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Effects of Gentle Topography on Forest-Atmosphere Gas Exchanges and Implications for Eddy-Covariance Measurements

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Peer reviewed

1       **Effects of Gentle Topography on Forest-Atmosphere**  
2       **Gas Exchanges and Implications for Eddy-Covariance**  
3       **Measurements**

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8       **Key Points:**

- 9       • Topography-induced flow structure causes strong heterogeneity in fluxes of gases  
10       emitted in forests  
11       • Flux heterogeneity is not reduced with increasing measurement height  
12       • Implications for tower-based eddy-covariance measurements are discussed

## Abstract

The interpretation of tower-based eddy-covariance (EC) turbulent flux measurements above forests hinges on three key assumptions: (1) steadiness in the flow statistics, (2) planar homogeneity of scalar sources or sinks, and (3) planar homogeneity in the flow statistics. Large eddy simulations (LES) were used to control the first two so as to explore the break-down of the third for idealized and real gentle topography such as those encountered in Amazonia. The LES runs were conducted using uniformly distributed sources inside homogeneous forests covering complex terrain to link the spatial patterns of scalar turbulent fluxes to topographic features. Results showed strong modulation of the fluxes by flow features induced by topography, including large area with negative fluxes compensating “chimney” regions with fluxes almost an order of magnitude larger than the landscape flux. Significant spatial heterogeneity persisted up to at least two canopy heights, where most eddy-covariance measurements are performed above tall forests. A heterogeneity index was introduced to characterize and contrast different scenarios and a topography categorization was shown to have predictive capabilities in identifying regions of negative and enhanced fluxes.

## 1 Introduction

Plant canopies such as forests and crops are major sources or sinks of gases including water vapor, carbon dioxide, ozone, and a variety of biogenic volatile organic compounds. The strength of these sources and sinks as well as their temporal dynamics is now routinely quantified using turbulent flux measurements near the canopy-atmosphere interface. The deployment of eddy-covariance (EC) systems on towers has become the standard method to measure scalar fluxes and now serves as ground truth for model evaluation. The majority of some 500 sites contributing data to FLUXNET network (Baldocchi et al., 2001; Baldocchi, 2008) use single point EC measurements to characterize scalar fluxes from a large region of relatively uniform surface cover. The validity of this approach hinges on the representativeness of the point where the tower is located. Typically, single-point EC-based turbulent flux measurements above canopies can be interpreted as landscape fluxes under stationary conditions, in the absence of subsidence or other mean advective terms, and for planar homogeneous source or sink strength distribution within the canopy (Baldocchi et al., 2000). However, such niceties remain rare in practice and the application of EC observations can lead to biased estimations of landscape fluxes even for gentle topographic variations (Katul et al., 2006; Belcher et al., 2012).

The focus of this work is on the canopy-atmosphere gas exchanges from a horizontally uniform forest situated on gentle topography for a neutrally stratified stationary atmospheric flow. Under these conditions, all the spatial variability of scalar fluxes is caused by topography-induced flow features, not variability in scalar sources or sinks or heterogeneity in canopy aerodynamic or physiological properties. Flow inside canopies covering cosine hilly terrain are known to experience flow separation leading to a recirculation region on the lee side of topographic features (Finnigan & Belcher, 2004; Poggi & Katul, 2007; Belcher et al., 2012). Early wind tunnel investigations of flow over forested and non-forested hills showed that forests reduced the velocity at the crest of the hill and led to an earlier flow separation (Ruck & Adams, 1991). Analytical solutions for the mean momentum balance within a uniform dense plant canopy covering a gentle (i.e., with small slopes) isolated hill were also used to explore the onset of recirculation (Finnigan & Belcher, 2004). Further extension of the theory led to the conclusion that the critical slope for flow separation over a canopy-covered hill is much lower than that over a hill covered with short roughness (Ross & Vosper, 2005), the latter being accurately predicted by (Wood, 1995). This effect was mainly explained by a balance between the adverse pressure gradient on the lee-side of the hill and the distributed canopy drag force (absent in rough surfaces). This dominant balance is caused by complete momentum absorption in the deep canopy layer, where turbulent fluxes (and their gradients) are small. Other work

65 extended these arguments by including longitudinal advection and mean vertical velocity-  
 66 pressure interactions, but the generic features of the recirculation zone were not altered  
 67 (Poggi et al., 2008). Most of these features have been supported by LES studies of idealized  
 68 topography such as isolated ridges (Dupont et al., 2008) and hills (Patton & Katul,  
 69 2009; Liu et al., 2019). The few studies that include real topography have focused on steeper  
 70 slopes, for which separation would occur even in the absence of canopy cover (e.g., Grant  
 71 et al., 2015, 2016; Liu et al., 2016).

72 The effects of flow separation on the transport of scalars emitted within the canopy  
 73 has been recently explored using elementary topography (such as isolated hills or sinusoidal  
 74 ridges, where one mode of topographic variability is considered) in flume exper-  
 75 iments and numerical simulations. The flow separation and the recirculation region lead  
 76 to strong spatial variability of scalar fluxes with enhanced fluxes in the separation re-  
 77 gion (Katul et al., 2006; Ross, 2011). This effect is stronger for gases emitted near the  
 78 ground than for gases emitted near the canopy top (Ross & Harman, 2015; Chen et al.,  
 79 2019). Flume experiments (Poggi & Katul, 2007) and numerical simulations (Chen et  
 80 al., 2019) revealed that the transport of fluid parcels out of the canopy in the flow sep-  
 81 aration region is mostly carried by turbulent eddies (and not by the mean recirculating  
 82 flow), displaying periodic cycles of gas accumulation within the canopy and ejection out  
 83 of the canopy. The separation point is a region of horizontal flow convergence, and the  
 84 build up of concentration inside the canopy at this location is promoted by horizontal  
 85 advection (Chen et al., 2019) towards the recirculation zone. The increased transport  
 86 out of the canopy at the separation point reflects a large effective footprint inside the  
 87 canopy, and this phenomenon was termed the “chimney effect” (Chen et al., 2019). No  
 88 systematic study has been performed over real topography to assess the role or persis-  
 89 tence of such chimney effect on turbulent fluxes above the canopy.

90 To progress on this issue, scalar fluxes over gentle forested topography were deter-  
 91 mined using large eddy simulations (LES) and then analyzed by extending an earlier study  
 92 (Chen et al., 2019) in two ways: (1) unlike the prior study that focused on escape of air  
 93 parcels released inside the canopy, gas fluxes were quantified by tracking particles mov-  
 94 ing into and out of the forest, and (2) results from an idealized topography consisting  
 95 of sinusoidal ridges were also contrasted with those obtained from a small region of real  
 96 topography from the Amazon forest.

## 97 **2 Methods**

### 98 **2.1 Numerical modeling**

99 Large eddy simulation (LES) was employed to generate the three-dimensional flow  
 100 field within and above the forest canopy, and a Lagrangian tracking model to study gas  
 101 transport. In the LES, a distributed drag force modeled by the quadratic drag law was  
 102 used to represent the main effects of the solid canopy on the flow (Shaw & Schumann,  
 103 1992; Pan et al., 2014). An immersed boundary method (IBM) with a signed-distance  
 104 function was employed to represent the topography on a cartesian grid (Peskin, 1972;  
 105 Chester et al., 2007), and a second-order accurate smoothing method (Li et al., 2016)  
 106 to reduce the Gibbs phenomenon at the fluid-solid interface caused by the pseudo-spectral  
 107 discretization. Lagrangian trajectories were determined using the resolved velocities from  
 108 the LES and a subgrid-scale velocity obtained from a Langevin equation (Weil et al., 2004).  
 109 Particle positions were integrated using the stable scheme described by Bailey (2016).  
 110 A more complete description of the model is given elsewhere (Chen et al., 2019).

### 111 **2.2 Simulation setup**

112 We employed three simulations to assess the effects of topography on the flux of  
 113 gases emitted from forests: (i) over flat topography, (ii) over an idealized topography with

114 sinusoidal ridges, and (iii) over real topography. All simulations were designed to rep-  
 115 resent the Amazon forest near the K34 research tower (Tóta et al., 2012; Fuentes et al.,  
 116 2016). A summary of simulation parameters is listed in Table 1. The flat topography  
 117 and the sinusoidal topography are the cases S0.0 and S0.2 described in Chen et al. (2019).

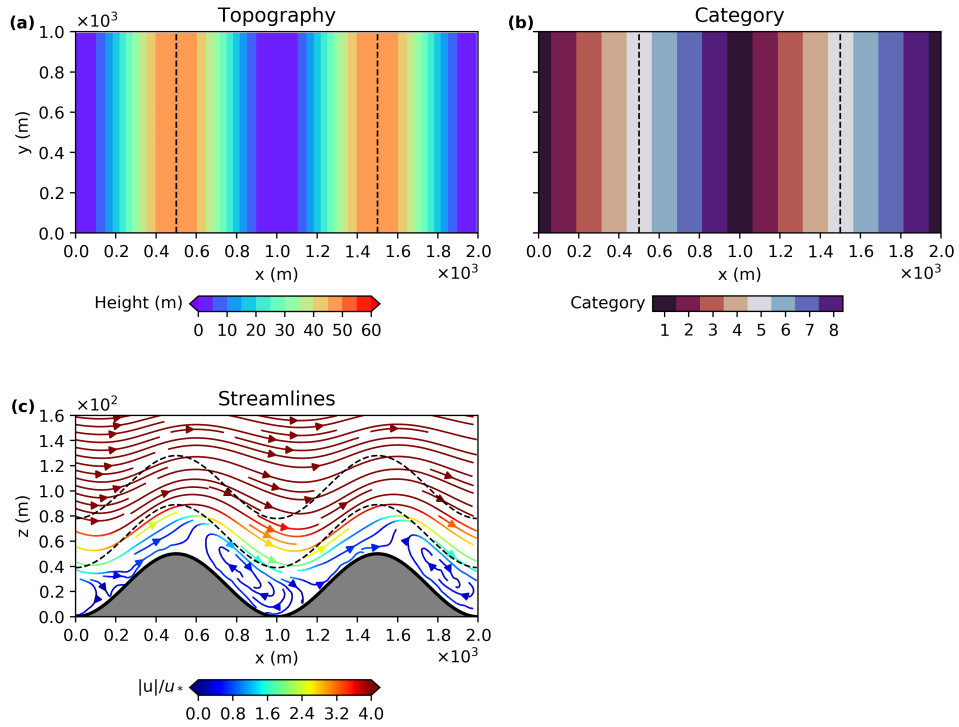
Variables	Symbols	Idealized	Real	Flat
Horizontal domain size (m)	$L_x \times L_y$	$2000 \times 1000$	$3000 \times 3000$	$2000 \times 1000$
Vertical domain size (m)	$L_z$	540	540	515
Horizontal grid resolution (m)	$dx \times dy$	$6.25 \times 6.25$	$8 \times 8$	$6.25 \times 6.25$
Vertical grid resolution (m)	$dz$	2	2	2
Mean topography height (m)	$\langle z_t \rangle$	25.00	26.46	0
Canopy height (m)	$h_c$	39	39	39
Leaf area index ( $\text{m}^2/\text{m}^2$ )	$LAI$	7.0	7.0	7.0
Pressure gradient acceleration ( $\text{m}/\text{s}^2$ )	$\frac{1}{\rho} \frac{dp_0}{dx}$	$3.11 \times 10^{-4}$	$3.11 \times 10^{-4}$	$3.11 \times 10^{-4}$
Total number of Lagrangian parcels	$N$	$1.71 \times 10^8$	$3.42 \times 10^8$	$3.42 \times 10^7$
Time step (s)	$dt$	0.1	0.1	0.1

**Table 1.** Configuration used in numerical simulations.

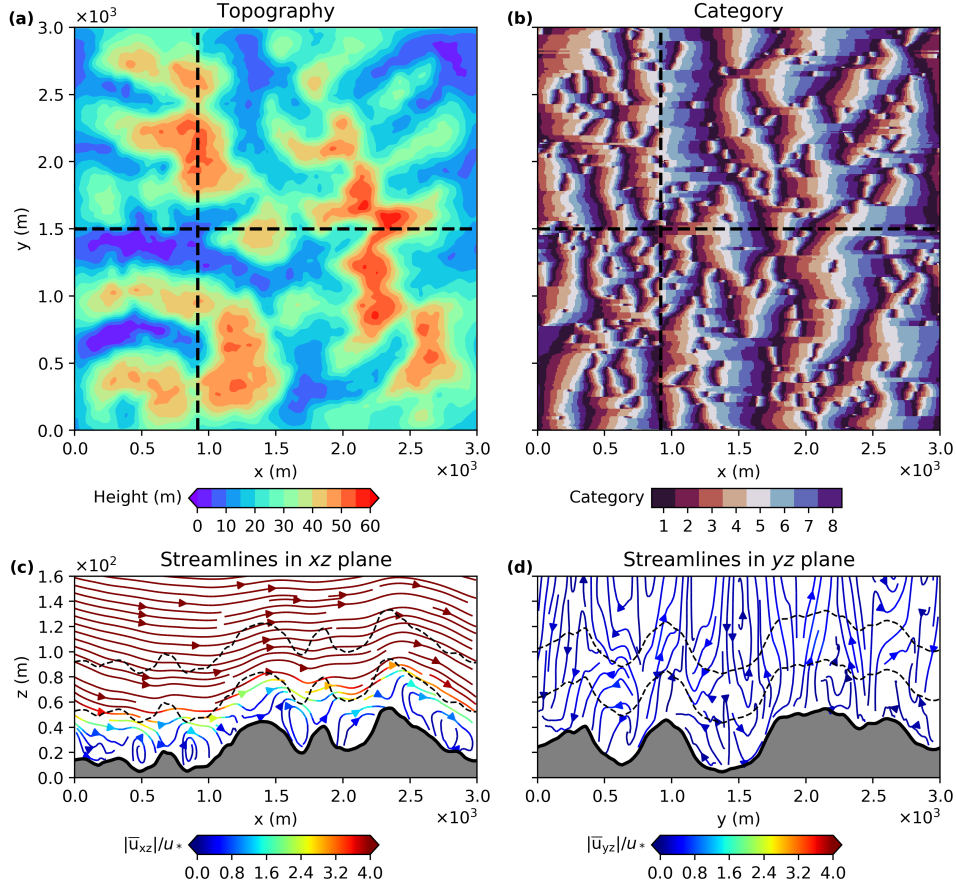
118 The forest canopy was assumed to be horizontally homogeneous and continuous  
 119 across the entire domain. The leaf area density (LAD) profile  $a(z)$  was based on data  
 120 from Tóta et al. (2012) reported in Fuentes et al. (2016), with a total leaf area index  $LAI =$   
 121  $7 \text{ m}^2/\text{m}^2$  and a canopy height  $h_c = 39 \text{ m}$  (note that estimates of  $LAI$  in the region near  
 122 the K34 tower vary between 6.1 (Marques Filho et al., 2005) and 7.3 (Tóta et al., 2012),  
 123 and prior simulation for this region have used  $LAI$  of 6.0 (Gerken et al., 2017) or 7.0 (Chen  
 124 et al., 2019)). The resulting canopy adjustment length (Belcher et al., 2003) was  $L_c =$   
 125  $1/(C_d \bar{a}) = 13.9 \text{ m}$ , where  $\bar{a} = 0.18 \text{ m}^{-1}$  was the average LAD of the canopy and  $C_d$   
 126 was the drag coefficient assumed constant. Note that for the idealized and real topogra-  
 127 phies we have  $L_c/\Delta x \approx 2.2$  and  $L_c/\Delta x \approx 1.7$ , respectively (even though these ratios  
 128 would be concerning in the simulation of forest edges, for the homogeneous canopy used  
 129 here this was not deemed a problem).

130 In the idealized topography case, the topography height  $z_t(x)$  was described by a  
 131 cosine function (Figure 1a). The idealized topography shape was defined by a ridge height  
 132  $H = 50 \text{ m}$  (twice of the amplitude of the cosine function) and a ridge half-length  $L =$   
 133  $250 \text{ m}$  (one forth of the topography wavelength), where the nomenclature follows Finnigan  
 134 and Belcher (2004). The canopy was categorized as a deep canopy because  $h_c/L_c > 1$   
 135 (Finnigan & Belcher, 2004; Poggi et al., 2008).

136 For the real topography simulation we selected a region centered at  $-2.413^\circ \text{ S}$ ,  $-60.504^\circ \text{ W}$ ,  
 137 because it was characterized by gentle topography and no large-scale valleys or ridges.  
 138 This ensured that the flow could be properly represented in a relatively small domain  
 139 ( $3 \text{ km} \times 3 \text{ km}$ ). The topography was obtained from the NASA shuttle radar topogra-  
 140 phy mission (SRTM) global 1 arc second data (Werner, 2001; Farr et al., 2007), which  
 141 has a horizontal resolution of about 30 meters. A simple bilinear scheme was applied to  
 142 interpolate the topography data to the grid resolution of the simulation. Then, to con-  
 143 form with periodic boundary conditions required by the pseudo-spectral discretization  
 144 in the LES, a special smoothing was applied to the topography on the edges of the do-  
 145 main. Details about the edge smoothing process and the original topography are pro-  
 146 vided in the Text S1 in the supporting information, while the final topography used in  
 147 the simulation is presented in Figure 2a.



**Figure 1.** (a) Topography, (b) topography categorization, and (c) mean flow streamlines on the  $xz$ -plane for the ideal topography simulation. The black dashed lines in (a) and (b) indicate the location of ridge crests. The black dashed lines in (c) indicate  $Z_m/h_c = 1$  and  $Z_m/h_c = 2$ . Notice that the aspect ratio is not one in panel (c).



**Figure 2.** (a) Topography, (b) topography categorization, and mean flow streamlines on the (c)  $xz$ -plane and (d)  $yz$ -plane for the real topography simulation. The black dashed lines in (a) and (b) indicate the location of the cross-sections shown in (c) and (d), respectively. The black dashed lines in (c) and (d) indicate  $Z_m/h_c = 1$  and  $Z_m/h_c = 2$ . Notice that the aspect ratio is not one in panels (c) and (d).

148 All simulations were driven by a constant mean pressure gradient force (correspond-  
 149 ing to an acceleration of  $3.11 \times 10^{-4} \text{ m/s}^2$ ) in the streamwise direction with no ther-  
 150 mal stratification and no buoyancy fluxes. For the simulation without topography, this  
 151 resulted in a friction velocity of approximately 0.4 m/s. Coriolis effects were neglected  
 152 due to the low latitude of the selected region. A wall model was applied at the ground  
 153 surface and a free-slip condition with a damping layer was applied at the top of the do-  
 154 main. A logarithmic mean velocity profile perturbed with random noise was used as ini-  
 155 tial condition. Simulations were integrated for 8 hours in total, and three-dimensional  
 156 velocity fields from the last 5 hours were saved every second to run the Lagrangian track-  
 157 ing model.

158 In the Lagrangian tracking model, air parcels were released from 19 levels equally  
 159 spaced between 1 m and 37 m above the ground. For data analysis purposes, these 19  
 160 source levels were further categorized into 4 layers: the lowest source height, character-  
 161 izing near-ground emissions and termed “near-surface source”; the remaining 18 source  
 162 heights were equally divided into three layers characterizing emissions in the “lower”, “mid-  
 163 dle” and “upper” canopy. The initial horizontal positions of air parcels were randomly  
 164 assigned from a uniform distribution, and a large number of air parcels (see Table 1) were  
 165 released to guarantee statistical convergence. Air parcel releases were evenly distributed  
 166 during the 5-hour simulation, and the last 4 hours corresponding to statistical steady  
 167 state for particle concentration and fluxes were used. Parcel trajectories were integrated  
 168 with 0.1 s time interval and the motion of each particle trajectory was terminated once  
 169 its horizontal displacement reached one domain length or width to prevent double count-  
 170 ing in the flux and footprint function. The position and velocity of each parcel were recorded  
 171 each time it crossed one of three sampling heights  $Z/h_c = 1, 1.5, \text{ and } 2$ , where  $Z =$   
 172  $(z - z_t)$  is the height above ground. These records were used to calculate the total flux  
 173 across the three sampling heights  $\overline{F}(x, y)$  and the source area contributing to that flux.  
 174 These fluxes correspond to the total time averaged values (including the mean flux and  
 175 the turbulent flux) in the direction perpendicular to the topography (and to the canopy  
 176 top). Only for the flat case and in special locations for the topography cases, this flux  
 177 corresponds to the vertical flux. The horizontal grid resolution of the flux calculation was  
 178  $33 \text{ m} \times 33 \text{ m}$ . We interpreted the local time averaged flux  $\overline{F}(x, y)$  as representative of  
 179 a tower measurement (using a planar-fit coordinate system) and the horizontally aver-  
 180 aged flux  $\langle \overline{F} \rangle$  as representative of the landscape flux. Thus, only when  $\overline{F}(x, y) / \langle \overline{F} \rangle \approx$   
 181 1, the local measurements can be considered as representative of the landscape fluxes.

### 182 3 Results

#### 183 3.1 Characteristics of the mean flow

184 For the idealized topography, mean flow separation was observed right after the top  
 185 of the ridge, and the recirculation flow spanned the entire vertical extent of the canopy  
 186 (Figure 1c). This result has been previously reported (Chen et al., 2019) and explained  
 187 by conventional arguments (Finnigan & Belcher, 2004): the canopy was deep compared  
 188 to the adjustment length ( $h_c/L_c = 2.8 > 1$ ) so that the momentum transported from  
 189 the air layer above the canopy was mostly absorbed by the upper canopy, not being able  
 190 to penetrate the entire canopy layer. The turbulent momentum flux gradient in the ver-  
 191 tical was small near the ground, so that the dominant balance was between the topography-  
 192 induced crest-oriented pressure gradient force and the drag force. This balance produced  
 193 an inverse flow on the leeward side of the ridge, leading to flow separation.

194 In the real topography case, flow can go around topographic features such as hills,  
 195 producing a complex pattern. However, the main pattern in the streamwise direction was  
 196 similar to the idealized topography, with flow separation and recirculation regions down-  
 197 stream of every major topographic feature (Figure 2c). Even fairly small hills such as  
 198 the small bump at  $x = 250 \text{ m}$  in Figure 2c generated flow separation with a recircu-



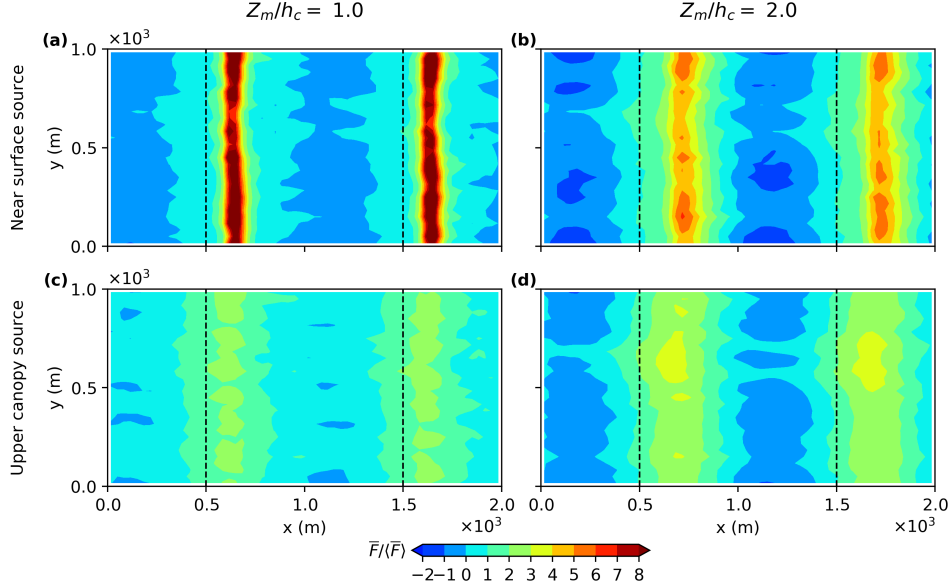
199 lation region. The spanwise direction was dominated by secondary flow structures, which  
 200 tended to be weaker than the streamwise recirculation regions. These secondary flow struc-  
 201 tures were not as clearly connected to the spanwise topography as the streamwise pat-  
 202 terns, being driven in large part by streamwise flow structures and conservation of mass.

### 203 3.2 Gas fluxes above the canopy

204 For the simulation over flat topography, the scalar fluxes at all three measurement  
 205 heights were approximately independent of horizontal location and equal to the land-  
 206 scape flux as expected, except for small randomly distributed deviations caused by sta-  
 207 tistical sampling (not shown). Results for the idealized topography were in stark con-  
 208 trast with those for flat topography, displaying organized regions of enhanced fluxes and  
 209 regions with negative fluxes (Figure 3). The region of enhanced fluxes was located down-  
 210 wind from the crest, near the separation point, consistently with the chimney effect (Chen  
 211 et al., 2019) and with other previous model results (Katul et al., 2006; Ross, 2011; Ross  
 212 & Harman, 2015). The amplitude of the enhanced fluxes depended on the combination  
 213 of source height and sampling height, with the largest fluxes being almost one order of  
 214 magnitude larger than the landscape fluxes in the worst case scenario of near-surface emis-  
 215 sions with sampling at canopy top (Figure 1a). The negative flux region downwind of  
 216 the trough in the topography was caused by the persistent mean flow directed into the  
 217 canopy in this region (see Figure 1c), which carried gas exported through the chimney  
 218 back into the forest. The negative fluxes were also large, with magnitude comparable to  
 219 the landscape flux. This dynamics led to a pattern of positive and negative fluxes that  
 220 was “attached” to the topography. Sampling fluxes at twice the canopy height led to a  
 221 modest reduction in the flux enhancement, but it increased the magnitude of the neg-  
 222 ative fluxes (Figure 3b). As the gas source was moved from the near-surface layer to the  
 223 upper canopy, a progressive reduction in the amplitude of the pattern was observed, reach-  
 224 ing a minimum for sources positioned at the canopy top (Figure 3c). This was, in part,  
 225 because sampling was very close to the source and there was less time for the flow or-  
 226 ganization to modulate transport. Note that, contrary to intuition, elevating the sam-  
 227 pling height amplified the non-uniformity of the fluxes for sources near the canopy top  
 228 (Figure 3d). This result may seem contradictory to those from Ross and Harman (2015),  
 229 who showed a decrease in non-uniformity with increasing height. However, the appar-  
 230 ent contradiction is caused by the different choice in coordinate systems: Ross and Har-  
 231 man (2015) uses a global cartesian coordinate system, and while their vertical flux be-  
 232 comes more uniform with height, the opposite is observed for the horizontal flux. Re-  
 233 sults presented here consider fluxes across surfaces parallel to the topography, which com-  
 234 bine vertical and horizontal fluxes.

235 Results were similar for the real topography case (Figure 4), where the flux pat-  
 236 terns were clearly connected to the topographical organization in the streamwise direc-  
 237 tion. The chimney effect still produced regions of large flux enhancement at every separ-  
 238 ation point (i.e., on the leeward side of each hill). The negative fluxes had larger mag-  
 239 nitude than those in the idealized topography and even for the sources in the upper canopy  
 240 with sampling at canopy top, negative fluxes were larger in magnitude than the land-  
 241 scape flux (Figure 4c). The similarity of the fluxes sampled at  $Z_m/h_c = 2$  for sources  
 242 near the surface and in the upper canopy was remarkable (Figures 4b,d), suggesting that  
 243 the flux patterns observed at this height were mostly determined by the flow field above  
 244 the canopy.

245 As a means to further quantify the flux non-uniformity, we defined the cumulative  
 246 normalized flux as the maximum fraction of the total normalized flux contributed by a  
 247 fraction of the total area. This was obtained by integrating the flux sorted in a mono-  
 248 tonically decreasing fashion. Mathematically, we represented this via  $CF(A_f)$ , where  $A_f$   
 249 is the area fraction increasing monotonically from 0 to 1, and  $CF$  is the cumulative flux  
 250 integrated over the area fraction. For a uniform flux, such as that from flat topography,

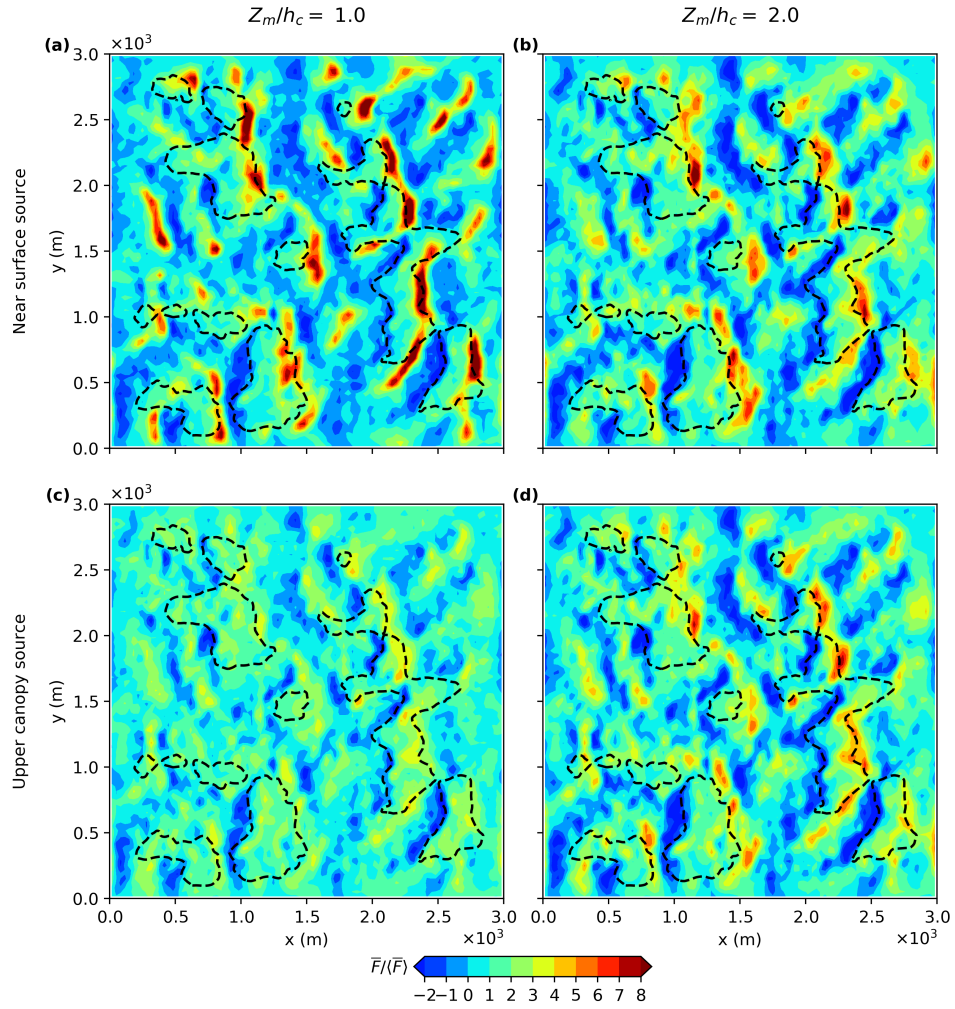


**Figure 3.** Normalized fluxes  $\bar{F}(x, y)/\langle \bar{F} \rangle$  from the ideal topography simulation for different combinations of source layers and sampling heights. Mean wind is from left to right. The black dashed lines indicate the location of ridge crests.

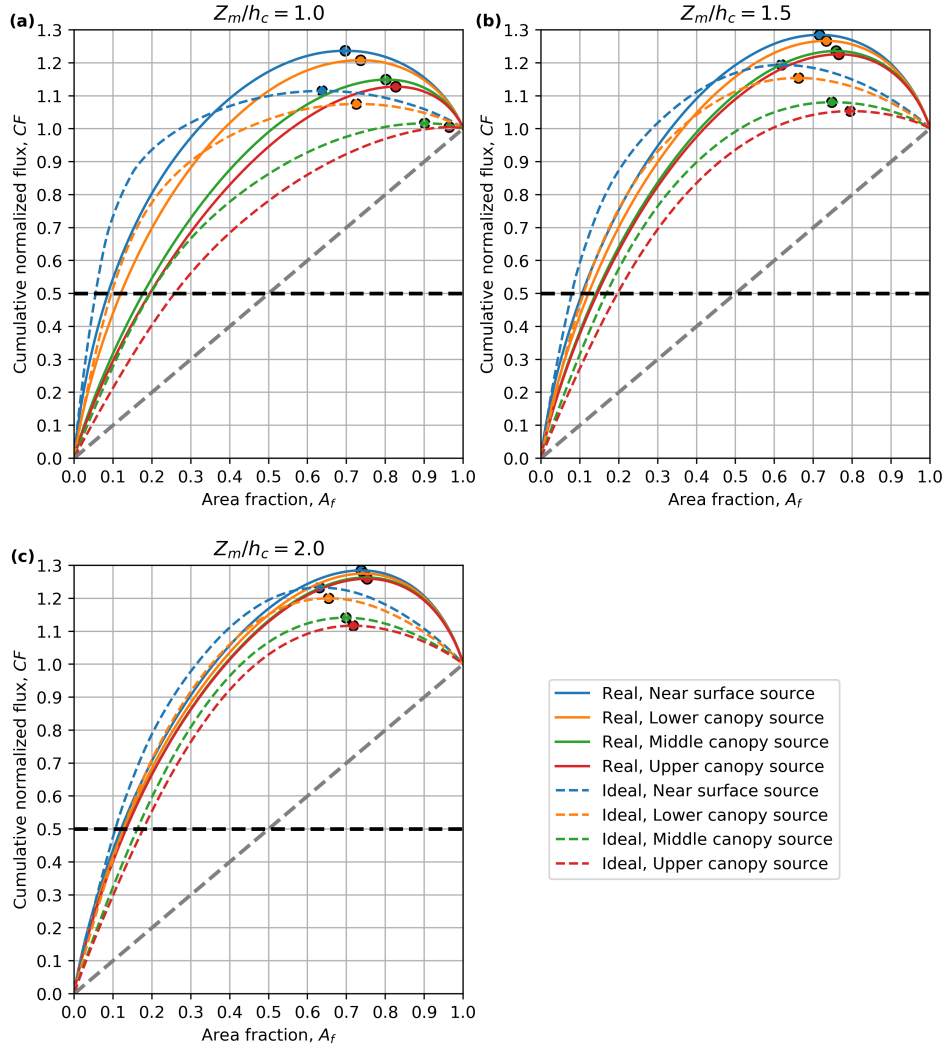
251  $CF(A_f) = A_f$ . For nonuniform flux distributions,  $CF(A_f)$  first increases faster than  
 252 the uniform case and then slower, due to the sorting of the fluxes in the integration. The  
 253 resulting curves for  $CF(A_f)$  are shown in Figure 5, where the curve for a uniform flux  
 254 is also shown for comparison. Note that the cumulative fluxes are not monotonic due to  
 255 the presence of negative fluxes. The black dashed line indicates 50% of the total flux over  
 256 the entire domain and its intercept with any  $CF$  gives the minimum fraction of the total  
 257 area contributing to 50% of the flux. As an example, take the most uniform case of  
 258 upper canopy source with sampling at canopy top for the idealized topography (red dashed  
 259 line in Figure 5a). The  $CF$  shows that approximately 50% of the flux originates from  
 260 the 25% of the total area, and 80% of the flux from 50% of the area. There are almost  
 261 no regions with negative fluxes, as the circle marking the peak in the  $CF$  is almost at  
 262 100% of the area. In contrast, for the near surface source (blue dashed line), 50% of the  
 263 fluxes originates from only 5% of the area and almost 35% of the area corresponds to  
 264 negative fluxes, as the maximum in the  $CF$  is close to 65% of the area. Note that for  
 265 almost all the combinations of source height and sampling height, and for both idealized  
 266 and real topography, less than 20% of the area contributes 50% of the total flux.

267 When interpreting the cumulative scalar fluxes, two key variables must be considered:  
 268 the slope of the curves at the low area fractions (a measure of the intensity of the  
 269 chimney effect) and the maximum value of the  $CF$ , which is a measure of the strength  
 270 of negative fluxes. A few general trends in the flux heterogeneity can be identified in the  
 271 results presented in Figure 5. The real topography showed less sensitivity to source height  
 272 than the idealized case, and the sensitivity decreased with increasing sampling height  
 273 for both cases. The real topography case showed a more pronounced influence of negative  
 274 fluxes, not necessarily in terms of spatial extension, but rather in total integrated  
 275 value.

As one bulk measure of flux non-uniformity, a heterogeneity index  $G_h$  can be introduced, which is defined as the area between the cumulative flux  $CF$  for any given case



**Figure 4.** Normalized fluxes  $\bar{F}(x, y)/\langle \bar{F} \rangle$  from the real topography simulation for different combinations of source layers and sampling heights. Mean wind is from left to right. The black dashed lines indicate the location where  $z_t = 40$  m.



**Figure 5.** Cumulative normalized fluxes as a function of area fractions at different sampling heights: (a)  $Z_m/h_c = 1.0$ , (b)  $Z_m/h_c = 1.5$ , and (c)  $Z_m/h_c = 2.0$ . The gray dashed line indicates behavior for a uniform flux and the black dashed line indicate 50% of the total flux. The dot on each curve marks the maximum cumulative distribution function.

and the uniform case (labeled  $CF_u$ ), normalized by the uniform case. That is,

$$G_h = \frac{\int_0^1 [CF(A_f) - CF_u(A_f)] dA_f}{\int_0^1 CF_u(A_f) dA_f} = 2 \int_0^1 CF(A_f) dA_f - 1. \quad (1)$$

276 The index  $G_h$  is analogous to the Gini index used in economics to quantify wealth dis-  
 277 tribution from a Lorenz curve representation (Lorenz, 1905). Similarly to the Gini in-  
 278 dex, the minimum value  $G_h = 0$  represents uniform fluxes and as the flux become less  
 279 uniform the value of  $G_h$  increases. However, differently from the Gini that is bounded  
 280 by 1,  $G_h$  does not have an upper bound because fluxes can be negative. Values of  $G_h$   
 281 are given in Table 2 and some interesting, more quantitative characterizations can be  
 282 made. For all combinations of source and sampling heights, fluxes over the real topog-  
 283 raphy were less uniform than over the ideal topography. In addition, lower sources al-  
 284 ways produced less uniform fluxes than sources higher up in the canopy even though the  
 285 differences became less pronounced as sampling height increased. Finally, increasing sam-  
 286 pling height had small influence on the non-uniformity of fluxes from the near surface  
 287 and lower canopy, increasing significantly the non-uniformity of fluxes from the middle  
 288 and upper canopy.

Source layer	Sampling height	Heterogeneity index			Mean source area	
		Ideal	Real	Flat	Ideal	Real
Near surface	1	0.97	1.00	2.27	4.16	5.40
	1.5	0.99	1.01	4.44	8.11	8.88
	2	0.97	0.97	7.86	11.12	12.30
Lower canopy	1	0.80	0.89	0.92	2.42	5.31
	1.5	0.87	0.95	2.72	7.29	10.15
	2	0.89	0.94	6.01	12.08	15.34
Middle canopy	1	0.51	0.70	0.30	0.65	1.83
	1.5	0.67	0.87	1.65	2.96	6.63
	2	0.75	0.92	4.79	7.62	12.65
Upper canopy	1	0.38	0.64	0.20	0.39	1.12
	1.5	0.58	0.85	1.74	2.42	5.82
	2	0.70	0.91	4.92	6.50	11.94

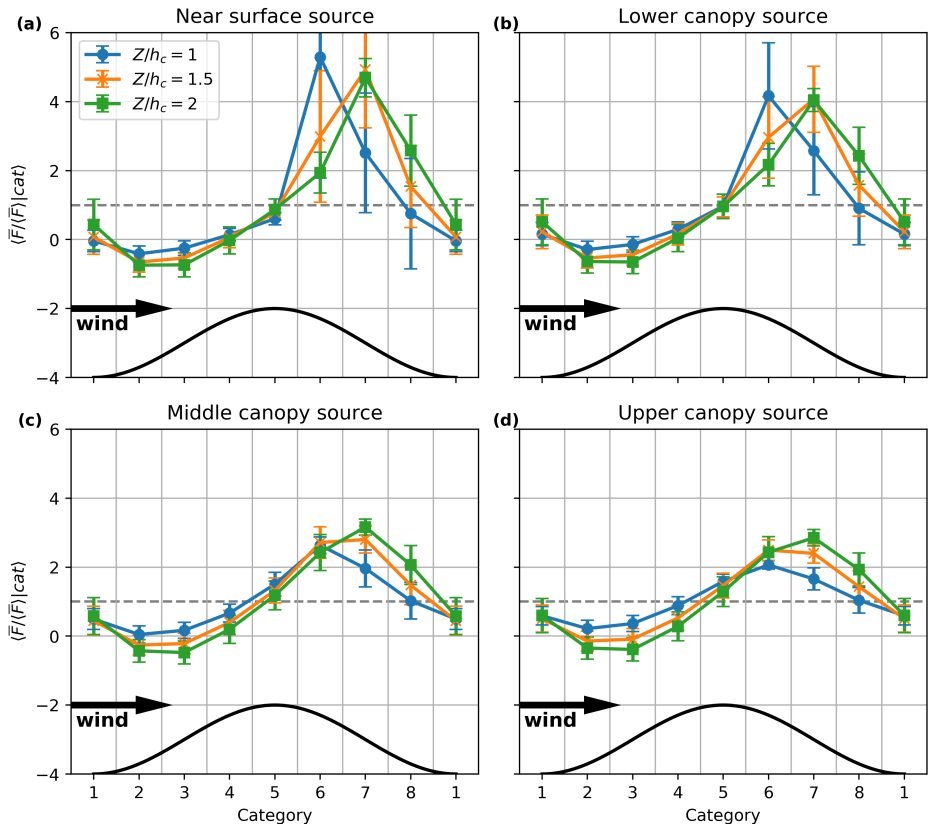
**Table 2.** Heterogeneity index ( $G_h$ ) and mean source area contributing 50% of the total flux ( $\Omega_{50}$  in  $\times 10^4$  m<sup>2</sup>).

### 289 3.3 Categorization of topography

290 It is evident from Figures 3 and 4 that the flux patterns share strong resemblance  
 291 with the topography underneath (albeit with some phase-differences due to advection).  
 292 To further explore this fact, we designed a topography categorization based on the re-  
 293 sults for the idealized case. We first divided the topography wavelength into 8 equal seg-  
 294 ments labeled category 1-8, with the category 1 centered on the trough and category 5  
 295 centered on the crest (Figure 1b). Because the flux patterns were strongly related to the  
 296 streamwise topography, in the real topography case only the streamwise direction was  
 297 taken into account. The categorization proceeded by finding two consecutive crests in  
 298 the streamwise direction, and splitting the crest–trough distance into 5 categories (1 to  
 299 5) and the trough–crest distance into another 5 (5 to 8 and then 1). This procedure re-

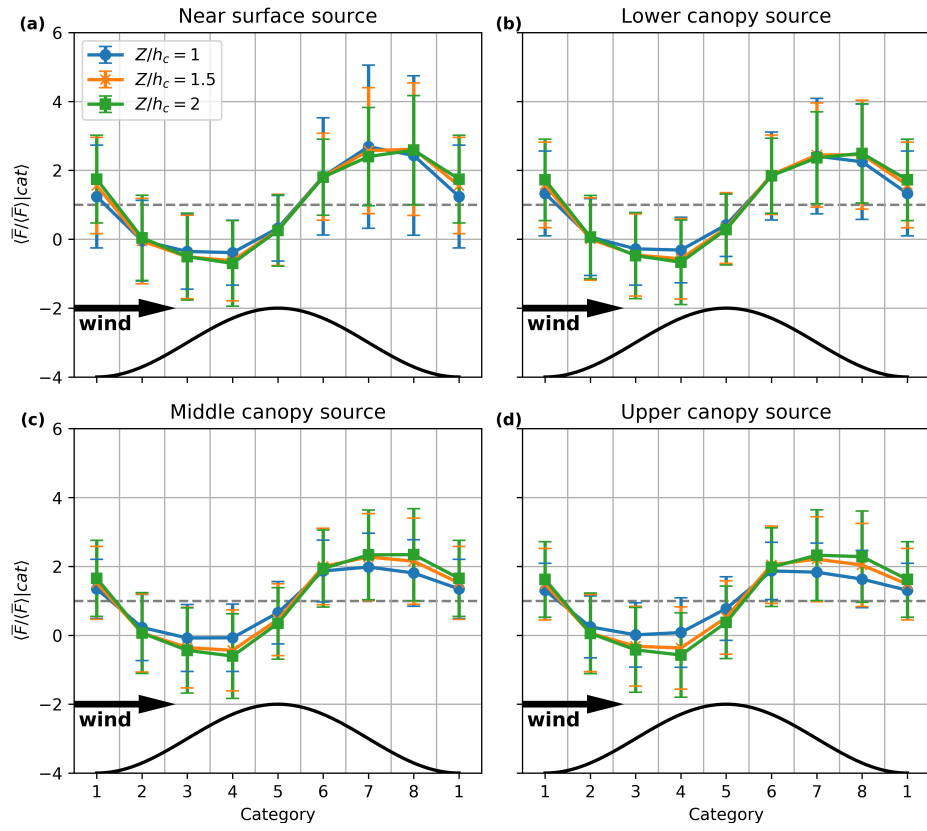
300 sulted in a complex pattern (Figure 2b). In the real topography, the area assigned to a  
 301 crest is asymmetric because the upwind and downwind troughs are not equally spaced  
 302 from the crest (the same is true for the area around troughs).

303 We calculated average fluxes conditioned on topography category,  $\langle \bar{F} / \langle \bar{F} \rangle | cat \rangle$ , and  
 304 the corresponding standard deviations. Results for the idealized topography (Figure 6)  
 305 presented large differences between categories with little variability within each category,  
 306 pointing to a strong coupling between topography and flux. The only exception to this  
 307 was the peak flux for near-ground and deep-canopy sources, for which the signature of  
 308 the chimney is concentrated in a narrow region causing large variability within the category  
 309 where the chimney is (Figure 6a,b).



**Figure 6.** Normalized flux conditionally averaged based on the topography categories for the ideal topography case for different combinations of source layers and sampling heights. Errorbars represent one standard deviation and the gray dashed line indicates the landscape flux.

310 The true test of the categorization was its application to the real topography (Fig-  
 311 ure 7). When compared to the ideal topography, the amplitude of the variation in the  
 312 conditional average flux was smaller and the variability within each category was much  
 313 larger. This was mostly because in this case there was a very large reduction in complex-  
 314 ity introduced by the categorization. All the hills, independently of length, height, and  
 315 slope received the same treatment. The crosswise topographical information was not taken  
 316 into account. Despite this simplification, a strong signal was still observed, with signif-  
 317 icant correlation between negative fluxes in the windward side and flux enhancement in  
 318 the leeward side of the hills. Increasing the number of categories or including informa-  
 319 tion about the crosswise topography did not seem to improve this relation (not shown).



**Figure 7.** Normalized flux conditionally averaged based on the topography categories for the real topography case for different combinations of source layers and sampling heights. Errorbars represent one standard deviation and the gray dashed line indicates the landscape flux.

320 To further test the topography categorization, we used the conditional averaged  
 321 fluxes and the topography categories to “reconstruct” the spatial structure of the fluxes.  
 322 As an example, we adopted the source from the upper-canopy with sampling at  $Z_m/h_c =$   
 323 2 as a test case, and simply assigned the mean values in Figure 7d to the topography cat-  
 324 egories, which resulted in the fluxes shown in Figure 8a. Even though the magnitude of  
 325 the fluxes were attenuated, this simple procedure was capable of separating regions of  
 326 flux enhancement and regions of negative flux when compared to the flux obtained di-  
 327 rectly from the LES (Figure 4d). This was confirmed by the fairly large correlation co-  
 328 efficient between the reconstructed fluxes and the original fluxes (Figure 8c), which in-  
 329 dicated that one could predict regions of flux enhancement and regions of negative fluxes  
 330 only based on the topography category. However, the accompanying large root-mean-  
 331 square-error (RMSE), which were close to or larger than the mean (Figure 8d), showed  
 332 that quantitative predictions solely based on the topography may not be possible. For  
 333 the real topography used here, in which no preferential directions exist, we assumed that  
 334 the conditional average fluxes were independent of wind direction, and applied the val-  
 335 ues in Figure 7d with a topography categorized for a different wind direction. As an ex-  
 336 ample, we used a mean wind blowing in the positive  $y$  direction, which resulted in the  
 337 fluxes shown in Figure 8b. This result highlighted the strong impact of wind direction  
 338 on the spatial patterns of the local flux.

### 339 3.4 Generalized footprint analysis

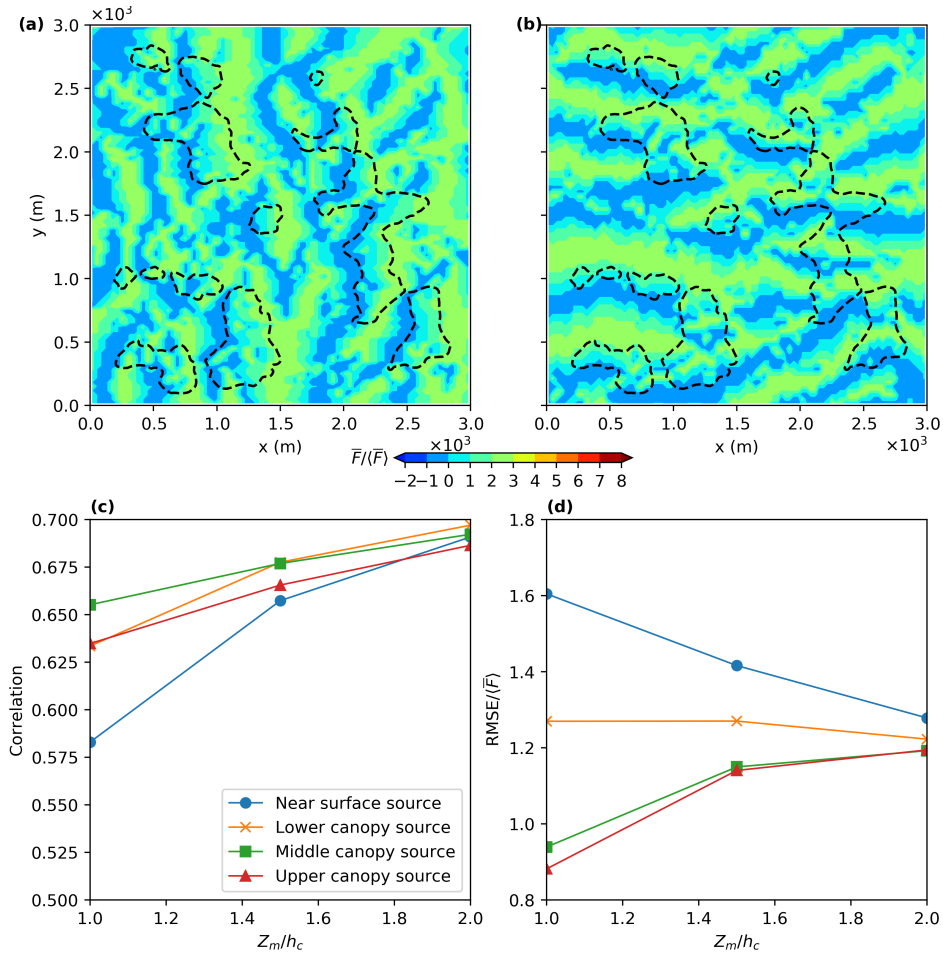
When considering EC measurements over flat heterogeneous landscapes, the foot-  
 print analysis plays an important role in placing flux towers so that the measured fluxes  
 are representative of the biome being studied (Finnigan, 2004). Following Schmid (2002),  
 the flux footprint function  $\phi_F(\mathbf{x}; \mathbf{x}')$  for measurement location  $\mathbf{x}$  and source/sink loca-  
 tion  $\mathbf{x}' = (x', y', Z')$  is defined by

$$F(\mathbf{x}) = \int_{\chi} Q(\mathbf{x}') \phi_F(\mathbf{x}; \mathbf{x}') d\mathbf{x}', \quad (2)$$

340 where  $Q(\mathbf{x}')$  is the distribution of source/sink in the vegetation volume  $\chi$ . In the present  
 341 case, the vertical extent of the four canopy layers defined in section 2.2 were used for the  
 342 vertical integration, resulting in footprint functions  $\phi_F(x, y, Z_m; Z')$  – two dimensional  
 343 fields for each pair of canopy source layer ( $Z'$ ) and measurement height ( $Z_m$ ). To char-  
 344 acterize the horizontal extension of the source area, we adopted the source area of level  
 345  $P$  for measurement location  $\mathbf{x}$ , denoted by  $\Omega_P(x, y, Z_m; Z')$  and defined as the integral  
 346 of the footprint function over the smallest possible area comprising  $P\%$  of the total source  
 347 influence on the measured signal (Schmid & Oke, 1990; Schmid, 1994). In practice, the  
 348 footprint function is sorted in decreasing order before integration so that the area to con-  
 349 tribute  $P\%$  of the total integration is the smallest one. We used  $P = 50\%$  to charac-  
 350 terize source areas for fluxes corresponding to each pair of source layer and observation  
 351 height for all 3 simulations (flat, idealized, and real topographies). Spatial patterns of  
 352 the resulting source areas corresponding to the fluxes shown in Figs. 3 and 4 are presented  
 353 in the supporting information. In general, regions of negative fluxes tended to have large  
 354 source areas, and in many cases the chimney regions also had large source areas. How-  
 355 ever, segregating results based on the 8 topography categories introduced in section 3.3  
 356 did not add much predictive value. We only reported the mean source areas  $\langle \Omega_{50} \rangle$  in Ta-  
 357 ble 2 (these were calculated from averages over the entire horizontal plane).

358 For the flat topography simulation, in most cases the source area increased with  
 359 vertical distance between source height and sampling height. Thus, at a fixed sampling  
 360 height, the source area increased as the source height was moved lower into the canopy.  
 361 The presence of topography increased significantly the source area for all pairs of source  
 362 and sampling heights, and this increase was more accentuated in the real topography than  
 363 in the idealized case. The latter was associated with the scalar transport by secondary  
 364 flow circulations in the crosswise direction.

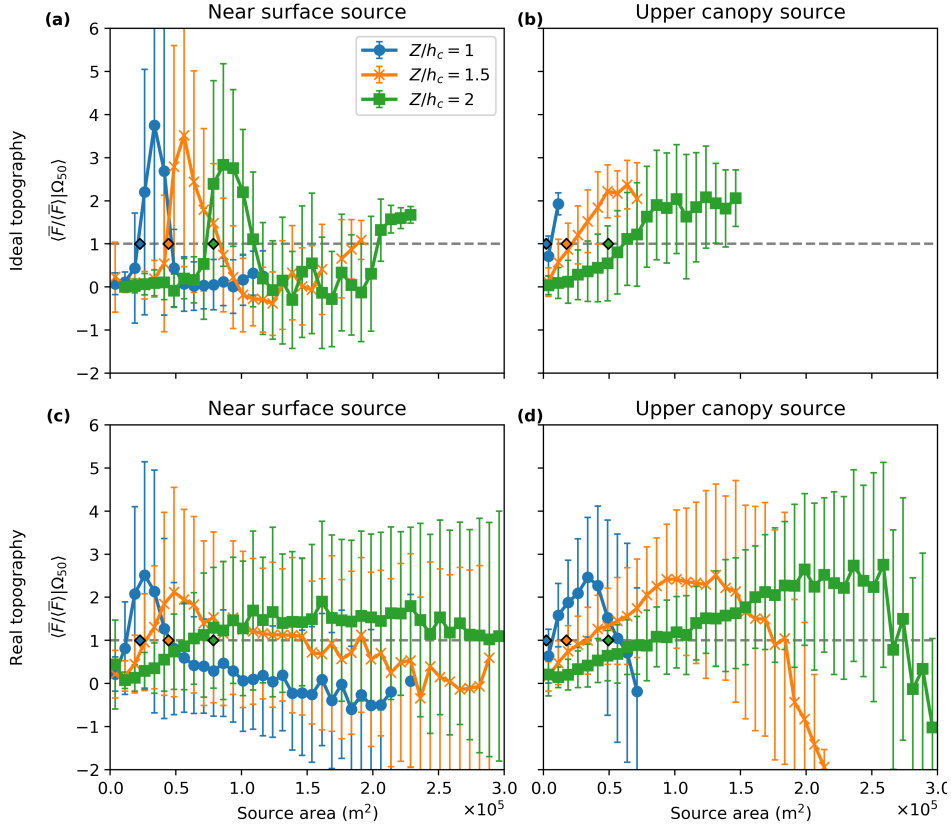




**Figure 8.** Normalized fluxes estimated from the topography categories for a source in the upper canopy and sampling at  $Z_m/h_c = 2.0$  for (a) mean wind from left to right and (b) mean wind from bottom to top. (c) Correlation coefficient and (d) root-mean-square-error (RMSE) between estimated flux shown in (a) and the real flux.

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The experience in scalar flux measurements over flat heterogeneous landscapes is that increasing the source area blends signatures of surface heterogeneity thereby increasing the representativeness of the observation (Schmid, 1994). The connection between source area and flux non-uniformity induced by topography was explored by calculating average fluxes and variances as a function of source area (i.e. conditional averages  $\langle \bar{F} / \langle \bar{F} \rangle | \Omega_{50} \rangle$  and conditional variances  $\langle (\bar{F} / \langle \bar{F} \rangle - \langle \bar{F} / \langle \bar{F} \rangle | \Omega_{50} \rangle)^2 | \Omega_{50} \rangle$ , where the operator  $\langle \cdot | \Omega_{50} \rangle$  represents the conditional average based on the value of  $\Omega_{50}$ ; Figure 9). The main feature of the conditional averages was the very large variability (quantified by the large errorbars corresponding to one standard deviation), which pointed to a very low correlation between the magnitude of the flux and the area of the footprint. This result confirmed the difficulty associated with interpreting footprints over complex terrain (Finnigan, 2004), and clearly showed that a larger footprint did not imply a better estimate of the landscape flux. Perhaps a surprising feature in Figure 9 was the fact that the largest fluxes were not necessarily associated with the largest source areas, but that the conditionally averaged flux was very close to the landscape flux when the source area matched the area over flat topography (indicated by the diamonds with black edges in the Figure). Note that in most cases the curves were not monotonic, and very large source areas tended to be associated with regions of negative fluxes.



**Figure 9.** Normalized flux conditionally averaged based on the source area  $\Omega_{50}$  for ideal and real topography.

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#### 4 Conclusions and implications for tower measurements

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In this work, LES was used to investigate the influences of gentle topography on the spatial distribution of fluxes of gases emitted uniformly within tall and dense forests.

386 Before any general conclusions can be drawn, we must emphasize that results presented  
 387 here were all based on one idealized topography and one realistic topography (note that  
 388 the idealized topography may be more representative of some real situations with quasi-  
 389 parallel ridges than the real topography). In addition, all simulations were performed  
 390 for neutral atmospheric stability. Fluxes were determined in the direction perpendicu-  
 391 lar to the topography (and to the canopy top), and interpreted as representative of tower-  
 392 like EC measurements using a planar-fit coordinate system. Simulations were performed  
 393 for a very dense forest ( $LAI = 7$ ), but we expect results to be applicable as long as the  
 394 deep canopy criterion  $h_c/L_c > 1$  is satisfied. Despite these restrictions, a number of con-  
 395 clusions can be drawn to guide EC observations over forests covering gentle topography.  
 396 Future studies should focus on effects of atmospheric stability and regional wind patterns  
 397 induce by topography and surface heterogeneities. Both extensions requires larger sim-  
 398 ulation domains than the one employed here.

399 It is clear from the results presented above that, for these conditions, estimating  
 400 landscape fluxes from a single tower measurement may lead to unacceptably large bias  
 401 in errors, and that the magnitude of these errors depend on the source height inside the  
 402 canopy. This is in agreement with the findings from Ross and Harman (2015) for an iso-  
 403 lated ridge. Local fluxes can be almost an order of magnitude larger than the landscape  
 404 flux. In a reasonably large area, they can even have the opposite sign (and a magnitude  
 405 comparable to the landscape flux). The presence of large negative fluxes may lead one  
 406 to conclude that the forest is a sink for a particular gas, when it is actually a source. This  
 407 problem cannot be avoided by increasing sampling height, at least within the range tested  
 408 here (i.e., up to two canopy heights). In reality, for sources in the middle and upper canopy,  
 409 the flux heterogeneity actually increases with increasing sampling height.

410 The other problem is the effect of source height on scalar flux non-uniformity across  
 411 the hill. The disproportionally strong chimney effect for near surface sources in the lee  
 412 of hills and ridges can lead to a local dominance of CO<sub>2</sub> fluxes from soil respiration and  
 413 produce positive net fluxes of CO<sub>2</sub> in this region despite the overall dominance of pho-  
 414 tosynthesis at the landscape scale. However, the same effect may have important con-  
 415 sequences for interpreting fluxes of other gases with sources that are vertically distributed  
 416 within the canopy, and it may lead to additional difficulties in partitioning evaporation  
 417 and evapotranspiration. In principle, one could use numerical simulations to aid in the  
 418 interpretation of eddy covariance fluxes obtained from tower measurements. In partic-  
 419 ular, one could develop upscaling factors  $UF = \overline{F}/\langle \overline{F} \rangle$  that would yield more robust  
 420 estimates of landscape fluxes from tower observations (i.e.,  $\overline{F}_{\text{landscape}} = UF \times \overline{F}_{\text{tower}}$ ).  
 421 However, these factors would be specific for each tower and, in principle, a function of  
 422 atmospheric conditions (such as wind speed and direction and atmospheric stability).  
 423 The issue with this approach is the requirement of a large number of dedicated high-resolution  
 424 LES runs. As shown above, it may be possible to devise a simpler method, based the  
 425 topography categorization. However, at this stage, this is only a blue-print on how to  
 426 proceed in organizing simulation results rather than offering any finality to the problem  
 427 at hand.

428 The general rule-of-thumb of siting towers at the top of hills is not a bad idea from  
 429 the perspective of topography effects on fluxes. For the idealized topography, the flux  
 430 at the crest of the ridge is the closest to the landscape flux, and the variability is small  
 431 (Figure 6). However, the bias can still be large depending on the source and sampling  
 432 heights (varying between 40% lower to 50% higher than the landscape mean). In the real  
 433 topography, the situation is more difficult. The crest is still the best location, but now  
 434 it consistently provides an underestimation of the landscape flux (varying from 22% to  
 435 75% of the landscape flux). The variation of fluxes observed at different crests is extremely  
 436 large, complicating the interpretation of measurements. At the moment, it is unclear if  
 437 the increased mixing promoted by buoyancy during daytime would alleviate this prob-  
 438 lem. The presence of topography, even gentle topography, can significantly enlarge the

439 source area and the “apparent” representativeness of the tower-based EC observations.  
 440 However, this larger footprint does not seem to ameliorate the flux spatial non-uniformity  
 441 induced by flow structure.

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 446 with assigned doi:10.5281/zenodo.3774817. For more questions regarding the dataset and  
 447 model, please contact chamecki@ucla.edu.

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