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1 Utilization of magnetic field-driven microscopic motion for
2 piezoelectric energy harvesting

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1 **Abstract**

2 In spite of recent advances in the development of high performing piezoelectric materials, their
3 applications are typically limited to the direct conversion of mechanical impact energy to electrical
4 energy, potentially risking mechanical failures. In this study, we developed piezoelectric
5 poly(vinylidene fluoride-trifluoroethylene) (P(VDF-TrFE)) nanofibers integrated with SiO₂-
6 shelled Fe₃O₄ magnetic nanoparticles, to utilize magnetic energy to reliably drive the piezoelectric
7 effect. Specifically, we show that the shape of the magnetic nanoparticle exerts a significant effect
8 on the efficiency of the magno-mechano-electrical energy conversion as magnetic nanorods
9 exhibit approximately 70% enhancement in the electric field generation under cyclic magnetic
10 fields as compared to nanospheres. Under an alternating magnetic field of 200 mT, the magnetic
11 nanorod-piezoelectric nanofiber composite generated a peak-to-peak voltage of approximately 30
12 mV_{p-p} with a superior durability without any performance degradation after over 1 million cycles.
13 This study demonstrates the potential of magnetic-field responsive, piezoelectric-based materials
14 in the energy harvesting applications from non-mechanical energy sources.

15

16 **Keywords:** Piezoelectric electrospun nanofiber, Magnetic nanoparticle, Waste energy harvesting

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1 **Introduction**

2 Energy demand for portable electronic devices has substantially increased due to the incorporation
3 of power-guzzling features such as powerful computational capability, various sensors and larger
4 screen size. To accommodate such a high energy demand, scavenging wasted energy sourced from
5 daily-life activities has been explored with diverse approaches for efficient energy conversion.
6 One of the most common and effective approaches is the conversion of mechanical energy to
7 electrical energy. The mechanical energy mainly originates from human body or machine motions,
8 and its energy output is considerably high among the other energy scavenging sources such as
9 light, radio-frequency electromagnetic radiation, and thermal gradient.^{1,2} Therefore, piezoelectric
10 materials, capable of converting mechanical energy to electrical energy, are the key to efficiently
11 harvest such wasted energy.^{3,4}

12 For low frequency, high strain applications, polymer-based piezoelectric materials have
13 significant advantages over piezo-ceramics due to their flexibility and impact resistance.⁵ Among
14 various polymeric piezoelectric materials, poly(vinylidene fluoride) (PVDF) has shown to exhibit
15 outstanding piezoelectric constants⁶ and fairly good thermal stability. Recently, the
16 copolymerization of a phase stabilizer, trifluoroethylene (TrFE), enables the maintenance of
17 electrically active β -phase at room temperature, achieving greater piezoelectric constants.⁴ We
18 have further demonstrated that electrospinning process induces P(VDF-TrFE) nanofibers to form
19 greater β -phase content without additional mechanical stretching and/or electric poling for piezo-
20 ceramic compatible performances.^{7,8}

21 To further improve its utilization, the addition of functional materials, i.e., magnetic
22 materials in the PVDF matrix, may enable to exploit other extrinsic stimuli, i.e. magnetic fields,
23 to actuate the piezoelectric polymer for energy generation. Indeed, several groups have attempted

1 to introduce Fe_3O_4 nanoparticles into PVDF films⁹ and nanofibers¹⁰, and demonstrated that the
2 addition of the nanoparticle enhances the piezoelectric performance due to an increase in β -phase
3 formation and electret doping effect¹¹. A few studies have reported to utilize magnetic fields to
4 actuate piezoelectric devices at macroscale in combination with an additional magnetic materials¹²,
5 ¹³. However, to the best of our knowledge, no report has yet demonstrated the magneto-mechano-
6 electrical energy conversion at nanoscale by utilizing microscopic movement of the magnetic
7 nanoparticles embedded within individual piezoelectric nanofibers, enabling a long-term structural
8 stability. In this study, we developed a composite of P(VDF-TrFE) and Fe_3O_4 encapsulated by
9 SiO_2 , and demonstrated its performance in producing electric fields under alternating magnetic
10 fields via the microscopic movement of magnetic nanoparticles, embedded in the piezoelectric
11 nanofibers. Specifically, the effects of the morphological anisotropy of the magnetic nanoparticles
12 on the piezoelectric performance of piezoelectric-magnetic composites were investigated to
13 enhance the energy conversion.

14

15 **Results and discussion**

16 In this study, we aimed to develop an electrospun piezoelectric P(VDF-TrFE) composite with
17 magnetic nanoparticles (MNPs) and demonstrate the actuation of the piezoelectric nanofibers by
18 the microscopic movements of the MNPs under magnetic fields for electric field generation
19 (Figure 1a). We particularly focused on examining the effects of MNP shape factor on the
20 efficiency of magneto-mechano-electrical conversion. The mechanism underlying the conversion
21 of magnetic field to mechanical strain to electrical energy is based on the microscopic movement
22 of the MNPs straining P(VDF-TrFE) nanofibers due to two major forces: attractive force and

1 torque. The attractive force (F_{att}) occurs when the MNPs are placed in a magnetic field gradient,
2 causing convectional movements, which can be described by the equation,

$$3 \quad F_{att} = \nabla(\mathbf{m} \cdot \mathbf{B}) = \nabla m B \cos\theta, \quad (1)$$

4 where \mathbf{m} is magnetic dipole moments, \mathbf{B} is magnetic field, and θ is angle between \mathbf{m} and \mathbf{B} vectors.

5 Another force that the MNP will experience in the magnetic field is torque,

$$6 \quad \tau_{mag} = \mathbf{m} \times \mathbf{B} = m B \sin\theta, \quad (2)$$

7 where its magnitude becomes maximum at $\theta = 90^\circ$ while the maximum of the attractive force is
8 at $\theta = 0^\circ$. The torque induced by the magnetic field causes the rotation of an MNP, further
9 microscopically straining the nanofiber, in addition to the tensile straining by F_{att} . Based on the
10 equations (1 and 2), the total force applied to the nanofiber is determined by \mathbf{m} , \mathbf{B} , and the
11 magnetization orientation of MNPs. Therefore, the uniform alignment of MNP orientation is the
12 key to maximize the overall force generated under magnetic fields. In this regard, the shape of
13 MNP is essential for its alignment when embedded within an electrospun nanofiber; the MNP with
14 an anisotropic morphology, i.e., rod shape, will promote the alignment of MNP magnetization
15 along the long axis of the fiber while that with the spherical shape will result in statistically random
16 magnetization orientation.

17 To investigate the effects of the MNP shape factor with different aspect ratios on the torque
18 strain generation to the nanofibers, numerical simulation using COMSOL Multiphysics was
19 conducted. In this simulation, maximum possible torque strains induced by the rotation of MNPs
20 were compared; the direction of the MNP dipoles is all aligned along the nanofiber axis regardless
21 of the particle shape. Figure 1c shows that the strain increases almost linearly with the increase of
22 the aspect ratio when the same magnitude of force was applied to the opposite sides of the MNP
23 surfaces in the axis parallel to nanofibers as shown in Figure 1b. Based on this simulation result,

1 we synthesized magnetic nanoparticles with a rod shape (magnetic nanorod (MNR)) or a spherical
2 shape (magnetic nanosphere (MNS)) as shown in Figure 2 to demonstrate the particle shape
3 dependency of magnetic field-induced piezoelectric nanofiber strain and its consequent electric
4 field generation. The average diameter and length of the MNRs are approximately 160 nm and 460
5 nm, respectively, with 40 nm SiO₂ layer, which was indispensable to form such a shape with high
6 aspect ratio¹⁴. The average diameter of the MNSs was controlled to match that of the MNRs at
7 approximately 168 nm with 30 nm SiO₂ layer. These MNPs were separately dispersed in P(VDF-
8 TrFE) solution prior to being subjected to electrospinning. We have previously reported that the
9 reduction of the nanofiber diameter results in the exponential enhancement of piezoelectric
10 properties due to the enhanced β -phase formation and Young's modulus¹⁵. For the present study,
11 nanofiber diameter is more significant factor in determining electric field generation as compared
12 to typical direct mechanical force induced applications due to minute strains generated by the
13 microscopic movements of MNPs. Therefore, the reduction of nanofiber diameter without
14 significantly deteriorating MNP distribution within the nanofibers, is critical to enhance the
15 piezoelectric performance by promoting the strain of individual fibers, and by improving
16 piezoelectric coefficients through dimensional reduction. In this regard, the diameters of both
17 MNR and MNS composite nanofibers were carefully controlled, minimized, and matched to
18 compare the magneto-mechano-electrical energy conversion induced by the MNP-derived
19 actuation on piezoelectric nanofibers under alternating magnetic fields. The SEM images of
20 Fe₃O₄@SiO₂ MNS and MNR/PVDF-TrFE nanofiber composites show that MNPs are uniformly
21 distributed along the individual nanofibers (Figure 2c-d). The average diameters of MNP-
22 containing fibers were approximately 58 nm (MNR) and 63 nm (MNS), respectively. It should be
23 noted that MNPs are not embedded in the center of the nanofibers. The height profiles of the AFM

1 images show that MNPs are surrounded with at least 20 ~ 30 nm thick-layer of P(VDF-TrFE)
2 resulting in robust mechanical bonding between MNPs and nanofibers, stable under strains (Figure
3 2e-f). Indeed, we did not observe any mechanical failure of MNPs separated from the nanofiber
4 matrix in the subsequent experiments.

5 The piezoelectric properties of the nanofibers were determined by piezo-response force
6 microscopy (PFM) (Figure 3a-b). Piezoelectric properties were analyzed by monitoring the
7 amplitude changes with respect to the applied electric bias and showed a relatively similar response
8 from MNR- and MNS-containing nanofibers. The values of the d_{33} for MNR-nanofiber and MNS-
9 nanofiber were 36 ± 7 and 40 ± 14 pm/V, respectively, with around 60 nm fiber diameter. It is
10 expected that the difference in the electric outputs under the same strain due to the discrepancy in
11 d_{33} between MNR and MNS will be within the range of 10%.

12 Shape-dependent magnetization was analyzed by magnetic hysteresis loops (MHLs) to
13 compare the magnetic properties of the MNR and MNS in nanofiber in Figure 3c-d. Higher
14 remanence to saturation magnetization ratio (M_r/M_s) and coercivity indicates an easy
15 magnetization direction or preferential direction of the magnetic dipole of the magnetic materials.
16 The MHLs were conducted in two magnetic field directions: in-plane ($H//$) and out-of-plane (H
17 \perp). Asymmetric shape of MNRs makes them aligned along the nanofiber axis during
18 electrospinning. In the MHLs under $H \perp$, the angle between MNRs and H_a is 90°. The parallel
19 MHLs of MNR show higher M_r/M_s and H_c than perpendicular MHLs elucidating that the easy
20 magnetization direction of the NR is the long axis of the NR (Figure 3c). Contrary to the MNRs,
21 the polarity of the MNS is randomly oriented in the nanofibers due to its spherically symmetry
22 structure. As expected from the structure, MHLs of MNS show that magnetic isotropy between
23 the in-plane and out-of-plane field orientation, resulting in almost the same M_r/M_s and H_c (Figure

1 3d). The identical curves regardless of the direction of the applied magnetic fields elucidate that
2 there is no preferential orientation of the MNS in the nanofiber mat (Figure 3f). These results
3 confirm the superiority of MNR to maximize force generated under magnetic fields as described
4 earlier (Figure 1). The amount of torqueing by MNPs under magnetic fields can be estimated by
5 the MHL. The total mechanical work by the torque for the cyclic integral $\tau d\theta = -dW$ is
6 proportional to the area of M-H loop.^{16, 17} When comparing the area (A) of perpendicular MHLs
7 of MNR and MNS, which represents the actual operating scheme of the experiment (perpendicular
8 approach of the magnet to the surface of nanofiber mats), the ratio of $A_{\text{MNR}}/A_{\text{MNS}}$ is approximately
9 1.4. Given the ratio, it is expected that 1.4 times larger torsional work is induced by the MNRs
10 during the approach of the external magnet.

11 To confirm the superior piezoelectric performance of MNR-nanofiber expected from the
12 piezoelectrical and magnetic characterization, electric outputs from the MNS and MNR composite
13 nanofibers with a similar thickness of approximately 25 μm were measured under the cyclic
14 movement of the magnet as shown in Figure 4a. The movement of the magnet was limited to the
15 perpendicular direction to the nanofiber mat, thereby minimizing the contribution from electro-
16 magnetic interference (EMI) on the electric output. The control experiment with P(VDF-TrFE)
17 nanofibers without any MNPs confirmed that the influence of EMI is negligible (Figure 4b). Au-
18 coated glass substrates were used as electrodes, sandwiching the samples to prevent macro-scale
19 deformation of the nanofiber mat during the measurement. Representative electric outputs from
20 MNR and MNS were plotted to compare their amplitude difference in Figure 4b. To validate the
21 reproducibility, five independent nanofiber mats with either MNRs or MNSs were independently
22 prepared and the electric outputs of each device were measured (Figure S1). The resultant electric
23 outputs from MNR were an average of 30 $\text{mV}_{\text{p-p}}$, approximately 70 % higher than that of MNS at

1 an average of 21 mV_{p-p}. The electric outputs from as-spun PVDF-TrFE nanofiber showed
2 negligible voltages, confirming that the generated voltages from MNP-containing fibers originates
3 from the strain induced by the movement of the MNPs in the nanofibers. The output voltage with
4 switching-polarity test further confirms that the signals were generated by the piezoelectric
5 response of the devices (Figure S2). This electric output difference is above the level of 40%
6 enhancement predicted from the magnetization area comparison in MHLs (Figure 3c-d), likely due
7 to the combination of slightly higher piezoelectric constant, enhanced torqueing and different
8 distribution of MNRs within the nanofiber matrix.

9 The electric outputs (voltage and current) of the current system under magnetic fields are
10 considerably lower than that generated under direct mechanical actuation (Figure S3). However,
11 this energy harvesting strategy has a significant advantage by providing a means to produce
12 electrical energy without a macro-scale mechanical actuation that typically leads to mechanical
13 failure and/or poor electrical contact after a long period usage. To demonstrate its long-term
14 durability, the system was subjected to over 1 million cycles and showed a consistent electric
15 output without any degradation as shown in Figure 4c. We expect that the electric output can be
16 further improved by optimizing the load of the MNPs or the mat thickness.

17

18 **Conclusion**

19 In this work, we investigated MNPs with different morphologies embedded within piezoelectric
20 P(VDF-TrFE) nanofibers for the magneto-mechano-electrical energy conversion. MNRs aligned
21 along the nanofiber by the electrospinning process, which resulted in their uniform magnetization
22 orientation in the direction of the long axis of MNR, enabling a full utilization of torque strain to
23 enhance electric field generation under cyclic magnetic fields. The combination of enhancements

1 in the out-of-plane magnetization, the torque-induced strain generation, and the piezoelectric
2 constant resulted in the enhanced energy conversion performance of the MNRs, generating 70%
3 greater electric outputs as compared to MNS. These results demonstrate the significant impact of
4 the particle shape factor on the MNP-based energy harvesting. Furthermore, the result from the
5 durability test demonstrates that the microscopic movement of the nanofibers without macro-scale
6 bending or compression enables long-term energy harvesting capability without degradation of
7 piezoelectric performance over 1 million cycles. Therefore, this work opens another revenue as a
8 waste energy harvesting strategy using a piezo electric polymer combined with magnetic
9 nanoparticles.

10

11 **Experimental**

12 **Synthesis of magnetic Fe₃O₄@SiO₂ nanorods (NRs)**

13 The synthesis of FeOOH NRs was based on a previously reported methods^{14, 18} with some
14 modifications. In a typical synthesis of 460 nm FeOOH NRs, 100 mL of 0.1 M FeCl₃ aqueous
15 solution was added into a glass vial, which was tightly sealed and kept at 87 °C for 24 h. After
16 cooling to room temperature, the particles were collected by centrifugation, washed with water for
17 several times, and dispersed in 20 mL of water. The surface of as-synthesized FeOOH NRs were
18 functionalized with polyacrylic acid (PAA). To 20 mL of the above FeOOH dispersions, 20 mL
19 of PAA solution (7.2 mg/mL) was added. The mixture was then stirred for 12 h, followed by
20 centrifugation to remove excess PAA and re-dispersing in 20 mL of water. A 20 ml aqueous
21 dispersion of PAA-modified FeOOH NRs was added into 100 mL of ethanol, followed by the
22 addition of 3 mL of ammonium hydroxide (~28 % wt) and 4 mL of tetraethyl orthosilicate. After
23 4 h of reaction, the FeOOH@SiO₂ NRs were isolated by centrifugation, washed with ethanol and

1 water for several times, and dried at 60 °C. The FeOOH@SiO₂ NRs was reduced at 360 °C by 5%
2 H₂ for 2 h to produce the Fe₃O₄@SiO₂ NRs.

3

4 **Synthesis of magnetic Fe₃O₄@SiO₂ nanospheres (NSs)**

5 Similar synthetic protocols were employed for the preparation of Fe₃O₄@SiO₂ NSs. In a typical
6 synthesis, 100 mL of mixed aqueous solution of 0.2 M FeCl₃ and 0.08 M cetyltrimethylammonium
7 chloride was tightly sealed in a glass bottle and kept at 87 °C for 24 h. The FeOOH NSs were then
8 collected and washed, functionalized with PAA, coated with silica, and finally converted to
9 Fe₃O₄@SiO₂ NSs by using the same protocols as for Fe₃O₄@SiO₂ NRs.

10

11 **Electrospinning of MNP composite P(VDF-TrFE) nanofibers**

12 0.36g of P(VDF-TrFE) (70/30 mol%, Solvay Group, France) was dissolved in 2.13g of N,N-
13 dimethylformamide (DMF) (Fisher Scientific, Pittsburgh, PA) and 1.19g of acetone, supplemented
14 with 0.31g of pyridinium formate (PF) buffer (Sigma-Aldrich, St Louis, MO) to increase the
15 solution conductivity. After complete dissolution of P(VDF-TrFE) under magnetic stirring, 0.252
16 g of MNPs were added to the solution and sonicated for 1 hour. The solution was then electrospun
17 for 4 hours at applied voltage of ~15 kV with the distance of 20 cm between the needle and
18 substrate at around 20 °C and a relative humidity of 9 g m⁻³. The deposited electrospun nanofibers
19 were then placed in an oven at 90 °C for 24 hours.

20

21 **Numerical simulations**

22 Solid mechanics module in COMSOL Multiphysics 5.3a was used for the numerical simulation
23 (Figure 1b-c). The diameter of MNR and MNS was set at 160 nm. Nanofibers of 60 nm in diameter

1 and 4 μm in length were used, and their Young's modulus, Poisson's ratio, and density of the
2 nanofiber were set at 50 GPa¹⁵, 0.39, and 1780kg/m³¹⁹, respectively. To calculate the torque strain
3 induced by the rotation of MNPs, the same magnitude of force (1 μN) was applied to the opposite
4 sides of the MNP surfaces in the axis parallel to nanofibers. The average of the first principle strain
5 in nanofibers was calculated with respect to the aspect ratio of the MNPs.

6

7 **Characterization of MNP composite P(VDF-TrFE) nanofibers**

8 The morphology of MNPs and MNP composite P(VDF-TrFE) nanofibers were characterized using
9 transmission electron microscope (TEM, Tecnai 12) and scanning electron microscope (SEM,
10 FEI NNS450). MFP-3D AFM (Asylum Research, Santa Barbara, CA) was used for topographic
11 images and piezoelectric coefficient measurement. The topographic images were obtained under
12 tapping imaging mode, and the probe was then placed on the top of the individual fiber in contact
13 mode subsequently by switching AFM to PFM mode. Under our PFM measurement system, single
14 point spectroscopy was measured on the nanofibers on Au substrate and step voltages from -3 to
15 +3 V were applied to the fiber and the amplitude change of the PFM cantilever (AC240TM,
16 Olympus) was recorded in the same direction to the electric field which corresponds to the
17 piezoelectric constant, d_{33} . Taking into account the quality factor (Q) of the AFM cantilever, the
18 d_{33} of the nanofibers was calculated using the following relation,

$$19 \quad d_{33} = \frac{A}{VQf} \quad (3)$$

20 where A is the amplitude of the piezoresponse, V is the applied bias, and f is the correctional
21 factor ($f=23.96$) from the periodically poled lithium niobite (PPLN) standard²⁰ which has a known
22 piezoelectric coefficient. Room temperature magnetic hysteresis loops of the MNR and MNS in
23 nanofiber were conducted with a vibrating sample magnetometer (DMS). Because the NR and NS

1 are integrated with the nanofiber mats with the same weight % and their thicknesses are similar
2 (~25 μm), nanofiber mat area was based instead of mass for the direct comparison of the MNR
3 and MNS in nanofiber. Hence, 1.5 cm by 1.5 cm nanofiber mats were cut into 9 small pieces (5
4 mm by 5 mm). The 9 small pieces of nanofibers were stacked and placed in the center of the
5 magnetic hysteresis. The fibers were placed in two direction: in-plane (H//) and out-of-plane (H
6 \perp) and the external magnetic field was applied to the film at 10 Oe increment and 3s dwell time.

7

8 **Electric output measurement under magnetic stimulus**

9 100 nm Au was deposited on the both sides of the nanofiber mats (Area: 2.25 cm^2 , Thickness: 25
10 μm) by sputtering and the samples were sandwiched with Au coated glasses for efficient collection
11 of the generated charges from the nanofibers. A cube Neodymium magnet (N42 1-1/2") was used
12 for the stimulus of the MNP-nanofiber mat. The magnetic field intensity measured using a gauss
13 meter (HT20, Resolution: 1mT) on the surface of the south pole was $\sim 200\text{mT}$. To minimize
14 electromagnetic interference and induced current due to the magnet, the magnet moved vertically
15 to the fiber mat and the fiber was completely sealed with grounded aluminum (Al) film. The
16 generated voltage was measured with an oscilloscope (Pico Technology, St Neots, United
17 Kingdom) under the magnetic stimulation by a vertical cyclic movement of the magnet at 3.3Hz.

18

19 **Conflicts of interest**

20 There are no conflicts to declare.

21

22 **Acknowledgement**

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2 Research Foundation of Korea funded by the Ministry of Science and ICT (2018M3D1A1057844),
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5

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1 **Figure Captions**

2 **Figure 1.** Conversion of magnetic energy to electric energy by utilizing dynamic strains induced
3 by microscopic movements of magnetic $\text{Fe}_3\text{O}_4@\text{SiO}_2$ nanorod (MNR)- and nanosphere (MNS)-
4 composite P(VDF-TrFE) nanofibers under magnetic fields. (a) Schematic illustration of MNR and
5 MNS embedded in P(VDF-TrFE) nanofibers under magnetic fields. (b) A schematic of nanofiber
6 strain induced by the torque of the magnetic nanoparticles. (c) Average first principle strain in
7 nanofibers due to the torque of the MNRs with different aspect ratio. Finite element analysis in
8 COMSOL Multiphysics was used to obtain the simulation results of (b) and (c). **The values are**
9 **normalized to that of MNS (i.e., aspect ratio = 1).**

10

11 **Figure 2.** Morphological characterization of magnetic nanoparticles (MNPs) and P(VDF-TrFE)
12 nanofibers. TEM images of magnetic $\text{Fe}_3\text{O}_4@\text{SiO}_2$ (a) nanorods (MNRs) and (b) nanospheres
13 (MNSs). SEM images of electrospun P(VDF-TrFE) nanofibers with (c) MNRs and (d) MNSs.
14 AFM images of (e) MNR and (f) MNS embedded in P(VDF-TrFE) nanofibers. Insets show the
15 cross-sectional topography of the fiber (A) with and (B) without MNPs.

16

17 **Figure 3.** Piezoelectric and magnetic characterization of electrospun P(VDF-TrFE) nanofibers
18 embedded with magnetic $\text{Fe}_3\text{O}_4@\text{SiO}_2$ nanorods (MNRs) and nanospheres (MNSs). Piezoelectric
19 responses of the nanofibers with (a) MNRs and (b) MNSs (top graphs) in response to applied
20 electric biases (bottom graphs). In-plane ($H//$) and out-of-plane ($H \perp$) magnetic hysteresis loops
21 of the nanofibers with (c) MNRs and (d) MNSs. Schematic illustration of magnetic nanoparticle
22 polarization under $H//$ and $H \perp$ showing that (e) all MNRs are aligned in the direction of
23 nanofibers and their magnetization orientation are also in the same direction with the nanofibers
24 while (f) MNSs have randomly oriented magnetization.

25

26

27 **Figure 4.** **Electric outputs of approximately 25 μm -thick electrospun mats composed of magnetic**
28 **$\text{Fe}_3\text{O}_4@\text{SiO}_2$ nanoparticle embedded P(VDF-TrFE) nanofibers under magnetic stimulation by a**
29 **vertical cyclic movement of a neodymium magnet.** (a) Schematic of the device assembly to
30 measure electric outputs under magnetic stimulation. (b) Comparison of electric outputs from as-

- 1 spun P(VDF-TrFE) nanofiber mat, its composite with MNSs, or MNR. (c) A long-term durability
- 2 test of P(VDF-TrFE) nanofibers embedded with MNRs.

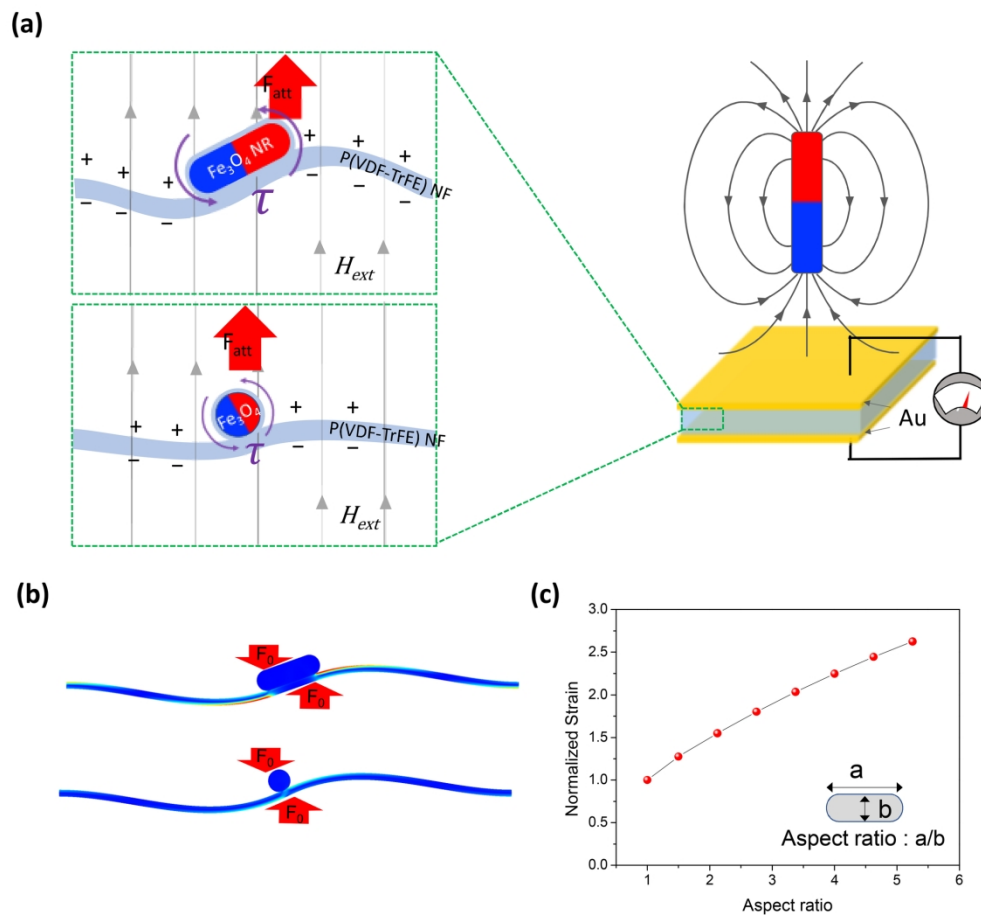


Figure 1. Conversion of magnetic energy to electric energy by utilizing dynamic strains induced by microscopic movements of magnetic $\text{Fe}_3\text{O}_4@SiO_2$ nanorod (MNR)- and nanosphere (MNS)- composite P(VDF-TrFE) nanofibers under magnetic fields. (a) Schematic illustration of MNR and MNS embedded in P(VDF-TrFE) nanofibers under magnetic fields. (b) A schematic of nanofiber strain induced by the torque of the magnetic nanoparticles. (c) Average first principle strain in nanofibers due to the torque of the MNRs with different aspect ratio. Finite element analysis in COMSOL Multiphysics was used to obtain the simulation results of (b) and (c). The values are normalized to that of MNS (i.e., aspect ratio = 1).

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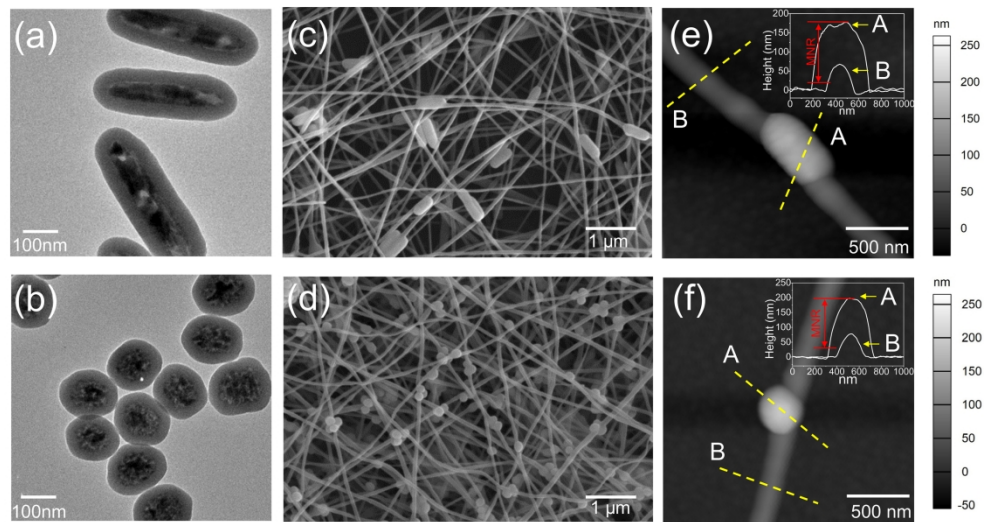


Figure 2. Morphological characterization of magnetic nanoparticles (MNPs) and P(VDF-TrFE) nanofibers. TEM images of magnetic $\text{Fe}_3\text{O}_4@\text{SiO}_2$ (a) nanorods (MNRs) and (b) nanospheres (MNSs). SEM images of electrospun P(VDF-TrFE) nanofibers with (c) MNRs and (d) MNSs. AFM images of (e) MNR and (f) MNS embedded in P(VDF-TrFE) nanofibers. Insets show the cross-sectional topography of the fiber (A) with and (B) without MNPs.

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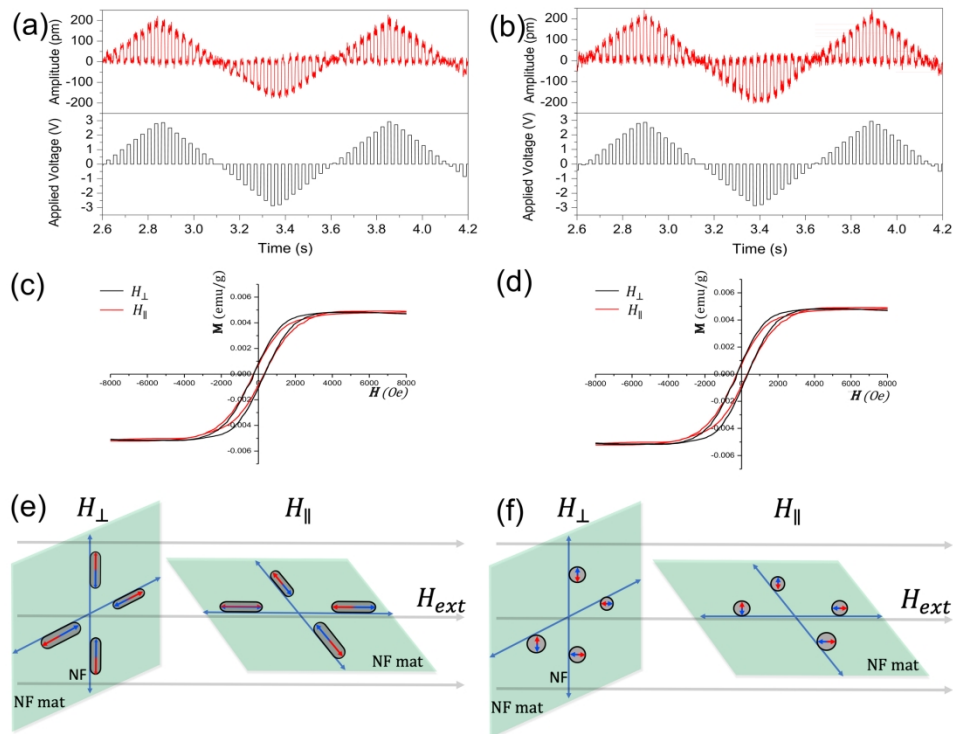


Figure 3. Piezoelectric and magnetic characterization of electrospun P(VDF-TrFE) nanofibers embedded with magnetic Fe₃O₄@SiO₂ nanorods (MNRs) and nanospheres (MNSs). Piezoelectric responses of the nanofibers with (a) MNRs and (b) MNSs (top graphs) in response to applied electric biases (bottom graphs). In-plane (H_{\parallel}) and out-of-plane (H_{\perp}) magnetic hysteresis loops of the nanofibers with (c) MNRs and (d) MNSs. Schematic illustration of magnetic nanoparticle polarization under H_{\parallel} and H_{\perp} showing that (e) all MNRs are aligned in the direction of nanofibers and their magnetization orientation are also in the same direction with the nanofibers while (f) MNSs have randomly oriented magnetization.

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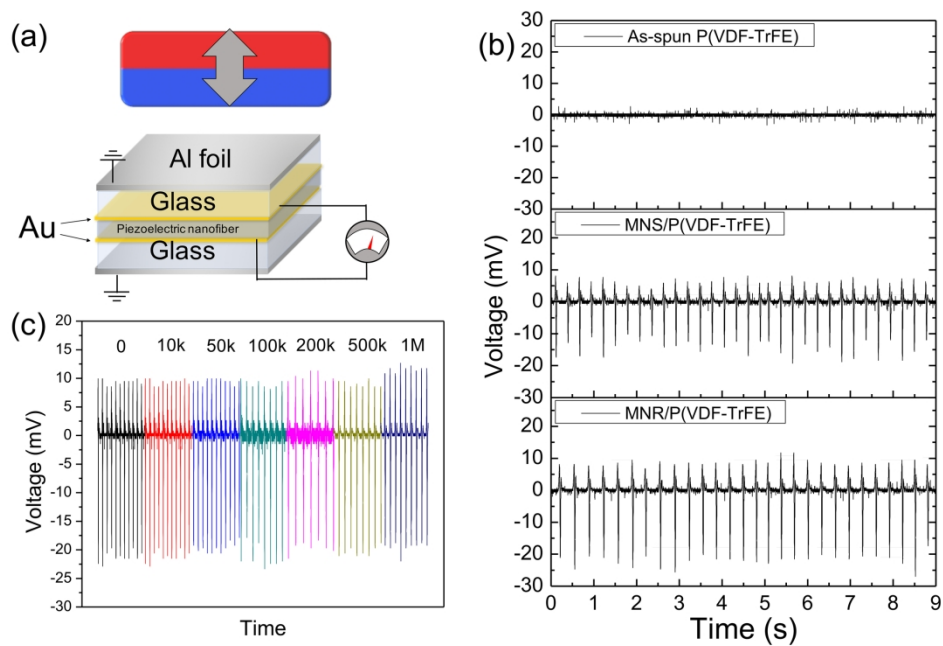
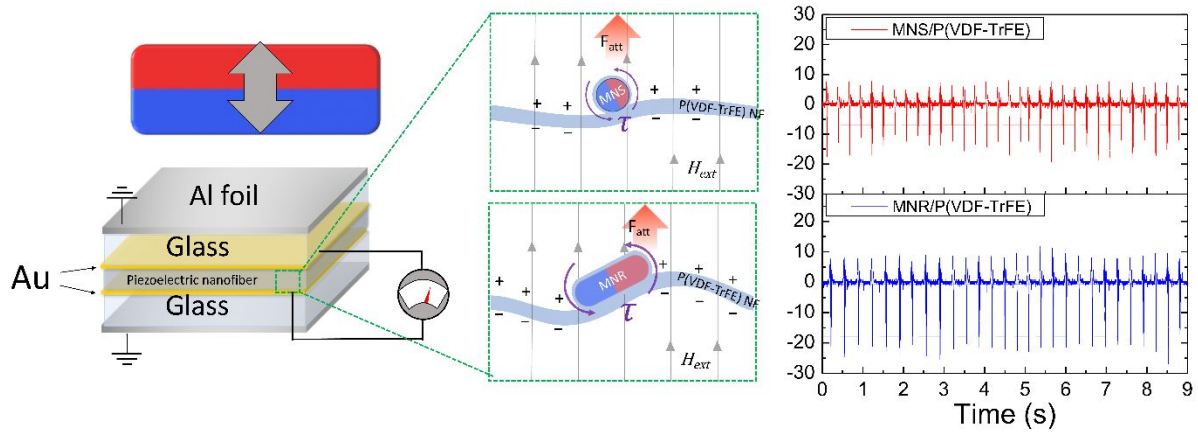


Figure 4. Electric outputs of approximately 25 μm -thick electrospun mats composed of magnetic $\text{Fe}_3\text{O}_4@\text{SiO}_2$ nanoparticle embedded P(VDF-TrFE) nanofibers under magnetic stimulation by a vertical cyclic movement of a neodymium magnet. (a) Schematic of the device assembly to measure electric outputs under magnetic stimulation. (b) Comparison of electric outputs from as-spun P(VDF-TrFE) nanofiber mat, its composite with MNSs, or MNR. (c) A long-term durability test of P(VDF-TrFE) nanofibers embedded with MNRs.

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Magneto-mechano-electrical energy conversion in poly(vinylidene fluoride-trifluoroethylene) piezoelectric nanofibers integrated with magnetic nanoparticles in a particle-shape dependent manner

Supporting information

Utilization of magnetic field-driven microscopic motion for piezoelectric energy harvesting

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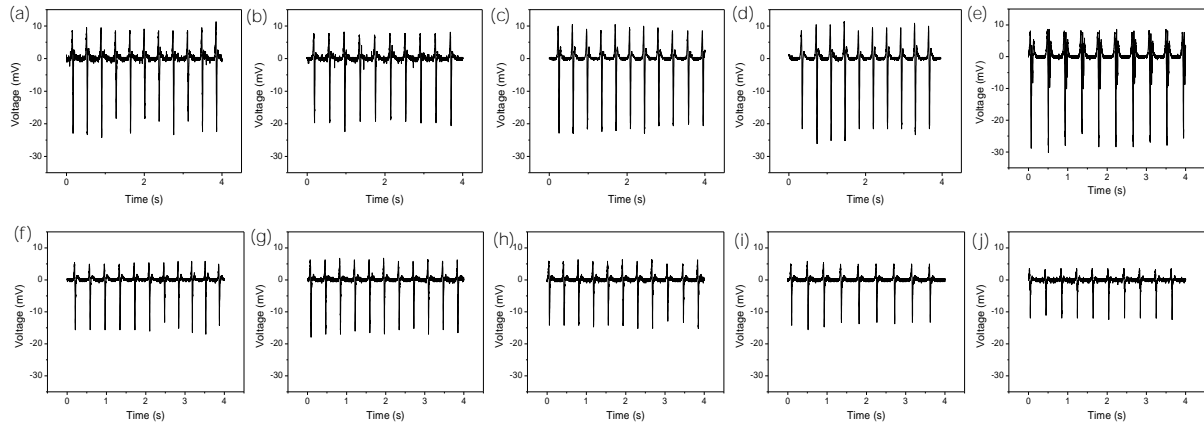


Figure S1. Reproducibility test of the piezoelectric output voltage measured from five independent P(VDF-TrFE) nanofiber mats with MNRs (a-e) and MNSs (f-j).

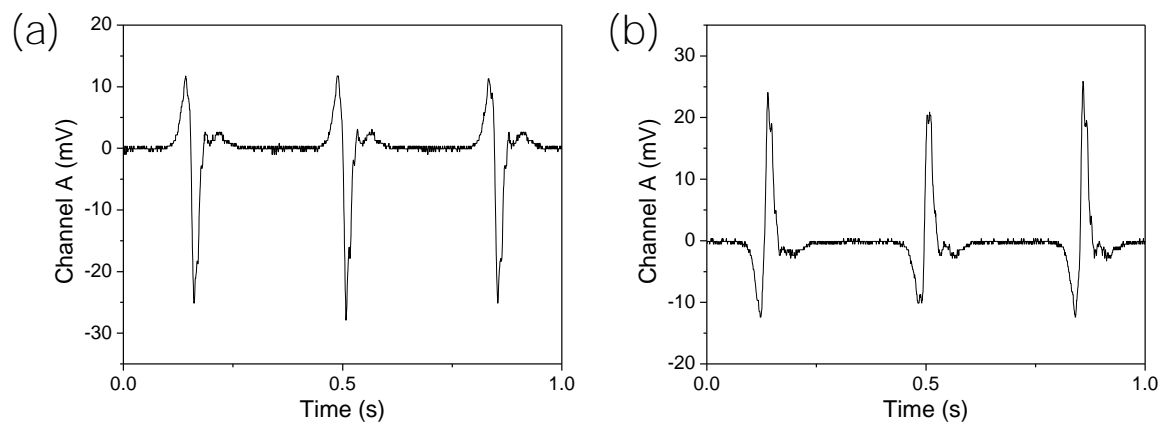


Figure S2. Piezoelectric output voltage measured from the magnetic $\text{Fe}_3\text{O}_4@ \text{SiO}_2$ nanorodes embedded P(VDF-TrFE) nanofiber mats by (a) forward and (b) reverse connections.

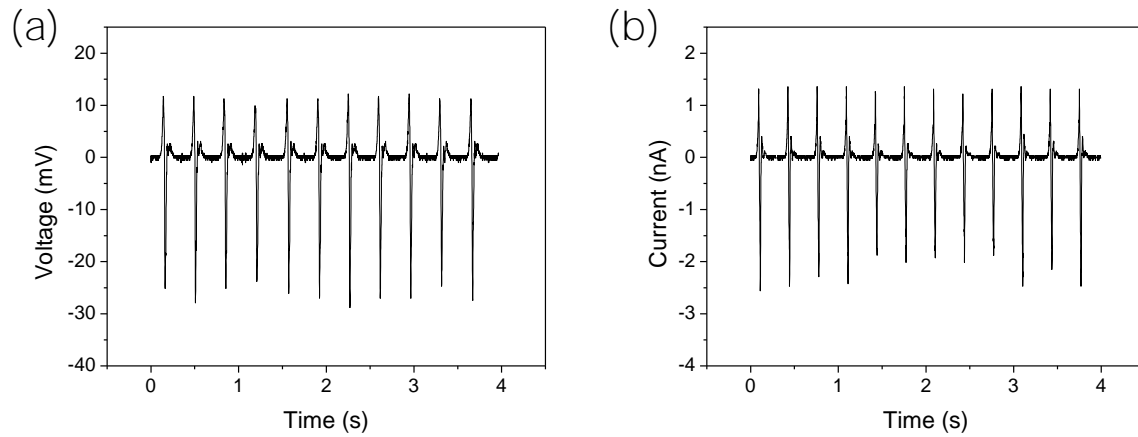


Figure S3. Piezoelectric (a) open-circuit voltage and (b) short-circuit current measured from the magnetic $\text{Fe}_3\text{O}_4@\text{SiO}_2$ nanorodes embedded P(VDF-TrFE) nanofiber mats.