

# Lawrence Berkeley National Laboratory

## Lawrence Berkeley National Laboratory

**Title**

Accurate Iterative Analysis of the K-V Equations

**Permalink**

<https://escholarship.org/uc/item/1p86n3cj>

**Author**

Anderson, O.A.

**Publication Date**

2005-05-09

## ACCURATE ITERATIVE ANALYSIS OF THE K-V EQUATIONS

O. A. Anderson, Lawrence Berkeley National Laboratory, 1 Cyclotron Road, Berkeley, CA 94720 USA

Those working with alternating-gradient (A-G) systems look for simple, accurate ways to analyze A-G performance for matched beams. The useful K-V equations [1] are easily solved in the smooth approximation [2], [3], [4]. This approximate solution becomes quite inaccurate for applications with large focusing fields and phase advances. Results of efforts to improve the accuracy [5], [6] have tended to be indirect or complex. Our generalizations presented previously [7] gave better accuracy in a simple explicit format. However, the method used to derive our results (expansion in powers of a small parameter) was complex and hard to follow; also, reference [7] only gave low-order correction formulas.

The present paper uses a straightforward iteration method and obtains equations of higher order than shown in our previous paper.

The K-V equations for the envelopes  $a(z)$  and  $b(z)$  are

$$a(z)'' = -K(z)a + \frac{\epsilon^2}{a^3} + \frac{2Q}{a+b} \quad (1)$$

$$b(z)'' = +K(z)b + \frac{\epsilon^2}{b^3} + \frac{2Q}{a+b} \quad (2)$$

with input parameters: normalized beam current  $Q$ ; emittance  $\epsilon$ ; and A-G focus function  $K(z)$ . The  $z$  origin is located at the midpoint of a quadrupole and  $K(z)$  is assumed here to be symmetric about  $z=0$ , periodic over a cell length  $2L$ , and antisymmetric about  $L/2$ . Thus

$$K(z-2L)=K(z), \quad K(-z)=K(z), \quad K(z-L)=-K(z). \quad (3)$$

We solve for the  $x$  and  $y$  beam envelopes  $a(z)$  and  $b(z)$ , assumed to be matched to the lattice, i.e., periodic over  $2L$ . To aid the solution of Eqs. (1) and (2), we define in Eqs. (4)–(19) the operators on even periodic functions  $\langle \dots \rangle$ ,  $\{ \dots \}$ ,  $\int$  and  $\int\int$ ; the even periodic functions  $h(z)$ ,  $g(z)$ ,  $\delta(z)$  and  $\rho(z)$ ; and the constants  $k$ ,  $\alpha$ ,  $\beta$ ,  $q$ ,  $A$ ,  $K_{\text{eff}}$ ,  $\Phi$ , and  $\rho_m$ . In Eq. (19),  $h_1$  is the first Fourier coefficient of  $h(z)$ .

The operator  $\langle \dots \rangle$  performs an average over a cell length  $2L$  while the operator  $\{ \dots \}$  removes the average part of a periodic

function: e.g.,  $2\{\cos^2 x\} = \{1 + \cos 2x\} = \cos 2x$ . The operator  $\int\int$  operates on periodic functions that have no average. It gives the repeated indefinite integral and removes the average part, if any, of the result.

### DECOUPLING AND DECOMPOSING

With the quadrupole symmetries of Eq. (3), our matched beam assumption implies  $b(z) = a(z+L)$ , so that Eqs. (1) and (2) are decoupled. We have  $\langle a \rangle = \langle b \rangle \equiv A$ , and

$$a = A(1 + \rho), \quad b = A(1 + \rho_b). \quad (20)$$

The  $Q$  terms in Eqs. (1) and (2) can be expanded as

$$\frac{2Q}{a+b} = \frac{Q}{A} (1 - (\rho + \rho_b)/2 + \dots) = \frac{Q}{A} (1 - k^2 \delta(z) + \dots), \quad (21)$$

since [8]

$$(\rho + \rho_b)/2 = k^2 \delta(z) + \dots \quad (22)$$

with  $\delta(z)$  [Eq. (11)] derived from the lattice waveform  $h(z)$ .

This decouples Eqs. (1) and (2). After the decoupled version of Eq. (1) is solved for  $a(z)$ , then  $b(z)$  is found by symmetry. Equation (2) is no longer needed.

Substituting  $a = A(1 + \rho)$  in the first three terms of Eq. (1), expanding  $1/a^3$ , dividing by  $A$ , and using (21) and (15), the first K-V equation is equivalent to

$$\rho(z)'' = -kh(z) - kh(z)\rho + \frac{\alpha}{3} (1 - 3\rho + 6\rho^2 - 10\rho^3 + 15\rho^4 \dots) + q(1 - k^2 \delta(z) \dots). \quad (23)$$

To solve for the ripple  $\rho(z)$  and the mean radius  $A$  (which appears in the definitions of  $\alpha$  and  $q$ ), we decompose Eq. (23) into a pair of equations. Averaging Eq. (23),

$$0 = -k\langle h\rho \rangle + \frac{\alpha}{3} + 2\alpha\langle \rho^2 \rangle - \frac{10}{3}\alpha\langle \rho^3 \rangle + 5\alpha\langle \rho^4 \rangle \dots + q. \quad (24)$$

Subtracting Eq. (24) from (23),

$$\rho'' = -kh(z) - k\{h\rho\} - \alpha\rho + 2\alpha\{\rho^2\} - \frac{10}{3}\alpha\{\rho^3\} + 5\alpha\{\rho^4\} \dots - qk^2\delta(z) \dots, \quad (25)$$

with  $\{ \dots \}$  from Eq. (5). There are now two equations, each containing  $A$  and  $\rho(z)$ . Because of our periodicity constraint these have the essence of the K-V equations (1) and (2).

### ITERATIVE SOLUTION OF K-V EQUATIONS

On the right of Eq. (25), the  $kh(z)$  term dominates the terms involving the unknown function  $\rho(z)$ . They are omitted for the initial integrations, which give  $\rho_{(0)}$ . Then we insert  $\rho_{(0)}$  into (25) and integrate again to get  $\rho_{(1)}$ . The process is repeated for  $\rho_{(2)}$ . The resulting terms of greatest significance are:

$$\rho_{(0)} = -kg, \quad (26a)$$

$$\rho_{(1)} = \rho_{(0)} + \alpha k \int\int g + k^2 \delta + \frac{10}{3} \alpha k^3 \int\int g^3, \quad (26b)$$

$$\rho_{(2)} = \rho_{(1)} - \alpha^2 k \int\int\int g - k^3 \int\int h \delta - 2\alpha k^3 \int\int g \delta. \quad (26c)$$

To complete the approximate solution of the K-V equations,  $\rho(z)$  from Eq. (26) is put in the matching equation (24). From

Table 1: Definitions to be used in this paper

$\langle f \rangle \equiv (1/2L) \int_0^{2L} f(z) dz,$ (4)	$\delta(z) \equiv \int\int \{hg\},$ (11)
$\{f\} \equiv f - \langle f \rangle.$ (5)	$A \equiv \langle a(z) \rangle,$ (12)
For even $\psi(z) \ni \langle \psi \rangle = 0:$	$\rho(z) \equiv (a(z) - A)/A,$ (13)
$\int \psi \equiv \int_0^z \psi(z') dz'$ and (6)	$\rho_b(z) \equiv (b(z) - A)/A,$ (14)
$\int\int \psi \equiv \left\{ \int_0^z dz' \int_0^{z'} \psi(z'') dz'' \right\}.$ (7)	$\alpha \equiv \frac{3\epsilon^2}{A^4}, \quad \beta \equiv \alpha \frac{L^2}{\pi^2},$ (15)
$k \equiv K^{\text{max}},$ (8)	$q \equiv Q/A^2,$ (16)
$h(z) \equiv K(z)/k,$ (9)	$K^{\text{eff}} \equiv k^2 \langle [h]^2 \rangle,$ (17)
$g \equiv \int\int h,$ (10)	$\Phi \equiv 3k^2 \langle g^2 \rangle,$ (18)
	$\rho_m \equiv h_1 k L^2 / \pi^2.$ (19)

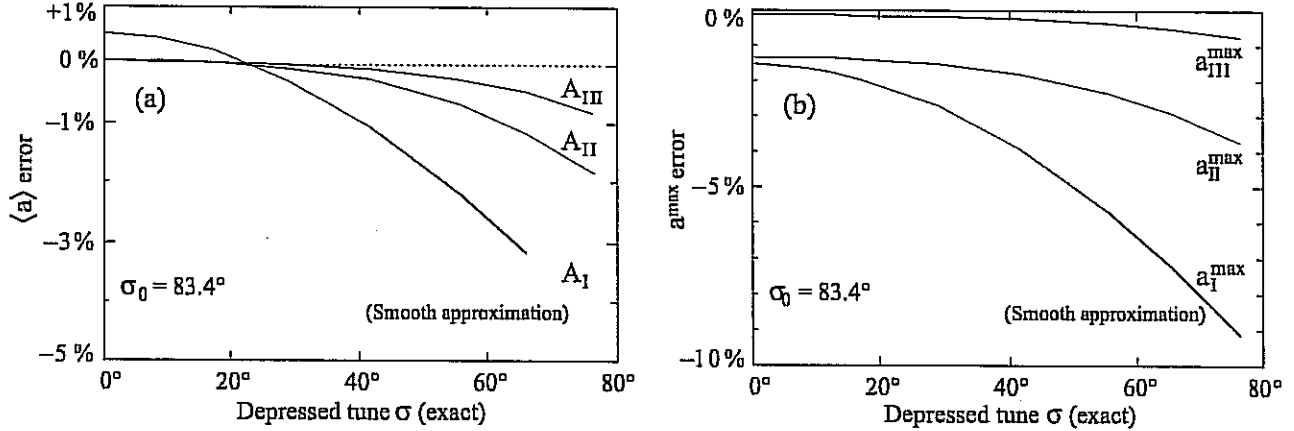


Fig. 1. Accuracy of: (a) mean radius  $A$  from Eqs. (30), (32), or (33) and (b) maximum radius  $a^{\max}$  from Eqs. (36), (37), or (38). Input quantities are  $Q$ ,  $\epsilon$ , and quadrupole voltage  $V_Q$  (proportional to  $K$ ). Quadrupole dimensions, etc., are in Ref. [8].  $V_Q$ , fixed at 20 kV, gives phase advance  $\sigma_0 = 83.37^\circ$ ;  $\epsilon$ ,  $Q$  are varied so that depressed tune  $\sigma$  ranges between  $0^\circ$  and  $76.5^\circ$ ; exact  $\sigma_0$  and  $\sigma$  are obtained numerically.

Eq. (26) we discarded items, such as  $2\alpha k^2 \int g^2$ , that would give terms in (24) higher than third power in the parameters  $k^2$ ,  $\alpha$ , and  $q$ . A miniscule term,  $qk^2 \int \delta(z)$ , in  $\rho_{(0)}$  is also omitted.

The order of a term in the matching equation is reckoned by counting the number of factors  $k^2$ ,  $\alpha$ , and  $q$ . (These would become small parameters in a non-dimensional formalism [8]. Here, we prefer to retain physical units for length  $z$ , etc.)

**Third Order:** Inserting Eq. (26) into Eq. (24) yields seven terms [8] through third order. Some terms combine, with result

$$K_{\dagger}^{\text{eff}} - \frac{\epsilon_{\text{III}}^2}{A_{\text{III}}^4} - \frac{Q}{A_{\text{III}}^2} = 0, \quad (27)$$

where

$$K_{\dagger}^{\text{eff}} \equiv \langle [K(z)]^2 \rangle \left[ 1 + \frac{1}{24} \Phi \left( 1 + \frac{20}{27} c_3 \right) \right]; \quad (28)$$

$$\epsilon_{\text{III}}^2 \equiv \epsilon^2 \left[ 1 + \Phi \left( 1 + \frac{1}{2} \Phi + 3\beta_1 \right) \right]. \quad (29)$$

Here  $c_3$  is of order unity [8]. Roman-numeral subscripts on  $A$  and  $\epsilon$  signify the order of approximation—third order in this case. The subscript on  $\beta \sim A^4$  indicates that  $A_{\text{I}}$  [Eq. (33)] is used to approximate  $A$ . The matching equation (27) is in the standard form of the smooth approximation, Eq. (33), and can be solved to find the third-order  $A$ :

$$A_{\text{III}}^2 = (Q/2K_{\dagger}^{\text{eff}}) + [(Q/2K_{\dagger}^{\text{eff}})^2 + \epsilon_{\text{III}}^2/K_{\dagger}^{\text{eff}}]^{1/2}. \quad (30)$$

If the input quantity is the mean radius  $A_{\text{inp}}$ , then Eq. (27) gives the allowable  $Q$  to third order,

$$Q_{\text{III}} = A_{\text{inp}}^2 K_{\dagger}^{\text{eff}} - \epsilon_{\text{III}}^2/A_{\text{inp}}^2.$$

**Second Order:** There are two second-order terms. One yields the correction to  $K^{\text{eff}}$  seen in Eq. (28). The other term is  $\alpha k^2 \langle g^2 \rangle$ , or, using definition (18),  $\frac{\alpha}{3} \Phi$ . We define

$$\epsilon_{\text{II}}^2 \equiv \epsilon^2 (1 + \Phi), \quad (31)$$

and get

$$K_{\dagger}^{\text{eff}} - \frac{\epsilon_{\text{II}}^2}{A_{\text{II}}^4} - \frac{Q}{A_{\text{II}}^2} = 0. \quad (32)$$

Eq. (32) can be solved for  $A_{\text{II}}$  or  $Q_{\text{II}}$  in the same way as for the third order, giving useful approximations when  $K(z)$  and  $\epsilon$  produce  $\sigma_0$  and  $\sigma$  less than about  $80^\circ$ .

**First Order:** The three terms of lowest order produce what is called the first-order matching equation in this paper (Ref. [7] used another terminology). This is the classic smooth approximation. These terms give  $k^2 \langle [h]^2 \rangle = \alpha/3 + q$ , or, using the definitions (15), (16), and (17)

$$K^{\text{eff}} - \frac{\epsilon^2}{A_{\text{I}}^4} - \frac{Q}{A_{\text{I}}^2} = 0. \quad (33)$$

First, second, and third-order results for  $A$ , from (33), (32) and (30), are plotted in Fig. 1a. The smooth approximation is relatively inaccurate except near the point where its error curve crosses the 0% line.

## MAXIMUM RADIUS

Knowing the matched mean radius  $A$ , one can complete the solution for the envelope  $a(z) = A[1 + \rho(z)]$  using  $\rho(z)$  from Eq. (26);  $b(z)$  can be found by changing the sign of the terms that contain odd powers of  $k$ .

Some terms of Eq. (26) can be written in exact form [8] for models such as FODO, but Fourier expansion is more useful in general:

$$h(z) = h_1 \left[ \cos \frac{\pi z}{L} + \frac{1}{3} c_3 \cos 3 \frac{\pi z}{L} + \frac{1}{5} c_5 \cos 5 \frac{\pi z}{L} \dots \right]. \quad (34)$$

Values (usually of order unity) of  $h_1$  and  $c_n$  for both FODO and smooth profiles are given in Ref. [8]. With the definition

$$\beta_1 \equiv 3 \frac{L^2}{\pi^2} \frac{\epsilon^2}{A_{\text{I}}^4} \quad (35)$$

we have

$$a_{\text{III}}^{\max} = A_{\text{III}} \left[ 1 + \rho_m \left( 1 + \frac{1}{27} c_3 + \frac{1}{125} c_5 \right) + \frac{1}{8} \rho_m^2 \left( 1 + \frac{25}{54} c_3 \right) + \beta_1 \rho_m \left( 1 + \frac{5}{2} \rho_m^2 + \beta_1 \right) \right] \quad (36)$$

using results from Ref [8]. The accuracy of Eq. (36) is shown in Fig. 1b, along with that of the truncations

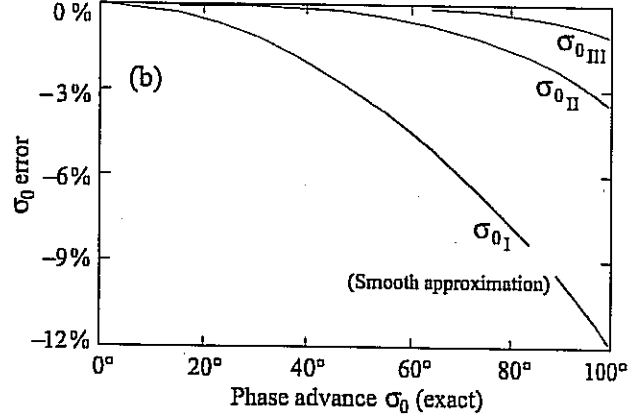
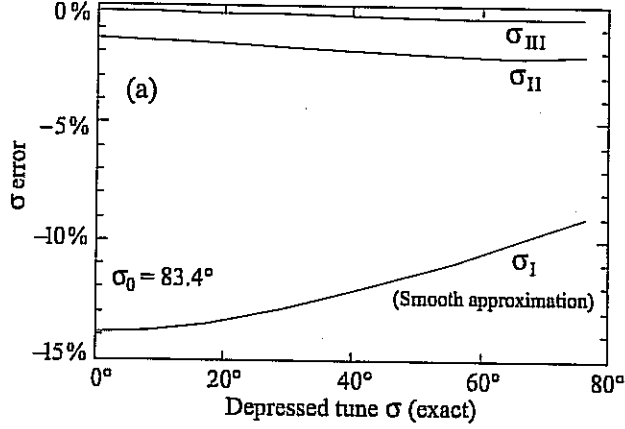


Fig. 2. (a) Accuracy of depressed tune  $\sigma$  from Eqs. (40), (41), and (42).  $V_Q$  is fixed at 20 kV as in Fig. 1.  
 (b) Accuracy of phase advance  $\sigma_0$  from Eqs. (43), (44), and (45).  $V_Q$  ranges from 5 kV to about 22 kV.

$$a_{II}^{\max} = A_{II} \left[ 1 + \rho_m \left( 1 + \frac{1}{27} c_3 + \frac{1}{125} c_5 \right) + \beta_I \rho_m \right] \quad (37)$$

and (the smooth approximation)

$$a_I^{\max} = A_I \left[ 1 + \rho_m \right]. \quad (38)$$

### PHASE ADVANCES

From the well-known phase-amplitude result [9], the phase advance per quadrupole cell of length  $2L$  is

$$\sigma = \epsilon \int_0^{2L} \frac{dz}{a^2} = 2L \epsilon \langle a^{-2} \rangle.$$

We approximate  $a(z)$  by  $A_{III} [1 + \rho(z)]$  with  $A_{III}$  from Eq. (30) and  $\rho(z)$  to third order from Eq. (26). Subscripts are omitted for brevity. Expanding  $a^{-2}$  and taking the average gives

$$\sigma = 2L \frac{\epsilon}{A_{III}^2} \left[ 1 + 3\langle \rho^2 \rangle - 4\langle \rho^3 \rangle + 5\langle \rho^4 \rangle - \dots \right]. \quad (39)$$

(The  $2\rho$  term has zero average by definition.) Ref. [8] shows that to third-order accuracy

$$\sigma_{III} = 2L \frac{\epsilon}{A_{III}^2} \left[ 1 + \Phi \left( 1 + \frac{3}{4} \Phi + 2\beta_I \right) \right]. \quad (40)$$

Errors with respect to exact values from simulations are shown in Fig. 2a. Useful accuracy is retained after dropping two terms and using  $A_{II}$  from Eq. (32):

$$\sigma_{II} = 2L \frac{\epsilon}{A_{II}^2} (1 + \Phi). \quad (41)$$

Figure 2a shows large errors for the first-order result (smooth approximation):

$$\sigma_I = 2L \frac{\epsilon}{A_I^2}. \quad (42)$$

The undepressed  $\sigma_0$  is found by setting  $Q = 0$  in Eq. (27), then eliminating  $\epsilon$  from Eq. (40). Details are in Ref. [8]. The result is

$$\sigma_{0III} = 2L (K_{\dagger}^{\text{eff}})^{1/2} \left[ 1 + \frac{1}{2} \Phi + \frac{7}{8} \Phi^2 \right]. \quad (43)$$

This equation is used to calculate  $\sigma_0$  as a function of the strength of the quadrupole field gradient. Figure 2b shows its accuracy and also illustrates the second-order case

$$\sigma_{0II} = 2L (K_{\dagger}^{\text{eff}})^{1/2} \left[ 1 + \frac{1}{2} \Phi \right] \quad (44)$$

and the smooth approximation,

$$\sigma_{0I} = 2L (K^{\text{eff}})^{1/2}. \quad (45)$$

### ACKNOWLEDGEMENTS

E.P. Lee and L.L. Lodestro offered helpful suggestions. Supported in part by the U.S. Department of Energy under Contract No. DE-AC03-76SF00098.

### REFERENCES

- [1] Kapchinskij and V.V. Vladimirskij, *Proc. Int. Conf. on High Energy Accel. and Instrum.* (CERN, 1959), p. 274.
- [2] M. Reiser, *Particle Accelerators* **8**, 167 (1978).
- [3] J. Struckmeier and M. Reiser, *Particle Accelerators* **14**, 227 (1984).
- [4] R.C. Davidson, *Physics of Nonneutral Plasmas*, N.Y., 1990; R.C. Davidson and Q. Qian, *Phys. Plasmas* **1**, 3104 (1994).
- [5] E.P. Lee, T.J. Fessenden, and L.J. Laslett, *IEEE Trans. Nuc. Sci.* **NS-32**, 2489 (1985).
- [6] E.P. Lee, *Particle Accelerators* **52** (1996).
- [7] O.A. Anderson, *Particle Accelerators* **52**, 133 (1996); O.A. Anderson, *Lawrence Berkeley Laboratory report LBL-261233* (Revised), 1995.
- [8] For derivation of equations, etc., see the appendices to: O.A. Anderson, *LBNL report LBNL-57388*, 2005 (to be submitted to *Accel. and Beams*).
- [9] E.D. Courant and H.S. Snyder, *Ann. of Phys.* **3**, 1 (1958).