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Publication Date

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**Development of the Non-Equilibrium Reactive
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J. Noorishad, C.L. Carnahan, and L.V. Benson

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DEVELOPMENT OF THE
NON-EQUILIBRIUM REACTIVE CHEMICAL TRANSPORT CODE
CHMTRNS

by

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September 1987

This work was done with support from the
U.S. Department of Energy under Contract No. DE-AC03-76SF00098

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ABSTRACT

A temperature-dependent non-equilibrium reactive chemical transport code has been developed on the basis of earlier work at Lawrence Berkeley Laboratory. The code is capable of simulating kinetic calcite and silica dissolution, irreversible glass dissolution, oxidation and reduction, and stable carbon isotope fractionation during transport. In the main part of the report necessary fundamentals and related algorithms are presented. Appendices 1-10 provide samples of inputs and outputs of solved problems. Appendices 11 and 12 include, respectively, the input preparation guide and the Fortran IV listing of the developed code CHMTRNS.

INTRODUCTION

Most reactive solute transport codes incorporate the assumption of chemical equilibrium (e.g., Miller and Benson, 1983; Kirkner et al., 1984; Cederberg, 1985; Carnahan, 1987a,b). The limits of validity of the local chemical equilibrium assumption have been explored to some degree (e.g., Palciauskas and Domenico, 1976; James and Rubin 1979), but further work is needed before the limits can be established on a firm basis. At this time, it is clear that imposing the equilibrium constraint on chemical reactions is a serious deficiency when modeling certain chemical systems. For example, comparison of theoretical computer simulations which assume chemical equilibrium with observed geothermal fluid compositions and mineral assemblages can reveal dissimilarities that are indicative of kinetic hindrance of certain reactions (Vallette-Silver et al., 1981).

For many chemical problems the slowness of reaction rates necessitates the implementation of kinetic calculations. Here, computer codes (e.g., Kirkner et al., 1985) that can simulate chemical reaction kinetics are only means to achieve realistic modeling time dependent phenomena. In the following the development of the non-isothermal, non-equilibrium, reactive chemical transport code CHMTRNS is described. This code, which is an outgrowth of the reactive chemical transport code CHEMTRN (Miller and Benson, 1983), can simulate the kinetic dissolution or precipitation of calcite and silica as well as irreversible dissolution of glass. Thermodynamic parameters are temperature dependent and are coupled to a companion heat transport simulator; thus, the effects of transient temperature conditions can be considered. Oxidation and

reduction and fractionation of carbon isotopes are also options in CHMTRNS. The performance of the code CHMTRNS is illustrated in a number of simulations. The inputs and outputs, which exhibit the details of the solved cases, and at the same time serve as guides for setting up problems for solution by CHMTRNS, are given in the Appendices.

THEORETICAL BASIS

Equilibrium Formulation

The chemical transport algorithm in CHMTRNS follows that of the CHEMTRN code (Miller and Benson, 1983). However, the re-equilibration process for reversible dissolution-precipitation of solids used in CHEMTRN has been replaced by a simpler algorithm which allows determination of solid variations simultaneously with solution of the transport equations. Treatment of Neuman and Dirichlet boundary conditions and the mesh generation schemes have also been changed. An optional upstreaming capability replaces the fixed upstream algorithm. This flexibility prevents convergence problems in low ranges of Peclet number where upstreaming is not correct.

The mass balance equation for any species j can be written as

$$L \left[C_{bj} + \sum_{i=1}^{N_c} a_{ij} C_{ci} \right] + \frac{\partial}{\partial t} \left[\bar{C}_{bj} + \sum_{i=1}^{\bar{N}_c} a_{ij} \bar{C}_{ci} \right] + \sum_{i=1}^{N_p} s_{ij} \frac{\partial C_{pi}}{\partial t} = 0 \quad ,$$

$$j = 1, \dots, N_b \quad , \quad (1)$$

where the operator L is defined by

$$L() = \frac{\partial}{\partial t} () + \nabla \cdot (() \mathbf{V} - D \nabla ()) \quad ,$$

and

C_{bj} is the concentration of basis ion j , mol/liter

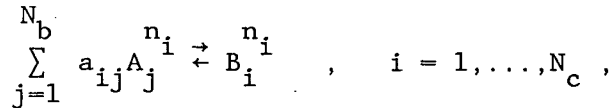
\bar{C}_{bj} is the concentration of sorbed basis ion j , mol/liter of fluid phase

C_{ci} is the concentration of complex ion i , mol/liter

\bar{C}_{ci} is the concentration of sorbed complex ion i , mol/liter of fluid phase

C_{pi} is the concentration of solid i , mol/liter of fluid phase
 a_{ij} are the stoichiometric coefficients for formation of complex i
 s_{ij} are the stoichiometric coefficients for formation of solid i
 V is the fluid velocity vector equal to Darcy velocity divided by porosity ϕ
 D is the longitudinal dispersion coefficient
 N_b is the number of basis species
 \bar{N}_b is the number of sorbed basis species
 N_c is the number of aqueous complexes
 \bar{N}_c is the number of sorbed complexes
 N_p is the number of solids.

The mass action equation for the complexation reaction expressed as

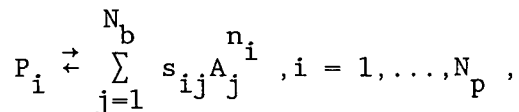


is

$$[B_i^{n_i}] = K_{ci} \prod_{j=1}^{N_b} [A_j^{n_j}]^{a_{ij}}, \quad i = 1, \dots, N_c, \quad (2)$$

where $[B_i^{n_i}] = \gamma_i C_{ci}$, $[A_j^{n_j}] = \gamma_j C_{bj}$, γ_i = activity coefficient of aqueous species i calculated by the Davies equation (Stumm and Morgan, 1970), n_i and n_j are the charges of the species i , j , and K_{ci} is the equilibrium constant for formation of the complex B_i .

For reversible dissolution of a solid expressed as

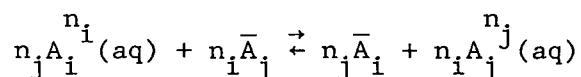


the mass action equation is

$$1 = \frac{1}{K_{P_i}} \prod_{j=1}^{N_b} [A_j]^{n_j s_{ij}}, \quad i = 1, \dots, N_p \quad (3)$$

where K_{P_i} is the solubility product of the solid P_i .

For sorption by ion exchange¹ expressed as



the algebraic equation is

$$[\bar{A}_i]^{n_j} [A_j]^{n_i} = K_{ij} [A_i]^{n_j} [\bar{A}_j]^{n_i} \quad (4)$$

where K_{ij} is the equilibrium constant, for the exchange reaction as written, A_i and A_j are activities of aqueous complexes or basis species, and \bar{A}_i and \bar{A}_j refer to activities of the sorbed species. The activity of a sorbed species \bar{C}_j is estimated as \bar{C}_j / \bar{C}_T , where \bar{C}_T is the total concentration of sorbed species given by

$$\bar{C}_T = \sum_{j=1}^{\bar{N}_b} \bar{C}_{bj} + \sum_{i=1}^{\bar{N}_c} \bar{C}_{ci}$$

In this sorption model it is assumed that the number of equivalents surface sites per unit volume of solution available for ion exchange, referred to as N_s , is constant. Thus,

¹The algorithm for surface complexation (Davis et al., 1978) is also included in CHMTRNS in its original form taken from CHEMTRN.

$$N_s = \sum_{j=1}^{\bar{N}_b} n_j \bar{C}_{bj} + \sum_{i=1}^{\bar{N}_c} n_i \bar{C}_{ci} \quad (5)$$

Variations of pH are treated by the method used in CHEMTRN. Because CHEMTRN and CHMTRNS both consider dilute solutions, it is assumed that the total mass of water (H_2O) is affected negligibly by chemical reactions, and H_2O is not included as a chemical species. However, a transport equation written for either H^+ or OH^- individually would necessarily include terms involving H_2O . To avoid this, the complete transport equation for OH^- is subtracted from the one for H^+ ; the result is

$$L \left[y + \sum_{i=1}^{\bar{N}_c} \left(a_{i,H^+} - a_{i,OH^-} \right) C_{ci} \right] + \frac{\partial}{\partial t} \left[\bar{C}_{H^+} + \sum_{i=1}^{\bar{N}_c} a_{i,H^+} \bar{C}_{ci} \right] + \sum_{i=1}^{\bar{N}_p} \left(s_{i,H^+} - s_{i,OH^-} \right) \frac{\partial C_{pi}}{\partial t} = 0, \quad (6)$$

where the new variable, y , is defined by

$$y = C_{H^+} - C_{OH^-}.$$

The other equation needed to determine both C_{H^+} and C_{OH^-} is the mass action equation for ionization of H_2O :

$$K_w = [H^+][OH^-],$$

where K_w is the ion product H_2O , the square brackets denote activities, and the activity of H_2O is assumed equal to unity.

Non-Equilibrium Formulation

The partial differential equation of dispersive-advective mass transport does not change fundamentally for consideration of non-equilibrium chemical reactions. If basis species are produced or consumed irreversibly at a finite rate, as in kinetic dissolution of glass, a source term must be added to the transport equation for each basis species involved in the irreversible reaction. Thus, Eq. (1) becomes

$$L \left[C_{bj} + \sum_{i=1}^{N_c} a_{ij} C_{ci} \right] + \frac{\partial}{\partial t} \left[\bar{C}_{bj} + \sum_{i=1}^{\bar{N}_c} a_{ij} \bar{C}_{ci} \right] + \sum_{i=1}^{N_p} s_{ij} \frac{\partial C_{pi}}{\partial t} + \delta_{kj} \nu_{kb} R_b = 0, \quad j = 1, \dots, N_b, \quad (8)$$

where \underline{k} refers to basis species involved in the reaction and has one or more discrete values in the range $1, \dots, N_b$, δ_{kj} is the Kronecker delta function, ν_{kb} is the stoichiometric coefficient of basis species k in the reaction, and R_b is the rate of the reaction.

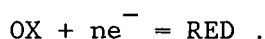
On the other hand, if complexes or solids participate in non-equilibrium reactions and if no mass enters or leaves the system irreversibly, then Eq. (1) is used without modification. However, the mass action equations (2) or (3) for each participating complex or solid must be replaced by rate equations of the type

$$\frac{\partial}{\partial t} (X_i) = -R_{X_i}, \quad (9)$$

where X_i represents the concentration of a complex or a solid and R_{X_i} is the appropriate rate. The mass action equations for non-participating complexes and solids remain unchanged.

Oxidation-Reduction Reactions

Oxidation-reduction reactions are treated by defining a hypothetical electron activity as a basis species subject to transport as are other aqueous basis species (Carnahan, 1987b). For multivalent elements, a species in the highest oxidation state is chosen to be the basis species. Reduction to a lower oxidation state is described formally by a half-cell reaction in which the higher valent species "reacts" with hypothetical electrons to form the lower-valent species. The general form of the half-cell reaction with transfer of n electrons is



The corresponding mass action equation is

$$[\text{RED}] = K[\text{OX}] a_e^n ,$$

where K is the equilibrium constant, square brackets denote activities, and a_e is the hypothetical electron activity. This process is analogous to the process by which aqueous complexes are formed by reactions between basis species. Thus, the reduced species are treated as though they are complexes of oxidized species with electrons. The electron activity is related to E_h , the oxidation potential on the hydrogen scale, by

activity is related to Eh, the oxidation potential on the hydrogen scale, by

$$a_{e^-} = \exp\left(\frac{F Eh}{RT}\right),$$

where F is the Faraday constant, R is the gas constant, and T is absolute temperature. It is noted that the electron activity is an artifice that allows treatment of reduction in the same manner as complexation; there is no implication that free electrons exist in aqueous solution.

Carbon Isotope Fractionation

Chemical reactions involving ^{13}C -rich carbonate rocks will change the relative amounts of the isotopes ^{13}C and ^{12}C within individual carbonate aqueous species. These changes are expressed as changes of the isotopic ratio, R_i , in species i, defined by

$$R_i = \frac{{}^{13}\text{C}_i}{{}^{12}\text{C}_i},$$

where the notation ${}^m\text{C}_i$ denote the concentration of that fraction of species i containing the isotope of mass m. Changes of R_i are measured by the isotopic shift, δ_i , defined by

$$\delta_i = 10^3 \left(\frac{R_i}{R_{\text{PDB}}} - 1 \right),$$

where R_{PDB} is the isotopic ratio of a standard.

To formulate the equations of change of isotopic composition during transport, we consider the aqueous species CO_3^{2-} , HCO_3^- , and H_2CO_3^0 and the solid $\text{CaCO}_3(\text{c})$ (calcite), and denote their respective concentrations by

C_2 , C_1 , C_0 , and C_s . The transport equation for these species is then

$$L(C_0 + C_1 + C_2) + \frac{\partial C_s}{\partial t} = 0$$

or

$$L(C_T) + \frac{\partial C_s}{\partial t} = 0, \quad (11)$$

where $C_T = C_0 + C_1 + C_2$. We can write also,

$$L({}^{13}C_0 + {}^{13}C_1 + {}^{13}C_2) + \frac{\partial {}^{13}C_s}{\partial t} = 0. \quad (12)$$

Because ${}^{13}C_i \ll {}^{12}C_i$, we have a good approximation

$${}^{13}C_i = R_i C_i, \quad i = 0, 1, 2, s. \quad (13)$$

Also,

$$R_i = R_{\text{PDB}} (10^{-3} \delta_i + 1) \quad (14)$$

The net isotopic shift of the fluid, δ_{sol} , is defined by

$$\sum_{i=0}^2 C_i \delta_i = C_T \delta_{\text{sol}} \quad (15)$$

We adopt the calcite precipitation mechanism proposed by Plummer et al.,

(1978), in which $\text{CaCO}_3(\text{c})$ precipitates directly from $\text{HCO}_3^-(\text{aq})$. Then,

substituting Eqs. (13) and (14) into (12) and using Eqs. (11) and (15)

gives

$$L(C_T \delta_{\text{sol}}) + \frac{\partial}{\partial t} (\delta_x C_s) = 0, \quad (16)$$

where

$$\delta_x = \delta_s \quad \text{if} \quad \frac{\partial C_s}{\partial t} < 0 \quad (\text{dissolution case}) ,$$

$$\delta_x = \delta_1 \quad \text{if} \quad \frac{\partial C_s}{\partial t} > 0 \quad (\text{precipitation case}) .$$

In the case of dissolution where carbonate from the rock is added to the solution Eq. (16) becomes

$$L(C_T \delta_{\text{sol}}) + \delta_s \frac{\partial C_s}{\partial t} > 0 . \quad (17)$$

Combining Eqs. (17) and (11) we obtain

$$L(\theta_d) = 0 \quad (18)$$

where

$$\theta_d = (\delta_{\text{sol}} - \delta_s) C_T$$

In the case of precipitation we can expand Eq. (16) to

$$L(C_T \delta_{\text{sol}}) + \delta_1 \frac{\partial C_s}{\partial t} + C_s \frac{\partial \delta_1}{\partial t} = 0 . \quad (19)$$

The shift of the bicarbonate species, δ_1 , originating from fractionation during dissolution of $\text{CO}_2(\text{gas})$ in water, can be referenced to δ_{CO_2} in the following manner. We have

$$R_{\text{CO}_2} = R_{\text{PDB}} (10^{-3} \delta_{\text{CO}_2} + 1) .$$

The partition coefficients, α_i , are defined by

$$\alpha_i = \frac{R_i}{R_{\text{CO}_2}} , \quad i = 0, 1, 2 ,$$

where i refers to H_2CO_3^0 , HCO_3^- and CO_3^{2-} respectively. Then, using Eq. (14),

$$\delta_i = \alpha_i \delta_{\text{CO}_2} + 10^3 (\alpha_i - 1) \quad , \quad i=0,1,2 \quad . \quad (20)$$

We can also reference the aqueous carbonate species to each other and eliminate δ_{CO_2} from Eq. (20). If we choose H_2CO_3^0 ($i=0$) as the reference species we get

$$\delta_1 = \frac{\alpha_1}{\alpha_0} \delta_0 + 10^3 \left[\frac{\alpha_1}{\alpha_0} - 1 \right] = A_1 \delta_0 + A_2 \quad , \quad (21a)$$

$$\delta_2 = \frac{\alpha_2}{\alpha_0} \delta_0 + 10^3 \left[\frac{\alpha_2}{\alpha_0} - 1 \right] = A_3 \delta_0 + A_4 \quad . \quad (21b)$$

Substituting Eqs. (21a) and (21b) into Eq. (15) and solving for δ_0 gives

$$\delta_0 = \frac{C_T \delta_{\text{sol}} - 10^3 \left[C_1 \left(\frac{\alpha_1}{\alpha_0} - 1 \right) + C_2 \left(\frac{\alpha_2}{\alpha_0} - 1 \right) \right]}{C_0 + \left[\frac{\alpha_1}{\alpha_0} \right] C_1 + \left[\frac{\alpha_2}{\alpha_0} \right] C_2} = \frac{C_T \delta_{\text{sol}} - A_5}{A_6} \quad (22)$$

Defining $\theta_p = C_T \delta_{\text{sol}}$ and substituting Eq. (22) into Eq. (21a) we obtain

$$\delta_1 = \frac{A_1}{A_6} \theta_p - \left[\frac{A_1 A_5}{A_6} - A_2 \right] = A_7 \theta_p + A_8 \quad (23)$$

where all A_i parameters are defined in terms of concentrations of carbonate species and α_i $i = 0,1,2$. The latter partition coefficients are given (Deines et al., 1974) as functions of absolute temperature, T , by

$$\ln \alpha_0 = -0.91 \times 10^{-3} + 6.3/T^2$$

$$\ln \alpha_1 = -4541 \times 10^{-3} + 1099/T^2$$

$$\ln \alpha_2 = -3.4 \times 10^{-3} + 870/T^2$$

Substituting Eq. (23) into Eq. (19) results in

$$L(\theta_p) = (A_7\theta_p + A_8) \frac{\delta C_s}{\delta t} + C_s \frac{\delta}{\delta t} (A_7\theta_p + A_8) \quad (24)$$

Equation (18) and (24) are partial differential equations of transport for the new variables θ_d and θ_p that keep track of $\delta^{13}C$ in the solution, in cases of dissolution or precipitation of calcite respectively.

Unlike Eq. (18), Eq. (24) (which can be further rearranged by explicit writing of the L operator) is a nonlinear equation coupled to the other reactive transport equations through the dependence of the "A_i" parameters on the concentrations of carbonate species. However, the solution of Eqs. (18) and (24) poses no difficulty and has been implemented along the same lines of approach explained in the section on the numerical solution of the reactive transport problem.

Heat Transport Formulation

The formulations presented so far are generally based on the assumption of isothermal conditions. However, considering the role of variation of temperature in many geochemical processes, it is necessary to include thermal effects in chemical reactions and to formulate heat transport as a companion to mass transport. Removing the restriction of constancy of temperature does not alter the mass transport formulation in any way. The only necessary addition is to formulate the functional relationship between the thermodynamic constants and temperature. The

relationship used has the thermodynamic equation of Clarke and Glew (1966):

$$\log_{10}K = A + \frac{B}{T} + C \log_{10}T + DT$$

where K is the thermodynamic equilibrium constant used in any mass action relation, A, B, C and D are parameters that vary for different chemical reactions, and T is the absolute temperature.

The governing equation of heat transport is

$$(\rho C)_M \frac{\partial T}{\partial t} + \phi \rho_\ell C_{v\ell} \mathbf{V} \cdot \nabla T - \nabla \cdot (K_M \nabla T) + Q = 0, \quad (25)$$

where

$$(\rho C)_M = \phi \rho_\ell C_{v\ell} + (1 - \phi) \rho_s C_{vs},$$

$$K_M = \phi K_\ell + (1 - \phi) K_s,$$

$$\rho_\ell = \rho_0 + \beta_t (T - T_0),$$

in which $C_{v\ell}$ and C_{vs} are fluid and solid specific heat capacities at constant volume, ρ_ℓ is the liquid mass density, K_ℓ and K_s are the thermal conductivities of the fluid and the solid, β_t is the fluid thermal expansion coefficient, ϕ is the porosity of the medium, and ρ_0 and T_0 are the initial fluid density and temperature, and v is the pore fluid velocity.

SOLUTION APPROACH

Differential Eqs. (8) for mass balance and aqueous species transport, rate Eq. (9) for non-equilibrium chemical reactions, differential Eq. (6) for transport of hydrogen and hydroxide ions, differential Eqs. (18) or (24) for isotopic fractionation tracking during transport, algebraic Eqs. (2)-(5) for equilibrium complexation, dissolution or precipitation, and ion exchange, algebraic Eq. (10) for oxidation-reduction reactions, and finally Eq. (25) for dispersive-conductive heat transport, provide the complete set of differential-algebraic equations for the coupled processes of non-isothermal equilibrium and non-equilibrium reactive chemical transport with oxidation-reduction and carbon isotope tracking options. Because of its complexity, the set of equations is only amenable to numerical solution. One-way coupling between the energy equation and the other equations makes an interlaced solution approach possible. With this approach, the differential-algebraic equations of chemical transport are solved separately from the heat equation. Temperatures calculated from the solution of the heat equation at each time level are used to update all temperature-dependent parameters for the next time step, and this scheme continues through the solution. The usually large time constant of the heat equation eliminates the need for iteration between the heat and transport equations.

Detailed one-dimensional space and time discretization of the reactive chemical transport equations will be addressed in this section. Because the heat transport equation is very similar to the mass transport equation, with the exception of parameters, no separate explanation is offered. However, as will be discussed later, the solution

method for the heat equation is much simpler because of the justifiable assumption of its linearity.

Space and Time Discretization

For a one-dimensional finite difference numerical solution we can choose either a uniform or nonuniform spatial discretization of the flow path. For uniform discretization, the location, x_i , of finite difference node i is computed from

$$x_i = \frac{i}{N-1} L_p \quad , \quad i = 1, \dots, N \quad ,$$

while for nonuniform discretization x_i is computed from

$$x_i = \frac{d \binom{i-1}{N-1} - 1}{d-1} L_p \quad , \quad i = 1, \dots, N \quad ,$$

where L_p is the flow path length, N is the number of finite difference nodes, and d is an arbitrary number. If d is chosen to be greater than one, the interval $x_i - x_{i-1}$ increases as x_i increases.

The reactive mass transport equations are approximated by replacing first the spatial derivatives with finite difference approximations.

Using

$$W_{j,n} = \left(C_{bj} + \sum_{i=1}^{N_c} a_{ij} C_{ci} \right)_n \quad (26)$$

$$\bar{W}_{j,n} = \left(\bar{C}_{bj} + \sum_{i=1}^{\bar{N}_c} a_{ij} \bar{C}_{ci} \right)_n \quad (27)$$

to represent respectively the total masses of aqueous and adsorbed

species at grid point n, the transport Eq. (8) is rewritten as

$$\begin{aligned}
& \frac{d}{dt} W_{j,n} + \frac{d}{dt} \bar{W}_{j,n} + \frac{d}{dt} \sum_{i=1}^{N_p} s_{ij} C_{Pi,n} \\
& + V \left[\left((1 - \gamma) \frac{x_n - x_{n-1}}{x_{n+1} - x_{n-1}} \right) \left(\frac{C_n^{\ell+1} - C_{n-1}^{\ell+1}}{x_n - x_{n-1}} \right) \right. \\
& \left. + \left(\gamma \frac{x_n - x_{n-1}}{x_n - x_{n-1}} \right) \left(\frac{C_{n+1}^{\ell+1} - C_n^{\ell+1}}{x_{n+1} - x_n} \right) \right] \\
& + \frac{D}{0.5*(x_{n+1} - x_{n-1})} \left[\left(\frac{W_{j,n+1}^{\ell+1} - W_{j,n}^{\ell+1}}{x_{n+1} - x_n} \right) - \left(\frac{W_{j,n}^{\ell+1} - W_{j,n-1}^{\ell+1}}{x_n - x_{n-1}} \right) \right] \\
& + \delta_{kj} \nu_{kb} R_b = 0 \quad , \quad j = 1, \dots, N_b, \quad n = 1, \dots, N \quad , \quad (28)
\end{aligned}$$

where $\ell + 1$ refers to the time level in which we seek a solution and γ is an upwind parameter between zero and one. Equations (2)-(5) and (9) remain basically the same except that they are referred to grid points:

$$[B_{i,n}^n] = K_{C_{i,n}} \prod_{j=1}^{N_b} [A_{j,n}^n]^{a_{ij}} \quad , \quad i = 1, \dots, N_c \quad , \quad n = 1, \dots, N \quad , \quad (29)$$

$$1 = \frac{1}{K_{Pi,n}} \prod_{j=1}^{N_b} [A_{j,n}^n]^{s_{ij}} \quad , \quad i = 1, \dots, N_p \quad , \quad n = 1, \dots, N \quad , \quad (30)$$

$$[\bar{A}_{i,n}]^{n_j} [A_{j,n}]^{n_i} = K_{ij,n} [A_{i,n}]^{n_j} [\bar{A}_{j,n}]^{n_i} \quad n = 1, \dots, N, \quad (31)$$

$$N_s = \sum_{j=1}^{\bar{N}_b} n_j \bar{C}_{bj,n} + \sum_{i=1}^{\bar{N}_c} n_i \bar{C}_{ci,n} \quad n = 1, \dots, N, \quad (32)$$

$$\frac{d}{dt} (X_{i,n}) = -R_{X_{i,n}}, \quad n=1, \dots, N. \quad (33)$$

For the sake of clarity we omit writing discretized forms of Eqs. (7) and (10), which will be similar to Eqs. (30) and (29), respectively. Because of their temperature dependence, the equilibrium constants have also been indexed. Among the above equations, only Eqs. (28) and (33) will require time discretization as well. Using a backward Euler's method (fully implicit) the time derivatives are approximated as follows:

$$\frac{d}{dt} W_{j,n} \approx \frac{W_{j,n}^{\ell+1} - W_{j,n}^{\ell}}{\Delta t}$$

$$\frac{d}{dt} \bar{W}_{j,n} \approx \frac{\bar{W}_{j,n}^{\ell+1} - \bar{W}_{j,n}^{\ell}}{\Delta t}$$

$$\frac{d}{dt} C_{Pi,n} \approx \frac{C_{Pi,n}^{\ell+1} - C_{Pi,n}^{\ell}}{\Delta t}$$

$$\frac{d}{dt} X_{i,n} = \frac{X_{i,n}^{\ell+1} - X_{i,n}^{\ell}}{\Delta t} \quad (34)$$

Equations (28)-(33) in conjunction with the time discretization expressions in Eq. (34) are a set of strongly nonlinear simultaneous

algebraic equations that can be written in matrix form as

$$F(\underline{X}) = A(\underline{X}) \underline{X} - B(\underline{X}) = 0 \quad (35)$$

where F is the residue vector, \underline{x} is the vector of unknowns, A and B are coefficient matrices, the number of unknowns, N_x , is equal to

$$N_x = (N_b + N_c + \bar{N}_b + \bar{N}_c + N_p) * N$$

and N is the number of grid points.

In the above discretization we used Cartesian coordinates. However, discretization for axially symmetric space can be achieved simply by replacing x_n , V and D in Eq. (28) with r_n , $V_0 \frac{R}{r_n}$ and $D = D(r_n)$ respectively where V_0 is the pore fluid velocity at radius R . The final discretized form of equations [i.e., Eq. (35)] will not be affected. Discretization of the heat equation can be performed similarly, leading to a set of simultaneous equations of the general form of Eq. (35). For the small temperature variations considered here the extent of non-linearity in the heat equations is small. Hence, we assume linearity of Eq. (35) for heat transport.

Implementation of Boundary Conditions

In dealing with boundary conditions the main concern is proper treatment of the spatial derivatives. In the following derivations we illustrate the method by using a simple form of Eq. (1) for a single species of concentration C and consider a backward time difference scheme.

Constant flux boundary condition (Crank, 1975) - Consider a boundary B at $x=0$ where the following governing equation of transport and flux boundary condition hold:

$$\frac{\partial C}{\partial t} - D \frac{\partial^2 C}{\partial x^2} + v \frac{\partial C}{\partial x} = 0 \quad (36)$$

$$\left[-D \frac{\partial C}{\partial x} + vC \right]_{x=0} = F \quad (37)$$

where F is the prescribed flux at the boundary. Using the difference approximations in the above equations at the boundary B results in

$$\frac{C_0^\ell - C_0^{\ell-1}}{\Delta t} - \frac{D}{(\Delta x)^2} (C_{-1}^\ell - 2C_0^\ell + C_1^\ell) + \frac{v}{2\Delta x} (C_1^\ell - C_{-1}^\ell) = 0 \quad (38)$$

$$C_{-1}^\ell = C_1^\ell + \frac{2\Delta x}{D} (F - vC_0^\ell) \quad (39)$$

where indices -1 , 0 and 1 designate an image node, the boundary node, and the first internal node, and Δx is the discretization distance, assumed uniform in this illustration. Combining Eqs. (38) and (39) to eliminate C_{-1}^ℓ and rearranging we obtain

$$\frac{C_0^\ell - C_0^{\ell-1}}{\Delta t} - 2D \left[\frac{C_1^\ell - C_0^\ell}{(\Delta x)^2} \right] + \left[\frac{vC_0^\ell - F}{\Delta x} \right] + \left[2 + \frac{v\Delta x}{D} \right] = 0 \quad (40)$$

Eq. (40) is the discretized form of the transport equation at the boundary B. For axially symmetric radial mass transport, we use the same arrangement for the imaginary point except that Δr replaces Δx . In this case the governing equation and boundary flux condition are given in the following form

$$\frac{\partial C}{\partial t} - D(r) \frac{\partial^2 C}{\partial r^2} + \left[V(r) - \frac{D_d}{r} \right] \frac{\partial C}{\partial r} = 0 , \quad (41)$$

$$\left[-D(r) \frac{\partial C}{\partial r} + V_c \right]_{r=R} = F , \quad (42)$$

where R is the radial coordinate of the boundary point B, D(r) is equal to $\partial_L V(r) + D_d$, ∂_L is longitudinal dispersivity, D_d is the molecular diffusion coefficient, V(r) is equal to $V_0 \frac{R}{r}$, and V_0 is the pore fluid velocity at the boundary. Again using difference approximations in Eqs. (41) and (42) and eliminating the image concentration value we obtain

$$\frac{C_0^\ell - C_0^{\ell-1}}{\Delta t} - 2D(R) \left[\frac{C_1^\ell - C_0^\ell}{(\Delta r)^2} \right] + \left[\frac{VC_0^\ell - F(R)}{\Delta r} \right] \left[2 + \frac{V_0 \Delta r}{D(R)} - \frac{D_d \Delta r}{RD(R)} \right] = 0 , \quad (43)$$

which is the discretized form of the governing equation at a flux boundary point. With exception of the contribution of D_d in the last term, the Eqs. (43) and (40) have the same form. Either of these equations replace the part of Eq. (28) related to mobile species, with C_0^ℓ and C_1^ℓ being replaced by $W_{j,1}^{\ell+1}$ and $W_{j,2}^{\ell+1}$ respectively, for boundary condition implementation.

Constant concentration boundary conditions - Implementation of this condition requires only simple manipulation of the matrix equations, Eq. (35). The equations for the known concentration boundary conditions are simply decoupled from those for the neighboring points. In the direct solution method used here it is enough to make all the

nondiagonal terms very small and the diagonal terms in the A matrix equal to unity. In the Newton-Raphson method, discussed later, we reduce both the residue for the corresponding boundary equations and the nondiagonal terms to very small quantities, thus assuring a correction closer to zero for the known quantities.

Solution Methods

As discussed earlier, time and space discretization of the governing equations for both reactive chemical transport and heat transport lead to matrix equations of the form presented in Eq. (35). For heat transport we have used the Crank-Nicholson approximation rather than fully implicit methods; however, the final form is the same. The almost linear form of the equations for heat transport, due to small variations of A and B during a time step, makes them amenable to a one-step direct solution method. We used an LU decomposition and backward substitution solution procedure in conjunction with the tridiagonal form of these equations.

In case of the reactive chemical transport equations, the strong nonlinearity of Eq. (35) makes the use of an iterative scheme imperative. We have used a generalized Newton-Raphson method which leads to following solution algorithm for Eq. (35):

$$\underline{X}_i = \underline{X}_{i-1} - \Delta \underline{X}_i \quad (44)$$

$$\underline{J}(\underline{X}_{i-1}) \Delta \underline{X}_i = \underline{F}(\underline{X}_{i-1}) \quad (45)$$

$$\underline{J}(\underline{X}_{i-1}) = \left[\frac{\partial}{\partial \underline{X}} F(\underline{x}) \right]_{i-1} \quad (46)$$

where i represents the iteration level and the Jacobian \underline{J} is a function of both time and space. In the CHMTRNS approach \underline{J} is evaluated numerically at each time step. Equation (45) is solved by LU decomposition and backward substitution in conjunction with its block tridiagonal nature (Miller and Benson, 1983). The convergence criterion for this iterative scheme is set by

$$||\delta Q|| \leq 10^{-4} ,$$

where the norm Q is defined as

$$||\delta Q|| = \left[\sum_{n=1}^N \sum_{j=1}^{N_T} \left(\frac{C_{xj,n}^{\ell+1,k+1} - C_{xj,n}^{\ell+1,k}}{\max_j C_{xj,n}^{\ell+1,k+1}} \right)^2 \right]^{1/2} ,$$

N_T is the total number of degrees of freedom at each node, equal to $N_b + N_c + \bar{N}_b + \bar{N}_c + N_p$, N is the number of mesh points, and k represents the iteration level. As in CHEMTRN (Miller and Benson, 1983), the elements of the Jacobian matrix are calculated numerically at each step by calculating the ratios of the variation of each residue F to ΔC , a small, arbitrary change of concentration. However, to save computation time during the solution process in CHMTRNS, two measures are taken. (1) The spatial part of the Jacobian is only calculated once and is stored for repeated use. (2) The Jacobian is not recomputed at each iteration. If a solution is not obtained within a specified number of iterations, then a new Jacobian is calculated and the process is repeated.

Treatment of Dissolution and Precipitation

Among the set of algebraic equations to be solved in the N-R numerical scheme, the solubility product equation does not include any direct representation of the solid for which it is formulated. Therefore, the diagonal elements of the Jacobians of such equations are not automatically determined in the numerical evaluation of the Jacobian matrix. In the cases of supersaturation or undersaturation when solid exists in contact with the solution, no numerical problem is posed. However, in the case of undersaturation and lack of enough available solid for dissolution, the terms of the Jacobian for the solubility (solid) equations must be modified. In this case the goal is to preserve the undersaturated state while not creating negative solid concentrations. To achieve this, we put all the non-diagonal terms of the Jacobian matrix, for that solid, equal to zero and assign a value of unity to the diagonal term. This uncouples the solid equation from the undersaturated aqueous species equations and prevents creation of negative concentrations of solids.

APPLICATIONS

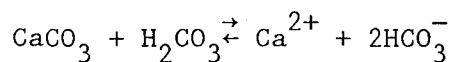
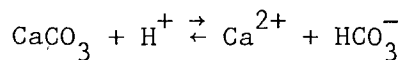
We have used CHMTRNS, to simulate a number of problems in kinetics, oxidation-reduction, and ^{13}C -fractionation in the process of transport along fluid-flow paths in geologic systems. The main purpose has been to test the performance of the CHMTRNS code and verify it whenever possible. However, due to unavailability of other comparable methods, as is often the case for problems of the degree of complexity addressed here, the soundness of the code in such cases can only be judged through its performance in various trials. The performance of the CHMTRNS thus far has created grounds for a high level of confidence in its soundness.

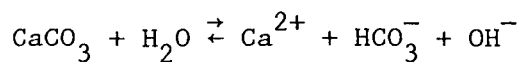
Simulation of Reversible Non-equilibrium Dissolution of Calcite in CO_2 -Water Systems

Formulation - Plummer et al. (1978) suggest a net rate of calcite dissolution (R) of the following form

$$R = \frac{dC_{\text{Ca}^{2+}}}{dt} = k_1 a_{\text{H}^+} + k_2 a_{\text{H}_2\text{CO}_3} + k_3 a_{\text{H}_2\text{O}} - k_4 a_{\text{Ca}^{2+}} a_{\text{HCO}_3^-} \quad (47)$$

where k_1 , k_2 and k_3 are first order rate constants dependent on temperature, k_4 is a function of temperature and P_{CO_2} , and R is in units of mmol of calcite per cm^2 per second. The following three mechanisms occur simultaneously during dissolution





The constants in the rate equation are given as follows

$$\log k_1 = 0.198 - 444./T ,$$

$$\log k_2 = 2.84 - 2177./T ,$$

$$\log k_3 = -5.86 - 317/T \quad \text{for} \quad 278 \text{ K} \leq T < 298 \text{ K} ,$$

$$\log k_3 = -1.10 - 1737./T \quad \text{for} \quad 298 \text{ K} \leq T \leq 321 \text{ K} ,$$

$$k_4 = \frac{K_2}{K_c} \left[15 K_1 + \frac{1}{a_{\text{H}^+(\text{s})}} \left(k_2 a_{\text{H}_2\text{CO}_3} + k_3 a_{\text{H}_2\text{O}} \right) \right] ,$$

$$a_{\text{H}^+(\text{s})} = \left(\frac{K_1 K_2 a_{\text{Ca}^{2+}} a_{\text{H}_2\text{CO}_3}}{K_c} \right)^{1/2} ,$$

$$\log K_1 = -40.366 + 5576.57/T + 11.331 \log T + 0.034655 T ,$$

$$\log K_2 = -77.3723 + 4593.31/T + 29.042 \log T + 5.9438 \times 10^{-4} T ,$$

$$\log K_c = -8.446 ,$$

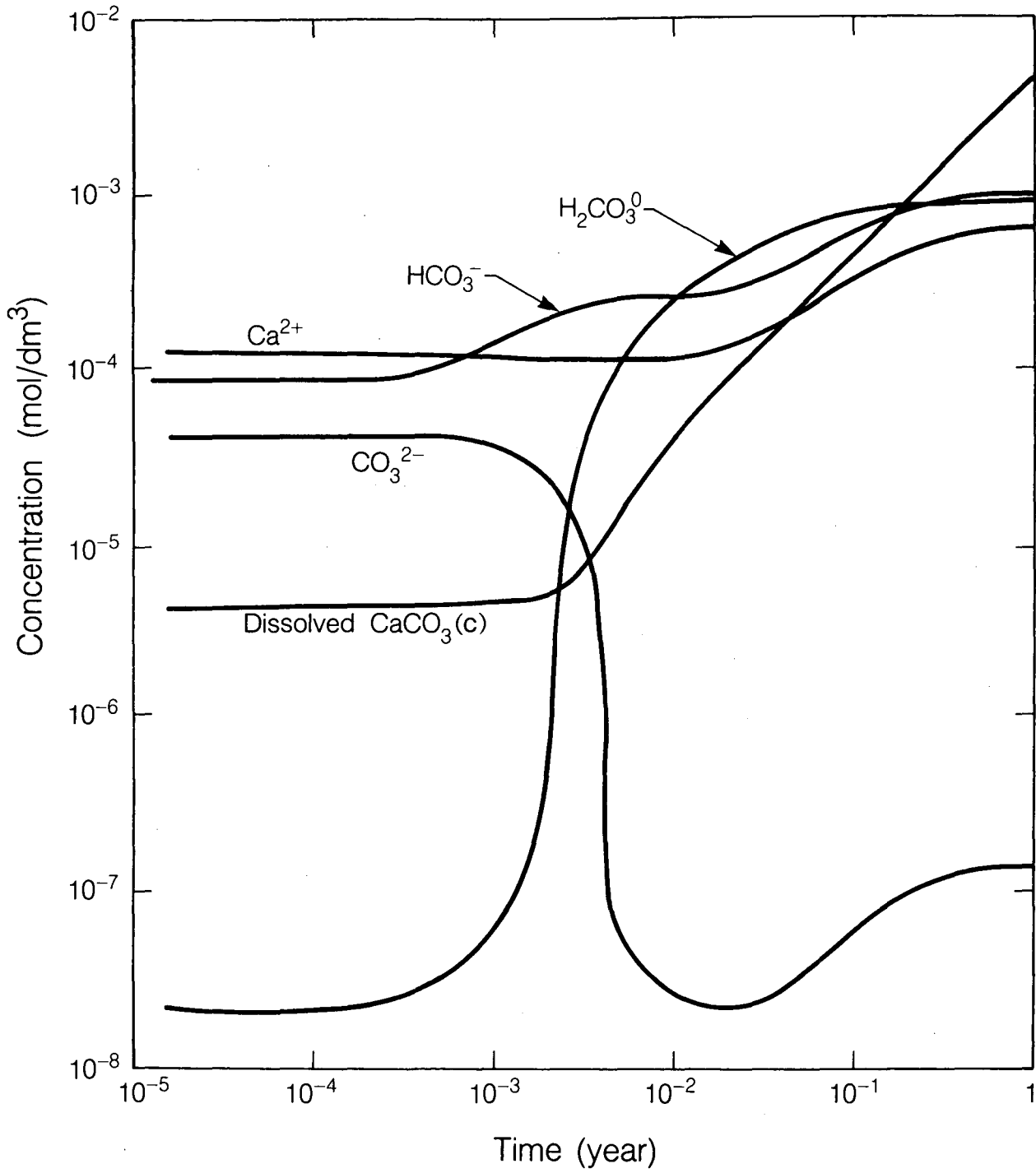
$$\log K_w = -80.3723 - 1395.46/T + 32.5514 \log T - 0.0318065 T .$$

With the above parameters defined, the rate term R_{x_i} in Eq. (8) is also defined. In the code, the rate (R) is quantified in subroutine SRATE and its value is fed to the right-hand side of Eq. (35).

Dissolution in a calcite lined tube - In this problem we assumed that recharge water, with pH of 5, at equilibrium with soil-zone CO_2 ($P_{\text{CO}_2} = 3.1623 \times 10^{-2}$ atm) flows through a calcite-lined tube. A preprocessing calculation, using CHMTRNS in static mode, provided the composition of this water (see Appendix 1 for input and output). The fluid, with the calculated concentrations

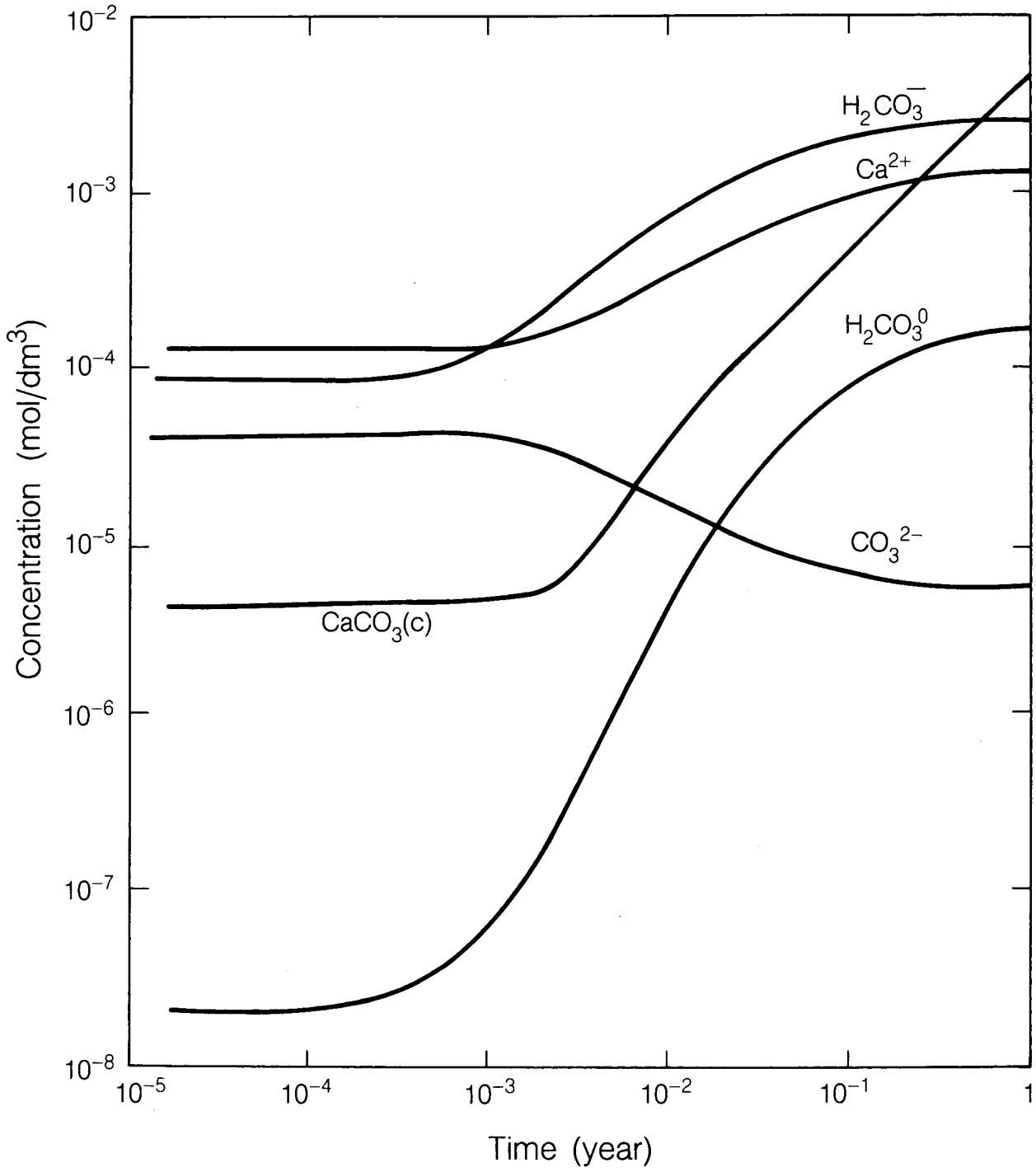
$$C_{\text{H}_2\text{CO}_3} = 1.473 \times 10^{-3} \text{ M}, \quad C_{\text{HCO}_3^-} = 5.637 \times 10^{-5} \text{ M} \text{ and}$$

$C_{\text{CO}_3^{2-}} = 1.865 \times 10^{-10} \text{ M}$, enters the calcite-lined tube with a velocity of 10^{-3} m/year. The tube length is 10 meters, variably discretized in 20 segments. The simulation time is 1 year. The input for this problem along with the output are included in Appendix 2. For performance demonstration purposes the results at a point near the entry of the tube are presented, where events can be observed for long periods without interference by effects due to the exit boundary. For the simulation time used here no appreciable exit boundary changes were observed, so an infinite tube-like behavior was obtained. Figure 1 shows the variation of concentrations of the aqueous species and the dissolved calcite with time. Equilibrium is reached at 1 year. However, the solid keeps dissolving continuously. To appreciate the role of kinetics in transport we solved the same transport problem with the assumption of total equilibrium. The results in Fig. 2 show the dramatic difference between the two cases. We also performed a batch (no transport) non-equilibrium



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Fig. 1. Breakthrough of the aqueous species at a point near the inflow boundary during kinetic transport.



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Fig. 2. Breakthrough of the aqueous species at a point near the inflow boundary during equilibrium transport.

calcite dissolution in pure water of pH = 5, which is shown in Fig. 3. Figures 4-6 compare the three mentioned cases for various species. As expected, the results of the equilibrium transport case always converge to those of the batch kinetic dissolution case. The inputs and outputs of the latter problems are given in Appendices 3 and 4.

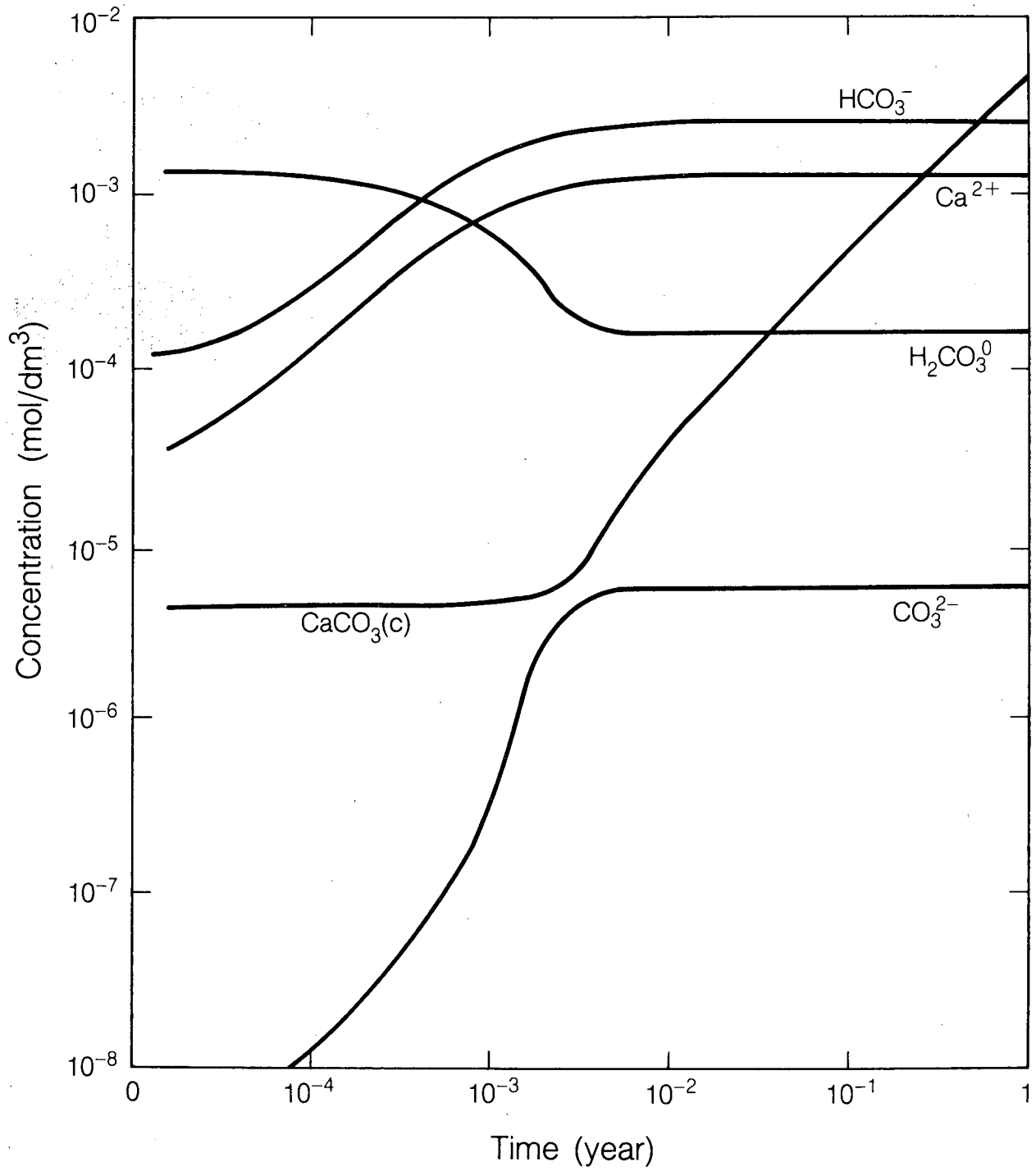
Precipitation in a smectite-lined tube - In this problem a water saturated with Ca^{2+} and also rich in Na^+ flows into a long smectite tube where ion exchange between the lining and the solutes can occur. The smectite initially is loaded with calcium which is then displaced by Na^+ in the influent water. Simulation time is 0.5 year. Input and output to this problem are given in Appendix 5. Figure 7 presents results for various species during the dissolution process. As can be observed in this figure, the solid builds up due to the release of Ca^{2+} from the $\bar{\text{Ca}}$ sites, and its subsequent kinetic precipitation (curve labeled ΔCaCO_3 (c)). The curve labeled CaCO_3 (c), shows the build up of the total amount of calcite in the tube.

Simulation of Kinetic Silica-Water Reactions

Formulation - Rimstidt and Barnes (1980) present a differential rate equation for silica-water reactions from 0-30°C of the following form:

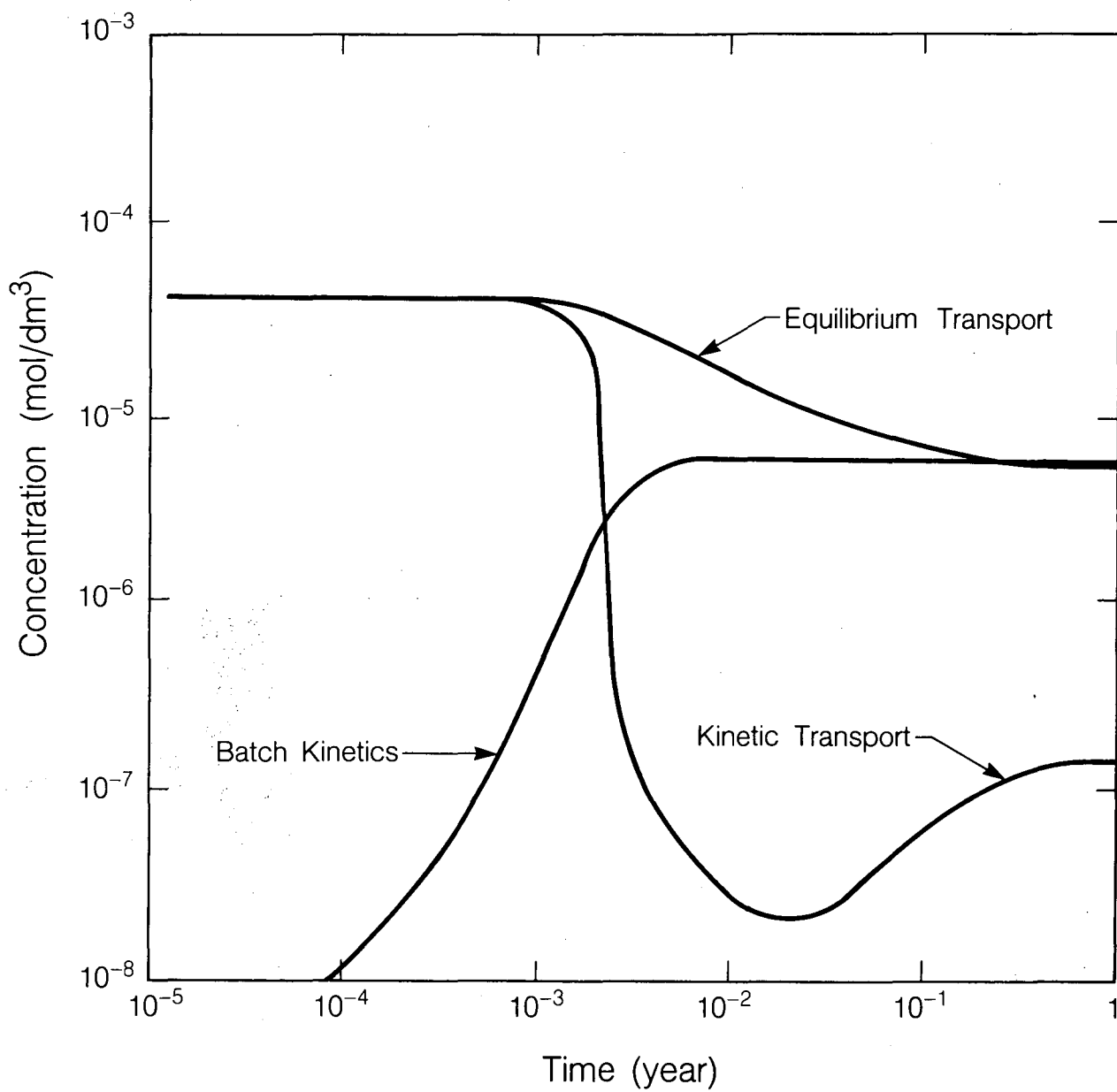
$$R = \frac{da_{\text{H}_4\text{SiO}_4}}{dt} = (A/M)(\gamma_{\text{H}_4\text{SiO}_4})(k_+ a_{\text{SiO}_2}^2 a_{\text{H}_2\text{O}}^2 - k_- a_{\text{H}_4\text{SiO}_4}) \quad (47)$$

where (A/M) is the ratio of interfacial area between the solid and aqueous phases to the mass of water in the system, $\gamma_{\text{H}_4\text{SiO}_4}$ is the activity of silica and k_+ and k_- are the rate constants for dissolution and



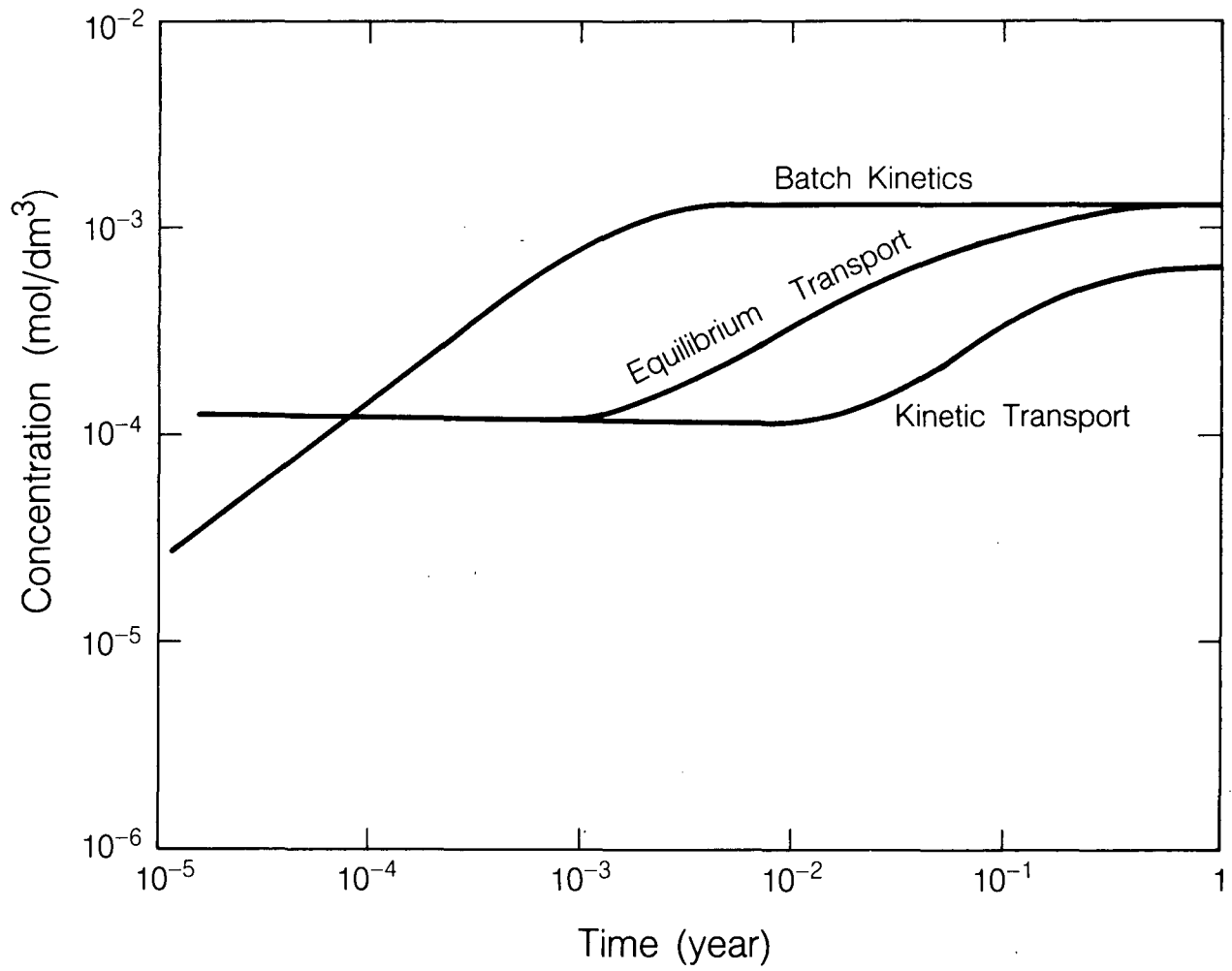
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Fig. 3. Variation of concentration of aqueous species vs. time in batch kinetic dissolution of calcite.



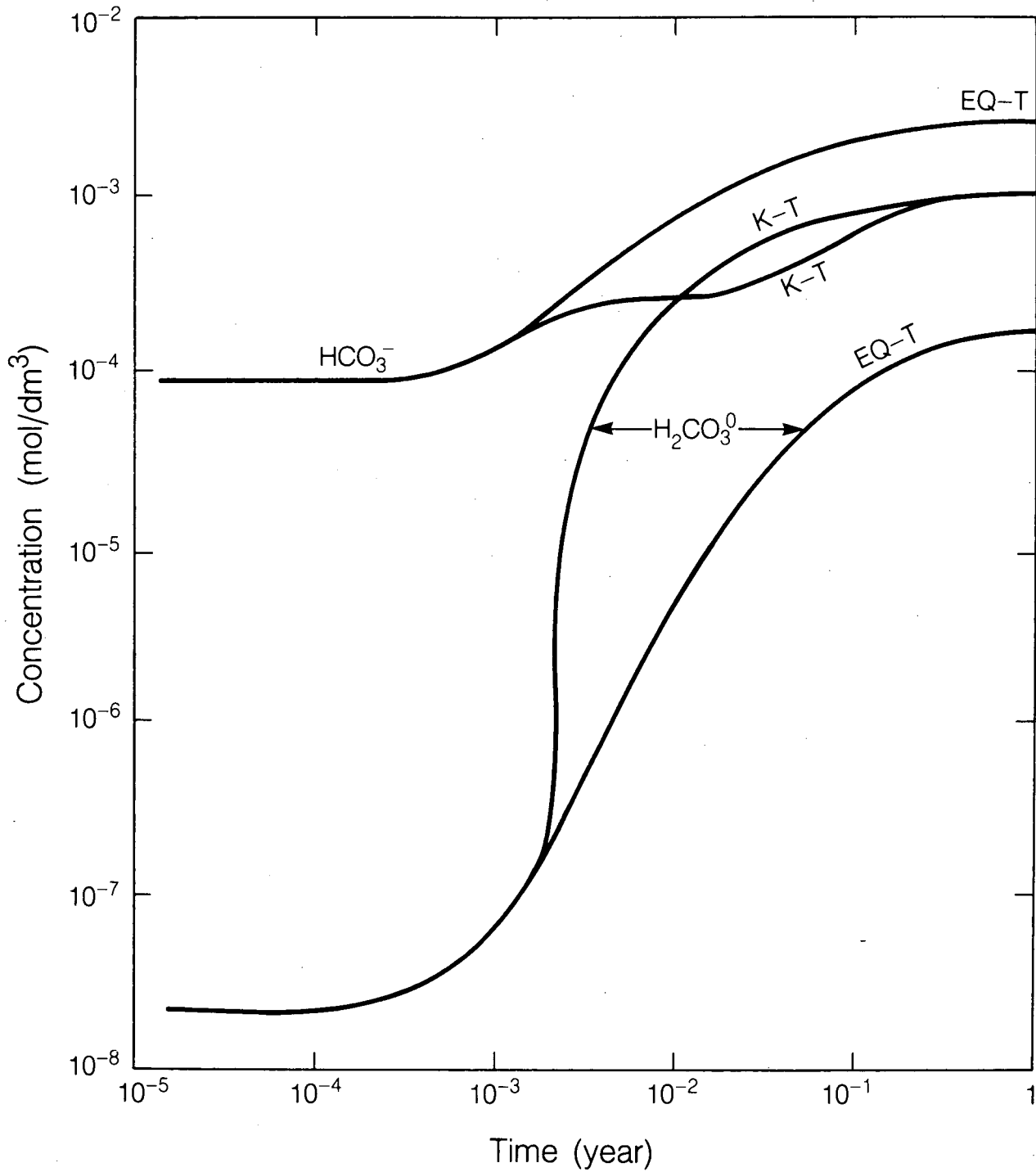
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Fig. 4. Variation of CO_3^{2-} concentration vs. time in batch kinetics, equilibrium transport and kinetic transport scenarios.



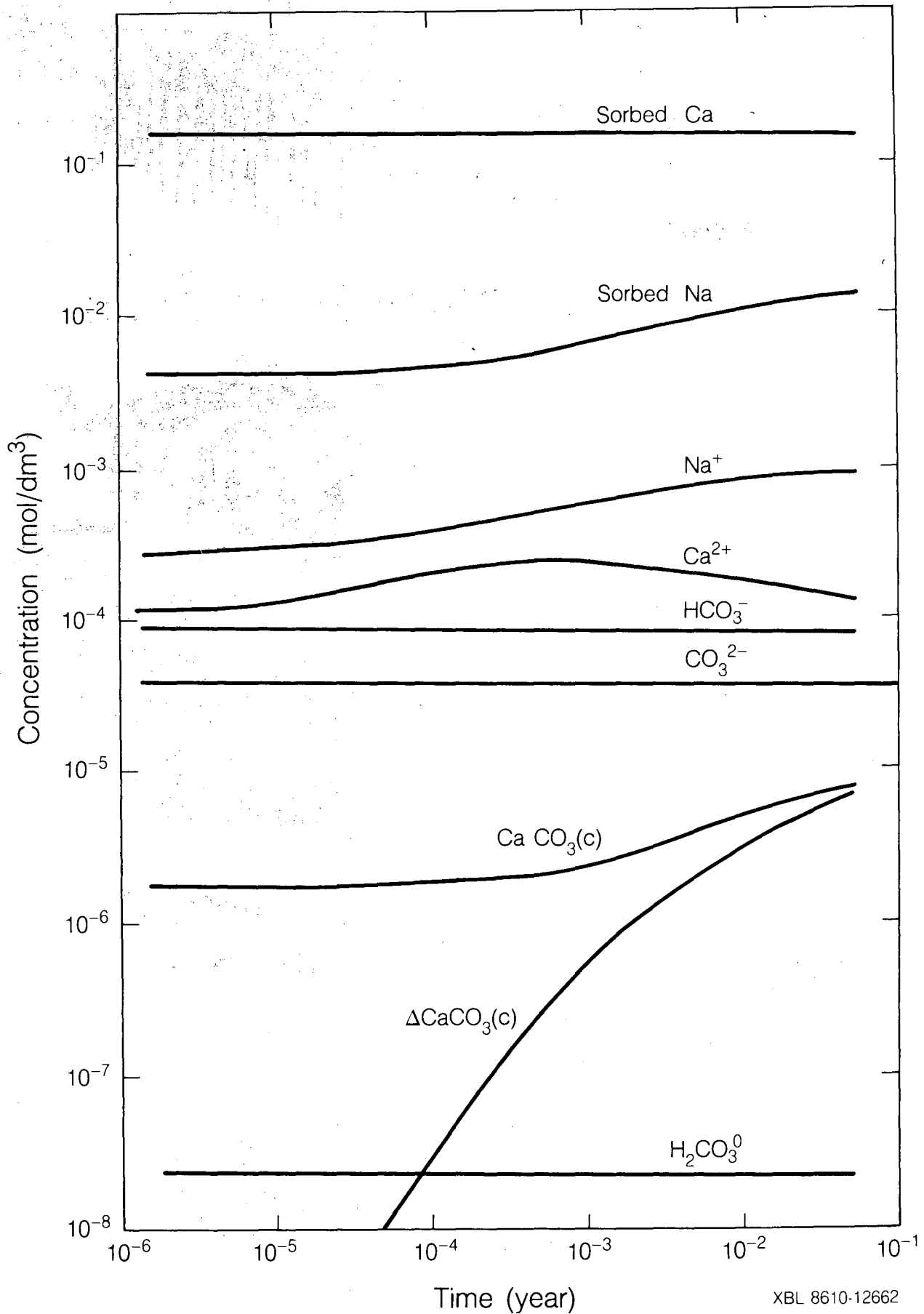
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Fig. 5. Ca^{2+} variations vs. time in batch kinetics, equilibrium and kinetic transport.



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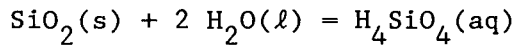
Fig. 6. HCO₃⁻ and H₂CO₃ breakthrough curves in kinetic transport (K-T) and equilibrium transport (EQ-T).



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Fig. 7. Variation of concentration of aqueous species, sorbed ions and solids vs. time.

precipitation respectively. The chemical reaction between silica and water is expressed as



The rate constants are given by

$$\log k_- = -707 - 2598/T$$

and

$$\log k_+ = A + BT + C/T$$

where T is absolute temperature and

$$A = 1.174, B = -2.028 \times 10^3, C = -4158 \text{ for quartz};$$

$$A = -0.739, B = 0, C = -3586 \text{ for } \alpha\text{-cristobalite};$$

$$A = -0.936, B = 0, C = -3392 \text{ for } \beta\text{-cristobalite};$$

$$A = -0.936, B = -7.890 \times 10^{-4}, C = -3438 \text{ for amorphous silica.}$$

With the above parameters given, the rate equation is completely defined. A subsection of subroutine SRATE implements the needed algorithm and calculates the right hand side of Eq. (35).

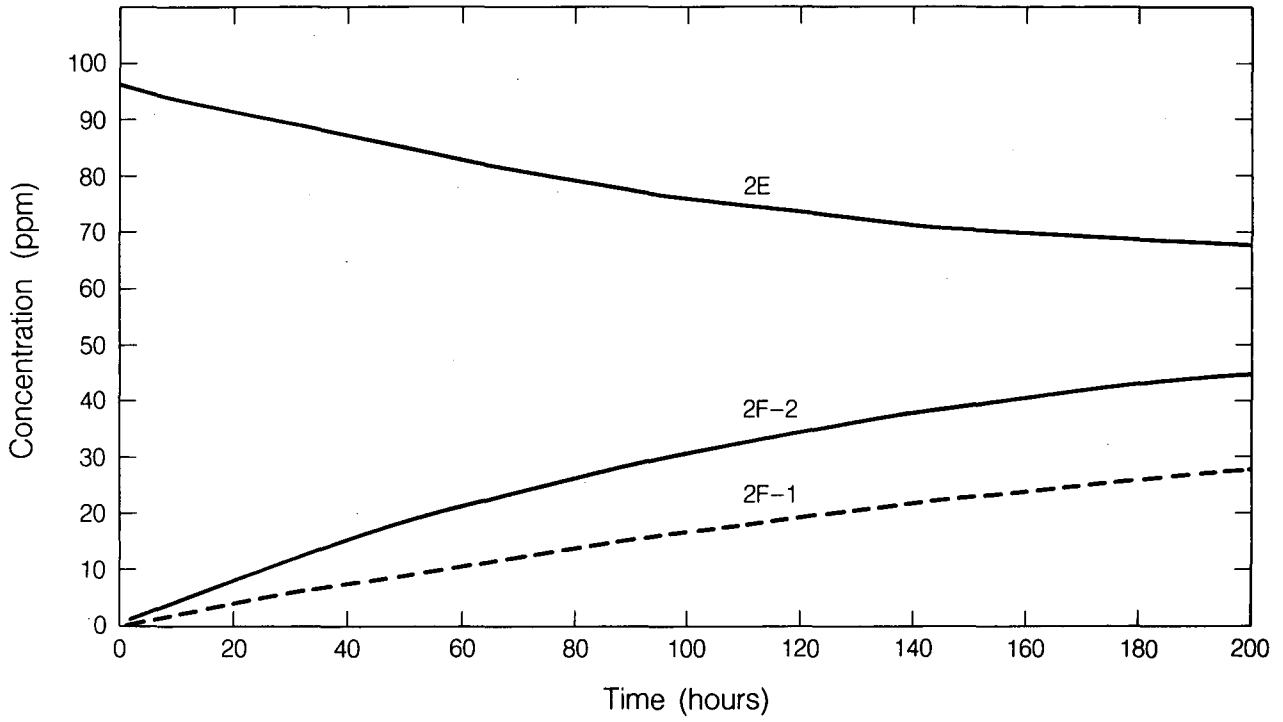
Precipitation of silica - In this problem we simulated the precipitation experiment of Rimstidt and Barnes (1980). The chemistry in this problem is kept quite simple by considering H_4SiO_4 as the only aqueous species and SiO_2 as the only solid that can form. The constants of the

rate equation in this problem are those of the curve 2E in the experiment. Simulation starts with a supersaturated solution of 10^{-3} M of silica at 105°C. To achieve this initial condition the equilibrium solubility of the SiO_2 (Quartz) is set equal to the assumed initial concentration. The input and output to this simulation are given in Appendix 6. The results of this run are shown by the curve labeled 2E in Fig. 8. This curve practically duplicates the results of the Rimstidt and Barnes (1980) experiment.

Dissolution of silica - In this problem we simulated the dissolution part of the Rimstidt and Barnes (1980) experiment. The chemistry in this case is identical to the precipitation case. However, here we start with an undersaturated solution of 10^{-20} M of silica. In this problem we made two different runs using different sets of rate constants. In the first run, we used the k_+ and k_- values of the curve 2F of the experiment which resulted in the dashed curve 2F-1 in Fig. 8. Obviously, this result varied largely from those of the experiment. However, when we used the data of the precipitation experiment (curve 2E), we obtained a perfect match for the dissolution experiment, as shown by curve 2F-2 in Fig. 8. We cannot explain the reason for failure of simulation when correct data is used and its unexpected success otherwise. However, we do not attribute this behavior to lack of soundness of the algorithm. The input and output for this problem are provided in Appendix 6.

Simulation of Non-Reversible Kinetic Dissolution of Glass

Formulation - Claassen and White (1979) suggest an empirical kinetic formula for the dissolution mechanism of glass in tuffs. This



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Fig. 8. Variation of silica concentration vs. time.

expresses the time-dependent release of various cations into an aqueous solution containing dissolved CO_2 . The formula has the form:

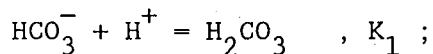
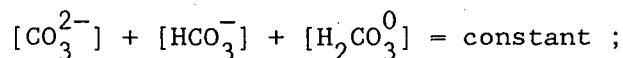
$$Q_{M,t} = Q_o + k_M t^{1/2}, \quad (48)$$

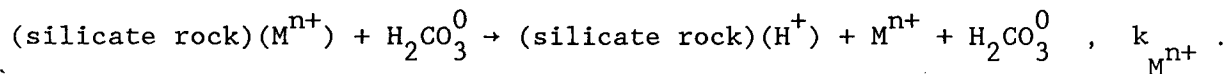
where $Q_{M,t}$ is the total mass of cation M transferred from solid to solution in time t, Q_o is the mass transferred from solid to solution by ion exchange at the fresh rock surface, and k_M is the rate constant associated with the transfer of cation M at a specific pH. The rate of dissolution, R_M , is therefore given by

$$R_M = \sigma \frac{dQ_{M,t}}{dt} = 0.5 \sigma k_M t^{-1/2},$$

where σ is aquifer surface area in contact with a unit volume of solution; σ has units of cm^2/liter . The above derivation neglects the secondary effects of pH variations on k_M .

The reaction in this dissolution mechanism is assumed to occur in the following steps. The recharging water dissolves soil-zone CO_2 to provide the aqueous carbonate constituents of the infiltrating water. Details of CO_2 dissolution are provided in Appendix 1. The distribution of the carbonate species in this water is governed by the equilibrium between HCO_3^- and H_2CO_3^0 at any pH. The H_2CO_3^0 of the groundwater reacts with the silicate rock leading to the release of various cations. These steps can be written as





The rate constants were calculated from data given by Claassen and White (1979), and are

$$\log k_{\text{Na}^+} = -0.17(\text{pH} - 5.75) + 13.73,$$

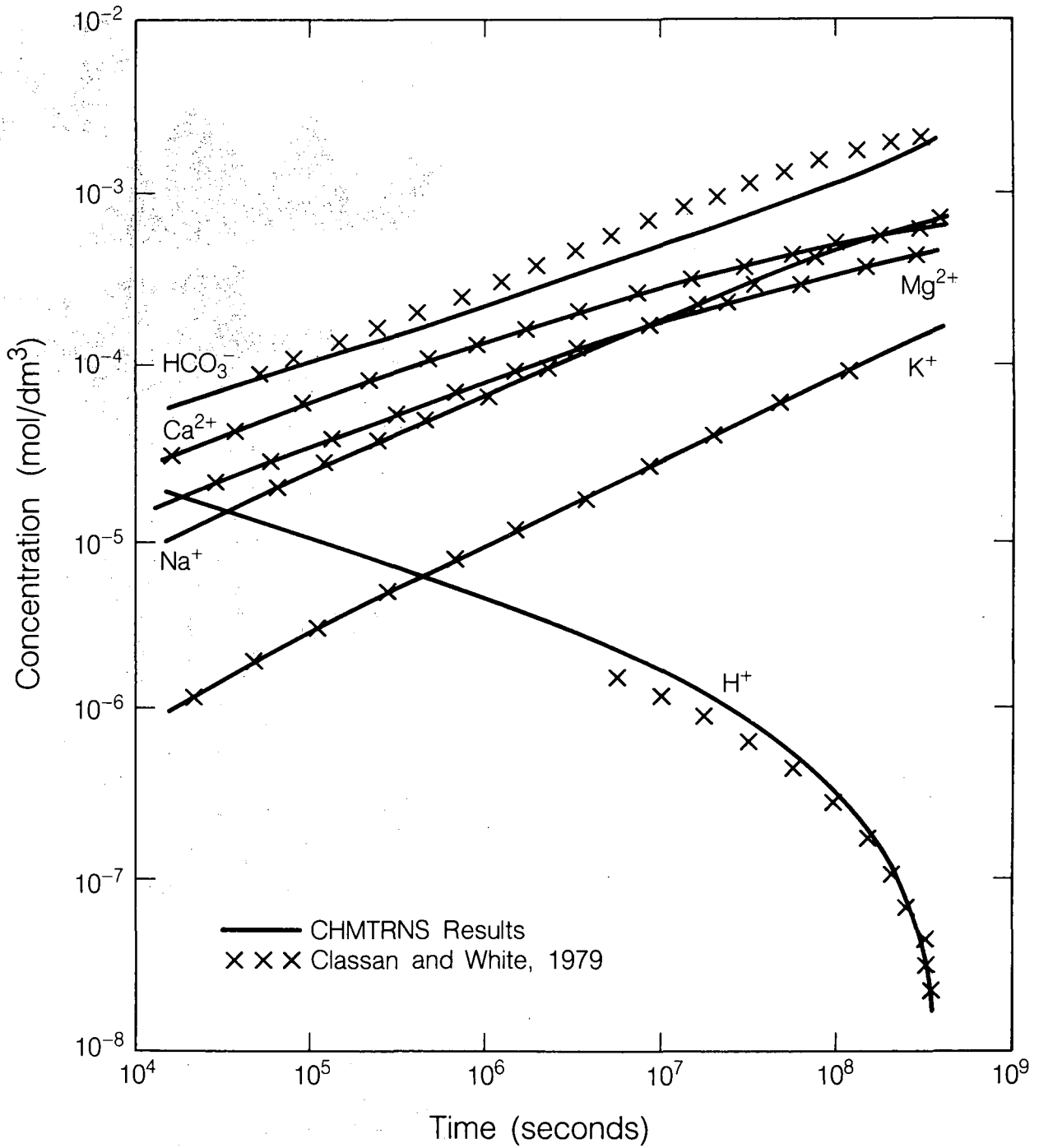
$$\log k_{\text{K}^+} = -14.54,$$

$$\log k_{\text{Ca}^{2+}} = -0.5(\text{pH} - 6.25) + 14.15,$$

$$\log k_{\text{Mg}^{2+}} = -0.4(\text{pH} - 5.25) + 13.88,$$

The algorithm for these empirical rate formulas has been implemented in the subroutine SRATE.

Dissolution of silicate rocks - In this section we repeat the calculations of Claassen and White (1979) using CHMTRNS. In this problem we assumed $\sigma = 1 \times 10^6 \text{ cm}^2/\text{liter}$ and the total carbonate concentration of $2.16 \times 10^{-3} \text{ mol/liter}$ at $\text{pH} = 4.5$. The total simulated time was 3.52×10^8 seconds. The results of our calculation along with those of Claassen and White (1979) are shown in Fig. 9. With the exception of the pH and HCO_3^- results, which are systematically overestimated, the calculations agree almost exactly. The mentioned discrepancies are due to linearization of the rate constants in our calculations. In another set of calculations, we included the contribution of the time variation of the rate coefficients in the rate formula. As a result the rate formula became



XBL 8610-12656

Fig. 9. Dissolution of various cations and HCO₃⁻ and H⁺ in time.

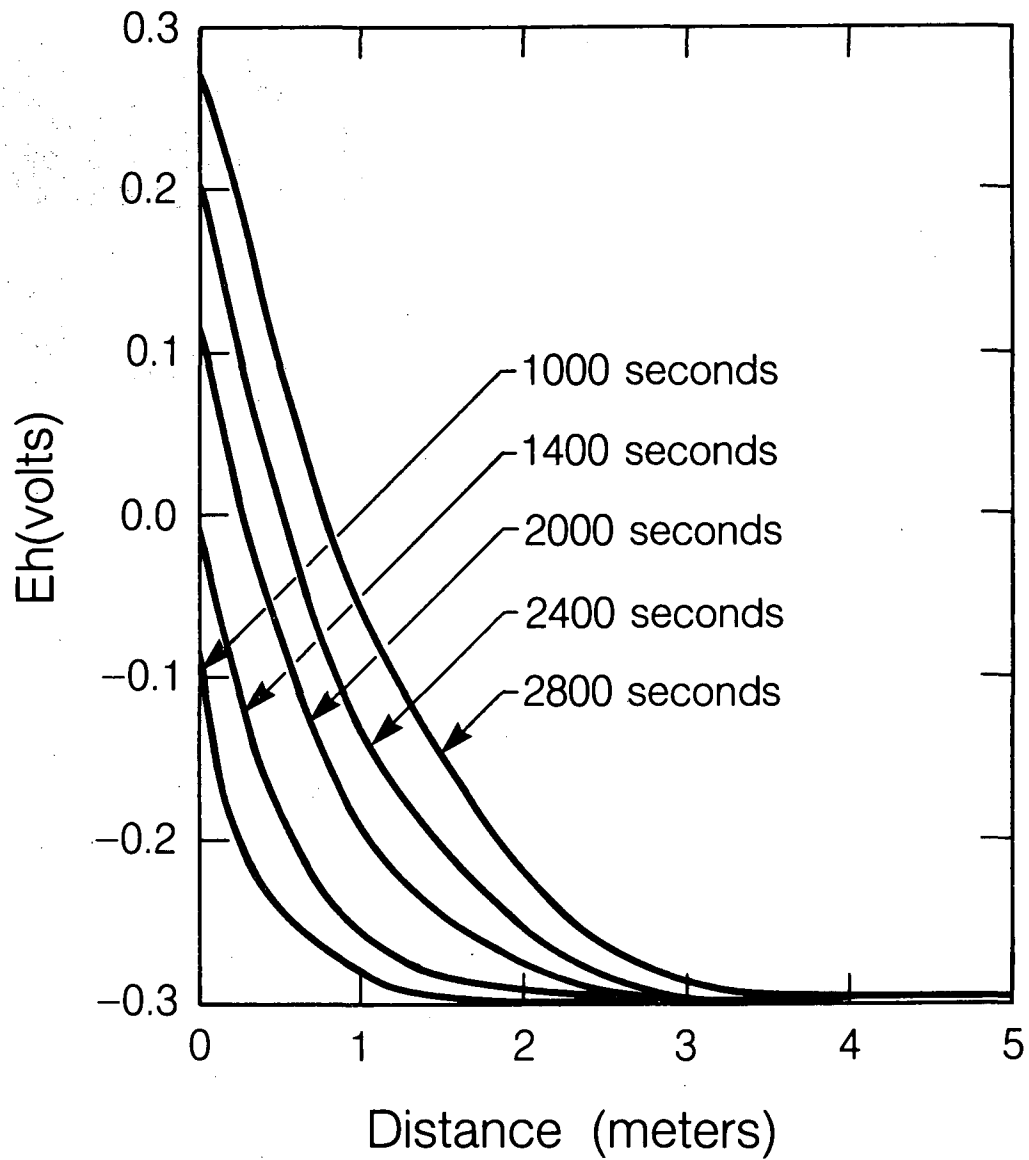
$$R_M = 0.5 \sigma k_M t^{-1/2} + \left[\frac{dk_M}{dpH} \cdot \frac{dpH}{dt} \right] \sigma t^{1/2} \quad (49)$$

However, the apparent improvement of the rate formula caused deterioration of the results. Considering the simple nature of the algorithms, such deviations are unexpected. Further examination seems to be necessary. The input and output for these simulations are included in Appendix 7.

Simulation of Non-Isothermal Oxidation-Reduction During Transport

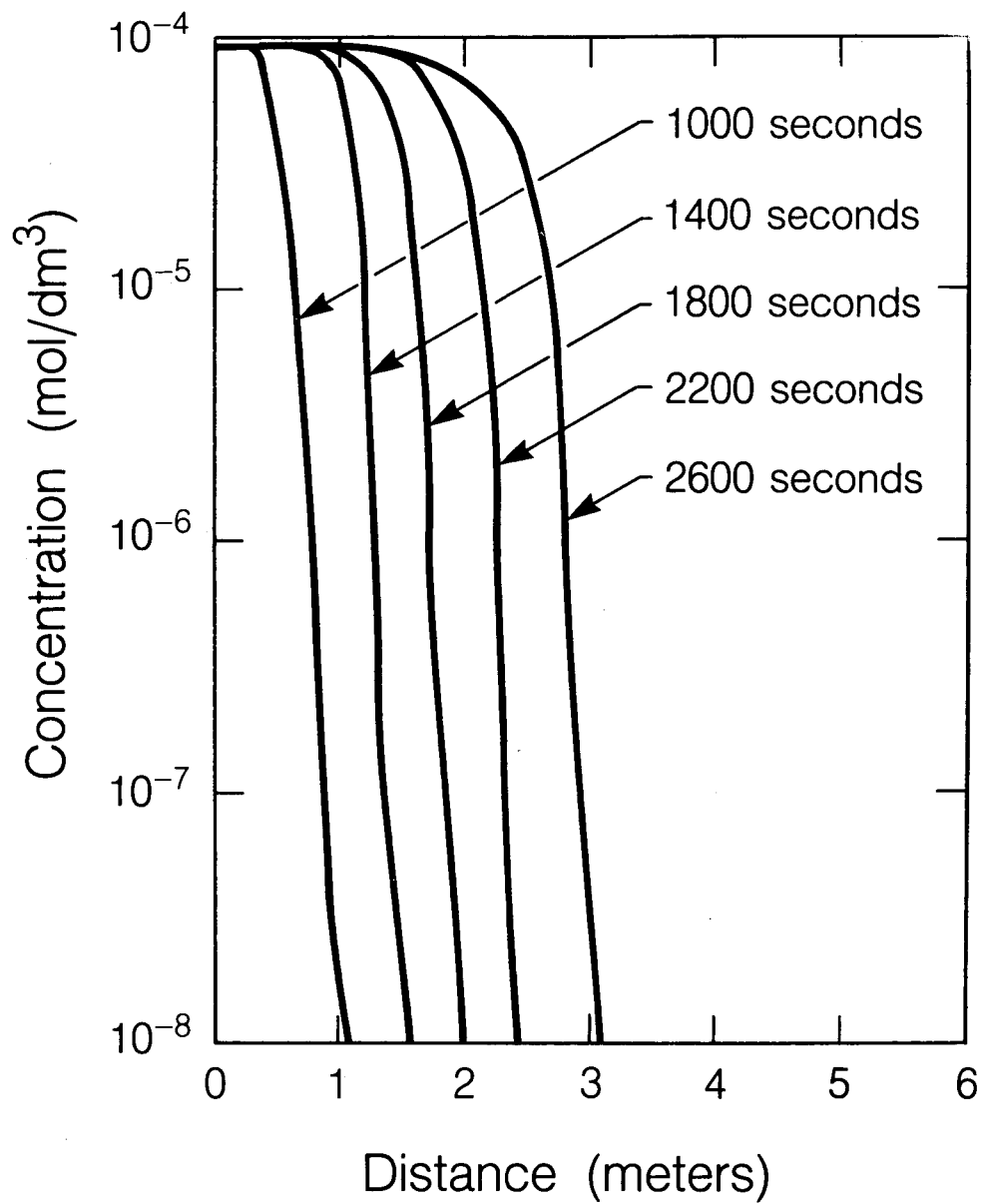
In this simulation an effort was made to test both the oxidation-reduction and the heat transport algorithms. The problem was that of 150°C water with Eh = 0.3 v and pH = 4 entering a long tube initially containing 50°C water with Eh = -0.3 v and pH = 10*. Convective-dispersive heat transport along with reactive solute transport are considered. The chemical reactions considered were redox, complexation, precipitation and dissolution. The tube length was taken to be 10 meters discretized into 40 sections. Fluid velocity was 10^{-3} m/second. The results of this simulation for 2800 seconds are shown in Figs. 10-14. The figures depict the evolution of Eh, aqueous species $H_2CO_3^0$ and UO_2^{+2} , precipitates $UO_2(c)$ and $UO_2(OH)_2(c)$ and the temperature along the flow path. Since the above problem had originally been simulated with the code THCC(Carnahan, 1976), we could compare the results of both simulations. In spite of the perfect agreement of the results in their evolutionary trend, there are discrepancies in the magnitudes of various species. However, these differences are attributed to variations in the numerical approaches. The general performance agreement of the two

*See Appendix 8 for input details



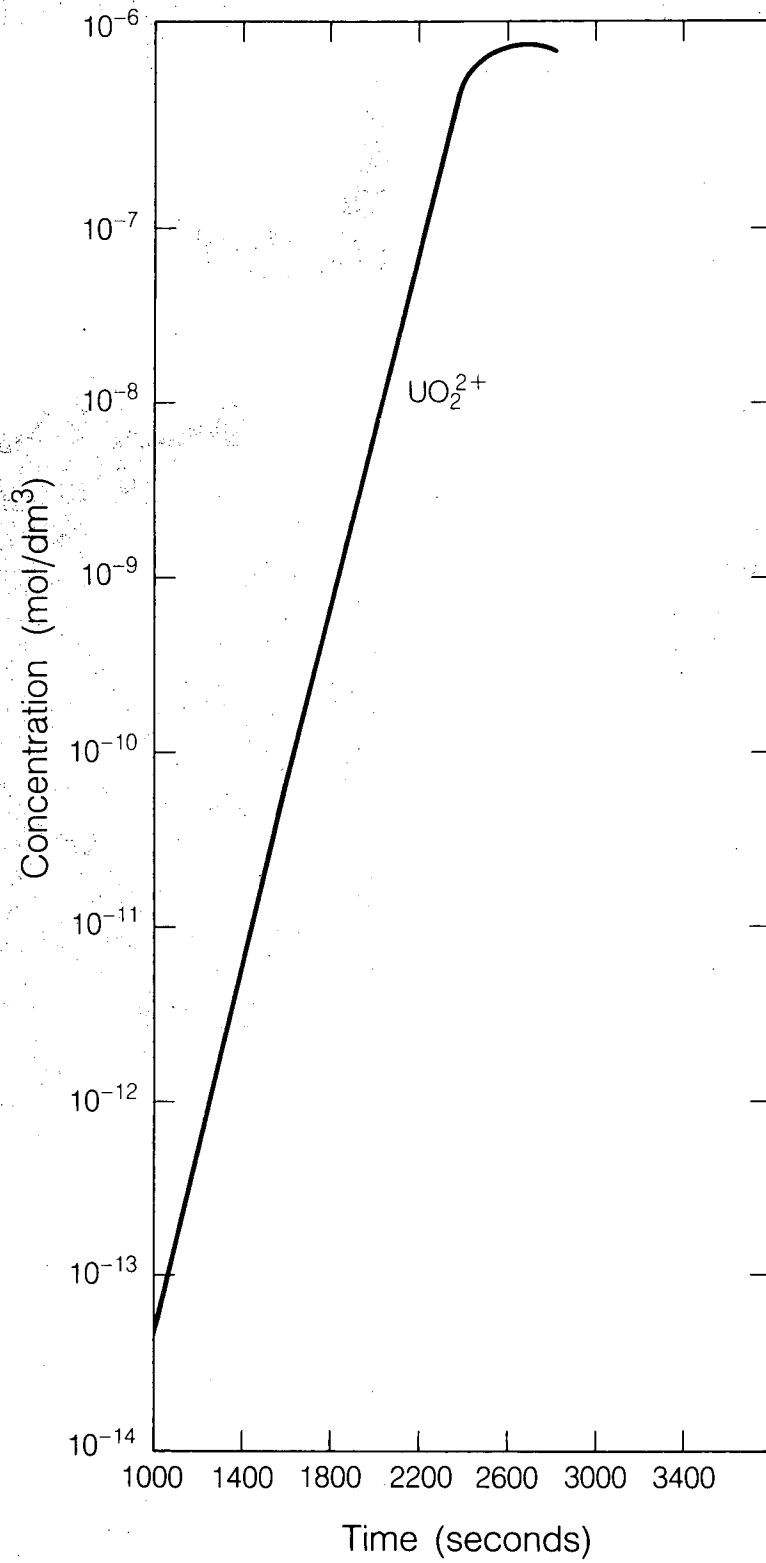
XBL 8610-12642

Fig. 10. Eh profiles along the flow path at various times.



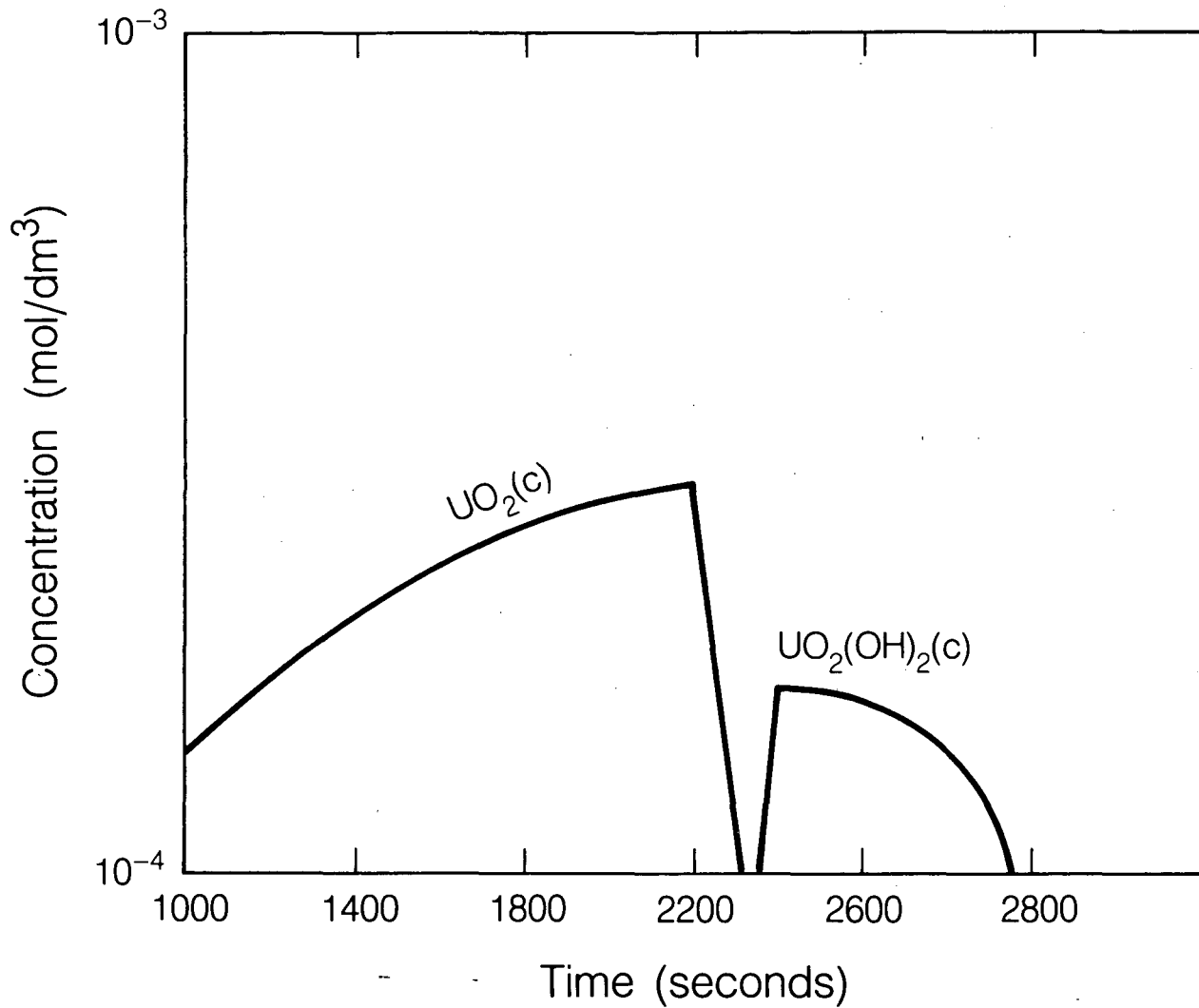
XBL 8610-12654

Fig. 11. Carbonic acid profile along the flow path at various times.



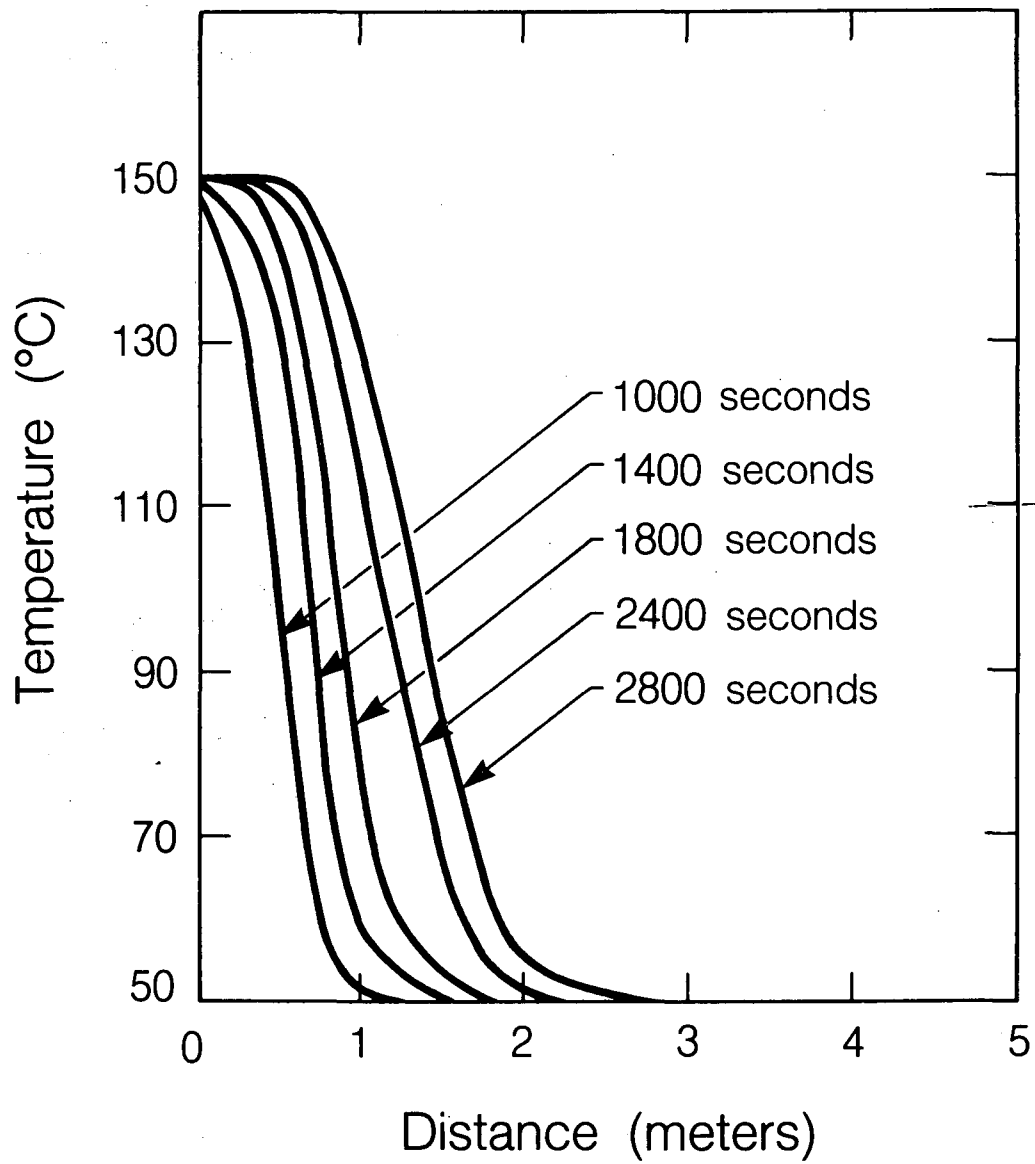
XBL 8610-12653

Fig. 12. Build up of UO_2^{2+} as a function of time near the inflow boundary.



XBL 8610-12644

Fig. 13. Precipitation and dissolution of UO₂(c) and UO₂(OH)₂(c) in time.



XBL 8610-12643

Fig. 14. Temperature profile along flow path at various times.

codes provides a strong basis for algorithm soundness. The input and output to this problem are provided in Appendix 8.

Simulation of ^{13}C Fractionation During Non-Equilibrium Reactive Solute Transport in Geologic Systems

Major issues regarding the evolution of groundwater are the composition of recharge waters, travel times to and from and within aquifers, and chemical processes that have occurred during the transport. Traditionally, studies of groundwater ages have been based on the assumption of dilution of carbon from various sources. In this approach the ^{13}C content of the water sample is measured by (Pearson and Hanshaw, 1970)

$$^{13}\delta_{\text{sol}_{\text{sm}}} = \frac{\sum ^{13}\delta_{\text{sol}j} m_{\text{c}j}}{\sum m_{\text{c}j}} \quad (50)$$

and the activity of ^{14}C is similarly

$$A_{\text{sm}}(^{14}\text{C}) = \frac{\sum m_{\text{c}j} A_j^0 e^{-\lambda t_j}}{\sum m_{\text{c}j}} \quad (51)$$

where $m_{\text{c}j}$ denotes the concentration of stable carbon from source j , t represents time and A^0 is taken as equal to close to 100% modern ^{14}C . Considering only two sources of carbon, one belonging to the recharge water and the other to that of a rock enriched in ^{13}C , Eq. (50) becomes

$$^{13}\delta_{\text{sol}_{\text{sm}}} = \frac{^{13}\delta_{\text{a}} m_{\text{C}_a} + ^{13}\delta_{\text{s}} m_{\text{C}_s}}{m_{\text{C}_a} + m_{\text{C}_s}}$$

where the subscripts a and s refer to the recharge water (air) and the rock. After simple manipulations of the above relationship we get

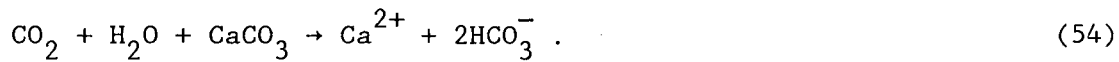
$$\frac{m_{C_a}}{m_{C_a} + m_{C_s}} = \frac{{}^{13}\delta_{sol_{sm}} - {}^{13}\delta_s}{{}^{13}\delta_a - {}^{13}\delta_s} \quad (52)$$

Equation (51), therefore, changes to

$$A_{sm}({}^{14}C) = \frac{m_{C_a} A_o e^{-\lambda t}}{m_{C_a} + m_{C_s}} \quad (53)$$

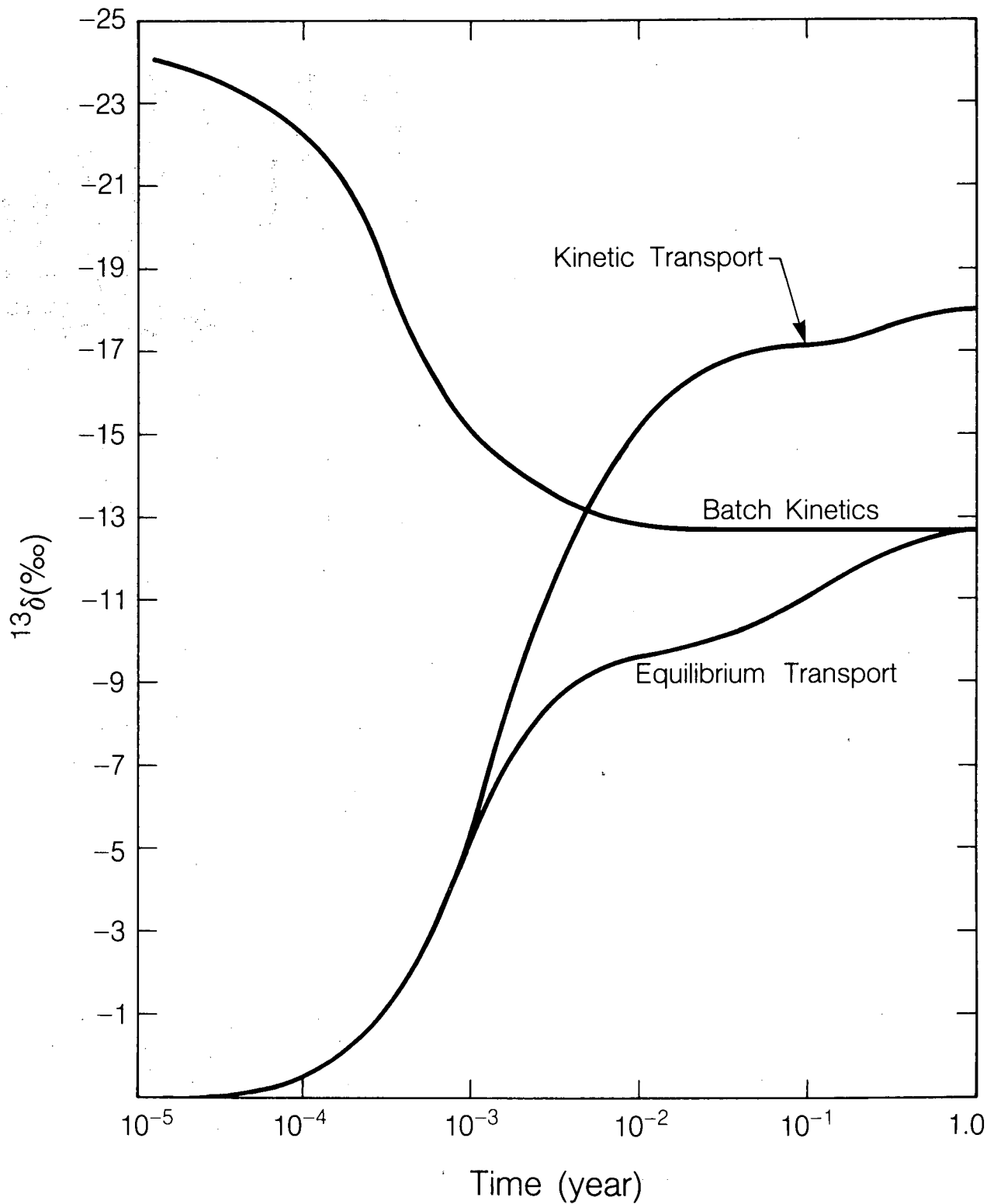
Assuming reasonable values for the parameters in Eq. (52) makes it possible to obtain a correct age for the waters. As mentioned earlier, derivations such as the above (e.g., Wigley, 1975), are based on simple batch mixing assumptions. However, the evolution of groundwater may have involved complex non-equilibrium chemical processes during transport through the earth material. CHMTRNS can serve as a basis for testing the validity of the simple dilution assumption for specific problems. Also, it can be employed for general investigation of groundwater evolution processes. In the following we provide accounts of such attempts.

Generic simulations - In this problem we investigated the ${}^{13}C$ fractionation of recharge waters as they percolate through heavy carbonate rocks. It is reported (Deines et al., 1974) that for most soil waters $\delta^{13}C \approx -25\text{o/oo}$ and P_{CO_2} ranges from $10^{-0.5}$ atm. to $10^{-3.5}$ atm. and pH ranges from 4.0 to 7.5 and ${}^{14}C = 100\%$ modern. Based on the above data, a typical water of this nature entering marine carbonate rocks that have $\delta^{13}C = 0 \text{ o/oo}$ and ${}^{14}C = 0\%$ will tend to have $\delta^{13}C \approx -12.5\text{o/oo}$ and ${}^{14}C = 50\%$ modern, after equilibrium has been reached in the dissolution reaction



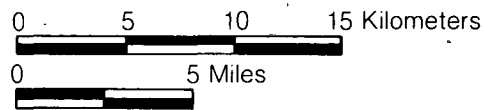
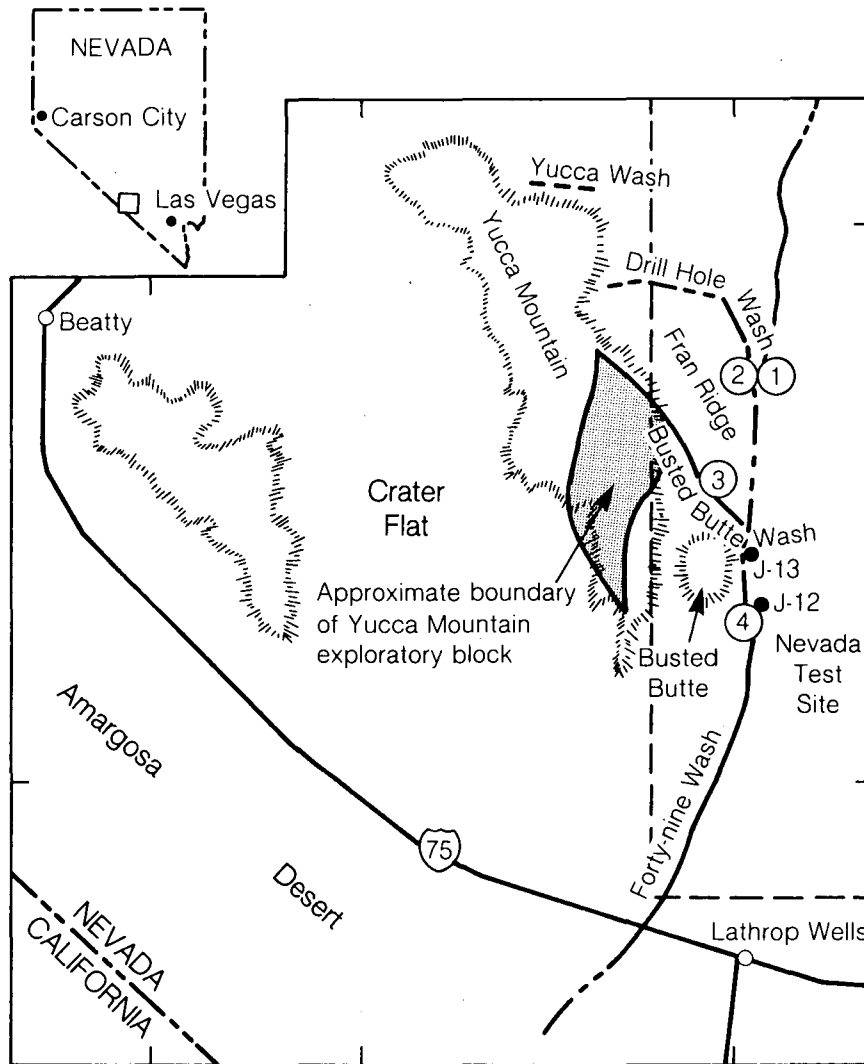
The reason is evident from the mass balance of Eq. (54). However, if this reaction does not go to completion, because of kinetic effects, reactive transport effects, or paucity of solid carbon in the flow path, the dilution by the dead rock would lead to $\delta^{13}\text{C}$ between -25o/oo to -12.5o/oo. Some of the above conditions are simulated in three hypothetical cases we have solved. Before discussing these results, attention is drawn to the fact that for all cases initial equilibrium calculations were based on CO_2 dissolution in water with $\text{pH} = 5$ in order to obtain the recharge water composition. These calculations are provided in Appendix 9. For initial conditions in the carbonate rock we assumed the composition of pure water at equilibrium with the rock. The flow path is a one-dimensional discretized space. The three runs simulate batch kinetic calcite dissolution, equilibrium dissolution of calcite with transport, and kinetic dissolution with transport. The results are exhibited in Fig. 15. While the first two simulations dilute the ^{13}C in the water by 50% and reduce $\delta^{13}\text{C}$ to 13o/oo, the kinetic transport is effective only by about 30%, even after a year. The input and output to these problems, which were also used in an other context, are given in Appendix 2.

Scoping calculations for Yucca Mountain (Nevada) groundwater - In this example the effect of kinetic dissolution during transport at a particular site is considered. In this first-order study of the Yucca Mountain groundwater evolution process, we used the typical composition of surface waters of the Busted Butte site [see Fig. (16) for site map], shown in Table 1, for the recharge water (Benson, 1986). In this



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Fig. 15. Time variation of $^{13}\delta_{\text{sol}}$ as a result of dilution of the carbonate species by marine calcium carbonate in various scenarios.



- ① Forty mile Wash above Drill Hole Wash on Rd. 'H'.
- ② Drill Hole Wash at the mouth.
- ③ Busted Butte Wash
- ④ Forty mile Wash at Well J-12

XBL 8610-12663

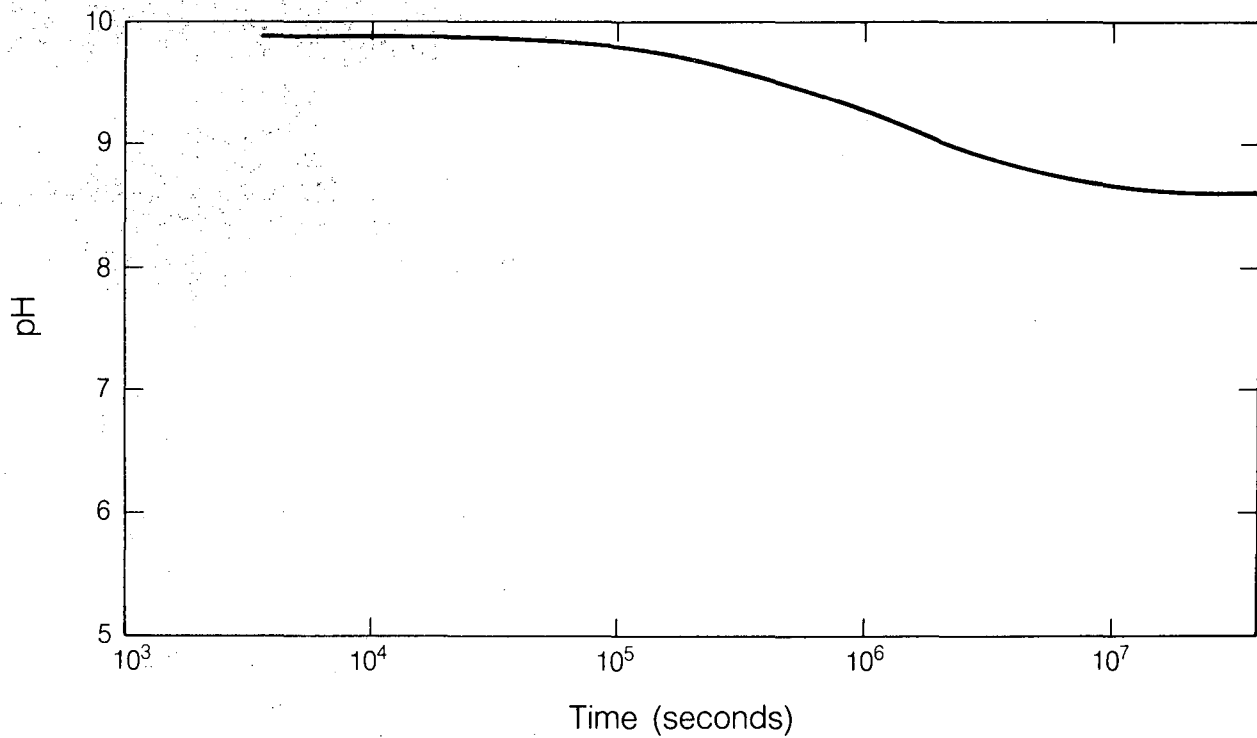
Fig. 16. Location of sampling sites near Yucca mountain.

Table 1. Chemical analysis from Forty-Mile Wash surface water samples.
 1 to 4 Forty-Mile Wash above Drill Hole Wash
 5 and 6 Drill Hole Wash
 7 and 8 Busted Butte
 9 Forty-Mile Wash near Well J-12

STATION	DATE	TIME	Na mg/c	Ca mg/c	Mg	K	HCO ₃ field	HCO ₃ lab	SO ₄	Cl	SiO ₂	Li µg/L	Sr µg/L	F	Dissolved Solids	pH field	pH lab	SC field	SC lab	δD	δO ¹⁸	C ¹⁴ yrs BP	C 13/12 ratio	
	1	7/22/84	1925	9.0	27	3.6	8.9	110	83	11	4.5	26	120	0.2	140	7.6	7.2	198	212	---	---	---	---	
	2	7/24/84	2005	8.1	24	3.3	7.8	106	125.6	10	3.7	25	6	100	0.2	145	7.3	7.4	182	201	-89	-12.3		
40 mile	3	8/14/84	1505	4.1	8.1	0.90	5.6	---	43.9	6.2	1.3	8.7	6	34	---	57	8.4	7.5	70	198	-60	-9.0	---	---
	4	3/15/84	2230	8.2	21	2.9	9.1	---	91.5	10	1.4	24	7	100	0.2	122	8.0	7.4	170	259	-96	-13.7	0	-13.8
	5	8/14/84	1510	8.6	9.5	1.3	7.4	---	51.2	12	2.2	20	14	66	0.3	92	8.3	7.8	100	218	-57.3	-8.9	---	-12.7
Drill Hole	6	7/19/85	1900	11	19	2.6	10	---	103.7	10	3.2	26	14	120	0.3	134	---	7.9	---	193	---	---	---	---
	7	8/14/84	1530	7.0	12	1.8	8.1	---	57.5	7.9	1.7	23	17	86	0.3	100	8.3	7.8	120	217	-69.5	-10.1	+846	-16.1
Busted Butte	8	8/15/84	0230	6.9	9.8	1.5	5.8	---	52.4	4.9	1.2	16	14	67	0.2	73	8.3	8.0	90	184	-70.5	-10.5	---	-17.4
40 m J-12	9	8/14/84	1600	2.4	6.7	0.7	6.3	---	31.7	6.3	2.0	4.5	5	31	---	45	8.2	7.0	59	100	-64.5	-9.5	---	-16.1

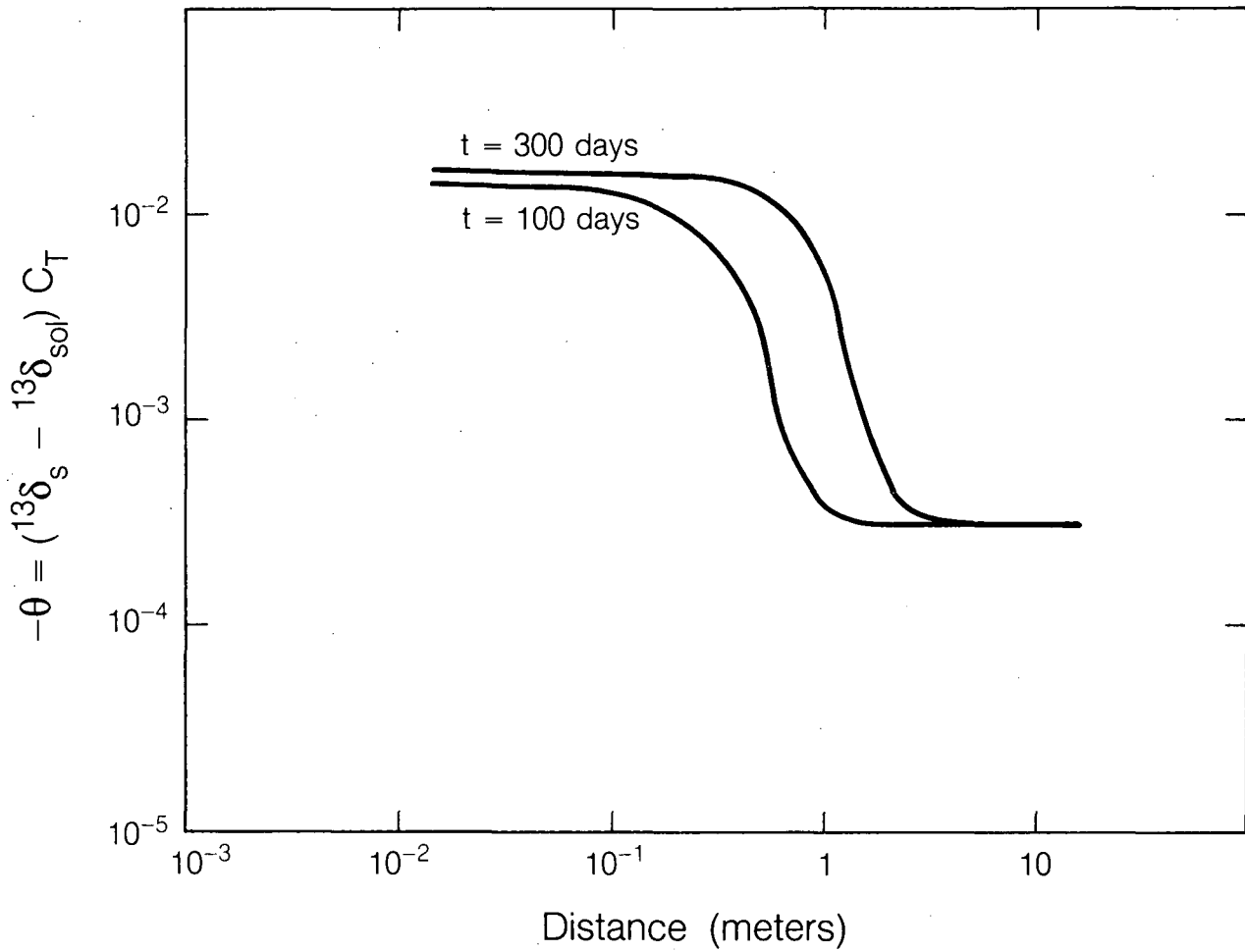
Reference: Benson, L.V., unpublished U.S.G.S. Report.

simulation a constant flux of surface water was input at the boundary of a one-dimensional column of tuff saturated with pure water. We allowed reversible kinetic dissolution of calcite and silica and non-reversible kinetic dissolution of glass. This study, having a scoping nature, precluded any other complex reactions which might be of relevance, and also used additional simplifications. In order to reduce simulation time, the percolation velocity was increased from the actual order of cm/year to m/year, and also the flow path was reduced to a 10-meter distance discretized into 20 segments. As has been pointed out before, the latter assumption posed no drawback because we considered the events which were not affected by exit boundary effects during the observation time. That is, we only analyzed near-entrance events that stabilized before the far boundary sensed any change. The results of this simulation are not very dramatic because of the very low dissolution capability of the water. Therefore, expectedly, a front with the composition of the flux water swept through the column. No appreciable change of $\delta^{13}\text{C}$ was observed due to the fact that little dilution took place. The results of this simulation are shown in Figs. 17-23. Figure 17 exhibits the small pH variations. Figure 18 shows the advance of the θ_d front and consequently, as seen in Fig. 19, a very sharp front of $\delta^{13}\text{C}$ of about -16 o/oo develops at around 100 days into the simulation. At the end of the one-year simulation $\delta^{13}\text{C}$ in the upstream part of the flow path approaches the value for the recharge water, as shown in Fig. 20. Figure 21 demonstrates the variations of the concentrations of carbonate species at a point near the entrance as a function of time. Dissolution of glass is very low because of the high pH of both the in situ water and the percolating water. It is therefore overshadowed by higher



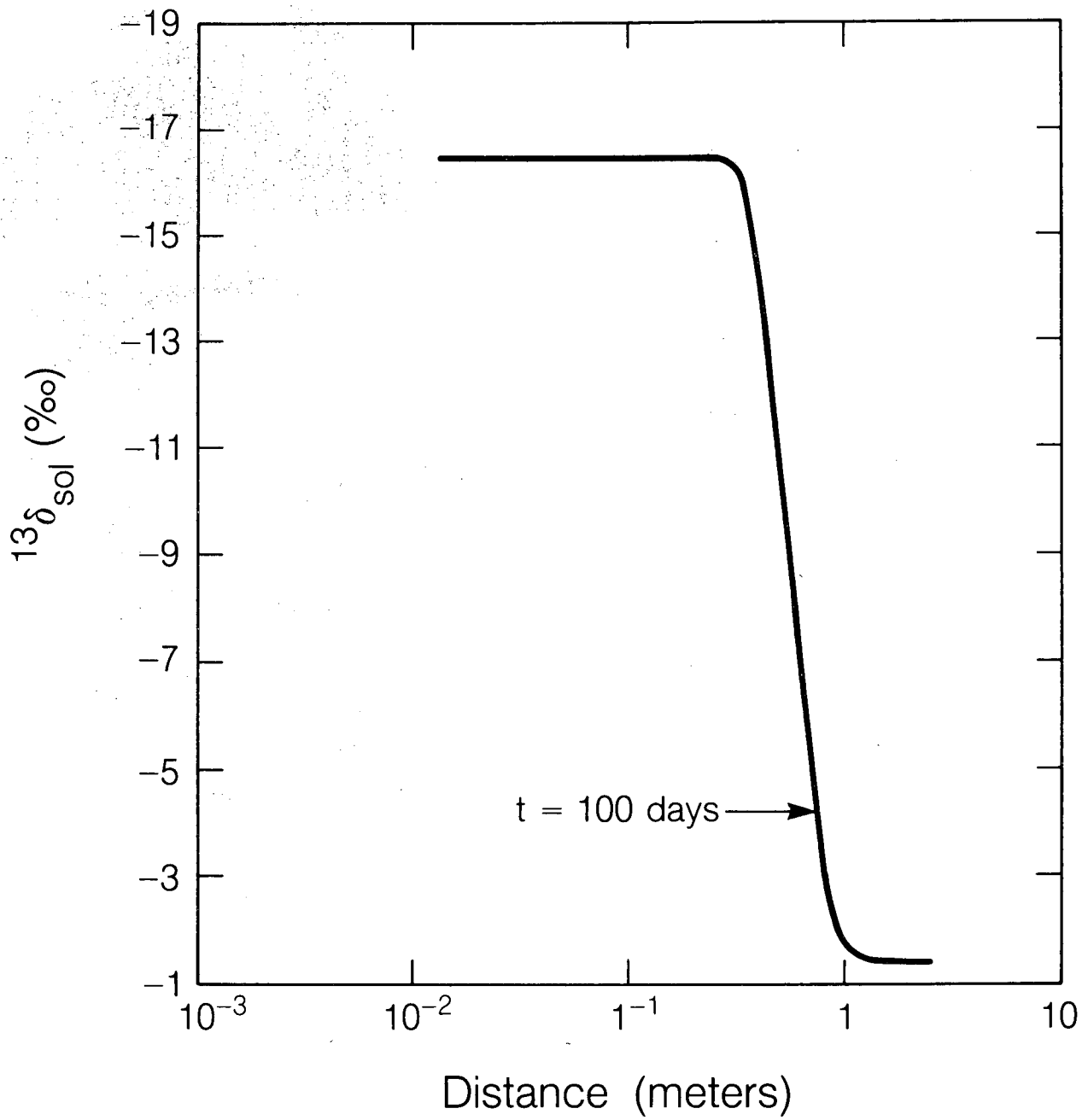
XBL 8610-12645

Fig. 17. pH variations vs. time.



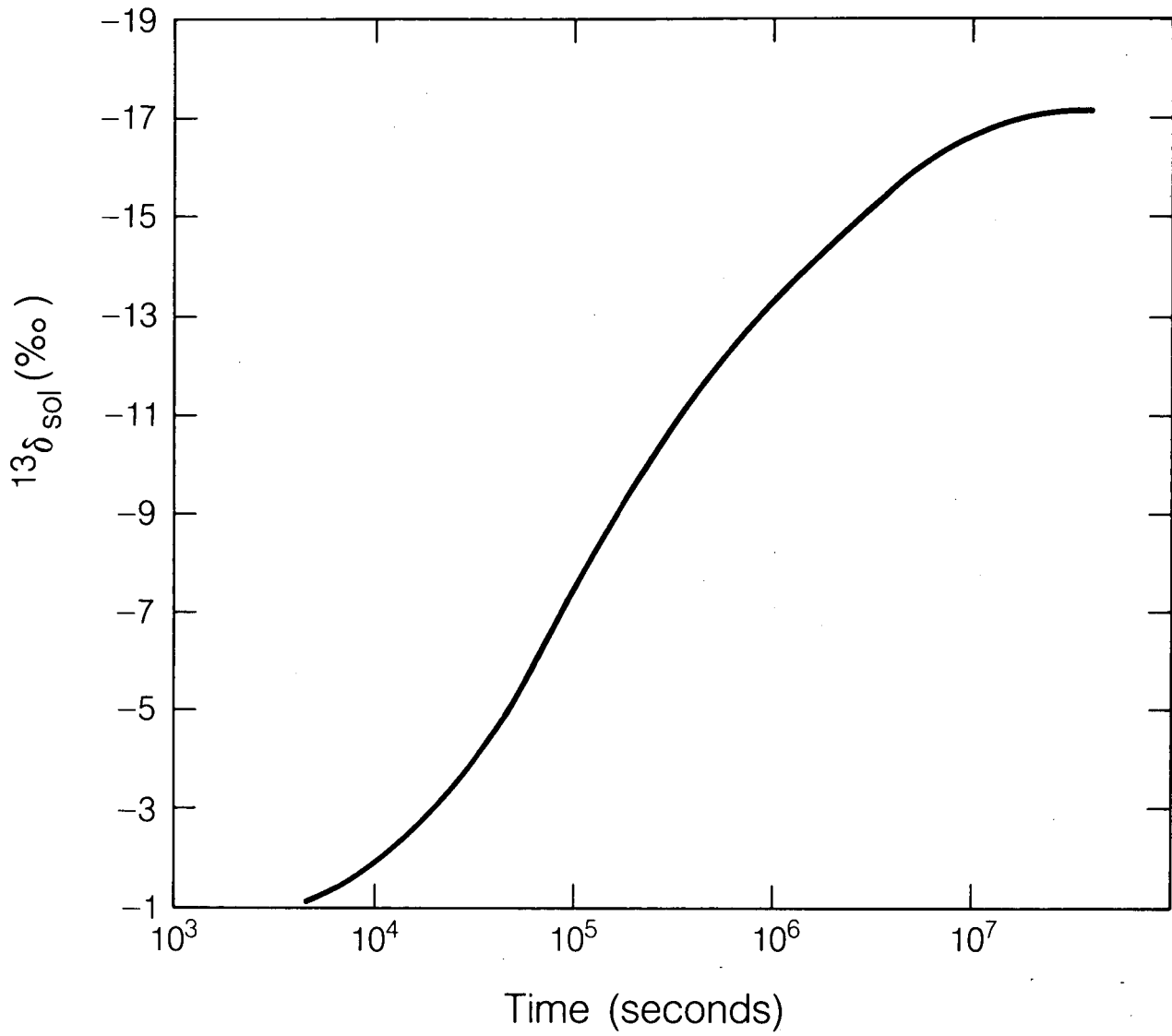
XBL 8610-12641

Fig. 18. Profile of θ_d along the flow path at two different times, ${}^{13}\delta_s$, ${}^{13}\delta_{\text{sol}}$ and c_T describe ${}^{13}\delta$ of rocks, ${}^{13}\delta$ of the infiltrating water and the total carbonate concentration of the solute.



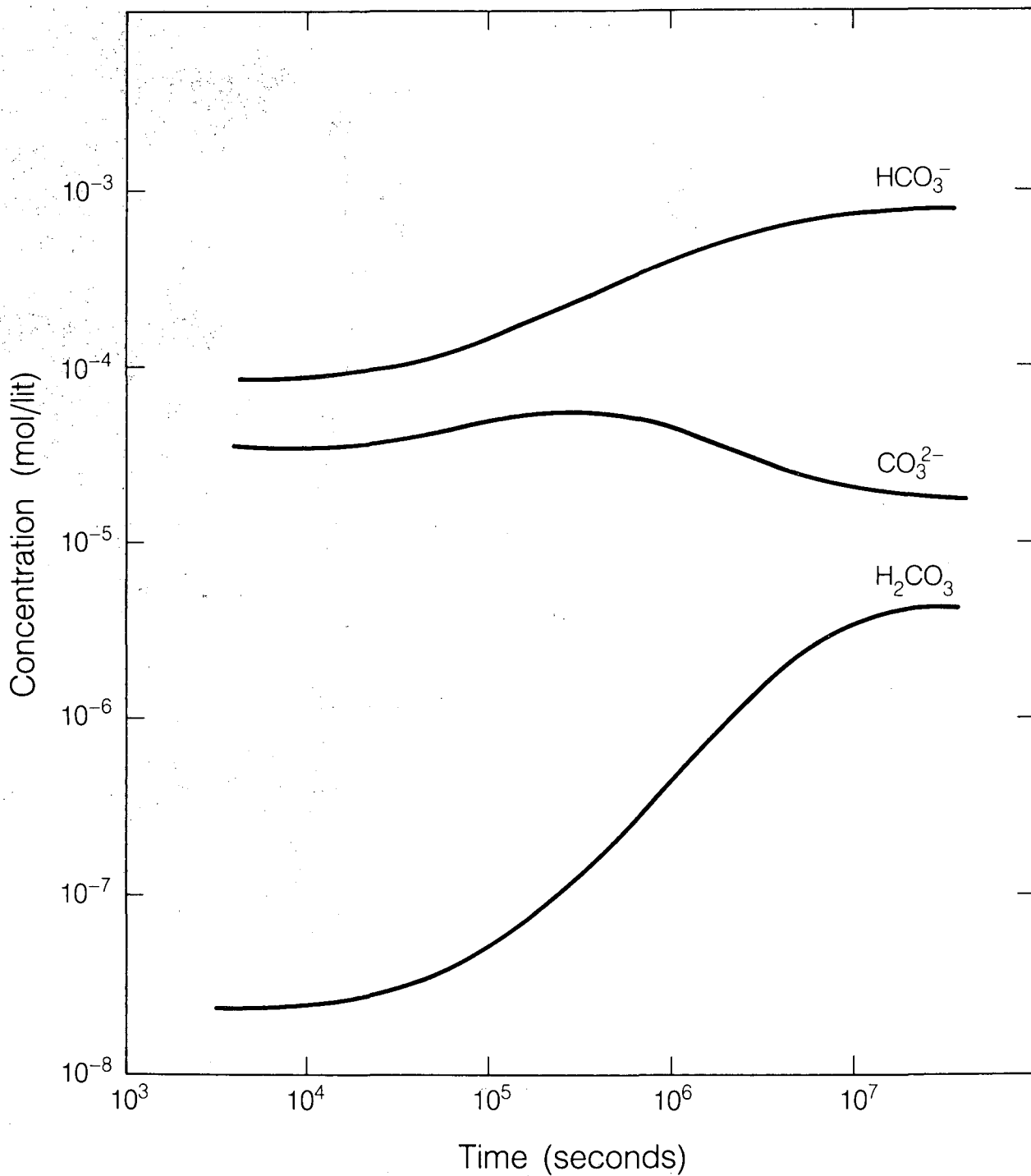
XBL 8610-12646

Fig. 19. Profile of $^{13}\delta_{\text{sol}}$ along the flow path for 100 days.



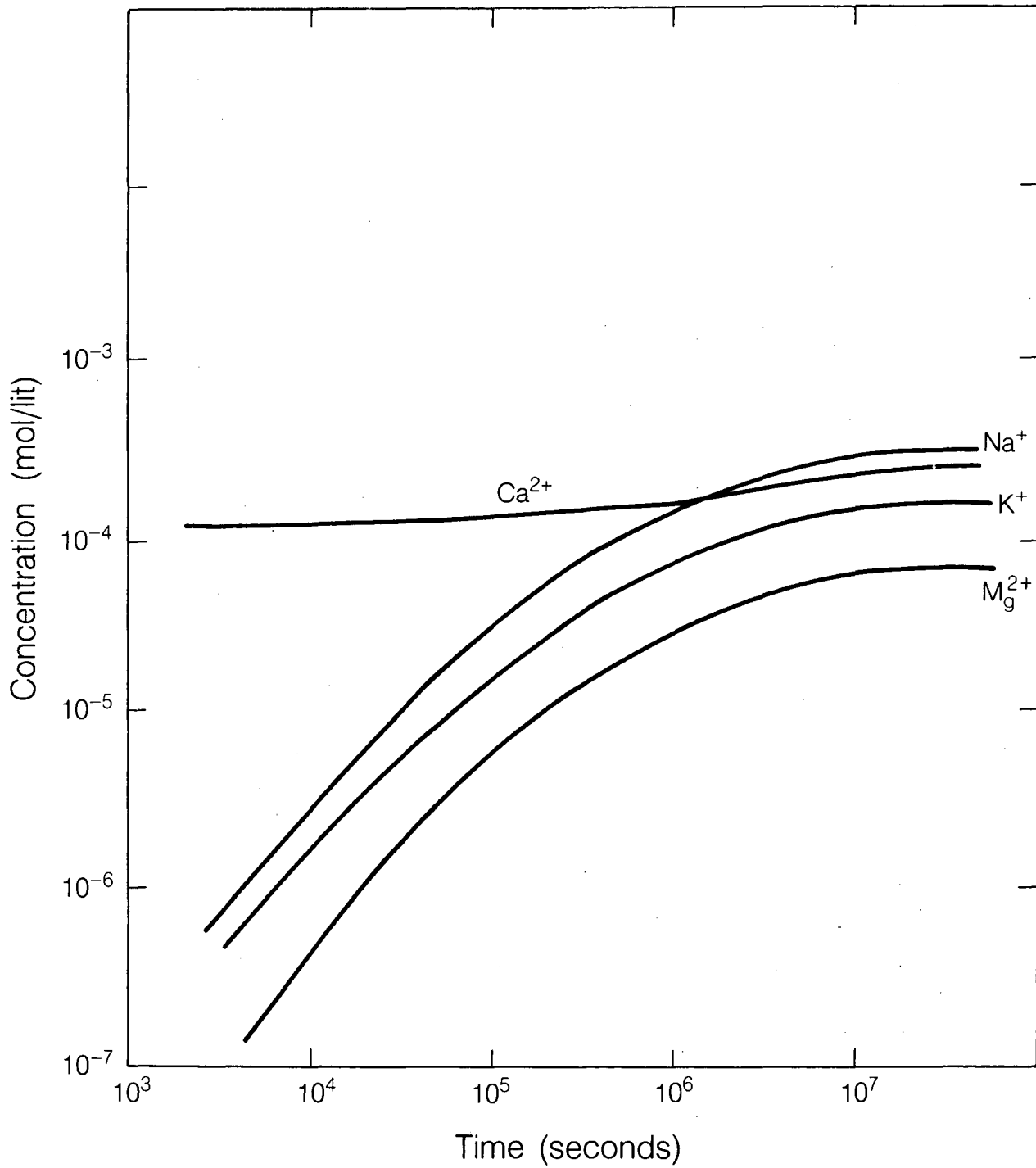
XBL 8610-12647

Fig. 20. Breakthrough of the solution shift in the percolating water.



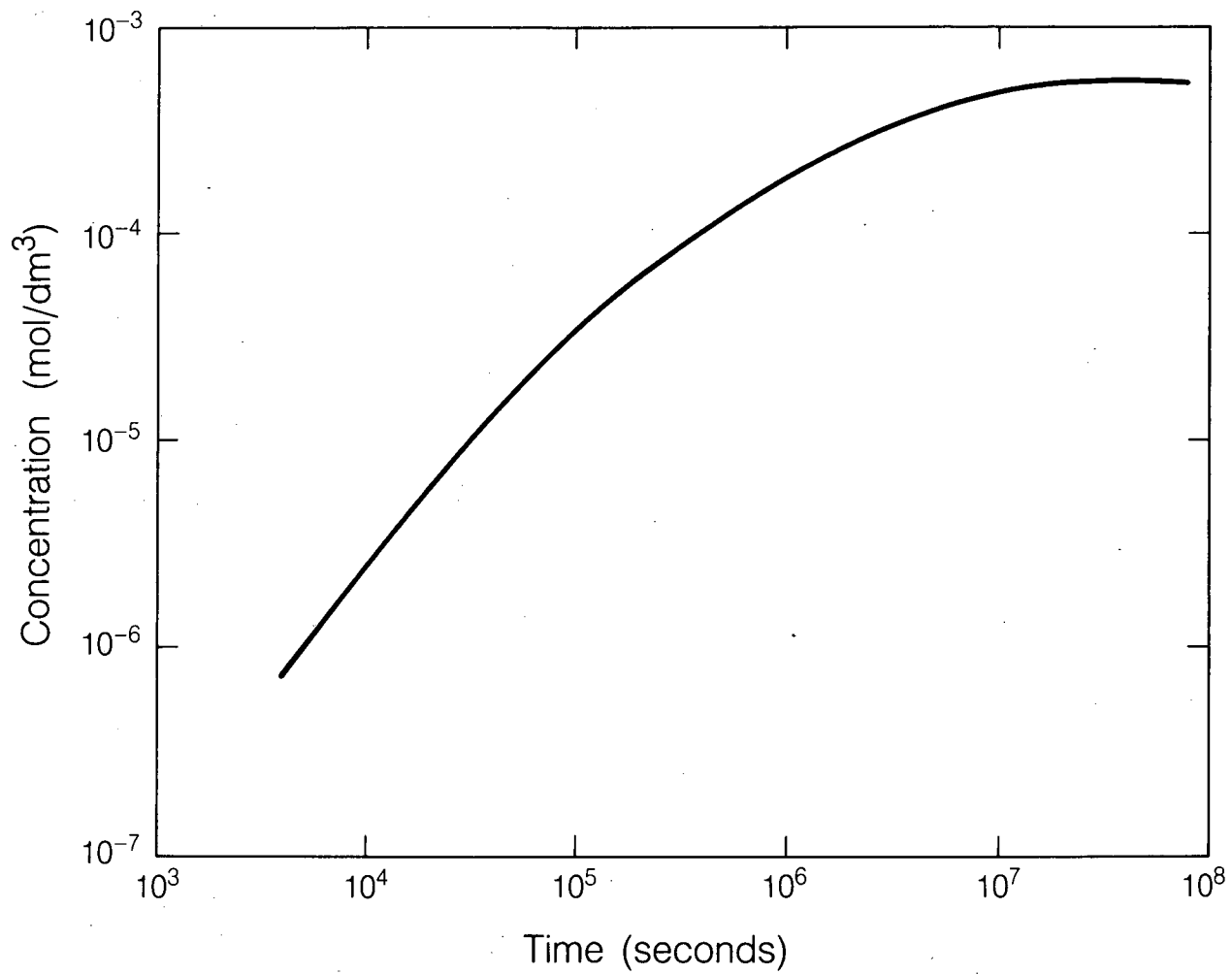
XBL 8610-12655

Fig. 21. Breakthrough of the aqueous carbonate species near the inflow boundary.



XBL 8610-12657

Fig. 22. Breakthrough of Mg^{2+} , Na^+ , Ca^{2+} and K^+ concentrations near the inflow boundary.



XBL 8610-12651

Fig. 23. Breakthrough of dissolved SiO₂ near the inflow boundary.

concentrations of the recharge water cations, as can be noticed in Fig. 22. Variation of the dissolved silica concentration in time is depicted in Fig. 23. Since the maximum solubility of amorphous silica in the in situ water at 30°C is about 2.10×10^{-3} M, the concentration of the amorphous silica in the water can only reach this level. However, because of convection, the breakthrough curve for a point near the inflow point shows the concentration stabilizing at around twice the incoming concentration (under saturated), as depicted in Fig. 23. Details of this application are provided in Appendix 10.

CONCLUSION

In this work, the geochemical equilibrium reactive transport code CHEMTRN was thoroughly revised, modified and supplemented. Specifically, the work included the following.

1. Thorough revision and optimization of the solution algorithms.
2. Options for reversible kinetic calcite and silica dissolution and irreversible glass dissolution added.
3. Option for oxidation-reduction added.
4. Option for carbon stable isotope fractionation during transport added.
5. Option for non-isothermal transport added.

Each stage of the development was verified against other methods if possible, otherwise assessed by examination of the code's performance in a multitude of hypothetical problems. Accounts of the applications are given in graphic presentations and also in the tabulations of the Appendices.

This new version of the code is called CHMTRNS.

ACKNOWLEDGEMENTS

This work was carried out under U.S. Department of Energy Contract No. DE-AC03-76SF00098 via the DOE-Nevada Office in cooperation with USGS-Denver. The authors are grateful to Dr.C.F. Tsang for his guidance and continuous support throughout the project.

REFERENCES

- Benson, L.V., 1986. Unpublished., U.S.G.S. report.
- Carnahan, C.L., 1987a. Simulation of chemically reactive solute transport under conditions of changing temperature In C.-F. Tsang, ed., Coupled Processes Associated with Nuclear Waste Repositories, Academic Press, Inc., Orlando, Florida, p. 249-257.
- Carnahan, C.L., 1987b. Simulation of uranium transport with variable temperature and oxidation potential: The computer program THCC. In J.K. Bates and W.B. Seefeldt, eds., Scientific Basis for Nuclear Waste Management X, Materials Research Society Symposia Proceedings Vol. 84, Materials Research Society, Pittsburgh, Pennsylvania, p. 713-721.
- Cederberg, G.A., Street, R.L., and Leckie, J.O., 1985. A groundwater mass transport and equilibrium chemistry model for multicomponent systems. Water Resour. Res., v. 21, p. 1095-1104.
- Claassen, H.C., and White, A.F., 1979. Application of geochemical kinetic data to groundwater systems. A tuffaceous-rock system in southern Nevada. In E.A. Jenne, ed., Chemical Modeling in Aqueous Systems, ACS Symposium Series, No. 93, American Chemical Society, Washington, D.C., p. 771-793.
- Clarke, E.C.W., and Glew, D.N., 1966. Evaluation of thermodynamic functions from equilibrium constants. Trans. Faraday Soc., v. 62, p. 539-547.
- Crank, J., 1975, The Mathematics of Diffusion, Clarendon Press, Oxford.
- Davis, J.A., James, R.O. and Leckie, J.O. 1978, Surface Ionization and the Oxide/Water Interface. I. Computation of Electrical Double Layer Properties in Simple Electrolytes, J. Colloid and Interface

- Science, V. 63, p. 480-499.
- Deines, P., Langmuir, D., and Harmon, R.S., 1974, Stable Carbon Isotope Ratios and Existence of a Gas Phase in the Evolution of Carbonate Ground Waters, *Geochimica et Cosmochimica Acta*, V. 38, p. 1147-1164.
- James, R.V. and Rubin, Jacob, 1979. Applicability of Local Equilibrium Assumption to Transport Through Soils Affected by Ion Exchange: in Jenne, E.A., ed. *Chemical Modeling in Aqueous Systems: American Chemical Society, Washington, D.C., ACS Symposium Series 93*, p. 225-235.
- Kirkner, D.J., Theis, T.L., and Jennings, A.A., 1984. Multicomponent solute transport with sorption and soluble complexation. *Adv. Water Resour.*, v. 7, p. 120-125.
- Kirkner, D.J., Jennings, A.A., and Theis, T.L., 1985. Multisolute mass transport with chemical interaction kinetics. *J. Hydrology*, v. 76, p. 107-117.
- Miller, C.W., and Benson, L.V., 1983, Simulation of Solute Transport in a Chemically Reactive Heterogeneous System: Model Development and Application: *Water Resources Research*, V. 19, p. 381-391.
- Palciauskas, V.V., and Domenico, P.A., 1976, Solution Chemistry, Mass Transfer, and the Approach to Chemical Equilibrium in Porous Carbonate Rocks and Sediments: *Geological Society of America Bulletin*, V. 87, p. 207-214.
- Pearson, J.F., and Hanshaw, B.B., 1970, Sources of Dissolved Carbonate Species in Groundwater and Their Effects on Carbon-14 Dating, *Proceedings, Isotope Hydrology 1970*, p. 271-286, International Atomic Energy, Vienna.
- Plummer, L.N., Wigley, T.M.L. and Parkhurst, D.L., 1978. *The Kinetics*

- of Calcite Dissolution in CO₂ - Water System at 5° to 60°C and 0.0 to 1.0 ATM CO₂; American J. of Science, V. 278, p. 179-216.
- Rimstidt, J.D., and Barnes, H.L., 1980. The kinetics of silica-water reactions. Geochim. Cosmochim. Acta, v. 44, p. 1683-1699.
- Stumm, W., Morgan, J.J., 1970, Aquatic Chemistry, Wiley-Interscience, New York.
- Valette-Silver, J.N., Thompson, J.M., and Ball, J.W., 1981: Relationship between water chemistry and sediment mineralogy in the Cerro Prieto Geothermal Field: A Preliminary Report, in Proceedings of Third Symposium on the Cerro Prieto Geothermal Field, Baja California, Mexico, March 24-26, 1981, San Francisco, California, U.S.A. Lawrence Berkeley Laboratory, LBL-11967, p. 263.
- Wigley, T.M.L., 1975, Carbon 14 Dating from Closed and Open Systems, Water Resources Research, V. 11, No. 2, p. 324-328.

APPENDICES

INPUTS AND OUTPUTS OF SOLVED PROBLEMS

APPENDIX 1

SOIL WATER COMPOSITION

INPUT AND OUTPUT

INPUT

```

Static equilibrium CO2(gas) in water--Sinpart
UNITS      meter      sec.
type       0          0          0          0
iteration   100        100        100
Calc.crtia 1.0e-30      1.0e-03      20          10          5          1.75          5
grid       05         10.0         0.0
time       1          1.0          5.0
print time 1.0
physical   0.05         0.0          0.0
tran bound 0            0
temp bound 0            0
isothermal 0
Intl.      10.0
leach      0            0
WORD       blank
no.species 3            0            0            3            0            2            0
CO2(g)     0.0          0            23.1623e-023.1623e-02  23.1623e-023.1623e-02
H+         1.0          0            2            1.0e-05      1.0e-05      2            1.0e-05      1.0e-05
OH-        -80.3723-1.395e+03  32.5514-3.181e-02
           3.24e-10  3.24e-10
H2CO3      0            1.0          0.0          0.0
           87.598   -1055.95    -38.7233.4506e-02
           0.0            0.0
HC03-      0            1.0          0.0          1.0
           127.844   -532.58    -52.2593.1543e-02
           0.0            0.0
CO3--      0            +1.0         0.0          2.0
           281.934   -3619.68   -112.5486.2045e-02
           0.0            0.0
    
```

OUTPUT

1Static equilibrium CO2(gas) in water--Sinpart

unit of length is meter unit of time is sec.

inner boundary is constant concentration outer boundary is constant initial concentration

dispersion coefficient= 0.1v+ 0. fluid velocity = 0. number of grid points = 5

number of print outs = 1
given at the following times= 1.000

errsqr= 0.10e-29 climit= 0.10e-02 iterj= 20 iterm= 10 iterd= 5 dtmult= 0.17e+01 ndiv= 5

number of sites(ion-exchange) 0.0000 number of sites(edl model) 0.0000
this simulation is isothermal, temperature = 10.

2 bare ions 0 sorbing ions (ionex) 0 sorbing ions (edl model)

component	charge	kinetic code	initial condition type	initial condition value	boundary condition type	boundary condition value
CO2(g)	0.	0	2	3.1623e-02	2	3.1623e-02
H+	1.	0	2	1.0000e-05	2	1.0000e-05

4 complexes 0 sorbing complexes(ionex) 0 sorbing complexes (edl model)

complex	charge	kcode	stoichiometry		
OH-	-1.	0	0.	0.	1.
H2CO3	0.	0	1.	0.	0.
HC03-	-1.	0	1.	0.	1.
CO3--	-2.	0	1.	0.	2.

** spatial grid **

0. 2.500 5.000 7.500 10.00

OUTPUT

1

initial conditions
temp= 10.00

component	total aqueous conc.	bare ion concentration	sorbed concentration		act. coef.	kd(ion ex)	kd(edl)
			(ionex)	(edl)			
CO2(g)	0.3162e-01	0.3009e-01	0.	0.	1.000	0.	0.
H+	0.1000e-04	0.1000e-04	0.	0.	0.9915	0.	0.
OH-	0.5637e-04	0.3296e-09	0.	0.	0.9915	0.	0.
complex	valence	aqueous conc.	sorption(io)	sorption(edl)			
H2CO3	0.	0.1473e-02	0.	0.			
HCO3-	-1.000	0.5637e-04	0.	0.			
CO3--	-2.000	0.1865e-09	0.	0.			

to have a net balance of zero charge, other species must be present (although not participating in the chemical reactions) with a total concentration times charge of 0.464e-04

7/4

1

boundary or influx conditions
temp= 10.00

component	total aqueous conc.	bare ion concentration	sorbed concentration		act. coef.	kd(ion ex)	kd(edl)
			(ionex)	(edl)			
CO2(g)	0.3162e-01	0.3009e-01	0.	0.	1.000	0.	0.
H+	0.1000e-04	0.1000e-04	0.	0.	0.9915	0.	0.
OH-	0.5637e-04	0.3296e-09	0.	0.	0.9915	0.	0.
complex	valence	aqueous conc.	sorption(io)	sorption(edl)			
H2CO3	0.	0.1473e-02	0.	0.			
HCO3-	-1.000	0.5637e-04	0.	0.			
CO3--	-2.000	0.1865e-09	0.	0.			

to have a net balance of zero charge, other species must be present (although not participating in the chemical reactions) with a total concentration times charge of 0.464e-04

APPENDIX 2

KINETIC DISSOLUTION OF CALCITE DURING REACTIVE TRANSPORT
INPUT AND OUTPUT

Table of Chemical Reactions

1. Equilibrium chemical reaction

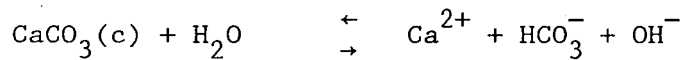
complexation



dissociation of water



2. Kinetic chemical reactions (Plummer et al, 1978)



Net rate of dissolution:

$$R = k_1 a_{\text{H}^+} + k_2 a_{\text{H}_2\text{CO}_3^0} + k_3 a_{\text{H}_2\text{O}} - k_4 a_{\text{Ca}^{2+}} a_{\text{HCO}_3^-}$$

INPUT

```

Partitioned Isothl.Kin. Calcite Diss.Tran.Int.shitsol=-24.5,shifts=1.0-sdypartd
UNITS      me      year
  type      0      1      0      1
iteration    100    100    100
Calc.crtia  1.0e-30 1.0e-03 20      10      5      1.75      5
grid        20      10.0  836.6835
time        14 1.585e-10 1.0e-03
print time  1.142e-05 1.142e-04 1.141e-03 4.566e-03 1.141e-02 2.740e-02 5.479e-02
print time  1.370e-01 2.740e-01 4.110e-01 5.480e-01 6.849e-01 8.219e-01 9.589e-01
Physical    0.1 1.0e-10 0.1e+01
tran bound  1      0
temp bound  0
isothermal  0
Intl. temp  10.0
leach       0      0
WORD        tpkin
**Carbonate Diss. Rate Data next 7 lines
1 PARAMS    5      100.0  4      prepc
CDATS       19.8  6.383  10.377  8.446 3.154e+04
2 INXI(i)   2      0  09  0  0  0  5  8
Carbonate1  -1.32  0  0  0  0  0
           2  -4.59  0  0  0  0
           3  -6.94  0  0  0  0
           4  0.0  0  0  0  0
WORD        blank
In.Sh.Info  -24.5  1.0
Iso.Ratio1  -0.91e-03 6.3
           2  -4.54e-03 1099.0
           3  -3.40e-03 870.0
           4  -3.63e-03 1194.0
no.species  7      0      0      2      1      2      0
Na+         1.0  0  2  1.0e-03 1.0e-03 2  1.0e-03 1.0e-03
H+          1.0  0  2  8.653e-05 1.237e-10 1. 1.0e-05 1.0e-05
Co3--       -2.0  31  31.0122e-02 3.521e-05 3 1.529e-03 1.865e-10
neg.KI      0.0  32  1 1.000e-10 1.000e-10 1 3.899e-02 3.899e-02
Ca++        2.0  0  31.0122e-02 1.217e-04 3  0.0  0.0
Cl-         -1.0  0  4  1.0e-03 1.0e-03 0  1.0e-03 1.0e-03
OH-         -13.990  0.0  0.0  0.0
           8.653e-05 3.296e-10
HC03-      33  0.0  1.0  1.0  0.0  0.0  0.0  0.0
           10.337  0.0  0.0  0.0
           8.649e-05 5.637e-05
H2C03      34  0.0  2.0  1.0  0.0  0.0  0.0  0.0
           16.700  0.0  0.0  0.0
           2.359e-08 1.473e-03
CaC03      10  0.0  0.0  1.0  0.0  1.0  0.0  0.0
           -8.446  0.0  0.0  0.0
           .01  0.0

```

77

OUTPUT

1Partitioned Isothl.Kin. Calcite Diss.Tran.Int.shitsol=-24.5,shifts=1.0-sdypartd

unit of length is meter unit of time is year

kinetics of rev. precipitate dissolution considered

inner boundary is constant flux outer' boundry is constant initial concentration

dispersion coefficient= 0.1v+ 0.10e-09 fluid velocity = 1.00 number of grid points = 20

number of print outs = 14

given at the following times= 0.1142e-040.1142e-030.1141e-020.4566e-020.1141e-010.2740e-010.5479e-010.1370
0.2740 0.4110 0.5480 0.6849 0.8219 0.9589

errsq= 0.10e-29 climit= 0.10e-02 iterj= 20 iterm= 10 iterd= 5 dtmult= 0.17e+01 ndiv= 5

number of sites(ion-exchange) 0.0000 number of sites(edl model) 0.0000
this simulation is isothermal, temperature = 10.

6 bare ions 0 sorbing ions (ionex) 0 sorbing ions (edl model)

component	charge	kinetic code	initial condition type	initial condition value	boundary condition type	boundary condition value
Na+	1.	0	2	1.0000e-03	2	1.0000e-03
H+	1.	0	2	8.6530e-05	1	1.0000e-05
Co3--	-2.	31	3	1.0122e-02	3	1.5290e-03
neg.KI	0.	32	1	1.0000e-10	1	3.8990e-02
Ca++	2.	0	3	1.0122e-02	3	0.
Cl-	-1.	0	4	1.0000e-03	0	1.0000e-03

3 complexes 0 sorbing complexes(ionex) 0 sorbing complexes (edl model)

complex	charge	kcode	stoichiometry						
OH-	-1.	0	0.	0.	0.	0.	0.	0.	1.
HCO3-	-1.	33	0.	1.	1.	0.	0.	0.	0.
H2CO3	0.	34	0.	2.	1.	0.	0.	0.	0.

OUTPUT

1 solid precipitates

precipitate	kinetic code	stoichiometry							
CaCO3	10	0.0	0.0	1.0	0.0	1.0	0.0	0.0	0.0

Calcite dissolution information:

no of terms in the rate formula = 4
 no of other additional data needed = 5
 representative surface parameter = 0.100e+03
 xdiag = prepc

additional data for rate calculation

0.198e+02 0.638e+01 0.104e+02 0.845e+01 0.315e+05

binary element nos. of the terms of the rate equation
 2 0 9 0 0 0 5 8

coefficients in log function of thermodynamic constants

-1.320	0.000	0.000	0.000
-4.590	0.000	0.000	0.000
-6.940	0.000	0.000	0.000
0.000	0.000	0.000	0.000

C-13 Fractionation parameters:

shiftr= -24.5000 shifts= 1.0000

coefficients in log function of thermodynamic constants

-0.001	6.300
-0.005	1099.000
-0.003	870.000
-0.004	1194.000

** spatial grid **

0.	0.5086e-02	0.1233e-01	0.2266e-01	0.3738e-01	0.5835e-01	0.8823e-01	0.1308	0.1915	0.2780
0.4012	0.5768	0.8271	1.184	1.692	2.416	3.448	4.918	7.014	10.00

OUTPUT

1

initial conditions
temp= 10.00

component	total aqueous conc.	bare ion concentration	sorbed concentration		act. coef.	kd(ion ex)	kd(edl)
			(ionex)	(edl)			
Na+	0.1000e-02	0.1000e-02	0.	0.	0.9596	0.	0.
H+	0.8653e-04	0.1188e-09	0.	0.	0.9596	0.	0.
Co3--	0.1260e-03	0.3953e-04	0.	0.	0.8478	0.	0.
neg.KI	0.1000e-09	0.1000e-09	0.	0.	1.000	0.	0.
Ca++	0.1260e-03	0.1260e-03	0.	0.	0.8478	0.	0.
Cl-	0.9930e-03	0.9930e-03	0.	0.	0.9596	0.	0.
OH-	0.9357e-04	0.9357e-04	0.	0.	0.9596	0.	0.
complex	valence	aqueous conc.	sorption(io)		sorption(edl)		
HC03-	-1.000	0.8649e-04	0.	0.			
H2C03	0.	0.2182e-07	0.	0.			

precipitate equivalent moles/liter solution

CaC03 0.100e-01

to have a net balance of zero charge, other species must be present (although not participating in the chemical reactions) with a total concentration times charge of 0.

1

boundary or influx conditions
temp= 10.00

component	total aqueous conc.	bare ion concentration	sorbed concentration		act. coef.	kd(ion ex)	kd(edl)
			(ionex)	(edl)			
Na+	0.1000e-02	0.1000e-02	0.	0.	0.9647	0.	0.
H+	0.3000e-02	0.1000e-04	0.	0.	0.9647	0.	0.
Co3--	0.1529e-02	0.3617e-09	0.	0.	0.8661	0.	0.
neg.KI	0.3899e-01	0.3899e-01	0.	0.	1.000	0.	0.
Ca++	0.1000e-34	0.1000e-34	0.	0.	0.8661	0.	0.
Cl-	0.9930e-03	0.9930e-03	0.	0.	0.9647	0.	0.
OH-	0.1100e-08	0.1100e-08	0.	0.	0.9647	0.	0.
complex	valence	aqueous conc.	sorption(io)		sorption(edl)		
HC03-	-1.000	0.6806e-04	0.	0.			
H2C03	0.	0.1461e-02	0.	0.			

precipitate equivalent moles/liter solution

CaC03 0.

to have a net balance of zero charge, other species must be present (although not participating in the chemical reactions) with a total concentration times charge of 0.510e-04

OUTPUT

1 time= 1.53364e-05 delt= 6.5728e-06 concentration of species in moles/liter solution

species	distance								
	0.000	0.005	0.012	0.023	0.037	0.058	0.088	0.131	0.192
Na+	1.0000e-03	1.0000e-03	1.0000e-03	1.0000e-03	1.0000e-03	1.0000e-03	1.0000e-03	1.0000e-03	1.0000e-03
H+	1.3124e-10	1.1913e-10	1.1878e-10	1.1878e-10	1.1878e-10	1.1877e-10	1.1877e-10	1.1877e-10	1.1877e-10
Co3--	3.9226e-05	3.9528e-05	3.9531e-05	3.9532e-05	3.9532e-05	3.9532e-05	3.9533e-05	3.9534e-05	3.9535e-05
neg.KI	2.2358e-04	6.9224e-06	9.0205e-08	6.3719e-10	1.0154e-10	1.0000e-10	1.0000e-10	1.0000e-10	1.0000e-10
Ca++	1.2532e-04	1.2602e-04	1.2604e-04	1.2604e-04	1.2604e-04	1.2604e-04	1.2604e-04	1.2605e-04	1.2605e-04
Cl-	9.9296e-04	9.9296e-04	9.9296e-04	9.9296e-04	9.9296e-04	9.9296e-04	9.9296e-04	9.9296e-04	9.9296e-04
OH-	8.4680e-05	9.3288e-05	9.3565e-05	9.3569e-05	9.3570e-05	9.3570e-05	9.3571e-05	9.3572e-05	9.3573e-05
shftsol	-6.6748e-01	9.4519e-01	9.9928e-01	9.9999e-01	1.0000e+00	1.0000e+00	1.0000e+00	1.0000e+00	1.0000e+00
shift0	-3.0951e+00	-1.6555e+00	-1.6068e+00	-1.6062e+00	-1.6062e+00	-1.6062e+00	-1.6062e+00	-1.6062e+00	-1.6063e+00
shift1	6.9231e+00	8.3772e+00	8.4263e+00	8.4270e+00	8.4270e+00	8.4269e+00	8.4269e+00	8.4269e+00	8.4269e+00
shift2	5.1964e+00	6.6480e+00	6.6970e+00	6.6977e+00	6.6977e+00	6.6977e+00	6.6977e+00	6.6976e+00	6.6976e+00

complexes

HCO3-	9.4832e-05	8.6739e-05	8.6490e-05	8.6487e-05	8.6487e-05	8.6488e-05	8.6489e-05	8.6490e-05	8.6491e-05
H2CO3	2.6435e-08	2.1948e-08	2.1820e-08	2.1818e-08	2.1818e-08	2.1818e-08	2.1818e-08	2.1818e-08	2.1818e-08

precipitates

CaCO3	9.9960e-03	9.9960e-03	9.9960e-03	9.9960e-03	9.9960e-03	9.9960e-03	9.9960e-03	9.9960e-03	9.9960e-03
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species	distance								
	0.278	0.401	0.577	0.827	1.184	1.692	2.416	3.448	4.918
Na+	1.0000e-03	1.0000e-03	1.0000e-03	1.0000e-03	1.0000e-03	1.0000e-03	1.0000e-03	1.0000e-03	1.0000e-03
H+	1.1877e-10	1.1876e-10	1.1876e-10	1.1875e-10	1.1874e-10	1.1873e-10	1.1871e-10	1.1868e-10	1.1864e-10
Co3--	3.9537e-05	3.9540e-05	3.9543e-05	3.9549e-05	3.9556e-05	3.9567e-05	3.9582e-05	3.9602e-05	3.9631e-05
neg.KI	1.0000e-10	1.0000e-10	1.0000e-10	1.0000e-10	1.0000e-10	1.0000e-10	1.0000e-10	1.0000e-10	1.0000e-10
Ca++	1.2605e-04	1.2606e-04	1.2607e-04	1.2608e-04	1.2609e-04	1.2612e-04	1.2615e-04	1.2619e-04	1.2625e-04
Cl-	9.9296e-04	9.9296e-04	9.9296e-04	9.9296e-04	9.9296e-04	9.9296e-04	9.9296e-04	9.9296e-04	9.9296e-04
OH-	9.3575e-05	9.3578e-05	9.3583e-05	9.3588e-05	9.3597e-05	9.3609e-05	9.3628e-05	9.3649e-05	9.3681e-05
shftsol	1.0000e+00	1.0000e+00	1.0000e+00	1.0000e+00	1.0000e+00	1.0000e+00	1.0000e+00	1.0000e+00	1.0000e+00
shift0	-1.6063e+00	-1.6064e+00	-1.6064e+00	-1.6066e+00	-1.6067e+00	-1.6069e+00	-1.6073e+00	-1.6077e+00	-1.6083e+00
shift1	8.4268e+00	8.4268e+00	8.4267e+00	8.4266e+00	8.4264e+00	8.4262e+00	8.4259e+00	8.4254e+00	8.4248e+00
shift2	6.6976e+00	6.6975e+00	6.6974e+00	6.6973e+00	6.6971e+00	6.6969e+00	6.6966e+00	6.6961e+00	6.6955e+00

complexes

HCO3-	8.6493e-05	8.6496e-05	8.6500e-05	8.6506e-05	8.6515e-05	8.6527e-05	8.6543e-05	8.6567e-05	8.6599e-05
H2CO3	2.1818e-08	2.1818e-08	2.1818e-08	2.1819e-08	2.1819e-08	2.1819e-08	2.1819e-08	2.1820e-08	2.1820e-08

precipitates

CaCO3	9.9959e-03	9.9959e-03	9.9959e-03	9.9959e-03	9.9959e-03	9.9959e-03	9.9959e-03	9.9958e-03	9.9957e-03
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OUTPUT

species	7.014	10.000
Na+	1.0000e-03	1.0000e-03
H+	1.1858e-10	1.1878e-10
Co3--	3.9670e-05	3.9531e-05
neg.KI	1.0000e-10	1.0000e-10
Ca++	1.2634e-04	1.2604e-04
Cl-	9.9296e-04	9.9296e-04
OH-	9.3725e-05	9.3568e-05
shftsol	1.0000e+00	1.0000e+00
shift0	-1.6092e+00	-1.6062e+00
shift1	8.4239e+00	8.4270e+00
shift2	6.6946e+00	6.6977e+00

complexes

HC03-	8.6643e-05	8.6486e-05
H2C03	2.1821e-08	2.1818e-08

precipitates

CaC03	9.9957e-03	9.9960e-03
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1 time= 9.59502e-01 delt= 1.0000e-03 concentration of species in moles/liter solution

species	distance								
	0.000	0.005	0.012	0.023	0.037	0.058	0.088	0.131	0.192
Na+	1.0000e-03	1.0000e-03	1.0000e-03	1.0000e-03	1.0000e-03	1.0000e-03	1.0000e-03	1.0000e-03	1.0000e-03
H+	4.0317e-07	3.7337e-07	3.3418e-07	2.8477e-07	2.2620e-07	1.6272e-07	1.0240e-07	5.6526e-08	3.4790e-08
Co3--	1.5940e-07	1.8116e-07	2.1735e-07	2.8109e-07	4.0213e-07	6.5450e-07	1.2370e-06	2.6046e-06	4.5485e-06
neg.KI	3.8759e-02	3.8747e-02	3.8730e-02	3.8703e-02	3.8663e-02	3.8598e-02	3.8492e-02	3.8309e-02	3.7970e-02
Ca++	5.3053e-04	5.5805e-04	5.9856e-04	6.5816e-04	7.4483e-04	8.6627e-04	1.0210e-03	1.1761e-03	1.2592e-03
Cl-	9.9296e-04	9.9296e-04	9.9296e-04	9.9296e-04	9.9296e-04	9.9296e-04	9.9296e-04	9.9296e-04	9.9296e-04
OH-	2.8354e-08	3.0666e-08	3.4341e-08	4.0433e-08	5.1138e-08	7.1523e-08	1.1449e-07	2.0882e-07	3.4048e-07
shftsol	-1.7903e+01	-1.7651e+01	-1.7292e+01	-1.6787e+01	-1.6100e+01	-1.5218e+01	-1.4212e+01	-1.3303e+01	-1.2816e+01
shift0	-2.2366e+01	-2.1926e+01	-2.1298e+01	-2.0416e+01	-1.9213e+01	-1.7669e+01	-1.5905e+01	-1.4316e+01	-1.3471e+01
shift1	-1.2542e+01	-1.2097e+01	-1.1463e+01	-1.0572e+01	-9.3573e+00	-7.7977e+00	-6.0157e+00	-4.4104e+00	-3.5574e+00
shift2	-1.4235e+01	-1.3791e+01	-1.3158e+01	-1.2269e+01	-1.1056e+01	-9.4992e+00	-7.7202e+00	-6.1176e+00	-5.2661e+00

complexes

HC03-	1.1189e-03	1.1738e-03	1.2547e-03	1.3737e-03	1.5467e-03	1.7889e-03	2.0969e-03	2.4041e-03	2.5658e-03
H2C03	9.3146e-04	9.0353e-04	8.6244e-04	8.0195e-04	7.1393e-04	5.9038e-04	4.3234e-04	2.7175e-04	1.7788e-04

precipitates

CaC03	8.8854e-03	7.3739e-03	6.4036e-03	5.1685e-03	3.7090e-03	2.2616e-03	1.6124e-03	3.8159e-03	8.1646e-03
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OUTPUT

species	distance									
	0.278	0.401	0.577	0.827	1.184	1.692	2.416	3.448	4.918	
Na+	1.0000e-03	1.0000e-03	1.0000e-03	1.0000e-03	1.0000e-03	1.0000e-03	1.0000e-03	1.0000e-03	1.0000e-03	1.0000e-03
H+	2.9503e-08	2.7295e-08	2.2853e-08	1.2491e-08	2.5866e-09	2.8882e-10	1.2993e-10	1.1800e-10	1.1725e-10	
Co3--	5.3675e-06	5.5907e-06	6.0126e-06	7.7430e-06	1.5425e-05	3.6023e-05	4.0673e-05	4.0668e-05	4.0662e-05	
neg.KI	3.7289e-02	3.5783e-02	3.2031e-02	2.2355e-02	9.3401e-03	2.0714e-03	2.4407e-04	1.5860e-05	5.9138e-07	
Ca++	1.2613e-03	1.2201e-03	1.1102e-03	8.0746e-04	3.6297e-04	1.4593e-04	1.2842e-04	1.2842e-04	1.2844e-04	
Cl-	9.9296e-04	9.9296e-04	9.9296e-04	9.9296e-04	9.9296e-04	9.9296e-04	9.9296e-04	9.9296e-04	9.9296e-04	
OH-	4.0153e-07	4.3326e-07	5.1501e-07	9.2882e-07	4.3713e-06	3.8542e-05	8.5559e-05	9.4209e-05	9.4812e-05	
shftsol	-1.2691e+01	-1.2640e+01	-1.2536e+01	-1.2274e+01	-1.1808e+01	-8.1188e+00	-7.6875e-01	8.7710e-01	9.9540e-01	
shift0	-1.3257e+01	-1.3169e+01	-1.2991e+01	-1.2556e+01	-1.2034e+01	-9.4304e+00	-3.2143e+00	-1.7413e+00	-1.6347e+00	
shift1	-3.3408e+00	-3.2520e+00	-3.0719e+00	-2.6334e+00	-2.1055e+00	5.2413e-01	6.8027e+00	8.2905e+00	8.3981e+00	
shift2	-5.0499e+00	-4.9612e+00	-4.7815e+00	-4.3437e+00	-3.8167e+00	-1.1916e+00	5.0762e+00	6.5614e+00	6.6689e+00	

complexes

HCO3-	2.5673e-03	2.4825e-03	2.2568e-03	1.6348e-03	7.0999e-04	1.9102e-04	9.7290e-05	8.8349e-05	8.7775e-05
H2CO3	1.5092e-04	1.3525e-04	1.0344e-04	4.1547e-05	3.8339e-06	1.1699e-07	2.6841e-08	2.2137e-08	2.1853e-08

precipitates

CaCO3	9.8299e-03	1.0013e-02	1.0020e-02	1.0020e-02	1.0032e-02	1.0016e-02	9.9947e-03	9.9936e-03	9.9936e-03
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distance

species	7.014	10.000
Na+	1.0000e-03	1.0000e-03
H+	1.1722e-10	1.1878e-10
Co3--	4.0662e-05	3.9531e-05
neg.KI	1.3181e-08	1.0000e-10
Ca++	1.2844e-04	1.2604e-04
Cl-	9.9296e-04	9.9296e-04
OH-	9.4835e-05	9.3568e-05
shftsol	9.9990e-01	1.0000e+00
shift0	-1.6307e+00	-1.6062e+00
shift1	8.4022e+00	8.4270e+00
shift2	6.6730e+00	6.6977e+00

complexes

HCO3-	8.7753e-05	8.6486e-05
H2CO3	2.1842e-08	2.1818e-08

precipitates

CaCO3	9.9940e-03	9.9960e-03
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APPENDIX 3

EQUILIBRIUM CALCITE DISSOLUTION DURING REACTIVE TRANSPORT

INPUT AND SAMPLE OUTPUT

INPUT

```

Partitioned Isothl.Equi.Calcite Diss.Tran.Int.shitsol=-24.5,shifts=1.0-sdyparte
UNITS      meter      year
type       0          1          0          1
iteration   100       100       100
Calc.crtia 1.0e-30   1.0e-03   20          10          5          1.75          5
grid       20          10.0     836.6835
time       14 1.585e-10  1.0e-03
print time 1.142e-05 1.142e-04 1.141e-03 4.566e-03 1.141e-02 2.740e-02 5.479e-02
print time 1.370e-01 2.740e-01 4.110e-01 5.480e-01 6.849e-01 8.219e-01 9.589e-01
Physical   0.1      1.0e-10  0.1e+01
tran bound 1          0
temp bound 0
isothermal 0
Intl. temp 10.0
leach      0          0
WORD       blank
In.Sh.Info -24.5      1.0
Iso.Ratio1 -0.91e-03  6.3
           2 -4.54e-03  1099.0
           3 -3.40e-03  870.0
           4 -3.63e-03  1194.0
no.species 7          0          0          2          1          2          0
Na+        1.0 0 2 1.0e-03 1.0e-03 2 1.0e-03 1.0e-03
H+         1.0 0 2 8.653e-05 1.237e-10 1 1.0e-05 1.0e-05
Co3--      -2.0 31 3 1.0001217 3.521e-05 3 1.529e-03 1.865e-10
neg.KI     0.0 32 1 1.000e-10 1.000e-10 1 3.899e-02 3.899e-02
Ca++       2.0 0 3 1.0001217 1.217e-04 3 0.0 0.0
Cl-        -1.0 0 4 1.0e-03 1.0e-03 0 1.0e-03 1.0e-03
OH-        -13.990 0.0 0.0 0.0 0.0
           8.653e-05 3.296e-10
HC03-     33 0.0 1.0 1.0 0.0 0.0 0.0 0.0
           10.337 0.0 0.0 0.0
           8.649e-05 5.637e-05
H2C03     34 0.0 2.0 1.0 0.0 0.0 0.0 0.0
           16.700 0.0 0.0 0.0
           2.359e-08 1.473e-03
CaC03     10 0.0 0.0 1.0 0.0 1.0 0.0 0.0
           -8.446 0.0 0.0 0.0
           1.0 0.0

```

OUTPUT

1Partitioned Isothl.Equi.Calcite Diss.Tran.Int.shitsol=-24.5,shifts=1.0-sdyparte

unit of length is meter unit of time is year

inner boundary is constant flux outer' boundry is constant initial concentration

dispersion coefficient= 0.1v+ 0.10e-09 fluid velocity = 1.00 number of grid points = 20

number of print outs = 14
 given at the following times= 0.1142e-04 0.1142e-03 0.1141e-02 0.4566e-02 0.1141e-01 0.2740e-01 0.5479e-01 0.1370
 0.2740 0.4110 0.5480 0.6849 0.8219 0.9589

errsqr= 0.10e-29 climit= 0.10e-02 iterj= 20 iterm= 10 iterd= 5 dtmult= 0.17e+01 ndiv= 5

number of sites(ion-exchange) 0.0000 number of sites(edl model) 0.0000
 this simulation is isothermal, temperature = 10.

87

6 bare ions 0 sorbing ions (ionex) 0 sorbing ions (edl model)

component	charge	kinetic code	initial condition		boundary condition	
			type	value	type	value
Na+	1.	0	2	1.0000e-03	2	1.0000e-03
H+	1.	0	2	8.6530e-05	1	1.0000e-05
Co3--	-2.	31	3	1.0001e+00	3	1.5290e-03
neg.KI	0.	32	1	1.0000e-10	1	3.8990e-02
Ca++	2.	0	3	1.0001e+00	3	0.
Cl-	-1.	0	4	1.0000e-03	0	1.0000e-03

OUTPUT

3	complexes	0	sorbing complexes(ionex)							0	sorbing complexes (edl model)
complex	charge	kcode	stoichiometry								
OH-	-1.	0	0.	0.	0.	0.	0.	0.	0.	1.	
HCO3-	-1.	33	0.	1.	1.	0.	0.	0.	0.	0.	
H2CO3	0.	34	0.	2.	1.	0.	0.	0.	0.	0.	

1 solid precipitates

precipitate	kinetic code	stoichiometry						
CaCO3	10	0.0	0.0	1.0	0.0	1.0	0.0	0.0

C-13 Fractionation parameters:

shiftr= -24.5000 shifts= 1.0000

∞

coefficients in log function of thermodynamic constants

-0.001	6.300
-0.005	1090.000
-0.003	870.000
-0.004	1194.000

** spatial grid **

0.	0.5086e-02	0.1233e-01	0.2266e-01	0.3738e-01	0.5835e-01	0.8823e-01	0.1308	0.1915	0.2780
0.4012	0.5768	0.8271	1.184	1.692	2.416	3.448	4.918	7.014	10.00

OUTPUT

1

initial conditions
temp= 10.00

component	total aqueous conc.	bare ion concentration	sorbed concentration		act. coef.	kd(ion ex)	kd(edl)
			(ionex)	(edl)			
Na+	0.1000e-02	0.1000e-02	0.	0.	0.9596	0.	0.
H+	0.8653e-04	0.1188e-09	0.	0.	0.9596	0.	0.
Co3--	0.1260e-03	0.3953e-04	0.	0.	0.8478	0.	0.
neg.KI	0.1000e-09	0.1000e-09	0.	0.	1.000	0.	0.
Ca++	0.1260e-03	0.1260e-03	0.	0.	0.8478	0.	0.
Cl-	0.9930e-03	0.9930e-03	0.	0.	0.9596	0.	0.
OH-	0.9357e-04	0.9357e-04	0.	0.	0.9596	0.	0.

complex	valence	aqueous conc.	sorption(io)	sorption(edl)
HCO3-	-1.000	0.8649e-04	0.	0.
H2CO3	0.	0.2182e-07	0.	0.

precipitate equivalent moles/liter solution

CaCO3 1.00

to have a net balance of zero charge, other 'species must be present (although not participating in the chemical reactions) with a total concentration times charge of 0.

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1

boundary or influx conditions
temp= 10.00

component	total aqueous conc.	bare ion concentration	sorbed concentration		act. coef.	kd(ion ex)	kd(edl)
			(ionex)	(edl)			
Na+	0.1000e-02	0.1000e-02	0.	0.	0.9647	0.	0.
H+	0.3000e-02	0.1000e-04	0.	0.	0.9647	0.	0.
Co3--	0.1529e-02	0.3617e-09	0.	0.	0.8661	0.	0.
neg.KI	0.3899e-01	0.3899e-01	0.	0.	1.000	0.	0.
Ca++	0.1000e-34	0.1000e-34	0.	0.	0.8661	0.	0.
Cl-	0.9930e-03	0.9930e-03	0.	0.	0.9647	0.	0.
OH-	0.1100e-08	0.1100e-08	0.	0.	0.9647	0.	0.

complex	valence	aqueous conc.	sorption(io)	sorption(edl)
HCO3-	-1.000	0.6806e-04	0.	0.
H2CO3	0.	0.1461e-02	0.	0.

precipitate equivalent moles/liter solution

CaCO3 0.

to have a net balance of zero charge, other 'species must be present (although not participating in the chemical reactions) with a total concentration times charge of 0.510e-04

OUTPUT

1 time= 1.53364e-05 delt= 6.5728e-06 concentration of species in moles/liter solution

species	distance									
	0.000	0.005	0.012	0.023	0.037	0.058	0.088	0.131	0.192	
Na+	1.0000e-03	1.0000e-03	1.0000e-03	1.0000e-03	1.0000e-03	1.0000e-03	1.0000e-03	1.0000e-03	1.0000e-03	1.0000e-03
H+	1.3069e-10	1.1913e-10	1.1878e-10	1.1878e-10	1.1878e-10	1.1878e-10	1.1878e-10	1.1878e-10	1.1878e-10	1.1878e-10
Co3--	3.9545e-05	3.9534e-05	3.9531e-05	3.9531e-05	3.9531e-05	3.9531e-05	3.9531e-05	3.9531e-05	3.9531e-05	3.9531e-05
neg.KI	2.2358e-04	6.9224e-06	9.0205e-08	6.3719e-10	1.0154e-10	1.0000e-10	1.0000e-10	1.0000e-10	1.0000e-10	1.0000e-10
Ca++	1.2600e-04	1.2603e-04	1.2604e-04	1.2604e-04	1.2604e-04	1.2604e-04	1.2604e-04	1.2604e-04	1.2604e-04	1.2604e-04
Cl-	9.9296e-04	9.9296e-04	9.9296e-04	9.9296e-04	9.9296e-04	9.9296e-04	9.9296e-04	9.9296e-04	9.9296e-04	9.9296e-04
OH-	8.5041e-05	9.3295e-05	9.3565e-05	9.3568e-05	9.3568e-05	9.3568e-05	9.3568e-05	9.3568e-05	9.3568e-05	9.3568e-05
shftsol	-6.5907e-01	9.4519e-01	9.9928e-01	9.9999e-01	1.0000e+00	1.0000e+00	1.0000e+00	1.0000e+00	1.0000e+00	1.0000e+00
shift0	-3.0941e+00	-1.6556e+00	-1.6068e+00	-1.6062e+00	-1.6062e+00	-1.6062e+00	-1.6062e+00	-1.6062e+00	-1.6062e+00	-1.6062e+00
shift1	6.9241e+00	8.3770e+00	8.4263e+00	8.4270e+00	8.4270e+00	8.4270e+00	8.4270e+00	8.4270e+00	8.4270e+00	8.4270e+00
shift2	5.1974e+00	6.6478e+00	6.6971e+00	6.6977e+00	6.6977e+00	6.6977e+00	6.6977e+00	6.6977e+00	6.6977e+00	6.6977e+00

complexes

HCO3-	9.5193e-05	8.6746e-05	8.6490e-05	8.6486e-05	8.6486e-05	8.6486e-05	8.6486e-05	8.6486e-05	8.6486e-05	8.6486e-05
H2CO3	2.6423e-08	2.1948e-08	2.1820e-08	2.1818e-08	2.1818e-08	2.1818e-08	2.1818e-08	2.1818e-08	2.1818e-08	2.1818e-08

precipitates

CaCO3	9.9999e-01	1.0000e+00	1.0000e+00	1.0000e+00	1.0000e+00	1.0000e+00	1.0000e+00	1.0000e+00	1.0000e+00	1.0000e+00
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species	distance									
	0.278	0.401	0.577	0.827	1.184	1.692	2.416	3.448	4.918	

Na+	1.0000e-03	1.0000e-03	1.0000e-03	1.0000e-03	1.0000e-03	1.0000e-03	1.0000e-03	1.0000e-03	1.0000e-03	1.0000e-03
H+	1.1878e-10	1.1878e-10	1.1878e-10	1.1878e-10	1.1878e-10	1.1878e-10	1.1878e-10	1.1878e-10	1.1878e-10	1.1878e-10
Co3--	3.9531e-05	3.9531e-05	3.9531e-05	3.9531e-05	3.9531e-05	3.9531e-05	3.9531e-05	3.9531e-05	3.9531e-05	3.9531e-05
neg.KI	1.0000e-10	1.0000e-10	1.0000e-10	1.0000e-10	1.0000e-10	1.0000e-10	1.0000e-10	1.0000e-10	1.0000e-10	1.0000e-10
Ca++	1.2604e-04	1.2604e-04	1.2604e-04	1.2604e-04	1.2604e-04	1.2604e-04	1.2604e-04	1.2604e-04	1.2604e-04	1.2604e-04
Cl-	9.9296e-04	9.9296e-04	9.9296e-04	9.9296e-04	9.9296e-04	9.9296e-04	9.9296e-04	9.9296e-04	9.9296e-04	9.9296e-04
OH-	9.3568e-05	9.3568e-05	9.3568e-05	9.3568e-05	9.3568e-05	9.3568e-05	9.3568e-05	9.3568e-05	9.3568e-05	9.3568e-05
shftsol	1.0000e+00	1.0000e+00	1.0000e+00	1.0000e+00	1.0000e+00	1.0000e+00	1.0000e+00	1.0000e+00	1.0000e+00	1.0000e+00
shift0	-1.6062e+00	-1.6062e+00	-1.6062e+00	-1.6062e+00	-1.6062e+00	-1.6062e+00	-1.6062e+00	-1.6062e+00	-1.6062e+00	-1.6062e+00
shift1	8.4270e+00	8.4270e+00	8.4270e+00	8.4270e+00	8.4270e+00	8.4270e+00	8.4270e+00	8.4270e+00	8.4270e+00	8.4270e+00
shift2	6.6977e+00	6.6977e+00	6.6977e+00	6.6977e+00	6.6977e+00	6.6977e+00	6.6977e+00	6.6977e+00	6.6977e+00	6.6977e+00

complexes

HCO3-	8.6486e-05	8.6486e-05	8.6486e-05	8.6486e-05	8.6486e-05	8.6486e-05	8.6486e-05	8.6486e-05	8.6486e-05	8.6486e-05
H2CO3	2.1818e-08	2.1818e-08	2.1818e-08	2.1818e-08	2.1818e-08	2.1818e-08	2.1818e-08	2.1818e-08	2.1818e-08	2.1818e-08

precipitates

CaCO3	1.0000e+00	1.0000e+00	1.0000e+00	1.0000e+00	1.0000e+00	1.0000e+00	1.0000e+00	1.0000e+00	1.0000e+00	1.0000e+00
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OUTPUT

species	7.014	10.000
Na+	1.0000e-03	1.0000e-03
H+	1.1878e-10	1.1878e-10
Co3--	3.9531e-05	3.9531e-05
neg.KI	1.0000e-10	1.0000e-10
Ca++	1.2604e-04	1.2604e-04
Cl-	9.9296e-04	9.9296e-04
OH-	9.3568e-05	9.3568e-05
shftsol	1.0000e+00	1.0000e+00
shift0	-1.6062e+00	-1.6062e+00
shift1	8.4270e+00	8.4270e+00
shift2	6.6977e+00	6.6977e+00

distance

complexes

HCO3-	8.6486e-05	8.6486e-05
H2CO3	2.1818e-08	2.1818e-08

precipitates

CaCO3	1.0000e+00	1.0000e+00
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1 time= 9.58995e-01 delt= 1.0000e-03 concentration of species in moles/liter solution

species	distance									
	0.000	0.005	0.012	0.023	0.037	0.058	0.088	0.131	0.192	
Na+	1.0000e-03	1.0000e-03	1.0000e-03	1.0000e-03	1.0000e-03	1.0000e-03	1.0000e-03	1.0000e-03	1.0000e-03	1.0000e-03
H+	3.2701e-08	3.2686e-08	3.2662e-08	3.2627e-08	3.2574e-08	3.2489e-08	3.2350e-08	3.2109e-08	3.1664e-08	3.1664e-08
Co3--	4.9922e-06	4.9932e-06	4.9946e-06	4.9968e-06	5.0002e-06	5.0056e-06	5.0145e-06	5.0300e-06	5.0592e-06	5.0592e-06
neg.KI	3.8759e-02	3.8747e-02	3.8729e-02	3.8703e-02	3.8662e-02	3.8597e-02	3.8491e-02	3.8308e-02	3.7968e-02	3.7968e-02
Ca++	1.2958e-03	1.2955e-03	1.2950e-03	1.2942e-03	1.2931e-03	1.2914e-03	1.2884e-03	1.2834e-03	1.2740e-03	1.2740e-03
Cl-	9.9296e-04	9.9296e-04	9.9296e-04	9.9296e-04	9.9296e-04	9.9296e-04	9.9296e-04	9.9296e-04	9.9296e-04	9.9296e-04
OH-	3.6278e-07	3.6295e-07	3.6320e-07	3.6358e-07	3.6416e-07	3.6508e-07	3.6661e-07	3.6928e-07	3.7433e-07	3.7433e-07
shftsol	-1.2765e+01	-1.2765e+01	-1.2764e+01	-1.2763e+01	-1.2762e+01	-1.2760e+01	-1.2757e+01	-1.2752e+01	-1.2742e+01	-1.2742e+01
shift0	-1.3384e+01	-1.3384e+01	-1.3383e+01	-1.3381e+01	-1.3379e+01	-1.3376e+01	-1.3371e+01	-1.3361e+01	-1.3344e+01	-1.3344e+01
shift1	-3.4695e+00	-3.4689e+00	-3.4680e+00	-3.4667e+00	-3.4646e+00	-3.4612e+00	-3.4558e+00	-3.4463e+00	-3.4288e+00	-3.4288e+00
shift2	-5.1784e+00	-5.1778e+00	-5.1769e+00	-5.1755e+00	-5.1734e+00	-5.1701e+00	-5.1647e+00	-5.1552e+00	-5.1378e+00	-5.1378e+00

complexes

HCO3-	2.6390e-03	2.6383e-03	2.6374e-03	2.6359e-03	2.6336e-03	2.6299e-03	2.6239e-03	2.6135e-03	2.5943e-03	2.5943e-03
H2CO3	1.7171e-04	1.7159e-04	1.7141e-04	1.7113e-04	1.7071e-04	1.7004e-04	1.6895e-04	1.6708e-04	1.6359e-04	1.6359e-04

precipitates

CaCO3	4.9410e-01	1.0000e+00	1.0000e+00	1.0000e+00	1.0000e+00	1.0000e+00	1.0000e+00	1.0000e+00	1.0000e+00	1.0000e+00
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OUTPUT

species	distance								
	0.278	0.401	0.577	0.827	1.184	1.692	2.416	3.448	4.918
Na+	1.0000e-03	1.0000e-03	1.0000e-03	1.0000e-03	1.0000e-03	1.0000e-03	1.0000e-03	1.0000e-03	1.0000e-03
H+	3.0775e-08	2.8827e-08	2.4105e-08	1.3110e-08	2.6959e-09	2.9611e-10	1.3181e-10	1.1957e-10	1.1881e-10
Co3--	5.1192e-06	5.2601e-06	5.6687e-06	7.3504e-06	1.4762e-05	3.4879e-05	3.9539e-05	3.9537e-05	3.9531e-05
neg.KI	3.7286e-02	3.5777e-02	3.2019e-02	2.2335e-02	9.3257e-03	2.0668e-03	2.4336e-04	1.5803e-05	5.8893e-07
Ca++	1.2551e-03	1.2127e-03	1.1042e-03	8.0436e-04	3.6143e-04	1.4365e-04	1.2602e-04	1.2602e-04	1.2604e-04
Cl-	9.9296e-04	9.9296e-04	9.9296e-04	9.9296e-04	9.9296e-04	9.9296e-04	9.9296e-04	9.9296e-04	9.9296e-04
OH-	3.8483e-07	4.1010e-07	4.8811e-07	8.8478e-07	4.1936e-06	3.7585e-05	8.4318e-05	9.2944e-05	9.3545e-05
shftsol	-1.2722e+01	-1.2678e+01	-1.2568e+01	-1.2293e+01	-1.1825e+01	-8.1980e+00	-7.9521e-01	8.7521e-01	9.9533e-01
shift0	-1.3309e+01	-1.3233e+01	-1.3044e+01	-1.2585e+01	-1.2046e+01	-9.4820e+00	-3.2153e+00	-1.7187e+00	-1.6104e+00
shift1	-3.3938e+00	-3.3165e+00	-3.1261e+00	-2.6627e+00	-2.1182e+00	4.7197e-01	6.8017e+00	8.3133e+00	8.4227e+00
shift2	-5.1028e+00	-5.0257e+00	-4.8356e+00	-4.3729e+00	-3.8294e+00	-1.2437e+00	5.0752e+00	6.5842e+00	6.6935e+00

complexes

HCO3-	2.5554e-03	2.4684e-03	2.2456e-03	1.6294e-03	7.0839e-04	1.8970e-04	9.5994e-05	8.7080e-05	8.6508e-05
H2CO3	1.5674e-04	1.4208e-04	1.0859e-04	4.3471e-05	3.9874e-06	1.1914e-07	2.6873e-08	2.2116e-08	2.1829e-08

precipitates

CaCO3	1.0000e+00	1.0000e+00	1.0000e+00	1.0000e+00	1.0000e+00	1.0000e+00	1.0000e+00	1.0000e+00	1.0000e+00
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distance

species	7.014	10.000
Na+	1.0000e-03	1.0000e-03
H+	1.1878e-10	1.1878e-10
Co3--	3.9531e-05	3.9531e-05
neg.KI	1.3119e-08	1.0000e-10
Ca++	1.2604e-04	1.2604e-04
Cl-	9.9296e-04	9.9296e-04
OH-	9.3568e-05	9.3568e-05
shftsol	9.9990e-01	1.0000e+00
shift0	-1.6063e+00	-1.6062e+00
shift1	8.4269e+00	8.4270e+00
shift2	6.6976e+00	6.6977e+00

complexes

HCO3-	8.6487e-05	8.6486e-05
H2CO3	2.1818e-08	2.1818e-08

precipitates

CaCO3	1.0000e+00	1.0000e+00
-------	------------	------------

APPENDIX 4

KINETIC CALCITE DISSOLUTION IN BATCH REACTIONS

INPUT AND SAMPLE OUTPUT

INPUT

```

Partitioned Isothl.Kin. Calcite Diss.NoTr.Int.shitsol=-24.5,shifts=1.0-sdypartk
UNITS      meter      year
type       0          1          0          1
iteration   100        100        100
Calc.crtia 1.0e-30    1.0e-03    20         10         5         1.75         5
grid       5          6.56       0.0
time       14        1.585e-10  1.0e-03
print time 1.142e-05    1.142e-04  1.141e-03  4.566e-03  1.141e-02  2.740e-02  5.479e-02
print time 1.370e-01    2.740e-01  4.110e-01  5.480e-01  6.849e-01  8.219e-01  9.589e-01
Physical   1.0e-20    1.0e-20    1.0e-20
tran bound 1          0
temp bound 0
isothermal 0
Intl. temp 10.0
leach      0          0
WORD      tpkin
**Carbonate Diss. Rate Data next 7 lines
1 PARAMS  5          100.0      4          prepc
2 CDATS   19.8        6.383     10.377     8.446 3.154e+04
3 INXI(i) 2          0          09         0          0          5          8
Carbonate1 -1.32       0          0          0
           2          -4.59      0          0          0
           3          -6.94      0          0          0
           4          0.0        0          0          0
WORD      blank
In.Sh.Info -24.5        1.0
Iso.Ratio1 -0.91e-03   6.3
           2          -4.54e-03  1099.0
           3          -3.40e-03  870.0
           4          -3.63e-03  1194.0
no.species 7          0          0          2          1          2          0
Na+        1.0      0          2          1.0e-03    1.0e-03    2          1.0e-03    1.0e-03
H+         1.0      0          1          1.000e-05  1.000e-05  1          1.0e-05    1.0e-05
Co3--      -2.0     31         3          1.529e-03  1.865e-10  3          1.529e-03  1.865e-10
neg.KI     0.0     32         1          3.899e-02  3.899e-02  1          3.899e-02  3.899e-02
Ca++       2.0     0          3          1.000e-19  1.000e-19  3          0.0        0.0
Cl-        -1.0     0          1          1.0e-03    1.0e-03    0          1.0e-03    1.0e-03
OH-        -13.990   0.0        0.0        0.0        0.0
           3.296e-10  3.296e-10
HC03-     33      0.0      1.0      1.0      0.0      0.0      0.0      0.0
           10.337     0.0        0.0        0.0
           5.637e-05  5.637e-05
H2CO3     34      0.0      2.0      1.0      0.0      0.0      0.0
           16.700     0.0        0.0        0.0
           1.473e-03  1.473e-03
CaCO3     10      0.0      0.0      1.0      0.0      1.0      0.0      0.0
           -8.446     0.0        0.0        0.0
           0.0        0.0

```

OUTPUT

1Partitioned Isothl.Kin. Calcite Diss.NoTr.Int.shitsol=-24.5,shifts=1.0-sdypartk

unit of length is meter unit of time is year

kinetics of rev. precipitate dissolution considered

inner boundary is constant flux outer' boundry is constant initial concentration

dispersion coefficient= 0.0v+ 0.10e-19 fluid velocity = 0.100e-19 number of grid points = 5

number of print outs = 14
 given at the following times= 0.1142e-04 0.1142e-03 0.1141e-02 0.4566e-02 0.1141e-01 0.2740e-01 0.5479e-01 0.1370
 0.2740 0.4110 0.5480 0.6849 0.8219 0.9589

errsqr= 0.10e-29 climit= 0.10e-02 iterj= 20 iterm= 10 iterd= 5 dtmult= 0.17e+01 ndiv=

number of sites(ion-exchange) 0.0000 number of sites(edl model) 0.0000
 this simulation is isothermal, temperature = 10.

95

6 bare ions 0 sorbing ions (ionex) 0 sorbing ions (edl model)

component	charge	kinetic code	initial condition type	initial condition value	boundary condition type	boundary condition value
Na+	1.	0	2	1.0000e-03	2	1.0000e-03
H+	1.	0	1	1.0000e-05	1	1.0000e-05
Co3--	-2.	31	3	1.5290e-03	3	1.5290e-03
neg.KI	0.	32	1	3.8990e-02	1	3.8990e-02
Ca++	2.	0	3	1.0000e-19	3	0.
Cl-	-1.	0	1	1.0000e-03	0	1.0000e-03

3 complexes 0 sorbing complexes(ionex) 0 sorbing complexes (edl model)

complex	charge	kcode	stoichiometry						
OH-	-1.	0	0.	0.	0.	0.	0.	0.	1.
HCO3-	-1.	33	0.	1.	1.	0.	0.	0.	0.
H2CO3	0.	34	0.	2.	1.	0.	0.	0.	0.

1 solid precipitates

OUTPUT

precipitate kinetic code stoichiometry
CaCO3 10 0.0 0.0 1.0 0.0 1.0 0.0 0.0

Calcite dissolution information:

no of terms in the rate formula = 4
no of other additional data needed = 5
representative surface parameter = 0.100e+03
xdiag = prepc

additional data for rate calculation

0.198e+02 0.638e+01 0.104e+02 0.845e+01 0.315e+05

binary element nos. of the terms of the rate equation
2 0 9 0 0 0 5 8

coefficients in log function of thermodynamic constants
-1.320 0.000 0.000 0.000
-4.590 0.000 0.000 0.000
-6.940 0.000 0.000 0.000
0.000 0.000 0.000 0.000

C-13 Fractionation parameters:

shiftr= -24.5000 shifts= 1.0000

coefficients in log function of thermodynamic constants
-0.001 6.300
-0.005 1099.000
-0.003 870.000
-0.004 1194.000

** spatial grid **

0. 1.640 3.280 4.920 6.560

OUTPUT

1

initial conditions
temp= 10.00

component	total aqueous conc.	bare ion concentration	sorbed concentration		act. coef.	kd(ion ex)	kd(edl)
			(ionex)	(edl)			
Na+	0.1000e-02	0.1000e-02	0.	0.	0.9646	0.	0.
H+	0.3000e-02	0.1000e-04	0.	0.	0.9646	0.	0.
Co3--	0.1529e-02	0.3619e-09	0.	0.	0.8657	0.	0.
neg.KI	0.3899e-01	0.3899e-01	0.	0.	1.000	0.	0.
Ca++	0.1000e-18	0.1000e-18	0.	0.	0.8657	0.	0.
Cl-	0.1000e-02	0.1000e-02	0.	0.	0.9646	0.	0.
OH-	0.1100e-08	0.1100e-08	0.	0.	0.9646	0.	0.
complex	valence	aqueous conc.	sorption(io)		sorption(edl)		
HCO3-	-1.000	0.6807e-04	0.	0.			
H2CO3	0.	0.1461e-02	0.	0.			

precipitate equivalent moles/liter solution

CaCO3 1.00

to have a net balance of zero charge, other 'species must be present (although not participating in the chemical reactions) with a total concentration times charge of 0.581e-04

1

boundary or influx conditions
temp= 10.00

component	total aqueous conc.	bare ion concentration	sorbed concentration		act. coef.	kd(ion ex)	kd(edl)
			(ionex)	(edl)			
Na+	0.1000e-02	0.1000e-02	0.	0.	0.9646	0.	0.
H+	0.3000e-02	0.1000e-04	0.	0.	0.9646	0.	0.
Co3--	0.1529e-02	0.3619e-09	0.	0.	0.8657	0.	0.
neg.KI	0.3899e-01	0.3899e-01	0.	0.	1.000	0.	0.
Ca++	0.1000e-34	0.1000e-34	0.	0.	0.8657	0.	0.
Cl-	0.1000e-02	0.1000e-02	0.	0.	0.9646	0.	0.
OH-	0.1100e-08	0.1100e-08	0.	0.	0.9646	0.	0.
complex	valence	aqueous conc.	sorption(io)		sorption(edl)		
HCO3-	-1.000	0.6807e-04	0.	0.			
H2CO3	0.	0.1461e-02	0.	0.			

precipitate equivalent moles/liter solution

CaCO3 0.

to have a net balance of zero charge, other 'species must be present (although not participating in the chemical reactions) with a total concentration times charge of 0.581e-04

OUTPUT

1 time= 1.53364e-05 delt= 6.5728e-06 concentration of species in moles/liter solution

species	distance									
	0.000	1.640	3.280	4.920	6.560	0.000	0.000	0.000	0.000	0.000
Na+	1.0000e-03	1.0000e-03	1.0000e-03	1.0000e-03	1.0000e-03	0.	0.	0.	0.	0.
H+	6.4738e-06	5.0116e-06	5.0116e-06	5.0116e-06	5.0116e-06	1.0000e-05	0.	0.	0.	0.
Co3--	8.5850e-10	1.4243e-09	1.4243e-09	1.4243e-09	1.4243e-09	3.6192e-10	0.	0.	0.	0.
neg.KI	3.8990e-02	3.8990e-02	3.8990e-02	3.8990e-02	3.8990e-02	3.8990e-02	0.	0.	0.	0.
Ca++	1.9809e-05	3.5175e-05	3.5175e-05	3.5175e-05	3.5175e-05	1.0000e-19	0.	0.	0.	0.
Cl-	1.0000e-03	1.0000e-03	1.0000e-03	1.0000e-03	1.0000e-03	0.	0.	0.	0.	0.
OH-	1.7019e-09	2.2013e-09	2.2013e-09	2.2013e-09	2.2013e-09	1.0998e-09	0.	0.	0.	0.
shftsol	-2.4174e+01	-2.3927e+01	-2.3927e+01	-2.3927e+01	-2.4500e+01	0.	0.	0.	0.	0.
shift0	-3.3236e+01	-3.2817e+01	-3.2817e+01	-3.2817e+01	-3.3778e+01	0.	0.	0.	0.	0.
shift1	-2.3521e+01	-2.3098e+01	-2.3098e+01	-2.3098e+01	-2.4068e+01	0.	0.	0.	0.	0.
shift2	-2.5195e+01	-2.4773e+01	-2.4773e+01	-2.4773e+01	-2.5742e+01	0.	0.	0.	0.	0.
complexes										
HCO3-	1.0416e-04	1.3343e-04	1.3343e-04	1.3343e-04	6.8070e-05	0.	0.	0.	0.	0.
H2CO3	1.4446e-03	1.4307e-03	1.4307e-03	1.4307e-03	1.4609e-03	0.	0.	0.	0.	0.
precipitates										
CaCO3	9.9998e-01	9.9996e-01	9.9996e-01	9.9996e-01	1.0000e+00	0.	0.	0.	0.	0.

OUTPUT

1 time= 8.21953e-01 delt= 1.0000e-03 concentration of species in moles/liter solution

species	distance					0.000	0.000	0.000	0.000
	0.000	1.640	3.280	4.920	6.560				
Na+	1.0000e-03	1.0000e-03	1.0000e-03	1.0000e-03	1.0000e-03	0.	0.	0.	0.
H+	3.1184e-08	3.1184e-08	3.1184e-08	3.1184e-08	1.0000e-05	0.	0.	0.	0.
Co3--	5.3028e-06	5.3028e-06	5.3028e-06	5.3028e-06	3.6192e-10	0.	0.	0.	0.
neg.KI	3.8990e-02	3.8990e-02	3.8990e-02	3.8990e-02	3.8990e-02	0.	0.	0.	0.
Ca++	1.3111e-03	1.3111e-03	1.3111e-03	1.3111e-03	1.0000e-19	0.	0.	0.	0.
Cl-	1.0000e-03	1.0000e-03	1.0000e-03	1.0000e-03	1.0000e-03	0.	0.	0.	0.
OH-	3.8071e-07	3.8071e-07	3.8071e-07	3.8071e-07	1.0998e-09	0.	0.	0.	0.
shftsol	-1.2728e+01	-1.2728e+01	-1.2728e+01	-1.2728e+01	-2.4500e+01	0.	0.	0.	0.
shift0	-1.3322e+01	-1.3322e+01	-1.3322e+01	-1.3322e+01	-3.3778e+01	0.	0.	0.	0.
shift1	-3.4062e+00	-3.4062e+00	-3.4062e+00	-3.4062e+00	-2.4068e+01	0.	0.	0.	0.
shift2	-5.1152e+00	-5.1152e+00	-5.1152e+00	-5.1152e+00	-2.5742e+01	0.	0.	0.	0.
complexes									
HCO3-	2.6693e-03	2.6693e-03	2.6693e-03	2.6693e-03	6.8070e-05	0.	0.	0.	0.
H2CO3	1.6550e-04	1.6550e-04	1.6550e-04	1.6550e-04	1.4609e-03	0.	0.	0.	0.
precipitates									
CaCO3	9.9869e-01	9.9869e-01	9.9869e-01	9.9869e-01	1.0000e+00	0.	0.	0.	0.

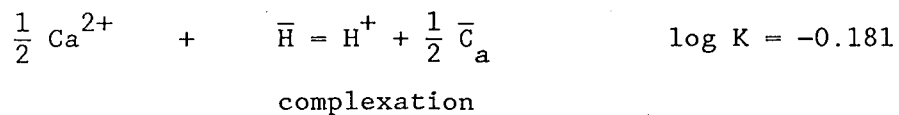
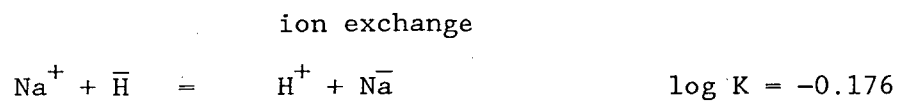
APPENDIX 5

KINETIC CALCITE PRECIPITATION DURING REACTIVE TRANSPORT

INPUT AND SAMPLE OUTPUT

Table of Chemical Reactions

1. Equilibrium chemical reaction



same as in Appendix 2

dissociation of water

same as in Appendix 2

2. Kinetic chemical reactions

Same rate rate formula as in problem 1 (in this case k_4 term will dominate and reverse reaction starts).

INPUT

```

Isothermal kinetic precip., aqueous complex, w. dissociation transport-chemd15t
UNITS      meter      year
type       0          1          0
iteration   100        100        100
Calc.crtia 1.0e-30      1.0e-03      20          10          5          1.75          5
Grid       20          10.0      836.68355
time       10          1.0e-10     1.0e-03
prin time  0.000001     0.000003    0.000005   0.000008   0.00001    0.00005    0.0001
print time 0.0005       0.001       0.01
physical   1.0          0.0         1.0e-01
tran bound 0            0
temp bound 0            0
isothermal 0
intl. temp 20.0
leach      0            0
WORD       tpkin
carbonate precip. rate equation data next three lines
1 PARAMS   5          100.0       4          prep
2 CDATS    19.8         6.383       10.377     8.446 3.154e+04
3 INXi(i)  2 0          10 0         0 0         4 9
4 CONK(1) -1.32        0           0          0
5 CONK(2) -4.59        0           0          0
6 CONK(3) -6.94        0           0          0
7 CONK(4) 0.0         0           0          0
WORD       blank
no.species 6          2          0          2          1          2
cecons     0.328
na 1.0      0          2 2.764e-04 2.764e-04  2  1.0e-03  1.0e-03  1  0
na 4.22e-03 1.52e-02
na -0.1760  0          0
h 1.0       1  1.2e-10  1.2e-10    1  1.232e-10 1.232e-10  0  0
co3 -2.0     0          31.3203e-04 3.200e-05  311.800e-05 3.209e-05  0  0
ca 2.0      0          3 1.168e-04 1.168e-04  3  1.169e-04 1.169e-04  1  0
ca 0.160    0.156
ca -0.3570  0
cl -1.0     4 2.764e-04 2.764e-04  4  1.0e-03  1.0e-03  0  0
oh -13.990
oh 1.0e-04 8.307e-05 0 0
hco3 0 0.0 1.0 1.0 0.0 0.0 0.0
hco3 10.337 0 0
hco3 1.0e-04 8.589e-05 0 0
h2co3 0 0.0 2.0 1.0 0.0 0.0 0.0
h2co3 16.700 0 0
h2co3 3.0e-08 2.441e-08 0 0
caco3 11 0.0 0.0 1.0 1.0 0.0 0.0
caco3 -8.446 0 0
caco3 0.0 0.00 0 0
  
```

OUTPUT

1 Isothermal kinetic precip., aqueous complex, w. dissoc. transport-chemd15t

unit of length is meter unit of time is year

kinetics of rev. precipitate dissolution considered

inner boundary is constant concentration outer boundary is constant initial concentration

dispersion coefficient = 1.0v+ 0. fluid velocity = 0.100 number of grid points = 20

number of print outs = 10
 given at the following times = 0.1000e-05 0.3000e-05 0.5000e-05 0.8000e-05 0.1000e-04 0.5000e-04 0.1000e-03 0.5000e-03
 0.1000e-02 0.1000e-01

errsq = 0.10e-29 climit = 0.10e-02 iterj = 20 iterm = 10 iterd = 5 dtmult = 0.17e+01 ndiv =

number of sites(ion-exchange) 0.3280 number of sites(edl model) 0.0000
 this simulation is isothermal, temperature = 20.

5 bare ions 2 sorbing ions (ionex) 0 sorbing ions (edl model)

component	charge	kinetic code	initial condition type	initial condition value	boundary condition type	boundary condition value
na	1.	0	2	2.7640e-04	2	1.0000e-03
h	1.	0	1	1.2000e-10	1	1.2320e-10
co3	-2.	0	3	1.3203e-04	3	1.1800e-04
ca	2.	0	3	1.1680e-04	3	1.1690e-04
cl	-1.	0	4	2.7640e-04	4	1.0000e-03

3 complexes 0 sorbing complexes(ionex) 0 sorbing complexes (edl model)

complex	charge	kcode	stoichiometry					
oh	-1.	0	0.	0.	0.	0.	0.	1.
hco3	-1.	0	0.	1.	1.	0.	0.	0.
h2co3	0.	0	0.	2.	1.	0.	0.	0.

OUTPUT

```

1      solid precipitates
precipitate kinetic code      stoichiometry
caco3      11      0.0 0.0 1.0 1.0 0.0 0.0
  
```

Calcite dissolution information:

```

no of terms in the rate formula =      4

no of other additional data needed =      5
representative surface parameter =      0.100e+03
xdiag = prepc
  
```

additional data for rate calculation

```

0.198e+02  0.638e+01  0.104e+02  0.845e+01  0.315e+05
  
```

```

binary element nos. of the terms of the rate equation
2      0  10      0      0      0      4      9
  
```

```

coefficients in log function of thermodynamic constants
-1.320      0.000      0.000      0.000
-4.590      0.000      0.000      0.000
-6.940      0.000      0.000      0.000
0.000      0.000      0.000      0.000
  
```

** spatial grid **

```

0.      0.5086e-02  0.1233e-01  0.2266e-01  0.3738e-01  0.5835e-01  0.8823e-01  0.1308  0.1915  0.2780
0.4012  0.5768      0.8271      1.184      1.692      2.416      3.448      4.918      7.014      10.00
  
```

OUTPUT

1

initial conditions
temp= 20.00

component	total aqueous conc.	bare ion concentration	sorbed concentration		act. coef.	kd(ion ex)	kd(edl)
			(ionex)	(edl)			
na	0.2764e-03	0.2764e-03	0.4375e-02	0.	0.9718	15.83	0.
h	0.9109e-04	0.1200e-09	0.	0.	0.9718	0.	0.
co3	0.1302e-03	0.3915e-04	0.	0.	0.8918	0.	0.
ca	0.1150e-03	0.1150e-03	0.1618	0.	0.8918	1407.	0.
cl	0.2467e-03	0.2467e-03	0.	0.	0.9718	0.	0.
oh	0.9030e-04	0.9030e-04	0.	0.	0.9718	0.	0.
complex	valence	aqueous conc.	sorption(io)	sorption(edl)			
hco3	-1.000	0.9104e-04	0.	0.			
h2co3	0.	0.2380e-07	0.	0.			

precipitate equivalent moles/liter solution

caco3 0.181e-05

to have a net balance of zero charge, other species must be present (although not participating in the chemical reactions) with a total concentration times charge of 0.

1

boundary or influx conditions
temp= 20.00

component	total aqueous conc.	bare ion concentration	sorbed concentration		act. coef.	kd(ion ex)	kd(edl)
			(ionex)	(edl)			
na	0.1000e-02	0.1000e-02	0.1587e-01	0.	0.9600	15.87	0.
h	0.8198e-04	0.1232e-09	0.	0.	0.9600	0.	0.
co3	0.1180e-03	0.3604e-04	0.	0.	0.8492	0.	0.
ca	0.1169e-03	0.1169e-03	0.1561	0.	0.8492	1335.	0.
cl	0.9896e-03	0.9896e-03	0.	0.	0.9600	0.	0.
oh	0.9013e-04	0.9013e-04	0.	0.	0.9600	0.	0.
complex	valence	aqueous conc.	sorption(io)	sorption(edl)			
hco3	-1.000	0.8193e-04	0.	0.			
h2co3	0.	0.2146e-07	0.	0.			

precipitate equivalent moles/liter solution

caco3 0.

to have a net balance of zero charge, other species must be present (although not participating in the chemical reactions) with a total concentration times charge of -0.121e-16

OUTPUT

1 time= 3.60156e-06 delt= 1.3541e-06 concentration of species in moles/liter solution									
species	distance								
	0.000	0.005	0.012	0.023	0.037	0.058	0.088	0.131	0.192
na	1.0000e-03	2.7966e-04	2.7641e-04	2.7640e-04	2.7640e-04	2.7640e-04	2.7640e-04	2.7640e-04	2.7640e-04
h	1.2320e-10	1.2006e-10	1.2000e-10	1.2000e-10	1.2000e-10	1.2000e-10	1.2000e-10	1.2000e-10	1.2000e-10
co3	3.6044e-05	3.9123e-05	3.9154e-05	3.9154e-05	3.9154e-05	3.9154e-05	3.9154e-05	3.9154e-05	3.9154e-05
ca	1.1690e-04	1.1750e-04	1.1500e-04	1.1499e-04	1.1499e-04	1.1499e-04	1.1499e-04	1.1499e-04	1.1499e-04
cl	9.8965e-04	2.5518e-04	2.4676e-04	2.4673e-04	2.4673e-04	2.4673e-04	2.4673e-04	2.4673e-04	2.4673e-04
oh	9.0131e-05	9.0292e-05	9.0298e-05	9.0298e-05	9.0298e-05	9.0298e-05	9.0298e-05	9.0298e-05	9.0298e-05
sorbed(ionex)									
na	1.5873e-02	4.3797e-03	4.3747e-03	4.3747e-03	4.3747e-03	4.3747e-03	4.3747e-03	4.3747e-03	4.3747e-03
ca	1.5606e-01	1.6181e-01	1.6181e-01	1.6181e-01	1.6181e-01	1.6181e-01	1.6181e-01	1.6181e-01	1.6181e-01
complexes									
hco3	8.1935e-05	9.0934e-05	9.1041e-05	9.1042e-05	9.1042e-05	9.1042e-05	9.1042e-05	9.1041e-05	9.1041e-05
h2co3	2.1458e-08	2.3773e-08	2.3799e-08	2.3799e-08	2.3799e-08	2.3799e-08	2.3799e-08	2.3799e-08	2.3799e-08
precipitates									
caco3	0.	1.8106e-06	1.8106e-06	1.8106e-06	1.8107e-06	1.8107e-06	1.8108e-06	1.8109e-06	1.8111e-06
species	distance								
	0.278	0.401	0.577	0.827	1.184	1.692	2.416	3.448	4.918
na	2.7640e-04	2.7640e-04	2.7640e-04	2.7640e-04	2.7640e-04	2.7640e-04	2.7640e-04	2.7639e-04	2.7639e-04
h	1.2000e-10	1.2000e-10	1.2000e-10	1.2000e-10	1.2000e-10	1.2000e-10	1.2000e-10	1.2001e-10	1.2001e-10
co3	3.9154e-05	3.9153e-05	3.9153e-05	3.9153e-05	3.9153e-05	3.9152e-05	3.9151e-05	3.9150e-05	3.9148e-05
ca	1.1499e-04	1.1499e-04	1.1499e-04	1.1499e-04	1.1499e-04	1.1499e-04	1.1499e-04	1.1498e-04	1.1498e-04
cl	2.4673e-04	2.4673e-04	2.4673e-04	2.4673e-04	2.4673e-04	2.4673e-04	2.4673e-04	2.4673e-04	2.4673e-04
oh	9.0297e-05	9.0297e-05	9.0297e-05	9.0297e-05	9.0296e-05	9.0295e-05	9.0294e-05	9.0293e-05	9.0291e-05
sorbed(ionex)									
na	4.3747e-03	4.3747e-03	4.3747e-03	4.3747e-03	4.3747e-03	4.3747e-03	4.3747e-03	4.3747e-03	4.3747e-03
ca	1.6181e-01	1.6181e-01	1.6181e-01	1.6181e-01	1.6181e-01	1.6181e-01	1.6181e-01	1.6181e-01	1.6181e-01
complexes									
hco3	9.1041e-05	9.1041e-05	9.1041e-05	9.1040e-05	9.1040e-05	9.1039e-05	9.1038e-05	9.1037e-05	9.1035e-05
h2co3	2.3799e-08	2.3799e-08	2.3799e-08	2.3799e-08	2.3799e-08	2.3799e-08	2.3799e-08	2.3799e-08	2.3799e-08
precipitates									
caco3	1.8113e-06	1.8116e-06	1.8121e-06	1.8127e-06	1.8137e-06	1.8150e-06	1.8169e-06	1.8195e-06	1.8233e-06

OUTPUT

	7.014	10.000
species		
na	2.7639e-04	2.7640e-04
h	1.2001e-10	1.2000e-10
co3	3.9146e-05	3.9154e-05
ca	1.1498e-04	1.1499e-04
cl	2.4673e-04	2.4673e-04
oh	9.0288e-05	9.0298e-05

distance

sorbed(ionex)

na	4.3747e-03	4.3747e-03
ca	1.6181e-01	1.6181e-01

complexes

hco3	9.1032e-05	9.1042e-05
h2co3	2.3799e-08	2.3799e-08

precipitates

caco3	1.8287e-06	1.8105e-06
-------	------------	------------

1

2

convergence is obtained in less than 6 iterations so time step is increased by 1.75
delt= 2.3697e-06 at time= 4.9556e-06

2

1

2

calculation time= 0.52040e+01seconds

convergence is obtained in less than 6 iterations so time step is increased by 1.75
delt= 2.3697e-06 at time= 7.3253e-06

OUTPUT

1 time= 1.01327e-02 delt= 1.0000e-03 concentration of species in moles/liter solution

species	distance								
	0.000	0.005	0.012	0.023	0.037	0.058	0.088	0.131	0.192
na	1.0000e-03	7.7995e-04	5.6810e-04	4.3485e-04	3.6853e-04	3.1981e-04	2.8809e-04	2.7763e-04	2.7609e-04
h	1.2320e-10	1.2443e-10	1.2591e-10	1.2714e-10	1.2712e-10	1.2506e-10	1.2215e-10	1.2068e-10	1.2042e-10
co3	3.6044e-05	3.5670e-05	3.5168e-05	3.4721e-05	3.4854e-05	3.6062e-05	3.7789e-05	3.8707e-05	3.8874e-05
ca	1.1690e-04	1.9211e-04	2.4914e-04	2.5037e-04	2.0517e-04	1.5489e-04	1.2508e-04	1.1601e-04	1.1471e-04
cl	9.8965e-04	9.2171e-04	8.2607e-04	6.9699e-04	5.3919e-04	3.8398e-04	2.8467e-04	2.5195e-04	2.4706e-04
oh	9.0131e-05	8.9252e-05	8.8099e-05	8.6917e-05	8.6378e-05	8.7197e-05	8.8857e-05	8.9803e-05	8.9978e-05
sorbed(ionex)									
na	1.5873e-02	9.6654e-03	6.1801e-03	4.7103e-03	4.3957e-03	4.3750e-03	4.3754e-03	4.3751e-03	4.3751e-03
ca	1.5606e-01	1.5917e-01	1.6091e-01	1.6164e-01	1.6180e-01	1.6181e-01	1.6181e-01	1.6181e-01	1.6181e-01
complexes									
hco3	8.1935e-05	8.1873e-05	8.1871e-05	8.2243e-05	8.3602e-05	8.6289e-05	8.9144e-05	9.0484e-05	9.0717e-05
h2co3	2.1458e-08	2.1653e-08	2.1936e-08	2.2335e-08	2.2846e-08	2.3359e-08	2.3681e-08	2.3784e-08	2.3799e-08
precipitates									
caco3	0.	8.0088e-06	1.3337e-05	1.4760e-05	1.1934e-05	7.1041e-06	3.5926e-06	2.4909e-06	2.3920e-06
species	distance								
	0.278	0.401	0.577	0.827	1.184	1.692	2.416	3.448	4.918
na	2.7597e-04	2.7595e-04	2.7594e-04	2.7594e-04	2.7594e-04	2.7594e-04	2.7594e-04	2.7594e-04	2.7594e-04
h	1.2043e-10	1.2044e-10	1.2045e-10	1.2045e-10	1.2045e-10	1.2045e-10	1.2045e-10	1.2045e-10	1.2045e-10
co3	3.8869e-05	3.8859e-05	3.8855e-05	3.8853e-05	3.8853e-05	3.8853e-05	3.8853e-05	3.8853e-05	3.8853e-05
ca	1.1460e-04	1.1458e-04	1.1458e-04	1.1457e-04	1.1457e-04	1.1457e-04	1.1457e-04	1.1457e-04	1.1457e-04
cl	2.4674e-04	2.4673e-04	2.4673e-04	2.4673e-04	2.4673e-04	2.4673e-04	2.4673e-04	2.4673e-04	2.4673e-04
oh	8.9971e-05	8.9959e-05	8.9954e-05	8.9953e-05	8.9953e-05	8.9953e-05	8.9953e-05	8.9953e-05	8.9953e-05
sorbed(ionex)									
na	4.3751e-03	4.3751e-03	4.3751e-03	4.3751e-03	4.3751e-03	4.3751e-03	4.3751e-03	4.3751e-03	4.3751e-03
ca	1.6181e-01	1.6181e-01	1.6181e-01	1.6181e-01	1.6181e-01	1.6181e-01	1.6181e-01	1.6181e-01	1.6181e-01
complexes									
hco3	9.0715e-05	9.0703e-05	9.0698e-05	9.0697e-05	9.0696e-05	9.0696e-05	9.0696e-05	9.0696e-05	9.0696e-05
h2co3	2.3800e-08	2.3800e-08	2.3800e-08	2.3800e-08	2.3800e-08	2.3800e-08	2.3800e-08	2.3800e-08	2.3800e-08
precipitates									
caco3	2.4245e-06	2.4460e-06	2.4543e-06	2.4565e-06	2.4568e-06	2.4568e-06	2.4568e-06	2.4568e-06	2.4568e-06

OUTPUT

		distance
species	7.014	10.000
na	2.7594e-04	2.7640e-04
h	1.2045e-10	1.2000e-10
co3	3.8853e-05	3.9154e-05
ca	1.1457e-04	1.1499e-04
cl	2.4673e-04	2.4673e-04
oh	8.9953e-05	9.0298e-05
sorbed(ionex)		
na	4.3751e-03	4.3747e-03
ca	1.6181e-01	1.6181e-01
complexes		
hco3	9.0696e-05	9.1042e-05
h2co3	2.3800e-08	2.3799e-08
precipitates		
caco3	2.4568e-06	1.8105e-06

APPENDIX 6

ISOTHERMAL SILICA WATER REACTION IN BATCH SIMULATION

INPUTS AND SAMPLE OUTPUT

1 - Kinetic Dissolution

2 - Kinetic Precipitation

INPUT

```

isothermal kinetic dissolution of SiO2--SiN
UNITS      meter      second
type       0          1          0
iteration   100        100        100
Calc.crtia 1.0e-30     1.0e-03     20          10          5          1.75          5
grid       20          6.56        0.0
Time       10          360.0       7.2e+05
print time 360.0       3600.0      18000.0     36000.0    108000.0    144000.0    216000.0
print time 360000.0 504000.0    648000.0
physical   0.0          0.0         0.0
tran bound 0           0
Temp bound 0
isothermal 0
Intl. temp 105.0
leach      0           0
WORD      tpkin
reversible rate constants next four lines
1 PARAM    0          265.0       2          preps
2 INXI(i)  0          0          -1         0
3 CONK(1)  -11.309
4 CONK(2)  -8.0888
WORD      blank
no.species 1          0          0          0          1          0          0
H4SiO4     0          1          3          0.1e+01    1.0e-20    3          0.1e+01    1.0e-20    0
SiO2       2          1.0
SiO2       -20.0000
SiO2       0.1e+01    0.1e+01

```

OUTPUT

isothermal kinetic dissolution of SiO₂--SiN

unit of length is meter unit of time is secon

kinetics of rev. precipitate dissolution considered

inner boundary is constant concentration outer boundary is constant initial concentration

dispersion coefficient= 0.0v+ 0. fluid velocity = 0. number of grid points = 20

number of print outs = 10
 given at the following times= 360.0 3600. 0.1800e+05 0.3600e+05 0.1080e+06 0.1440e+06 0.2160e+06 0.3600e+06
 0.5040e+06 0.6480e+06

errsq= 0.10e-29 climit= 0.10e-02 iterj= 20 iterm= 10 iterd= 5 dtmult= 0.17e+01 ndiv=

number of sites(ion-exchange) 0.0000 number of sites(edl model) 0.0000
 this simulation is isothermal, temperature = 105.

component	charge	kinetic code	initial condition type	initial condition value	boundary condition type	boundary condition value
H4SiO4	0.	1	3	1.0000e+00	3	1.0000e+00

precipitate	kinetic code	stoichiometry
1 solid precipitates		
SiO2	2	1.0

OUTPUT

Silicate-water reaction information:

no of terms in the rate formula = 2
no of other additional data needed = 0
representative surface parameter = 0.265e+03
xdiag = preps

binary element nos. of the terms of the rate equation
0 0 -1 0

coefficients in log function of thermodynamic constants
-11.309 0.000 0.000 0.000
-8.089 0.000 0.000 0.000

** spatial grid **

0.	0.3453	0.6905	1.036	1.381	1.726	2.072	2.417	2.762	3.107
3.453	3.798	4.143	4.488	4.834	5.179	5.524	5.869	6.215	6.560

OUTPUT

1

initial conditions
temp= 105.00

component	total aqueous conc.	bare ion concentration	sorbed concentration		act. coef.	kd(ion ex)	kd(edl)
			(ionex)	(edl)			
H4SiO4	0.1000e-19	0.1000e-19	0.	0.	1.000	0.	0.

precipitate equivalent moles/liter solution

Sio2 1.00

to have a net balance of zero charge, other 'species must be present (although not participating in the chemical reactions) with a total concentration times charge of 0.

1

boundary or influx conditions
temp= 105.00

component	total aqueous conc.	bare ion concentration	sorbed concentration		act. coef.	kd(ion ex)	kd(edl)
			(ionex)	(edl)			
H4SiO4	0.1000e-19	0.1000e-19	0.	0.	1.000	0.	0.

precipitate equivalent moles/liter solution

Sio2 1.00

to have a net balance of zero charge, other 'species must be present (although not participating in the chemical reactions) with a total concentration times charge of 0.

1

2

calculation time= 0.92900e-02seconds

convergence is obtained in less than 6 iterations so time step is increased by 1.75
delt= 3.6000e+02 at time= 3.6000e+02

OUTPUT

```

1   time= 4.38187e+03      delt= 1.9294e+03      concentration of species in moles/liter solution

                                distance
species      0.000      0.345      0.691      1.036      1.381      1.726      2.072      2.417      2.762
H4SiO4      1.0000e-20  5.6657e-06  5.6657e-06  5.6657e-06  5.6657e-06  5.6657e-06  5.6657e-06  5.6657e-06  5.6657e-06
precipitates
SiO2        1.0000e+00  9.9999e-01  9.9999e-01  9.9999e-01  9.9999e-01  9.9999e-01  9.9999e-01  9.9999e-01  9.9999e-01

                                distance
species      3.107      3.453      3.798      4.143      4.488      4.834      5.179      5.524      5.869
H4SiO4      5.6657e-06  5.6657e-06  5.6657e-06  5.6657e-06  5.6657e-06  5.6657e-06  5.6657e-06  5.6657e-06  5.6657e-06
precipitates
SiO2        9.9999e-01  9.9999e-01  9.9999e-01  9.9999e-01  9.9999e-01  9.9999e-01  9.9999e-01  9.9999e-01  9.9999e-01

                                distance
species      6.215      6.560
H4SiO4      5.6657e-06  1.0000e-20
precipitates
SiO2        9.9999e-01  1.0000e+00

1
2

convergence is obtained in less than 6 iterations so time step is increased by 1.75
delt= 3.3764e+03      at time= 6.3113e+03
2

1
2

convergence is obtained in less than 6 iterations so time step is increased by 1.75
delt= 5.9087e+03      at time= 9.6877e+03
2

```

OUTPUT

```

1   time= 7.78704e+05      delt= 1.6972e+05      concentration of species in moles/liter solution

      species      0.000      0.345      0.691      distance
                        1.036      1.381      1.726      2.072      2.417      2.762
H4SiO4  1.0000e-20  4.7309e-04  4.7309e-04  4.7309e-04  4.7309e-04  4.7309e-04  4.7309e-04  4.7309e-04  4.7309e-04  4.7309e-04
precipitates
SiO2    1.0000e+00  9.9953e-01  9.9953e-01  9.9953e-01  9.9953e-01  9.9953e-01  9.9953e-01  9.9953e-01  9.9953e-01  9.9953e-01

      species      3.107      3.453      3.798      distance
                        4.143      4.488      4.834      5.179      5.524      5.869
H4SiO4  4.7309e-04  4.7309e-04  4.7309e-04  4.7309e-04  4.7309e-04  4.7309e-04  4.7309e-04  4.7309e-04  4.7309e-04  4.7309e-04
precipitates
SiO2    9.9953e-01  9.9953e-01  9.9953e-01  9.9953e-01  9.9953e-01  9.9953e-01  9.9953e-01  9.9953e-01  9.9953e-01  9.9953e-01

      species      6.215      6.560      distance
H4SiO4  4.7309e-04  1.0000e-20
precipitates
SiO2    9.9953e-01  1.0000e+00
  
```

INPUT

```

isothermal kinetic precipitation of SiO2--S3N
UNITS      meter      second
type       0          1          0
iteration   100        100        100
Calc.crtia 1.0e-30      1.0e-03      20          10          5          1.75          5
grid       20          6.56         0.0
Time       10          360.0        7.2e+05
print time 360.0         3600.0       18000.0     36000.0     108000.0     144000.0     216000.0
print time 360000.0 504000.0     648000.0
physical   0.0           0.0           0.0
tran bound 0             0
Temp bound 0
isothermal 0
Intl. temp 105.0
leach      0             0
WORD       tpkin
reversible rate constants next four lines
1 PARAM    0          261.0         2          preps
2 INXI(i)  0          0          -1          0
3 CONK(1)  -11.309
4 CONK(2)  -8.0888
WORD       blank
no.species 1          0          0          0          1          0          0
H4sio4     0          1          3          1.0e-03     1.0e-03     3          1.0e-03     1.0e-03     0
Sio2       2          1.0
Sio2       -3.0000
Sio2       1.0e-20     1.0e-20

```


OUTPUT

isothermal kinetic precipitation of SiO2--S3N

unit of length is meter unit of time is secon

kinetics of rev. precipitate dissolution considered

inner boundary is constant concentration outer boundary is constant initial concentration

dispersion coefficient= 0.0v+ 0. fluid velocity = 0. number of grid points = 20

number of print outs = 10
 given at the following times= 360.0 3600. 0.1800e+05 0.3600e+05 0.1080e+06 0.1440e+06 0.2160e+06 0.3600e+06
 0.5040e+06 0.6480e+06

errsqr= 0.10e-29 climit= 0.10e-02 iterj= 20 iterm= 10 iterd= 5 dtmult= 0.17e+01 ndiv=

number of sites(ion-exchange) 0.0000 number of sites(edl model) 0.0000
 this simulation is isothermal, temperature = 105.

1	bare ions	0	sorbing ions (ionex)	0	sorbing ions (edl model)
component charge	kinetic code	initial condition type	initial condition value	boundary condition type	boundary condition value
H4sio4	0.	1	3 1.0000e-03	3	1.0000e-03

1	solid precipitates	
precipitate	kinetic code	stoichiometry
SiO2	2	1.0

OUTPUT

Silicate-water reaction information:

no of terms in the rate formula = 2
no of other additional data needed = 0
representative surface parameter = 0.261e+03
xdiag = preps

binary element nos. of the terms of the rate equation
0 0 -1 0

coefficients in log function of thermodynamic constants
-11.309 0.000 0.000 0.000
-8.089 0.000 0.000 0.000

** spatial grid **

0.	0.3453	0.6905	1.036	1.381	1.726	2.072	2.417	2.762	3.107
3.453	3.798	4.143	4.488	4.834	5.179	5.524	5.869	6.215	6.560

OUTPUT

1

initial conditions
temp= 105.00

component	total aqueous conc.	bare ion concentration	sorbed concentration		act. coef.	kd(ion ex)	kd(edl)
			(ionex)	(edl)			
H4sio4	0.1000e-02	0.1000e-02	0.	0.	1.000	0.	0.

precipitate equivalent moles/liter solution

Sio2 0.100e-19

to have a net balance of zero charge, other species must be present (although not participating in the chemical reactions) with a total concentration times charge of 0.

1

boundary or influx conditions
temp= 105.00

component	total aqueous conc.	bare ion concentration	sorbed concentration		act. coef.	kd(ion ex)	kd(edl)
			(ionex)	(edl)			
H4sio4	0.1000e-02	0.1000e-02	0.	0.	1.000	0.	0.

precipitate equivalent moles/liter solution

Sio2 0.100e-19

to have a net balance of zero charge, other species must be present (although not participating in the chemical reactions) with a total concentration times charge of 0.

1

2
calculation time= 0.91630e-02seconds

convergence is obtained in less than 6 iterations so time step is increased by 1.75
delt= 3.6000e+02 at time= 3.6000e+02

OUTPUT

```

1   time= 7.78704e+05      delt= 1.6972e+05      concentration of species in moles/liter solution

      species      0.000      0.345      0.691      distance
                        1.036      1.381      1.726      2.072      2.417      2.762
H4sio4      1.0000e-03  6.8944e-04  6.8944e-04  6.8944e-04  6.8944e-04  6.8944e-04  6.8944e-04  6.8944e-04  6.8944e-04  6.8944e-04
precipitates
Sio2      1.0000e-20  3.1056e-04  3.1056e-04  3.1056e-04  3.1056e-04  3.1056e-04  3.1056e-04  3.1056e-04  3.1056e-04  3.1056e-04

      species      3.107      3.453      3.798      distance
                        4.143      4.488      4.834      5.179      5.524      5.869
H4sio4      6.8944e-04  6.8944e-04  6.8944e-04  6.8944e-04  6.8944e-04  6.8944e-04  6.8944e-04  6.8944e-04  6.8944e-04  6.8944e-04
precipitates
Sio2      3.1056e-04  3.1056e-04  3.1056e-04  3.1056e-04  3.1056e-04  3.1056e-04  3.1056e-04  3.1056e-04  3.1056e-04  3.1056e-04

      species      6.215      6.560      distance
H4sio4      6.8944e-04  1.0000e-03
precipitates
Sio2      3.1056e-04  1.0000e-20

```

OUTPUT

1	time= 4.38187e+03	delt= 1.9294e+03	concentration of species in moles/liter solution							
			distance							
species	0.000	0.345	0.691	1.036	1.381	1.726	2.072	2.417	2.762	
H4sio4	1.0000e-03	9.9631e-04	9.9631e-04	9.9631e-04	9.9631e-04	9.9631e-04	9.9631e-04	9.9631e-04	9.9631e-04	
precipitates										
Sio2	1.0000e-20	3.6852e-06	3.6852e-06	3.6852e-06	3.6852e-06	3.6852e-06	3.6852e-06	3.6852e-06	3.6852e-06	
			distance							
species	3.107	3.453	3.798	4.143	4.488	4.834	5.179	5.524	5.869	
H4sio4	9.9631e-04	9.9631e-04	9.9631e-04	9.9631e-04	9.9631e-04	9.9631e-04	9.9631e-04	9.9631e-04	9.9631e-04	
precipitates										
Sio2	3.6852e-06	3.6852e-06	3.6852e-06	3.6852e-06	3.6852e-06	3.6852e-06	3.6852e-06	3.6852e-06	3.6852e-06	
			distance							
species	6.215	6.560								
H4sio4	9.9631e-04	1.0000e-03								
precipitates										
Sio2	3.6852e-06	1.0000e-20								

APPENDIX 7

KINETIC DISSOLUTION OF GLASS IN BATCH SIMULATION

INPUT AND SAMPLE OUTPUT

INPUT

```

Kinetic imperial glass dissolution-batch case      setglss2
UNITS      meter      second
type              0              1              0
iteration         100           100           100
Calc.crtia      1.0e-30      1.0e-03      20           10           5           1.75           5
grid            5              6.56         0.0
time            7              1.50e+00     1.00e+06
print time      1.58e+04     4.93e+05     7.48e+06     5.36e+07     1.66e+08     2.82e+08     3.52e+08
Physical        1.0e-30      1.0e-30      1.0e-30
boundary        1              0
temp bound      0
Isothermal      0
Intl. temp      20.0
leach           0              0
WORD            exkin
glass rate equation data next line
1 PARAMS        0              3.0e+06      0              0              dissg
WORD            blank
no.species      6              0              0              1              0              0
na 1.0          1              1              1.0e-10      1.0e-10      1              1.0e-10      1.0e-10
h 1.0           2              1              3.16e-05     3.16e-05     1              3.16e-05     3.16e-05     0              0
k 1.0           3              1              1.0e-10      1.0e-10      1              1.0e-10      1.0e-10
ca +2.0         4              1              1.0e-10      1.0e-10      1              1.0e-10      1.0e-10
mg +2.0         5              1              1.0e-10      1.0e-10      1              1.0e-10      1.0e-10
hco3 -1.0        0              2              2.16e-03     2.16e-03     2              2.16e-03     2.16e-03     0              0
h2co3          0 0.0 1.0 0.0 0.0 0.0 1.0
h2co3          +6.3655 0.0 0.0 0.0 0.0
h2co3          2.13e-03 2.13e-03
  
```

OUTPUT

1Kinetic imperical glass dissolution-batch case setglss2

unit of length is meter unit of time is second

kinetics of non-rev. silica dissolution considered

inner boundary is constant flux outer' boundry is constant initial concentration

dispersion coefficient= 0.0v+ 0.10e-29 fluid velocity = 0.100e-29 number of grid points = 5

number of print outs = 7
 given at the following times= 0.1580e+05 0.4930e+06 0.7480e+07 0.5360e+08 0.1660e+09 0.2820e+09 0.3520e+09

errsq= 0.10e-29 climit= 0.10e-02 iterj= 20 iterm= 10 iterd= 5 dtmult= 0.17e+01 ndiv=

number of sites(ion-exchange) 0.0000 number of sites(edl model) 0.0000
 this simulation is isothermal, temperature = 20.

6 bare ions 0 sorbing ions (ionex) 0 sorbing ions (edl model)

component	charge	kinetic code	initial condition type	initial condition value	boundary condition type	boundary condition value
na	1.	1	1	1.0000e-10	1	1.0000e-10
h	1.	2	1	3.1600e-05	1	3.1600e-05
k	1.	3	1	1.0000e-10	1	1.0000e-10
ca	2.	4	1	1.0000e-10	1	1.0000e-10
mg	2.	5	1	1.0000e-10	1	1.0000e-10
hco3	-1.	0	2	2.1600e-03	2	2.1600e-03

1 complexes 0 sorbing complexes(ionex) 0 sorbing complexes (edl model)

complex	charge	kcode	stoichiometry					
h2co3	0.	0	0.	1.	0.	0.	0.	1.

OUTPUT

Glass dissolution information:

no of terms in the rate formula = 0
no of other additional data needed = 0
representative surface parameter = 0.300e+07
xdiag = dissg

** spatial grid **

0. 1.640 3.280 4.920 6.560

OUTPUT

1

initial conditions
temp= 20.00

component	total aqueous conc.	bare ion concentration	sorbed concentration		act. coef.	kd(ion ex)	kd(edl)
			(ionex)	(edl)			
na	0.1000e-09	0.1000e-09	0.	0.	0.9936	0.	0.
h	0.2162e-02	0.3160e-04	0.	0.	0.9936	0.	0.
k	0.1000e-09	0.1000e-09	0.	0.	0.9936	0.	0.
ca	0.1000e-09	0.1000e-09	0.	0.	0.9746	0.	0.
mg	0.1000e-09	0.1000e-09	0.	0.	0.9746	0.	0.
hco3	0.2160e-02	0.2944e-04	0.	0.	0.9936	0.	0.
complex	valence	aqueous conc.	sorption(io)	sorption(edl)			
h2co3	0.	0.2131e-02	0.	0.			

to have a net balance of zero charge, other 'species must be present (although not participating in the chemical reactions) with a total concentration times charge of -0.216e-05

129

1

boundary or influx conditions
temp= 20.00

component	total aqueous conc.	bare ion concentration	sorbed concentration		act. coef.	kd(ion ex)	kd(edl)
			(ionex)	(edl)			
na	0.1000e-09	0.1000e-09	0.	0.	0.9936	0.	0.
h	0.2162e-02	0.3160e-04	0.	0.	0.9936	0.	0.
k	0.1000e-09	0.1000e-09	0.	0.	0.9936	0.	0.
ca	0.1000e-09	0.1000e-09	0.	0.	0.9746	0.	0.
mg	0.1000e-09	0.1000e-09	0.	0.	0.9746	0.	0.
hco3	0.2160e-02	0.2944e-04	0.	0.	0.9936	0.	0.
complex	valence	aqueous conc.	sorption(io)	sorption(edl)			
h2co3	0.	0.2131e-02	0.	0.			

to have a net balance of zero charge, other 'species must be present (although not participating in the chemical reactions) with a total concentration times charge of -0.216e-05

OUTPUT

1 time= 2.70798e+04 delt= 1.1606e+04 concentration of species in moles/liter solution

species	distance									
	0.000	1.640	3.280	4.920	6.560	0.000	0.000	0.000	0.000	0.000
na	1.1081e-05	1.1081e-05	1.1081e-05	1.1081e-05	1.0000e-10	0.	0.	0.	0.	0.
h	1.3839e-05	1.3839e-05	1.3839e-05	1.3839e-05	3.1600e-05	0.	0.	0.	0.	0.
k	1.2447e-06	1.2447e-06	1.2447e-06	1.2447e-06	1.0000e-10	0.	0.	0.	0.	0.
ca	2.7805e-05	2.7805e-05	2.7805e-05	2.7805e-05	1.0000e-10	0.	0.	0.	0.	0.
mg	1.5245e-05	1.5245e-05	1.5245e-05	1.5245e-05	1.0000e-10	0.	0.	0.	0.	0.
hco3	6.7051e-05	6.7051e-05	6.7051e-05	6.7051e-05	2.9437e-05	0.	0.	0.	0.	0.
complexes										
h2co3	2.0929e-03	2.0929e-03	2.0929e-03	2.0929e-03	2.1306e-03	0.	0.	0.	0.	0.

species	distance				
	0.000	0.000	0.000	0.000	0.000
na	0.	0.	0.	0.	0.
h	0.	0.	0.	0.	0.
k	0.	0.	0.	0.	0.
ca	0.	0.	0.	0.	0.
mg	0.	0.	0.	0.	0.
hco3	0.	0.	0.	0.	0.
complexes					
h2co3	0.	0.	0.	0.	0.

OUTPUT

1 time= 3.52706e+08 delt= 1.0000e+06 concentration of species in moles/liter solution

species	distance								
	0.000	1.640	3.280	4.920	6.560	0.000	0.000	0.000	0.000
na	6.8549e-04	6.8549e-04	6.8549e-04	6.8549e-04	1.0000e-10	0.	0.	0.	0.
h	1.7803e-07	1.7803e-07	1.7803e-07	1.7803e-07	3.1600e-05	0.	0.	0.	0.
k	1.5982e-04	1.5982e-04	1.5982e-04	1.5982e-04	1.0000e-10	0.	0.	0.	0.
ca	3.9455e-04	3.9455e-04	3.9455e-04	3.9455e-04	1.0000e-10	0.	0.	0.	0.
mg	3.4236e-04	3.4236e-04	3.4236e-04	3.4236e-04	1.0000e-10	0.	0.	0.	0.
hco3	1.5802e-03	1.5802e-03	1.5802e-03	1.5802e-03	2.9437e-05	0.	0.	0.	0.
complexes									
h2co3	5.7977e-04	5.7977e-04	5.7977e-04	5.7977e-04	2.1306e-03	0.	0.	0.	0.

species	distance				
	0.000	0.000	0.000	0.000	0.000
na	0.	0.	0.	0.	0.
h	0.	0.	0.	0.	0.
k	0.	0.	0.	0.	0.
ca	0.	0.	0.	0.	0.
mg	0.	0.	0.	0.	0.
hco3	0.	0.	0.	0.	0.
complexes					
h2co3	0.	0.	0.	0.	0.

APPENDIX 8

EQUILIBRIUM TRANSPORT CONSIDERING REDOX

INPUT AND SAMPLE OUTPUT

INPUT

Equilibrium redox pH=4/EH=.3/Pco2=e-02/150C, Into water/pH=10/EH=-.3/50C

UNITS	meter	second						
type	0	1	0					
iteration	100	100	100					
Calc.crtia	1.0e-30	1.0e-03	20	10	5	1.75	5	
grid	41	10.0	57.665					
time	11	1.0	5.0					
print time	1.0e+03	1.2e+03	1.4e+03	1.6e+03	1.8e+03	2.0e+03	2.2e+03	
print time	2.4e+03	2.6e+03	2.8e+03					
physical	0.05	1.0e-09	1.0e-03					
tran bound	1	0						
temp bound	1	0						
nonisothml	1							
Intl&Bound	50.0	150.0	8.4e+05	8.8+05	1.0			
leach	0	0						
WORD	redox							
R-F consts	8.3143	96487.0						
WORD	blank							
no.species	5	0	0	7	2	3	4	
UO2++	2.0	0	3 00.00000	00.00000	3 2.0e-06	5.0e-07		
CO3--	-2.0	0	3 00.00000	00.00000	1 5.75e-14	5.75e-14		
H+	1.0	0	1 1.0e-10	1.0e-10	1 1.0e-04	1.0e-04		
E-	-1.0	0	1 4.78e+04	4.78e+04	1 2.67e-04	2.67e-04		
OH-	-80.3723	-1.395e+03	32.5514	-3.181e-02				
OH-	1.4956e-06	5.4758e-04						
HCO3	0 0.0	1.0 1.0	0.0 0.0					
HCO3-	-77.105	4593.31	29.0425	9.438e-04				
HCO3-	00.00000	1.1e-07						
H2CO3	0 0.0	1.0 2.0	0.0 0.0					
H2CO3	-40.366	5576.57	11.3313	4.655e-02				
H2CO3	00.00000	1.0e-04						
UO2OH+	0 1.0	0.0 0.0	0.0 1.0					
UO2OH+	83.003	-1107.24	-32.4563	0.0666e-02				
UO2OH+	00.00000	1.5e-06						
UO2CO3	0 1.0	1.0 0.0	0.0 0.0					
UO2CO3	-275.356	13160.7	97.666	-1.221e-03				
UO2CO3	00.00000	1.6e-08						
UO2CO3)2	0 1.0	2.0 0.0	0.0 0.0					
	-59.815	2717.83	27.543	-1.091e-03				
	00.00000	5.0e-15						
UO2+	0 1.0	0.0 0.0	1.0 0.0					
	-356.197	13420.1	133.24	-5.501e-02				
	00.00000	1.0e-10						
U(OH)5-	0 1.0	0.0 0.0	2.0 1.0					
	-406.5	18088.5	152.77	-7.661e-02				
	00.00000	00.00000						
UO2OH)2C	0 1.0	0.0 0.0	0.0 2.0					
	-150.747	-72.008	58.326	-5.563e-02				
	00.00000	00.00000						
UO2(C)	0 1.0	0.0 0.0	2.0 0.0					
	644.664	-26101.3	-243.741	0.0999e-01				
	00.00000	00.00000						

OUTPUT

1Equilibrium redox pH=4/EH=.3/Pco2=e-02/150C,Into water/pH=10/EH=-.3/50C

unit of length is meter unit of time is second

redox is considered

inner boundary is constant flux outer' boundry is constant initial concentration

dispersion coefficient= 0.1v+ 0.10e-08 fluid velocity = 0.100e-02 number of grid points = 41

number of print outs = 11
 given at the following times= 1000. 1200. 1400. 1600. 1800. 2000. 2200. 2400.
 2600. 2800. 0.

errsq= 0.10e-29 climit= 0.10e-02 iterj= 20 item= 10 iterd= 5 dtmult= 0.17e+01 ndiv=

number of sites(ion-exchange) 0.0000 number of sites(edl model) 0.0000
 simulation of mixing with heat transport, with initial temperature = 50.
 heat capacities of fluid and solid are 0.84e+06 and 0.88e+06
 thermal conductivity of solid 1.0
 inner boundary condition is constant flux of fluid with temperature = 150.
 temperature is held at initial value at outer boundary

4 bare ions 0 sorbing ions (ionex) 0 sorbing ions (edl model)

component	charge	kinetic code	initial condition		boundary condition	
			type	value	type	value
UO2++	2.	0	3	0.	3	2.0000e-06
CO3--	-2.	0	3	0.	1	5.7500e-14
H+	1.	0	1	1.0000e-10	1	1.0000e-04
E-	-1.	0	1	4.7800e+04	1	2.6700e-04

OUTPUT

8	complexes	0	sorbing complexes(ionex)					0	sorbing complexes (edl model)
complex	charge	kcode	stoichiometry						
OH-	-1.	0	0.	0.	0.	0.	0.	1.	
HCO3	-1.	0	0.	1.	1.	0.	0.		
H2CO3	0.	0	0.	1.	2.	0.	0.		
UO2OH+	1.	0	1.	0.	0.	0.	1.		
UO2CO3	0.	0	1.	1.	0.	0.	0.		
UO2CO3)2	-2.	0	1.	2.	0.	0.	0.		
UO2+	1.	0	1.	0.	0.	1.	0.		
U(OH)5-	-1.	0	1.	0.	0.	2.	1.		

2 solid precipitates

precipitate	kinetic code	stoichiometry				
UO2OH)2C	0	1.0	0.0	0.0	0.0	2.0
UO2(C)	0	1.0	0.0	0.0	2.0	0.0

redox constants
 gas constant R= 0.831e+01 Faraday constant F= 0.965e+05

** spatial grid **

0.	0.1883e-01	0.3966e-01	0.6272e-01	0.8824e-01	0.1165	0.1477	0.1823	0.2206	0.2630
0.3098	0.3617	0.4191	0.4827	0.5530	0.6308	0.7169	0.8122	0.9177	1.034
1.164	1.307	1.465	1.640	1.834	2.048	2.285	2.548	2.839	3.160
3.516	3.910	4.346	4.829	5.363	5.954	6.608	7.332	8.133	9.019
10.00									

OUTPUT

1

initial conditions
temp= 50.00

component	total aqueous conc.	bare ion concentration	sorbed concentration		act. coef.	kd(ion ex)	kd(edl)
			(ionex)	(edl)			
UO2++	0.1183e-34	0.1000e-37	0.	0.	0.9007	0.	0.
CO3--	0.1565e-43	0.1565e-43	0.	0.	0.9007	0.	0.
H+	0.1000e-09	0.1000e-09	0.	0.	0.9742	0.	0.
E-	0.4780e+05	0.4780e+05	0.	0.	1.000	0.	0.
OH-	0.5480e-03	0.5480e-03	0.	0.	0.9742	0.	0.
complex	valence	aqueous conc.	sorption				
HCO3	-1.000	0.	0.	0.			
H2CO3	0.	0.	0.	0.			
UO2OH+	1.000	0.5693e-44	0.	0.			
UO2CO3	0.	0.	0.	0.			
UO2C(O3)2	-2.000	0.	0.	0.			
UO2+	1.000	0.	0.	0.			
U(OH)5-	-1.000	0.1182e-34	0.	0.			

precipitate equivalent moles/liter solution

UO2OH)2C 0.
UO2(C) 0.

to have a net balance of zero charge, other species must be present (although not participating in the chemical reactions) with a total concentration times charge of 0.478e+05

OUTPUT

1 boundary or influx conditions								
temp= 150.00								
component	total aqueous conc.	bare ion concentration	sorbed concentration		act. coef.	kd(ion ex)	kd(edl)	
			(ionex)	(edl)				
UO2++	0.2000e-05	0.4942e-06	0.	0.	0.9549	0.	0.	0.
CO3--	0.9289e-04	0.5750e-13	0.	0.	0.9549	0.	0.	0.
H+	0.2856e-03	0.1000e-03	0.	0.	0.9885	0.	0.	0.
E-	0.2670e-03	0.2670e-03	0.	0.	1.000	0.	0.	0.
OH-	0.1495e-05	0.2381e-07	0.	0.	0.9885	0.	0.	0.
complex	valence	aqueous conc.	sorption(io)		sorption(edl)			
HCO3	-1.000	0.1047e-06	0.	0.				
H2CO3	0.	0.9277e-04	0.	0.				
UO2OH+	1.000	0.1471e-05	0.	0.				
UO2CO3	0.	0.1451e-07	0.	0.				
UO2CO3)2	-2.000	0.4581e-14	0.	0.				
UO2+	1.000	0.1994e-07	0.	0.				
U(OH)5-	-1.000	0.9613e-16	0.	0.				
precipitate	equivalent moles/liter solution							
UO2OH)2C	0.							
UO2(C)	0.							

to have a net balance of zero charge, other species must be present (although not participating in the chemical reactions) with a total concentration times charge of 0.165e-03

OUTPUT

1 time= 1.00256e+03 delt= 5.0000e+00 concentration of species in moles/liter solution

species	distance								
	0.000	0.019	0.040	0.063	0.088	0.116	0.148	0.182	0.221
UO2++	2.2515e-13	1.1054e-13	5.3930e-14	2.5946e-14	1.2230e-14	5.6152e-15	2.4973e-15	1.0697e-15	4.3836e-16
CO3--	6.0703e-14	6.1341e-14	6.2243e-14	6.3536e-14	6.5414e-14	6.8178e-14	7.2315e-14	7.8621e-14	8.8451e-14
H+	9.8367e-05	9.8310e-05	9.8228e-05	9.8109e-05	9.7932e-05	9.7667e-05	9.7263e-05	9.6638e-05	9.5657e-05
E-	1.0053e+01	1.4322e+01	2.0453e+01	2.9383e+01	4.2581e+01	6.2381e+01	9.2542e+01	1.3919e+02	2.1241e+02
OH-	2.3845e-08	2.3717e-08	2.3540e-08	2.3293e-08	2.2946e-08	2.2459e-08	2.1778e-08	2.0832e-08	1.9543e-08
E-	-8.3927e-02	-9.6735e-02	-1.0959e-01	-1.2259e-01	-1.3579e-01	-1.4923e-01	-1.6288e-01	-1.7664e-01	-1.9035e-01
tempx	1.4934e+02	1.4907e+02	1.4869e+02	1.4816e+02	1.4740e+02	1.4633e+02	1.4480e+02	1.4262e+02	1.3954e+02
complexes									
HC03	1.0803e-07	1.0879e-07	1.0985e-07	1.1135e-07	1.1352e-07	1.1668e-07	1.2131e-07	1.2819e-07	1.3853e-07
H2CO3	9.2760e-05	9.2751e-05	9.2738e-05	9.2719e-05	9.2692e-05	9.2650e-05	9.2587e-05	9.2489e-05	9.2337e-05
UO2OH+	6.6850e-13	3.2575e-13	1.5727e-13	7.4552e-14	3.4413e-14	1.5337e-14	6.5377e-15	2.6362e-15	9.9172e-16
UO2CO3	6.7295e-15	3.2861e-15	1.5912e-15	7.5752e-16	3.5183e-16	1.5822e-16	6.8355e-17	2.8121e-17	1.0907e-17
UO2(CO3)2	2.2885e-21	1.1387e-21	5.6610e-22	2.7965e-22	1.3685e-22	6.6269e-23	3.1794e-23	1.5165e-23	7.2310e-24
UO2+	3.3884e-10	2.3600e-10	1.6347e-10	1.1205e-10	7.5653e-11	5.0054e-11	3.2263e-11	2.0114e-11	1.2017e-11
U(OH)5-	6.4257e-14	6.4525e-14	6.4902e-14	6.5435e-14	6.6194e-14	6.7282e-14	6.8847e-14	7.1099e-14	7.4330e-14
precipitates									
UO2OH)2C	0.	0.	0.	0.	0.	0.	0.	0.	0.
UO2(C)	2.5305e-04	3.1980e-09	1.8956e-09	1.2167e-09	8.4168e-10	5.8621e-10	4.3575e-10	3.2533e-10	2.5851e-10

species	distance								
	0.263	0.310	0.362	0.419	0.483	0.553	0.631	0.717	0.812
UO2++	1.7048e-16	6.2240e-17	2.1020e-17	6.4442e-18	1.7600e-18	4.2654e-19	9.5181e-20	2.1968e-20	6.1494e-22
CO3--	1.0419e-13	1.3022e-13	1.7510e-13	2.5728e-13	4.2622e-13	8.9254e-13	4.2583e-12	1.5022e-09	9.7450e-07
H+	9.4095e-05	9.1579e-05	8.7484e-05	8.0786e-05	6.9837e-05	5.2119e-05	2.4388e-05	1.0844e-06	4.9208e-09
E-	3.2895e+02	5.1671e+02	8.2212e+02	1.3217e+03	2.1388e+03	3.4638e+03	5.5695e+03	8.7950e+03	1.3452e+04
OH-	1.7834e-08	1.5674e-08	1.3128e-08	1.0435e-08	8.0215e-09	6.5197e-09	8.0654e-09	1.0942e-07	1.6514e-05
E-	-2.0374e-01	-2.1646e-01	-2.2806e-01	-2.3812e-01	-2.4638e-01	-2.5300e-01	-2.5863e-01	-2.6426e-01	-2.7061e-01
tempx	1.3525e+02	1.2938e+02	1.2161e+02	1.1179e+02	1.0014e+02	8.7496e+01	7.5232e+01	6.4903e+01	5.7547e+01
complexes									
HC03	1.5425e-07	1.7844e-07	2.1617e-07	2.7625e-07	3.7703e-07	5.7779e-07	1.3175e-06	2.1523e-05	6.5063e-05
H2CO3	9.2094e-05	9.1705e-05	9.1074e-05	9.0043e-05	8.8355e-05	8.5579e-05	8.0747e-05	5.4273e-05	7.0898e-07
UO2OH+	3.4214e-16	1.0600e-16	2.8817e-17	6.7538e-18	1.3774e-18	2.6895e-19	7.5623e-20	2.4283e-19	1.0325e-18
UO2CO3	3.9436e-18	1.3143e-18	4.0084e-19	1.1271e-19	3.0748e-20	9.7171e-21	7.1749e-21	4.5497e-19	6.9359e-18
UO2(CO3)2	3.4706e-24	1.6878e-24	8.3592e-25	4.2593e-25	2.3558e-25	1.8190e-25	6.9102e-25	1.5426e-20	1.4642e-16
UO2+	6.8016e-12	3.5949e-12	1.7458e-12	7.6740e-13	3.0335e-13	1.0950e-13	3.8040e-14	1.3994e-14	6.1025e-16
U(OH)5-	7.8916e-14	8.5305e-14	9.3958e-14	1.0542e-13	1.2140e-13	1.5171e-13	2.8105e-13	5.2815e-12	1.0068e-10

OUTPUT

precipitates

U020H) 2C	0.	0.	0.	0.	0.	0.	0.	0.	0.
U02(C)	2.0104e-10	1.6543e-10	1.3386e-10	1.1372e-10	9.5677e-11	8.1888e-11	6.9937e-11	5.5445e-11	0.

species	distance									
	0.918	1.034	1.164	1.307	1.465	1.640	1.834	2.048	2.285	
U02++	6.7171e-23	2.0801e-23	8.4004e-24	3.7960e-24	1.7375e-24	7.4170e-25	2.7604e-25	8.5634e-26	2.1677e-26	
C03--	5.8344e-06	8.6313e-06	8.0121e-06	5.4209e-06	2.8232e-06	1.1618e-06	3.8399e-07	1.0308e-07	2.2643e-08	
H+	6.0656e-10	2.6830e-10	1.6922e-10	1.2963e-10	1.1208e-10	1.0442e-10	1.0139e-10	1.0037e-10	1.0008e-10	
E-	1.9609e+04	2.6816e+04	3.4033e+04	4.0043e+04	4.4121e+04	4.6351e+04	4.7329e+04	4.7674e+04	4.7772e+04	
OH-	1.0622e-04	2.1483e-04	3.2705e-04	4.2257e-04	4.8823e-04	5.2438e-04	5.4029e-04	5.4591e-04	5.4751e-04	
E-	-2.7765e-01	-2.8461e-01	-2.9054e-01	-2.9484e-01	-2.9748e-01	-2.9884e-01	-2.9942e-01	-2.9962e-01	-2.9968e-01	
tempx	5.3212e+01	5.1133e+01	5.0328e+01	5.0077e+01	5.0015e+01	5.0002e+01	5.0000e+01	5.0000e+01	5.0000e+01	

complexes

HCO3	4.8883e-05	3.2128e-05	1.8734e-05	9.6513e-06	4.3260e-06	1.6543e-06	5.3029e-07	1.4085e-07	3.0849e-08
H2CO3	6.4102e-08	1.8397e-08	6.7140e-09	2.6370e-09	1.0192e-09	3.6260e-10	1.1280e-10	2.9651e-11	6.4753e-12
U020H+	7.2691e-19	4.5324e-19	2.7652e-19	1.6030e-19	8.4360e-20	3.8574e-20	1.4775e-20	4.6293e-21	1.1751e-21
U02C03	4.1255e-18	1.7925e-18	6.5094e-19	1.9520e-19	4.6021e-20	8.0395e-21	9.8657e-22	8.2089e-23	4.5636e-24
U02C03) 2	4.9996e-16	3.1348e-16	1.0457e-16	2.1145e-17	2.5941e-18	1.8646e-19	7.5623e-21	1.6891e-22	2.0627e-24
U02+	9.9019e-17	4.2255e-17	2.1635e-17	1.1459e-17	5.7602e-18	2.5782e-18	9.7894e-19	3.0581e-19	7.7563e-20
U(OH)5-	2.2513e-10	3.2004e-10	3.3990e-10	2.7946e-10	1.7964e-10	9.0765e-11	3.6256e-11	1.1526e-11	2.9379e-12

precipitates

U020H) 2C	0.	0.	0.	0.	0.	0.	0.	0.	0.
U02(C)	0.	0.	0.	0.	0.	0.	0.	0.	0.

species	distance									
	2.548	2.839	3.160	3.516	3.910	4.346	4.829	5.363	5.954	
U02++	4.4562e-27	7.4653e-28	1.0253e-28	1.1621e-29	1.0937e-30	8.5957e-32	5.6720e-33	3.1577e-34	1.4898e-35	
C03--	4.0924e-09	6.1126e-10	7.5788e-11	7.8350e-12	6.7841e-13	4.9415e-14	3.0407e-15	1.5870e-16	7.0519e-18	
H+	1.0001e-10	1.0000e-10	1.0000e-10	1.0000e-10	1.0000e-10	1.0000e-10	1.0000e-10	1.0000e-10	1.0000e-10	
E-	4.7795e+04	4.7799e+04	4.7800e+04	4.7800e+04	4.7800e+04	4.7800e+04	4.7800e+04	4.7800e+04	4.7800e+04	
OH-	5.4787e-04	5.4794e-04	5.4795e-04	5.4795e-04	5.4796e-04	5.4796e-04	5.4796e-04	5.4796e-04	5.4796e-04	
E-	-2.9969e-01	-2.9970e-01	-2.9970e-01	-2.9970e-01	-2.9970e-01	-2.9970e-01	-2.9970e-01	-2.9970e-01	-2.9970e-01	
tempx	5.0000e+01	5.0000e+01	5.0000e+01	5.0000e+01	5.0000e+01	5.0000e+01	5.0000e+01	5.0000e+01	5.0000e+01	

complexes

HCO3	5.5717e-09	8.3211e-10	1.0317e-10	1.0666e-11	9.2350e-13	6.7267e-14	4.1392e-15	2.1604e-16	9.5995e-18
H2CO3	1.1687e-12	1.7452e-13	2.1638e-14	2.2369e-15	1.9368e-16	1.4108e-17	8.6812e-19	4.5309e-20	2.0133e-21
U020H+	2.4173e-22	4.0501e-23	5.5628e-24	6.3049e-25	5.9336e-26	4.6635e-27	3.0772e-28	1.7131e-29	8.0826e-31
U02C03	1.6955e-25	4.2426e-27	7.2248e-29	8.4654e-31	6.8981e-33	3.9490e-35	1.6035e-37	4.6591e-40	9.7675e-43
U02C03) 2	1.3851e-26	5.1768e-29	1.0930e-31	1.3240e-34	9.3417e-38	3.8954e-41	9.7329e-45	1.4760e-48	1.3750e-52
U02+	1.5953e-20	2.6727e-21	3.6709e-22	4.1606e-23	3.9156e-24	3.0774e-25	2.0307e-26	1.1305e-27	5.3337e-29
U(OH)5-	6.0493e-13	1.0137e-13	1.3924e-14	1.5781e-15	1.4852e-16	1.1673e-17	7.7023e-19	4.2880e-20	2.0231e-21

OUTPUT

precipitates

U02OH)2C	0.	0.	0.	0.	0.	0.	0.	0.	0.
U02(C)	0.	0.	0.	0.	0.	0.	0.	0.	0.

	distance				
species	6.608	7.332	8.133	9.019	10.000
U02++	5.9811e-37	2.0511e-38	6.0284e-40	1.5261e-41	1.0000e-1363
C03--	2.6772e-19	8.7119e-21	2.4375e-22	5.8824e-24	1.5653e-1369
H+	1.0000e-10	1.0000e-10	1.0000e-10	1.0000e-10	1.0000e-10
E-	4.7800e+04	4.7800e+04	4.7800e+04	4.7800e+04	4.7800e+04
OH-	5.4796e-04	5.4796e-04	5.4796e-04	5.4796e-04	5.4796e-04
E-	-2.9970e-01	-2.9970e-01	-2.9970e-01	-2.9970e-01	-2.9970e-01

tempx 5.0000e+01 5.0000e+01 5.0000e+01 5.0000e+01 5.0000e+01

complexes

HC03	3.6443e-19	1.1859e-20	3.3181e-22	8.0075e-24	0.
H2C03	7.6433e-23	2.4872e-24	6.9590e-26	1.6794e-27	0.
U02OH+	3.2450e-32	1.1128e-33	3.2706e-35	8.2794e-37	5.6928e-1370
U02C03	1.4887e-45	1.6613e-48	1.3662e-51	8.3460e-55	0.
U02C03)2	7.9559e-57	2.8891e-61	6.6473e-66	9.7458e-71	0.
U02+	2.1414e-30	7.3432e-32	2.1583e-33	5.4636e-35	0.
U(OH)5-	8.1222e-23	2.7853e-24	8.1864e-26	2.0723e-27	1.1821e-1360

precipitates

U02OH)2C	0.	0.	0.	0.	0.
U02(C)	0.	0.	0.	0.	0.

1 time= 2.40381e+03 delt= 5.0000e+00 concentration of species in moles/liter solution

	distance								
species	0.000	0.019	0.040	0.063	0.088	0.116	0.148	0.182	0.221
U02++	1.7018e-06	2.1257e-06	1.0999e-06	5.4821e-07	2.6316e-07	1.2140e-07	5.3658e-08	2.2656e-08	9.1079e-09
C03--	3.5306e-14	2.8454e-14	3.1207e-14	3.3390e-14	3.5860e-14	3.9227e-14	4.3520e-14	4.8235e-14	5.2604e-14
H+	1.2833e-04	1.4330e-04	1.3663e-04	1.3196e-04	1.2725e-04	1.2158e-04	1.1536e-04	1.0954e-04	1.0492e-04
E-	2.3951e-03	3.3042e-03	4.5884e-03	6.4941e-03	9.3666e-03	1.3781e-02	2.0710e-02	3.1843e-02	5.0177e-02
OH-	1.8613e-08	1.6694e-08	1.7488e-08	1.8090e-08	1.8744e-08	1.9599e-08	2.0630e-08	2.1693e-08	2.2606e-08
E-	2.1978e-01	2.0806e-01	1.9610e-01	1.8344e-01	1.7010e-01	1.5603e-01	1.4119e-01	1.2551e-01	1.0894e-01
tempx	1.4999e+02	1.4999e+02	1.4998e+02	1.4997e+02	1.4996e+02	1.4995e+02	1.4992e+02	1.4988e+02	1.4982e+02

OUTPUT

complexes

HC03	8.1883e-08	7.3456e-08	7.6976e-08	7.9658e-08	8.2584e-08	8.6411e-08	9.1061e-08	9.5920e-08	1.0023e-07
H2C03	9.2776e-05	9.2784e-05	9.2794e-05	9.2799e-05	9.2801e-05	9.2799e-05	9.2796e-05	9.2791e-05	9.2787e-05
U020H+	3.9331e-06	4.3920e-06	2.3857e-06	1.2318e-06	6.1340e-07	2.9619e-07	1.3797e-07	6.1317e-08	2.5701e-08
U02C03	3.0237e-08	3.0240e-08	1.7231e-08	9.2120e-09	4.7579e-09	2.4047e-09	1.1807e-09	5.5269e-10	2.4193e-10
U02C03)2	5.8609e-15	4.7246e-15	2.9529e-15	1.6895e-15	9.3750e-16	5.1859e-16	2.8272e-16	1.4685e-16	7.0241e-17
U02+	6.1265e-07	1.0532e-06	7.5788e-07	5.3517e-07	3.7082e-07	2.5184e-07	1.6740e-07	1.0871e-07	6.8853e-08
U(OH)5-	2.0687e-14	4.3977e-14	4.6076e-14	4.7676e-14	4.9420e-14	5.1702e-14	5.4472e-14	5.7357e-14	5.9901e-14

precipitates

U020H)2C	2.9091e-04	2.2686e-05	0.	0.	0.	0.	0.	0.	0.
U02(C)	0.	1.0618e-05	3.0100e-05	1.4199e-05	6.6223e-06	3.0653e-06	1.4129e-06	6.5135e-07	3.0199e-07

species	distance									
	0.263	0.310	0.362	0.419	0.483	0.553	0.631	0.717	0.812	
U02++	3.4734e-09	1.2516e-09	4.2424e-10	1.3463e-10	3.9785e-11	1.0879e-11	2.7298e-12	6.2133e-13	1.2604e-13	
C03--	5.6028e-14	5.8378e-14	5.9979e-14	6.1369e-14	6.3144e-14	6.5999e-14	7.0951e-14	7.9744e-14	9.5467e-14	
H+	1.0179e-04	9.9963e-05	9.9060e-05	9.8681e-05	9.8546e-05	9.8501e-05	9.8477e-05	9.8444e-05	9.8372e-05	
E-	8.1172e-02	1.3506e-01	2.3155e-01	4.0982e-01	7.5013e-01	1.4223e+00	2.7974e+00	5.7136e+00	1.2126e+01	
OH-	2.3245e-08	2.3581e-08	2.3656e-08	2.3516e-08	2.3162e-08	2.2525e-08	2.1460e-08	1.9750e-08	1.7164e-08	
E-	9.1402e-02	7.2844e-02	5.3196e-02	3.2402e-02	1.0425e-02	-1.2734e-02	-3.6997e-02	-6.2151e-02	-8.7766e-02	
tempx	1.4972e+02	1.4956e+02	1.4930e+02	1.4885e+02	1.4810e+02	1.4683e+02	1.4469e+02	1.4115e+02	1.3547e+02	

complexes

HC03	1.0353e-07	1.0580e-07	1.0743e-07	1.0898e-07	1.1108e-07	1.1449e-07	1.2035e-07	1.3048e-07	1.4791e-07
H2C03	9.2784e-05	9.2782e-05	9.2780e-05	9.2778e-05	9.2775e-05	9.2771e-05	9.2762e-05	9.2746e-05	9.2716e-05
U020H+	1.0077e-08	3.6804e-09	1.2491e-09	3.9265e-10	1.1361e-10	2.9911e-11	7.0347e-12	1.4358e-12	2.4355e-13
U02C03	9.7838e-11	3.6418e-11	1.2492e-11	3.9524e-12	1.1503e-12	3.0539e-13	7.2832e-14	1.5234e-14	2.6985e-15
U02C03)2	3.0347e-17	1.1829e-17	4.2032e-18	1.3796e-18	4.2278e-19	1.2195e-19	3.3341e-20	8.6959e-21	2.1631e-21
U02+	4.2435e-08	2.5385e-08	1.4693e-08	8.1963e-09	4.3822e-09	2.2278e-09	1.0641e-09	4.6900e-10	1.8582e-10
U(OH)5-	6.1807e-14	6.3057e-14	6.3851e-14	6.4472e-14	6.5196e-14	6.6297e-14	6.8093e-14	7.0986e-14	7.5364e-14

precipitates

U020H)2C	0.	0.	0.	0.	0.	0.	0.	0.	0.
U02(C)	1.4159e-07	6.7333e-08	3.2407e-08	1.5685e-08	7.5632e-09	3.6010e-09	1.6797e-09	7.6356e-10	3.3879e-10

species	distance									
	0.918	1.034	1.164	1.307	1.465	1.640	1.834	2.048	2.285	
U02++	2.2172e-14	3.2514e-15	3.8094e-16	3.5696e-17	2.9278e-18	2.4967e-19	2.7864e-20	4.5683e-21	2.2586e-23	
C03--	1.2323e-13	1.6943e-13	2.3590e-13	3.1247e-13	3.9949e-13	6.2458e-13	4.0784e-12	6.4197e-08	7.3326e-06	
H+	9.8200e-05	9.7776e-05	9.6701e-05	9.3946e-05	8.6842e-05	6.8448e-05	2.5103e-05	6.5828e-08	4.2940e-10	
E-	2.6741e+01	6.1215e+01	1.4515e+02	3.5414e+02	8.8520e+02	2.2555e+03	5.5265e+03	1.1858e+04	2.1100e+04	
OH-	1.3630e-08	9.5250e-09	5.7463e-09	3.1279e-09	1.7736e-09	1.3409e-09	2.6400e-09	8.6725e-07	1.2776e-04	
E-	-1.1314e-01	-1.3739e-01	-1.5981e-01	-1.8041e-01	-2.0037e-01	-2.2130e-01	-2.4268e-01	-2.6202e-01	-2.7727e-01	
tempx	1.2684e+02	1.1479e+02	9.9835e+01	8.3939e+01	6.9906e+01	5.9837e+01	5.4035e+01	5.1362e+01	5.0377e+01	

OUTPUT

complexes

HC03	1.7713e-07	2.2307e-07	2.8675e-07	3.6035e-07	4.3872e-07	5.7291e-07	1.4563e-06	6.1036e-05	4.4511e-05
H2C03	9.2659e-05	9.2546e-05	9.2319e-05	9.1839e-05	9.0729e-05	8.7932e-05	8.0692e-05	8.7446e-06	4.0958e-08
U020H+	3.2327e-14	3.1324e-15	2.1202e-16	1.0680e-17	5.0671e-19	3.3861e-20	7.7423e-21	4.1858e-19	2.9722e-19
U02C03	3.8672e-16	4.2777e-17	3.5888e-18	2.4667e-19	1.7316e-20	1.8888e-21	1.3001e-21	3.1822e-18	1.6791e-18
U02C03)2	5.0089e-22	1.0021e-22	1.5288e-23	1.6655e-24	1.5755e-25	2.5983e-26	1.1113e-25	4.1522e-18	2.4702e-16
U02+	6.3974e-11	1.8490e-11	4.4222e-12	9.1381e-13	1.8305e-13	4.1124e-14	1.1817e-14	4.2148e-15	3.6684e-17
U(OH)5-	8.1131e-14	8.6623e-14	8.7894e-14	8.1956e-14	7.3247e-14	7.5491e-14	1.7626e-13	5.6534e-11	1.3976e-10

precipitates

U020H)2C	0.	0.	0.	0.	0.	0.	0.	0.	0.
U02(C)	1.5107e-10	7.2994e-11	4.3192e-11	3.2092e-11	2.7151e-11	2.3952e-11	2.3605e-11	0.	0.

species	distance								
	2.548	2.839	3.160	3.516	3.910	4.346	4.829	5.363	5.954
U02++	5.6795e-24	1.9733e-24	7.5474e-25	2.7617e-25	8.7905e-26	2.3154e-26	4.9658e-27	8.6828e-28	1.2464e-28
C03--	8.7748e-06	5.8869e-06	2.7659e-06	9.8617e-07	2.7802e-07	6.3428e-08	1.1867e-08	1.8364e-09	2.3654e-10
H+	1.9372e-10	1.3328e-10	1.1170e-10	1.0370e-10	1.0100e-10	1.0023e-10	1.0004e-10	1.0001e-10	1.0000e-10
E-	3.1108e+04	3.9214e+04	4.4203e+04	4.6575e+04	4.7460e+04	4.7723e+04	4.7786e+04	4.7798e+04	4.7800e+04
OH-	2.8105e-04	4.0929e-04	4.8956e-04	5.2802e-04	5.4242e-04	5.4670e-04	5.4772e-04	5.4792e-04	5.4795e-04
E-	-2.8782e-01	-2.9420e-01	-2.9752e-01	-2.9897e-01	-2.9950e-01	-2.9965e-01	-2.9969e-01	-2.9970e-01	-2.9970e-01
tempx	5.0086e+01	5.0016e+01	5.0002e+01	5.0000e+01	5.0000e+01	5.0000e+01	5.0000e+01	5.0000e+01	5.0000e+01

complexes

HC03	2.3652e-05	1.0795e-05	4.2239e-06	1.3942e-06	3.8240e-07	8.6545e-08	1.6162e-08	2.5001e-09	3.2200e-10
H2C03	9.7213e-09	3.0341e-09	9.9169e-10	3.0344e-10	8.1019e-11	1.8193e-11	3.3911e-12	5.2437e-13	6.7534e-14
U020H+	1.6161e-19	8.0826e-20	3.6742e-20	1.4459e-20	4.7229e-21	1.2534e-21	2.6930e-22	4.7104e-23	6.7624e-24
U02C03	4.8529e-19	1.1038e-19	1.9578e-20	2.5394e-21	2.2740e-22	1.3656e-23	5.4792e-25	1.4825e-26	2.7412e-28
U02C03)2	8.5104e-17	1.2974e-17	1.0810e-18	4.9992e-20	1.2620e-21	1.7291e-23	1.2980e-25	5.4347e-28	1.2944e-30
U02+	1.3449e-17	5.8419e-18	2.5068e-18	9.6443e-19	3.1257e-19	8.2767e-20	1.7773e-20	3.1085e-21	4.4625e-22
U(OH)5-	1.6990e-10	1.3595e-10	7.8625e-11	3.4358e-11	1.1654e-11	3.1272e-12	6.7366e-13	1.1789e-13	1.6926e-14

precipitates

U020H)2C	0.	0.	0.	0.	0.	0.	0.	0.	0.
U02(C)	0.	0.	0.	0.	0.	0.	0.	0.	0.

OUTPUT

species	distance				
	6.608	7.332	8.133	9.019	10.000
UO2++	1.4805e-29	1.4653e-30	1.2162e-31	8.5367e-33	1.0000-2419
CO3--	2.5501e-11	2.3127e-12	1.7725e-13	1.1561e-14	1.5653-2425
H+	1.0000e-10	1.0000e-10	1.0000e-10	1.0000e-10	1.0000e-10
E-	4.7800e+04	4.7800e+04	4.7800e+04	4.7800e+04	4.7800e+04
OH-	5.4795e-04	5.4796e-04	5.4796e-04	5.4796e-04	5.4796e-04
E-	-2.9970e-01	-2.9970e-01	-2.9970e-01	-2.9970e-01	-2.9970e-01
tempx	5.0000e+01	5.0000e+01	5.0000e+01	5.0000e+01	5.0000e+01
complexes					
HCO3	3.4714e-11	3.1482e-12	2.4129e-13	1.5737e-14	0.
H2CO3	7.2806e-15	6.6027e-16	5.0605e-17	3.3005e-18	0.
UO2OH+	8.0322e-25	7.9500e-26	6.5982e-27	4.6314e-28	5.6928-2426
UO2CO3	3.5101e-30	3.1507e-32	2.0042e-34	9.1753e-37	0.
UO2CO3)2	1.7868e-33	1.4546e-36	7.0914e-40	2.1174e-43	0.
UO2+	5.3004e-23	5.2462e-24	4.3541e-25	3.0563e-26	0.
U(OH)5-	2.0104e-15	1.9899e-16	1.6515e-17	1.1592e-18	1.1821-2416
precipitates					
UO2OH)2C	0.	0.	0.	0.	0.
UO2(C)	0.	0.	0.	0.	0.

APPENDIX 9

RECHARGE WATER COMPOSITION

INPUT AND SAMPLE OUTPUT

INPUT

Static equilibrium co2(g) dissolving in water-partitioning of C considered

UNITS	meter	sec.					
type	0	0	0	1			
iteration	100	100	100				
Calc.crtia	1.0e-30	1.0e-03	20	10	5	1.75	5
grid	05	10.0	0.0				
time	1	1.0	5.0				
print time	1.0						
physical	0.05	0.0	0.0				
tran bound	0	0					
temp bound	0	0					
isothermal	0						
Intl.	10.0						
leach	0	0					
WORD	blank						
In.sh.Info	-24.50	+0.01					
Iso.Ratio1	-0.91e-03	6.3					
	2 -4.54e-03	1099.0					
	3 -3.40e-03	870.0					
	4 -3.63e-03	1194.0					
no.species	3	0	0	3	0	2	0
CO2(g)	0.0 0	23.1623e-02	23.1623e-02	23.1623e-02	23.1623e-02		
H+	1.0 0	2 1.0e-05	1.0e-05	2 1.0e-05	1.0e-05		
OH-	-80.3723	-1.395e+03	32.5514	-3.181e-02			
	3.24e-10	3.24e-10					
H2CO3	0 1.0 0.0 0.0						
	87.598	-1055.95	-38.7233	4506e-02			
	0.0	0.0					
HC03-	0 1.0 0.0 1.0						
	127.844	-532.58	-52.2593	1543e-02			
	0.0	0.0					
CO3--	0 +1.0 0.0 2.0						
	281.934	-3619.68	-112.5486	2045e-02			
	0.0	0.0					

OUTPUT

1 Static equilibrium co2(g) dissolving in water-partitioning of C considered

unit of length is meter unit of time is sec.

inner boundary is constant concentration outer boundary is constant initial concentration

dispersion coefficient= 0.1v+ 0. fluid velocity = 0. number of grid points = 5

number of print outs = 1
given at the following times= 1.000

errsqr= 0.10e-29 climite= 0.10e-02 iterj= 20 iterm= 10 iterd= 5 dtmult= 0.17e+01 ndiv=

number of sites(ion-exchange) 0.0000 number of sites(edl model) 0.0000
this simulation is isothermal, temperature = 10.

2 bare ions 0 sorbing ions (ionex) 0 sorbing ions (edl model)

component	charge	kinetic code	initial condition type	initial condition value	boundary condition type	boundary condition value
CO2(g)	0.	0	2	3.1623e-02	2	3.1623e-02
H+	1.	0	2	1.0000e-05	2	1.0000e-05

4 complexes 0 sorbing complexes(ionex) 0 sorbing complexes (edl model)

complex	charge	kcode	stoichiometry		
OH-	-1.	0	0.	0.	1.
H2CO3	0.	0	1.	0.	0.
HCO3-	-1.	0	1.	0.	1.
CO3--	-2.	0	1.	0.	2.

C-13 Fractionation parameters:

shiftr= -24.5000 shifts= 0.0100

coefficients in log function of thermodynamic constants

-0.001 6.300
-0.005 1099.000
-0.003 870.000
-0.004 1194.000

APPENDIX 10

SCOPING SIMULATION OF YUCCA MOUNTAIN (NEVADA) GROUNDWATER
INPUT AND SAMPLE OUTPUT

INPUT

```

Groundwater evolution. Kinetic diss. of Calcit silica and glass-C-13 partition
UNITS      meter      second
Type       0          01          0          1
Iteration  100        100        100
Calc.crtia 1.0e-30      1.0e-03      20          10          5          1.75          5
Grid       20          10.0      836.68355
Time       17          5.0e-03      3.15e+04
Print time 360.0        3600.0      36000.0     144000.0     360000.0     864000.0     17.28e+05
print time 43.20e+05  86.40e+05   12.96e+06   17.28e+06   21.60e+06   25.92e+06   30.24e+06
print time 34.56e+06  38.88e+06   43.20e+06
Physical   0.10         1.0e-10      3.17e-08
Tran bound 1            0
Temp bound 0
Isothermal 0
Intl. temp 30.0
Leach      0            0
WORD      tpkin
*****Carbonate rock dissolution data; next 7 lines*****
1 PARAMS  5          100.0        4          prepc
2 CDATS   19.8        6.383        10.377      8.446 1.000e-03
3 INXi(i) 2 0         12 0         0 0         5 11
4 CONK(1) -1.32        0            0            0
5 CONK(2) -4.59        0            0            0
6 CONK(3) -6.94        0            0            0
7 CONK(4) 0.0          0            0            0
WORD      tpkin
*****Silica dissolution data; next 4 lines*****
1 PARAMS  0          100.0        2          preps
2 INXi(i) 0 0         -9 0
3 CONK(1) -0.369      -3438.0      0.0-7.890e-04
4 CONK(2) -0.707      -2598.0      0.0          0.0
WORD      exkin
*****Glass dissolution data; next 1 line*****
1 PARAMS  0          3.0e+06      0          dissg
WORD      blank
C-13 data -17.4        1.4
1 CONP(1) -0.91e-03      6.3
2 CONP(2) -4.54e-03      1099.0
3 CONP(3) -3.40e-03      870.0
4 CONP(4) -3.63e-03      1194.0
No.species 10          0            0            2            2            2            0
Na+        +1.0 1        2 1.0e-10     1.0e-10     2 3.00e-04     3.0e-04
H+         +1.0 2        2 8.653e-05    1.237e-10   2 8.59e-04     5.1e-09
Co3--      -2.0 31       3 1.012e-02    3.521e-05   3 8.59e-04     1.0e-06
neg.KI     0.0 32       1 1.000e-10    1.000e-10   1 1.615e-02     1.615e-02
Ca++       +2.0 4        3 1.012e-02    1.217e-04   1 2.45e-04     2.45e-04
Cl-        -1.0 0         1 1.0e-10     1.0e-10     1 3.39e-05     3.39e-05
K+         +1.0 3         1 1.0e-10     1.0e-10     1 1.49e-04     1.49e-04
Mg++       +2.0 5         1 1.0e-10     1.0e-10     1 6.17e-05     6.17e-05
H4SiO4     0.0 0         3 1.0e-02     1.0e-10     3 2.67e-04     2.67e-04
OH-        -13.990      0.0          0.0          0.0
           8.653e-05  2.0e-06

```

INPUT

HC03-	33	0.0	1.0	1.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.0		10.337		0.0		0.0		0.0		0.0	
		8.649e-05	8.59e-04								
H2CO3	34	0.0	2.0	1.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.0		16.700		0.0		0.0		0.0		0.0	
		2.359e-08		0.0							
CaCO3	13	0.0	0.0	1.0	0.0	1.0	0.0	0.0	0.0	0.0	
0.0		-8.446		0.0		0.0		0.0		0.0	
		0.01		0.0							
SiO2	14	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.0	0.0
0.0		-20.0									
		0.01		0.0							

OUTPUT

1Groundwater evolution. Kinetic diss. of Calcit silica and glass-C-13 partition

unit of length is meter unit of time is second

kinetics of rev. precipitate dissolution considered

kinetics of rev. precipitate dissolution considered

kinetics of non-rev. silica dissolution considered

inner boundary is constant flux outer' boundry is constant initial concentration

dispersion coefficient= 0.1v+ 0.10e-09 fluid velocity = 0.317e-07 number of grid points = 20

number of print outs = 17
 given at the following times= 360.0 3600. 0.3600e+050.1440e+060.3600e+060.8640e+060.1728e+070.4320e+07
 0.8640e+070.1296e+080.1728e+080.2160e+080.2592e+080.3024e+080.3456e+080.3888e+080.4320e+08

errsq= 0.10e-29 climit= 0.10e-02 iterj= 20 item= 10 iterd= 5 dtmult= 0.17e+01 ndiv=

number of sites(ion-exchange) 0.0000 number of sites(edl model) 0.0000
 this simulation is isothermal, temperature = 30.

9 bare ions 0 sorbing ions (ionex) 0 sorbing ions (edl model)

component	charge	kinetic code	initial condition type	initial condition value	boundary condition type	boundary condition value
Na+	1.	1	2	1.0000e-10	2	3.0000e-04
H+	1.	2	2	8.6530e-05	2	8.5900e-04
Co3--	-2.	31	3	1.0120e-02	3	8.5900e-04
neg.KI	0.	32	1	1.0000e-10	1	1.6150e-02
Ca++	2.	4	3	1.0120e-02	1	2.4500e-04
Cl-	-1.	0	1	1.0000e-10	1	3.3900e-05
K+	1.	3	1	1.0000e-10	1	1.4900e-04
Mg++	2.	5	1	1.0000e-10	1	6.1700e-05
H4SiO4	0.	0	3	1.0000e-02	3	2.6700e-04

3 complexes 0 sorbing complexes(ionex) 0 sorbing complexes (edl model)

OUTPUT

complex	charge	kcode	stoichiometry								
OH-	-1.	0	0.	0.	0.	0.	0.	0.	0.	0.	1.
HCO3-	-1.	33	0.	1.	1.	0.	0.	0.	0.	0.	0.
H2CO3	0.	34	0.	2.	1.	0.	0.	0.	0.	0.	0.

2 solid precipitates

precipitate	kinetic code	stoichiometry									
CaCO3	13	0.0	0.0	1.0	0.0	1.0	0.0	0.0	0.0	0.0	0.0
SiO2	14	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.0

Calcite dissolution information:

no of terms in the rate formula = 4
 no of other additional data needed = 5
 representative surface parameter = 0.100e+03
 xdiag = prepc

additional data for rate calculation

0.198e+02 0.638e+01 0.104e+02 0.845e+01 0.100e-02

binary element nos. of the terms of the rate equation
 2 0 12 0 0 0 5 11

coefficients in log function of thermodynamic constants

-1.320	0.000	0.000	0.000
-4.590	0.000	0.000	0.000
-6.940	0.000	0.000	0.000
0.000	0.000	0.000	0.000

Silicate-water reaction information:

no of terms in the rate formula = 2
 no of other additional data needed = 0
 representative surface parameter = 0.100e+03
 xdiag = preps

OUTPUT

binary element nos. of the terms of the rate equation
0 0 -9 0

coefficients in log function of thermodynamic constants
-0.369 -3438.000 0.000 -0.001
-0.707 -2598.000 0.000 0.000

Glass dissolution information:

no of terms in the rate formula = 0
no of other additional data needed = 0
representative surface parameter = 0.300e+07

xdiag = dissg

C-13 Fractionation parameters:

shiftr= -17.4000 shifts= 1.4000

coefficients in log function of thermodynamic constants
-0.001 6.300
-0.005 1099.000
-0.003 870.000
-0.004 1194.000

** spatial grid **

0.	0.5086e-02	0.1233e-01	0.2266e-01	0.3738e-01	0.5835e-01	0.8823e-01	0.1308	0.1915	0.2780
0.4012	0.5768	0.8271	1.184	1.692	2.416	3.448	4.918	7.014	10.00

OUTPUT

1

initial conditions
temp= 30.00

component	total aqueous conc.	bare ion concentration	sorbed concentration		act. coef.	kd(ion ex)	kd(edl)
			(ionex)	(edl)			
Na+	0.1000e-09	0.1000e-09	0.	0.	0.9778	0.	0.
H+	0.8653e-04	0.1237e-09	0.	0.	0.9778	0.	0.
Co3--	0.1217e-03	0.3521e-04	0.	0.	0.9141	0.	0.
neg.KI	0.1000e-09	0.1000e-09	0.	0.	1.000	0.	0.
Ca++	0.1217e-03	0.1217e-03	0.	0.	0.9141	0.	0.
Cl-	0.1000e-09	0.1000e-09	0.	0.	0.9778	0.	0.
K+	0.1000e-09	0.1000e-09	0.	0.	0.9778	0.	0.
Mg++	0.1000e-09	0.1000e-09	0.	0.	0.9141	0.	0.
H4SiO4	0.1000e-19	0.1000e-19	0.	0.	1.000	0.	0.
OH-	0.8654e-04	0.8654e-04	0.	0.	0.9778	0.	0.

complex	valence	aqueous conc.	sorption(io)	sorption(edl)
HCO3-	-1.000	0.8648e-04	0.	0.
H2CO3	0.	0.2359e-07	0.	0.

precipitate equivalent moles/liter solution

CaCO3	0.100e-01
SiO2	0.100e-01

to have a net balance of zero charge, other species must be present (although not participating in the chemical reactions) with a total concentration times charge of 0.990e-08

OUTPUT

1								
component	boundary or influx conditions					act. coef.	kd(ion ex)	kd(edl)
	total aqueous conc.	bare ion concentration	temp= 30.00	sorbed concentration (ionex)	sorbed concentration (edl)			
Na+	0.3000e-03	0.3000e-03	0.	0.	0.	0.9601	0.	0.
H+	0.8590e-03	0.5046e-08	0.	0.	0.	0.9601	0.	0.
Co3--	0.8590e-03	0.9028e-05	0.	0.	0.	0.8496	0.	0.
neg.KI	0.1615e-01	0.1615e-01	0.	0.	0.	1.000	0.	0.
Ca++	0.2450e-03	0.2450e-03	0.	0.	0.	0.8496	0.	0.
Cl-	0.3390e-04	0.3390e-04	0.	0.	0.	0.9601	0.	0.
K+	0.1490e-03	0.1490e-03	0.	0.	0.	0.9601	0.	0.
Mg++	0.6170e-04	0.6170e-04	0.	0.	0.	0.8496	0.	0.
H4SiO4	0.2670e-03	0.2670e-03	0.	0.	0.	1.000	0.	0.
OH-	0.2200e-05	0.2200e-05	0.	0.	0.	0.9601	0.	0.
complex	valence	aqueous conc.	sorption(io)	sorption(edl)				
HCO3-	-1.000	0.8409e-03	0.	0.				
H2CO3	0.	0.9023e-05	0.	0.				
precipitate	equivalent moles/liter solution							
CaCO3	0.							
SiO2	0.							

to have a net balance of zero charge, other species must be present (although not participating in the chemical reactions) with a total concentration times charge of -0.167e-03

OUTPUT

1 time= 4.74489e+03 delt= 1.9447e+03 concentration of species in moles/liter solution

species	distance									
	0.000	0.005	0.012	0.023	0.037	0.058	0.088	0.131	0.192	
Na+	1.1344e-05	3.2266e-06	9.6824e-07	6.8630e-07	6.8993e-07	6.6946e-07	6.6945e-07	6.6943e-07	6.6942e-07	
H+	1.3624e-10	1.2547e-10	1.2262e-10	1.2227e-10	1.2225e-10	1.2224e-10	1.2223e-10	1.2222e-10	1.2220e-10	
Co3--	4.0049e-05	3.6681e-05	3.5646e-05	3.5515e-05	3.5510e-05	3.5514e-05	3.5519e-05	3.5526e-05	3.5537e-05	
neg.KI	5.7509e-04	1.3760e-04	1.6056e-05	9.0329e-07	2.4882e-08	4.3726e-10	1.0232e-10	1.0001e-10	1.0000e-10	
Ca++	1.2614e-04	1.2281e-04	1.2188e-04	1.2177e-04	1.2177e-04	1.2178e-04	1.2179e-04	1.2181e-04	1.2183e-04	
Cl-	1.2073e-06	2.8893e-07	3.3802e-08	1.9959e-09	1.5202e-10	1.0071e-10	1.0000e-10	1.0000e-10	1.0000e-10	
K+	5.8201e-06	1.7955e-06	6.7695e-07	5.3747e-07	5.2938e-07	5.2916e-07	5.2916e-07	5.2916e-07	5.2916e-07	
Mg++	2.2637e-06	5.9250e-07	1.2754e-07	6.9489e-08	6.6117e-08	6.6022e-08	6.6018e-08	6.6015e-08	6.6010e-08	
H4SiO4	1.0027e-05	2.8053e-06	7.9851e-07	5.4831e-07	5.3381e-07	5.3341e-07	5.3340e-07	5.3340e-07	5.3340e-07	
OH-	7.8732e-05	8.5356e-05	8.7295e-05	8.7542e-05	8.7559e-05	8.7564e-05	8.7570e-05	8.7579e-05	8.7591e-05	
shftsol	-2.4866e+00	3.2499e-01	1.2689e+00	1.3926e+00	1.3998e+00	1.4000e+00	1.4000e+00	1.4000e+00	1.4000e+00	
shift0	-4.3565e+00	-1.6599e+00	-7.4909e-01	-6.2959e-01	-6.2267e-01	-6.2255e-01	-6.2265e-01	-6.2279e-01	-6.2300e-01	
shift1	3.9017e+00	6.6206e+00	7.5390e+00	7.6595e+00	7.6665e+00	7.6666e+00	7.6665e+00	7.6664e+00	7.6661e+00	
shift2	2.5455e+00	5.2608e+00	6.1779e+00	6.2982e+00	6.3052e+00	6.3053e+00	6.3052e+00	6.3051e+00	6.3049e+00	

complexes

HCO3-	1.0789e-04	9.1293e-05	8.6787e-05	8.6230e-05	8.6201e-05	8.6205e-05	8.6211e-05	8.6220e-05	8.6232e-05
H2CO3	3.2346e-08	2.5247e-08	2.3467e-08	2.3251e-08	2.3239e-08	2.3238e-08	2.3238e-08	2.3238e-08	2.3238e-08

precipitates

CaCO3	9.9983e-03	9.9983e-03	9.9983e-03	9.9983e-03	9.9983e-03	9.9983e-03	9.9982e-03	9.9982e-03	9.9982e-03
SiO2	9.9995e-03	9.9995e-03	9.9995e-03	9.9995e-03	9.9995e-03	9.9995e-03	9.9995e-03	9.9995e-03	9.9995e-03

species	distance									
	0.278	0.401	0.577	0.827	1.184	1.692	2.416	3.448	4.918	
Na+	6.6939e-07	6.6935e-07	6.6930e-07	6.6923e-07	6.6914e-07	6.6902e-07	6.6887e-07	6.6870e-07	6.6852e-07	
H+	1.2218e-10	1.2215e-10	1.2210e-10	1.2204e-10	1.2196e-10	1.2186e-10	1.2173e-10	1.2158e-10	1.2142e-10	
Co3--	3.5551e-05	3.5571e-05	3.5598e-05	3.5636e-05	3.5685e-05	3.5749e-05	3.5827e-05	3.5920e-05	3.6022e-05	
neg.KI	1.0000e-10	1.0000e-10	1.0000e-10	1.0000e-10	1.0000e-10	1.0000e-10	1.0000e-10	1.0000e-10	1.0000e-10	
Ca++	1.2186e-04	1.2191e-04	1.2197e-04	1.2205e-04	1.2216e-04	1.2230e-04	1.2247e-04	1.2268e-04	1.2290e-04	
Cl-	1.0000e-10	1.0000e-10	1.0000e-10	1.0000e-10	1.0000e-10	1.0000e-10	1.0000e-10	1.0000e-10	1.0000e-10	
K+	5.2916e-07	5.2916e-07	5.2916e-07	5.2916e-07	5.2916e-07	5.2916e-07	5.2916e-07	5.2916e-07	5.2916e-07	
Mg++	6.6004e-08	6.5995e-08	6.5983e-08	6.5967e-08	6.5945e-08	6.5918e-08	6.5884e-08	6.5845e-08	6.5804e-08	
H4SiO4	5.3340e-07	5.3340e-07	5.3340e-07	5.3340e-07	5.3340e-07	5.3340e-07	5.3340e-07	5.3340e-07	5.3340e-07	
OH-	8.7609e-05	8.7633e-05	8.7666e-05	8.7711e-05	8.7770e-05	8.7846e-05	8.7941e-05	8.8052e-05	8.8174e-05	
shftsol	1.4000e+00	1.4000e+00	1.4000e+00	1.4000e+00	1.4000e+00	1.4000e+00	1.4000e+00	1.4000e+00	1.4000e+00	
shift0	-6.2329e-01	-6.2370e-01	-6.2425e-01	-6.2500e-01	-6.2600e-01	-6.2728e-01	-6.2886e-01	-6.3072e-01	-6.3276e-01	
shift1	7.6659e+00	7.6654e+00	7.6649e+00	7.6641e+00	7.6631e+00	7.6618e+00	7.6602e+00	7.6584e+00	7.6563e+00	
shift2	6.3046e+00	6.3042e+00	6.3036e+00	6.3029e+00	6.3018e+00	6.3006e+00	6.2990e+00	6.2971e+00	6.2950e+00	

OUTPUT

complexes

HC03-	8.6249e-05	8.6274e-05	8.6307e-05	8.6351e-05	8.6411e-05	8.6487e-05	8.6582e-05	8.6694e-05	8.6816e-05
H2C03	-2.3239e-08	2.3239e-08	2.3239e-08	2.3239e-08	2.3239e-08	2.3240e-08	2.3240e-08	2.3241e-08	2.3241e-08

precipitates

CaC03	9.9982e-03	9.9981e-03	9.9981e-03	9.9980e-03	9.9979e-03	9.9977e-03	9.9976e-03	9.9974e-03	9.9971e-03
Si02	9.9995e-03	9.9995e-03	9.9995e-03	9.9995e-03	9.9995e-03	9.9995e-03	9.9995e-03	9.9995e-03	9.9995e-03

distance

species	7.014	10.000
Na+	6.6836e-07	1.0000e-10
H+	1.2126e-10	1.2367e-10
Co3--	3.6124e-05	3.5208e-05
neg.KI	1.0000e-10	1.0000e-10
Ca++	1.2312e-04	1.2171e-04
Cl-	1.0000e-10	1.0000e-10
K+	5.2917e-07	1.0000e-10
Mg++	6.5764e-08	1.0000e-10
H4Si04	5.3341e-07	1.0000e-20
OH-	8.8296e-05	8.6540e-05
shftsol	1.4000e+00	1.4000e+00
shift0	-6.3480e-01	-6.0566e-01
shift1	7.6543e+00	7.6836e+00
shift2	6.2930e+00	6.3223e+00

complexes

HC03-	8.6938e-05	8.6483e-05
H2C03	2.3242e-08	2.3589e-08

precipitates

CaC03	9.9969e-03	9.9983e-03
Si02	9.9995e-03	1.0000e-02

OUTPUT

1 time= 4.32179e+07 delt= 3.1500e+04 concentration of species in moles/liter solution

species	distance								
	0.000	0.005	0.012	0.023	0.037	0.058	0.088	0.131	0.192
Na+	3.0470e-04	3.0493e-04	3.0526e-04	3.0573e-04	3.0640e-04	3.0735e-04	3.0871e-04	3.1064e-04	3.1339e-04
H+	2.6808e-09	2.6106e-09	2.5212e-09	2.4159e-09	2.3063e-09	2.2117e-09	2.1456e-09	2.0965e-09	2.0380e-09
Co3--	1.7020e-05	1.7476e-05	1.8092e-05	1.8871e-05	1.9748e-05	2.0551e-05	2.1106e-05	2.1489e-05	2.1893e-05
neg.KI	1.6126e-02	1.6125e-02	1.6123e-02	1.6120e-02	1.6116e-02	1.6110e-02	1.6099e-02	1.6081e-02	1.6046e-02
Ca++	2.5025e-04	2.5051e-04	2.5080e-04	2.5106e-04	2.5106e-04	2.5036e-04	2.4846e-04	2.4499e-04	2.3960e-04
Cl-	3.3849e-05	3.3847e-05	3.3843e-05	3.3838e-05	3.3829e-05	3.3815e-05	3.3793e-05	3.3754e-05	3.3682e-05
K+	1.5115e-04	1.5126e-04	1.5141e-04	1.5162e-04	1.5193e-04	1.5236e-04	1.5298e-04	1.5384e-04	1.5504e-04
Mg++	6.2651e-05	6.2697e-05	6.2764e-05	6.2859e-05	6.2994e-05	6.3186e-05	6.3462e-05	6.3858e-05	6.4427e-05
H4SiO4	5.1032e-04	5.2228e-04	5.3917e-04	5.6294e-04	5.9623e-04	6.4250e-04	7.0612e-04	7.9227e-04	9.0637e-04
OH-	4.1450e-06	4.2567e-06	4.4079e-06	4.6003e-06	4.8192e-06	5.0255e-06	5.1800e-06	5.3005e-06	5.4564e-06
shftsol	-1.7296e+01	-1.7291e+01	-1.7286e+01	-1.7281e+01	-1.7282e+01	-1.7299e+01	-1.7342e+01	-1.7420e+01	-1.7541e+01
shift0	-1.7476e+01	-1.7473e+01	-1.7471e+01	-1.7471e+01	-1.7477e+01	-1.7499e+01	-1.7546e+01	-1.7627e+01	-1.7751e+01
shift1	-9.3267e+00	-9.3241e+00	-9.3216e+00	-9.3212e+00	-9.3276e+00	-9.3494e+00	-9.3969e+00	-9.4784e+00	-9.6039e+00
shift2	-1.0665e+01	-1.0662e+01	-1.0660e+01	-1.0660e+01	-1.0666e+01	-1.0688e+01	-1.0735e+01	-1.0817e+01	-1.0942e+01
complexes									
HC03-	8.4071e-04	8.4054e-04	8.4026e-04	8.3975e-04	8.3879e-04	8.3705e-04	8.3406e-04	8.2927e-04	8.2173e-04
H2C03	4.7876e-06	4.6611e-06	4.4997e-06	4.3088e-06	4.1084e-06	3.9316e-06	3.8008e-06	3.6930e-06	3.5548e-06
precipitates									
CaC03	9.9107e-03	9.8216e-03	9.8115e-03	9.8410e-03	9.9299e-03	1.0065e-02	1.0178e-02	1.0213e-02	1.0201e-02
SiO2	6.2162e-03	6.2391e-03	6.2712e-03	6.3162e-03	6.3787e-03	6.4644e-03	6.5804e-03	6.7335e-03	6.9288e-03

species	distance								
	0.278	0.401	0.577	0.827	1.184	1.692	2.416	3.448	4.918
Na+	3.1723e-04	3.2240e-04	3.2880e-04	3.2923e-04	2.6114e-04	1.4402e-04	8.0063e-05	6.5135e-05	6.2020e-05
H+	1.9409e-09	1.7840e-09	1.5119e-09	9.6662e-10	3.2675e-10	1.0654e-10	6.6051e-11	6.0041e-11	6.0243e-11
Co3--	2.2601e-05	2.3890e-05	2.6577e-05	3.4904e-05	5.8280e-05	8.3547e-05	4.9508e-05	4.5675e-05	4.5084e-05
neg.KI	1.5977e-02	1.5821e-02	1.5435e-02	1.4031e-02	9.2288e-03	3.4089e-03	6.8229e-04	6.9372e-05	4.0841e-06
Ca++	2.3128e-04	2.1784e-04	1.9441e-04	1.4542e-04	8.3433e-05	7.3212e-05	9.2452e-05	9.9991e-05	1.0123e-04
Cl-	3.3537e-05	3.3210e-05	3.2399e-05	2.9452e-05	1.9372e-05	7.1555e-06	1.3903e-06	1.4572e-07	8.6725e-09
K+	1.5666e-04	1.5863e-04	1.6040e-04	1.5648e-04	1.2574e-04	8.2922e-05	6.1652e-05	5.7124e-05	5.5211e-05
Mg++	6.5243e-05	6.6399e-05	6.8017e-05	6.8514e-05	5.1893e-05	2.3752e-05	9.0588e-06	5.6852e-06	5.2057e-06
H4SiO4	1.0527e-03	1.2319e-03	1.4366e-03	1.6458e-03	1.8097e-03	1.8875e-03	1.9074e-03	1.9116e-03	1.8969e-03
OH-	5.7211e-06	6.2192e-06	7.3272e-06	1.1412e-05	3.3409e-05	1.0135e-04	1.6284e-04	1.7904e-04	1.7841e-04
shftsol	-1.7726e+01	-1.8023e+01	-1.8543e+01	-1.9636e+01	-2.0464e+01	-1.6021e+01	-4.4182e+00	7.0401e-01	1.3586e+00
shift0	-1.7943e+01	-1.8252e+01	-1.8802e+01	-2.0007e+01	-2.1406e+01	-1.8233e+01	-7.4116e+00	-2.4654e+00	-1.8066e+00
shift1	-9.7971e+00	-1.0109e+01	-1.0664e+01	-1.1879e+01	-1.3289e+01	-1.0090e+01	8.2124e-01	5.8085e+00	6.4727e+00
shift2	-1.1135e+01	-1.1446e+01	-1.2000e+01	-1.3214e+01	-1.4622e+01	-1.1427e+01	-5.3079e-01	4.4497e+00	5.1131e+00

OUTPUT

complexes

HC03-	8.0942e-04	7.8770e-04	7.4495e-04	6.3079e-04	3.6356e-04	1.3209e-04	6.4313e-05	5.3992e-05	5.3490e-05
H2CO3	3.3396e-06	2.9897e-06	2.3999e-06	1.3047e-06	2.5687e-07	3.0764e-08	9.3228e-09	7.1183e-09	7.0770e-09

precipitates

CaCO3	1.0182e-02	1.0160e-02	1.0135e-02	1.0103e-02	1.0065e-02	1.0037e-02	1.0024e-02	1.0022e-02	1.0022e-02
SiO2	7.1658e-03	7.4320e-03	7.6973e-03	7.9132e-03	8.0370e-03	8.0801e-03	8.0885e-03	8.0903e-03	8.0785e-03

distance

species	7.014	10.000
Na+	7.2687e-05	1.0000e-10
H+	5.4590e-11	1.2367e-10
Co3--	4.6232e-05	3.5208e-05
neg.KI	1.4048e-07	1.0000e-10
Ca++	9.9067e-05	1.2171e-04
Cl-	3.9466e-10	1.0000e-10
K+	6.5540e-05	1.0000e-10
Mg++	5.9913e-06	1.0000e-10
H4SiO4	2.0633e-03	1.0000e-20
OH-	1.9706e-04	8.6540e-05
shftsol	1.3985e+00	1.4000e+00
shift0	-1.9390e+00	-6.0566e-01
shift1	6.3392e+00	7.6836e+00
shift2	4.9797e+00	6.3223e+00

complexes

HC03-	4.9617e-05	8.6483e-05
H2CO3	5.9433e-09	2.3589e-08

precipitates

CaCO3	1.0020e-02	9.9983e-03
SiO2	8.2560e-03	1.0000e-02

APPENDIX 11

INPUT PREPARATION GUIDE

CHMTRNS

USER'S GUIDE

Card 1a: The title of the problem can be up to 80 characters long.

variable	Title
columns	1-80
format	20A4

TITLE title information for the problem

Card 1b: List of units of length and time.

variable	UIENGHT	UTIME
columns	11-18	19-26
format	A8	A8

ULENGHT Unit of length

UTIME Unit of time

Card 2: geometry (1-D or radial), mode (static or dynamic), initial guess (given or calculated) and C-13 isotop partition option

variable	ITYPE	IDYNAM	IG	IPART
columns	11-20	21-30	31-40	41-50
format	I10	I10	I10	I10

ITYPE geometry:
0-one-dimensional; 1-radial

IDYNAM code to indicate if the problem should stop after computing equilibrium distribution of species for initial and boundary conditions
0-stop; 1-continue execution for time and transport effects

IG code to indicate whether the program or the user will provide initial guesses of the concentrations:
0-user will; 1-program will

IPART code to indicate if C-13 partition should be considered
 0-no partition; 1-partition

Card 3a: These parameters control the number of iterations performed, when calculating the equilibrium distribution of species, before intermediate calculations are printed. If the calculations converge slowly because of a poor initial guess, for example, then examining the old and new guesses will provide an idea of how the guess can be improved. To suppress printing intermediate calculations, values of 100 are recommended for all of these parameters. If the calculations do not converge after 100 iterations, the program will stop executing and print a message.

variable	IN1	IN2	IN3
columns	11-20	21-30	31-40
format	I10	I10	I10

IN1 number of iterations before printing when calculating the equilibrium distribution of the initial conditions

IN2 number of iterations before printing when calculating the equilibrium distribution at the grid point where the boundary condition is specified

IN3 number of iterations before printing when calculating the equilibrium distribution at a node where a new precipitate is forming

Card 3b: These parameters specify the convergence criterion (ERRSQR) in dynamic mode, the concentration threshold (CLIMIT), the interval of iteration (ITERJ) when a new jacobian matrix is calculated, the number of iterations at which the current time step may be increased, upon convergence (ITERM), or decrease, when problem does not converge (ITERD), the multiplier DTMULT and the number (NDIV) of times that the time step can be decreased before the program stops due to nonconvergence

variable	CLIMIT	ERRSQR	ITERJ	ITERM	ITERD	DTMULT	NDIV
column	11-20	21-30	31-40	41-50	51-60	61-70	71-80
format	E10.3	E10.3	I10	I10	I10	E10.3	I10

CLIMIT minimum concentration threshold of any species

ERRSQR maximum least square error limit

ITERJ interval of iterations when a new jacobian is calculated

ITERM if solution converges within this number of iterations the time step is multiplied by DTMULT

ITERD if the solution does not converge within this number of iterations, the time step is divided by DTDIV and the solution procedure is restarted at the previous time level plus the new time step

ITMULT the time step multiplier

NDIV number of times DELT can be decreased

Card 4: The user must supply several parameters which control the grid spacing. For an evenly spaced grid (GC = 0), the grid spacing DX is equal to XMAX/(NMAX-1). For a variable grid, DX varies and is the difference between adjacent grid points. X(i) calculated from

$$X(i) = \left[\frac{GC \left(\frac{i-1}{N-1} \right) - 1}{GC - 1} \right] XMAX + X(1) \quad i = 2, NMAX$$

where X(1) = 0 for one-dimensional geometry and X(1) = R_w for radial geometry

variable	NMAX	XMAX	GC	R _w
columns	11-20	21-30	31-40	41-50
format	I10	F10.3	F10.3	F10.3

NMAX number of grid points

XMAX distance between the first and last grid points (L)

GC parameter used to calculate the grid spacing (see equation above)

R_w radius of inner boundary in axial symmetry case. To be left blank for one-dimensional geometry

Card 5: The user must specify the number of times at which the results are to be printed, the size of the first time step and the size of the maximum time step allowed. The initial time step is usually between 10⁻⁴ and 10⁻⁵ (in units of time used for the flow velocity). To minimize numerical dispersion, the maximum time step should be approximately DX/VO, where DX is the grid spacing calculated from the grid parameters of Card 4 and VO is the velocity of CARD 7.

variable	KMAX	DTINI	DTMAX
columns	11-20	21-30	31-40
format	I10	F10.3	F10.3

KMAX number of times at which the results are to be printed

DTINI size of the initial time step [t]
 DTMAX size of the maximum time step permitted [t]

Card 6: The program will print the results at times nearest those specified, KMAX times, where KMAX was given on Card 5, are read, seven to a card.

variable TPRINT(K), K = 1, KMAX
 columns 11-80/1-80
 format 7F10.3/8F10.3

TPRINT array which holds the times at which the results are to be printed [t]

Card 7: The hydrodynamic dispersion coefficient is calculated from the dispersivity, diffusion coefficient and fluid velocity given by the user (DOA * VO + DOB).

variable DOA DOB VO
 columns 11-20 21-30 31-40
 format F10.3 F10.3 F10.3

DOA dispersivity [L]
 DOB diffusion coefficient [L²/t]
 VO for one-dimensional flow (ITYPE = 0 on Card 2), this is the mean fluid velocity (i.e., the specific discharge divided by the porosity) [L/t]; for radial flow (ITYPE = 1 on Card 2), it is a constant equal to the radial distance times the mean fluid velocity [l/t]

Card 8: the user must provide integer codes for the type of flow boundary conditions at both the inner and outer boundaries. At the inner boundary, either a concentration or a flux boundary condition is possible. At the outer boundary, either a concentration boundary where the fluid remains at the initial conditions or a no-flux boundary is possible.

variable IBND(1) IBND(2)
 columns 11-20 21-30
 format I10 I10

IBND(1) type of boundary condition to be imposed at the inner boundary:
 0-constant concentration; 1-constant flux

IBND(2) type of boundary condition to be imposed at the outer boundary:
0-constant concentration equal to initial conditions;
1-no flux

Card 9: Integer codes for the type of thermal boundary conditions

variable	IBNDT(1)	IBNDT(2)
column	11-20	21-30
format	I10	I10

IBNDT(1) type of boundary conditions imposed at the inner boundary: 0-constant temperature; 1-constant flux

IBNDT(2) type of boundary conditions imposed at the outer boundary: 0-constant temperature equal to initial conditions; 1-no flux

Card 10: The thermal mode is specified here. The choices are constant temperature, mixing of waters with different temperatures, or a fixed temperature gradient.

variable	ITEMP
columns	11-20
format	I10

ITEMP code for type of thermal mode:
0-constant temperature; 1-mixing; 2-fixed gradient

Card 10a: read only if ITEMP = 0 on Card 10

variable	TEMP
columns	11-20
format	F10.3

TEMP constant temperature for this simulation

Card 10b: read only if ITEMP = 1 on Card 10.

variable	TEMP	TEMPI	HCW	HCM	TCM
columns	11-20	21-30	31-40	41-50	51-60
format	F10.3	F10.3	E10.2	E10.2	E10.2

TEMP	initial temperature
TEMPI	if IBND(2) = 0, constant temperature at inner boundary; if IBND(2) = 1, temperature of incoming fluid
HGW	heat capacity of fluid per unit volume of porous medium
HCM	heat capacity of fluid per unit volume of porous medium
TCM	thermal conductivity of saturated porous medium

Card 10c: read only if TEMP = 2 on Card 10.

variable	TEMPI	TEMPO
columns	11-20	21-30
format	F10.3	F10.3

TEMPI	temperature at inner boundary
TEMPO	temperature at outer boundary

Card 11: There is an option in the program to allow a solid to leach into the groundwater; however, at this time, the option is limited to one solid located at the first grid point. The user must include the solid in the list of precipitates and give its position in that list on this card.

variable	LEACH	NB
columns	11-20	21-30
format	I10	I10

LEACH	position in the list of precipitates of the solid which is leaching: 0-no leaching
NB	location of the solid which is leaching: 0-no leaching; 1-solid is leaching at the first grid point

Card 12a: redox and kinetic option indicator—omit cards 12 if WORD is BLANK

variable	WORD
column	11-15
format	A5

WORD	option activator:
------	-------------------

exkin-Claassen and White's (1979) imperical glass dis-
sulation rate activated

tpkin-plummer et al. (1978)'s rate equation and/or Rim-
stidt and Barnes (1980) silica-water rate equa-
tion activated

redox-redox option activated

Card 12b: redox constants-needed only if WORD is REDOX

variable	GASCON	FARCON
column	11-20	21-30
format	F10.3	F10.3

GASCON	Universal gas constant
FARCON	Faraday constant

Card 12c: Information regrading the kinetic option considered

variable	non
column	1-80
format	80X

Card 12d: kinetic dissolution constants-glass dissolution information
to be read last

variable	NPARAM	SAREA	NSRT	XDIAG
column	11-20	21-30	31-40	41-45
format	I10	F10.3	I10	A5

NPARAM	number of additional data for a kinetic equation to be read in the next card
SAREA	a constant representing surface influence in the kinetic mass transfer
NSRT	number of terms in the rate equation
XDIAG	prepc-calcite kinetics considered; preps-Silica kinet- ics considered; dissg-glass dissolution con- sidered

Card 12e: additional constants used in the rate equation-disregard if
NPARAM = 0

variable CDAT(i), i = 1, NPARAM
column 1-80
format 8e10.2

CDAT Array for rate equation parameters

Card 12f: designation of elements participating in the rate equation
(not used for glass kinetics)-4 sets of data per card

variable INXI(i) INX2(i) i = 1, NSRT
column 1-5 6-10
format 4(2I5)

INX1, INX2 designate the binary components of each term of the rate equation in the list of species of the problem. Forward reaction terms get a positive sequence number while back reactions elements are negative. 0 specifies a non-existing term. When both INX1 and INX2 are zero it implies just a value of 1.0 for the binary expression.

Card 12g: parameters for calculation of reaction terms in the rate equation-one card for each thermodynamic parameter

variable CONK(i,j) j = 1,4 ; i = 1, NSRT
column 11-80
format 10x, 7f10.3

CONK coefficients in function for log of reaction constants

Card 13a: omit if IPART = 0, Delta-13 for water and rock if IPART = 1.

variable SHIFTR SHIFTS
columns 11-20 21-30
format 10X, 2F10.3

SHIFTR delta C-13 in the sail water

SHIFTS delta C-13 of the rocks

Card 13b: omit if IPART = 0, 4 cards are read here

variable CONP(i,j) j = 1,2, i = 1,4
column 11-80
format 10X, 2F10.3

CONP coefficients in function for log of equilibrium con-

Card 14: Integer data are read on this card: the number of basis species, the number of species which are sorbed following either an ion exchange mechanism or a surface complexation model, the number of aqueous complexes, the number of solid precipitates and the position of H⁺ and e⁻ in the list of basis species which follows.

variable	NUM(1)	NUM(2)	NUM(3)	NUM(4)	NUM(5)	LNH	LNO
columns	11-20	21-30	31-40	41-50	51-60	61-70	71-80
format	I10	I10	I10	I10	I10	I10	I10

NUM(1) number of basis species (OH⁻ must be included in the count if the dissociation of water is to be incorporated in the model)

NUM(2) number of species (both basis species and complexes) which are sorbed according to an ion exchange mechanism

NUM(3) number of species (both basis species and complexes) which are sorbed according to a surface complexation model

NUM(4) number of aqueous complexes

NUM(5) number of solid precipitates

LNH position of H⁺ in the list of basis species:
0-dissociation of water not included

LNO position of e⁻ in the list of basis species:
0-redox not considered

Card 15: If any of the species are sorbed according to an ion exchange mechanism, then the user must specify the number of equivalents of sites per liter of solution that are available for sorption. This value is obtained from the cation exchange capacity (CEC), usually given in meq/g of solid, by multiplying the CEC by $10^{-3} \rho_s (1 - \phi) / \phi$, where ϕ is the porosity and ρ_s is the solid density (g/cm³). This card should be omitted if none of the species is sorbed according to an ion exchange mechanism.

variable	CECNS
columns	11-20
format	F10.3

CECNS concentration of sites in [equivalents/l solution] available for sorption in ion exchange model

Card 16a,b,c: If any of the species is sorbed according to the surface complexation model, then the user must specify the 3 parameters described below. This set of cards are omitted if none of the species is sorbed according to the surface complexation model.

variable	C1	C2	AREA	SOH
columns	11-20	21-30	41-50	51-60
format	F10.3	F10.3	F10.3	F10.3

C1 capacitance between the surface plane and the beta plane [$\mu\text{F}/\text{L}^2$]

C2 capacitance between the beta plane and the diffuse layer [$\mu\text{F}/\text{L}^2$]

AREA sorption area [L^2/l solution]

SOH concentration of sites in [equivalents/ l solution] available for forming complexes in surface complexation model

Card 16b: surface complexation parameters

variable	CON(1)	CON(2)	CON(3)	CON(4)
columns	11-20	21-30	31-40	41-50
format	F10.3	F10.3	F10.3	F10.3

CON(i) coefficients in function for log of SOH^{2+} dissociation

Card 16b: surface complexation parameters

variable	CON(1)	CON(2)	CON(3)	CON(4)
columns	11-20	21-30	31-40	41-50
format	F10.3	F10.3	F10.3	F10.3

CON(i) coefficient in function for log of SOH dissociation constant

Card 17a-e: This set of cards reads information about the basis species and constants involved in the processes of ion exchange or surface complexation. Card 17a is always read; both Card 17b,c and Card 17c,d are omitted if the basis species is not sorbed ($\text{ISORPI} = \text{ISORPE} = 0$). Card 17b,c are read if the basis species is sorbed according to an ion exchange mechanism ($\text{ISORPI} = 1$); Card 17d-e is read if the basis species is sorbed according to a surface complexation model ($\text{ISORPE} = 1$). GUESSI and GUESSB can all be left blank if the program is to provide the guesses ($\text{IG} = 1$ on Card 2).

Card 17a

variable	DUM	VJ	KCODE	INDEXI	BI	GUESSI
columns	1-10	11-15	16-20	21-25	26-35	36-45
format	A10	F5.2	I5	I5	F10.3	F10.3

Card 17a continued

variable	INDEXB	BC	GUESSB	ISORPI	ISORPE
columns	46-50	51-60	61-70	71-75	76-80
format	I5	F10.3	F10.3	I5	I5

DUM name of the species

VJ charge of the species

KCODE An integer code that assumes location numbers when kinetics or C-13 fractionation is considered. For glass dissolution consideration, the KCODE for species Na^+ , H^+ , K^+ , Ca^+ and Mg^{+2} assumes 1, 2, 3, 4, and 5 respectively. For isotope studies KCODE assumes 32, 31, 33 and 34. For CO_3^{2-} , KI , HCO_3^- and H_2CO_3 respectively.

INDEXI type of initial condition:
 0-the total concentration of the species will be given (including sorbed phase, aqueous phase and precipitate);
 1-only the concentration of the basis species will be given;
 2-the combined concentration of the basis species and the aqueous complexes will be given (if a species can form a precipitate, option 3 must be used instead of option 2 to allow for the inclusion of the solubility product if necessary)
 3-the combined concentration of the basis species, aqueous complexes and precipitates will be given;
 4-the initial concentration will be determined from a charge balance;

BI value of the initial concentration according to the value of INDEXI [moles/l]

GUESSI guess for the initial concentration according to the value of INDEXI [moles/l]

INDEXB takes the same values as INDEXI and describes what type of concentration is being specified at the boundary

BC value of the concentration at the boundary [moles/l] according to the value of INDEXB [moles/l]; if a solid is leaching into the ground water at the inner boundary, the value of BC for the first species making up this solid is the amount of the solid while the value of BC need not be specified for the other species making up the solid

GUESSB guess for the boundary concentration of the basis species [moles/l]; can be left blank if the program is to provide the guess (IG = 1 on Card 2)

ISORPI code to indicate whether the species is sorbed according to an ion exchange mechanism:
 0-is not sorbed; 1-is sorbed

ISORPE code to indicate whether the species is sorbed according to a surface complexation model:
 0-is not sorbed; 1-is sorbed

Card 17b: ion exchange sorption

variable	GUESSI	GUESSB
columns	11-20	21-30
format	F10.3	F10.3

GUESSI guess for the amount of this species which is sorbed initially [moles/1]; can be left blank if the program is to provide the guess (IG = 1 on Card 2)

GUESSB guess for the amount of this species which is sorbed initially at the boundary conditions [moles/1]; can be left blank if the program is to provide the guess (IG = 1 on Card 2)

Card 17c: ion exchange equilibrium parameters

variable	CON(i)	CON(i)	CON(3)	CON(4)
column	11-20	21-30	31-40	41-50
format	F10.3	F10.3	F10.3	F10.3

CON(i) coefficients in function for log of equilibrium constant

Card 17d: surface complexation

variable	GUESSI	GUESSB	AH
columns	11-20	21-30	31-40
format	F10.3	F10.3	10.3

GUESSI guess for the amount of this species which is sorbed initially [moles/1]; can be left blank if the program is to provide the guess (IB = 1 on Card 2)

GUESSB guess for the amount of this species which is sorbed initially at the inner boundary; [moles/1] can be left blank if the program is to provide the guess (IB = 1 on Card 2)

AH amount of charge which is displaced or sorbed for each surface complexation reaction with a SOH site:
 +1-a H⁺ ion is displaced,
 0-used for the H⁺ ion,

-1-a H⁺ ion is sorbed

Card 17e: surface complexation equilibrium parameters

variable	CON(1)	CON(2)	CON(3)	CON(4)
column	11-20	21-30	31-40	41-50
format	F10.3	F10.3	F10.3	F10.3

CON(i) coefficients in function for log of equilibrium constant

Cards 18a,b: These two cards are omitted if water dissociation is not included in the simulation (LNH = 0 on Card 14). If water dissociation is allowed, information about OH must be read immediately after all of the information about the basis species has been read. OH must be included in the number of basis species (see NUM(1)) read on Card 14. If Card 18 is used, Card 18 must be included.

Card 18a

variable	DUM	H2OC(1)	H2OC(2)	H2OC(3)	H2OC(4)
columns	1-10	11-20	21-30	31-40	41-50
format	A10	F10.3	F10.3	F10.3	F10.3

DUM name of the species

H2OC(i) coefficients in function for log of dissociation constant of water

Card 18b

variable	GUESSI	GUESSB
columns	11-20	21-30
format	F10.3	F10.3

GUESSI guess for the amount of this species which is sorbed initially [moles/l]; can be left blank if the program is to provide the guess (IG = 1 on Card 2)

GUESSB guess for the amount of this species which is sorbed initially at the boundary [moles/l]; can be left blank if the program is to provide the guess (IG = 1 on Card 2)

Cards 19a-g: These seven cards are omitted if NUM(4) = 0 on Card 14, that is, if no aqueous complexes form. If the aqueous complex is sorbed according to an ion exchange mechanism, then Cards 19a-e are read; if the complex is sorbed according to a surface complexation reaction, then Cards 19a-c and f,g are read. If the complex is not sorbed, then only Cards 19a-c are read.

Card 19a

variable	DUM	KCODE	S(J), J = 1, NUM(1)	
columns	1-10	11-20	21-70,/,1-75	
format	A10	I10.3	10F5.1,/,15F5.1	

DUM name of the complex

KCODE integer code used in kinetic options. For details see information about the basis species given above

S array which holds the stoichiometric coefficients for the reaction, read in the same order in which the basis species are read

Card 19b: complexation equilibrium constant parameters

variable	CON(1)	CON(2)	CON(3)	CON(4)
column	11-20	21-30	31-40	41-50
format	F10.3	F10.3	F10.3	F10.3

CON(i) coefficients in function for log of formation of the complex

Card 19c

variable	GUESSI	GUESSB	ISORPI	ISORPE
columns	11-20	21-30	31-35	36-40
format	F10.3	F10.3	I5	I5

GUESSI guess for the initial concentration of this complex [moles/l]; can be left blank if the program is to provide the guess (IG = 1 on Card 2)

GUESSB guess for the concentration of this complex at the boundary [moles/l]; can be left blank if the program is to provide the guess (IG = 1 on Card 2)

ISORPI code to indicate whether the complex is sorbed according to an ion exchange mechanism:

0-is not sorbed; 1-is sorbed

ISORPE code to indicate whether the complex is sorbed according to a surface complexation model:
0-is not sorbed; 1-is sorbed

Card 19d: ion exchange

variable	GUESSI	GUESSB
columns	11-20	21-31
format	F10.3	F10.3

GUESSI guess for the amount of this complex which is sorbed initially [moles/1]; can be left blank if the program is to provide the guess (IG = 1 on Card 2)

GUESSB guess for the amount of the complex which is sorbed at the boundary conditions [moles/1]; can be left blank if the program is to provide the guess (IG = 1 on Card 2)

Card 19e: ion exchange equilibrium parameters

variable	CON(1)	CON(2)	CON(3)	CON(4)
column	11-20	21-30	31-40	41-50
format	F10.3	F10.3	F10.3	F10.3

CON(i) coefficients in function for log of thermodynamic equilibrium constant

Card 19f: surface complexation parameters

variable	GUESSI	GUESSB	AH
columns	11-20	21-30	31-40
format	F10.3	I10.3	F10.3

GUESSI guess for the amount of this complex which is sorbed initially [moles/1]; can be left blank if the program is to provide the guess (IG = 1 on Card 2)

GUESSB guess for the amount of this complex which is sorbed at the boundary [moles/1]; can be left blank if the program is to provide the guess (IG = 1 on Card 2)

AH amount of charge which is displaced or sorbed for each surface complexation reaction with a SOH site:
+1-a H⁺ ion is displaced,
0-used for the H⁺ ion,

-1-a H⁺ ion is sorbed

Card 19g: surface complexation equilibrium parameters

variable	CON(1)	CON(2)	CON(3)	CON(4)
column	11-20	21-30	31-40	41-50
format	F10.3	F10.3	F10.3	F10.3

CON(i) constants in function for log of thermodynamic surface exchange constant

Cards 20a,b,c: These three cards are omitted if NUM(5) = 0 on Card 14, that is if no precipitates form. The concentration units for the precipitate are in equivalent moles/l of solution.

Card 19a

variable	DUM	KCODE	SS(J), J = 1, NUM(1)
columns	1-10	11-20	21-70,/,1-75
format	A10	I10.3	10F5.1,/,15F5.1

DUM name of the precipitate

SS array which holds the stoichiometric coefficients for the reaction, read in the same order in which the basis species are read

KCODE integer code that assumes the rank of the solid in the list of species as they appear in the input

Card 20b: solubility product parameters

variable	CON(1)	CON(2)	CON(3)	CON(4)
column	11-20	21-30	31-40	41-50
format	F10.3	F10.3	F10.3	F10.3

CON(i) coefficients in function for log of solubility product

Card 20c

variable	GUESSI	GUESSB
columns	11-20	21-30
format	F10.3	F10.3

GUESSI guess for the initial concentration of this precipitate
[moles/l]; can be left blank if the program is to provide the guess (IG = 1 on Card 2)

GUESSI guess for the concentration of this precipitate at the
boundary [moles/l]; can be left blank if the program is to provide the guess (IG = 1 on Card 2)

APPENDIX 12

FORTRAN IV LISTING OF CHMTRNS

c
c *****
c CHMTRNS CODE
c (CHEMICAL TRANSPORT NUMERICAL SIMULATOR)
c *****
c This version of the CHEMTRN code(originally developed by C. W. Miller
c and L. V. Benson, 1983) called CHMTRNS includes kinetic dissolution/
c precipitation, redox, temprature variation, and C-13 fractionation
c options.
c
c Authors Noorishad, J., Carnahan, C. L.
c earth sciences division
c lawrence berkeley lab
c berkeley, ca 94720
c and
c Benson, L. V
c U.S. Geological Survey
c Denver, Colorado
c
c Description CHMTRNS simulates solute transport for steady one-dim.
c fluid flow by convection and diffusion/dispersion in a
c saturated porous medium based on the assumption of loca
c chemical equilibrium*. the chemical interactions includ
c in the model are aqueous-phase complexation, solid-phas
c ion exchange of bare ions and complexes, solid-phase
c sorption of bare ions and complexes using the surface
c complexation model, and precipitation/dissolution of
c solids.
c * The code is also capable of handling kinetic
c * dissolution/precipitation for Calcite and Silica and
c * kinetic dissolution for Glass. Also, options for redox
c * and C-13 fractionation as well as non-isothermal
c * conditions are included .
c
c solution procedure for chemical transport the finite differnce
c approaximation along with Newton-Raphson
c method is used. for the heat transport a
c direct LU solution of the crank-Nicholson
c approaximation is employed.
c
c
c
c
c description of input variables
c
c title = title of run up to 80 characters
c
c ulength = unit of length used in the problem
c utime = unit of time used in the problem
c
c itype = 0 if one-dimensional flow is modelled
c = 1 if radial flow is modelled
c idynam = 0 static distribution of species calculated
c = 1 dynamic transport calculation
c ig = 0 user provides the initial guesses
c ipart # 0 C-13 fractionation considered
c gascon = gas constant
c farcon = Faradays constant
c = 1 program provides the initial guesses
c nsrt = 0 if kinetic option is not used

chmtrns.2
chmtrns.3
chmtrns.4
chmtrns.5
chmtrns.6
chmtrns.7
chmtrns.8
chmtrns.9
chmtrns.10
chmtrns.11
chmtrns.12
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chmtrns.58
chmtrns.59
chmtrns.60
chmtrns.61

c	hcm	=	heat capacity of solid per unit volume of	chmtrns.122
c			porous medium	chmtrns.123
c	tcm	=	thermal conductivity of saturated porous medium	chmtrns.124
c				chmtrns.125
c	lnh	=	the position of the H+ ion in basis species list	chmtrns.126
c			0, when water dissociatin is not considered	chmtrns.127
c	lno	=	the place of e- in the list of basis elements	chmtrns.128
c				chmtrns.129
c				chmtrns.130
c	leach	=	position in the list of precipitates of the solid wh	chmtrns.131
c			has been put in contact with the groundwater. the eq	chmtrns.132
c			condition used is that the total concentration of thi	chmtrns.133
c			precipitate is given and that the species making up t	chmtrns.134
c			precipitate are entering the groundwater equivalent t	chmtrns.135
c			stoichiometric coefficients; equals 0 it no leaching	chmtrns.136
c	nb	=	the number of the node where the solid was placed in c	chmtrns.137
c			with the groundwater. in this version it must be at n	chmtrns.138
c			if no solid is put in contact with the groundwater, nb	chmtrns.139
c				chmtrns.140
c	num(1)	=	number of basis species (must include hydroxyl ion i	chmtrns.141
c			dissociation is included)	chmtrns.142
c	num(2)	=	number of cations and complexes sorbed by ion exchan	chmtrns.143
c	num(3)	=	number of ions and complexes sorbed by surface compl	chmtrns.144
c			model (value is increased by 2 in program to allow f	chmtrns.145
c			inclusion of negatively charged surface site and pos	chmtrns.146
c			charged surface site)	chmtrns.147
c	num(4)	=	number of aqueous complexes	chmtrns.148
c	num(5)	=	number of precipitates that could form	chmtrns.149
c				chmtrns.150
c	cecns	=	concentration of sites available for sorption in ion	chmtrns.151
c			model; expressed in equivalents/liter solution	chmtrns.152
c				chmtrns.153
c	c1	=	capacitance between the surface plane and the beta plan	chmtrns.154
c			surface complexation model (microfarads/length2)	chmtrns.155
c	c2	=	capacitance between the beta plane and the diffuse laye	chmtrns.156
c			complexation model (microfarads/length2)	chmtrns.157
c	area	=	area of sites for sorption in surface complexation in	chmtrns.158
c			length2/liter solution	chmtrns.159
c	soh	=	concentration of sites for forming complexes in surfac	chmtrns.160
c			complexation model; in equivalents/liter solution	chmtrns.161
c				chmtrns.162
c	dum	=	array containing the names of the basis species, compl	chmtrns.163
c			the precipitates	chmtrns.164
c	vj	=	array containing ion valences and complex valences; the	chmtrns.165
c			valances are computed from the valences of the basis spec	chmtrns.166
c	kcode(j)	=	code for the rate generation of basis species	chmtrns.167
c			used presently for Glass dissociation option	chmtrns.168
c	con(i,j)	=	parameters of the thermodynamic constants in	chmtrns.169
c			mass action equations	chmtrns.170
c	h2oc(i)	=	parameters of the thermodynamic constants for	chmtrns.171
c			water dissociation	chmtrns.172
c	indexi	=	array giving type of initial conditions used for	chmtrns.173
c			each particular species	chmtrns.174
c			value of 0 means total concentration is specified	chmtrns.175
c			value of 1 means basis species concentration is give	chmtrns.176
c			value of 2 means total aqueous concentration is	chmtrns.177
c			given excluding any precipitates (however, if a spec	chmtrns.178
c			form a precipitate, the value of 3 should be used in	chmtrns.179
c			2 to allow for the inclusion of the solubility produ	chmtrns.180
c			necessary);	chmtrns.181

```

c          value of 3 means total aqueous concentration plus      chmtrns.182
c          any precipitates is given                               chmtrns.183
c          value of 4 means that the concentration of this        chmtrns.184
c          species comes from a charge balance                     chmtrns.185
c          bi = array of initial conditions                        chmtrns.186
c          guessi = guess of equilibrated initial conditions      chmtrns.187
c                   for all the species                          chmtrns.188
c          indexb = array giving type of conditions used to determine chmtrns.189
c                   boundary or influx conditions; values of 0 to 4 are chmtrns.190
c                   same as given in indexi above                chmtrns.191
c          bc = array of boundary conditions                       chmtrns.192
c          guessb = guess of equilibrated boundary or influx conditions chmtrns.193
c                   for all the species                          chmtrns.194
c          isorpi = array containing information about whether the basi chmtrns.195
c                   or the complex sorbs via ion exchange;      chmtrns.196
c                   0 - no sorption                              chmtrns.197
c                   1 - sorption                                 chmtrns.198
c          isorpe = array containing information about whether the basi chmtrns.199
c                   or complex sorbs via surface complexation  chmtrns.200
c                   0 - no sorption                              chmtrns.201
c                   1 - sorption                                 chmtrns.202
c          mass action equations describing sorption via ion exch chmtrns.203
c          pke = array containing negative log of the equilibrium const chmtrns.204
c                   mass action equations describing sorption via surface chmtrns.205
c                   chmtrns.206
c          s(j,i) = the stoichiometric coefficients for the aqueous chmtrns.207
c                   phase complexes; given for 1 mole of the complex and chmtrns.208
c                   same order as the basis species are given   chmtrns.209
c                   chmtrns.210
c                   chmtrns.211
c          h2ok = negative log of the dissociation of water       chmtrns.212
c                   chmtrns.213
c          ss(j,i) = stoichiometric coefficients for precipitates; given chmtrns.214
c                   same order as the list of the basis species chmtrns.215
c                   chmtrns.216
c          ah(i) = number of h ions released or taken up by the surfa chmtrns.217
c                   in surface complexation model               chmtrns.218
c                   +1 - if h+ ion is released                  chmtrns.219
c                   0 - special case for h+ ion                 chmtrns.220
c                   -1 - if h+ ion is sorbed                    chmtrns.221
c                   chmtrns.222
c          description of other important variables used in the program chmtrns.223
c                   chmtrns.224
c                   chmtrns.225
c          cdat(i) = array containing pk of needed equilib. constants chmtrns.226
c                   for calculation of reaction constants of the rate chmtrns.227
c                   equation and some other needed data        chmtrns.228
c          inx1(j),inx2(j) = array designating the binary components chmtrns.229
c                   of each term of the rate equation          chmtrns.230
c          reactsk(i,j,n) = array containing reaction constants    chmtrns.231
c                   in the rate equation                        chmtrns.232
c          cn(j) = array containing all the unknown species. the order i chmtrns.233
c                   those in node 1, then those in node 2, etc. the order chmtrns.234
c                   at each node is first the basis species (the last bas chmtrns.235
c                   is always oh if water dissociation is included), then chmtrns.236
c                   basis species and complexes via simple ion exchange, chmtrns.237
c                   basis species and complexes via surface complexation, chmtrns.238
c                   and the last are the precipitates.         chmtrns.239
c          co(j) = array containing all the old values of the species in chmtrns.240
c                   order as listed for cn(j)                   chmtrns.241

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c      r(i,n) = residues from the equations are stored here. n is t chmtrns.242
c      i is the number of the equation. the order of the e chmtrns.243
c      at each node is (1)transport equations, (2)the site chmtrns.244
c      (3)mass action equations for sorption via ion exchan chmtrns.245
c      (4) site constraint for sorption via surface complex chmtrns.246
c      action equations for surface complexation, (6) mass chmtrns.247
c      for formation of complexes in the aqueous phase, and chmtrns.248
c      products chmtrns.249
c      ac(i,n) = activities of the basis species and complexes in t chmtrns.250
c      phase are stored here chmtrns.251
c      equconst(j,n) array containing the equilibrium constants chmtrns.252
c      first for sorbed species via ion exchange, chmtrns.253
c      then for species sorbed via surface complexation chmtrns.254
c      then for aqueous phase complexation, chmtrns.255
c      then solubility products chmtrns.256
c      a(i,j,n) = the diagonal matrix of the block tridiagonal jacob chmtrns.257
c      it is change in residue divided by the change in c chmtrns.258
c      at the node n chmtrns.259
c      b(i,j,n) = off diagonal matrix of the block tridiagonal jacob chmtrns.260
c      c(i,j,n) = off diagonal matrix of the block tridiagonal jacob chmtrns.261
c
c      dimension cn(3000),co(3000),dum(20),title(20),pki(30),pke(30) chmtrns.262
c      dimension cm(25),wconst(25),bi(25),bc(25),tprint(25),num(20), chmtrns.263
c      1index1(10),index2(25),indexb(25),cmax(25),ibnd(2),bc2(25), chmtrns.264
c      2iip(3000),guessi(30),guessb(30),indexi(25),com(100),ibndt(2) chmtrns.265
c      dimension tmp(100),tmpold(100),eh(100) chmtrns.266
c      common/ab/vj(75),ac(75,100),eqconst(25,100),h2ok(100),alfa(4,100), /ab/.2
c      1s(25,25),ss(25,25),ah(25),h2oc(8),con(25,8),conk(20,8),comp(4,2), /ab/.3
c      2 ilbli(25),ilble(25),q(10,100) /ab/.4
c      common/edl/c1,c2,area,soh /edl/.2
c      common/edl2/sigo,sigb,sigd,psio,psibeta,psid /edl2/.2
c      common/nj/isorpi(30),isorpe(30),iion,ieion /nj/.2
c      common/ad/x(200),delt,doa,dob,vo,cecns /ad/.2
c      common/const/rel,absv /const/.2
c      common/lcm/a(25,25,100),b(25,25,100) /lcm/.2
c      common/lcm1/r(25,100) /lcm1/.2
c      common/lcm2/c(25,25,100) /lcm2/.2
c      common/oxred/lno,lnh /oxred/.2
c      common/spec/leach1(5),nb,pini(5) /spec/.2
c      common/crate/rate(50),kcode(25),inx1(5,25),inx2(5,25),cdat(5,25), /crate/.2
c      1 reactsk(5,10,100),nsrt(5),sarea(5),nparam(5),xkinet(5),xmax,time, /crate/.3
c      2 gc,excode,tpcode,kinr,xdiag(5),shift(4,100),shftsol(100) /crate/.4
c
c      data redox/5Hredox/ chmtrns.280
c      data xtemp/5Htempx/ chmtrns.281
c      data xkinet/5Hdiss,5Hexkin,5Htpkin,5Hprepc,5Hpreps/ chmtrns.282
c      data blank/5Hblank/ chmtrns.283
c      data rel/1.e-02/,absv/1.e-12/ chmtrns.284
c      call link(" unit5=(input,open,text),read5,unit6=(output,create,hc) chmtrns.285
c      x,print6 //" ) chmtrns.286
c      chmtrns.287
c      chmtrns.288
c      chmtrns.289
c      chmtrns.290
c      mdim=25 chmtrns.291
c      ipart=0 chmtrns.292
c      kinr=0 chmtrns.293
c      ktsum=0 chmtrns.294
c      oxcde=0.0 chmtrns.295
c      tpcde=0.0 chmtrns.296
c      excde=0.0 chmtrns.297
c      *****

```



```

c read in input parameters
c *****
  read(5,1000) title
  write(6,999) title
  read 1010, ulength, utime
  write (6,1011) ulength, utime
  read 910, itype, idynam, ig, ipart
  read 910, in1, in2, in3
c read parameters of the numerical calculations
  read 918, climit, errsqr, iterj, iterm, iterd, dtmult, ndiv
  read 920, nmax, xmax, gc, rw
  read 920, kmax, dtini, dtmax
  read 900, (tprint(k), k=1, kmax)
  read 900, doa, dob, vo
  read 910, ibnd(1), ibnd(2)
  read 910, ibndt(1), ibndt(2)
  read 910, itemp
  if(itemp.eq.0) read 900, temp
  if(itemp.eq.1) read 900, temp, tempi, hcw, hcm, tcm
  if(itemp.eq.2) read 900, tempi, tempo
  read 910, leach, nb
c kinetic rate information
  1 read 510, word
  if(word.eq.redox) go to 9
  if( word.eq.xkinet(2) ) go to 11
  if( word.eq.xkinet(3) ) go to 12
  if( word.eq.blank ) go to 3
c
  9 write(6,3000)
  oxcde=1.0
  go to 13
  11 write(6,3200)
  excde=1.0
  go to 2
  12 write(6,3300)
  tpcde=1.0
  go to 2
c read redox constants R and F
  13 read 900, gascon, farcon
  go to 1
c
c read binary components of the rate equations and constants
c Here, the order for the solids with reversible reactions must
c be the same as those in the input list. Also, parameters for
c the Glass dissolution option are the last ones to be read.
c The position of H+ in the list of species must be number 2 if
c Glass dissolution option is invoked.
  2 kinr=kinr+1
  i=kinr
  read 915, nparam(i), sarea(i), nsrt(i), xdiag(i)
  if(nparam(i).ne.0) read 916, (cdat(i,j), j=1, nparam(i))
  if(nsrt(i).eq.0) go to 1
  read 917, (inx1(i,j), inx2(i,j), j=1, nsrt(i) )
  do 14 j=1, nsrt(i)
  l=j+ktsum
  read 900, (conk(l,k), k=1,4)
  14 continue
  ktsum=ktsum+nsrt(i)
c
c go to 1

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chmtrns.356
chmtrns.357

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c      3 continue
c      read C-13 partition parameters
      if(ipart.eq.0.0) go to 65
      read 900, shiftr, shifts
      do 66 j=1,4
      read 900, (comp(j,k), k=1,2)
66 continue
65 continue
      read 910, (num(i),i=1,5), lnh, lno
      num(10)=num(1)+num(4)
      num(11)=num(10)+num(5)
      if (num(2).eq.0) cecns=0.
      if (num(2).gt.0) read 900, cecns
      if (num(3).eq.0) soh=0.
      if (num(3).eq.0) go to 5
      read 900, c1, c2, area, soh
c      read exchange surface site dissociation information
c      to be used for aqueous species surface complexation
      read 900, ( con((num(2)+1),j), j=1,4 )
      read 900, ( con((num(2)+2),j), j=1,4 )
      num(3)=num(3)+2
      dum(num(11)+1)=2hso
      dum(num(11)+2)=4hsoh2
      ilble(1)=num(11)+1
      ilble(2)=num(11)+2
      5 continue
      num(6)=num(1)+num(2)
      num(7)=num(6)+num(3)
      num(8)=num(7)+num(4)
      num(9)=num(8)+num(5)
      num(12)=num(2)+num(3)
      num(14)=nmax
      num(15)=num(12)+num(4)+num(5)
      ntotp=num(9)
      leach1(1)=leach
      if (leach1(1).ne.0) go to 7
c
      do 6 i=2,5
c      6 leach1(i)=0
c
      7 if (lnh.eq.0) go to 8
      s0=0
      s1=1
      8 continue
c *****
c write out some of the constants used
c *****
      if ((ibnd(1).eq.0).and.(ibnd(2).eq.1)) write(6,2060)
      if ((ibnd(1).eq.1).and.(ibnd(2).eq.1)) write(6,2061)
      if ((ibnd(1).eq.0).and.(ibnd(2).eq.0)) write(6,2062)
      if ((ibnd(1).eq.1).and.(ibnd(2).eq.0)) write(6,2063)
      if (itype.eq.0) write(6,600) doa,dob,vo,nmax
      if (itype.eq.1) write(6,601) doa,dob,vo,nmax
      write(6,610) kmax,(tprint(i),i=1,kmax)
      write(6,612) climt,errsqr,iterj,iterm,iterd,dtmult,ndiv
      write(6,611) cecns,soh
      if(itemp.eq.0) write (6,2065) temp
      if(itemp.eq.1) write (6,2067) temp,hcw,hcm,tcn
      if((itemp.eq.1).and.(ibndt(1).eq.0)) write (6,2068) tempi
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      chmtrns.416
      chmtrns.417

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      if((itemp.eq.1).and.(ibndt(1).eq.1)) write (6,2069) tempi           chmtrns.418
      if(itemp.eq.2) write (6,2070) tempi,tempo                          chmtrns.419
      if(itemp.eq.1) write (6,2073)                                     chmtrns.420
      ii=0                                                            chmtrns.421
      ie=3                                                            chmtrns.422
      li=0                                                            chmtrns.423
      lb=0                                                            chmtrns.424
c *****                                                            chmtrns.425
c read in information on bare ions and type of sorption                chmtrns.426
c *****                                                            chmtrns.427
c Note:if Glass dissolution option is activated use 1,2,3,4, and 5    chmtrns.428
c     for kcode(j) of Na, H, K, Ca, and Mg, respectively, regardless chmtrns.429
c     of the order of appearance of these species in the input list  chmtrns.430
c     H+ must be at position number 2 in the input for Glass option.  chmtrns.431
c     Also, if C-13 partition is included use 31 and 32 for kcode(j)  chmtrns.432
c     of CO3 and neg.KI respectively.                                  chmtrns.433
c     m1=num(1)                                                       chmtrns.434
c     nspecm=num(1)                                                   chmtrns.435
c     if (lnh.gt.0) nspecm=num(1)-1                                   chmtrns.436
c                                                                 chmtrns.437
c     do 17 j=1,nspecm                                               chmtrns.438
c     read 950, dum(j),vj(j),kcode(j),indexi(j),bi(j),guessi(j),    chmtrns.439
1  indexb(j),bc(j),guessb(j),isorpi(j),isorpe(j)                    chmtrns.440
c     if (indexi(j).eq.4) li=j                                        chmtrns.441
c     if (indexb(j).eq.4) lb=j                                        chmtrns.442
c                                                                 chmtrns.443
c if the species is sorbed via ion exchange, read in equilibrium consta chmtrns.444
c and guesses if they are being provided                               chmtrns.445
c                                                                 chmtrns.446
c     if (isorpi(j).eq.0) go to 15                                    chmtrns.447
c     ii=ii+1                                                         chmtrns.448
c     ilbli(ii)=j                                                    chmtrns.449
c     k=ii+num(1)                                                    chmtrns.450
c     read 960, guessi(k),guessb(k)                                   chmtrns.451
c     read 900, (con(ii,ji), ji=1,4)                                 chmtrns.452
c                                                                 chmtrns.453
c if the species is sorbed via surface complexation, read in equilibriu chmtrns.454
c constant and number of h ions sorbed or released from the surface, an chmtrns.455
c guesses if being provided                                          chmtrns.456
c                                                                 chmtrns.457
c 15 if (isorpe(j).eq.0) go to 17                                    chmtrns.458
c     if (j.eq.lnh) iej=3                                            chmtrns.459
c     if (j.eq.lnh) go to 16                                         chmtrns.460
c     ie=ie+1                                                         chmtrns.461
c     iej=ie                                                           chmtrns.462
c 16 continue                                                       chmtrns.463
c     ilble(iej)=j                                                  chmtrns.464
c     k=iej+num(6)                                                  chmtrns.465
c     read 960, guessi(k),guessb(k),ah(iej)                          chmtrns.466
c     iejn=num(2)+iej                                               chmtrns.467
c     read 900, (con(iejn,ji), ji=1,4)                               chmtrns.468
c 17 continue                                                       chmtrns.469
c                                                                 chmtrns.470
c *****                                                            chmtrns.471
c write out the conditons on the basis species                       chmtrns.472
c *****                                                            chmtrns.473
c     iie=ie-2                                                       chmtrns.474
c     if (num(3).eq.0) iie=0                                         chmtrns.475
c     write (6,800) nspecm,ii,iie                                    chmtrns.476
c     iion=ii                                                        chmtrns.477

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        ieion=ie
        ii=0
        ie=3
c
    do 20 j=1,nspecm
        if (isorpi(j).eq.1) ii=ii+1
        if (j.eq.lnh.and.isorpe(j).eq.1) iek=3
        if (j.eq.lnh.and.isorpe(j).eq.1) go to 19
        if (isorpe(j).eq.1) ie=ie+1
        iek=ie
19 continue
    write(6,805) dum(j),vj(j),kcode(j),indexi(j),bi(j),indexb(j),bc(j)
20 continue
c
    ncmplx=num(4)
c *****
c if water dissociation is considered, need to read and write out
c information about the oh ion
c *****
    if (lnh.eq.0) go to 21
    read 974, dum(num(1)),(h2oc(j), j=1,4)
    vj(num(1))=-1.0
    indexi(num(1))=1
    indexb(num(1))=1
    read 980,guessi(num(1)),guessb(num(1))
    isorpi(num(1))=0
    isorpe(num(1))=0
    ncmplx=num(4)+1
    bi(num(1))=guessi(num(1))
    bc(num(1))=guessb(num(1))
21 if (num(4).eq.0) go to 35
c *****
c read in information on complexes and type of sorption
c *****
c NOTE: If C-13 fractionation is included use 33 and 34 for
c KCODE(knu) HCO3- and H2CO3 respectively.
c m4=num(4)
c
    do 27 i=1,m4
        kk=i+num(1)
        knu=num(7)+i
        read 972, dum(kk), kcode(knu), (s(j,i),j=1,m1)
        in=num(12)+i
        read 900, (con(in,j), j=1,4)
        vj(kk)=0.
        do 22 j=1,m1
22 vj(kk)= vj(kk)+(s(j,i)*vj(j))
        ic=kk+num(12)
        read 980, guessi(ic),guessb(ic),isorpi(kk),isorpe(kk)
c
c if complex is sorbed via ion exchange need to read in equilibrium con
c
    if (isorpi(kk).eq.0) go to 25
    ii=ii+1
    k=ii+num(1)
    read 960, guessi(k),guessb(k)
    ilble(ii)=ic
    read 900, (con(ii,j), j=1,4)
c
c if complex is sorbed via surface complexation need to read in equilib

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chmtrns.537

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c constant and number of h ions sorbed or released by the surface
c
25 if (isorpe(kk).eq.0) go to 27
   ie=ie+1
   ilble(ie)=ic
   k=ie+num(6)
   read 960, guessi(k),guessb(k),ah(ie)
   ien=num(2)+ie
   read 900, (con(ien,j), j=1,4)
27 continue
c
c write out information about the complexes
c
   icmplx=ii-iion
   iecmplx=ie-ieion
   write (6,802) ncmplx,icmplx,iecmplx
   if (ii.ne.num(2)) write (6,990) ii,num(2),ie,num(3)
   ii=iion
   ie=ieion
   if(lnh.gt.0) kcode(num(1))=0
   if(lnh.gt.0) write(6,820) dum(num(1)),vj(num(1)),kcode(num(1)),
1 (s0, j=1,nspecm), s1
c
   do 30 i=1,m4
   if (isorpi(i).eq.1) ii=ii+1
   if (isorpe(i).eq.1) ie=ie+1
   kk=i+num(1)
   inp=num(12)+i
   write(6,820) dum(kk),vj(kk),kcode(kk),(s(j,i),j=1,m1)
30 continue
c
35 continue
c *****
c read in information on precipitates
c *****
   if (num(5).eq.0) go to 41
   write (6,840) num(5)
   m5=num(5)
c
   do 40 i=1,m5
   kk=num(10)+i
   knu=num(8)+i
   kl=kk+num(12)
   read 972,dum(kk),kcode(knu),(ss(j,i),j=1,m1)
   inun=num(12)+num(4)+i
   read 900, (con(inun,j), j=1,4)
   read 960,guessi(kl),guessb(kl)
c
c if a solid is being placed in contact with the initial groundwater
c need to determine the species making up this solid
c
   if (i.ne.leach1(1)) go to 39
   ileach=1
   do 38 j=1,m1
   if (ss(j,i).eq.0) go to 38
   ileach=ileach+1
   leach1(ileach)=j
38 continue
c *****

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chmtrns.538
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chmtrns.596
chmtrns.597

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<pre> c write out information about the precipitates c ***** 39 write(6,971) dum(kk),kcode(knu), 1 (ss(j,i),j=1,m1) 40 continue 41 continue m15=num(15) delt=dtini ntot=num(8) neq=num(9)*nmax c ***** c write out kinetic rate information,and other related data c ***** if(kinr.eq.0) go to 43 ktsum=0 do 42 i=1,kinr if(xdiag(i).eq.xkinet(4)) write(6,901) if(xdiag(i).eq.xkinet(5)) write(6,902) if(xdiag(i).eq.xkinet(1)) write(6,903) print 976, nsrt(i),nparam(i),sarea(i),xdiag(i) if(nparam(i).ne.0) print 977, (cdat(i,j),j=1,nparam(i)) if(nsrt(i).eq.0) go to 42 print 919, (inx1(i,j),inx2(i,j),j=1,nsrt(i)) write(6,905) do 44 j=1,nsrt(i) l=j+ktsum print 900, (conk(l,k), k=1,4) 44 continue ktsum=ktsum+nsrt(i) 42 continue 43 continue c ***** c print of C-13 partition parameters c ***** if(ipart.eq.0) go to 68 write(6,615) write(6,616) shiftr,shifts write(6,905) do 67 j=1,4 print 900, (conp(j,k), k=1,2) 67 continue 68 continue c ***** c write out redox constants c ***** if(oxcode.eq.1.0) print 978, gascon, farcon c ***** c set up grid c ***** call setup(xmax,nmax,itype,gc,rw) index=0 c ***** c equilibrate initial conditions c ***** c c assign initial temp. to nodes c if(itemp.lt.2) go to 48 call gradt(nmax,tempi,tempo,itype,x,tmp) </pre>	<pre> chmtrns.598 chmtrns.599 chmtrns.600 chmtrns.601 chmtrns.602 chmtrns.603 chmtrns.604 chmtrns.605 chmtrns.606 chmtrns.607 chmtrns.608 chmtrns.609 chmtrns.610 chmtrns.611 chmtrns.612 chmtrns.613 chmtrns.614 chmtrns.615 chmtrns.616 chmtrns.617 chmtrns.618 chmtrns.619 chmtrns.620 chmtrns.621 chmtrns.622 chmtrns.623 chmtrns.624 chmtrns.625 chmtrns.626 chmtrns.627 chmtrns.628 chmtrns.629 chmtrns.630 chmtrns.631 chmtrns.632 chmtrns.633 chmtrns.634 chmtrns.635 chmtrns.636 chmtrns.637 chmtrns.638 chmtrns.639 chmtrns.640 chmtrns.641 chmtrns.642 chmtrns.643 chmtrns.644 chmtrns.645 chmtrns.646 chmtrns.647 chmtrns.648 chmtrns.649 chmtrns.650 chmtrns.651 chmtrns.652 chmtrns.653 chmtrns.654 chmtrns.655 chmtrns.656 chmtrns.657 </pre>
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go to 47
46 do 45 n=1,nmax
45 tmp(n)=temp
   if(itemp.eq.1) tmp(1)=temp1
   if(itemp.eq.0) tb=temp
   if(itemp.eq.1) tb=temp1
47 continue
   n2=2
   if(itemp.eq.2) n2=nmax
   call eqcon(1,n2,con,conk,h2oc,m15,kinr,lnh,tmp,h2ok,eqconst,
1      nsrt,reactsk,alfa,conp,ipart,0 )
   m9=num(9)
c
c determine here whether the program or the user is
c providing the first guesses
c
   do 165 n=2,n2
   if(ig.eq.1) call iguess(com,bi,num,n,lnh)
   do 50 j=1,m9
   ac(j,n)=1.0
   if(ig.eq.1) cm(j)=com(j)
   if(ig.eq.1) go to 50
   cm(j)=guessi(j)
50 continue
   if((num(3).eq.0).or.(ig.eq.1)) go to 51
   nn2=num(2)+2
   nn1=num(2)+1
   cm(num(6)+1)=eqconst(nn2,n)*soh/cm(lnh)
   cm(num(6)+2)=cm(lnh)*soh/eqconst(nn1,n)
   cm(num(6)+2)=cm(num(6)+2)/10.
51 continue
c
   ctot=0.
c *****
c determine the equilibrium concentrations for the initial conditions
c *****
   call eqlib(cm,bi,index1,indexi,num,n,ss,eqconst,ctot,ac,
1      lli,lnh,in1)
c *****
c out initial conditions
   if(n.ne.2) go to 165
   if(n2.eq.nmax) write(6,765) n
   write(6,760) temp
   write(6,780)
   ii=0
   ie=0
   ileach=2
c
c calcualte conventional kd's here, the total amount of the
c species in the aqueous phase
c
   do 80 j=1,m1
   if(cm(j).eq.0.0) cm(j)=1.0e-30
   cmtotaq=cm(j)
   if(isorpi(j).eq.0) sorb=0.
   if(isorpi(j).eq.0) go to 55
   ii=ii+1
   sorb=cm(ii+num(1))
55 continue
   if(isorpe(j).eq.0) sorbe=0.
chmtrns.658
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chmtrns.716
chmtrns.717

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    if (isorpe(j).eq.0) go to 56
    ie=ie+1
    sorbe=cm(ie+num(6)+3)
    if (j.eq.lnh) sorbe=cm(3+num(6))
    if (j.eq.lnh) ie=ie-1
56 continue
    if (num(4).eq.0) go to 61
    do 60 i=1,m4
60 cmtotaq=cmtotaq+s(j,i)*cm(num(7)+i)
    dk= sorb/cmtotaq
    dke=sorbe/cmtotaq
c
c if a solid is going to be placed in contact with the groundwater,
c need to calculate how much of each species that makes up this
c solid already exists in the groundwater
c
61 if (leach1(1).eq.0) go to 79
    if (j.ne.leach1(ileach)) go to 70
    pini(ileach-1)=cmtotaq
    indexb(j)=3
    ileach=ileach+1
70 continue
79 if (indexi(j).eq.4) indexb(j)=2
    if (indexi(j).eq.4) bc(j)=cmtotaq
c
c write out this information
c
80 write (6,700) dum(j),cmtotaq,cm(j),sorb,sorbe,ac(j,2),dk,dke
c
    if (num(4).eq.0) go to 91
    write (6,740)
c
    do 90 i=1,m4
    kk=i+num(1)
    if (isorpi(kk).eq.0) sorb=0.
    if (isorpi(kk).eq.0) go to 85
    ii=ii+1
    sorb=cm(ii+num(1))
85 continue
    if (isorpe(kk).eq.0) sorbe=0.
    if (isorpe(kk).eq.0) go to 86
    ie=ie+1
    sorbe=cm(ie+num(6)+3)
86 continue
    ik=i+num(7)
c
c write out information about the aqueous phase complexes
c
90 write (6,750) dum(kk),vj(kk),cm(ik),sorb,sorbe
c
91 continue
    do 95 j=1,m9
    cn((n-1)*num(9)+j)=cm(j)
95 continue
c
    if (li.ne.0) go to 141
c
c a species at the boundary may be calculated from a charge balance
c therefore it is necessary to know the charge that
c is not being considered in these calculations and which is being

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chmtrns.718
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chmtrns.739
chmtrns.740
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chmtrns.770
chmtrns.771
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chmtrns.774
chmtrns.775
chmtrns.776
chmtrns.777

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c made up by species not participating in the chemical changes
c
c   ctot=0.
c
c   do 130 j=1,m1
130 ctot=cm(j)*vj(j)+ctot
c
c   if (num(4).eq.0) go to 141
c
c   do 140 i=1,m4
140 ctot=ctot+cm(num(7)+i)*vj(num(1)+i)
c
c 141 if (num(5).eq.0) go to 160
c
c   write (6,841)
c
c   do 150 i=1,m5
c   ii=num(10)+i
c   write (6,845) dum(ii),cm(ii+num(12))
c
c if a solid is being placed in contact with the initial groundwater
c need to calculate how much of each particular species in this
c solid was initially in the groundwater; this calculation includes
c the aqueous phase complexes
c
c   if (leach1(1).eq.0) go to 150
c   ileach=2
c
c   do 145 j=1,nspecm
c   if (ss(j,i).eq.0) go to 145
c   if (j.ne.leach1(ileach)) go to 145
c   pini(ileach-1)=pini(ileach-1)+ss(j,i)*cm(num(8)+i)
c   ileach=ileach+1
145 continue
c
c 150 continue
c 160 continue
c
c if a surface complexation model is used for sorption,
c then write out the charges developed at the layers and
c the potentials between these layers
c
c   if (num(3).eq.0) go to 161
c   write (6,597) sigo,sigb,sigd,psio,psibeta,psid
c   write (6,598) cm(num(6)+1),cm(num(6)+2)
161 continue
c   ctot2 = -ctot
c   write (6,596) ctot2
165 continue
c   if(n2.eq.nmax) go to 115
c   do 110 n=1,nmax
c   do 110 j=1,m9
c   cn((n-1)*num(9)+j)=cm(j)
c   ac(j,n)=ac(j,2)
110 continue
c 115 continue
c Note: The subroutine shiftb is only used for calculation of rechar
c water make up, in a pre-processing stage of C-13 partition
c studies. In such run we only consider co2(g), H+ and OH- as
c basis species and H2CO3, HCO3-, and CO3-- as complexes, in

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chmtrns.778
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chmtrns.789
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chmtrns.794
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chmtrns.818
chmtrns.819
chmtrns.820
chmtrns.821
chmtrns.822
chmtrns.823
chmtrns.824
chmtrns.825
chmtrns.826
chmtrns.827
chmtrns.828
chmtrns.829
chmtrns.830
chmtrns.831
chmtrns.832
chmtrns.833
chmtrns.834
chmtrns.835
chmtrns.836
chmtrns.837

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c      this order.
c
c      if(idynam.eq.0.and.ipart.eq.1) call shiftb(cm,num,alfa,shiftr)
c *****
c      equilibrate boundary conditions
c *****
c      decide if the program is supplying the first guesses
c      for the species concentrations
c
c      if(ig.eq.1) call iguess(com,bc,num,n,lnh)
c      do 170 j=1,m9
c      ac(j,1)=1.0
c      if(ig.eq.1) cm(j)=com(j)
c      if(ig.eq.1) go to 170
c      cm(j)=guessb(j)
170 continue
c      if((num(3).eq.0).or.(ig.eq.1)) go to 171
c      nn2=num(2)+2
c      nn1=num(2)+1
c      cm(num(6)+1)=eqconst(nn2,1)*soh/cm(lnh)
c      cm(num(6)+2)=cm(lnh)*soh/eqconst(nn1,1)
c      cm(num(6)+2)=cm(num(6)+2)/1000.
171 continue
c *****
c      determine the equilibrium distribution of species for the boundary
c      or influx conditions
c *****
c      call eqlib(cm,bc,index1,indexb,num,1,ss,eqconst,ctot,ac,
c      1lb,lnh,in2)
c      tbound=tb
c      if(itemp.eq.2) tbound=tmp(1)
c      write(6,790) tbound
c      write(6,780)
c      ii=0
c      ie=0
c      nend=(nmax-1)*num(9)
c *****
c      write out the boundary or influx conditions
c *****
c
c      also calculate conventional kd's, and the total aqueous
c      phase concentration of the species
c
c      do 180 j=1,m1
c      if(ibnd(2).eq.0) bc2(j)=cn(nend+j)
c      if(cm(j).eq.0.0) cm(j)=1.0e-35
c      cmtotaq=cm(j)
c      if(isorpi(j).eq.0) sorb=0.
c      if(isorpi(j).eq.0) go to 172
c      ii=ii+1
c      sorb=cm(ii+num(1))
172 continue
c      if(isorpe(j).eq.0) sorbe=0.
c      if(isorpe(j).eq.0) go to 173
c      ie=ie+1
c      sorbe=cm(ie+num(6)+3)
c      if(j.eq.lnh) sorbe=cm(num(6)+3)
c      if(j.eq.lnh) ie=ie-1
173 continue

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chmtrns.838
chmtrns.839
chmtrns.840
chmtrns.841
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chmtrns.847
chmtrns.848
chmtrns.849
chmtrns.850
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chmtrns.890
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chmtrns.892
chmtrns.893
chmtrns.894
chmtrns.895
chmtrns.896
chmtrns.897

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        if (num(4).eq.0) go to 176
        do 175 i=1,m4
175  cmtotaq=cmtotaq+s(j,i)*cm(num(7)+i)
        dk= sorb/cmtotaq
        dke=sorbe/cmtotaq
176  bbc=cmtotaq
        if (num(5).eq.0) go to 179
        do 177 i=1,m5
        bbc=bbc+ss(j,i)*cm(num(8)+i)
177  continue
c  *****
c  set inner boundary condition
c  *****
c
c  set up the actual boundary conditions for the inner
c  boundary
c
179  if (ibnd(1).eq.0) bc(j)=bbc
        if (ibnd(1).eq.1) bc(j)=vo*cmtotaq
        if((ibnd(1).eq.1).and.(itype.eq.1)) bc(j)=vo*cmtotaq/x(1)
        index2(j)=0
180  write (6,700) dum(j),cmtotaq,cm(j),sorb,sorbe,ac(j,1),dk,dke
c
c  do calculations for the complexes
c
        if (num(4).eq.0) go to 191
        write (6,740)
c
        do 190 i=1,m4
        kk=i+num(1)
        if (isorpi(kk).eq.0) sorb=0.
        if (isorpi(kk).eq.0) go to 192
        ii=ii+1
        sorb=cm(ii+num(1))
192  continue
        if (isorpe(kk).eq.0) sorbe=0
        if (isorpe(kk).eq.0) go to 193
        ie=ie+1
        sorbe=cm(num(6)+ie+3)
193  continue
        ik=i+num(7)
190  write (6,750) dum(kk),vj(kk),cm(ik),sorb,sorbe
c
191  continue
c  *****
c  if flux condition is used, then first grid is the same
c  as the rest of the grids
c  *****
        if(ibndt(1).eq.1) tmp(1)=temp
        if (ibnd(1).eq.1) go to 201
        n=1
c
        do 200 j=1,m9
        cn((n-1)*num(9)+j)=cm(j)
200  continue
c
201  continue
c
c  write out information about the precipitates
c

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chmtrns.898
chmtrns.899
chmtrns.900
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chmtrns.956
chmtrns.957

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        if (num(5).eq.0) go to 210
        write (6,841)
c
        do 205 i=1,m5
        ii=num(10)+i
        write (6,845) dum(ii),cm(ii+num(12))
205 continue
c
210 continue
    ctot1=0.
c
c do a check of the charge balance
c
        do 215 j=1,m1
215 ctot1=cm(j)*vj(j)+ctot1
c
        if (num(4).eq.0) go to 221
c
        do 220 i=1,m4
220 ctot1=ctot1+cm(num(7)+i)*vj(num(1)+i)
c
221 continue
    ctot2 = -ctot1
    write (6,596) ctot2
c
c if surface complexation is used for sorption, write
c out the charges developed at the surfaces and the
c potentials between the surfaces for the boundary conditions
c
        if (num(3).eq.0) go to 231
        write (6,597) sigo,sigb,sigd,psio,psibeta,psid
        write (6,598) cm(num(6)+1),cm(num(6)+2)
231 continue
    time=0.
    kl=1
    delt=dtini
    if (idynam.eq.0) go to 500
c *****
c calculate new values of the concentration as a function of time
c *****
c
c set old values of concentration = to new values
c
        iiij=0
        call second(ts)
235 do 240 n=1,nmax
        tmpold(n)=tmp(n)
        do 240 j=1,m9
240 co((n-1)*num(9)+j)=cn((n-1)*num(9)+j)
c
        time=time+delt
        iiij=iiij+1
        iter3=0
c
c calculate temperatures
c
242 if(iter3.gt.ndiv) go to 500
    if(iiij.eq.1.and.itemp.eq.0) go to 245
    if(itemp.ne.1) go to 250
    call tmpcal(ibndt(1),nmax,hcm,hcw,vo,tcm,doa,ittype,tb,delt,

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chmtrns.958
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chmtrns.1010
chmtrns.1011
chmtrns.1012
chmtrns.1013
chmtrns.1014
chmtrns.1015
chmtrns.1016
chmtrns.1017

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1          x,tmpold,tmp )
245 continue
c
c   calculate equilibrium constants
c
c   call eqcon(1,nmax,con,conk,h2oc,m15,kinr,lnh,tmp,h2ok,eqconst,
1          nsrt,reactsk,alfa,comp,ipart,1)
250 iter=0
   iter2=0
c
c   calculate the residues of the equations for the new guess of
c   concentrations at this time
c
c   call res(cn,co,bc,bc2,r,num,mdim,lnh,ibnd,itpe,0)
c
c   calculate the jacobian
c
260 call jacobi(a,b,c,co,cn,bc,bc2,num,r,mdim,lnh,ibnd,itpe,
1          tpcode,kcode )
c   the subroutines decbt and solbt invert the jacobian
c
263 call decbt(num(9),nmax,mdim,a,b,c,iip,ier)
270 continue
   iter=iter+1
   print 915,iter
   call solbt(num(9),nmax,mdim,a,b,c,r,iip)
c
c   do 280 i=1,m9
280 cmax(i)=0.
c
c *****
c determine the new value of the concentrations from the old values
c and the inversion of the jacobian
c *****
c   do 291 n=1,nmax
c   do 290 j=1,m9
c   cold=cn((n-1)*num(9)+j)
c   cn((n-1)*num(9)+j)=cn((n-1)*num(9)+j)-r(j,n)
c   if(j.eq.lno) eh(n)=-alog10(cn((n-1)*num(9)+j))/( farcon/
1          (2.3*gascon*(tmp(n)+273.15)) )
c   if (cn((n-1)*num(9)+j).lt.0.) cn((n-1)*num(9)+j)=cold/10.
c   npnsne=num(7)+1
c   if((j.gt.num(6)).and.(j.lt.npnsne).and.
1  (cn((n-1)*num(9)+j).gt.soh)) cn((n-1)*num(9)+j)=soh
c   cmax(j)=amax1(cn((n-1)*num(9)+j),cmax(j) )
290 continue
291 continue
c
c *****
c determine if the changes in the concentrations are within the error
c range
c *****
c   err=0.
c
c   do 300 n=1,nmax
c   do 300 i=1,m9
c   aaa=r(i,n)
c   bbb=cmax(i)
c   if(bbb.lt.climit) go to 300
c   aaa=aaa/bbb

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chmtrns.1018
chmtrns.1019
chmtrns.1020
chmtrns.1021
chmtrns.1022
chmtrns.1023
chmtrns.1024
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chmtrns.1074
chmtrns.1075
chmtrns.1076
chmtrns.1077

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err=err + aaa*aaa
300 continue
err=sqrt(err)
c
  if(err.lt.errsqr) go to 310
c *****
c if convergence is not obtained calculate the residues for the next gu
c *****
  call res(cn,co,bc,bc2,r,num,mdim,lnh,ibnd,itpe,0)
  if(iter.lt.iterj) go to 270
301 continue
  iter2=iter2+1
  if(iter2.lt.iterd) go to 260
  iter3=iter3+1
c *****
c if convergence is not obtained within 7 iterations reduce the time st
c *****
  time=time-delt
  delt=delt/2.0
  write (6,2022) delt
  k6=1
c
c set new values equal to old values and start this time step over
c
  do 306 n=1,nmax
  tmp(n)=tmpold(n)
  do 306 j=1,m9
306 cn((n-1)*num(9)+j)=co((n-1)*num(9)+j)
  time=time+delt
  go to 242
c
c convergence is obtained, so start next time step
c
310 continue
  if(ipart.ne.0) call shifc(cn,num,shftsol,shift,shiftr,shifts,
  1 alfa,nmax,kcode )
c *****
c
  call second(te)
  deltc=te-ts
  if( (time-tprint(k1)).ge.0. ) go to 401
  if(iter.lt.iterm) delt=delt*dtmult
  if (delt.gt.dtmx) delt=dtmx
  if(iter.lt.iterm.and.delt.lt.dtmx) write(6,2023) delt,time
  write (6,2024) iter
  go to 235
401 continue
  write(6,2080) deltc
  if(iter.lt.iterm.and.delt.lt.dtmx) write(6,2023) delt,time
c *****
c write out the species concentrations
c *****
  k1=k1+1
  write (6,530) time,delt
  npri=nmax/9
  i1=1
  i5=1
  i4=9
  k2p=0
  i3=0
chmtrns.1078
chmtrns.1079
chmtrns.1080
chmtrns.1081
chmtrns.1082
chmtrns.1083
chmtrns.1084
chmtrns.1085
chmtrns.1086
chmtrns.1087
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chmtrns.1102
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chmtrns.1110
chmtrns.1111
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chmtrns.1119
chmtrns.1120
chmtrns.1121
chmtrns.1122
chmtrns.1123
chmtrns.1124
chmtrns.1125
chmtrns.1126
chmtrns.1127
chmtrns.1128
chmtrns.1129
chmtrns.1130
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chmtrns.1134
chmtrns.1135
chmtrns.1136
chmtrns.1137

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405 continue
    k1p=k2p+1
    k2p=k1p+(i4-1)
    i2=i3
    i3=i2+num(9)*i4
    write (6,620) (x(k),k=k1p,k2p)
c
c basis species
c
    do 410 j=1,m1
    i22=i2+j
    write (6,625) dum(j),(cn(k),k=i22,i3,m9)
410 continue
c
    if(ipart.ne.0) write(6,630) (shftsol(k),k=k1p,k2p)
    if(ipart.ne.0) write(6,631) (shift(1,k),k=k1p,k2p)
    if(ipart.ne.0) write(6,632) (shift(2,k),k=k1p,k2p)
    if(ipart.ne.0) write(6,633) (shift(3,k),k=k1p,k2p)
630 format('shftsol',6x,9(1pe12.4))
631 format('shift0',6x,9(1pe12.4))
632 format('shift1',6x,9(1pe12.4))
633 format('shift2',6x,9(1pe12.4))
    if(lno.ne.0) write(6,625) dum(lno),(eh(k),k=k1p,k2p)
    if(itemp.ne.0) write(6,625) xtemp,(tmp(k),k=k1p,k2p)
c sorbed species via ion exchange
c
    if (num(2).eq.0) go to 420
    write (6,621)
    m2=num(2)
c
    do 415 j=1,m2
    i22=i2+num(1)+j
    kk=ilbli(j)
    write (6,625) dum(kk),(cn(k),k=i22,i3,m9)
415 continue
c
c sorbed species via surface complexation
c
420 if (num(3).eq.0) go to 435
    write (6,622)
    m3=num(3)
c
    do 430 j=1,m3
    i22=i2+num(6)+j
    kk=ilble(j)
    if (kk.gt.num(1)) kk=kk-num(2)-num(3)
    if ((j.eq.1).or.(j.eq.2)) kk=ilble(j)
    write (6,625) dum(kk),(cn(k),k=i22,i3,m9)
430 continue
c
c aqueous phase complexes
c
435 if (num(4).eq.0) go to 445
    write(6,623)
c
    do 440 i=1,m4
    i22=i2+num(7)+i
    kk=i+num(1)
    write (6,625) dum(kk),(cn(k),k=i22,i3,m9)
440 continue
chmtrns.1138
chmtrns.1139
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chmtrns.1188
chmtrns.1189
chmtrns.1190
chmtrns.1191
chmtrns.1192
chmtrns.1193
chmtrns.1194
chmtrns.1195
chmtrns.1196
chmtrns.1197

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c
c precipitates
c
445 if (num(5).eq.0) go to 470
    write (6,624)
c
    do 460 i=1,m5
    kk=num(10)+i
    i22=i2+num(8)+i
    write (6,625) dum(kk),(cn(k),k=i22,i3,m9)
460 continue
c
470 continue
    il=i1+1
    if (i1.le.npri) go to 405
    npri2=npri*9
    if (npri2.eq.nmax) go to 490
    i4=nmax-npri2
    if (i5.eq.5) go to 490
    i5=5
    go to 405
490 if (k1.gt.kmax) go to 500
    go to 235
500 continue
    stop
c
c format statements for the main program
c
510 format(10x,a5)
530 format ('1',4x,'time=',1pe12.5,10x,'delt=',1pe12.4,10x,
1'concentration of species in moles/liter solution',/)
596 format (//,4x,'to have a net balance of zero charge, other '
1'species must be present (although not participating in the',/,
2 4x, 'chemical reactions) with a total concentration times ',
2 'charge of ',g10.3,/)
597 format (///,5x,'sigo=',(1pe10.3),5x,'sigb=',(1pe10.3),5x,'sigd=',
1 (1pe10.3),/,5x,'psio=',(1pe10.3),5x,'psibeta=',(1pe10.3),5x,
2'psid=',(1pe10.3),/)
598 format (4x,'so- =',1pe12.4,10x,'soh2+ =',1pe12.4,/)
600 format(//,4x,'dispersion coefficient=',f4.1,'v+'e10.2,5x,
1'fluid velocity =',g10.3,5x, 'number of grid points =',i5,/)
601 format(//,4x,'dispersion coefficient=',f4.1,'v+'e10.2,5x,
1'fluid velocity =',f10.3,'/ r',5x,
2 'number of grid points =',i5,/)
610 format(/,4x,'number of print outs =',i5,/,4x,
1 'given at the following times= ',8g10.4,/,34x,9g10.4)
611 format (/,4x,'number of sites(ion-exchange)',f10.4,10x,
1'number of sites(edl model)',f10.4)
612 format(/,'errsq= 'e10.2,5x,'climit= 'e10.2,5x,'iterj= 'i5,5x,
1 'iterm= 'i5,5x,'iterd= 'i5,5x,'dtmult= 'e10.2,5x,'ndiv= 'i5)
615 format(/,10x,'C-13 Fractionation parameters:')
616 format(/,10x,'shiftr= 'f10.4,10x,'shifts= 'f10.4)
620 format (//,4x,55x,'distance',/,4x,'species',1x,9f12.3,/)
622 format (/,4x,'sorbed(edl)',/)
623 format(/,4x,'complexes',/)
621 format(/,1x,'sorbed(ionex)',/)
624 format(/,2x,'precipitates',/)
625 format (3x,a8,2x,9(1pe12.4))
700 format(' 'a8,2g15.4,4x,2g11.4,6x,3g15.4)
740 format(/' complex          valence          aqueous conc.  sorption(io

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chmtrns.1198
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chmtrns.1200
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chmtrns.1257

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1) sorption(edl)')
750 format(' a8,5g15.4)
760 format('1',60x,'initial conditions',/,63x,'temp= ',f7.2
1 //)
765 format(60x,' for nodal point no ',i5,/)
780 format(' component',5x,' total ',5x,
1'bare ion ',5x,'sorbed concentration',8x,'act. coef.',5x,
2'kd(ion ex) kd(edl) ',/,13x,'aqueous conc.',4x,
3 'concentration',3x,' (ionex) (edl) ',/)
790 format('1',30x,'boundary or influx conditions',/,40x,
1 'temp= ',f7.2)
800 format (////,2x,i4,' bare ions',10x,i4,5x,'sorbing ions',
1 '(ionex)',10x,i4,5x,'sorbing ions (edl model)',///,
2 'component charge ',5x,'kinetic',
3 5x,'initial condition',7x,'boundary condition',/,
4 25x,'code',7x,'type',7x,'value',9x,'type',7x,'value',/)
802 format (///,2x,i4,' complexes',10x,i4,7x,'sorbing complexes',
1 '(ionex)',10x,i4,5x,'sorbing complexes (edl model)',///,
2'complex charge ',5x,'kcode',25x,'stoichiometry',/)
805 format(a8,f6.0,6x,i5,6x,i5,4x,1p12.4,4x,i5,4x,1p12.4,10x,
1 )
820 format(a8,f6.0,5x,i5,5x,10(0pf5.0) )
840 format (///,2x,i5,7x,'solid precipitates',//,2x,'precipitate',
1 2x,'kinetic code',10x,'stoichiometry',/)
841 format (//,2x,'precipitate',3x,'equivalent moles',
1 '/liter solution',/)
845 format (1x,a8,g10.3)
900 format (10x,7f10.3)
901 format(/,'Calcite dissolution information:',/)
902 format(/,'Silicate-water reaction information:',/)
903 format(/,'Glass dissolution information:',/)
905 format(/,'coefficients in log function of thermodynamic constants'
1 )
910 format (10x,7i10)
915 format(80x,/10x,i10,f10.3,i10,5x,a5)
916 format(10x,7e10.2)
917 format(10x,4(2i5))
919 format(/,' binary element nos. of the terms of the rate equation',
1 /,10x,4(2i5) )
918 format(10x,2e10.3,3i10,e10.3,i10)
920 format (10x,i10,6f10.3)
950 format(a8,f5.0,2i5,2f10.3,i5,2f10.3,2i5)
960 format(10x,3f10.3,f5.1)
970 format (a8,f10.3,10f5.1,/,20f5.1)
971 format(a8,6x,i5,9x,10(0pf5.1) )
972 format(a8,i5,10f5.1,/,20f5.1 )
974 format(a8,7e10.3)
978 format(/,'redox constants',/, 'gas constant R= ',e12.3,
1 10x,'Faraday constant F= ',e12.3 )
979 format(a8,10f5.1,/,20f5.1 )
975 format(' binary print of species no. participating in each'/
1 ' term of rate formulla and the reaction constants ',//
2 4( 2i5,f10.3 ))
976 format(/' no of terms in the rate formulla = 'i5 ,//
1 ' no of other additional data needed = 'i5 ,//
2 ' representative surface parameter = 'e12.3,//
3 ' xdiag = 'a5,/)
977 format( ' additional data for rate calculation',// 10e12.3 )
980 format (10x,2f10.3,2i5)
990 format (/,4x,'your number of sorbing ions input does not equal the

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chmtrns.1258
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chmtrns.1311
chmtrns.1312
chmtrns.1313
chmtrns.1314
chmtrns.1315
chmtrns.1316
chmtrns.1317

```

```

1 number that was listed initially',2i5,10x,2i5)
999 format ('1',20a4)
2065 format(1x,'this simulation is isothermal, temperature =',f5.0)
2067 format(1x,'simulation of mixing with heat transport, with initial
1temperature =',f5.0,/,4x,'heat capacities of fluid and solid are',
2g10.2,2x,'and',g10.2,/,4x,'thermal conductivity of solid',g10.2)
2068 format(1x,'inner boundary condition is constant temperature =',f5.
10)
2069 format(1x,'inner boundary condition is constant flux of fluid with
1 temperature =',f5.0)
2070 format(1x,'fixed temperature gradient:',/,4x,f10.3,2x,'at inner bou
1ndary',/,4x,f10.3,2x,'at outer boundary')
2073 format(1x,'temperature is held at initial value at outer boundary'
1)
1000 format (20a4)
1001 format (10x,5(1pe12.4,/))
1010 format(10x,2a8)
1011 format (/,4x,'unit of length is',2x,a8,10x,'unit of time is'
1,2x,a8)
2000 format (/,4x,'the activity product is',1pe10.3,5x,
1'which now exceeds the solubility product of',1pe10.3)
2021 format (/,4x,'precipitation at node',i5,5x,'for species',a8,
1'at time',1pe11.3)
2022 format (/,4x,'convergence is not obtained, so time step is '
1, 'divided by 2, delt=',1pe12.4)
2023 format (/,4x,'convergence is obtained in less than 6 ',
1'iterations so time step is increased by 1.75',/,4x,'delt=',
11pe12.4,10x, 'at time=',1pe12.4)
2024 format(i10)
2050 format (/,4x,'at node',i5,4x,'species',a8,'has redissolved',/,
1' the concentration of this species at time' 1pe8.2,4x, 'is',
2 e12.4,/, 'and the concentration of this species at time',e8.2,
3 4x,'is', e12.4)
2060 format (/,4x,'inner boundary is constant concentration',10x,
1'outer boundary is zero flux')
2061 format (/,4x,'inner boundary is constant flux',10x,'outer',
1' boundary is zero flux')
2062 format (/,4x,'inner boundary is constant concentration',10x,
1'outer boundary is constant initial concentration')
2063 format (/,4x,'inner boundary is constant flux',10x,'outer'
1' boundry is constant initial concentration')
2080 format('calculation time= ',e15.5,'seconds')
3000 format(/,'redox is considered'/)
3100 format(/,'kinetics of reversible silica dissolution considered'/)
3200 format(/,'kinetics of non-rev. silica dissolution considered',/)
3300 format(/,'kinetics of rev. precipitate dissolution considered',/)
end
subroutine iguess(cm,cbasis,num,n,lnh)
c
c *****
c this subroutine calculates the first guess of the values of the
c basis species, complexes, sorbed components and precipitates
c for an equilibrium distribution of species calculation. it assumes
c that the concentration of the basis species is equal to value set
c for the initial condition for that species, i.e. it is set equal to
c bi(j); the concentrations of the complexes and the sorbed components
c are then calculated from the mass action equations assuming these
c basis species concentrations. the concentration of the precipitates
c set equal to 0 for the first guess. the subroutine does not necessari
c make the best guess. the user can read in guesses instead of calling

```

```

chmtrns.1318
chmtrns.1319
chmtrns.1320
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chmtrns.1351
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chmtrns.1359
chmtrns.1360
chmtrns.1361
chmtrns.1362
chmtrns.1363
chmtrns.1364
iguess.2
iguess.3
iguess.4
iguess.5
iguess.6
iguess.7
iguess.8
iguess.9
iguess.10
iguess.11
iguess.12
iguess.13
iguess.14

```

```

c this routine. set ig=1 if you want to call this routine, otherwise s iguess.15
c it equal to 0. iguess.16
c ***** iguess.17
dimension cm(1),num(1),cbasis(25) iguess.18
common/ab/vj(75),ac(75,100),eqconst(25,100),h2ok(100),alfa(4,100), /ab/.2
1s(25,25),ss(25,25),ah(25),h2oc(8),con(25,8),conk(20,8),comp(4,2), /ab/.3
2 ilbli(25),ilble(25),q(10,100) /ab/.4
common/edl/c1,c2,area,soh /edl/.2
common/ad/x(200),delt,doa,dob,vo,cecns /ad/.2
m5=num(5) iguess.22
nspecm=num(1) iguess.23
if (lnh.gt.0) nspecm=num(1)-1 iguess.24
c iguess.25
c set the concentration of the basis species equal to the concentration iguess.26
c read in for that basis species even though that value may be for iguess.27
c the total aqueous phase concentration of that species. iguess.28
c iguess.29
do 10 j=1,nspecm iguess.30
10 cm(j)=cbasis(j) iguess.31
if(lnh.gt.0) cm(num(1))=h2ok(n)/cm(lnh) iguess.32
c iguess.33
c calculate the sorbed concentrations from the mass action equations iguess.34
c iguess.35
if (num(2).eq.0) go to 100 iguess.36
cm(num(1)+1)=cecns iguess.37
amttotal=0 iguess.38
j1=ilbli(1) iguess.39
m2=num(2) iguess.40
do 20 j=2,m2 iguess.41
jj=ilbli(j) iguess.42
cm(num(1)+j)=(eqconst(j,n)/eqconst(1,n))**(1./vj(j1))*cm(num(1)+1) iguess.43
1** (vj(jj)/vj(j1))/(cm(j1)**(vj(jj)/vj(j1))) iguess.44
cm(num(1)+j)=cm(jj)*cm(num(1)+j) iguess.45
20 continue iguess.46
100 if (num(3).eq.0) go to 200 iguess.47
ij1=num(2)+1 iguess.48
ij2=num(2)+2 iguess.49
cm(num(6)+3)=soh iguess.50
kk=num(6) iguess.51
cm(kk+2)=cm(lnh)*soh*0.1/eqconst(num(2)+1,n) iguess.52
cm(kk+1)=eqconst(num(2)+2,n)*cm(kk+3)/cm(lnh) iguess.53
if (num(3).lt.4) go to 200 iguess.54
m3=num(3) iguess.55
do 120 i=4,m3 iguess.56
jj=ilble(i) iguess.57
ij=num(2)+i iguess.58
cm(kk+i)=eqconst(ij,n)*cm(kk+3)/((cm(lnh))**ah(i)) iguess.59
120 continue iguess.60
200 continue iguess.61
c iguess.62
c calculate the concentration of the complexes iguess.63
c using the mass action equations iguess.64
c iguess.65
if (num(4).eq.0) go to 300 iguess.66
m4=num(4) iguess.67
do 250 i=1,m4 iguess.68
ccm=eqconst(num(12)+i,n) iguess.69
m1=num(1) iguess.70
do 220 j=1,m1 iguess.71
if (s(j,i).eq.0.) go to 220 iguess.72

```

```

      ccm=ccm*cm(j)**s(j,i)
220 continue
      cm(num(7)+i)=ccm
250 continue
c
c set the first guess for the precipitates to be 0
c
300 if (num(5).eq.0) go to 400
      do 350 j=1,m5
350 cm(num(8)+j)=0.0
400 return
      end
      subroutine equilb(cm,wconst,index1,index2,num,n,ss,eqconst,ctot,
c
c
c      lac,lchrg,lnh,in)
c *****
c this subroutine calculates the equilibrium distribution of species.
c calls the subroutine reseq which calculates the residues of the equil
c equations. the equilibrium distribution of species is calculated giv
c the type of conditions set for each species, i.e. total concentration
c species, bare ion concentration, etc. this set of conditions must eq
c the number of basis species. the mass action expressions, solubility
c equations, and the site constraint equation are used to calculate the
c concentrations of the rest of the species.
c *****
      dimension cm(1),wconst(1),z(25,25),y(25),index1(1),index2(1)
      1, ss(25,1),eqconst(25,1),ac(75,1),iterp(35),num(1)
      common/edl/c1,c2,area,soh
      common/spec/leach1(5),nb,pini(5)
c
      mdim=25
      ntot=num(8)
c
      if (num(3).eq.0) soh=20.
      iter=1
      if (num(5).eq.0) go to 2
      m5=num(5)
      do 1 i=1,m5
1 iterp(i)=1
2 iter=iter+1
c
c if convergence is not obtained within 100 iterations, the
c calculations are stopped
c
      if (iter.gt.100) go to 9
      nsol=0
c
c the solubility product for a precipitate is only included when
c the product of the activities of the species making up that
c precipitate exceeds this product; to avoid oscillations between
c the precipitate wanting to form or not, the solubility product
c is included only when it is exceeded for two calculations
c
      if (num(5).eq.0) go to 40
      do 4 i=1,m5
      aksol=1.0
      m1=num(1)
      do 5 j=1,m1
      if (cm(j).eq.0.0) cm(j)=1.0e-35

```

```

iguess.73
iguess.74
iguess.75
iguess.76
iguess.77
iguess.78
iguess.79
iguess.80
iguess.81
iguess.82
iguess.83
iguess.84
equilib.2
equilib.3
equilib.4
equilib.5
equilib.6
equilib.7
equilib.8
equilib.9
equilib.10
equilib.11
equilib.12
equilib.13
equilib.14
equilib.15
equilib.16
equilib.17
/edl/.2
/spec/.2
equilib.20
equilib.21
equilib.22
equilib.23
equilib.24
equilib.25
equilib.26
equilib.27
equilib.28
equilib.29
equilib.30
equilib.31
equilib.32
equilib.33
equilib.34
equilib.35
equilib.36
equilib.37
equilib.38
equilib.39
equilib.40
equilib.41
equilib.42
equilib.43
equilib.44
equilib.45
equilib.46
equilib.47
equilib.48
equilib.49

```

```

      aksol=aksol*(ac(j,n)*cm(j))**ss(j,i)
      5 continue
c
c if a solid has been put in contact with the groundwater at the
c first node point, the solubility product of that precipitate will
c always be included for the distribution of species at the inner
c boundary condition.
c
      if ((leach1(1).eq.i).and.(n.eq.nb)) index1(i)=1
      if ((leach1(1).eq.i).and.(n.eq.nb)) go to 77
      index1(i)=0
      ij=num(12)+num(4)+i
      ek=0.001*eqconst(ij,n)
      if ((eqconst(ij,n).lt.aksol).or.(cm(ntot+i).gt.1.e-16)) iterp(i)
1 =iterp(i)+1
      if((eqconst(ij,n).lt.aksol).or.(cm(ntot+i).gt.1.e-16)) go to 76
      iterp(i)=0
76 if (iterp(i).ge.2) index1(i)=1
77 if (index1(i).eq.1) nsol=nsol+1
      m9=num(9)
      if(iter.gt.in) write (6,900) i,aksol,eqconst(ij,n)
900 format (4x,'precipitate no.',4x,i5,10x,'precipitation check',
      1 10x,'product of concentrations is',
      24x,e12.4,/,4x,'solubility product is ',4x,e12.5)
      4 continue
      40 continue
c
c residues of the constraint equations for the initial and boundary
c conditions and the mass action and site constraint equation are
c calculated in the subroutine reseq
c
      call reseq(wconst,cm,index1,index2,y,n,ctot,mdim,num,lchrg,lnh,
      1 nsol,0)
      ntotp=ntot+nsol
      print 4000 , ntot, nsol, ntotp
c 4000 format(3i10)
      if (iter.gt.in) write (6,1010) (y(i),i=1,ntotp)
1010 format (/,4x,'residues are',/,4(8e12.4,/))
c
c the jacobian for the equilibrium distribution of species; i.e. for th
c equations in subroutine reseq is calculated here
c
      call jacob2(z,cm,wconst,index1,index2,y,num,n,ctot,nsol,lchrg,
      1lnh,mdim)
c
c from the jacobian and the residues for the last guess, calculate the
c new guess for the all the species
c
      call simq(z,y,ntotp,mdim)
c
101 format(4x,i5,10x,'values for this iteration',/,/,4x,
      1'species no.',10x,'old value',
      2 10x,'new value',10x,'error',/)
      if (iter.gt.in) write (6,101) iter
      do 6 j=1,ntot
      ccl=cm(j)
      cm(j)=cm(j)-y(j)
      if (iter.gt.in) write (6,1000) j,ccl,cm(j),y(j)
1000 format (/,4x,i10,10x,1pe12.4,9x,1pe12.4,9x,1pe12.4)
c

```

```

eq lib.50
eq lib.51
eq lib.52
eq lib.53
eq lib.54
eq lib.55
eq lib.56
eq lib.57
eq lib.58
eq lib.59
eq lib.60
eq lib.61
eq lib.62
eq lib.63
eq lib.64
eq lib.65
eq lib.66
eq lib.67
eq lib.68
eq lib.69
eq lib.70
eq lib.71
eq lib.72
eq lib.73
eq lib.74
eq lib.75
eq lib.76
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eq lib.79
eq lib.80
eq lib.81
eq lib.82
eq lib.83
eq lib.84
eq lib.85
eq lib.86
eq lib.87
eq lib.88
eq lib.89
eq lib.90
eq lib.91
eq lib.92
eq lib.93
eq lib.94
eq lib.95
eq lib.96
eq lib.97
eq lib.98
eq lib.99
eq lib.100
eq lib.101
eq lib.102
eq lib.103
eq lib.104
eq lib.105
eq lib.106
eq lib.107
eq lib.108
eq lib.109

```

```

c the concentration of the species is not allowed to go negative or
c for the surface complexation model, the sorbed concentration cannot
c be greater than the total number of sites
c
c   if(cm(j).lt.0.) cm(j)=cc1/10.
c   if ((j.gt.num(6)).and.(j.lt.num(7)).and.(cm(j).gt.soh)) cm(j)=soh
c   6 continue
c
c   index=0
c
c calculate the amount of the precipitates; only precipitates that are
c forming are included in this calculation
c
c   if (num(5).eq.0) go to 66
c   do 65 i=1,m5
c   if (index1(i).eq.0) go to 65
c   index=index+1
c   cc1=cm(ntot+i)
c   cm(ntot+i)=cm(ntot+i)-y(ntot+index)
c   ii=ntot+i
c   iii=ntot+index
c   if (iter.gt.in) write (6,1000) i,cc1,cm(ii),y(iii)
c   if (cm(ntot+i).lt.0.) iterp(i)=0
c   if (cm(ntot+i).lt.0.) cm(ntot+i)=0.
c 65 continue
c 66 continue
c
c check convergence; if within the criteria set, then end the
c iterations, otherwise continue
c
c   do 7 j=1,ntotp
c   if (cm(j).lt.1.e-30) go to 7
c   if(abs(y(j)/cm(j)).gt.1.0e-04) go to 2
c 7 continue
c   return
c 9 write(6,100) iter
c 100 format(' no convergence in eqlib after iter ='i3)
c   stop
c   end
c   subroutine simq(z,y,n,mdim)
c
c
c *****
c inversion of a matrix; it is used in calculating
c an equilibrium distribution of species such as
c in the initial conditions and the boundary conditions.
c the jacobian is stored in z while the residues are in
c y. this subroutine solves the equation zx=y for x
c *****
c   dimension z(mdim,1),y(1)
c   provision for n=1
c   if(n.ne.1) go to 50
c   y(1)=y(1)/z(1,1)
c   return
c 50 continue
c element of elimination
c n1=n-1
c do 10 m=1,n1
c   zmax=0.
c   imax=0

```

```

eqlib.110
eqlib.111
eqlib.112
eqlib.113
eqlib.114
eqlib.115
eqlib.116
eqlib.117
eqlib.118
eqlib.119
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eqlib.121
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eqlib.139
eqlib.140
eqlib.141
eqlib.142
eqlib.143
eqlib.144
eqlib.145
eqlib.146
eqlib.147
eqlib.148
simq.2
simq.3
simq.4
simq.5
simq.6
simq.7
simq.8
simq.9
simq.10
simq.11
simq.12
simq.13
simq.14
simq.15
simq.16
simq.17
simq.18
simq.19
simq.20
simq.21
simq.22

```

```

c      find max of column
      do 20 i=m,n
      if(abs(z(i,m)).le.zmax) go to 20
      imax=i
      zmax=abs(z(i,m))
20    continue
c      error return
      if(imax.ne.0) go to 30
      write(6,1000)
      write(6,9000) i,m
      write(6,990) (z(i,m),i=1,n)
30    continue
c      row interchange
      if(imax.eq.m) go to 35
      v=y(m)
      y(m)=y(imax)
      y(imax)=v
      do 40 j=m,n
      v=z(m,j)
      z(m,j)=z(imax,j)
      z(imax,j)=v
40    continue
35    continue
c      diagonalize
      m1=m+1
      do 70 i=m1,n
      v=z(i,m)/z(m,m)
      y(i)=y(i)-v*y(m)
      do 70 j=m,n
      z(i,j)=z(i,j)-v*z(m,j)
70    continue
10    continue
c      back substitute
      y(n)=y(n)/z(n,n)
      n1=n-1
      do 100 k=1,n1
      i=n-k
      i1=i+1
      do 90 j=i1,n
90    y(i)=y(i)-y(j)*z(i,j)
100  y(i)=y(i)/z(i,i)
      return
900  format(4x,2i10)
990  format(4x,5(19e12.4))
1000 format(' singular jacobian matrix')
      end
      subroutine setup(xmax,nmax,itpe,gc,rw)
c
c
c *****
c calculates the grid based on an exponential law; if gc is set
c to 0, a uniform grid is calculated.
c *****
      common/ad/x(200),delt,doa,dob,vo,cecn
c
      dn=1./float(nmax-1)
      x(1)=0.
      if(itype.eq.1) x(1)=rw

```

```

simq.23
simq.24
simq.25
simq.26
simq.27
simq.28
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simq.30
simq.31
simq.32
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simq.62
simq.63
simq.64
simq.65
simq.66
simq.67
simq.68
setup.2
setup.3
setup.4
setup.5
setup.6
setup.7
setup.8
/ad/.2
setup.10
setup.11
setup.12
setup.13
setup.14
setup.15

```

```

      x1=x(1)
      do 10 i=2,nmax
      pip=float(i-1)
      if(gc.gt.0.) go to 5
c      calculation for uniform grid
c
      x(i)=xmax*dn*pip+x1
      go to 10
c
c      calculation for variable grid
c
      5 x(i)=xmax*(gc**((pip)*dn)-1.)/(gc-1.)+x1
      10 continue
      write(6,190) (x(n),n=1,nmax)
      190 format(/55x,' ** spatial grid ** ',//,' ',10g13.4))
      return
      end
      subroutine res(cn,co,bc,bc2,r,num,mdim,lnh,ibnd,itype,jacob)
c
c
c
c
c
c
c *****
c calculates the residues of the transport equations, the site
c constraint equation, the mass action equations, and the boundary
c conditions. the boundary conditions are stored in the arrays bc
c and bc2. if boundary conditions other than the concentration and
c flux conditions are of interest, the user would have to supply how
c the values of bc and bc2 would change. for the concentration boundar
c condition at the inner node, bc stores the total concentration of a
c species in the aqueous phase and in the form of a precipitate. for t
c flux condition at this boundary, bc stores the fluid velocity times
c the total aqueous phase concentration of each species. for the outer
c boundary, for the concentration condition, bc2 stores the basis
c species concentration of the initial conditions, and for the no flux
c condition it is not used.
c the subroutine is called from both the main program and the subroutin
c jacobi.
c *****
      dimension cn(1),co(1),bc(1),r(mdim,1),num(1),ibnd(1),bc2(1)
      common/ab/vj(75),ac(75,100),eqconst(25,100),h2ok(100),alfa(4,100),
      1s(25,25),ss(25,25),ah(25),h2oc(8),con(25,8),conk(20,8),comp(4,2),
      2 ilbli(25),ilble(25),q(10,100)
      common/ac/elconc(100)
      common/nj/isorpi(30),isorpe(30),iion,ieion
      common/ad/x(200),delt,doa,dob,vo,cecns
      common/crate/rate(50),kcode(25),inx1(5,25),inx2(5,25),cdat(5,25),
      1 reactsk(5,10,100),nsrt(5),sarea(5),nparam(5),xkinet(5),xmax,time,
      2 gc,excode,tpcode,kinr,xdiag(5),shift(4,100),shftsol(100)
      nmax=num(14)
      nmaxm=nmax-1
      m1=num(1)
      m2=num(2)
      m3=num(3)
      m4=num(4)
      m5=num(5)
      ntot=num(9)
c
c calculate the activities of the aqueous phase species

```

```

      setup.16
      setup.17
      setup.18
      setup.19
      setup.20
      setup.21
      setup.22
      setup.23
      setup.24
      setup.25
      setup.26
      setup.27
      setup.28
      setup.29
      setup.30
      setup.31
      setup.32
      res.2
      res.3
      res.4
      res.5
      res.6
      res.7
      res.8
      res.9
      res.10
      res.11
      res.12
      res.13
      res.14
      res.15
      res.16
      res.17
      res.18
      res.19
      res.20
      res.21
      res.22
      res.23
      res.24
      res.25
      /ab/.2
      /ab/.3
      /ab/.4
      /ac/.2
      /nj/.2
      /ad/.2
      /crate/.2
      /crate/.3
      /crate/.4
      res.31
      res.32
      res.33
      res.34
      res.35
      res.36
      res.37
      res.38
      res.39
      res.40

```



```

c          call active(num,cn,vj,ac,elconc,75,1,num(14))          res.41
c                                                                res.42
c                                                                res.43
c          *****          res.44
c          inner boundary condition set here          res.45
c          *****          res.46
c          n=1          res.47
c          n1=2          res.48
c                                                                res.49
c          if( ibnd(1).eq.1 ) n1=1          res.50
c                                                                res.51
c          residue calculations for internal boundary drichlet condition          res.52
c                                                                res.53
c          if(n1.eq.1) go to 10          res.54
c          do 20 j=1,ntot          res.55
c          20 r(j,1)=1.0e-30          res.56
c          go to 25          res.57
c                                                                res.58
c          calculate the residues for the mass action equations          res.59
c                                                                res.60
c                                                                res.61
c                                                                res.62
c          10 call algebrc(num,cn,co,r,1,1,mdim,elconc,lnh,0,jcob)          res.63
c          25 continue          res.64
c                                                                res.65
c          *****          res.66
c          calculation of changes in the porous medium          res.67
c          *****          res.68
c          do 170 n=n1,nmaxm          res.69
c          neven=(n-1)*ntot          res.70
c          nplus=neven+ntot          res.71
c          nminus=neven-ntot          res.72
c          ii=0          res.73
c          ie=3          res.74
c          do 40 i=1,50          res.75
c          rate(i)=0.0          res.76
c          40 continue          res.77
c          if(kinr.eq.0) go to 45          res.78
c          if(excode.eq.0) go to 45          res.79
c          call srate(n,num,co,cn,ac,neven,delt,0)          res.80
c          45 continue          res.81
c          do 78 j=1,m1          res.82
c          vv=vo          res.83
c          if (itype.eq.1) vv=vo/x(n)          res.84
c          dd=doa*vv+dob          res.85
c                                                                res.86
c          for a flux condition at the inner boundary and for          res.87
c          radial flow, the dispersion coefficient and the fluid velocity          res.88
c          for the first grid are calculated here          res.89
c                                                                res.90
c          if (itype.eq.1) vv=vv-( dob/x(n) )          res.91
c          if (n.eq.1) go to 50          res.92
c                                                                res.93
c          calculate the residues of the transport equations for nodes          res.94
c          2 through nmax-1 including the changes in the basis species          res.95
c                                                                res.96
c          r(j,n)=(cn(neven+j)-co(neven+j))/delt-dd*((cn(nplus+j)-          res.97
c          1cn(neven+j))/(x(n+1)-x(n))-(cn(neven+j)-cn(nminus+j))          res.98
c          2/(x(n)-x(n-1)))/(0.5*(x(n+1)-x(n-1)))+vv*(cn(nplus+j)-          res.99
c          3 cn(nminus+j))/(x(n+1)-x(n-1))+rate(kcode(j))          res.100

```

```

      go to 51
c
c for the flux boundary condition at the first node point,
c calculate the changes in the first node point for the
c basis species
c
50 r(j,1)=(cn(neven+j)-co(neven+j))/delt
   r(j,1)=r(j,1)-2.0*dd*(cn(nplus+j)-cn(neven+j))/((x(2)-x(1))**2)
   r(j,1)=r(j,1)+(vv*cn(neven+j)-bc(j))/(x(2)-x(1))
1   *(2.0+vv*(x(2)-x(1))/dd)+rate(kcode(j))
51 continue
c
c include the change in the sorption of the basis species
c for nodes 2 thru nmax-1 or 1 thru nmax-1 depending on the
c boundary conditions; first is for sorption via ion exchange
c next is for any sorption via surface complexation
c
   if (num(2).eq.0) go to 68
   if (isorpi(j).eq.0) go to 68
   ii=ii+1
   ip=num(1)+ii
   r(j,n)=r(j,n)+(cn(neven+ip)-co(neven+ip))/delt
68 continue
   if (num(3).eq.0) go to 69
   if (isorpe(j).eq.0) go to 69
   if (j.eq.lnh) go to 70
   ie=ie+1
   ip=num(6)+ie
   r(j,n)=r(j,n)+(cn(neven+ip)-co(neven+ip))/delt
   go to 69
70 ip=num(6)
c
c for sorption via surface complexation, need to consider the
c changes in the soh and soh2+ sites
c
   r(j,n)=r(j,n)+2*(cn(neven+ip+2)-co(neven+ip+2))/delt
1   +(cn(neven+ip+3)-co(neven+ip+3))/delt
c
c next include changes in the complexes at the node points;
c time changes, advection and dispersion
c
69 if (num(4).eq.0) go to 72
   do 71 i=1,m4
   ip=num(7)+i
   if (n.eq.1) go to 52
   r(j,n)=r(j,n)+s(j,i)*(cn(neven+ip)-co(neven+ip))/delt-s(j,i)*
1dd*((cn(nplus+ip)-cn(neven+ip))/(x(n+1)-x(n))-
2(cn(neven+ip)-cn(nminus+ip))/(x(n)-x(n-1)))/(0.5*(x(n+1)-x(n-1))))+
1 s(j,i)*vv*(cn(nplus+ip)-cn(nminus+ip))/(x(n+1)-x(n-1))
   go to 53
52 continue
c
c special case for considering these last changes at the first
c node point if flux boundary condition at the inner boundary
c
   r(j,1)=r(j,1)+s(j,i)*(cn(neven+ip)-co(neven+ip))/delt
   r(j,1)=r(j,1)-2.0*s(j,i)*dd*(cn(nplus+ip)-cn(neven+ip))/
1 (x(2)-x(1))**2.0)
   r(j,1)=r(j,1)+s(j,i)*vv*cn(neven+ip)*(2.0/(x(2)-x(1))+vv/dd)
53 continue

```

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res.101
res.102
res.103
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res.160

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```

c
c need to also include the changes in the sorption of the complexes
c whether via ion exchange or surface complexation.
c
    if (num(2).le.iion) go to 568
    if (isorpi(j+num(1)).eq.0) go to 568
    ii=ii+1
    ip=num(1)+ii
    r(j,n)=r(j,n)+s(j,i)*(cn(neven+ip)-co(neven+ip))/delt
568 continue
    if (num(3).le.ieion) go to 71
    if (isorpe(num(1)+j).eq.0) go to 71
    ie=ie+1
    ip=num(6)+ie
    r(j,n)=r(j,n)+s(j,i)*(cn(neven+ip)-co(neven+ip))/delt
71 continue
72 continue
c
c include the changes in the precipitates at a node point
c
    if (num(5).eq.0) go to 78
    do 74 i=1,m5
    ip=num(8)+i
    r(j,n)=r(j,n)+ss(j,i)*(cn(neven+ip)-co(neven+ip))/delt
74 continue
78 continue
c
c when water dissociation is included, need to actually calculate
c the changes for the dummy variable which is the concentration of
c the h+ ion minus the concentration of the oh- ion
c
    if (lnh.ne.0) r(lnh,n)=r(lnh,n)-r(num(1),n)
    if (lnh.ne.0) r(num(1),n)=h2ok(n)-ac(lnh,n)*cn(neven+lnh)*
1      ac(num(1),n)*cn(neven+num(1))
c
c calculate the changes in the site constraint, the mass action,
c and the solubility products at the node points
c
170 continue
c
c
c call algebrc(num,cn,co,r,n1,nmax,mdim,elconc,lnh,0,jcob)
c
c calculation of the conditions at the last node point
c
    n=nmax
    neven=(n-1)*ntot
    nminus=(n-2)*ntot
    if (ibnd(2).eq.0) go to 210
c
c no flux condition
c
    do 200 j=1,m1
    r(j,n)=( cn(neven+j)-cn(nminus+j) )/( x(nmax)-x(nmax-1) )
200 continue
    go to 220
c
c concentration boundary condition
c
210 do 215 j=1,m1

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res.217
res.218
res.219
res.220

```

```

215 r(j,n)=cn(neven+j)-bc2(j)
220 continue
c
  if (lnh.ne.0) r(lnh,n)=r(lnh,n)-r(num(1),n)
  if (lnh.ne.0) r(num(1),n)=h2ok(n)-ac(lnh,n)*cn(neven+lnh)*
1      ac(num(1),n)*cn(neven+num(1))
c
c calculate the residues for the algebraic equations for the
c conditions at the last node point
c
c
c residue calculations for external boundary drichlet condition
c
  if( ibnd(2).ne.0 ) go to 225
  do 230 j=1,ntot
230 r(j,nmax)=1.0e-30
  go to 235
225 call algebrc(num,cn,co,r,nmax,nmax,mdim,elconc,lnh,0,jcob)
235 continue
  return
  end
  subroutine active(num,cn,vj,ac,elconc,mdim,nbegin,nend)
c
c *****
c calculates the activities based on the davies equation
c the ionic strength at each node point is stored in elconc,
c the activities are in the matrix ac(i,n)
c *****
  dimension num(1),cn(1),vj(1),ac(mdim,1),elconc(1)
  common/oxred/lno,lnh
c
200 format(i10)
  m1=num(1)
  m4=num(4)
  ntot=num(9)
  if (nbegin.eq.nend) ntot=0
  do 50 n=nbegin,nend
c
c calculation of ionic strength
c
  ctot=0.
  si=0.
  do 10 j=1,m1
  if(j.eq.lno) go to 10
  if (cn((n-1)*ntot+j) .lt.0.) go to 60
  ctot=ctot+vj(j)*cn((n-1)*ntot+j)
  si=si+vj(j)**2*cn((n-1)*ntot+j)
10 continue
  if (num(4).eq.0) go to 16
  do 15 i=1,m4
  if (cn((n-1)*ntot+num(7)+i).lt.0) go to 60
  ctot=ctot+vj(num(1)+i)*cn((n-1)*ntot+num(7)+i)
15 si=si+vj(num(1)+i)**2*cn((n-1)*ntot+num(7)+i)
16 continue
c
c although the net charge of the species being considered is in the
c calculations may not be equal to zero, for an accurate calculation
c of the ionic strength, all the chemical species must be considered
c therefore, it is assumed here that the balance of the charge is made
c up by a chemical species of a +1 or -1 charge and a concentration

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res.221
res.222
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active.40

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```

c of ctot. if this is not reasonable, then the actual calculation      active.41
c should be done with a net charge of 0.                                active.42
c                                                                           active.43
c   si=si+abs(ctot)                                                    active.44
c   cionst=0.5*si                                                       active.45
c   elconc(n)=cionst                                                    active.46
c   si=sqrt(cionst)                                                     active.47
c   fi=0.5*(si/(1.+si))-0.3*cionst                                     active.48
c                                                                           active.49
c calculation of activity coefficients                                   active.50
c                                                                           active.51
c   do 20 j=1,m1                                                        active.52
c   if(j.eq.lno) go to 20                                              active.53
c   g=fi*vj(j)**2                                                       active.54
c   ac(j,n)=10.**(-g)                                                  active.55
c 20 continue                                                            active.56
c   if (num(4).eq.0) go to 50                                           active.57
c   do 25 i=1,m4                                                        active.58
c   gcx=fi*vj(num(1)+i)**2                                             active.59
c 25 ac(num(1)+i,n)=10.**(-gcx)                                        active.60
c 50 continue                                                            active.61
c   return                                                              active.62
c 60 write (6,100)                                                      active.63
c 100 format (/,'4x','the concentration is less than zero which is not' active.64
c   1 ' allowed, therefore the program has stopped',/)                active.65
c   return                                                              active.66
c   end                                                                  active.67
c   subroutine algebrc(num,cn,co,r,n1,n2,mdim,elconc,lnh,k1,jcob)      algebrc.2
c                                                                           algebrc.3
c                                                                           algebrc.4
c *****                                                                algebrc.5
c calculates the residue for the site constraint equations             algebrc.6
c and the mass action equations describing the sorption              algebrc.7
c reactions and the formation of complexes and precipitates         algebrc.8
c *****                                                                algebrc.9
c                                                                           algebrc.10
c   dimension num(1),cn(1),r(mdim,1),residue(25),elconc(1)          algebrc.11
c   dimension co(1)                                                    algebrc.12
c   common/ab/vj(75),ac(75,100),eqconst(25,100),h2ok(100),alfa(4,100), /ab/.2
c   1s(25,25),ss(25,25),ah(25),h2oc(8),con(25,8),conk(20,8),conp(4,2), /ab/.3
c   2 ilbli(25),ilble(25),q(10,100) /ab/.4
c   common/nj/isorpi(30),isorpe(30),iion,ieion /nj/.2
c   common/ad/x(200),delt,doa,dob,vo,cecns /ad/.2
c   common/crate/rate(50),kcode(25),inx1(5,25),inx2(5,25),cdat(5,25), /crate/.2
c   1 reactsk(5,10,100),nsrt(5),sarea(5),nparam(5),xkinet(5),xmax,time, /crate/.3
c   2 gc,excode,tpcode,kinr,xdiag(5),shift(4,100),shftsol(100) /crate/.4
c   m1=num(1)                                                            algebrc.17
c   m2=num(2)                                                            algebrc.18
c   m3=num(3)                                                            algebrc.19
c   m4=num(4)                                                            algebrc.20
c   m5=num(5)                                                            algebrc.21
c   nmax=num(14)                                                        algebrc.22
c   nmaxm=nmax-1                                                       algebrc.23
c   kk=k1                                                                algebrc.24
c   do 200 n=n1,n2                                                     algebrc.25
c   nstart=(n-1)*num(9)                                               algebrc.26
c                                                                           algebrc.27
c kinetic rate calculations for dissolution                            algebrc.28
c                                                                           algebrc.29
c   do 15 i=1,50                                                       algebrc.30

```

```

rate(i)=0.0
15 continue
  if(k1.eq.1.or.tpcode.eq.0) go to 25
  call srate(n,num,co,cn,ac,nstart,delt,1)
  ddelx= xmax/nmaxm
  if(gc.eq.0.0) go to 20
  ddelx=( x(n+1)-x(n) )/2.0+( x(n)-x(n-1) )/2.0
  if( n.eq.1 ) ddelx= ( x(n+1)-x(n) )/2.0
  if( n.eq.nmax ) ddelx=( x(n)-x(n-1) )/2.0
  go to 25
20 if( n.eq.1.or.n.eq.nmax ) ddelx=ddelx/2.0
25 continue

c
c site constant equation for sorption via ion exchange
c
  if (kk.eq.1) nstart=0
  if (num(2).eq.0) go to 45
  r(num(1)+1,n)=cecns
  amttotal=0.
  do 35 j=1,m2
    jj=ilbli(j)
    r(num(1)+1,n)=r(num(1)+1,n)-vj(jj)*cn(nstart+num(1)+j)
35 amttotal=amttotal+cn(nstart+num(1)+j)

c
c mass action equations describing sorption via ion exchange
c
  if (num(2).eq.1) go to 45
  j1=ilbli(1)
  do 40 j=2,m2
    jj=ilbli(j)
    aj=(cn(nstart+num(1)+j)/amttotal)**vj(jj)
    al=(cn(nstart+num(1)+1)/amttotal)**vj(jj)
36 r(num(1)+j,n)=(eqconst(j,n)*cn(nstart+jj)*ac(jj,n))**vj(jj)*
  1 al-(eqconst(1,n)*cn(nstart+j1)*ac(j1,n))**vj(jj)*aj
40 continue
45 continue
  if (num(3).eq.0) go to 52

c
c for soption via surface complexation, mass action equations
c are solved in subroutine redl
c
  call redl(cn,residue,nstart,n,elconc(n),lnh,num)
  do 50 i=1,m3
    r(num(6)+i,n)=residue(i)
50 continue
52 continue

c
c dissociation equation for water
c
  if (num(4).eq.0) go to 58

c
c mass actions equations for formation of complexes in the aqueous
c phase
c
  do 56 i=1,m4
    cm=eqconst(num(12)+i,n)
    do 54 j=1,m1
      if (s(j,i).eq.0) go to 54
      cm=cm*(ac(j,n)*cn(nstart+j))**s(j,i)
54 continue

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algebrc.31
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algebrc.89
algebrc.90

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56 r(num(7)+i,n)=ac(num(1)+i,n)*cn(nstart+num(7)+i)-cm
58 continue
   if (num(5).eq.0) go to 170
c
c  solubility product equations for the formations of precipitates
c
   do 168 i=1,m5
   kk=nstart+num(8)+i
   kn=num(8)+i
   if( tpcode.eq.0.0 ) go to 150
   if(kcode(kn).eq.0) go to 150
   if(rate(kn).eq.0.or.k1.eq.1) go to 150
   r(kn,n)=ddelx*rate(kn)+(cn(kk)-co(kk))/delt
c-----watch this when having different mass productions-----
   if(xdiag(i).eq.xkinet(5)) r(kn,n)=rate(kn)+(cn(kk)-co(kk))/delt
   go to 168
150 continue
   aksol=1.0
   do 162 j=1,m1
   if (ss(j,i).lt.1.e-15) go to 162
   aksol=aksol*(ac(j,n)*cn(nstart+j))*ss(j,i)
162 continue
   if( jacob.eq.0) q(i,n)=aksol
   r(kn,n)=aksol-eqconst(num(12)+num(4)+i,n)
   if(cn(kk).lt.1.0e-20.and.r(kn,n).lt.0.) r(kn,n)=cn(kk)

168 continue
170 continue
200 continue
   return
   end
   subroutine srate(n,num,co,cn,ac,neven,delt,kp)
c *****
c This subroutine calculates the rate equations for the reversible
c Calcite and Silica dissolutions according to equations proposed
c by Plummer et al (1978) and Rimstidt and Barnes (1980). Also,
c imperical Glass dissolution rates suggested by Claassen and
c White, (1979) are calculated here.
c *****
   common/crate/rate(50),kcode(25),inx1(5,25),inx2(5,25),cdat(5,25),
   1 reactsk(5,10,100),nsrt(5),sarea(5),nparam(5),xkinet(5),xmax,time,
   2 gc,excode,tpcode,kinr,xdiag(5),shift(4,100),shftsol(100)
   common/oxred/lno,lnh
   dimension num(1),co(1),cn(1),ac(75,1),rsk(25)

c
   ii=1
   if( kp.eq.1 ) go to 200
c *****
c kinetic rate calculation for non-rev. silica dissolution
c *****
c
100 if( excode.ne.1.0 ) go to 300
   phyd=-alog10(cn(neven+2))
   phydo=-alog10(co(neven+2))
   ddtph=(phyd-phydo)/delt
   cddtph=2.3*(time)**(0.5)*ddtph
   xlna=-0.17*(phyd-5.75)-13.73
   xlna=10.0**(xlna)
   xlk=-14.54
   xlk=10.0**(xlna)

```

```

algebrc.91
algebrc.92
algebrc.93
algebrc.94
algebrc.95
algebrc.96
algebrc.97
algebrc.98
algebrc.99
algebrc.100
algebrc.101
algebrc.102
algebrc.103
algebrc.104
algebrc.105
algebrc.106
algebrc.107
algebrc.108
algebrc.109
algebrc.110
algebrc.111
algebrc.112
algebrc.113
algebrc.114
algebrc.115
algebrc.116
algebrc.117
algebrc.118
algebrc.119
algebrc.120
algebrc.121
srate.2
srate.3
srate.4
srate.5
srate.6
srate.7
srate.8
srate.9
/crate/.2
/crate/.3
/crate/.4
/oxred/.2
srate.12
srate.13
srate.14
srate.15
srate.16
srate.17
srate.18
srate.19
srate.20
srate.21
srate.22
srate.23
srate.24
srate.25
srate.26
srate.27
srate.28

```

```

xlca=-0.50*(phyd-6.25)-14.15
xlca=10.0**(xlca)
xlmg=-0.4*(phyd-5.25)-13.88
xlmg=10.0**(xlmg)
c the unit of sigma is per liter which may be wrong!
c assign rate to designated species
sigma=sarea(kinr)
rate(1)=-sigma*xlna*(0.5*(time)**(-0.5)-0.17*cddtph)
rate(3)=-sigma*xlk*(0.5*(time)**(-0.5))
rate(4)=-2.0*sigma*xlca*(0.5*(time)**(-0.5)-0.5*cddtph)
rate(5)=-2.0*sigma*xlmg*(0.5*(time)**(-0.5)-0.4*cddtph)
rate(2)=-(rate(1)+rate(3)+rate(4)+rate(5))
go to 300
c *****
c kinetic rate calculation for rev. carbonate dissolution
c *****
200 if(xdiag(ii).ne.xkinet(4)) go to 250
c-----assign data
c
skp=10.0**(-cdat(ii,1) )
bk1=10.0**(-cdat(ii,2) )
bk2=10.0**(-cdat(ii,3) )
bkc=10.0**(-cdat(ii,4) )
tfactor= (+cdat(ii,5) )
xrate=0.0
c-----calculate reaction constant
c
do 150 i=1,nsrt(ii)
if( reactsk(ii,i,n).ne.1.0 ) go to 155
ni2=inx1(ii,2)
ni4=inx1(ii,4)
c-----calculate back reaction const.in the last rate term
ahs=( bk1*bk2*ac(ni4,n)*cn(neven+ni4)*ac(ni2,n)*
1 cn(neven+ni2)/bkc)**0.5
fiahs=( rsk(2)*ac(ni2,n)*cn(neven+ni2)+rsk(3) )/ahs+ skp
rsk(i)=-bk2*fiahs/bkc
go to 171
155 rsk(i)=( +reactsk(ii,i,n) )
c-----calculate rate according to the formula
171 ccn1=1.0
ccn2=1.0
in1=inx1(ii,i)
in2=inx2(ii,i)
if( in1.ne.0 ) ccn1=ac(in1,n)*cn(neven+in1)
if( in2.ne.0 ) ccn2=ac(in2,n)*cn(neven+in2)
xrate=xrate+rsk(i)*ccn1*ccn2
150 continue
c assign rate to designated precipitant replacing its m-action
rate(num(8)+ii)=tfactor*sarea(ii)*xrate
ii=ii+1
c *****
c kinetic rate calculation fo rev. silica dissolution
c *****
250 continue
coef=1.0
xrate=0.0
if( xdiag(ii).ne.xkinet(5) ) go to 300
c
do 10 i=1,nsrt(ii)
if(inx1(ii,i).lt.0.or.inx2(ii,i).lt.0) coef=-1.0

```

```

srate.29
srate.30
srate.31
srate.32
srate.33
srate.34
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srate.36
srate.37
srate.38
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srate.74
srate.75
srate.76
srate.77
srate.78
srate.79
srate.80
srate.81
srate.82
srate.83
srate.84
srate.85
srate.86
srate.87
srate.88

```



```

ccn1=1.0
ccn2=1.0
in1=iabs(inx1(ii,i))
in2=iabs(inx2(ii,i))
if(in1.ne.0) ccn1=cn(neven+in1)
if(in2.ne.0) ccn2=cn(neven+in2)
rsk(i)=(+reactsk(ii,i,n) )
xrate=xrate+coef*rsk(i)*ccn1*ccn2
10 continue
c assign rate to designated precipitate
rate(num(8)+ii)=+sarea(ii)*xrate
400 format(5e12.4)
300 continue
return
end
subroutine jacobi(a,b,c,co,cn,bc,bc2,num,ro,mdim,lnh,ibnd,itpe,
1 tpcode,kcode)
c
c *****
c calculation of the jacobian which is the change in the residues
c of the transport equations, site constraint equation and the
c mass action equations for a change in the concentrations. this subro
c considers the residues for the time dependent equations
c it is called from the main program chemtrn only
c *****
dimension ro(mdim,1),cn(1),co(1),cno(100),bc(1),num(1),ibnd(1)
dimension a(mdim,mdim,1),b(mdim,mdim,1),c(mdim,mdim,1),bc2(1)
dimension kcode(1)
common/ab/vj(75),ac(75,100),eqconst(25,100),h2ok(100),alfa(4,100),
1s(25,25),ss(25,25),ah(25),h2oc(8),con(25,8),conk(20,8),conp(4,2),
2 ilbli(25),ilble(25),q(10,100)
common/const/rel,absv
common/lcm3/rn(25,100)
c
ntot=num(9)
nmax=num(14)
do 50 k=1,3
do 50 j=1,ntot
do 30 n=k,nmax,3
cno(n)=cn((n-1)*ntot+j)
30 cn((n-1)*ntot+j)=cn((n-1)*ntot+j)*(1.+rel)+absv
call res(cn,co,bc,bc2,rn,num,mdim,lnh,ibnd,itpe,1)
do 45 n=k,nmax,3
do 40 i=1,ntot
kk=(n-1)*ntot+i
if(i.le.num(8)) go to 33
if(tpcode.eq.1.0.and.kcode(i).ne.0) go to 33
b(i,j,n-1)=0.0
a(i,j,n) =0.0
c(i,j,n+1)=0.0
if(j.gt.i) go to 40
kp=i-num(8)
ip=num(12)+num(4)+kp
if(i.eq.j) go to 32
if((q(kp,n).le.eqconst(ip,n)).and.(cn(kk).le.1.e-20)) go to 40
a(i,j,n)=(rn(i,n)-ro(i,n))/(cn((n-1)*ntot+j)-cno(n))
go to 40
32 continue
if((q(kp,n).gt.eqconst(ip,n)).or.(cno(n).gt.1.e-20))go to 34
a(i,j,n)=1.0

```

```

srate.89
srate.90
srate.91
srate.92
srate.93
srate.94
srate.95
srate.96
srate.97
srate.98
srate.99
srate.100
srate.101
srate.102
srate.103
jacobi.2
jacobi.3
jacobi.4
jacobi.5
jacobi.6
jacobi.7
jacobi.8
jacobi.9
jacobi.10
jacobi.11
jacobi.12
jacobi.13
jacobi.14
/ab/.2
/ab/.3
/ab/.4
/const/.2
/lcm3/.2
jacobi.18
jacobi.19
jacobi.20
jacobi.21
jacobi.22
jacobi.23
jacobi.24
jacobi.25
jacobi.26
jacobi.27
jacobi.28
jacobi.29
jacobi.30
jacobi.31
jacobi.32
jacobi.33
jacobi.34
jacobi.35
jacobi.36
jacobi.37
jacobi.38
jacobi.39
jacobi.40
jacobi.41
jacobi.42
jacobi.43
jacobi.44

```

```

34 if(n.eq.1.and.ibnd(1).eq.0.) a(i,i,1)=1.0
   if(n.eq.nmax.and.ibnd(2).eq.0.) a(i,i,nmax)=1.0
   go to 40
33 continue
   if (n.eq.1) c(i,j,1)=0.
   if (n.lt.2) go to 35
   b(i,j,n-1)=(rn(i,n-1)-ro(i,n-1))/(cn((n-1)*ntot+j)-
1cno(n))
35 a(i,j,n)=(rn(i,n)-ro(i,n))/(cn((n-1)*ntot+j)-
1cno(n))
   if(n.eq.1.and.ibnd(1).eq.0.) a(i,i,1)=1.0
   if (n.eq.nmax) b(i,j,n)=0.
   if(n.eq.nmax.and.ibnd(2).eq.0.) a(i,i,nmax)=1.0
   if (n.eq.nmax) go to 40
   c(i,j,n+1)=(rn(i,n+1)-ro(i,n+1))/(cn((n-1)*ntot+j)-cno(n))
40 continue
   cn((n-1)*ntot+j)=cno(n)
45 continue
50 continue
   return
   end
   subroutine jacob2(z,cm,wconst,index1,index2,re,num,n,ctot,nsol,
c
1lchrg,lnh,mdim)
c *****
c calculation of the jacobian done for the calculation of the
c equilibrium conditions; it is called from the subroutine eqlib only
c *****
   dimension re(1),ren(25),cm(1),wconst(1),index1(1),
1z(25,25),index2(1),num(1)
   common/ab/vj(75),ac(75,100),eqconst(25,100),h2ok(100),alfa(4,100),
1s(25,25),ss(25,25),ah(25),h2oc(8),con(25,8),conk(20,8),conp(4,2),
2 ilbli(25),ilble(25),q(10,100)
   common/const/rel,absv
c
   ntot=num(9)
   do 15 j=1,ntot
   cold=cm(j)
   cm(j)=cm(j)*(1.+rel)+absv
   call reseq(wconst,cm,index1,index2,ren,n,ctot,mdim,
1 num,lchrg,lnh,nsol,1)
   do 20 i=1,ntot
   if(i.le.num(8)) go to 13
   z(i,j)=0.0
   if(j.gt.i) go to 20
   kp=i-num(8)
   ip=num(12)+num(4)+kp
   if(i.eq.j) go to 12
   if((q(kp,n).le.eqconst(ip,n)).and.cm(i).le.1.e-20) go to 20
   z(i,j)=(ren(i)-re(i))/(cm(j)-cold)
   go to 20
12 continue
   if((q(kp,n).gt.eqconst(ip,n)).or.cold.gt.1.e-20)go to 20
   z(i,j)=1.0
   go to 20
13 continue
   z(i,j)=(ren(i)-re(i))/(cm(j)-cold)
20 continue
   cm(j)=cold
15 continue
jacob1.45
jacob1.46
jacob1.47
jacob1.48
jacob1.49
jacob1.50
jacob1.51
jacob1.52
jacob1.53
jacob1.54
jacob1.55
jacob1.56
jacob1.57
jacob1.58
jacob1.59
jacob1.60
jacob1.61
jacob1.62
jacob1.63
jacob1.64
jacob1.65
jacob2.2
jacob2.3
jacob2.4
jacob2.5
jacob2.6
jacob2.7
jacob2.8
jacob2.9
jacob2.10
/ab/.2
/ab/.3
/ab/.4
/const/.2
jacob2.13
jacob2.14
jacob2.15
jacob2.16
jacob2.17
jacob2.18
jacob2.19
jacob2.20
jacob2.21
jacob2.22
jacob2.23
jacob2.24
jacob2.25
jacob2.26
jacob2.27
jacob2.28
jacob2.29
jacob2.30
jacob2.31
jacob2.32
jacob2.33
jacob2.34
jacob2.35
jacob2.36
jacob2.37
jacob2.38

```

```

return
end
subroutine reseq(wconst,cm,index1,index2,re,n,ctot,mdim,
c
1 num,lchrg,lnh,nsol,jcob)
c *****
c residues of the equilibrium equations; it is called from
c the subroutines eqlib and jacob2
c *****
c dimension wconst(1),cm(1),index1(1),index2(1),re(1),num(1)
c common/ac/elconc(100)
c common/lcm1/r(25,100)
c common/ab/vj(75),ac(75,100),eqconst(25,100),h2ok(100),alfa(4,100),
1s(25,25),ss(25,25),ah(25),h2oc(8),con(25,8),conk(20,8),comp(4,2),
2 ilbli(25),ilble(25),q(10,100)
c common/nj/isorpi(30),isorpe(30),iion,ieion
c common/ad/x(200),delt,doa,dob,vo,cecn
c common/spec/leach1(5),nb,pini(5)
c ntot=num(8)
c ii=0
c ie=3
c m1=num(1)
c m4=num(4)
c m5=num(5)
c m2=num(2)
c m3=num(3)
c
c calculate the activities of the species in the aqueous phase
c
c call active(num,cm,vj,ac,elconc,75,n,n)
c
c the first set of equations are setting the conditions to what
c were specified for each species;
c
26 do 60 j=1,m1
r(j,n)=wconst(j)-cm(j)
if (isorpi(j).eq.0) go to 30
ii=ii+1
c
c if index2 .ne. 0 then the amount of the species which is sorbed
c onto the solid matrix is not included in the specified amount of
c this species
c
if (index2(j).ne.0) go to 30
r(j,n)=r(j,n)-cm(num(1)+ii)
30 continue
if (isorpe(j).eq.0) go to 35
ie=ie+1
iej=ie
if (j.eq.lnh) iej=3
if (j.eq.lnh) ie=ie-1
if (index2(j).ne.0) go to 35
r(j,n)=r(j,n)-cm(num(6)+iej)
if (j.eq.lnh) r(j,n)=r(j,n)-2*cm(num(6)+2)
35 continue
if (num(4).eq.0) go to 41
icmplx=iion
iecmplx=ieion
c
c if index2 = 1 then only the concentration of the basis species

```

```

jacob2.39
jacob2.40
reseq.2
reseq.3
reseq.4
reseq.5
reseq.6
reseq.7
reseq.8
reseq.9
reseq.10
/lcm1/.2
/ab/.2
/ab/.3
/ab/.4
/nj/.2
/ad/.2
/spec/.2
reseq.16
reseq.17
reseq.18
reseq.19
reseq.20
reseq.21
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reseq.52
reseq.53
reseq.54
reseq.55
reseq.56
reseq.57

```

```

c itself is being given for this species
c
  if (index2(j).eq.1) go to 41
  do 40 i=1,m4
  kk=i+num(1)
  if (isorpi(kk).eq.0) go to 37
  icmplx=icmplx+1
  if (index2(j).ne.0) go to 37
  r(j,n)=r(j,n)-s(j,i)*cm(num(1)+icmplx)
37 continue
  if (isorpe(kk).eq.0) go to 38
  iecmplx=iecmplx+1
  if (index2(j).ne.0) go to 38
  r(j,n)=r(j,n)-s(j,i)*cm(num(6)+iecmplx)
38 continue
40 r(j,n)=r(j,n)-s(j,i)*cm(num(7)+i)
41 if (num(5).eq.0) go to 60
c
c index2 must = 3 for the concentration of the precipitate
c to be included in the specification of that species; however
c if the species may form in a precipitate, than index2 =3 instead
c of index2 = 2 should be used because of the way the equations are
c set up at present
c
  if ((index2(j).eq.1).or.(index2(j).eq.2)) go to 60
  do 50 i=1,m5
  50 r(j,n)=r(j,n)-index1(i)*ss(j,i)*cm(num(8)+i)
1000 format (10x,i5,10x,10(4(1p12.4)),/)
60 continue
  if (lnh.eq.0) go to 72
c
c the dissociation of water is included if it has been specified
c
  r(num(1),n)=h2ok(n)-cm(lnh)*ac(lnh,n)*cm(num(1))*ac(num(1),n)
72 continue
c
c it is possible to use a charge balance to specify one of the
c concentrations
c
  if (lchrg.eq.0) go to 77
  r(lchrg,n)=ctot
  do 75 j=1,m1
75 r(lchrg,n)=r(lchrg,n)-cm(j)*vj(j)
  if (num(4).eq.0) go to 77
  do 78 i=1,m4
76 r(lchrg,n)=r(lchrg,n)-cm(num(7)+i)*vj(num(1)+i)
c
c this is for a special condition of leaching of a solid so that
c the increase in the amount of the species in the aqueous phase
c making up the solid is in equal amounts; occurs where a solid has
c been placed in contact with the groundwater. it can only occur
c at the first node at present
c
77 if ((n.ne.nb).or.(leach1(1).eq.0)) go to 80
  r(leach1(2),n)=wconst(leach1(2))-cm(num(8)+leach1(1))
  index1(leach1(1))=1
  ileach=3
  j1=leach1(2)+1
  do 78 j=j1,m1
  if (j.ne.leach1(ileach)) go to 78

```

```

reseq.58
reseq.59
reseq.60
reseq.61
reseq.62
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reseq.115
reseq.116
reseq.117

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```

      r(leach1(ileach),n)=wconst(leach1(ileach))-r(leach1(ileach),n)-
      1 pini(ileach-1)-(wconst(leach1(2))-r(leach1(2),n)-
      2 pini(1))
      ileach=ileach+1
      78 continue
      80 continue
c
c calculation of the residues of the site constraint, and the
c mass action equations for sorption and formation of complexes
c in the aqueous phase
c
c-----caution for transferring cm to fill co in agebrc-----
      call agebrc(num,cm,cm,r,n,n,25,elconc,lnh,1,jcob)
c
      if (num(5).eq.0) go to 90
c
c for any precipitates, include the residues for the solubility product
c equations
c
      call ressol(index1,cm,num,ntot,r,n,mdim)
      90 nnn=ntot+nsol
      do 100 i=1,nnn
      100 re(i)= r(i,n)
      return
      end
      subroutine ressol(index1,cm,num,ntot,r,n,mdim)
c
c *****
c residues for the solubility constraint equations; it is
c only used for the initial equilibrium distribution of species
c calculation; the subroutine res also has the solubility
c product equations for the time changes at the nodes after
c a precipitate has formed
c *****
      dimension cm(1),index1(1),r(mdim,1),num(12)
      common/ab/vj(75),ac(75,100),eqconst(25,100),h2ok(100),alfa(4,100),
      1s(25,25),ss(25,25),ah(25),h2oc(8),con(25,8),conk(20,8),comp(4,2),
      2 ilbli(25),ilble(25),q(10,100)
      index=0
      m5=num(5)
      m1=num(1)
      do 10 i=1,m5
      aksol=1.
      if (index1(i).eq.0) go to 10
      index=index+1
      do 20 j=1,m1
      if (ss(j,i).lt.1.e-15) go to 20
      aksol=aksol*(ac(j,n)*cm(j))*ss(j,i)
      20 continue
      r(ntot+index,n)=aksol-eqconst(num(12)+num(4)+i,n)
      print 100,r(ntot+index,n),aksol,eqconst(num(12)+num(4)+i,n)
      100 format(3e12.4)
      10 continue
      return
      end
      subroutine redl(conc,residue,np,n,elconc,lnh,num)
c
c *****
c calculates the residues for the mass action equations, and a site
c constraint equation for the surface complexation model for sorption;

```

```

      reseq.118
      reseq.119
      reseq.120
      reseq.121
      reseq.122
      reseq.123
      reseq.124
      reseq.125
      reseq.126
      reseq.127
      reseq.128
      reseq.129
      reseq.130
      reseq.131
      reseq.132
      reseq.133
      reseq.134
      reseq.135
      reseq.136
      reseq.137
      reseq.138
      reseq.139
      reseq.140
      reseq.141
      reseq.142
      ressol.2
      ressol.3
      ressol.4
      ressol.5
      ressol.6
      ressol.7
      ressol.8
      ressol.9
      ressol.10
      ressol.11
      /ab/.2
      /ab/.3
      /ab/.4
      ressol.13
      ressol.14
      ressol.15
      ressol.16
      ressol.17
      ressol.18
      ressol.19
      ressol.20
      ressol.21
      ressol.22
      ressol.23
      ressol.24
      ressol.25
      ressol.26
      ressol.27
      ressol.28
      ressol.29
      redl.2
      redl.3
      redl.4
      redl.5
      redl.6

```

```

c the actual surface complexation model is described in
c detail in the paper by j.a. davis, r.o. james, and j.o. leckie
c in j. colloid and interface science, vol 63, no. 3, march, 1978
c *****
c dimension conc(1),residue(1),num(1)
c common/ab/vj(75),ac(75,100),eqconst(25,100),h2ok(100),alfa(4,100),
c 1s(25,25),ss(25,25),ah(25),h2oc(8),con(25,8),conk(20,8),comp(4,2),
c 2 ilbli(25),ible(25),q(10,100)
c common/edl/c1,c2,area,soh
c common/edl2/sigo,sigb,sigd,psio,psibeta,psid
c data elec/1.602e-19/, avogad/6.025e23/, boltz/1.38e-23/
c data dielec/78.84/
c data temp/298.15/,faraday/9.6487e4/,epsil/8.85e-12/
c arcsinh(x)=alog(x+sqrt(x*x+1))
c kk=num(6)
c m3=num(3)
c
c calculate the charge developed at the surface (sigo) and
c the beta plane (sigb) for the given concentration of sorbed
c species
c
c sigo=conc(kk+2+np)-conc(kk+1+np)
c sigb=0.
c if (num(3).eq.3) go to 115
c do 110 i=4,m3
c jj=ible(i)
c if (jj.gt.num(1)) jj=jj-num(12)
c sigo=sigo - ah(i)*conc(kk+i+np)
c sigb=sigb+vj(jj)*conc(kk+i+np)
c 110 continue
c 115 continue
c 1000 format (4x,5(1pe12.4))
c sigo=sigo*1.e6*faraday/area
c sigb=sigb*1.e6*faraday/area
c sigd=-sigo-sigb
c a1=arcsinh(abs(sigd)/(8.*avogad*epsil*boltz*
c 1dielec*temp*1.e7*elconc)**0.5)
c
c calculate the potentials developed between the surface plane, beta
c plane, diffuse plane, and the bulk solution
c
c psid=-(sigd/abs(sigd))*(2.*boltz*temp/elec)*a1
c psibeta=psid-sigd/c2
c psio=psibeta+sigo/c1
c aconst=elec/(boltz*temp)
c surpln=exp(-aconst*psio)
c betapln=exp(-aconst*psibeta)
c
c site constraint equation for all the sites (soh, soh-, soh2+)
c
c residue(1)=soh-conc(kk+1+np)-conc(kk+2+np)-conc(kk+3+np)
c if (num(3).lt.4) go to 120
c do 125 i=4,m3
c residue(1)=residue(1)-conc(kk+i+np)
c 125 continue
c 120 continue
c
c mass action equation describing the dissociation of soh2+ site
c
c residue(2)=eqconst(num(2)+1,n)*conc(kk+2+np)/surpln-conc(kk+3+np)*

```

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redl.7
redl.8
redl.9
redl.10
redl.11
/ab/.2
/ab/.3
/ab/.4
/edl/.2
/edl2/.2
redl.15
redl.16
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redl.60
redl.61
redl.62
redl.63
redl.64

```

```

c      lconc(lnh+np)
c      mass action equation describing the dissociation of the soh site
c      residue(3)=eqconst(num(2)+2,n)*conc(kk+3+np)/surpln-conc(kk+1+np)*
      lconc(lnh+np)
      if (num(3).lt.4) go to 126
c      mass action equations for the formation of sites (so-species) or
c      (soh2+ -species)
c
      do 127 i=4,m3
      jj=ilble(i)
      j2=jj
      if (jj.gt.num(1)) j2=jj-num(12)
      quan=conc(kk+i+np)*(conc(lnh+np)*surpln)**ah(i)
      denom=conc(jj+np)*conc(kk+3+np)*betapln**vj(j2)
      residue(i)=(denom)-quan/eqconst(num(2)+i,n)
127 continue
126 continue
      return
      end
      subroutine decbt(m,n,mdim,a,b,c,ip,ier)
c
c      *****
c      this set of four subroutines are to invert the block tri-diagonal
c      matrix to get the new guesses for the concentrations. the
c      subroutines involved here are decbt, dec, sol, and solbt and were
c      written by a.c. hindmarsh of lawrence livermore laboratory. these
c      subroutines are covered in a separate document ucid-30150
c      "solution of block-tridiagonal systems of linear algebraic equations
c      *****
      integer m,n,mdim,ip(mdim,n),ier
      dimension a(mdim,mdim,n),b(mdim,mdim,n),c(mdim,mdim,n)
      real dp
      if (m .lt. 1 .or. n .lt. 4) go to 210
      nm1 = n - 1
      nm2 = n - 2
      call dec(m,mdim,a,ip,ier)
      k = 1
      if (ier .ne. 0) go to 200
      do 10 j = 1,m
      call sol(m,mdim,a,b(1,j,1),ip)
      call sol(m,mdim,a,c(1,j,1),ip)
10      continue
      do 40 j = 1,m
      do 30 i = 1,m
      dp = 0.
      do 20 l = 1,m
      dp = dp + c(i,l,2)*c(l,j,1)
20      b(i,j,2) = b(i,j,2) - dp
30      continue
40      continue
      do 100 k = 2,nm1
      km1 = k - 1
      do 70 j = 1,m
      do 60 i = 1,m
      dp = 0.
      do 50 l = 1,m
50      dp = dp + c(i,l,k)*b(l,j,km1)

```

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redl.65
redl.66
redl.67
redl.68
redl.69
redl.70
redl.71
redl.72
redl.73
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redl.76
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redl.79
redl.80
redl.81
redl.82
redl.83
redl.84
redl.85
redl.86
decbt.2
decbt.3
decbt.4
decbt.5
decbt.6
decbt.7
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decbt.37
decbt.38
decbt.39

```

	a(i,j,k) = a(i,j,k) - dp	decbt.40
60	continue	decbt.41
70	continue	decbt.42
	call dec(m,mdim,a(1,1,k),ip(1,k),ier)	decbt.43
	if (ier .ne. 0) go to 200	decbt.44
	do 80 j = 1,m	decbt.45
80	call sol(m,mdim,a(1,1,k),b(1,j,k),ip(1,k))	decbt.46
100	continue	decbt.47
	do 130 j = 1,m	decbt.48
	do 120 i = 1,m	decbt.49
	dp = 0.	decbt.50
	do 110 l = 1,m	decbt.51
110	dp = dp + b(i,l,n)*b(l,j,nm2)	decbt.52
	c(i,j,n) = c(i,j,n) - dp	decbt.53
120	continue	decbt.54
130	continue	decbt.55
	do 160 j = 1,m	decbt.56
	do 150 i = 1,m	decbt.57
	dp = 0.	decbt.58
	do 140 l = 1,m	decbt.59
140	dp = dp + c(i,l,n)*b(l,j,nm1)	decbt.60
	a(i,j,n) = a(i,j,n) - dp	decbt.61
150	continue	decbt.62
160	continue	decbt.63
	call dec(m,mdim,a(1,1,n),ip(1,n),ier)	decbt.64
	k = n	decbt.65
	if (ier .ne. 0) go to 200	decbt.66
	return	decbt.67
200	ier = k	decbt.68
	return	decbt.69
210	ier = -1	decbt.70
	return	decbt.71
	end	decbt.72
	subroutine solbt(m,n,mdim,a,b,c,y,ip)	solbt.2
c	dimension y(mdim,n)	solbt.3
	integer m,n,ip(mdim,n),mdim	solbt.4
	dimension a(mdim,mdim,n),b(mdim,mdim,n),c(mdim,mdim,n)	solbt.5
	real dp	solbt.6
	nm1 = n - 1	solbt.7
	nm2 = n - 2	solbt.8
	call sol(m,mdim,a,y,ip)	solbt.9
	do 30 k = 2,nm1	solbt.10
	km1 = k - 1	solbt.11
	do 20 i = 1,m	solbt.12
	dp = 0.	solbt.13
	do 10 j = 1,m	solbt.14
10	dp = dp + c(i,j,k)*y(j,km1)	solbt.15
	y(i,k) = y(i,k) - dp	solbt.16
20	continue	solbt.17
	call sol(m,mdim,a(1,1,k),y(1,k),ip(1,k))	solbt.18
30	continue	solbt.19
	do 50 i = 1,m	solbt.20
	dp = 0.	solbt.21
	do 40 j = 1,m	solbt.22
40	dp = dp + c(i,j,n)*y(j,nm1) + b(i,j,n)*y(j,nm2)	solbt.23
	y(i,n) = y(i,n) - dp	solbt.24
50	continue	solbt.25
	call sol(m,mdim,a(1,1,n),y(1,n),ip(1,n))	solbt.26
	do 80 kb = 1,nm1	solbt.27
		solbt.28


```

        k = n - kb
        kp1 = k + 1
        do 70 i = 1,m
            dp = 0.
            do 60 j = 1,m
                60 dp = dp + b(i,j,k)*y(j,kp1)
                y(i,k) = y(i,k) - dp
            70 continue
        80 continue
        do 100 i = 1,m
            dp = 0.
            do 90 j = 1,m
                90 dp = dp + c(i,j,1)*y(j,3)
                y(i,1) = y(i,1) - dp
            100 continue
        return
    end
    subroutine dec (n, ndim, a, ip, ier)
c
        dimension ip(n)
        dimension a(ndim,n)
        ier = 0
        ip(n) = 1
        if (n .eq. 1) go to 70
        nml = n - 1
        do 60 k = 1,nml
            kp1 = k + 1
            m = k
            do 10 i = kp1,n
                10 if (abs(a(i,k)) .gt. abs(a(m,k))) m = i
                ip(k) = m
                t = a(m,k)
                if (m .eq. k) go to 20
                ip(n) = -ip(n)
                a(m,k) = a(k,k)
                a(k,k) = t
            20 if (t .eq. 0.) go to 80
                t = 1./t
                do 30 i = kp1,n
                    30 a(i,k) = -a(i,k)*t
                do 50 j = kp1,n
                    t = a(m,j)
                    a(m,j) = a(k,j)
                    a(k,j) = t
                    if (t .eq. 0.) go to 50
                do 40 i = kp1,n
                    40 a(i,j) = a(i,j) + a(i,k)*t
            50 continue
        60 continue
        70 k = n
            if (a(n,n) .eq. 0.) go to 80
            return
        80 ier = k
            ip(n) = 0
            return
        end
        subroutine sol (n, ndim, a, b, ip)
c
        dimension b(n), ip(n), a(ndim,n)
        if (n .eq. 1) go to 50
        solbt.29
        solbt.30
        solbt.31
        solbt.32
        solbt.33
        solbt.34
        solbt.35
        solbt.36
        solbt.37
        solbt.38
        solbt.39
        solbt.40
        solbt.41
        solbt.42
        solbt.43
        solbt.44
        solbt.45
        dec.2
        dec.3
        dec.4
        dec.5
        dec.6
        dec.7
        dec.8
        dec.9
        dec.10
        dec.11
        dec.12
        dec.13
        dec.14
        dec.15
        dec.16
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        dec.18
        dec.19
        dec.20
        dec.21
        dec.22
        dec.23
        dec.24
        dec.25
        dec.26
        dec.27
        dec.28
        dec.29
        dec.30
        dec.31
        dec.32
        dec.33
        dec.34
        dec.35
        dec.36
        dec.37
        dec.38
        dec.39
        dec.40
        sol.2
        sol.3
        sol.4
        sol.5

```

```

nml = n - 1
do 20 k = 1,nml
  kpl = k + 1
  m = ip(k)
  t = b(m)
  b(m) = b(k)
  b(k) = t
  do 10 i = kpl,n
10    b(i) = b(i) + a(i,k)*t
20    continue
do 40 kb = 1,nml
  km1 = n - kb
  k = km1 + 1
  b(k) = b(k)/a(k,k)
  t = -b(k)
  do 30 i = 1,km1
30    b(i) = b(i) + a(i,k)*t
40    continue
50    b(1) = b(1)/a(1,1)
return
end
subroutine shiftb(cm,num,alfa,shiftr)
c
c *****
c this routine is only called to calculate the initial condition
cc of recharging groundwater. only used in static mode.
c *****
c dimension cm(25),num(1),alfa(4,100)
c
c calculate del0,del1,del2,del3
c
shift1=alfa(1,1)*shiftr+1000.0*(alfa(1,1)-1.0)
shift2=alfa(2,1)*shiftr+1000.0*(alfa(2,1)-1.0)
shift3=alfa(3,1)*shiftr+1000.0*(alfa(3,1)-1.0)
shift4=alfa(4,1)*shiftr+1000.0*(alfa(4,1)-1.0)
cm1=cm(num(7)+1)
cm2=cm(num(7)+2)
cm3=cm(num(7)+3)
xmc=cm1+cm2+cm3
write(6,400)
print 500, (alfa(i,1), i=1,4)
print 600,shiftr, cm1, cm2, cm3
shftsol=( cm1*shift1+cm2*shift2+cm3*shift3 )/xmc
print 700, xmc,shftsol,shift1,shift2,shift3,shift4
400 format(//,'** Recharge water stable isotope characteristics **')
500 format(/'Alfa(1) = 'e12.4,5x,'Alfa(2) = 'e12.4,5x,'Alfa(3) = '
1 e12.4,5x,'Alfa(4) = 'e12.4)
600 format(/'shiftr = 'e12.3,5x,'H2CO3 = 'e12.3,5x,'HCO3- = '
1 e12.3,5x,'CO3-- = 'e12.3)
700 format(/'xmc = 'e12.3,5x,'shftsol = 'e12.3,5x,'shift1 = 'e12.3,
1 5x,'shift2 = 'e12.3,5x,'shift3 = 'e12.3,5x,
2 'shifts = 'e12.3)
c
return
end
subroutine shiftc(cn,num,shftsol,shift,shiftr,shifts,
1 alfa,nmax,kcode )
c
c *****
c this subroutine calculate variations of del0,del1,del2,del3 as

```

```

sol.6
sol.7
sol.8
sol.9
sol.10
sol.11
sol.12
sol.13
sol.14
sol.15
sol.16
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sol.19
sol.20
sol.21
sol.22
sol.23
sol.24
sol.25
sol.26
shiftb.2
shiftb.3
shiftb.4
shiftb.5
shiftb.6
shiftb.7
shiftb.8
shiftb.9
shiftb.10
shiftb.11
shiftb.12
shiftb.13
shiftb.14
shiftb.15
shiftb.16
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shiftb.18
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shiftb.25
shiftb.26
shiftb.27
shiftb.28
shiftb.29
shiftb.30
shiftb.31
shiftb.32
shiftb.33
shiftb.34
shiftb.35
shiftc.2
shiftc.3
shiftc.4
shiftc.5
shiftc.6

```

```

c   the recharging groundwater dissolves the carbonate rocks.
c   *****
c   dimension cn(1),shftsol(1),shift(4,1),num(1),alfa(4,1)
c   dimension kcode(1)
c
c   do 100 n=1,nmax
c   nstart=(n-1)*num(9)
c   do 200 j=1,num(8)
c   if( kcode(j).le.30) go to 200
c   if( kcode(j).eq.31) xmco3=cn(nstart+j)
c   if( kcode(j).eq.32) xmki =cn(nstart+j)
c   if( kcode(j).eq.33) xmhco3=cn(nstart+j)
c   if( kcode(j).eq.34) xmh2co3=cn(nstart+j)
200 continue
c   cn3=xmco3
c   cn4=xmki
c   cnp=xmhco3
c   cnp1=xmh2co3
c   xmc=cn3+cnp+cnp1
c   shftsol(n)=shfts-cn4/xmc
c   alfr2=alfa(2,n)/alfa(1,n)
c   alfr3=alfa(3,n)/alfa(1,n)
c   rxmc=cnp+alfr2*cnp1+alfr3*cn3
c   shift(1,n)=(xmc*shftsol(n)-1000.0*(cnp1*(alfr2-1.)+cn3*(alfr3-1.
1  )))/rxmc
c   shift(2,n)=alfr2*shift(1,n)+1000.0*(alfr2-1.0)
c   shift(3,n)=alfr3*shift(1,n)+1000.0*(alfr3-1.0)
100 continue
c   return
c   end
c   subroutine eqcon(n1,n2,con,conk,h2oc,m15,kinr,lnh,tmp,h2ok,eqconst
1   ,nsrt,reactsk,alfa,conp,ipart,kt)
c
c   *****
c   subroutine calculates the kinetic dissolution constants of solids
c   ,C-13 partition constants,the dissociation of water constants,the
c   formation constants of aqueous complexes, and the solubility products
c   of solids at the temperature tmp. the constants are calculated from
c   expressions of the form
c
c           log k = c1 + c2/tk + c3*(log tk) + c4*tk
c
c   where tk = tmp + 273.15.
c   *****
c
c   implicit real*8 (a-h,o-z)
c   dimension con(25,8),h2oc(8),eqconst(25,100),h2ok(100),tmp(100),
1   conk(20,8),conp(4,2),alfa(4,100),reactsk(5,10,100),
2   nsrt(5)
c
c   do 40 node=n1,n2
c   tk=tmp(node)+273.15
c   if(kinr.eq.0) go to 20
c   if(kt.ne.1) go to 20
c   ktsum=0
c   do 12 i=1,kinr
c   do 11 j=1,nsrt(i)
c   l=j+ktsum
c   term=conk(l,1)+conk(l,2)/tk+conk(l,3)*alog10(tk)+conk(l,4)*tk

```

```

shiftc.7
shiftc.8
shiftc.9
shiftc.10
shiftc.11
shiftc.12
shiftc.13
shiftc.14
shiftc.15
shiftc.16
shiftc.17
shiftc.18
shiftc.19
shiftc.20
shiftc.21
shiftc.22
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shiftc.26
shiftc.27
shiftc.28
shiftc.29
shiftc.30
shiftc.31
shiftc.32
shiftc.33
shiftc.34
shiftc.35
shiftc.36
shiftc.37
eqcon.2
eqcon.3
eqcon.4
eqcon.5
eqcon.6
eqcon.7
eqcon.8
eqcon.9
eqcon.10
eqcon.11
eqcon.12
eqcon.13
eqcon.14
eqcon.15
eqcon.16
eqcon.17
eqcon.18
eqcon.19
eqcon.20
eqcon.21
eqcon.22
eqcon.23
eqcon.24
eqcon.25
eqcon.26
eqcon.27
eqcon.28
eqcon.29
eqcon.30

```

```

      reactsk(i,j,node)=10.**term
11  continue
      ktsum=ktsum+nsrt(i)
12  continue
c
20  continue
      if(ipart.eq.0) go to 18
      do 15 j=1,4
      term=conp(j,1)+conp(j,2)/(tk**2)
      alfa(j,node)=exp(term)
15  continue
c
18  continue
      if (lnh.eq.0) go to 13
      term=h2oc(1)+h2oc(2)/tk+h2oc(3)*alog10(tk)+h2oc(4)*tk
      h2ok(node)=10.**term
13  continue
      do 30 j=1,m15
      term=con(j,1)+con(j,2)/tk+con(j,3)*alog10(tk)+con(j,4)*tk
      eqconst(j,node)=10.**term
c      print 100, node, j, eqconst(j,node)
100 format(2i10,10x,e12.3)
30  continue
40  continue
      return
      end
c
      subroutine gradt(nmax,tempi,tempo,itype,x,tmp)
c
c *****
c this subroutine calculates the fixed temperature gradient when
c itemp = 2. steady-state expressions for diffusion of heat in 1-d
c and radial geometries with fixed temperatures at inner and outer
c boundaries are used.
c *****
c
      implicit real*8 (a-h,o-z)
      dimension x(101),tmp(101)
c
      xi=x(1)
      xo=x(nmax)
      dt=tempi-tempo
      tmp(1)=tempi
      tmp(nmax)=tempo
      if (itype.eq.1) const=alog(xo/xi)
      nm=nmax-1
      do 30 n=2,nm
      xx=x(n)
      if (itype.eq.1) go to 10
      xterm=xx/xo
      go to 20
10  xterm=(alog(xx/xi))/const
20  tmp(n)=tempo-dt*xterm
30  continue
      return
      end
c
      subroutine tmpcal(ibnd2,nmax,hcm,hcw,vo,tcm,doa,itype,tb,delt,x,
1tmpold,tmp)
c

```

```

eqcon.31
eqcon.32
eqcon.33
eqcon.34
eqcon.35
eqcon.36
eqcon.37
eqcon.38
eqcon.39
eqcon.40
eqcon.41
eqcon.42
eqcon.43
eqcon.44
eqcon.45
eqcon.46
eqcon.47
eqcon.48
eqcon.49
eqcon.50
eqcon.51
eqcon.52
eqcon.53
eqcon.54
eqcon.55
eqcon.56
eqcon.57
gradt.2
gradt.3
gradt.4
gradt.5
gradt.6
gradt.7
gradt.8
gradt.9
gradt.10
gradt.11
gradt.12
gradt.13
gradt.14
gradt.15
gradt.16
gradt.17
gradt.18
gradt.19
gradt.20
gradt.21
gradt.22
gradt.23
gradt.24
gradt.25
gradt.26
gradt.27
gradt.28
gradt.29
gradt.30
gradt.31
tmpcal.2
tmpcal.3
tmpcal.4

```

```

c *****
c this subroutine calculates the temperature at each node for each new
c time step, using the crank-nicholson method.
c it solves the tridiagonal system of equations (a)(tmp)=(f), where
c (a) is the coefficient matrix, by lu decomposition of (a) such that
c (l)(u)(tmp)=(f).
c if (a) has the structure
c
c      (aa1 cc1  0  ... ..)
c      (bb2 aa2 cc2  0  ... ..)
c      (  0  bb3 aa3 cc3  0  ...),
c      (... ..)
c      (... ..  0  bbn aan)
c
c then (l) has the structure
c
c      ( 1  0  ... ..)
c      (be2 1  0  ... ..)
c      (  0  be3 1  0  ... ..)
c      (... ..)
c      (... ..  0  ben 1)
c
c and (u) has the structure
c
c      (a11 cc1  0  ... ..)
c      (  0  a12 cc2  0  ... ..)
c      (...  0  a13 cc3  0  ...).
c      (... ..)
c      (... ..  0  ain)
c
c the forward process solves (l)(g)=(f) for vector (g).
c the backward process solves (u)(tmp)=(g) for the temperatures (tmp).
c the solution algorithm was furnished by Janet Remer.
c *****
c      implicit real*8 (a-h,o-z)
c      dimension aa(100),bb(100),cc(100),al(100),be(100),f(100),g(100),
c      1x(100),tmpold(100),tmp(100)
c
c calculate matrix of coefficients (a) and vector of knowns (f).
c
c      nm=nmax-1
c      hcmw=hcm+hcw
c      vv=vo*hcw/hcmw
c      dif=tcm/hcmw
c      av=vv*doa
c      cap=av+dif
c      vm=vv
c      vb=vv
c
c      inner boundary
c
c      x1=x(1)
c      x2=x(2)
c      x3=x(3)
c      x21=x2-x1
c      x31=x3-x1
c      x32=x3-x2
c      if (ibnd2.eq.1) go to 10
c      nin=2

```

```

tmpcal.5
tmpcal.6
tmpcal.7
tmpcal.8
tmpcal.9
tmpcal.10
tmpcal.11
tmpcal.12
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tmpcal.14
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tmpcal.58
tmpcal.59
tmpcal.60
tmpcal.61
tmpcal.62
tmpcal.63
tmpcal.64

```

```

      if (itype.eq.1) cap=dif+av/x2
      if (itype.eq.1) vm=(vv-dif)/x2
      t1=delt*(cap+vm*x32/2.)/(x31*x21)
      t2=delt*(cap*(1./x32+1./x21)+(vm/2.)*(x32/x21-x21/x32))/x31
      t3=delt*(cap-vm*x21/2.)/(x31*x32)
      aa(2)=1.+t2
      cc(2)=-t3
      f(2)=t1*tb+(1.-t2)*tmpold(2)+t1*tmpold(1)+t3*tmpold(3)
      go to 20
10  nin=1
      if (itype.eq.1) cap=dif+av/x1
      if (itype.eq.1) vm=(vv-dif)/x1
      if (itype.eq.1) vb=vv/x1
      aa(1)=1.+delt*(cap/(x21*x21)+vb/x21+vm*vb/(2.*cap))
      cc(1)=-cap*delt/(x21*x21)
      f(1)=tmpold(1)+(2.+vm*x21/cap)*vb*tb*delt/x21+cap*delt*(tmpold(2)-
1 tmpold(1))/(x21*x21)-(1.+vm*x21/(2.*cap))*vb*delt*tmpold(1)/x21
c
c   interior nodes
c
20  ninp=nin+1
      xn=x(nin)
      xp=x(ninp)
      do 30 n=ninp,nm
      xm=xn
      xn=xp
      xp=x(n+1)
      xnm=xn-xm
      xpm=xp-xm
      xpn=xp-xn
      if (itype.eq.1) cap=dif+av/xn
      if (itype.eq.1) vm=(vv-dif)/xn
      tm=delt*(cap+vm*xpn/2.)/(xpm*xnm)
      tn=delt*(cap*(1./xpn+1./xnm)+(vm/2.)*(xpn/xnm-xnm/xpn))/xpm
      tp=delt*(cap-vm*xnm/2.)/(xpm*xpn)
      bb(n)=-tm
      aa(n)=1.+tn
      cc(n)=-tp
      f(n)=tm*tmpold(n-1)+(1.-tn)*tmpold(n)+tp*tmpold(n+1)
      if (n.eq.nm) f(n)=f(n)+tp*tmpold(nmax)
30  continue
c
c   calculate decomposition matrices
c
      alk=aa(nin)
      al(nin)=alk
      do 40 k=ninp,nm
      bek=bb(k)/alk
      alk=aa(k)-bek*cc(k-1)
      al(k)=alk
      be(k)=bek
40  continue
c
c   forward substitution
c
      gi=f(nin)
      g(nin)=gi
      do 50 i=ninp,nm
      gi=f(i)-be(i)*gi
      g(i)=gi

```

```

tmpcal.65
tmpcal.66
tmpcal.67
tmpcal.68
tmpcal.69
tmpcal.70
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tmpcal.72
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tmpcal.117
tmpcal.118
tmpcal.119
tmpcal.120
tmpcal.121
tmpcal.122
tmpcal.123
tmpcal.124

```

```
50 continue
c
c backward substitution
c
  ti=g(nm)/al(nm)
  tmp(nm)=ti
  nmm=nm-nin
  do 60 j=1,nmm
    i=nm-j
    ti=(g(i)-cc(i)*ti)/al(i)
    tmp(i)=ti
60 continue
  return
  end
c
```

```
tmpcal.125
tmpcal.126
tmpcal.127
tmpcal.128
tmpcal.129
tmpcal.130
tmpcal.131
tmpcal.132
tmpcal.133
tmpcal.134
tmpcal.135
tmpcal.136
tmpcal.137
tmpcal.138
tmpcal.139
```

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