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## ORIGINAL RESEARCH ARTICLE

# Influence of agricultural managed aquifer recharge on nitrate transport: The role of soil texture and flooding frequency

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## Abstract

Agricultural managed aquifer recharge (Ag-MAR) is a concept in which farmland is flooded during the winter using excess surface water to recharge the underlying groundwater. In this study, we show how different recharge practices affect  $\text{NO}_3^-$  leaching and mineralization–denitrification processes in different soil systems. Two contrasting soil textures (sand and fine sandy loam) from the Central Valley, California, were repeatedly flooded with 15 cm of water at varying time intervals in field and soil column experiments. Nitrogen species ( $\text{NO}_3^-$ ,  $\text{NH}_4^+$ , total N), total C, dissolved  $\text{O}_2$ , and moisture content were measured throughout the experiments. Results show that when flooding occurs at longer intervals (every 1–2 wk), N mineralization increases, leading to an increase of mobile  $\text{NO}_3^-$  in the upper root zone and leaching of significant quantities of  $\text{NO}_3^-$  from both soil textures ( $137.3 \pm 6.6\%$  [sand] and  $145.7 \pm 5.8\%$  [fine sandy loam] of initial residual soil  $\text{NO}_3^-$ ) during subsequent flooding events. Laboratory mineralization incubations show that long flooding intervals promote mineralization and production of excess  $\text{NO}_3^-$  at rates of  $0.11\text{--}3.93$  mg N  $\text{kg}^{-1}$   $\text{wk}^{-1}$  (sand) and  $0.08\text{--}3.41$  mg N  $\text{kg}^{-1}$   $\text{wk}^{-1}$  (fine sandy loam). Decreasing the flooding frequency to 72 h reduces potential mineralization, decreasing the amount of  $\text{NO}_3^-$  leached during flooding events ( $31.7 \pm 3.8\%$  [sand] and  $64.7 \pm 10.4\%$  [fine sandy loam] of initial residual soil  $\text{NO}_3^-$ ). The results indicate that implementing recharge as repeated events over a long (multiple-week) time horizon might increase the total amount of  $\text{NO}_3^-$  potentially available for leaching to groundwater.

## 1 | INTRODUCTION

Dependence on groundwater for irrigation and consumptive use has resulted in the widespread depletion of groundwater aquifers across the world (Dalin et al., 2019; Wada et al.,

2014). In most of the semiarid U.S. Southwest, groundwater is increasingly being regulated in efforts to sustainably manage this limited resource. Sustainably managing groundwater in California has increased the interest in and use of managed aquifer recharge (MAR) technologies that purposefully recharge water to aquifers for subsequent recovery or environmental benefit (Dillon et al., 2009).

Agricultural managed aquifer recharge (Ag-MAR) is a promising form of managed aquifer recharge, where farmland is flooded during the winter using excess surface water in

**Abbreviations:** Ag-MAR, agricultural managed aquifer recharge; HF, high-frequency flooding; LF, low-frequency flooding; MAR, managed aquifer recharge; TC, total carbon; TN, total nitrogen; VWC, volumetric soil water content; WA, water application.

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order to recharge the underlying groundwater aquifer (Kocis & Dahlke, 2017). Over 3.6 million ha of suitable farmland that is connected to water conveyance systems has been identified for Ag-MAR throughout the Central Valley of California (O'Geen et al., 2015). Some of these lands support infiltration rates in excess of  $50 \text{ cm d}^{-1}$ , raising questions on how Ag-MAR could be implemented on suitable but fertilized agricultural fields such that  $\text{NO}_3^-$  leaching from the root zone to the groundwater is minimized.

The risk of  $\text{NO}_3^-$  leaching to the underlying groundwater stems from N accumulation in the soil profile as a result of repeated fertilizer applications and incomplete N uptake by crops (Di & Cameron, 2002b). Overapplication of N fertilizer has been reported as a major contributing factor to the accumulation of  $\text{NO}_3^-$  in the soil profile (0–400 cm) as shown by Zhou et al. (2016), who observed a residual  $\text{NO}_3^-$  load of 453–2,155  $\text{kg N ha}^{-1}$  in the North China Plain and Loess Plateau, China. Harter et al. (2005) observed the accumulation of 218–477  $\text{kg N ha}^{-1}$  in the deep vadose zone (1,600-cm depth) under a citrus (*Citrus L. spp.*) orchard in California. These residual  $\text{NO}_3^-$  loads in the root zone or deep vadose zone are at risk of being leached when large amounts of water (e.g.  $>10\text{--}15 \text{ cm d}^{-1}$ ) are applied for Ag-MAR, which could potentially lead to water quality degradation of underlying groundwater resources (Botros et al., 2012; Onsoy et al., 2005).

Research regarding  $\text{NO}_3^-$  transport in the vadose zone has been conducted in agricultural settings under various irrigation practices, such as drip (Baram et al., 2016; Lv et al., 2019; Phogat et al., 2014), sprinkler (Baram et al., 2016; Gheysari et al., 2009), and flood irrigation (Di & Cameron, 2002a; Wang et al., 2010). These studies have concluded that N supply from the vadose zone to the groundwater is transport limited rather than source limited, with the most efficient irrigation systems (drip and sprinkler) leaching lower amounts of  $\text{NO}_3^-$  from the soil profile. Drip irrigation paired with optimized N fertilization has been shown to reduce  $\text{NO}_3^-$  leaching by 90% compared with conventional flood irrigation practices (Di & Cameron, 2002; Lv et al., 2019; Wang et al., 2010). Flood irrigation is an irrigation method similar to Ag-MAR, often with a smaller ponding depth and shorter application duration than is applied during Ag-MAR. As such, these studies provide insights into how larger water applications and ponded conditions might influence  $\text{NO}_3^-$  leaching. Wang et al. (2010) flooded a winter wheat (*Triticum aestivum L.*)–summer maize (*Zea mays L.*) cropping systems on a silt loam soil in the North China Plain every 72 h with two 25-cm water applications and found that  $62 \pm 7\%$  of the  $\text{NO}_3^-$  within the upper 200 cm of the soil profile was leached. Lv et al. (2019) reported that flood irrigation of tomato (*Solanum lycopersicum L.*) fields in a silt loam at an agricultural experimental station in Tianjin City, China, showed low N use efficiency resulting in 50% of total N input being leached ( $300 \text{ kg N ha}^{-1}$

### Core Ideas

- Short-lived Ag-MAR flooding events cause  $\text{NO}_3^-$  leaching and organic N mineralization.
- Soil texture affects the timing of  $\text{NO}_3^-$  leaching under Ag-MAR.
- Soil texture affects the conditions for biogeochemical processes under Ag-MAR.
- Reducing time between flooding events for Ag-MAR reduces  $\text{NO}_3^-$  produced by mineralization.

per season). Hence, in many irrigated agricultural regions, precision irrigation and/or deficit irrigation are increasingly used to minimize  $\text{NO}_3^-$  leaching and to trap residual  $\text{NO}_3^-$  in or below the root zone (Baram et al., 2016; Gheysari et al., 2009; Waddell et al., 2000). Therefore, AgMAR represents a significant hydrologic regime shift from current growing season irrigation practices in semiarid climates.

To date, not many studies exist that have investigated the impact of Ag-MAR on  $\text{NO}_3^-$  leaching and N transformation processes in the root zone. Among the few studies that do exist, Bachand et al. (2014) concluded that although  $\text{NO}_3^-$  will initially be leached to the groundwater under Ag-MAR, there is the potential to improve groundwater quality over time through subsequent flooding applications with low-N water. Waterhouse et al. (2020) assessed the root zone residual  $\text{NO}_3^-$  load of farm fields representing different soil textures, crop types, and management practices to quantify the risk of groundwater contamination under Ag-MAR, concluding that wine grape (*Vitis vinifera L.*) vineyards on permeable soils had the lowest observed  $\text{NO}_3^-$  leaching risk. They noted that further research is needed regarding the relationship between  $\text{NO}_3^-$  leaching, Ag-MAR practices (e.g., frequency and duration of floodwater applications), and soil texture.

Soil texture has been shown to significantly affect both the hydrologic flow properties and conditions favorable to biogeochemical transformations. Soil texture affects infiltration rates and residence time of applied water and thus  $\text{NO}_3^-$  mobilization, potential sorption of N species,  $\text{O}_2$  content, oxidation–reduction potential, and microbial activity, all factors that may affect biogeochemical processes (Aronsson & Bergström, 2001; Bergström & Johansson, 1991; Kaiser et al., 1992; Sogbedji et al., 2000). Gaines and Gaines (1994) examined the impact of soil texture and organic matter content on  $\text{NO}_3^-$  leaching potential and found that increased fractions of silt, clay, and organic matter in a soil decrease the amount of  $\text{NO}_3^-$  leaching observed. Mineralization of organic N, under favorable temperature ( $>25^\circ\text{C}$ ) and moisture conditions ( $\sim 55\%$  water holding capacity), increases inorganic N concentrations within the soil profile, which are then

susceptible to leaching (Cabrera, 1993; Cambardella et al., 1999; Linn & Doran, 1984). Conversely, the transition from an oxic to an anoxic soil environment affects the potential for denitrification, which can decrease the  $\text{NO}_3^-$  leaching potential of a soil due to the transformation of  $\text{NO}_3^-$  to  $\text{N}_2$  gas.

Nitrate leaching and N transformation processes have been studied in more detail in traditional MAR systems such as storm water or treated wastewater infiltration basins (Abiye et al., 2009; Ben Moshe et al., 2020; Goren et al., 2014; Gorski et al., 2019; Schmidt et al., 2011). Depending on the infiltration rate of the native soil, Schmidt et al. (2011) observed a 30–60% removal of  $\text{NO}_3^-$  in agricultural storm runoff recharged in a 3-ha infiltration basin. Soil aquifer treatment (SAT) systems, a special form of MAR aimed at infiltrating wastewater or reclaimed water, can result in dramatic water quality improvements by forcing soil systems towards favorable (e.g., anoxic) biogeochemical conditions. The physical and biochemical processes that occur during passage of the wastewater through the biologically active infiltration interface in the top meter of the infiltration basin sediments are key to N removal due to denitrification (Miller et al., 2006). Soil aquifer treatment research has further highlighted the utility of controlled soil column experiments in examining spatially and temporally complex soil conditions and their impact on biogeochemical transformations (Ben Moshe et al., 2020; Goren et al., 2014; Quanrud et al., 1996). However, traditional MAR and SAT systems are often focused on remediating  $\text{NO}_3^-$  loads or other contaminants from the infiltrating recharge water, as opposed to Ag-MAR where the  $\text{NO}_3^-$  leaching potential stems from the residual  $\text{NO}_3^-$  stored in the soil matrix or vadose zone.

Although traditional MAR systems have similar end goals to Ag-MAR, major hydrologic differences exist between these systems. In contrast with MAR infiltration basins, which often maintain a constant head of several meters for several weeks, creating a thick saturated layer beneath the basin surface (Gorski et al., 2019; Schmidt et al., 2011), previous Ag-MAR projects often had smaller heads (10–50 cm). In addition, on agricultural fields planted with perennial crops, the water was applied in short-lived pulses on high-infiltration-capacity soils to avoid waterlogged conditions that could potentially harm the crops. These pulsed water applications create more distinct wetting–drying cycles and dynamic changes in environmental conditions and biogeochemical processes than are found in continuously flooded systems (Dahlke et al., 2018). For these highly dynamic systems, not much is known about the effect that soil texture or Ag-MAR flooding frequency (how often water is applied for recharge) have on  $\text{NO}_3^-$  leaching potential.

The aim of this research is to quantify  $\text{NO}_3^-$  leaching and N transformation processes in the soil and shallow vadose zone of agricultural soils subject to different Ag-MAR practices. Our study specifically investigates the following questions:

1. What effect does soil texture have on  $\text{NO}_3^-$  leaching and N transformation processes during Ag-MAR?
2. What effect does varying flooding frequency have on  $\text{NO}_3^-$  leaching and N transformation processes during Ag-MAR?

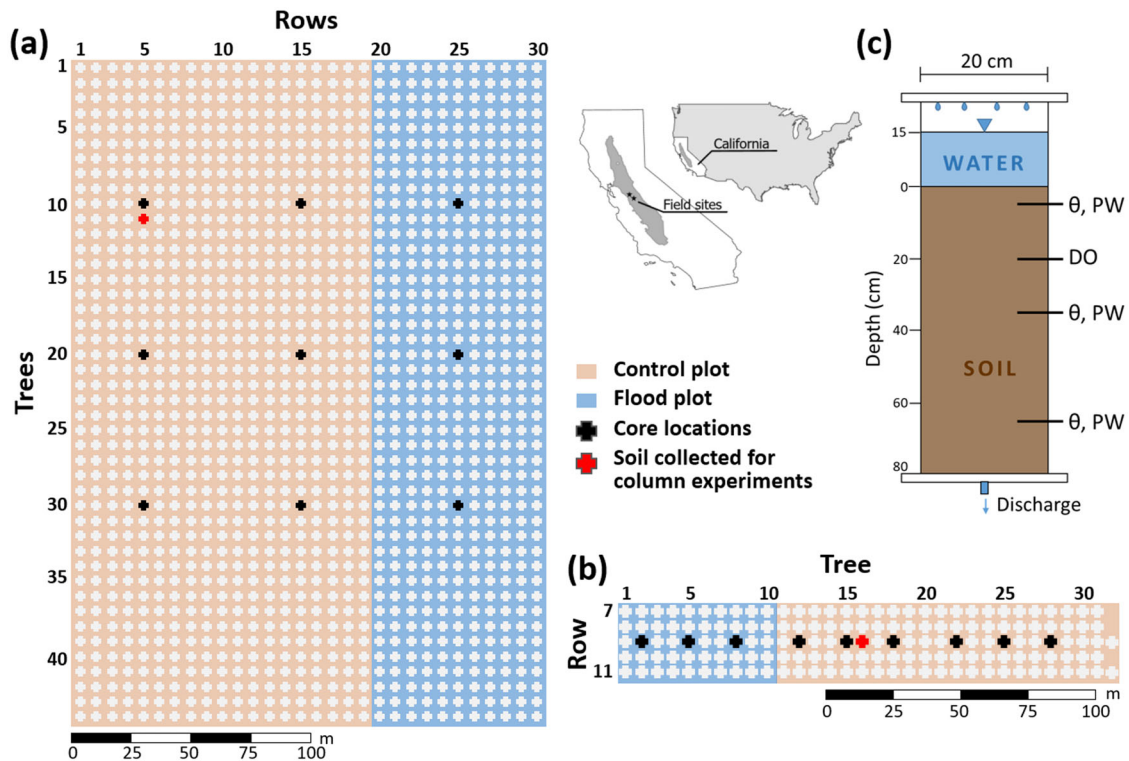
We hypothesize that soil texture and flooding frequency are controlling factors on the amount of residual soil  $\text{NO}_3^-$  that is being leached from the root zone, since both parameters influence the wetting and drainage,  $\text{O}_2$ , and redox regime of the soil and with that the environmental conditions favoring specific N transformation processes such as denitrification or mineralization. Soil texture is hypothesized to be particularly influential on the amount of  $\text{NO}_3^-$  leached from the profile, with coarser textures allowing more leaching than finer textured soils. Flooding frequency is hypothesized to affect mineralization and denitrification potential in both soils, with higher flooding frequencies promoting environmental conditions more favorable for denitrification and less for mineralization. To evaluate the posed questions and hypotheses, we used data from field experiments at two almond [*Prunus dulcis* (Mill.) D.A. Webb] orchards in the Central Valley of California and laboratory soil column experiments, in which we tested the effects of flooding frequency and soil texture in a controlled environment. In addition, we completed incubation experiments to gain a mechanistic understanding of N transformation processes and rates for these soil textures.

## 2 | MATERIALS AND METHODS

### 2.1 | Field experiments

#### 2.1.1 | Study sites

Two almond orchards were investigated during the winters of 2015–2016 and 2016–2017, both located in the Central Valley of California. The first site is located south of Delhi, CA (37°24'12" N, 120°47'19" W), whereas the second is located southwest of Modesto, CA (37°36'26" N, 121° 4'21" W) (Figure 1). The soil at Delhi is a sand (Delhi sand series; mixed, thermic, Typic Xeropsamments), a rapidly draining soil with high infiltration rates (average profile saturated hydraulic conductivity [ $K_{\text{sat}}$ ]  $\sim 30 \text{ cm h}^{-1}$ ). The presence of a hardpan layer around 100-cm depth was previously observed at Delhi; however, deep ripping of the hardpan occurred prior to the original planting of the orchard in the early 2000s. The soil at Modesto is a fine sandy loam, a moderately draining soil derived from granitic alluvium (Dinuba series; coarse-loamy, mixed, active, thermic Typic Haploxeralfs; Soil Series USDA). Hereafter, the two field sites will be referenced to as sand (Delhi) and fine sandy loam (Modesto). The two sites are rated as “excellent” (sand) and “moderately good” (fine sandy



**FIGURE 1** Study locations and experimental setup. (a) Fine sandy loam experimental field design; (b) sand experimental field design; and (c) experimental laboratory column design, where  $\theta$  is volumetric water content sensor, PW is pore water sampler, and DO is dissolved  $O_2$  sensor

loam) by the Soil Agricultural Groundwater Banking Index (SAGBI; O'Geen et al., 2015), a recently proposed measure of Ag-MAR soil suitability. The mean annual precipitation at both sites varied between 17.8 and 36.1 cm from 2015 to 2018: 2015 was a critical dry year, and 2017 was the second wettest year on the 100-yr climate record in California. The majority of precipitation at both sites occurs during the winter months (November–April), and the mean annual temperature is 17.25 °C (January 2015–2018) (Soil Series USDA, California Irrigation Management Information System [CIMIS] Station 206).

### 2.1.2 | Field instrumentation and monitoring

Two treatments were tested at each orchard: a flood treatment (i.e., Ag-MAR) in which 61 cm of water was applied during December–January (2015–2016 and 2016–2017) in three or four separate flooding events, with 15.24–25.4 cm of applied water during each event (supplemental material; Table 1), and the grower standard irrigation practices, defined as the control. The average  $NO_3^-$ -N concentration of the applied water was 9.63 mg  $L^{-1}$  for the sand field site, and 1.45 mg  $L^{-1}$  for the fine sandy loam field site. The variation in  $NO_3^-$  concentration of the applied water between sites is reflective of the water source that was used for flooding: the fine sandy loam site used local surface water, and the sand site used pumped

groundwater in lieu of available surface water resources. Soil cores (5-cm diam.) were collected using a direct push drill method (Geoprobe Systems) before and after winter flooding events, to a depth of 300–400 cm.

Cores were analyzed for soil texture,  $NO_3^-$ -N,  $NH_4^+$ -N, total C (TC), and total N (TN). Soil samples were prepared for N analysis using 0.5 M  $K_2SO_4$  extractions, whereby 15 g of soil (corrected for soil water content) was extracted with 36 ml  $K_2SO_4$ , with extracted supernatant representing soil extractable N. All  $NO_3^-$ -N and  $NH_4^+$ -N samples in both field and laboratory experiments were analyzed using the vanadium (III) reduction (Doane & Horwath, 2003) and the Berthelot reaction (Forster, 1995; Verdouw et al., 1978), respectively. The TC and TN soil samples were ball milled and analyzed using the Costech ECS 4010. Soil samples taken before and after recharge events were analyzed in triplicate samples for  $NO_3^-$ -N,  $NH_4^+$ -N, and TN, in 10-cm intervals, which allowed constraining both the organic N and inorganic N pools within the soil matrix.

## 2.2 | Laboratory experiments

### 2.2.1 | Soil column experiments

Laboratory soil column experiments were designed to corroborate data collected from field-scale experiments and to

**TABLE 1** Sand and fine sandy loam field core  $\text{NO}_3^-$ -N loads. The root zone (RZ) is defined as the first 100 cm of the core, whereas “full” denotes the entire 400-cm profile or core length

Parameter	$\text{NO}_3^-$ -N load	$\text{NO}_3^-$ -N load	Change	$\text{NO}_3^-$ -N load	$\text{NO}_3^-$ -N load	Change
	before flood (RZ)	after flood (RZ)		before flood (full profile)	after flood (full profile)	
	kg ha <sup>-1</sup>		%	kg ha <sup>-1</sup>		%
<b>Sand (2015–2016)</b>						
Flood avg. ( <i>n</i> = 3)	44.12 ± 28.55	5.41 ± 0.65	-82 ± 15	286.03 ± 257.49	115.36 ± 54.39	-23 ± 85
Control avg. ( <i>n</i> = 6)	182.39 ± 186.79	9.72 ± 3.97	-90 ± 9	668.84 ± 275.92	644.12 ± 252.80	1 ± 40
<b>Sand (2016–2017)</b>						
Flood avg. ( <i>n</i> = 3)	19.78 ± 5.01 <sup>a</sup>	15.98 ± 6.71	-11 ± 16	124.74 ± 104.03	88.62 ± 31.25	6 ± 83
Control avg. ( <i>n</i> = 2)	52.81 ± 4.01 <sup>ab</sup>	9.25 ± 2.16 <sup>b</sup>	-83 ± 3	1165.08 ± 781.98	354.45 ± 111.96	-65 ± 14
<b>Fine sandy loam (2015–2016)</b>						
Flood avg. ( <i>n</i> = 3)	13.98 ± 4.59	22.99 ± 20.04	56 ± 142	59.70 ± 36.88	114.98 ± 69.64	107 ± 113
Control avg. ( <i>n</i> = 6)	12.02 ± 5.30 <sup>b</sup>	32.39 ± 11.12 <sup>b</sup>	209 ± 149	122.03 ± 70.66	118.11 ± 70.63	20 ± 79
<b>Fine sandy loam (2016–2017)</b>						
Flood avg. ( <i>n</i> = 2)	53.20 ± 49.06	65.24 ± 0.06	113 ± 197	233.70 ± 288.74	66.61 ± 1.99	23 ± 152
Control avg. ( <i>n</i> = 2)	64.35 ± 8.96	49.96 ± 14.11	-23 ± 11	123.6 ± 5.54	316.59 ± 391.19	164 ± 329

<sup>a</sup>Significance of a two-sample *t* test comparing initial  $\text{NO}_3^-$ -N load between flood and control plots.

<sup>b</sup>Significant difference between the before and after  $\text{NO}_3^-$ -N load within a plot.

quantify  $\text{NO}_3^-$  leaching and major N transformation processes in the root zone induced by the application of large water amounts typical for Ag-MAR practices. Large soil columns (80 cm tall, 20 cm in diameter) were built from polyvinyl chloride (PVC) pipe (Figure 1). This column size was chosen to minimize sidewall flow (1:4 width/depth ratio) and to encompass some of the heterogeneity of the  $\text{NO}_3^-$  distribution observed within the field cores. The soils for the laboratory experiments were excavated in 10-cm intervals from the control treatment at both field sites in order to represent pre-flooding conditions. The columns were packed with the soil collected from the field sites in 10-cm intervals, to a depth of 80 cm and a measured average bulk density of 1.58 g cm<sup>-3</sup> (sand) and 1.65 g cm<sup>-3</sup> (fine sandy loam). Prior to and after completion of the flooding experiments, soil samples were taken at 10-cm intervals to constrain both the organic N and inorganic N pools within the soil matrix. Soil samples were analyzed in triplicate samples for  $\text{NO}_3^-$ -N,  $\text{NH}_4^+$ -N, and TN using the standard protocols as detailed above.

Each soil column was equipped with three volumetric soil water content (VWC) sensors at 5-, 35-, and 65-cm depth (Acclima TDR-310S), a dissolved O<sub>2</sub> sensor at 20-cm depth (PreSens, Fibox 4), and three discrete pore water sampling ports at 5-, 35-, and 65-cm depth (Soil Moisture, Model 190D4). The VWC was measured continuously at 1-min intervals. Discharge from the soil column was continuously measured in 5-min intervals using a tipping bucket rain gauge (Acurite, Model 00899). A vacuum of 50.80–67.73 mbar (1.5–2 inches Hg) was applied to the bottom of the soil columns in order to represent the matric potential and prevent

the buildup of an artificial water table (Lewis & Sjöström, 2010). From the discharge, 50-ml water samples were collected at flow-dependent intervals ranging from 5 to 60 min and then analyzed for  $\text{NO}_3^-$ -N and  $\text{NH}_4^+$ -N.

Two flooding frequency treatments (low frequency [LF; flooding every 1–2 wk] and high frequency [HF; flooding every 72 h]) and two soil textures (sand [Delhi site] and fine sandy loam [Modesto site]) were tested with the soil column experiments for a total of four treatments. During each column experiment, three water applications (WAs), each of 15 cm, were made to each soil column (hereafter referred to as WA1, WA2, and WA3 respectively). Each 15 cm of water added represented 0.47 pore volumes of the 80-cm column for the sand, and 0.51 pore volumes for the fine sandy loam. The LF treatment was a true replicate of the water applications made at both field sites, consisting of three consecutive WAs in total with a 168-h (1-wk) break between WA1 and WA2, and a 336-h (2-wk) break between WA2 and WA3. In the HF treatment three WAs were made, each 72 h apart. An individual WA consisted of applying tap water (with nondetect concentrations of  $\text{NO}_3^-$ -N) equivalent to 15 cm of water depth over a period of 0.5 h onto the soil surface of the column using a perforated bucket to minimize erosion. Twenty-four hours before the start of the column experiments, the soil columns were brought up to the same VWC as was observed at each field site prior to the start of the Ag-MAR field experiments (sand: 0.1–0.15 cm<sup>3</sup> cm<sup>-3</sup>; fine sandy loam: 0.2–0.25 cm<sup>3</sup> cm<sup>-3</sup>), by applying a water application of ~8 cm such that soil volumetric water contents increased to between 0.1 and 0.2 cm<sup>3</sup> cm<sup>-3</sup>.

## 2.2.2 | Soil incubations and $\text{NO}_3^-$ -N mass balance calculations

Mineralization and denitrification incubations were performed on field soils in order to constrain transformation rates under ideal conditions. Net mineralization potential, the rate at which a soil converts organic N into inorganic N, was evaluated using methods outlined in Wade et al. (2018), where 10 g of soil from each 10-cm soil layer was air dried and sieved through a 2-mm sieve. Initial inorganic N levels were measured in each soil layer according to the methods described in Section 2.1.2 before samples were brought up to 55% water holding capacity, in order to maximize aerobic microbial activity (Linn & Doran, 1984), and incubated for 2 wk. Inorganic N levels were remeasured and mineralization rates were calculated as the difference in N concentrations between the initial and ending time of the experiment.

Denitrification incubations were measured according to the acetylene-inhibition method described in Smith et al. (1978), and gas samples were collected after 30 min, 90 min, and 1 d of incubation time. Samples were analyzed by gas chromatography for  $\text{N}_2\text{O}$  (Model GC-2014; Shimadzu Scientific Instruments).

In order to evaluate  $\text{NO}_3^-$  leaching potential (i.e., the potential for soil residual  $\text{NO}_3^-$  to be transported out of the soil profile), a  $\text{NO}_3^-$  mass balance for each soil column was calculated. Total mass of specific N species ( $\text{NO}_3^-$ -N,  $\text{NH}_4^+$ -N) in the soil (solid samples) was calculated as

$$M_{\text{soil}} = \sum_{i=1}^n C_n V_n \rho_n \quad (1)$$

where  $M_{\text{soil}}$  is the mass of the N species within the soil column ( $\mu\text{g}$ ),  $n$  is the soil layer of the column (10-cm intervals to a depth of 80 cm),  $C$  is the concentration of the N species in the soil ( $\mu\text{g g}^{-1}$  soil),  $V$  is the volume of the soil layer ( $\text{cm}^3$ ) and  $\rho$  is the density of the soil ( $\text{g cm}^{-3}$ ). Mass loads of  $\text{NO}_3^-$  leaving the column as leachate (liquid samples) were calculated by

$$M_{\text{eff}} = \sum_{i=1}^n q_t C_t \Delta t \quad (2)$$

where  $M_{\text{eff}}$  is the mass of  $\text{NO}_3^-$ -N leaving the column during a flooding event,  $C_t$  is the concentration in an effluent sample ( $\mu\text{g N ml}^{-1}$ ),  $q_t$  is the flow rate out of the column ( $\text{ml min}^{-1}$ ) and  $\Delta t$  is the time step associated with  $C_t$  and  $q_t$ . The mass balance for  $\text{NO}_3^-$  within the soil column is then represented by the typical mass balance equation:

$$I - O = \Delta S \quad (3)$$

where  $I$  represents the biogeochemical creation or addition of  $\text{NO}_3^-$  to the system,  $O$  represents the biogeochemical con-

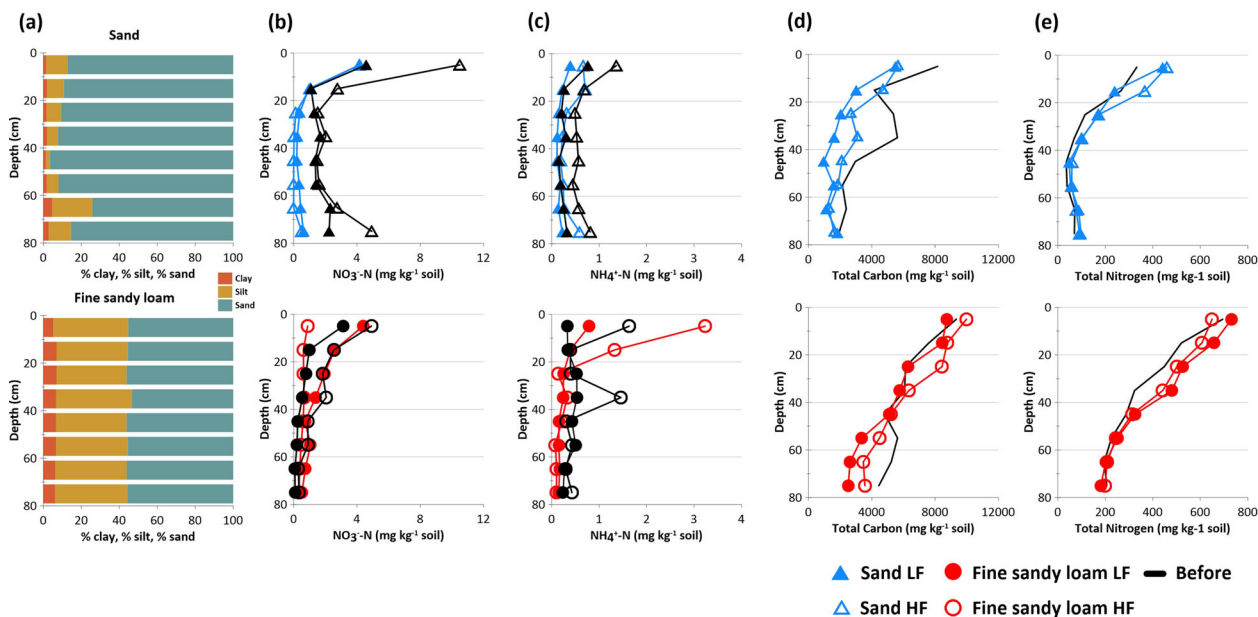
sumption or leaching of  $\text{NO}_3^-$  from the system, and  $\Delta S$  represents the change of storage of  $\text{NO}_3^-$  mass within the system. When considering the  $\text{NO}_3^-$  mass balance, the only input considered in this mass balance is the creation of  $\text{NO}_3^-$  through mineralization and subsequent nitrification (conversion of organic N to  $\text{NH}_4^+$ , and conversion of  $\text{NH}_4^+$  to  $\text{NO}_3^-$  measured in the soil profile). The water used for flooding contained negligible amounts of N species ( $<0.05 \text{ mg L}^{-1} \text{ NO}_3^-$ -N,  $\text{NH}_4^+$ -N). Outputs considered can include N transformations such as immobilization and denitrification, or physical processes such as  $\text{NO}_3^-$  leaching measured in the effluent (i.e.,  $M_{\text{eff}}$ ). Change in storage is represented by the difference between the before and after N profiles in the soil column experiments.

## 3 | RESULTS

### 3.1 | Field trials

The two almond orchards were flooded with 61–66.4 cm (about 2 ft) of water during the winters (December–January) of 2015–2016 and 2016–2017 (Supplemental Table S2). Soil moisture in the flood treatment for the sand reached saturation ( $0.4 \text{ cm}^3 \text{ cm}^{-3}$ ) and returned back to pre-flooding soil water content ( $0.1$ – $0.15 \text{ cm}^3 \text{ cm}^{-3}$ ) within 12 h after Ag-MAR water application. Infiltration rates for the fine sandy loam were less rapid than for the sand, and an estimated 81–96% of the applied water for Ag-MAR left the root zone, depending on the year (Supplemental Table S3). Moisture sensors showed that flooding events on the fine sandy loam took between 48 and 72 h to return from saturation ( $0.35$ – $0.4 \text{ cm}^3 \text{ cm}^{-3}$ ) to pre-flooding soil water content ( $0.15$ – $0.2 \text{ cm}^3 \text{ cm}^{-3}$ ).

The data from the field experiments show large amounts of variance in  $\text{NO}_3^-$ , across both treatments and year. The  $\text{NO}_3^-$ -N load within the 400-cm soil cores taken from the sand site before the flooding events ranged between 68.0 and 570.1  $\text{kg ha}^{-1}$  in the flood treatment and between 446.9 and 1,501.3  $\text{kg ha}^{-1}$  in the control (plots only receiving winter precipitation) in 2015–2016. In 2016–2017,  $\text{NO}_3^-$ -N load ranged between 60.2 and 244.7  $\text{kg ha}^{-1}$  in the flood treatment and between 612.1 and 1,718.0  $\text{kg ha}^{-1}$  in the control (Table 1). Total  $\text{NO}_3^-$ -N loads in the 400-cm soil cores taken from the flood-irrigated fine sandy loam before Ag-MAR flooding were lower than those from the sand, between 26.0 and 99.1  $\text{kg ha}^{-1}$  in the Ag-MAR treatment and 21.3 and 201.6  $\text{kg ha}^{-1}$  in the control in 2015–2016. In 2016–2017, the observed range was between 29.5 and 437.9  $\text{kg ha}^{-1}$  in the Ag-MAR treatment and between 119.7 and 127.5  $\text{kg ha}^{-1}$  in the control (Table 1). Although the differences in the field data are mostly non-significant, there are general directional trends that can be identified.



**FIGURE 2** Initial characterization of field soils with depth for (a) texture, (b)  $\text{NO}_3^-$ -N, (c)  $\text{NH}_4^+$ -N, (d) total C (TC), and (e) total N (TN). LF, low frequency treatment (1–2 wk), HF, high frequency treatment (72 h)

The two sites exhibited opposing trends in the  $\text{NO}_3^-$  profiles resulting from the Ag-MAR flooding events in the 2015–2016 field experiments. The sand shows a general decrease in  $\text{NO}_3^-$ -N load in the soil profile after Ag-MAR flooding, whereas the fine sandy loam shows a general increase in  $\text{NO}_3^-$ -N load after flooding events. These trends are not as apparent in the 2016–2017 season, where the sand profile shows no strong directional shift following Ag-MAR flooding events, and the fine sandy loam shows only a slight increase in  $\text{NO}_3^-$ -N load after flooding (Table 1). The high variance of  $\text{NO}_3^-$ -N measured across the field sites results in a lack of significant conclusions that can be made regarding  $\text{NO}_3^-$ -N leaching due to Ag-MAR flooding events from the field data. Additionally, in the case of the fine sandy loam, where there is a net increase in  $\text{NO}_3^-$  between the before and after residual soil profile, an estimation of  $\text{NO}_3^-$  leached during Ag-MAR is not possible, highlighting the importance of controlled, high-resolution laboratory experiments.

## 3.2 | Soil column experiments

### 3.2.1 | Soil $\text{NO}_3^-$ -N mass balance and transport

The initial soil  $\text{NO}_3^-$ -N and  $\text{NH}_4^+$ -N concentrations for the sand LF column ranged from 1.09 to 4.58  $\text{mg kg}^{-1}$  for  $\text{NO}_3^-$ -N, and 0.15 to 0.76  $\text{mg kg}^{-1}$   $\text{NH}_4^+$ -N (Figure 2). The highest concentrations were located in the top 10 cm, whereas the lowest were found in the 30-to-50-cm range. The soil for the fine sandy loam LF column showed concentrations ranging

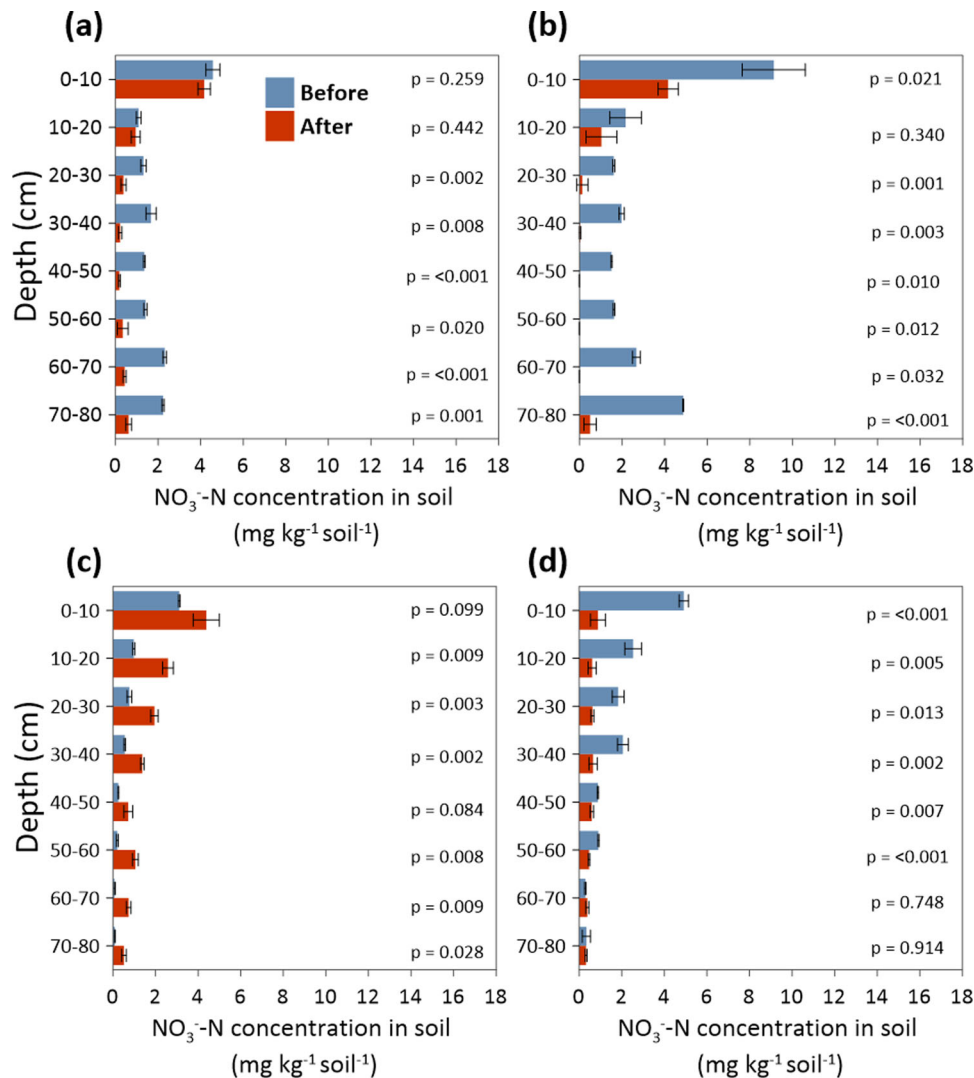
from 0.09 to 3.12  $\text{mg kg}^{-1}$   $\text{NO}_3^-$ -N, and 0.237 to 0.531  $\text{mg kg}^{-1}$   $\text{NH}_4^+$ -N. Nitrate concentrations for the fine sandy loam decreased with increasing depth, whereas ammonium concentrations were greatest at 20-to-60-cm depth (Figure 2).

The initial soil  $\text{NO}_3^-$ -N and  $\text{NH}_4^+$ -N concentrations for sand HF ranged from 1.50 to 9.13  $\text{mg kg}^{-1}$   $\text{NO}_3^-$ -N, and 0.49 to 1.36  $\text{mg kg}^{-1}$   $\text{NH}_4^+$ -N. The fine sandy loam HF concentrations ranged from 0.29 to 4.91  $\text{mg kg}^{-1}$   $\text{NO}_3^-$ -N, and 0.29 to 2.20  $\text{mg kg}^{-1}$   $\text{NH}_4^+$ -N (Figure 3). This is an average total increase of  $60 \pm 28\%$  for the sand and  $127 \pm 15.8\%$  for the fine sandy loam in initial  $\text{NO}_3^-$  mass compared with the LF initial conditions in the soil profile before flooding.

The  $\text{NO}_3^-$  breakthrough curves of the fine sandy loam LF and HF column experiments were similar in shape, but the peak concentration reached during WA1 in the HF experiment was twice the peak concentration during the LF experiment (Figure 4c, d). Interestingly, the fine sandy loam LF experiment showed a distinct secondary peak during WA1 and WA2 around 30 h after water application. During the fine sandy loam HF experiment, the late secondary peak seen in the LF experiment (Figure 4c, d) was missing. Effluent concentrations in the fine sandy loam HF were much lower in WA2 and WA3, never exceeding 1  $\text{mg L}^{-1}$   $\text{NO}_3^-$ -N, with long periods of zero  $\text{NO}_3^-$ -N concentration.

Both of the sand LF and HF experiments showed narrow peaks in the  $\text{NO}_3^-$  breakthrough curve in WA1 with peak  $\text{NO}_3^-$ -N concentrations in the effluent of 18.4 and 26.72  $\text{mg L}^{-1}$  during the sand LF and sand HF, respectively (Figure 4a, b). The sand HF did show the same shift in the  $\text{NO}_3^-$  peak as observed in sand LF WA2 and WA3, but the sand HF peaks





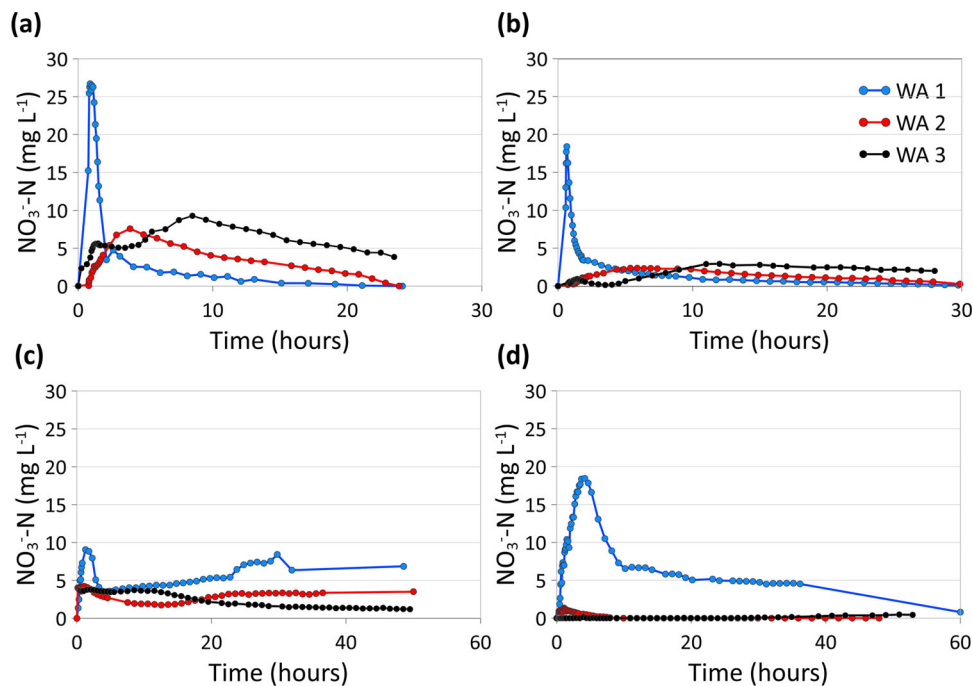
**FIGURE 3** Comparison of before (blue bars) and after (red bars)  $\text{NO}_3^-$ -N loads in the soil profiles of the soil column experiments, (a) sand low-frequency treatment (LF), (b) sand high-frequency treatment (HF), (c) fine sandy loam LF, and (d) fine sandy loam HF. Error bars represent one standard deviation of  $\text{NO}_3^-$ -N in soil profile.  $P$  values represent the statistical significance that the before and after values measured in the respective soil layer are not equal

were of lower magnitude (LF WA2 and WA3  $\text{NO}_3^-$ -N peaks were 7.58 and 9.27  $\text{mg L}^{-1}$  compared with HF WA2 and WA3  $\text{NO}_3^-$ -N peaks of 2.35 and 2.93  $\text{mg L}^{-1}$ ; Figure 4a, b).

The same directional trends in the residual soil  $\text{NO}_3^-$ -N of the 2015–2016 field experiments (Section 3.1) were observed in the corresponding LF soil column experiments (Figure 3). For the fine sandy loam, there was a greater amount of  $\text{NO}_3^-$ -N measured in the soil profile post-flooding than was initially present. In contrast, the sand profile showed a general decrease in  $\text{NO}_3^-$ -N measured in the soil profile post-flooding (Figure 3). However, effluent loads measured during the soil column experiments indicate that both sites were leaching discernible quantities of  $\text{NO}_3^-$  from the upper root zone (top 80 cm, Figure 4). Both soil textures leached over 100% of the initially present  $\text{NO}_3^-$ -N during the LF soil column experiments (Figure 5).

The effluent mass balance of the fine sandy loam LF experiment showed that  $145.7 \pm 5.8\%$  (47.1  $\text{mg NO}_3^-$ -N) of the initially measured  $\text{NO}_3^-$  (32.4  $\text{mg NO}_3^-$ -N) in the soil profile leached after three WAs (73.0, 45.2, and 27.5% leached during WA1, WA2, and WA3, respectively) (Figure 5a). The fine sandy loam HF effluent concentrations showed that the majority of the initially measured soil  $\text{NO}_3^-$  (73.5  $\text{mg NO}_3^-$ -N) leached during WA1 (62.8% of the initial  $\text{NO}_3^-$  load), with only 1.0 and 0.9% leached during WA2 and WA3 (Figure 5b) for a total of  $64.7 \pm 10.4\%$  (47.6  $\text{mg NO}_3^-$ -N) (Figure 5b).

For the sand LF column experiment the total amount of  $\text{NO}_3^-$  leached was slightly lower than the fine sandy loam LF, with  $137.3 \pm 6.6\%$  (112.4  $\text{mg NO}_3^-$ -N) of the initially measured  $\text{NO}_3^-$  (81.9  $\text{mg NO}_3^-$ -N) leached after three WAs (72.7, 25.5, and 39.2% leached during WA1, WA2, and WA3 respectively; Figure 5a). Overall,  $\text{NO}_3^-$  mass loss from the sand HF



**FIGURE 4** Observed  $\text{NO}_3^-$ -N concentrations in discharge through time, (a) sand low-frequency treatment (LF), (b) sand high-frequency treatment (HF), (c) fine sandy loam LF, and (d) fine sandy loam HF. WA, water application

column was lower than from sand LF. The percentage of  $\text{NO}_3^-$  leached from the initial sand HF profile (130.9 mg  $\text{NO}_3^-$ -N) during each WA was 24.5, 3.0, and 4.2% of the initial  $\text{NO}_3^-$  mass for a total of  $31.7 \pm 3.8\%$  (41.6 mg  $\text{NO}_3^-$ -N) (Figure 5b).

### 3.2.2 | Mineralization incubations and $\text{NO}_3^-$ mass balance

Both soil profiles showed similar mineralization rates, both in the maximum rate and in the depth distribution (Figure 6). The highest mineralization rates observed were  $3.93 \text{ mg N kg}^{-1} \text{ wk}^{-1}$  (sand) and  $3.41 \text{ mg N kg}^{-1} \text{ wk}^{-1}$  (fine sandy loam) in the top soil (0–10 cm), which decreased to  $0.11 \text{ mg N kg}^{-1} \text{ wk}^{-1}$  (sand) and  $0.08 \text{ mg N kg}^{-1} \text{ wk}^{-1}$  (fine sandy loam) at 50-to-70-cm depth. For the sand, the 50-to-70-cm depth showed indications of immobilization rather than mineralization, with a C/N ratio ranging from 53 to 61.

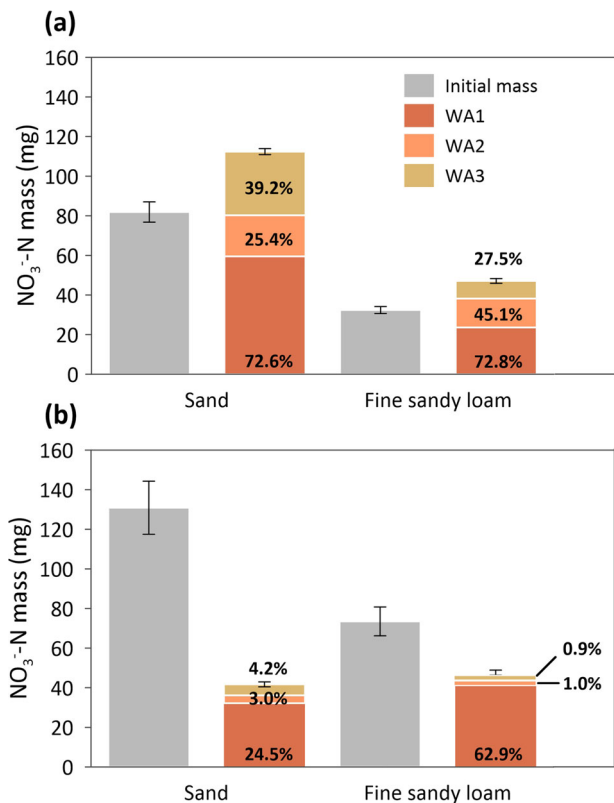
To account for the difference between the excess  $\text{NO}_3^-$  leached ( $137.3 \pm 6.6\%$  or 112.4 mg  $\text{NO}_3^-$ -N) during the sand LF column experiment and the change in residual  $\text{NO}_3^-$  left in the soil after flooding (a decrease of 43.8 mg  $\text{NO}_3^-$ -N), the mass balance required a mineralization contribution of  $64.0 \pm 8.2 \text{ mg N}$  (Figure 7). The mineralization incubation assays for the sand determined a total mineralization potential of 103 mg N for the duration of the flooding experiment. The fine sandy loam LF mass balance required an even greater amount of  $81.6 \pm 10.9 \text{ mg N}$  to explain the discrepancy between the

$145.7 \pm 5.8\%$  (47.1 mg  $\text{NO}_3^-$ -N) of  $\text{NO}_3^-$  leached during the fine sandy loam LF experiment and the change in residual  $\text{NO}_3^-$  left in the soil after flooding (an increase of 34.5 mg  $\text{NO}_3^-$ -N) (Figure 7). The total mineralization potential determined for the fine sandy loam from the assays was 133 mg N for the duration of the flooding experiment. When scaled for mineralization potential as a function of water content (Paul et al., 2003), the mineralization potential was  $46.57 \pm 14.29$  and  $68.55 \pm 19.34 \text{ mg N}$  for the sand and fine sandy loam. This indicates that the positive mass balance for both soil textures may be explained by mineralization processes (Figure 7). The HF experiments both showed a decrease in residual  $\text{NO}_3^-$  left in the soil after flooding. In general, they both have lower mineralization potential, and a higher denitrification potential, due to increased frequency of the water applications and higher water contents in the columns, conditions more conducive to denitrification (Butterbach-Bahl et al., 2013) (Figure 7).

## 4 | DISCUSSION

### 4.1 | Field scale residual $\text{NO}_3^-$ -N profile trends

Wetting–drying cycles have been shown to affect microbial activity, and semiarid regions like California particularly exhibit pulses of increased microbial activity during



**FIGURE 5** Initial soil  $\text{NO}_3^-$  mass and amount of  $\text{NO}_3^-$  leached during each water application (WA) during the (a) low frequency and (b) high frequency column experiments using sand and fine sandy loam soils. Percentages represent the percentage of initially present  $\text{NO}_3^-$ -N (gray bar) leached in each WA

significant precipitation events following long, dry periods (Austin et al., 2004; Noy-Meir, 1973). Our results indicate that the soil residual  $\text{NO}_3^-$  content after Ag-MAR can either increase or decrease in response to the pulsed water applications and related soil moisture-dependent N transformation processes. The 2015–2016 water year was ranked as a below average precipitation year in California and marked the final year of a 4-yr drought. In contrast, the 2016–2017 water year was the second wettest year in a 100-yr record (California Department of Water Resources, 2017). Thus, variation in precipitation between the 2015–2016 and 2016–2017 Ag-MAR field experiments may have distinctly affected biogeochemical processes and their potential rates and magnitudes at the field scale as indicated in Table 1. Although there is a lack of statistically significant trends between treatments and years in the field data, the finer texture soil (i.e., fine sandy loam) showed a clear increase in residual soil  $\text{NO}_3^-$  after flooding. Similar trends have been observed in previous studies by Chau et al. (2011) and Gregorich et al. (1991), who found greater amounts of mineralization and microbial activity in finer textured soils after irrigation or precipitation events. They concluded that the fine sandy loam in conjunction with a low  $K_{\text{sat}}$  of  $3.3 \text{ mm h}^{-1}$  in the deeper profile may create an environment

where mineralization and nitrification processes are dominating over advective transport, resulting in a net increase of  $\text{NO}_3^-$  in the residual soil profile post-Ag-MAR. However, it is also important to note that in the flood treatment of the fine sandy loam residual  $\text{NO}_3^-$  increase was less than the increase observed in the control, indicating that the flood treatment likely experienced more  $\text{NO}_3^-$  leaching than the control. This is further supported by our soil column experiments, where the fine sandy loam LF shows a net increase in residual  $\text{NO}_3^-$  in the soil profile, but also a large amount of  $\text{NO}_3^-$  exported out of the column with the effluent.

## 4.2 | Biogeochemical processes under varying flooding frequencies

During the LF treatment, over 100% of the initially present  $\text{NO}_3^-$  was leached from the soil columns, indicating that organic N mineralization was occurring at significant rates in between flooding events. Under ideal conditions (i.e., 55% water holding capacity,  $\sim 0.16\text{--}0.25 \text{ cm}^3 \text{ cm}^{-3}$  depending on soil layer) both soils would have the potential to mineralize inorganic  $\text{NO}_3^-$  at a profile average rate of  $7.0 \text{ mg N kg}^{-1} \text{ wk}^{-1}$  for the sand and  $8.3 \text{ mg N kg}^{-1} \text{ soil wk}^{-1}$  for the fine sandy loam. Mineralization at these rates well exceed the amounts needed to explain the positive N mass balance observed in the column experiments. Moisture conditions for mineralization were near ideal 24–48 hours after each WA (e.g., water content ranged between 55 and 100% of water holding capacity, Supplemental Figure S3 and S4). Although  $72.6 \pm 4.3\%$  (sand) and  $72.8 \pm 3.7\%$  (fine sandy loam) of the initial soil  $\text{NO}_3^-$  was leached during WA1, we estimate that  $46.6 \pm 14.29 \text{ mg}$  (sand) and  $68.55 \pm 19.34 \text{ mg}$  (fine sandy loam) of new  $\text{NO}_3^-$  was mineralized between flooding events, which then became susceptible to leaching during subsequent WAs. This is further supported by the amounts of  $\text{NO}_3^-$  leached during LF WA2 and 3 (64.6 and 72.6% of initial soil  $\text{NO}_3^-$  for the sand and fine sandy loam, respectively), which combined with WA1 exceeded the initial soil  $\text{NO}_3^-$  amount by 30.5 (sand) and 14.7 mg (fine sandy loam), respectively.

When the timing between flooding events was decreased to 72 h (HF treatment),  $24.5 \pm 2.9\%$  (sand) to  $62.9 \pm 5.6\%$  (fine sandy loam) of the initial soil  $\text{NO}_3^-$  was leached during WA1, and markedly lower  $\text{NO}_3^-$  concentrations were observed in the effluent during WA2 and WA3 than during the LF experiment. The total amounts of  $\text{NO}_3^-$  leached during HF WA2 and WA3 only accounted for 6.7% (sand) and 1.9% (fine sandy loam) of the initially present  $\text{NO}_3^-$ , indicating lower contributions from mineralization, likely due to the shorter time periods between flooding events. This is further supported by the pore water  $\text{NO}_3^-$  data shown in Supplemental Figures S1 and S2. The sand HF experiment clearly lacks the increase in pore

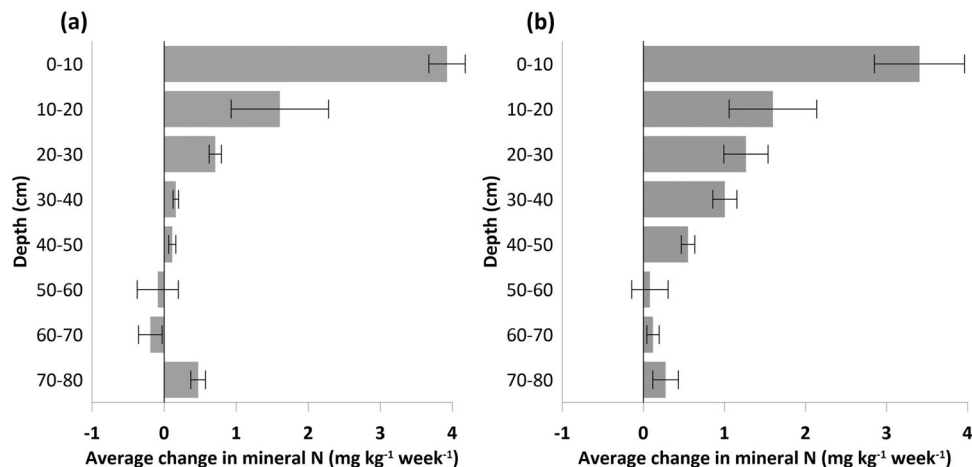


FIGURE 6 Mineralization rates for the (a) sand and (b) fine sandy loam

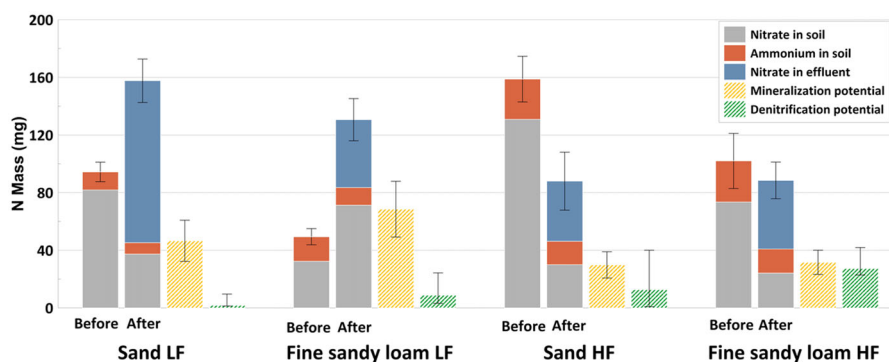


FIGURE 7 Total  $\text{NO}_3^-$  mass balance for soil columns. Error bars represent one standard deviation of the aggregated error for all components of a single column. LF, low-frequency treatment; HF, high-frequency treatment

water  $\text{NO}_3^-$  concentrations at the beginning of WA2 and WA3 that were observed during the LF experiment, indicating that a breakthrough of recently mobilized  $\text{NO}_3^-$  through the column was not occurring during the HF experiment. Similar patterns were observed for the HF experiment conducted with the fine sandy loam (Supplemental Figure S2). These dynamics support the hypothesis that less mineralization occurred in the shorter frequency (72-h) recharge experiment.

The  $\text{NO}_3^-$  mass balance of the HF experiments indicates that biogeochemical processes other than mineralization might have played a role. Although  $\text{O}_2$  levels stayed well above 10% during the HF experiment (Supplemental Figures S3 and S4), the  $\text{NO}_3^-$  mass balance indicates that there likely was a significant amount of denitrification occurring, possibly restricted to microsites (i.e., saturated immobile pore space) of the soil profile that provided conditions supportive of denitrification (Groffman et al., 2009; Parkin, 1987). In addition, temporary microbial immobilization of inorganic N to organic N within the soil profile might have occurred (Johnsson et al.,

1987, Paul & Clark, 2000, Romero et al., 2015). Based upon the denitrification incubations, and previous research concerning anaerobic microbial activity as a function of percent water filled pore space (Bateman & Baggs, 2005), the estimated denitrification potentials of the soil columns were 0.89–40.04 mg N (sand HF) and 22.83–41.91 mg N (fine sandy loam HF), respectively (Figure 7). Several layers in both soil textures had negative rates of net mineralization in the incubations (Figure 6), indicating that immobilization could also play a role in transforming inorganic N into organic N following WAs, which could act as a temporary sink of  $\text{NO}_3^-$  (Azam et al., 1988; Burger & Jackson, 2003; Recous et al., 1990).

The mineralization rates for the sand and fine sandy loam observed in this experiment are comparable with the rates found in other agricultural soils. Springob and Kirchmann (2003) found mineralization rates of 0.42–5.39 mg N  $\text{kg}^{-1}$   $\text{wk}^{-1}$  in sandy and sandy loam soils in the top 28 cm, whereas Wade et al. (2016) found mineralization rates in the top 25 cm

of soil to be, on average,  $1.61 \text{ mg N kg}^{-1} \text{ wk}^{-1}$ , which is comparable to our soils that mineralized  $3.93 \text{ mg N kg}^{-1} \text{ wk}^{-1}$  (sand) and  $3.41 \text{ mg N kg}^{-1} \text{ wk}^{-1}$  (fine sandy loam) in the top soil (0–10 cm) (Figure 6).

### 4.3 | Implications for field-scale $\text{NO}_3^-$ leaching

The soil column Ag-MAR experiments allowed for a controlled setting to investigate N cycling and N transport processes at finer temporal and spatial scales than was possible in the field. The column experiments confirmed our hypothesis that both soil texture and the time interval between water applications influence  $\text{NO}_3^-$  leaching amounts. We found that irrespective of soil texture or treatment, most  $\text{NO}_3^-$  was leached during the first water application, transporting 50–97% of the total observed effluent  $\text{NO}_3^-$  mass out of the column. Although we conducted two sets of column experiments comparing two soil textures and flooding frequencies, the soil core data collected from the field sites highlight the huge variability in residual soil  $\text{NO}_3^-$  mass that can be observed just at the plot or field scale and the need for appropriate scaling techniques to reliably estimate  $\text{NO}_3^-$  leaching potential in agricultural soils subject to Ag-MAR at the field scale. Baram et al. (2016) showed that using the spatial average of all observed  $\text{NO}_3^-$  concentrations within a field can sufficiently capture the variability in N mass balance.

Our analysis showed that when scaled up to the field, the amount of  $\text{NO}_3^-$  leached from the soil columns in response to the 45 cm of applied water for the LF and HF experiments were  $33.11 (0.72 \text{ kg ha}^{-1} \cdot \text{cm H}_2\text{O})$  and  $12.82 \text{ kg ha}^{-1} (0.28 \text{ kg ha}^{-1} \cdot \text{cm H}_2\text{O}) \text{ NO}_3^- \text{-N}$  for the sand, whereas the fine sandy loam LF and HF were  $14.53 (0.32 \text{ kg ha}^{-1} \text{ cm}^{-1} \text{ H}_2\text{O})$  and  $14.90 \text{ kg ha}^{-1} (0.33 \text{ kg ha}^{-1} \text{ cm}^{-1} \text{ H}_2\text{O}) \text{ NO}_3^- \text{-N}$ , respectively. These amounts are comparable with a  $\text{NO}_3^-$  leaching study conducted by Onsoy et al. (2005) in a citrus orchard near Fresno, CA, where intensive irrigation of  $174 \text{ cm yr}^{-1}$  resulted in  $93$  and  $275 \text{ kg ha}^{-1} \text{ yr}^{-1} \text{ NO}_3^- \text{-N}$  leached from the 180-cm root zone, which translates to  $0.53$  and  $1.58 \text{ kg ha}^{-1} \text{ yr}^{-1} \text{ NO}_3^- \text{-N cm}^{-1} \text{ H}_2\text{O}$  respectively, depending on fertilizer application rate ( $110$ – $365 \text{ kg ha}^{-1} \text{ yr}^{-1} \text{ NO}_3^- \text{-N}$ ). Bachand et al. (2016) reported an estimated  $\text{NO}_3^- \text{-N}$  loss of  $1.64 \text{ kg ha}^{-1} \text{ cm}^{-1} \text{ H}_2\text{O}$  recharged on a mixture of sandy loam and loamy sand soils, growing alfalfa (*Medicago sativa* L.) and wine grapes, in California's Central Valley.

For our soil column experiments,  $\text{NO}_3^-$  leaching for the sand LF and HF was estimated at  $0.72$  and  $0.28 \text{ kg ha}^{-1} \text{ cm}^{-1} \text{ H}_2\text{O}$  respectively, and the fine sandy loam LF and HF to be  $0.32$  and  $0.33 \text{ kg ha}^{-1} \text{ cm}^{-1} \text{ H}_2\text{O}$ , respectively. The sand soil column estimates are similar to the average  $\text{NO}_3^-$  leaching amount of  $0.77 \text{ kg ha}^{-1} \text{ cm}^{-1} \text{ H}_2\text{O}$  we estimated for the 2016 field-collected soil cores. Our numbers are 30–50% of what

Bachand et al. (2016) reported but are comparable with the  $\text{NO}_3^-$  leaching estimates Onsoy et al. (2005) estimated for the low fertilizer application rate treatment ( $110 \text{ kg ha}^{-1} \text{ yr}^{-1} \text{ NO}_3^- \text{-N}$ ). Comparison of our  $\text{NO}_3^-$  leaching amounts with Onsoy et al. (2005) highlights that the  $\text{NO}_3^-$  leaching amounts observed during our winter recharge event are comparable in magnitude with the amount of  $\text{NO}_3^-$  leached during the growing season in the citrus orchard near Fresno, CA. This opens the question whether the combination of winter Ag-MAR and growing season irrigation would effectively double the annual amount of  $\text{NO}_3^-$  leached from the root zone or whether the increase in soil  $\text{NO}_3^-$  due to mineralization after Ag-MAR events could potentially reduce fertilizer needs in subsequent growing seasons.

Some answers can be provided to this question based on our field and column experiments. First, it is important to note that in all soil column experiments, regardless of treatment or soil texture, the  $\text{NO}_3^-$  concentration of the total recharge was always below the USEPA maximum contaminant level of  $10 \text{ mg NO}_3^- \text{-N L}^{-1}$  (sand LF =  $7.22 \text{ mg L}^{-1}$ , sand HF =  $2.81 \text{ mg L}^{-1}$ , fine sandy loam LF =  $3.18 \text{ mg L}^{-1}$ , fine sandy loam HF =  $3.26 \text{ mg L}^{-1}$ ). Additionally, the bulk of  $\text{NO}_3^-$  transport comes at the beginning of the water application, often within the first few hours in coarse-textured soils.

These dynamics have several implications both for the Ag-MAR best practices to minimize  $\text{NO}_3^-$  leaching, as well as growing season N management. Because the majority of the residual soil  $\text{NO}_3^-$  is leached at the beginning of Ag-MAR events, growing season nutrient needs need to be carefully managed on fields considered for winter Ag-MAR to reduce the residual  $\text{NO}_3^-$  content of the soil at the end of the growing season. Management practices that reduce the residual N at the end of a growing season (cover cropping, high nutrient use efficiency strategies, etc.) will be beneficial at Ag-MAR sites in decreasing the  $\text{NO}_3^-$  leaching potential from the root zone. At the same time, our results highlight that coarse-textured or high- $K_{\text{sat}}$  soils promote fast and nearly complete (>70%) leaching of residual soil  $\text{NO}_3^-$  within hours of the first water application. Thus, it is unlikely that managing Ag-MAR systems for environmental conditions that promote denitrification, which often can be achieved by continuous flooding over several hours or days, will have much of an effect on reducing the leaching of  $\text{NO}_3^-$  already present in the soil at the beginning of the water application. However, prioritizing continuous flooding and decreasing the time between water applications will likely decrease the mineralization potential and thus decrease total leached  $\text{NO}_3^-$  amounts.

Although this research study highlighted the impact that the time interval between water applications may have on biogeochemical forcing, other Ag-MAR management variables exist that may influence  $\text{NO}_3^-$  leaching potential and site suitability for Ag-MAR projects. These include

physically manageable factors, such as flooding duration and timing within the season, and site-specific considerations, such as textural properties, hydrogeology, organic C/N pools, and the mineralization–denitrification potential of the site’s soils. Future research should place emphasis on the development of models that can represent the biogeochemical processes observed under Ag-MAR more fully to evaluate best Ag-MAR practices (Waterhouse et al., 2021).

## 5 | CONCLUSIONS

The field and soil column experiments conducted in this study highlight the importance of biogeochemical processes when considering  $\text{NO}_3^-$  leaching potential during winter groundwater recharge on agricultural fields (Ag-MAR). With  $137.3 \pm 6.6\%$  (sand) and  $145.7 \pm 5.8\%$  (fine sandy loam) of the initially present  $\text{NO}_3^-$  leached during low-frequency (1–2 wk apart) flooding, our results show that using soil cores obtained in the field before and after winter recharge events to estimate  $\text{NO}_3^-$  leaching potential do not adequately capture total  $\text{NO}_3^-$  leaching amounts. This is because repeated, pulsed water applications for groundwater recharge, particularly if applied with long time intervals between events, provide environmental conditions promoting the mineralization of organic N to  $\text{NO}_3^-$ . Despite their contrasting soil texture, both soils studied here were capable of mineralizing organic N at a profile-average rate of  $7.0\text{--}8.3 \text{ mg N kg}^{-1} \text{ wk}^{-1}$ . Comparison of different flooding frequencies (e.g. 72-h vs 1-wk time intervals between flooding events) showed that longer time intervals resulted in increased N mineralization potential, and consequently higher amounts of  $\text{NO}_3^-$  leached during subsequent flooding events. The column experiments further showed that the majority of the total  $\text{NO}_3^-$  leached over the course of the groundwater recharge event was leached during the first few hours of the first water application when environmental conditions were unfavorable for denitrification (such as anoxic conditions), a process that reduces  $\text{NO}_3^-$  to different gaseous  $\text{N}_2\text{O}$  products.

Our results helped identify and quantify important biogeochemical processes that need to be considered when assessing the environmental tradeoffs of practicing Ag-MAR on agricultural fields in production. Specifically, our results indicate that winter flooding on agricultural fields for groundwater recharge produces environmental conditions that promote N transformation processes that can produce more residual soil  $\text{NO}_3^-$ . However, more research is needed comparing different soil textures and Ag-MAR practices to fully understand the impact of winter recharge (amounts, timing, flooding duration) on the organic C/N pools and N cycling processes, including  $\text{NO}_3^-$  leaching and mineralization–denitrification potential. Simulating these biogeochemical processes with reactive transport instead of conservative transport models

should allow improving estimates of total  $\text{NO}_3^-$  leaching amounts during Ag-MAR, which can guide Ag-MAR best practice development.

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## AUTHOR CONTRIBUTIONS

Nicholas Paul Murphy: Conceptualization; Data curation; Formal analysis; Investigation; Methodology; Project administration; Resources; Validation; Visualization; Writing-original draft; Writing-review & editing. Hannah Waterhouse: Conceptualization; Investigation; Resources; Writing-review & editing. Helen E. Dahlke: Conceptualization; Funding acquisition; Investigation; Methodology; Project administration; Resources; Supervision; Visualization; Writing-review & editing.

## CONFLICT OF INTEREST

The authors declare no conflict of interest.

## DATA AVAILABILITY STATEMENT

Raw data are available from the corresponding author upon request for both field and laboratory experiments. Data include soil, pore water, and effluent analysis for field and laboratory experiments outlined in Section 2, soil column  $\text{NO}_3^-$ –N leaching mass balance calculations, mineralization potential and the conditional analysis based on water content, estimated deep percolation calculations, and soil column instrumentation data (VWC, dissolved  $\text{O}_2$ ).

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## SUPPORTING INFORMATION

Additional supporting information may be found online in the Supporting Information section at the end of the article.

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