1 Comparing measurements of limiting

current of electrolytes with theoretical predictions up to the solubility limit

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Abstract

21mposing a steady ionic current through an electrolyte results in the 3formation of salt concentration gradients that compromise battery 4performance. The limiting current is usually defined as the current at which 5the salt concentration at the cathode approaches zero. Higher currents 6cannot be imposed on the cell as larger concentration gradients are 7unsustainable. We study the limiting current in electrolytes comprising a 8perfluorinated oligomer, C8-DMC, and lithium bis(fluorosulfonyl)imide salt in 9symmetric lithium cells. The time-dependence of the potential, which 10 increases as salt concentration gradients develop, was also measured. Both 11steady-state and transient behaviors are modeled using Newman's 12concentrated solution theory; transport and thermodynamic parameters 13needed to perform the calculations were measured independently and 14 reported in a previous publication [Shah et al., Phys. Chem. Chem. Phys., 152019, **21**, 7857-66]. The limiting current is a non-monotonic function of salt 16concentration in both theory and experiment. The model shows that at low 17salt concentrations (below 0.88 mol/kg solvent), the concentration at the 18cathode approaches zero at limiting current. In contrast, at high salt 19concentrations (above 0.88 mol/kg solvent), the concentration at the anode 20approaches the solubility limit (2.03 mol/kg solvent). The experimentally 21 determined salt concentration at which the limiting current is maximized is in 22excellent agreement with theoretical predictions made without resorting to 23any adjustable parameters.

Keywords

2Fluorinated electrolyte, limiting current, lithium batteries, modeling, PFPE,

3PFE, solubility limit

11. Introduction

2A barrier to the development of next-generation rechargeable lithium-based 3batteries is the electrolyte. Conventional electrolytes, comprising a lithium 4salt, LiPF₆, dissolved in a mixture of cyclic carbonates, exhibit limited 5electrochemical stability windows (< 4.5 V vs Li⁺/Li), and are susceptible to 6thermal runaway.^{1,2} One approach has been to replace conventional, 7carbonate electrolytes with fluorinated, electrolytes that have reduced 8flammability.³⁻⁷ Fluorinated electrolytes also exhibit high oxidation potentials 9(> 5 V vs. Li⁺/Li), and thus have the potential to enable high voltage 10cathodes.^{8,9}

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12The operation of a battery results in the development of salt concentration 13gradients within the electrolyte. These gradients arise due to existence of 14two mobile charge carriers: the anion and cation, and the magnitudes of the 15gradients increase with increasing current density. The limiting current is 16defined as the largest current that can be imposed on the electrolyte. 17Conventional wisdom suggests that at the limiting current, the salt 18concentration gradient is so large that the salt concentration at the cathode 19approaches zero.¹⁰ A few studies report experimentally determined liming 20current, but the factors that govern this parameter have not been fully 21elucidated.^{11,12}

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1Complete electrochemical characterization for a binary electrolyte requires 2the measurement of the thermodynamic factor, $T_{\rm f}$, and three transport 3properties: conductivity, κ , the salt diffusion coefficient, D, the cation 4transference number with respect to the solvent t_{+i^0i} .¹⁰ All of the parameters 5must be measured as a function of salt concentration to obtain a complete 6picture.¹³⁻¹⁷ In a recent study, Pesko et al. used measured values of $T_{\rm f}$, κ , D, 7and t_{+i^0i} in mixture of poly(ethylene oxide) (PEO) and lithium 8bis(trifluoromethanesulfonyl)imide salt (LiTFSI) to predict limiting current 9based on the conventional definition of limiting current.¹⁸

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11Recently, we reported T_{f} , κ , D, and t_{*i^0i} for a perfluoropolyether, C8-DMC, 12mixed with lithium bis(fluorosulfonyl)imide salt (LiFSI).¹⁹ We use Newman's 13concentrated solution theory to predict concentration and potential profiles 14as a function of salt concentration and current density in lithium symmetric 15cells at steady-state. We also use the theory to calculate transient 16concentration and potential profiles in the electrolyte. We note conditions 17(salt concentration and current density) under which the salt concentration 18at the cathode approaches zero. We also note the conditions under which 19salt concentration at the anode approaches the solubility limit. These 20predictions are compared with experimental data without the use of any 21adjustable parameters.

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12. Experimental Details

2Electrolyte Preparation

3The perfluoroether, C8-DMC (CAS-No. 1976035-41-2), was synthesized from 4a diol terminated precursor following procedures described in previous 5work.^{3,5,19,20} The chemical formula of C8-DMC is given in Figure 1a. All sample 6 preparation was done within an argon filled Vac glovebox with H_2O and O_2 7concentrations kept below 1 ppm. Lithium bis(fluorosulfonyl)imide (LiFSI) 8(cat. no. 097602) was purchased from Oakwood Products, Inc. Figure 1b 9contains the chemical formula of the FSI anion. The salt was \geq 99% pure, as 10confirmed by a Certificate of Analysis form. The salt was dried at 100 °C 11under dynamic vacuum for three days inside a glovebox antechamber. Prior 12to transfer into the glovebox, C8-DMC was dried under active vacuum inside 13the glovebox antechamber at 50 °C for 72 hours. In order to form 14electrolytes, a predetermined amount of Li salt was added to a known mass 15of C8-DMC. Once the salt was added, the electrolytes were placed on a 16magnetic stirrer and were allowed to mix for 12 hours or more using a 17magnetic stir bar. The salt concentration of prepared electrolytes is 18 described as $m_{\rm av}$, the molality of the electrolyte in units of mol LiFSI/kg C8-19DMC. Electrolytes were prepared within a concentration window of 0.28 $20 \le m_{av} \le 1.78 \text{ mol/kg}.$



3 4Lithium symmetric cells and limiting current measurements

5Lithium symmetric cells were assembled by sandwiching an electrolyte-6soaked separator, Celgard 2500 (Celgard Company), with lithium discs, cut 7from lithium chips (MTI Corp.). Celgard 2500 was cut to 19 mm in diameter 8 and had an average thickness, L, of 25.4 \pm 0.6 μ m. The diameter of the 150 9µm thick Li disc was 12.7 mm. Three replicate cells were produced for each 10electrolyte and the reported data is the average of those three cells, with 11error bars representing the standard deviation between the replicate cells. 12Data were collected on a Bio-Logic VMP3 potentiostat. Each sample cell was 13subjected to a conditioning treatment, which consisted of charge and 14discharge cycles at 0.02 mA/cm² in order to help stabilize the interfacial 15 layer. The sequence performed was a 4 hour charge, 30 minutes rest, a 4 16hour discharge, 30 minutes rest, and repeated for a total of 6 times. To track 17the cell impedance with time, ac impedance spectroscopy was performed 18before the beginning of conditioning, after each rest step, and at the end of 19conditioning. Complex impedance plots were obtained within a frequency 20range of 1 MHz to 100 mHz. Each sample was then polarized at all of the 21 following current densities for 30 minutes: $i_{ss} = 0.20, 0.40, 0.50, 0.60, 0.70,$

10.75, 0.80, and 1.00 mA/cm² with potential and current data recorded every 2five seconds. Ac impedance spectroscopy followed each polarization and the 3data were analyzed in the form of a Nyquist plot. The data were fit to an 4equivalent electrical circuit and the interfacial impedance, R_i , was extracted, 5as described in a previous publication.⁵ The interfacial impedance was used 6to correct for the potential drop, ϕ , across an electrolyte, as described in Eq. 71 below

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$$\boldsymbol{\Phi}(t) = \boldsymbol{\Phi}_{measured}(t) - \boldsymbol{R}_i \boldsymbol{i}_{ss} \boldsymbol{A}$$
(1)

9where $\Phi_{measured}$ is the potential across the lithium symmetric cell as measured 10by the potentiostat under a given steady-state current density, i_{ss} , and A is 11the active area of the electrode. All electrochemical characterization was 12done at 30 C.

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14**3. Theory**

15Steady-state model

16The relationship between i_{ss} and the electrochemical properties of an 17electrolyte, based on Newman's concentrated solution theory,¹⁰ was derived 18in ref. 18. This relationship changes slightly when the electrolyte is contained 19in a porous separator (we call this the electrolyte/separator composite), and 20is given by Eq. 2

$$\int_{m(x=0)}^{m(x)} \frac{c(m)D_{s}(m)}{mt_{-\iota^{0}(m)}} dm = \frac{i_{ss}L}{F Z_{-\iota v_{-\iota}\left(\frac{x}{L}\right)} \iota} \iota$$
(2)

2where *c* is the concentration of the salt in the electrolytic phase in mol/cm³, 3*D*_s is the salt diffusion coefficient measured by restricted diffusion on the 4electrolyte/separator composite, *m* is the molality, $t_{-i^{\theta}i}$ is the anion 5transference number relative to the velocity of the solvent ($t_{-i^{\theta}=1-t_{i,0}i}$), z_{-ii} is 6the charge number on the anion, v_{-ii} is the number of anions the salt 7disassociates into, *L* is the thickness of the electrolyte/separator composite, 8*x/L* is the normalized thickness, and *F* is Faraday's constant (the transference 9number is unaffected by the presence of the separator). All of the ion 10transport properties depend on salt concentration, as indicated in Eq. 2. 11During an experiment, the average salt concentration of the electrolyte, m_{av} , 12is controlled. The molality profile predicted by Eq. 2 must be averaged from 13*x* = 0 to *x* = *L* to ensure that the model predicted average concentration is 14equal to m_{av} .

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16The relationship between the electric potential within an

17electrolyte/separator composite to the measurable transport properties is 18given by

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20where $t_{+,id}$ is the ideal transference number (unaffected by the presence of 21the separator) and κ_s is the conductivity of the electrolyte/separator

1composite. The ideal transference number, $t_{+,id}$, is determined by the steady-2state current method.^{21,22} The relationship between the ideal transference

3number and κ , $t_{-\iota^{0}\iota}$, $1 + \frac{d \ln \gamma_{\pm}}{d \ln m}$ (the thermodynamic factor), and *D* is given in 4ref. 23 and a relationship was first noted in ref. 24. In this paper, Eqs 2 and 3 5were solved numerically using MATLAB and published data¹⁹ for the relevant 6parameters.

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8Transient model

9As is the case for the steady-state model, the transient model is also based 10on Newman's concentrated solution theory.¹⁰ We solve the governing 11differential equation along the thickness direction (denoted as the x-direction 12in the present analysis) of the polymer electrolyte. Since lithium metal exists 13on both ends of the electrolyte domain, these lithium/polymer interfaces 14have been considered as the two boundaries of the one-dimensional 15computational domain. Table 1 summarizes the governing equations and 16boundary conditions used in this study. The mass balance relation for 17electrolyte salt is expressed in Eq. 4, which was derived based on 18concentrated solution theory, is used to obtain transient concentration 19profiles [c(x,t)] across the polymer electrolyte. Note that the effect of 20transference number gradient is also taken into account, as shown in the 21second term on the right of Eq. 4. The modified Ohm's law expressed in Eq. 227, which includes the polarization in the electrolyte due to concentration 1gradients, is used to obtain transient ionic potential profiles, $\Phi_1(x,t)$, across 2the polymer. The potential drop across the polymer electrolyte is denoted as $3\Phi_{1,(x=0)}-\Phi_{1,(x=L)}$. The model parameters used in this study are listed in Table 2. 4

	Governing equation	Boundary conditions
Mass balance	$\frac{\partial c}{\partial t} = \nabla \cdot \left[D_s \left(1 - \frac{d \ln c}{d \ln c} \right) \nabla c \right] - i_{ss} \cdot \nabla$	$-D_{s}\frac{\partial c}{\partial x}\Big _{x=0} = 1 - \frac{t_{+i^{0}}}{F}i_{ss}i_{s$
electrolyte)	(4)	$-D_{s}\frac{\partial C}{\partial x}\Big _{x=L} = -1 - \frac{t_{+i}}{F}i_{ss}i$
Modified Ohm's law (Ionic phase)	$i_{ss} = -\kappa_s \nabla \Phi_2 + \frac{2\kappa_s RT}{F} \left(1 + \frac{\partial \ln f_{\pm}}{\partial \ln c} \right) i$	${m \phi}_{2,L}\!=\!0$ (8)
	(7)	

5 Table 1: Summary of governing equations	<mark>for C8-DMC/LiFSI א</mark>	with a Celgard
62500 separator in a Li symmetric cell		

8**Table 2:** Parameters used for Li symmetric transient modeling of 9C8-DMC/LiFSI with a Celgard 2500 separator

Symbol	Parameter	Initial Value	Reference
L	Thickness of <mark>separator</mark>	2.54e-3 [cm]	Measured
К	lon <mark>ic</mark> conductivity of <mark>C8-DMC</mark>	Function of concentration	Measured
D	Diffusion coefficient of LiFSI in C8-DMC	Function of concentration	Measured
t_+;°;	Cation transference number	Function of concentration	Measured
F	Faraday constant	96450 [C/mol]	-
R	Universal gas constant	8.314 [J/mol/K]	-
Т	Temperature	<mark>30 [°C]</mark>	-

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114. Results and Discussion

12Our objective is to compare potential versus time curves determined 13experimentally in Li symmetric cells as a function of average salt 14concentration and current density up to the salt solubility limit and the 15limiting current with theoretical predictions. Table 3 shows the 16aforementioned transport and thermodynamic properties of lelectrolyte/separator composites for a range of salt concentrations taken 2from ref. 19. It is convenient to work with units of molality for steady-state 3calculations while transient calculations are best done using molar 4concentrations. In Table 3, we list both *m* and *c*, based on measurements 5reported in ref. 19. Note that t_{+c^0t} is negative over the entire concentration 6range, indicating the formation of charged clusters. The interactions that 7lead to the formation of these clusters has not yet been elucidated.

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10**Table 3:** Transport properties of C8-DMC/LiFSI with a Celgard 2500 $11_{separator}^{separator}$ at 30 °C¹⁹

_	<i>m</i> (mol/kg)	<i>c</i> (mol/cm ³)	К _s (S/ст)	D_s (cm ² /s)	$t_{+,id}$	t _{+i°i}	$1 + \frac{d ln \gamma_{\pm}}{d ln m}$
-	0.28	3.87 x 10 ⁻⁴	$[2.91 \pm 0.19] \times 10^{-6}$	$[3.66 \pm 0.39] \times 10^{-8}$	0.89 ± 0.01	-1.002 ± 0.06	0.15 ± 0.02
	0.60	8.89 x 10 ⁻⁴	$[9.82 \pm 0.90] \times 10^{-6}$	$[2.24 \pm 0.12] \times 10^{-8}$	0.77 ± 0.01	-0.751 ± 0.04	0.19 ± 0.02
	0.94	1.36 x 10 ⁻³	$[1.17 \pm 0.07] \times 10^{-5}$	$[1.72 \pm 0.13] \times 10^{-8}$	0.71 ± 0.07	-0.378 ± 0.04	0.42 ± 0.06
	1.30	1.70 x 10 ⁻³	$[1.14 \pm 0.09] \times 10^{-5}$	$[1.34 \pm 0.11] \times 10^{-8}$	0.67 ± 0.02	-0.070 ± 0.00	0.85 ± 0.11
12	1.78	2.36 x 10 ⁻³	$[7.92 \pm 0.75] \times 10^{-6}$	$[1.20 \pm 0.21] \times 10^{-8}$	0.67 ± 0.02	-0.232 ± 0.01	1.12 ± 0.23



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2**Figure 2:** Fit of the integrand term of Eq. 2, $\frac{cD_s}{mt_{-\iota}}$, with LiFSI salt molality. 3The solid curve shows the least-squares polynomial fit given by Eq. 9.

5To calculate the concentration profile within an electrolyte given a steady-6state current density, i_{ss} , and thickness, *L*, the transport parameters given in 7Table 3 were fit as a continuous function to salt concentration. In Figure 2, 8we show the 4th order polynomial fit to the product appearing on the right 9side of Eq. 2,

$$\frac{c(m)D_{s}(m)}{mt_{-\iota^{0}(m)}=k_{0}+k_{1}m+k_{2}m^{2}+k_{3}m^{3}+k_{4}m^{4}\iota}$$
(9)

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11 with fitting parameters

 $12 \begin{array}{ccc} k_0 = 2.03 \times 10^{-10} & k_1 = -4.52 \times 10^{-10} & k_2 = 6.46 \times 10^{-10} \\ k_3 = -3.99 \times 10^{-9} & k_4 = 8.861 \times 10^{-11} & \& \end{array}$

13where $t_{-i^{\circ}i}$ is equal to $1 - t_{+i^{\circ}i}$, D_{s} is in cm²/s, c is in mol/cm³, and m is in 14mol/kg. The parameters apply to the range $0.28 \le m \le 1.78$ mol/kg and for T 15= 30 °C.

2The concentration profile within a lithium symmetric cell under a steady-3state operation is governed by the thickness of the electrolyte, *L*, the salt 4concentration, m_{av} , and the steady-state current density, i_{ss} .

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7Figure 3: Concentration profiles of LiFSI in C8-DMC predicted by Eq. 2 at 8steady-state for three different normalized current densities: (a) $i_{ss}L = 5.08 \times 10^{-5}$, (b) $i_{ss}L = 5.08 \times 10^{-4}$, and (c) $i_{ss}L = 1.02 \times 10^{-3}$ mA/cm. 10

11Fig. 3 shows the concentration profiles across a mixture of C8-DMC/LiFSI for 12three initial concentrations of $m_{av} = 0.60$, 0.94, and 1.30 mol/kg and for 13three values of normalized current density, $i_{ss}L$. We have chosen the product 14 $i_{ss}L$ for this plot because i_{ss} is inversely proportional to L; Fig. 3 may thus be 15used to determine i_{ss} values for L values different from that used in this 16particular study. The concentration profiles were obtained by numerically 17solving Eq. 2 using the fitted Eq. 4. The figures correspond to $i_{ss}L = 5.08 \times 10^{-1}$ 18⁵, 5.08 x 10⁻⁴, and 1.02 x 10⁻³ mA/cm (relating to $i_{ss} = 0.02$, 0.20, and 0.40 1mA/cm² for L = 0.00254 cm). It is evident from Fig. 3a that under small 2applied normalized current densities ($i_{ss}L = 5.08 \times 10^{-5}$ mA/cm), the 3concentration profiles are approximately linear and the gradients are small. 4However, with increasing normalized current densities, the concentration 5gradients become steeper, as shown in Figs. 3b and c. Note that the overall 6flux of lithium cations, at steady-state, is toward the negative electrode in 7spite of the fact that the transference number is negative at all salt 8concentrations. The sign of the transference number only gives the direction 9of the flux of lithium cations in a solution of uniform composition in response 10to an applied electrochemical potential. Thus, at the instant that a dc 11potential is applied to the cell, the net lithium cation flux is toward the 12positive electrode. At steady-state after the salt concentration gradients are 13fully developed, the net lithium cation flux is toward the negative electrode.²⁵

15One can estimate the normalized limiting current, $i_{\text{limit}}L$, within an electrolyte 16using model predicted concentration profiles. In order to do so, an electrolyte 17of known m_{av} must be modeled under a number of $i_{\text{ss}}L$ values and the salt 18concentration at the cathode (x/L = 1) is extracted at each normalized 19current density. An example of such an analysis is shown in Fig. 4a. In Fig. 204a, $i_{\text{ss}}L$ is plotted against the model predicted salt concentration, m, at x/L =211 in blue circles for an electrolyte with an average salt concentration of m_{av} 22= 0.94 mol/kg. As the model is limited between 0.28 $\leq m \leq$ 1.78 mol/kg, the 23conventional limiting current must be predicted by extrapolating m(at x/L =

11) to zero. The dashed, black curve is a 2nd order polynomial fit to the model 2predicted values in Fig. 4a, and predicts $i_{limit}L = 3.7 \times 10^{-3}$ mA/cm. It should 3be noted that the solubility limit of LiFSI in C8-DMC is 2.03 mol/kg.⁵ It is 4obvious that the concentration at any x/L in the cell must not exceed this 5value for stable operation. The highest salt concentration occurs at the 6anode (x/L = 0). In Fig. 4b, we thus plot $i_{ss}L$ versus m(x/L = 0) for the same 7average salt concentration used in Fig. 4a ($m_{av} = 0.94$ mol/kg). A 2nd order 8polynomial is fit through the data and extrapolated to m = 2.03 mol/kg is 9shown as a dashed curve. We define the normalized limiting current at which 10this occurs as $i_{limit,sat}L$ which is 3.2×10^{-3} mA/cm for $m_{av} = 0.94$ mol/kg.



Figure 4: Concentration predictions at the anode (x/L = 1) and cathode (x/L = 0) for varying $i_{ss}L$ values for an electrolyte with an average concentration 15 of $m_{av} = 0.94$ mol/kg. (a) Model predictions of the concentration at the 16 anode, x/L = 1. The black dashed curve shows the least-squares polynomial 17 fit, which was extrapolated to m = 0 mol/kg to determine the normalized 18 limiting current density (marked as $i_{limit}L$). (b) Model predictions of the 19 concentration at the cathode, x/L = 0. The black dashed curve is a least-20 squares polynomial fit, which was extrapolated to the salt solubility limit of

1m = 2.03 mol/kg. This determined the normalized limiting current density 2caused by salt saturation at the cathode (marked as $i_{limit,sat}L$). 3

4There is an important question: for a given m_{av} , which mode of the limiting 5current will be observed? We posit that the mode will correspond to the one 6that is obtained at the lower normalized limiting current. For $m_{av} = 0.94$ mol/ 7kg, we conclude that the normalized limiting current will occur due to salt 8precipitation. Similar analysis was repeated at all values of m_{av} .

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11**Figure 5:** Time dependent potential behavior of C8-DMC/LiFSI with an 12average salt concentration of $m_{av} = 0.94$ mol/kg in response to applied 13current densities from i = 0.20 to 1.0 mA/cm^2 (no interfacial impedance 14correction). The largest sustainable current density, *i*, as determined by 15plateau in measured potential, was 0.60 mA/cm², shown as a solid red curve. 16The smallest unsustainable *i*, as determined by the lack of a plateau in the 17potential within the measurement window, was 0.80 mA/cm² and is shown as 18a solid yellow curve.

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20Turning to experiments, we now discuss potential versus time curves for an

21electrolyte/separator composite in a lithium symmetric cell (L = 0.00254 cm)

1at a fixed applied current. In Fig. 5, we show the potential profile versus time 2for current densities ranging from $i_{ss} = 0.20 \text{ mA/cm}^2$ to 1.00 mA/cm² in 0.2 3mA/cm² increments for an initial concentration of $m_{av} = 0.94$ mol/kg. At low 4current densities (below 0.60 mA/cm²), the potential increases 6concentration is uniform, increases with time as concentration gradients 7develop, and reaches a plateau when the concentration profile in the cell 8approaches steady-state. At a slightly higher current density of 0.80 mA/cm², 9the potential increases monotonically with time and does not reach a 10plateau. We refer to 0.60 mA/cm² as the largest sustainable current density 11and 0.80 mA/cm² as the smallest unsustainable current density. Increasing 12the current density beyond 0.80 mA/cm² leads to potential increases 13exponentially with time with no hint of a plateau. Data similar to that shown 14in Fig. 5 was obtained for all of the electrolytes. The normalized limiting 15current density, $i_{\text{limit}}L$, was determined for each electrolyte by averaging the 16 largest sustainable current and smallest unsustainable current. In Fig. 6, we 17 plot the experimental limiting current, $i_{\text{limit}}L$, as a function of m_{av} . The 18normalized limiting current for $m_{av} = 0.28$ mol/kg is 1 x 10⁻³ mA/cm. It 19 increases with increasing salt concentration, reaching a broad maximum of $20i_{\text{limit}}L = 1.8 \times 10^{-3} \text{ mA/cm}$ between $m_{av} = 0.60$ and 0.94 mol/kg. Further 21 increase in m_{av} results in a decrease in $i_{limit}L$ until $m_{av} = 1.78$ mol/kg, a value 22that is close to the salt solubility limit.

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2Figure 6: Experimental limiting current as a function of salt concentration.
3The limiting current was taken as the average between the largest
4sustainable current and smallest unsustainable current. The solid line is
5drawn to guide the eye.
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7In Fig. 7a, $i_{limit}L$ is plotted against m_{av} ; the black diamonds show experimental 8measurements that were shown in Fig. 6, red squares represent the 9predicted $i_{limit}L$ when concentration reaches zero at the cathode (x/L = 1), 10and blue circles are the predicted $i_{limit}L$ values when the solubility limit of m = 112.03 is reached at the anode (x/L = 0). The cathode-dominated $i_{limit}L$ (the 12traditional limiting current) increases with increasing concentration. In 13contrast, the anode-dominated $i_{limit,sat}L$ decreases with increasing 14concentration. The two normalized limiting currents are equal to each other 15at $m_{av} = 0.88$ mol/kg. Following our assumption that the failure mode 16obtained experimentally corresponds to the one that requires the lower 17current density, we conclude that salt depletion at the cathode causes the 18limiting current at $m_{av} < 0.88$ mol/kg, while salt precipitation at the anode 19causes the limiting current at $m_{av} > 0.88$ mol/kg. The two solid curves

1through the theoretical predictions in Fig. 7a show these two branches. The 2theoretical predictions provide a qualitative explanation for the observed 3non-monotonic dependence of the measured limiting current on salt 4concentration. There are two important quantitative differences between 5theory and experiment in Fig. 7a: (1) The theoretical limiting currents are 6about a factor of 2 higher than those measured experimentally and (2) The 7peak in the limiting current versus salt concentration predicted by theory is 8sharper than that observed experimentally. We do not have definitive 9explanations for these deviations, except to note that the interface between 10the electrode and electrolyte is complex, and that failure in the experimental 11cells may begin before the salt concentration at the cathode reaches zero or 12the salt concentration at the anode reaches the solubility limit.

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14Approximate expressions are often used to determine the normalized 15limiting current due to salt depletion at the cathode. ²⁶⁻²⁸ One such 16expression can be derived by combining equations 11.22, 11.41, 11.43, and 1711.57 in ref. 10:

$$i_{limit} L = \frac{2 c_{av} D_{S} F}{1 - t_{+, id}}$$
(10)

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19where c_{av} is the average electrolyte concentration in mol/cm³, D_s is the 20restricted diffusion coefficient in the electrolyte/separator composite, and we 21have taken the liberty of using the $t_{+,id}$. Similarly, the normalized limiting

1current that causes the concentration at the anode to approach the solubility 2limit is:

$$i_{limit,sat}L = 2 \frac{(c_{sat} - c_{i}iav)D_{s}F}{1 - t_{+,id}}i$$
(11)

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4where c_{sat} is salt solubility limit. For mixtures of C8-DMC and LiFSI, $c_{sat} = 2.61$ 5x 10⁻³ mol/cm³. Equations 10 and 11 were derived using dilute solution 6theory, thus the ideal transference number, $t_{+,id}$, is used in both equations. In 7Fig. 7b, we plot $i_{\text{limit}}L$ vs. m_{av} ; red squares denote the predicted $i_{\text{limit}}L$ using Eq. 810, and blue circles represent the predicted $i_{\text{limit,sat}}L$ using Eq. 11. Both 9predictions for the normalized limiting current decrease with increasing salt 10concentration. The cross-over from the salt-depletion limit to the salt 11precipitation limit occurs at a reasonable value of m_{av} , but the predicted 12trend is monotonic with salt concentration and inconsistent with the 13experimental data. In addition, the theoretical predictions for normalized 14limiting current based on dilute solution theory are an order of magnitude 15 higher than those measured experimentally (black squares in Fig. 7b). It is 16obvious from Fig. 7 that concentrated solution theory is essential for 17establishing the underpinnings of the normalized limiting current in our 18system.



2Figure 7: Normalized limiting current predictions as a function of m_{av} and 3 compared to experimental values (shown in black). (a) Concentrated solution 4 theory predictions of the normalized limiting current. The red dashed and 5 solid curves are the $i_{limit}L$ predicted when extrapolating m_{av} to 0 mol/kg at the 6 cathode (x/L = 1). The blue dashed and solid curves are the $i_{limit,sat}L$ 7 predicted by extrapolating m_{av} to 2.03 mol/kg at the anode (x/L = 0). (b) 8 Normalized limiting current predictions using dilute solution theory. The red 9 dashed and solid curves are the $i_{limit}L$ predicted by Eq. 10 (concentration 10 equal to 0 mol/cm³ at the cathode). The blue dashed and solid curves are the $11i_{limit,sat}L$ predicted by Eq. 11 (salt saturation at the anode, $c_{sat} = 2.61 \times 10^{-3}$ 12 mol/cm³). Normalized limiting current predictions using dilute solution theory 13 are an order of magnitude higher than the experimental values.

15We now return to the potential that can be predicted using Eq. 3. In Fig. 8,

16we plot the integrand in Eq. 3 along with a fit to the following empirically

17determined function:

$$\frac{c(m)D_s(m)}{mt_{+,id}(m)\kappa_s(m)t_{-i^{\circ}(m)}=b_0\exp\left(-\tau_3m\right)+b_1\exp\left(-\tau_4m\right)i}$$
(12)

18

19 with fitting parameters

$$20 \frac{b_0 = 1.802 \times 10^{-6}}{\tau_3 = 0.1541} \frac{b_1 = 8.566 \times 10^{-5}}{\tau_4 = 8.525}$$

1where κ_s is the conductivity of the separator/electrolyte composite in S/cm.

2



3

4**Figure 8:** Fit of the integrand term of Eq. 3, $\frac{cD_s}{mt_{+,id}\kappa_s t_{-i^{\circ}}i}$, with LiFSI salt 5molality. The solid curve shows the least-squares fit to the double 6exponential given by Eq. 7.

8The fit from Fig. 8 allows for potential predictions across the C8-DMC/LiFSI 9electrolyte. In Fig. 9, we show the predicted potential profile, $\Phi(x/L)$, across 10the electrolyte from x/L = 0 to 1 for selected values of m_{av} and $i_{ss}L$. We define $11\Phi = 0$ at x/L = 1. The purple, yellow, and green solid curves are potential 12profiles for $m_{av} = 0.60$, 0.94, and 1.30 mol/kg, respectively. From left to right, 13each figure provides profiles for $i_{ss}L = 5.08 \times 10^{-5}$, 5.08 $\times 10^{-4}$, and 1.02 $\times 10^{-3}$ 14mA/cm, respectively. Note that these values of $i_{ss}L$ correspond to the applied 15 i_{ss} in our cell equal to 0.02, 0.20, and 0.40 mA/cm² (L = 0.00254 cm). At $i_{ss}L =$ 165.08 $\times 10^{-5}$ mA/cm, the potential profile across the electrolyte is linear and 17the gradient is small, as shown in Fig. 9a, but the potential behavior 1becomes less linear with increasing $i_{ss}L$. Interestingly, the intermediate 2concentration of $m_{av} = 0.94$ mol/kg shows a lower $\Phi(x)$ across the electrolyte 3at all values of $i_{ss}L$, compared to $m_{av} = 0.60$ or 1.30 mol/kg. The potential 4drop for $m_{av} = 0.60$ shows more complex behavior: it has a lower potential 5drop across the electrolyte when compared to $m_{av} = 1.30$ at both $i_{ss}L = 5.08$ 6x 10⁻⁵ and 5.08 x 10⁻⁴ mA/cm, but has the largest potential drop across the 7electrolyte at $i_{ss}L = 1.02 \times 10^{-3}$ mA/cm. Next, we compare the model 8predicted potential drop across the electrolyte to experimental 9measurements of potential, Φ_{exp} , for a range of m_{av} . The experimentally 10accessible potential is at x/L = 0. We thus define Φ_0 as to be the theoretically 11predicted potential at x/L = 0 for a given m_{av} and i_{ss} .

12



14**Figure 9:** Potential profiles in C8-DMC/LiFSI electrolytes predicted by 15concentrated solution theory at steady-state. These are calculated using Eq. 163 based on the fit shown in Fig. 8. Potential profile for (a) $i_{ss}L = 5.08 \times 10^{-5}$ 17mA/cm, (b) $i_{ss}L = 5.08 \times 10^{-4}$ mA/cm, and (c) $i_{ss}L = 1.02 \times 10^{-3}$ mA/cm. 18Interestingly, the potential drop across C8-DMC/LiFSI with $m_{av} = 0.60$ at $i_{ss}L$

1= 5.08 x 10⁻⁵ mA/cm is less than that of m_{av} = 1.30, but has a higher 2potential drop at $i_{ss}L$ = 1.02 x 10⁻³ mA/cm. 3

4The experimentally applied potential drop, Φ_{exp}/L , for the electrolyte with m_{av} 5= 0.94 mol/kg is plotted as a function of i_{ss} in Fig. 10a. The experimental 6potential drop is corrected for the lithium/electrolyte interfacial impedance 7using Eq. 1. Also shown in Fig. 10a is the predicted potential drop, Φ_0/L , 8calculated from Fig. 9 for $m_{av} = 0.94$ mol/kg. Both theory and experiment 9indicate that Φ/L increases with increasing i_{ss} . At $i_{ss} = 0.20$ mA/cm², the 10theoretically predicted potential drop, Φ_0/L , is within experimental error. The 11deviation between experiments and theory increases with increasing current 12density. Further work is needed to resolve this discrepancy. In Fig. 10b, we 13plot Φ_{exp}/L versus m_{av} for $i_{ss} = 0.4$ mA/cm². Φ_{exp}/L is a weak function of m_{av} . 14Theoretical predictions, also shown in Fig, 10b, support this observation. 15While the theoretical predictions generally lie below the experimental data, 16they are within experimental error at $m_{av} = 0.60$ and 1.30 mol/kg.



2Figure 10: Experimental (black) and model predicted (blue) potential as a 3funtion of (a) i_{ss} for a concentration of $m_{av} = 0.94$ mol/kg and (b) m_{av} for $i_{ss} = 40.40$ mA/cm².

6Figure 11 shows the comparison between the experimentally measured and 7predicted time evolution of cell potential based on the transient model (Table 81) using the same thermodynamic and transport parameters used in the 9analysis of steady-state data presented in Figs. 2-10. The transient model, as 10described in Table 1, is used for the numerical predictions of cell potential for 11different average salt concentrations of $m_{av} = 0.60$ mol/kg ($c_{av} = 8.89 \times 10^{-4}$ 12mol/cm³), $m_{av} = 0.94$ mol/kg ($c_{av} = 1.36 \times 10^{-3}$ mol/cm³), and $m_{av} = 1.30$ 13mol/kg ($c_{av} = 1.70 \times 10^{-3}$ mol/m³). The experimental results, denoted by the 14solid curves, are obtained from averaged potentials measured from three 15separate cells; whereas, the highlighted regions show the range of measured 16potentials across the cells. The dashed curves indicate the transient model 17results. As shown in Figure 11a and b, the transient model predictions are in 18quantitative agreement with experiments at all applied current densities for $1m_{av} = 0.60$ and 0.94 mol/kg. The theoretical and experimental potential 2jumps at $t = 0^+$ are in agreement, as is the approach to steady-state wherein 3the cell potential increases with time as concentration gradients develop. 4The agreement between theory and experiment is only qualitative at $m_{av} = 51.30$ mol/kg (Figure 11c). While the time-scale over which concentration 6gradients develop are similar in both theory and experiment, both the 7instantaneous potential at $t = 0^+$ and the steady-state potential measured 8experimentally are higher than theoretical predictions. While it is not clear 9why this discrepancy is seen at $m_{av} = 1.30$, the agreement between the 10model and the data seen in Figure 11 is noteworthy, as there are no 11adjustable parameters in the model.



2Figure 11: Time dependent experimental potentials (solid curves) are 3compared to our transient model (dashed curves) for litihium symmetric 4cells. The experimental data was averaged from three replicate cells (solid 5curves) and the error is given by the standard deviation (light shaded areas). 6Transient potential behavior for $i_{ss} = 0.02$, 0.20, and 0.40 mA/cm² for (a) m_{av} 7= 0.60 mol/kg, (b) $m_{av} = 0.94$ mol/kg, and (c) $m_{av} = 1.30$ mol/kg. 8

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25. Conclusion

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3The performance of an electrolyte in a battery is limited, in part, by the 4maximum current that can be drawn through it. Traditionally, this maximum 5 s calculated by predicting salt concentration profiles as a function of current 6density and noting the current density at which the salt concentration at the 7cathode is zero. Another limitation arises when the salt concentration at the 8anode exceeds the solubility limit. Our analysis considers both possibilities. 9We have used Newman's concentrated solution theory to predict steady-10state salt concentration profiles as a function of current density for mixtures 11of C8-DMC and LiFSI. These predictions were enabled by the complete 12electrochemical characterization of these mixtures (i.e., measurement of κ , 13D, t_{+i^0i} and T_f as functions of salt concentration) that was reported in ref. 19. 14An interesting feature of these electrolytes is that t_{+i^0i} is negative across all 15salt concentrations. The dc potential across Li symmetric cells containing C8-16DMC/LiFSI was measured experimentally as a function of applied current 17density and salt concentrations. At high enough current densities, clear 18 signatures of the limiting current were observed. The experimentally 19determined limiting current was a non-monotonic function of salt 20concentration. It increases with increasing salt concentration up to $m_{av} =$ 210.94 mol/kg and decreases with increasing salt concentration at higher 22values of m_{av} . The solubility limit of LiFSI in C8-DMC is 2.03 mol/kg. Our 23theoretical analysis indicates that the limiting current, up to $m_{av} = 0.88$

1mol/kg, occurs due to depletion of salt at the cathode, while the limiting 2current at higher values of m_{av} occurs due to the salt saturation at the anode. 3The experimentally determined time dependence of the potential across the 4lithium symmetric cells was also compared to predictions based on 5Newman's concentrated solution theory. Our approach enables comparing 6theory with experiment with no adjustable parameters.

Conflicts of interest

2There are no conflicts to declare.

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Acknowledgements

2This work was intellectually led by the Joint Center for Energy Storage 3Research (JCESR), an Energy Innovation Hub funded by the U.S. Department 4of Energy (DOE), Office of Science, Basic Energy sciences (BES), under 5Contract No. DEAC02-06CH11357. Early work by D.B.S. was supported by the 6National Science Foundation, grant number 1505669, under the SusChEM 7initiative. We thank Dr. Kevin R. Olson, Dr. Sue J. Mecham, and Prof. Joseph 8M. DeSimone for their helpful guidance in synthesizing C8-DMC.

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1		Nomenclature
2		
_	A	Active surface area of electrode (cm ²)
	С	Concentration (mol/cm ³)
	D	Salt diffusion coefficient of electrolytic phase (cm ² /s)
	D_s	Salt diffusion coefficient of electrolyte in separator (cm ² /s)
	F	Faraday's constant (96,485 C/mol)
	i _{ss}	Steady-state current density (mA/cm ²)
	i _{limit}	Limiting current density (mA/cm ²)
	i _{limit , sat}	Limiting current density due to salt precipitation (mA/cm ²)
	L	Thickness of electrolyte/separator (cm)
	т	Molality (mol/kg)
	R	Ideal gas constant (J/mol K)
	R_{i}	Resistance of electrolyte/electrode interface when i_{ss} is reached (Ω)
	Т	Temperature (K)
	T_{f}	Thermodynamic factor
	t	Time (s)
	t _{+ 2° i}	Cation transference number relative to the solvent velocity. Obtained using the Balsara and Newman method
	$t_{-\iota^{0}\iota}$	Anion transference number relative to the solvent velocity; $t_{-i^0=1-t_{i,0}i}$
	$t_{+,id}$	Ideal transference number using steady-state current method
	X	Position (cm)
	Z_{-ii}	Anion charge
~	$1 + \frac{dln\gamma_{\pm}}{dlnm}$	Thermodynamic factor
3		
4(Greek	Maan malal activity as officiant of the solt
	γ_{\pm}	Mean molal activity coefficient of the salt
	K	Conductivity of the electrolytic phase; (S/cm)
	K _s	Conductivity of the electrolyte and separator combined; (S/cm)
	Vi	Number of cations/anions per molecule of salt ($i=+or-i$)
	Φ	Electrolyte potential (mV)
	$oldsymbol{\Phi}_{exp}$	Experimental electrolyte potential (mV)

- $\Phi_{measured}$ Measured cell potential (mV)
- Φ_0 Steady-state model predicted electrolyte potential taken at x = 0 (mV)

1Table of Contents Graphic

