ac., H.L., D.L. M.R., B.H., G.V., M.As. K.P., and L.W.M. completed the formal analyses of the data. M.Ac. and L.W.M. wrote the original draft. M.Ac., H.L., B.H., G.V., M.As., K.P., and L.W.M. reviewed and edited the final manuscript. M.As., K.P., and L.W.M. provided funding and supervision for the work.

Notes

The authors declare no competing financial interest.

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