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**STUDIES OF CONCRETE
FOR WOLF CREEK
KANSAS GAS AND ELECTRIC COMPANY
POST TENSIONED REACTOR BUILDING**

Final Report

by

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Report to
Bechtel Power Corporation
Gaithersburg, Maryland

April 1977

STRUCTURAL ENGINEERING LABORATORY
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Final Report - Option I

STUDIES OF CONCRETE FOR WOLF CREEK, KANSAS GAS AND ELECTRIC COMPANY, POST TENSIONED REACTOR BUILDING

1.0 SCOPE

The purpose of this test program was to establish the uniaxial creep and other mechanical and thermal properties of the proposed concrete mix design for the Wolf Creek, Kansas Gas and Electric Company, Reactor Building. The work consisted of furnishing all supervision, labor, materials, and equipment, and performance of all operation and incidentals necessary for the concrete material properties test, except as noted in Section 2.7.

The test program consisted of two options: Option I, the final test program; and, Option II, a preliminary test program, which was not performed for this reactor building.

The Option I test program required the testing of three concrete mixes.

1.1 Mix No. E-2

- 1.1.1 A mix with 1-1/2 in. maximum size aggregate.
- 1.1.2 Compressive strength of 6000 psi at 90 days.
- 1.1.3 Mix design supplied by Owner.

1.2 Mix No. E-1

- 1.2.1 A mix with 3/4-in. maximum size aggregate.
- 1.2.2 Compressive strength of 6000 psi at 90 days.
- 1.2.3 Mix design supplied by Owner.

1.3 Mix No. E-2-S (Special)

- 1.3.1 A mix with 1-1/2 in. maximum size aggregate.
- 1.3.2 Compressive strength less than that of the E-2 mix.
- 1.3.3 Mix design supplied by U.C.
- 1.3.4 This mix was required because the compressive strength for the 28-day E-2 mix was considerably higher than the 6000 psi compressive strength specified.

2.0 TEST PROGRAM

The Option I test program comprised the evaluation of the following properties of the concrete.

- 2.1 Compressive Strength determined on sealed concrete specimens, stored at 73°F, at ages of 7, 28, 90, 180, and 365 days for Class E-2 and E-2-S concrete and at ages of 28, 90, and 180 days for Class E-1 concrete.
- 2.2 Modulus of Elasticity and Poisson's Ratio determined on 6 by 12-in. sealed concrete specimens, stored at 73°F, at ages of 7, 28, 90, 180, and 365 days for Class E-2 and E-2-S concrete and at the age of 180 days only for Class E-1 concrete.
- 2.3 Coefficient of Thermal Expansion determined on two 6 by 16-in. sealed concrete specimens, stored at 73°F, at ages of 28, 180, and 365 days for Class E-2 concrete.
- 2.4 Specific Heat determined on two 8 by 16-in. sealed concrete specimens, stored at 73°F, at ages of 28 and 365 days for Class E-2 concrete.
- 2.5 Diffusivity determined on two 8-1/2 by 17-in. sealed concrete specimens, stored at 73°F, at ages of 28 and 365 days for Class E-2 concrete.
- 2.6 Creep Characteristics of sealed concrete specimens were determined at a sustained stress of 2100 psi, initially applied at ages of 28, 180, and 365 days for Class E-2 concrete, at age 28 days for Class E-2-S concrete, and at age 180 days for Class E-1 concrete. The autogenous strain change for the Class E-2 concrete was determined for a period of one year on sealed creep specimens that were loaded at age one year. No autogenous strain change was determined for the Class E-1 or Class E-2-S concretes. The creep tests were carried out at 73°F and 110°F for the Class E-2 concrete and at 73°F only for the Class E-1 and E-2-S concretes. Each creep test was conducted on a set of two 6 by 16-in. sealed concrete specimens.

2.7 The following related work was not included.

2.7.1 Design of concrete mixes, except for Mix E-2-S.

2.7.2 Supply of portland cement, admixtures, and aggregate used for the test program.

2.7.3 Performance of acceptance or user tests for concrete materials.

3.0 ABBREVIATIONS

ACI	-	American Concrete Institute
ASTM	-	American Society for Testing and Materials
AISI	-	American Iron Steel Institute

4.0 CODES AND STANDARDS

Codes and standards referenced herein are listed below, together with their common abbreviations and year of adoption, as used in this Specification. Standards or codes, including the year of adoption or revision, appearing in referenced documents other than those describing test procedures or methods of sampling shall not be considered as part of this Specification unless specifically referenced below.

ASTM C 33-74	Standard Specification for Concrete Aggregates
ASTM C 39-72	Standard Method of Test for Compressive Strength of Cylindrical Concrete Specimens
ASTM C 125-74	Standard Definitions of Terms Relating to Concrete and Concrete Aggregates
ASTM C 127-73	Standard Method of Test for Specific Gravity and Absorption of Coarse Aggregate
ASTM C 128-73	Standard Method of Test for Specific Gravity and Absorption of Fine Aggregate
ASTM C 138-75	Standard Method of Test for Unit Weight, Yield, and Air Content (Gravimetric) of Concrete
ASTM C 143-74	Standard Method of Test for Slump of Portland Cement Concrete
ASTM C 150-74	Standard Specification for Portland Cement
ASTM C 192-69	Standard Method of Making and Curing Concrete Test Specimens in the Laboratory
ASTM C 231-75	Standard Method of Test for Air Content of Freshly Mixed Concrete by the Pressure Method

ASTM C 469-65	Standard Method of Test for Static Modulus of Elasticity and Poisson's Ratio of Concrete in Compression
ASTM C 566-67	Standard Method of Test for Total Moisture Content of Aggregate by Drying
ASTM C 617-73	Standard Method of Capping Cylindrical Concrete Specimens
ASTM E 4-72	Standard Method of Capping Cylindrical Concrete Specimens
ASTM E 6-73	Standard Definitions of Terms Relating to Methods of Mechanical Testing
ASTM E 12-70	Standard Definitions of Terms Relating to Density and Specific Gravity of Solids, Liquids and Gases
ASTM E 83-67	Standard Method of Verification and Classification of Extensometers

5.0 MANUFACTURE OF CONCRETE SPECIMENS

5.1 Mixing and Placing

Concrete was proportioned in accordance with the mix design and materials supplied by the Owner. The mix designs are shown in Table A.

Aggregates were prepared in accordance with ASTM C 192, Section 4.3. Bulk specific gravity and absorption were determined for the aggregates in accordance with ASTM C 127 and C 128, and are reported in Table B. Cement was stored in a steel moisture-proof container.

Mixing of concrete was in accordance with ASTM C 192, Section 5.1.2. Cement and aggregates were stored at $73^{\circ}\pm 3^{\circ}\text{F}$ for at least two days before mixing to assure a uniform temperature of these materials. Slump was measured in accordance with ASTM Method C 143. Entrained air content was measured in accordance with ASTM Method C 231. Unit weight and yield were determined in accordance with ASTM C 138. Specimens were made and consolidated in accordance with ASTM C 192, Sections 5.3 and 5.4.3, respectively. Accurate records of the mix proportions, moisture content of aggregate, air content, unit weight, and yield were retained.

The specimens for the creep and thermal coefficient of expansion were cast in 6.000 inches (within a tolerance of $-.002$ inches) by 18 inches machined split cast iron molds. Prior to casting, one Carlson 8-inch strain gage, properly calibrated, was centered on the axis of the

cast iron mold. The lead wire from the strain gage was brought out through a hole drilled in the center of a 2-inch thick plate placed at the bottom of the mold and sealed by means of an "O" ring. The final specimen length was 16 inches.

A 1/8-in. by 8-in. metal rod was placed diametrically across the top of this mold to serve as a support for a wire which held the meter in an axial position during casting. After casting, the wire was cut-off, the rod removed, and the top of the cast iron mold sealed with Saran wrap.

The creep and thermal expansion specimens were allowed to set for five hours after casting to allow bleeding water to be reabsorbed prior to capping. Then, a conical-shaped layer of mortar made from the original mix was formed on the top of each cylinder. The 1-1/2 in. thick steel top-plates were then worked back and forth into position until the mortar appeared to be spread uniformly between the plate and the specimen. A leveling plate was used to assure that each top-plate was normal to the axis of the specimen. The creep and thermal expansion specimens were then moved to the 73°F, 50 percent relative humidity room.

The split cast iron molds were stripped from the creep and thermal expansion specimens at the age of one day. Within three minutes after removal of the cast iron mold, a 1/16-in. thick butyl rubber sheet was wrapped and bonded to the top and bottom steel plates with rubber cement. A 3-in. wide lap splice was used to join the butyl rubber sheet. Large hose clamps were placed over the butyl rubber and the end steel plates to assure that the specimens would be internally sealed. The specimens tested at 73°F remained in the 73°F, 50 percent relative humidity room. The specimens tested at 110°F were moved to a 90°F room at the age of eight days. At the age of 16 days, they were moved to the 110°F room where they remained until the end of the test.

Compressive strength specimens were cast in 6 by 12-in. sheet-metal cans. The lid and all joints were sealed with silicon rubber to internally seal the specimens. All sealed compressive strength specimens remained in the 100 percent relative humidity room until just prior to testing, at which time they were stripped, capped, and covered with Saran wrap to ensure water retention throughout the test period.

Modulus of elasticity and Poisson's ratio were determined on the compressive strength cylinders.

Specimens for thermal diffusivity tests were cast in 8-1/2 by 17 by 0.020-in. thick steel cans. They were cast solid, except for a 3/8-in. diameter by 8-1/2 in. deep thermometer well centered on the axis of the specimen. After casting, lids were placed on the specimens and the cans were sealed with silicon rubber prior to being moved to the 73°F, 100 percent relative humidity room. The external metal container was left on the cylinders throughout the duration of the test.

Specimens for the specific heat tests were cast in 8 by 16 by 0.020-in. thick copper cans. They were cast solid, except for a 1-5/8 in. O.D. by 1-1/2 in. I.D. brass tube centered on the axis for the full length of the specimen. After casting, lids were placed on the specimens and the cans were sealed with silicon rubber prior to being moved to the 73°F, 100 percent relative humidity room. The external metal container remained on the cylinders throughout the duration of the test.

5.2 Curing Procedure

After each specimen was consolidated and finishing of the top surface was completed, it was placed in a room under the environmental conditions specified herein for the required test.

6.0 TEST RESULTS

6.1 Mix Design Data

The mix design and data for the concrete mixes used in casting the specimens are shown in Tables C to H. In Tables C to F, the mix designs were computed using absorptions of the aggregate supplied by the Owner. In Tables F to H, the mix designs were computed using absorption of the aggregate determined at Berkeley. In Tables C to H, the weight of cement, water, sand, 3/4-in. and 1-1/2-in. aggregates per cubic yard of concrete were computed using the measured unit weight of the concrete and the batch weights of each material. [Weight of each material, pcy = (Batch weight of each material, lbs.) x (Unit weight of concrete, pcy) ÷ (Total batch weight, lbs.)]

6.2 Compressive Strength and Elastic Properties

Compressive strengths were determined at the ages of 7, 28, 90, 180, and 365 days for Class E-2 and Class E-2-S concretes, and at ages 7, 28, 90, and 180 days for Class E-1 concrete. The average diameter of each specimen was between 5.96 in. and 5.98 in. The ends of the cylinders, to which loads were applied, were plane square end surfaces at right angles to the axis of the specimen and met the planeness requirements of Section 1.2 of ASTM Method C 617. Each specimen was checked for planeness. Testing procedures were in accordance with ASTM C 469, Sections 4.3 through 4.7, inclusive. The testing machine and compressometer used comply with ASTM C 469, Section 2. Each strength determination represents the average obtained from three 6 by 12-in. cylinders. The same three 6 by 12-in. concrete cylinders were used in the determination of compressive strength, modulus of elasticity (E), and Poisson's ratio (μ). The modulus of elasticity and Poisson's ratio were determined by use of an XYZ recorder employing differential transformers. This arrangement produces a continuous plot of stress versus longitudinal strain and lateral strain versus longitudinal strain from which both the modulus of elasticity (E) and Poisson's ratio (μ) were computed. The loading rate used was 60,000 lbs. per minute, which is equivalent to 35 psi per second for a 6-in. diameter specimen. Compressive strength, modulus of elasticity, and Poisson's ratio for sealed concrete specimens stored at 73°F and 100 percent relative humidity are shown in Table I.

6.3 Thermal Diffusivity

The average 28 and 365-day thermal diffusivities for Class E-2 concrete, as determined on two 8-1/2 in. diameter by 17-in. long concrete cylinders, were 0.031 and 0.032 ft²/hr, respectively, and are shown in Table I. The hot water bath and cold water bath were approximately 120°F and 40°F, respectively, for the thermal diffusivity tests.

Thermal diffusivity was determined by the cooling test described in "Thermal Properties of Concrete," Bulletin 1, United States Bureau of Reclamation, Boulder Canyon Project, Final Reports, 1940, pp. 66-86 and pp. 133-143.

6.4 Specific Heat

The average 28 and 365-day specific heat for Class E-2 concrete, as determined on two 8-in. diameter by 16-in. long concrete cylinders, were 0.262 and 0.252 Btu/lb. x °F, respectively, and are shown in Table I.

Specific heat was determined with an adiabatic calorimeter designed to measure the amount of heat required to raise the temperature of a cylindrical test specimen. The calorimeter consisted essentially of two double-walled containers, one within the other, with provision for the measurement of heat input and temperature rise. The equipment and method used were essentially the same as described in "Thermal Properties of Concrete," Bulletin 1, U.S. Bureau of Reclamation, Boulder Canyon Project, Final Report, 1946, pp. 26 and 27 and pp. 112 to 117.

6.5 Thermal Coefficient of Expansion

The two sealed 6-in. by 16-in. thermal coefficient of expansion specimens containing Class E-2 concrete were measured for length changes by means of a Carlson strain meter at successive temperatures of 73°F, 40°F, 100°F, 73°F, 100°F, and 73°F. Specimens were left for at least 24 hours at each temperature before strain readings were taken. At the end of the cycling period, the specimens were stored at 73°F. The average linear thermal expansion for the two specimens at ages of 28, 180, and 365 days were 3.3, 3.4, and 3.5 micro-strain per 1°F temperature change, respectively.

6.6 Sustained Modulus of Elastic, Creep, and Autogenous Strains

Creep characteristics for the concrete were determined on sealed 6-in. by 16-in. cylinders with centrally embedded Carlson strain meters. Sixteen specimens were initially loaded at different ages and temperatures as shown in the table below.

<u>Class of Concrete</u>	<u>Temp. of Specimen</u>	<u>Number of Specimens at Each Loading Age, days</u>		
		<u>28</u>	<u>180</u>	<u>365</u>
E-2	73°F	2	2	2
E-2	110°F	2	2	2
E-1	73°F	-	2	-
E-2-S	73°F	2	-	-

The autogenous strains for the 28 and 180-day loaded creep specimens with Class E-2 concrete were determined from strain data before loading on the specimens with Class E-2 concrete, which were loaded at 365 days. No specimens were cast to determine autogenous strains for the Class E-1 concrete so the strains were assumed to be zero. The autogenous strains for the 28-day loaded creep specimens with Class E-2-S concrete were determined from data before loading on the specimens with Class E-2 concrete, which were loaded at 365 days.

The loading frames used are capable of applying and maintaining a stress level of 2100 psi to all loaded creep specimens despite any change in the dimension of the specimen. Each frame is capable of accepting two specimens in tandem (lengthwise) for simultaneous loading. The frame consists of two header plates (thickness of 1 inch) connected by three 1-1/2 in. (AISI C 1215) steel rods. Care was taken to prevent eccentric loading on all specimens. The hydraulic load-maintaining element consisted of accumulators, regulators, indicator gages, and a high pressure pump which is used to maintain the load on each frame. Pressure gages provide a means for measuring the load to the nearest 2 percent of the total applied stress.

For applying the initial stress of 2100 psi, a manual hand pump was used to apply the stress at a uniform rate of 35 ± 5 psi per second. At this rate the total stress was applied in 60 seconds. Each loaded creep specimen's strain gage was read at: -60 seconds (no load applied); zero time (full load applied); one minute; 10 minutes; two hours; eight hours; 24 hours; daily for one week; weekly for one month; and, twice monthly thereafter.

Sustained modulus of elasticity, creep characteristics, and autogenous strains for sealed concrete specimens are shown in Tables J to Q.

- Table J - Class E-2 concrete stored at 73°F and stressed for 339 days starting at age 28 days.
- Table K - Class E-2 concrete stored at 110°F and stressed for 339 days starting at age 28 days.
- Table L - Class E-2 concrete stored at 73°F and stressed for 217 days starting at age 180 days.
- Table M - Class E-2 concrete stored at 110°F and stressed for 217 days starting at age 180 days.

- Table N - Class E-2 concrete stored at 73°F and stressed for 60 days starting at age 365 days.
- Table O - Class E-2 concrete stored at 110°F and stressed for 60 days starting at age 365 days.
- Table P - Class E-1 concrete stored at 73°F and stressed for 166 days starting at age 180 days.
- Table Q - Class E-2-S concrete stored at 73°F and stressed for 318 days starting at age 28 days.

In the above tables, a minus time under stress indicates a time prior to full load and zero time under stress indicates the time when full load was reached. The sustained modulus of elasticity was computed by dividing the applied stress of 2100 psi by the sum of elastic, creep, and autogenous strains. The autogenous strain values shown are based on a zero value at time of full load.

Elastic plus creep plus autogenous strains, creep plus autogenous strains, and creep strains are all shown plotted versus log of time plus one day for the average of two unsealed concrete specimens in Figures 1 to 8.

- Figure 1 - Class E-2 concrete stressed at age 28 days and stored at 73°F.
- Figure 2 - Class E-2 concrete stressed at age 28 days and stored at 110°F.
- Figure 3 - Class E-2 concrete stressed at age 180 days and stored at 73°F.
- Figure 4 - Class E-2 concrete stressed at age 180 days and stored at 110°F.
- Figure 5 - Class E-2 concrete stressed at age 365 days and stored at 73°F.
- Figure 6 - Class E-2 concrete stressed at age 365 days and stored at 110°F.
- Figure 7 - Class E-1 concrete stressed at age 180 days and stored at 73°F.
- Figure 8 - Class E-2-S concrete stressed at age 28 days and stored at 73°F.

Elastic plus creep plus autogenous strains are plotted versus time for the average of two sealed concrete specimens in Figures 9 and 10.

- Figure 9 - Class E-2 concrete stressed at ages of 28, 180, and 365 days and stored at 73°F.
- Figure 10 - Class E-2 concrete stressed at ages of 28, 180, and 365 days and stored at 110°F.

The complete computer calculations for determining the strains due to loading the sealed concrete specimens are shown in Tables 1A/1B to 8A/8B.

Tables 1A & 1B - Class E-2 concrete stressed at age 28 days and stored at 73°F.

Tables 2A & 2B - Class E-2 concrete stressed at age 28 days and stored at 110°F.

Tables 3A & 3B - Class E-2 concrete stressed at age 180 days and stored at 73°F.

Tables 4A & 4B - Class E-2 concrete stressed at age 180 days and stored at 110°F.

Tables 5A & 5B - Class E-2 concrete stressed at age 365 days and stored at 73°F.

Tables 6A & 6B - Class E-2 concrete stressed at age 365 days and stored at 110°F.

Tables 7A & 7B - Class E-1 concrete stressed at age 180 days and stored at 73°F.

Tables 8A & 8B - Class E-2-S concrete stressed at age 28 days and stored at 73°F.

The complete computer calculations for determining the autogenous strains are shown in Tables 9A/9B and 10A/10B.

Tables 9A & 9B - Class E-2 concrete stored at 73°F.

Tables 10A & 10B - Class E-2 concrete stored at 110°

7.0 COMMENTS

7.1 For the first mix, Class E-2 concrete, using the mix design supplied by Kansas Gas and Electric Company, aggregate absorptions obtained at Berkeley, a pan-type mixer slump of 5-1/2 in., and an air content of 14 percent were measured. Because the slump and air content were greater than specified, Mr. Daye of the Bechtel Corporation was contacted by phone on February 4, 1976, prior to casting any specimens. A decision was then made to use the aggregate absorptions as given by Mr. Daye for all further mixes since this reduced the calculated free water and, therefore, the slump.

7.2 A Lancaster counter current batch pan mixer, Type 30 DH, was used for all of the mixes. Use of this mixer may have accounted for the decrease in air-entraining agent used to obtain the required 3 to 6

percent air. Also, due to better mixing, this pan mixer may have accounted for some of the increase in compressive strength for mixes made at Berkeley.

7.3 Bechtel specifications for slump are given for field conditions measured at point and time of placement. Clarification was needed as to what procedure to follow in the laboratory to measure the desired slump. For the mixes made at Berkeley, slump was measured three minutes and eight minutes after end of mixing.

7.4 All work was performed in accordance with the "Quality Assurance Program" submitted prior to the start of testing.

TABLE A

WOLF CREEK POST TENSIONED REACTOR BUILDING

<u>Material</u>	<u>Source</u>
Cement:	Ashgrove Type II
Sand:	Christie Quarry, Lomont, Kansas
3/4 in. Aggregate:	Christie Quarry, Lomont, Kansas
1-1/2 in. Aggregate:	Christie Quarry, Lomont, Kansas
WRA Admixture:	Master Builders, Pozzolith 300N
AEA Admixture:	Master Builders, MV-BR

Specifications

Compressive Strength:	6,000 psi at 90 days
Slump: Working limit at point of placement - Inadvertency Margin - Rejection Limit -	3 inches - Mix E-1 2-1/2 inches - Mix E-2 2 inches - Mix E-1 and Mix E-2 5 inches - Mix E-1 4-1/2 inches - Mix E-2
Air:	3 to 6 percent
Temperature:	73°F ± 3°F

Weights (S.S.D.) for One Cubic Yard of Concrete

(as per letter from Mr. Thomas F. Regan, Kansas Gas & Electric Company, dated September 24, 1975)

Mix No.	E-1	E-2
Maximum Size Aggregate:	3/4 in.	1-1/2 in.
Cement, lbs.	750	740
Water, lbs.	307	290
Sand, lbs.	1400	1271
3/4 in. Aggregate, lbs.	1480	820
1-1/2 in. Aggregate, lbs.	--	820
WRA, fl. oz.	37.5	37.0
AEA, fl. oz.	6.6	6.9

TABLE B

WOLF CREEK POST TENSIONED REACTOR BUILDING

Bulk Specific Gravity and Absorption Capacity

Aggregate	Bulk Specific Gravity (Saturated Surface Dry)	Absorption Capacity, percent	
		Berkeley	Owner
Sand	2.62	2.6	1.9
3/4 in. Aggregate	2.62	2.2	1.8
1-1/2 in. Aggregate	2.61	1.9	1.4

Note: Aggregates not initially oven dried in the determination of these values.

TABLE C

CASTING DATA FOR MIX E-2

Mix designs are computed using absorption
of aggregates supplied by Owner.

Date	February 4, 1976				March 26, 1976		
Specimens Cast	12 - 6x16-in. creep specimens 2 - 6x16-in. thermal expansion cylinders 14 - 6x12-in. cylinders 1 - 8-1/2x17 in. diffusivity cylinder 1 - 8x16-in. specific heat cylinder				9 - 6x12-in. cylinders 1 - 8-1/2x17-in. diffusivity cylinder 1 - 8x16-in. specific heat cylinder		
Batch No.	3	4	5	6	11	12	Avg.
Batch Size, cu. ft.							
Cement, pcy	737	742	738	741	737	743	740
Water, pcy	289	291	289	290	289	291	290
Sand, pcy S.S.D.	1266	1274	1267	1272	1266	1276	1271
3/4 in. Aggregate, pcy S.S.D.	817	822	817	821	817	823	819
1-1/2 in. Aggregate, pcy S.S.D.	817	822	817	821	817	823	819
AEA, oz./cu. yd.	6.9	6.9	6.9	6.9	6.9	7.0	6.9
WRA, oz./cu. yd.	37.0	37.0	37.0	37.0	37.0	37.1	37.0
Unit Wt., pcf	145.4	146.4	145.5	146.1	145.4	146.5	145.9
1st Slump, in.	3-1/2	3-1/4	3-3/4	4	4-3/4	3	3-3/4
2nd Slump, in.	2-1/2	2	2-1/2	2-3/4	3-1/4	2-1/4	2-1/2
Air, % by volume	4.2	4.2	4.7	4.7	4.8	3.7	4.4
Temp., °F ^(b)	68	68	68	69	72	72	69
W/C Ratio by wt.	0.392	0.392	0.392	0.391	0.392	0.392	0.392

- (1) First slump was taken three minutes after the end of mixing.
 (2) Second slump was taken eight minutes after the end of mixing.

TABLE D

CASTING DATA FOR MIX E-2-S

Mix designs are computed using absorption
of aggregates supplied by Owner.

Date	March 26, 1976		
Specimens Cast	2 - 6x16-in. creep specimens 15 - 6x12-in. cylinders		
Batch No.	13	14	Avg.
Batch Size, cu. ft.	1.8	1.8	
Cement, pcy	591	593	592
Water, pcy	270	270	270
Sand, pcy S.S.D.	1387	1391	1389
3/4 in. Aggregate, pcy S.S.D.	832	834	833
1-1/2 in. Aggregate, pcy S.S.D.	832	834	833
AEA, oz./cu. yd.	1.9	1.9	1.9
WRA, oz./cu. yd.	30.2	30.2	30.2
Unit Wt., pcf	144.9	145.3	145.1
1st Slump, in.	3-3/4	4	3-3/4
2nd Slump, in.	2-3/4	2-1/2	2-5/8
Air, % by volume	4.3	4.4	4.4
Temp., °F ^(b)	71	72	72
W/C Ratio by wt.	0.457	0.455	0.456

- (1) First slump was taken three minutes after the end of mixing.
(2) Second slump was taken eight minutes after the end of mixing.

TABLE E

CASTING DATA FOR MIX E-1

Mix designs are computed using absorption
of aggregates supplied by Owner.

Date	March 17, 1976	March 26, 1976		
Specimens Cast	9 - 6x12-in. cylinders	2 - 6x16-in. creep specimens 9 - 6x12-in. cylinders		
Batch No.	8	9	10	Avg.
Batch Size, cu. ft.	1.8	1.8	1.8	
Cement, pcy	747	746	742	745
Water, pcy	305	305	304	305
Sand, pcy S.S.D.	1393	1392	1385	1390
3/4-in. Aggregate, pcy S.S.D.	1473	1472	1464	1470
1-1/2 in. Aggregate, pcy S.S.D.	---	---	---	---
AEA, oz./cu. yd.	2.2	2.2	2.2	2.2
WRA, oz/cu. yd.	37.5	37.5	37.5	37.5
Unit Wt., pcf	145.3	145.0	144.2	144.8
1st Slump, in.	2-3/4	3-1/4	3-1/2	3-1/8
2nd Slump, in.	2	2-1/2	2-1/2	2-1/3
Air, % by volume	4.6	4.9	4.9	4.8
Temp., °F ^(b)	73	71	72	72
W/C Ratio by wt.	0.408	0.409	0.410	0.409

- (1) First slump was taken three minutes after the end of mixing.
 (2) Second slump was taken eight minutes after the end of mixing.

TABLE F

CASTING DATA FOR MIX E-2

Mix designs are computed using absorption of aggregates determined at Berkeley.

Date	February 4, 1976				March 26, 1976		
Specimens Cast	12 - 6x16-in. creep specimens 2 - 6x16-in. thermal expansion cylinders 14 - 6x12-in. cylinders 1 - 8-1/2x17-in. diffusivity cylinder 1 - 8x16-in. specific heat cylinder				9 - 6x12-in. cylinders 1 - 8-1/2x17-in. diffusivity cylinder 1 - 8x16-in. specific heat cylinder		
Batch No.	3	4	5	6	11	12	Avg.
Batch Size, cu. ft.							
Cement, pcy	737	742	738	741	737	743	740
Water, pcy	272	274	273	274	272	274	273
Sand, pcy S.S.D.	1275	1284	1276	1282	1275	1285	1279
3/4-in. Aggregate, pcy S.S.D.	820	826	821	824	820	826	823
1-1/2-in. Aggregate, pcy S.S.D.	820	826	821	825	820	826	823
AEA, oz./cu. yd.	6.9	6.9	6.9	6.9	6.9	7.0	6.9
WRA, oz./cu. yd.	37.0	37.0	37.0	37.0	37.0	37.1	37.0
Unit Wt., pcf	145.4	146.4	145.5	146.1	145.4	146.5	145.9
1st Slump, in.	3-1/2	3-1/4	3-3/4	4	4-3/4	3	3-3/4
2nd Slump, in.	2-1/2	2	2-1/2	2-3/4	3-1/4	2-1/4	2-1/2
Air, % by volume	4.2	4.2	4.7	4.7	4.8	3.7	4.4
Temp., °F ^(b)	68	68	68	69	72	72	69
W/C Ratio by wt.	0.369	0.369	0.370	0.370	0.369	0.369	0.369

(1) First slump was taken three minutes after the end of mixing.
 (2) Second slump was taken eight minutes after the end of mixing.

TABLE G

CASTING DATA FOR MIX E-2-S

Mix designs are computed using absorption
of aggregates determined at Berkeley.

Date	March 26, 1976		
Specimens Cast	2 - 6x16-in. creep specimens		
	15 - 6x12-in. cylinders		
Batch No.	13	14	Avg.
Batch Size, cu. ft.	1.8	1.8	
Cement, pcy	591	593	592
Water, pcy	254	254	254
Sand, pcy S.S.D.	1397	1401	1399
3/4-in. Aggregate, pcy S.S.D.	835	837	836
1-1/2-in. Aggregate, pcy S.S.D.	835	837	836
AEA, oz./cu. yd.	1.9	1.9	1.9
WRA, oz./cu. yd.	30.2	30.2	30.2
Unit Wt., pcf	144.9	145.3	145.1
1st Slump, in.	3-3/4	4	3-7/8
2nd Slump, in.	2-3/4	2-1/2	2-3/8
Air, % by volume	4.3	4.4	4.4
Temp., °F ^(b)	71	72	72
W/C Ratio by wt.	0.430	0.428	0.429

- (1) First slump was taken three minutes after the end of mixing.
 (2) Second slump was taken eight minutes after the end of mixing.

TABLE H

CASTING DATA FOR MIX E-1

Mix designs are computed using absorption
of aggregates determined at Berkeley.

Date	March 17, 1976		March 26, 1976	
Specimens Cast	9 - 6x12-in. cylinders		2 - 6x16-in. creep specimens 9 - 6x12-in. cylinders	
Batch	8	9	10	Avg.
Batch Size, cu. ft.				
Cement, pcy	747	746	742	745
Water, pcy	287	287	286	287
Sand, pcy S.S.D.	1403	1402	1395	1400
3/4-in. Aggregate, pcy S.S.D.	1478	1477	1469	1475
1-1/2-in. Aggregate, pcy S.S.D.	---	---	---	---
AEA, oz./cu. yd.	2.2	2.2	2.2	2.2
WRA, oz./cu. yd.	37.5	37.5	37.5	37.5
Unit Wt., pcf	145.3	145.0	144.2	144.8
1st Slump, in.	2-3/4	3-1/4	3-1/2	3-1/8
2nd Slump, in.	2	2-1/2	2-1/2	2-1/3
Air, % by volume	4.6	4.9	4.9	4.8
Temp., °F ^(b)	73	71	72	72
W/C Ratio by wt.	0.384	0.385	0.385	0.385

- (1) First slump was taken three minutes after the end of mixing.
 (2) Second slump was taken eight minutes after the end of mixing.

TABLE I
MECHANICAL AND THERMAL PROPERTIES

Property	Age, days	Concrete, class		
		E-1 3/4"	E-2 1-1/2"	E-2-S 1-1/2"
Compressive Strength, psi (a)	7	6820	6625	5540
	28	8050	8200	6770
	90	9110(c)	9030(e)	7580
		8900(d)	8740(f)	xxxx
	180	9210	9340	7750
	365	xxxx	9990	7940
Poisson's Ratio (a)	7	xxxx	0.23	xxxx
	28	xxxx	0.23	0.23
	90	xxxx	0.24	xxxx
	180	0.23	0.24	xxxx
	365	xxxx	0.25	xxxx
Modulus of Elasticity, psi (psi x 10 ⁶) (a)	7	xxxx	4.5	xxxx
	28	xxxx	4.7	4.6
	90	xxxx	4.8	xxxx
	180	4.7	5.1	xxxx
	365	xxxx	5.1	xxxx
Linear Thermal Expansion, micro-strain/°F (b)	28	xxxx	3.3	xxxx
	180	xxxx	3.4	xxxx
	365	xxxx	3.5	xxxx
Diffusivity, ft ² /hr	28	xxxx	0.031	xxxx
	365	xxxx	0.032	xxxx
Specific Heat, Btu/lb. °F	28	xxxx	0.262	xxxx
	365	xxxx	0.242	xxxx

Notes: All tests done on sealed specimens.

xxxx - specimens not tested at these ages

(a) Average of three specimens.

(b) Average of two specimens.

(c) Specimens from Mix No. 8 cast on 3/17/76.

(d) Specimens from Mix No. 9 and Mix No. 10 cast on 3/26/76.

(e) Specimens from Mix Nos. 3, 4, & 5 cast on 2/4/76.

(f) Specimens from Mix No. 11 and 12 cast on 3/26/76.

TABLE J

AVERAGE ELASTIC, CREEP AND AUTOGENOUS STRAINS
 WOLF CREEK OPTION 1 CLASS E-2 (ES7388)
 (SPECIMEN: SEALED & BY 16 IN. CONCRETE CYL.)

AGE OF LOADING : 28 DAYS
 TEST TEMPERATURE : 73 DEG. F.
 ULT. STP. : 8200. PSI
 APPLIED TEST STRESS : 2100. PSI
 PER. ULT. STP. APPLIED: 25.6 PERCENT
 PETER NUMBERS :
 AUTOGENOUS : 73 12 AND 73 13
 CREEP : 73 00 AND 73 01

TIME	*SUSTAINED *ELASTIC* *CREEP *	*MODULUS OF *CREEP *	*PLUS *AUTOG- *CREEP *SPECIFIC
DAYS	*STRESS *ELASTICITY* *PLUS *AUTOG- *CREEP *SPECIFIC	*AUTOG- *CREEP *	*CREEP *SPECIFIC
	* (A) * ENOUS *****	* ENOUS *****	* (R) *****
0.007	4.57	0	0
0.007	4.42	-25	-25
0.053	4.09	-65	-65
0.214	3.53	-83	-83
0.371	3.28	-104	-103
1.1745	3.62	-560	-124
2.3	3.55	-591	-140
3.2	3.45	-607	-156
4.2	3.36	-612	-178
5.2	3.31	-627	-178
6.2	3.27	-643	-175
7.2	3.24	-648	-182
8.2	3.21	-652	-190
9.2	3.18	-657	-196
14.2	3.08	-704	-224
20.2	2.97	-730	-252
27.2	2.84	-753	-276
37.0	2.76	-767	-299
44.3	2.69	-780	-314
52.1	2.67	-787	-329
58.1	2.65	-791	-335
76.2	2.62	-801	-351
74.2	2.59	-811	-361
83.2	2.57	-816	-368
92.1	2.52	-827	-383
107.2	2.49	-847	-391
112.2	2.46	-853	-403
131.0	2.43	-863	-413
148.3	2.40	-875	-425
152.1	2.38	-881	-433
155.1	2.34	-884	-441
166.2	2.36	-891	-441
173.7	2.34	-896	-446
182.5	2.33	-903	-453
197.2	2.31	-907	-457
202.2	2.31	-910	-458
212.0	2.29	-914	-460
216.2	2.29	-921	-468
246.1	2.24	-927	-471
261.2	2.27	-934	-476
292.2	2.25	-940	-484
317.1	2.23	-941	-490
322.0	2.23	-945	-491
337.0	2.22	-946	-495
343.5	2.22	-946	-495
343.0	2.22	-946	-495

(A) SUSTAINED MODULUS OF ELASTIC = 2100. PSI DIVIDED BY SUM OF ELASTIC, CREEP, AND AUTOGENOUS STRAINS.
 (R) SPECIFIC CREEP = CREEP STRAIN DIVIDED BY 2100. PSI

AVERAGE ELASTIC, CREEP AND AUTOGENOUS STRAINS
 WCE CRACK OPTION 1 CLASS E-2 E5784
 (SPECIMEN: SCALED 6 BY 16 IN. CONCRETE CYL.)

AGE OF LOADING : 28 DAYS
 TEST TEMPERATURE : 110 DEG. F.
 ULT. STR. : 8500. PSI
 APPLIED TEST STRESS : 2100. PSI
 REG. ULT. STR. APPLIED : 24.7 PERCENT
 METER NUMBER :
 AUTOGENOUS : 11 04 AND 11 05
 CREEP : 11 00 AND 11 01

TIME	*SUSTAINED *ELASTIC* CREEP	*FLUS * AUTOG- * ENOUS *	*CREEP * SPECIFIC
DAYS	* (A)	* (B)	* (H)
0.0007	0	0	0
0.000	-467	0	0
0.1028	-525	-57	-0.271
0.3748	-557	-90	-0.429
1.0755	-550	-122	-0.581
2.2	-517	-150	-0.714
3.1	-632	-165	-0.795
4.1	-655	-184	-0.874
5.2	-670	-203	-0.914
6.2	-681	-213	-0.955
7.2	-697	-229	-1.048
8.2	-703	-236	-1.129
14.2	-708	-241	-1.167
20.2	-733	-271	-1.190
27.2	-765	-297	-1.329
34.2	-747	-319	-1.438
44.2	-811	-343	-1.567
58.2	-822	-356	-1.724
70.2	-845	-377	-1.819
78.2	-854	-387	-1.867
83.2	-867	-400	-1.924
93.2	-874	-406	-1.943
107.2	-893	-425	-2.033
117.2	-903	-436	-2.076
132.2	-911	-444	-2.114
155.2	-922	-455	-2.157
158.2	-937	-470	-2.210
173.2	-950	-483	-2.276
186.2	-967	-493	-2.350
197.2	-984	-496	-2.436
208.2	-971	-504	-2.419
211.2	-975	-507	-2.467
246.2	-980	-513	-2.481
247.2	-996	-525	-2.526
251.2	-957	-525	-2.426
255.2	-1020	-525	-2.419
317.2	-1027	-552	-2.500
323.2	-1040	-549	-2.543
338.2	-1046	-572	-2.582
338.2	-1047	-579	-2.571

(A) SUSTAINED MODULUS OF ELASTIC = 2100. PSI DIVIDED BY SUM OF ELASTIC, CREEP, AND AUTOGENOUS STRAINS.
 (H) SPECIFIC CREEP = CREEP STRAIN DIVIDED BY 2100. PSI

TABLE K

AVERAGE ELASTIC, CREEP AND AUTOGENOUS STRAINS
 W/LEAK OPTION 1 CLASS E-2 EST 388
 (SPECIMEN: SEALED 6 BY 16 IN. CONCRETE CVL.)

AGE OF LOADING : 180 DAYS
 TEST TEMPERATURE : 73 DEG. F.
 ULT. STR. : 9340. PSI
 APPLIED TEST STRESS : 2100. PSI
 PER ULT. STR. APPLIED: 22.5 PERCENT
 METER NUMBERS :
 AUTOGENOUS : 73 12 AND 73 13
 CREEP : 73 04 AND 73 05

TIME	*SUSTAINED ELASTIC*	*CREEP*	*MICROSTRAIN*	*SPECIFIC CREEP*
UNDER	*MODULUS OF CREEP*	*PLUS*	*AUTOGENOUS*	*CREEP*
DAYS	*ELASTICITY*	*ENOUS*	*ENOUS*	*CREEP*
	(A)	(B)	(R)	(R)
0.0007	0	0	0	0
0.000	4.95	-423	0	0.0076
0.028	4.78	-473	-16	-0.0055
0.057	4.74	-443	-20	-0.0132
0.201	4.66	-451	-28	-0.0238
1.833	4.44	-473	-50	-0.0243
2.250	4.43	-474	-51	-0.0271
3.635	4.39	-480	-57	-0.0348
1.0757	4.24	-465	-72	-0.0390
2.1	4.18	-505	-72	-0.0448
3.1	4.06	-517	-98	-0.0448
4.1	4.03	-521	-68	-0.0462
7.0	3.95	-532	-109	-0.0519
9.2	3.88	-541	-118	-0.0562
14.1	3.75	-558	-135	-0.0589
21.2	3.65	-576	-153	-0.0729
34.9	3.50	-600	-177	-0.0843
45.1	3.44	-611	-188	-0.0845
50.1	3.41	-615	-192	-0.0919
55.5	3.38	-622	-199	-0.0971
79.1	3.28	-641	-218	-0.1071
94.0	3.23	-650	-227	-0.1110
105.1	3.18	-660	-237	-0.1162
140.1	3.12	-674	-251	-0.1248
165.0	3.07	-685	-262	-0.1300
170.0	3.06	-687	-264	-0.1314
184.5	3.03	-693	-270	-0.1348
186.9	3.03	-694	-271	-0.1348
203.5	3.00	-703	-276	-0.1361
214.5	2.95	-703	-280	-0.1405
216.5	2.99	-703	-280	-0.1405

(A) SUSTAINED MODULUS OF ELASTIC = 2100. PSI DIVIDED BY SUM OF ELASTIC, CREEP, AND AUTOGENOUS STRAINS.
 (B) SPECIFIC CREEP = CREEP STRAIN DIVIDED BY 2100. PSI

TABLE L

AVERAGE ELASTIC, CREEP AND AUTOGENOUS STRAINS
 UNDER CREEP CYCLES CLASS E-2 (F57388)
 (SPECIMEN: SEALED 6 CY 16 IN. CONCRETE CYL.)

AGE OF LOADING : 180 DAYS
 TEST TEMPERATURE : 110 DEG. F.
 ULT. STR. : 9340. PSI
 APPLIED 1ST STRESS : 2100. PSI
 PER. ULT. STR. APPLIED: 22.5 PERCENT
 TEST NUMBER :
 AUTOGENOUS : 11 04 AND 11 05
 CREEP : 11 02 AND 11 03

TIME	*SUSTAINED ELASTIC*	*CREEP*	*ELUS*	*CREEP*	*SPECIFIC
DAYS	*FLASTICITY*	*PLUS*	*AUTOG*	*AUTOG*	*CREEP*
	* (A)	* ENOUS	* ENOUS	* ENOUS	* (B)
0.0007	0	0	0	0	0
0.0000	5.06	-415	0	-17	-.0081
0.0024	4.85	-432	0	-20	-.0095
0.0043	4.83	-433	0	-25	-.0124
0.0201	4.75	-441	0	-31	-.0137
0.0424	4.65	-448	0	-39	-.0186
0.0861	4.63	-454	0	-43	-.0205
0.1278	4.59	-458	0	-51	-.0243
0.2657	4.51	-466	0	-68	-.0324
0.5785	4.34	-466	-1	-83	-.0395
2.0	4.20	-500	-2	-83	-.0438
3.0	4.11	-511	-4	-94	-.0467
4.0	4.04	-520	-7	-107	-.0510
6.0	3.98	-528	-6	-122	-.0581
9.1	3.87	-542	-5	-149	-.0710
14.0	3.69	-570	-6	-164	-.0781
21.1	3.57	-598	-9	-193	-.0919
34.8	3.42	-614	-6	-203	-.0967
45.0	3.34	-624	-10	-209	-.0995
50.0	3.31	-635	-11	-209	-.1038
50.0	3.25	-647	-14	-219	-.1092
74.0	3.18	-661	-12	-230	-.1146
93.0	3.07	-683	-19	-249	-.1219
109.1	3.03	-693	-22	-256	-.1307
140.0	2.89	-730	-31	-287	-.1444
125.0	2.78	-755	-34	-308	-.1467
170.0	2.76	-760	-37	-314	-.1495
184.0	2.73	-769	-40	-315	-.1500
186.8	2.77	-770	-40	-334	-.1590
203.8	2.66	-786	-41	-344	-.1638
214.6	2.53	-800	-41	-345	-.1643
216.9	2.52	-801	-41	-345	-.1643

TABLE M

(A) SUSTAINED MODULUS OF ELASTIC = 2100. PSI DIVIDED BY SUM OF ELASTIC, CREEP, AND AUTOGENOUS STRAINS.
 (B) SPECIFIC CREEP = CREEP STRAIN DIVIDED BY 2100. PSI

TABLE N

AVERAGE ELASTIC, CREEP AND AUTOGENOUS STRAINS
 WOLF CREEP OPTION CLASS E-2 P-2700
 (SPECIMEN: SEALED 6 IN. CONCRETE CYL.)

AGE OF LOADING : 74 DAYS
 TEST TEMPERATURE : 74 DEG. F.
 ULT. STP. : R200 PSI
 APPLIED TEST STRESS : 2100 PSI
 PER. ULT. STP. APPLIED : 29.6 PERCENT
 METER NUMBERS : 73 12 AND 73 13
 AUTOGENOUS : 73 12 AND 73 13
 CREEP

TIME	*SUSTAINED ELASTIC*	* CREEP *	* AUTOG-*	* CREEP *	* SPECIFIC
UNDER	*VOLUME OF*	* PLUS *	* AUTOG-*	* CREEP *	* (CREEP
STRESS	* ELASTICITY*	* PLUS *	* AUTOG-*	* CREEP *	* (PI)
DAYS	* (A)	* ENDS *	* ENDS *	* ENDS *	* ENDS *
0.007	0	0	0	0	0
0.000	5.24	-191	0	-2	0.0010
0.024	5.30	-195	-4	-4	-0.0019
0.063	5.28	-258	-4	-12	-0.0027
0.075	5.17	-405	-12	-17	-0.0081
0.061	5.12	-410	-17	-21	-0.0100
0.143	5.06	-415	-21	-38	-0.0141
1.1875	4.84	-430	-34	-38	-0.0229
2.0	4.77	-440	-46	-48	-0.0347
3.0	4.71	-445	-52	-54	-0.0271
4.3	4.69	-448	-55	-57	-0.0250
5.0	4.64	-453	-59	-61	-0.0324
7.2	4.58	-459	-66	-68	-0.0365
14.3	4.44	-473	-76	-81	-0.0410
17.0	4.39	-478	-84	-86	-0.0448
23.0	4.34	-484	-91	-94	-0.0490
27.9	4.25	-493	-100	-103	-0.0524
39.2	4.19	-501	-107	-110	-0.0582
47.1	4.13	-508	-115	-118	-0.0652
60.2	3.98	-527	-134	-137	-0.0652

(A) SUSTAINED VOLUME OF ELASTIC = 2100 PSI DIVIDED BY SUM OF ELASTIC, CREEP, AND AUTOGENOUS STRAINS.
 (R) SPECIFIC CREEP = CREEP STRAIN DIVIDED BY 2100. PSI

AVERAGE ELASTIC, CREEP AND AUTOGENOUS STRAINS
 WLF CREEP OPTION 1 CLASS E-2 FS73RD
 (SPECIMEN: SEALED 6 BY 16 IN. CONCRETE CYL.)

AGE OF LOADING : 365 DAYS
 TEST TEMPERATURE : 110 DEG. F.
 ULT. STR. : 9900 PSI
 APPLIED TEST STRESS : 2100. PSI
 PER. CMT. STR. APPLIED: 21.0 PERCENT
 METER NUMBERS :
 AUTOGENOUS : 11 04 AND 11 05
 CREEP : 11 04 AND 11 05

TIME	*SUSTAINED ELASTIC*	*CREEP*	*MICROSTRAIN*	*CREEP*	*SUSTAINED ELASTIC*	*CREEP*	*MICROSTRAIN*	*CREEP*	*SUSTAINED ELASTIC*	*CREEP*	*MICROSTRAIN*	*CREEP*	
UNDER	*MODULUS CF*	*CREEP*	*PLUS*	*CREEP*	*UNDER	*MODULUS CF*	*CREEP*	*PLUS*	*CREEP*	*UNDER	*MODULUS CF*	*CREEP*	
STRESS,	*ELASTICITY*	*PLUS*	*AUTOG*	*ENOUS*	STRESS,	*ELASTICITY*	*PLUS*	*AUTOG*	*ENOUS*	STRESS,	*ELASTICITY*	*PLUS*	
DAYS	* (A)	* ENOUS	* (R)	* (R)	DAYS	* (A)	* ENOUS	* (R)	* (R)	DAYS	* (A)	* ENOUS	* (R)
0.007	0	0	0	0	0.007	0	0	0	0	0.007	0	0	0
0.000	2.40	-189	0	0	0.000	2.40	-189	0	0	0.000	2.40	-189	0
0.008	5.34	-303	-4	-4	0.008	5.34	-303	-4	-4	0.008	5.34	-303	-4
0.009	5.30	-306	-7	-7	0.009	5.30	-306	-7	-7	0.009	5.30	-306	-7
0.024	5.15	-408	-14	-14	0.024	5.15	-408	-14	-14	0.024	5.15	-408	-14
0.052	5.07	-414	-24	-24	0.052	5.07	-414	-24	-24	0.052	5.07	-414	-24
0.153	5.04	-417	-28	-28	0.153	5.04	-417	-28	-28	0.153	5.04	-417	-28
1.1674	4.76	-441	-51	-51	1.1674	4.76	-441	-51	-51	1.1674	4.76	-441	-51
2.0	4.65	-452	-62	-62	2.0	4.65	-452	-62	-62	2.0	4.65	-452	-62
4.3	4.52	-468	-76	-76	4.3	4.52	-468	-76	-76	4.3	4.52	-468	-76
5.0	4.47	-470	-80	-80	5.0	4.47	-470	-80	-80	5.0	4.47	-470	-80
7.2	4.38	-475	-91	-91	7.2	4.38	-475	-91	-91	7.2	4.38	-475	-91
14.7	4.18	-502	-112	-112	14.7	4.18	-502	-112	-112	14.7	4.18	-502	-112
17.9	4.13	-509	-119	-119	17.9	4.13	-509	-119	-119	17.9	4.13	-509	-119
22.9	4.02	-523	-134	-134	22.9	4.02	-523	-134	-134	22.9	4.02	-523	-134
27.9	3.95	-531	-142	-142	27.9	3.95	-531	-142	-142	27.9	3.95	-531	-142
30.3	3.81	-551	-162	-162	30.3	3.81	-551	-162	-162	30.3	3.81	-551	-162
47.1	3.73	-563	-173	-173	47.1	3.73	-563	-173	-173	47.1	3.73	-563	-173
60.2	3.72	-565	-176	-176	60.2	3.72	-565	-176	-176	60.2	3.72	-565	-176

(A) SUSTAINED MODULUS OF ELASTIC = 2100. PSI DIVIDED BY SUM OF ELASTIC, CREEP, AND AUTOGENOUS STRAINS.
 (R) SPECIFIC CREEP = CREEP STRAIN DIVIDED BY 2100. PSI

TABLE 0

AVERAGE ELASTIC, CREEP AND AUTOGENOUS STRAINS
 WOLF CREEK OPTION 1 CLASS E-1 ESTYRBR
 (SPECIMEN: SEALED & BY 16 IN. CONCRETE CYL.)

AGE OF LOADING : 180 DAYS
 TEST TEMPERATURE : 73 DEG. F.
 ULT. STR. : 9210. PSI
 APPLIED TEST STRESS : 2100. PSI
 PER. ULT. STR. APPLIED: 22.8 PERCENT
 METER KUPPERS

AUTOGENOUS CREEP : 20 41 AND 20 42

TABLE P

TIME UNDER STRESS	SUSTAINED ELASTIC STRESS	ELASTIC MODULUS	ELASTIC CREEP	AUTOGENOUS CREEP	SPECIFIC CREEP
DAYS	PSI	PSI	PERCENT	PERCENT	(R)
0.000	5.10	4.12	0	0	0.0071
0.028	4.92	-4.27	-15	-15	-0.0095
0.097	4.85	-4.52	-20	-20	-0.0119
0.201	4.81	-4.77	-25	-25	-0.0171
0.824	4.59	-4.28	-36	-36	-0.0243
3.325	4.54	-4.63	-51	-51	-0.0319
9.993	4.34	-4.79	-57	-57	-0.0371
2.0	4.29	-4.50	-78	-78	-0.0410
3.1	4.22	-4.33	-86	-86	-0.0438
4.1	4.17	-5.04	-92	-92	-0.0462
5.0	4.13	-5.09	-97	-97	-0.0486
6.0	4.07	-5.14	-102	-102	-0.0509
7.0	4.03	-5.18	-105	-105	-0.0538
9.0	4.00	-5.25	-113	-113	-0.0643
15.3	3.94	-5.47	-135	-135	-0.0700
21.0	3.76	-5.59	-147	-147	-0.0748
25.2	3.69	-5.69	-157	-157	-0.0843
43.1	3.57	-5.89	-177	-177	-0.0929
58.2	3.45	-6.07	-195	-195	-0.1038
83.3	3.33	-6.30	-218	-218	-0.1114
112.1	3.23	-6.45	-234	-234	-0.1129
134.1	3.24	-6.49	-237	-237	-0.1162
154.1	3.20	-6.56	-244	-244	-0.1187
155.0	3.20	-6.57	-245	-245	-0.1200
153.0	3.18	-6.47	-252	-252	-0.1219
164.0	3.14	-6.68	-256	-256	-0.1219
166.0	3.14	-6.68	-256	-256	-0.1219

(A) SUSTAINED MODULUS OF ELASTIC = 2100. PSI DIVIDED BY SUM OF ELASTIC, CREEP, AND AUTOGENOUS STRAINS.
 (B) SPECIFIC CREEP = CREEP STRAIN DIVIDED BY 2100. PSI

AVERAGE ELASTIC, CREEP AND AUTOGENOUS STRAINS
 WOLF CREEK DIVISION 1 CLASS E-2-5 F 57388
 (SPECIMEN: SEALED 6 BY 15 IN. CONCRETE CYL.)

AGE OF LOADING : 28 DAYS
 TEST TEMPERATURE : 73 DEG. F.
 ULT. STR. : 6770. PSI
 APPLIED TEST STRESS : 2100. PSI
 DEC. ULT. STR. APPLIED: 31.0 PERCENT
 METER NUMBERS : 73 12 AND 73 13
 AUTOGENOUS CREEP : 73 02 AND 73 03

TIME	*SUSTAINED ELASTIC	*CREEP	*ELUS	*AUTOG-	*ENOUS	*CREEP	*SPECIFIC
UNDER	*MODULUS OF CREEP	*PLUS	*AUTOG-	*ENOUS	*CREEP	*CREEP	
DAYS	*ELASTICITY	*PLUS	*AUTOG-	*ENOUS	*CREEP	*CREEP	
	*MPSI	*MPSI	*MPSI	*MPSI	*MPSI	*MPSI	(F)
	(A)	(A)	(A)	(A)	(A)	(A)	(F)
0.000	4.32	-485	0	0	0	0	0
0.028	4.15	-505	-20	0	-20	-20	-.0055
0.062	4.08	-517	-31	0	-31	-31	-.0124
0.070	3.87	-542	-56	0	-56	-56	-.0267
0.145	3.78	-556	-70	0	-70	-70	-.0332
0.185	3.50	-600	-114	-1	-113	-113	-.0538
2.0	3.38	-621	-135	0	-135	-135	-.0643
3.1	3.28	-641	-155	0	-155	-155	-.0734
4.1	3.21	-655	-169	0	-169	-169	-.0805
5.1	3.15	-667	-181	0	-181	-181	-.0862
6.9	3.07	-685	-198	-1	-194	-194	-.0943
11.1	2.94	-714	-224	-1	-227	-227	-.1041
19.0	2.81	-748	-262	-2	-260	-260	-.1235
27.0	2.72	-773	-287	-1	-286	-286	-.1362
32.0	2.68	-785	-299	-1	-298	-298	-.1419
47.0	2.57	-810	-340	0	-340	-340	-.1571
57.0	2.52	-833	-347	2	-349	-349	-.1662
81.0	2.48	-845	-360	3	-363	-363	-.1729
97.1	2.44	-859	-373	4	-377	-377	-.1755
100.0	2.43	-863	-377	4	-381	-381	-.1814
105.0	2.43	-865	-379	5	-384	-384	-.1874
115.0	2.40	-874	-388	7	-395	-395	-.1961
122.1	2.39	-879	-393	7	-401	-401	-.1910
135.6	2.37	-887	-401	7	-408	-408	-.1942
140.0	2.36	-891	-405	10	-415	-415	-.1976
151.0	2.35	-892	-406	10	-416	-416	-.1981
160.0	2.35	-895	-409	10	-419	-419	-.1995
181.0	2.34	-897	-411	11	-422	-422	-.2010
184.0	2.33	-899	-404	11	-415	-415	-.1976
210.0	2.34	-897	-411	16	-427	-427	-.2033
241.1	2.32	-905	-419	17	-436	-436	-.2076
265.5	2.30	-912	-426	19	-445	-445	-.2119
270.0	2.30	-914	-428	19	-447	-447	-.2129
285.0	2.29	-917	-431	21	-452	-452	-.2152
287.0	2.29	-917	-431	22	-453	-453	-.2157
304.0	2.28	-921	-435	22	-457	-457	-.2175
315.0	2.28	-923	-437	22	-458	-458	-.2181
317.0	2.27	-924	-438	22	-460	-460	-.2190

(A) SUSTAINED MODULUS OF ELASTIC = 2100. PSI DIVIDED BY SUM OF ELASTIC, CREEP, AND AUTOGENOUS STRAINS.
 (R) SPECIFIC CREEP = CREEP STRAIN DIVIDED BY 2100. PSI

TABLE Q

TABLE 2A

ELASTIC AND CREEP STRAINS (NOT CORRECTED FOR AUTGENOUS STRAINS)
 WOLF CREEK BOTTOM 1 CLASS E-2 E573A
 (SPECIMEN SEALED 6 BY 16 IN. CONCRETE CVL.)

CALIBRATION CONSTANTS:
 WELD RESISTANCE AT 0.0 DEGREES F. = 49.72 OHMS
 TEMP. CALIBRATION CONSTANT = 10.72 MICROVOLTS/VOLT/DEGREE F.
 STRAIN CALIBRATION CONSTANT = 19.14 MICROVOLTS/VOLT/MICROSTRAIN
 CALIBRATED RANGE = 111.0 TO 101.00 MICROVOLTS/VOLT
 METER COEFF. OF THERMAL EXPANSION = 6.7 MICROSTRAIN/DEGREE F.
 CONCRETE COEFF. OF THERMAL EXPANSION = 3.6 MICROSTRAIN/DEGREE F.
 STRAIN INCREMENT FACTOR = 0 PERCENT

NOTE: FOR MODE A OR 5 VOLTS, AND MODE 3 MICROVOLTS -- THE BRIDGE VOLTAGE WAS 2.00000 VOLTS.

DATE	* TIME	* AGE	* DAYS	* MODE	* RESIST.	* TEMP.	* CHANGE	* MICRO	* MODE	* MICRO	* TEMPERATURE	* CORRECTED
		* DAYS			* OHMS	* DEGREE	* MICRO			* MICRO	* FROM	* ELASTIC
											* MICRO	* CREEP
											* MICRO	* CREEP
2-4-74	1400	0	0	0	58.59	77.6	7725	0	0	0	0	0
2-5-74	1100	1.9	1.9	0	58.08	80.4	7592	-132	-35	-471	-59	0
2-10-74	1900	17.4	17.4	0	57.126	80.1	6137	-1548	-50	-505	-59	0
2-20-74	1204	26.9	26.9	0	57.01	80.1	6137	-1548	-50	-505	-59	0
3-3-74	1304	29.9	29.9	0	57.01	80.1	6137	-1548	-50	-505	-59	0
3-7-74	1205	26.9	26.9	0	57.01	80.1	6137	-1548	-50	-505	-59	0
3-11-74	1437	30.9	30.9	0	57.01	80.1	6137	-1548	-50	-505	-59	0
3-15-74	1437	30.9	30.9	0	57.01	80.1	6137	-1548	-50	-505	-59	0
3-19-74	1400	28.0	28.0	0	57.01	80.1	6137	-1548	-50	-505	-59	0
3-23-74	1400	28.0	28.0	0	57.01	80.1	6137	-1548	-50	-505	-59	0
3-27-74	1410	29.0	29.0	0	57.01	80.1	6137	-1548	-50	-505	-59	0
3-31-74	1530	31.1	31.1	0	57.01	80.1	6137	-1548	-50	-505	-59	0
3-10-76	1545	33.1	33.1	0	57.01	80.1	6137	-1548	-50	-505	-59	0
3-14-76	1545	34.1	34.1	0	57.01	80.1	6137	-1548	-50	-505	-59	0
3-18-76	1515	35.1	35.1	0	57.01	80.1	6137	-1548	-50	-505	-59	0
3-22-76	1745	41.1	41.1	0	57.01	80.1	6137	-1548	-50	-505	-59	0
3-26-76	1615	45.1	45.1	0	57.01	80.1	6137	-1548	-50	-505	-59	0
3-30-76	1615	45.1	45.1	0	57.01	80.1	6137	-1548	-50	-505	-59	0
4-3-76	1600	47.1	47.1	0	57.01	80.1	6137	-1548	-50	-505	-59	0
4-7-76	1100	49.1	49.1	0	57.01	80.1	6137	-1548	-50	-505	-59	0
4-11-76	1340	51.1	51.1	0	57.01	80.1	6137	-1548	-50	-505	-59	0
4-15-76	1415	53.1	53.1	0	57.01	80.1	6137	-1548	-50	-505	-59	0
4-19-76	1320	55.1	55.1	0	57.01	80.1	6137	-1548	-50	-505	-59	0
4-23-76	1150	57.1	57.1	0	57.01	80.1	6137	-1548	-50	-505	-59	0
4-27-76	1330	59.1	59.1	0	57.01	80.1	6137	-1548	-50	-505	-59	0
4-31-76	1430	61.1	61.1	0	57.01	80.1	6137	-1548	-50	-505	-59	0
5-5-76	1430	63.1	63.1	0	57.01	80.1	6137	-1548	-50	-505	-59	0
5-9-76	1430	65.1	65.1	0	57.01	80.1	6137	-1548	-50	-505	-59	0
5-13-76	1430	67.1	67.1	0	57.01	80.1	6137	-1548	-50	-505	-59	0
5-17-76	1430	69.1	69.1	0	57.01	80.1	6137	-1548	-50	-505	-59	0
5-21-76	1430	71.1	71.1	0	57.01	80.1	6137	-1548	-50	-505	-59	0
5-25-76	1430	73.1	73.1	0	57.01	80.1	6137	-1548	-50	-505	-59	0
5-29-76	1430	75.1	75.1	0	57.01	80.1	6137	-1548	-50	-505	-59	0
6-2-76	1430	77.1	77.1	0	57.01	80.1	6137	-1548	-50	-505	-59	0
6-6-76	1430	79.1	79.1	0	57.01	80.1	6137	-1548	-50	-505	-59	0
6-10-76	1430	81.1	81.1	0	57.01	80.1	6137	-1548	-50	-505	-59	0
6-14-76	1430	83.1	83.1	0	57.01	80.1	6137	-1548	-50	-505	-59	0
6-18-76	1430	85.1	85.1	0	57.01	80.1	6137	-1548	-50	-505	-59	0
6-22-76	1430	87.1	87.1	0	57.01	80.1	6137	-1548	-50	-505	-59	0
6-26-76	1430	89.1	89.1	0	57.01	80.1	6137	-1548	-50	-505	-59	0
6-30-76	1430	91.1	91.1	0	57.01	80.1	6137	-1548	-50	-505	-59	0
7-4-76	1430	93.1	93.1	0	57.01	80.1	6137	-1548	-50	-505	-59	0
7-8-76	1430	95.1	95.1	0	57.01	80.1	6137	-1548	-50	-505	-59	0
7-12-76	1430	97.1	97.1	0	57.01	80.1	6137	-1548	-50	-505	-59	0
7-16-76	1430	99.1	99.1	0	57.01	80.1	6137	-1548	-50	-505	-59	0
7-20-76	1430	101.1	101.1	0	57.01	80.1	6137	-1548	-50	-505	-59	0
7-24-76	1430	103.1	103.1	0	57.01	80.1	6137	-1548	-50	-505	-59	0
7-28-76	1430	105.1	105.1	0	57.01	80.1	6137	-1548	-50	-505	-59	0
8-1-76	1430	107.1	107.1	0	57.01	80.1	6137	-1548	-50	-505	-59	0
8-5-76	1430	109.1	109.1	0	57.01	80.1	6137	-1548	-50	-505	-59	0
8-9-76	1430	111.1	111.1	0	57.01	80.1	6137	-1548	-50	-505	-59	0
8-13-76	1430	113.1	113.1	0	57.01	80.1	6137	-1548	-50	-505	-59	0
8-17-76	1430	115.1	115.1	0	57.01	80.1	6137	-1548	-50	-505	-59	0
8-21-76	1430	117.1	117.1	0	57.01	80.1	6137	-1548	-50	-505	-59	0
8-25-76	1430	119.1	119.1	0	57.01	80.1	6137	-1548	-50	-505	-59	0
8-29-76	1430	121.1	121.1	0	57.01	80.1	6137	-1548	-50	-505	-59	0
9-2-76	1430	123.1	123.1	0	57.01	80.1	6137	-1548	-50	-505	-59	0
9-6-76	1430	125.1	125.1	0	57.01	80.1	6137	-1548	-50	-505	-59	0
9-10-76	1430	127.1	127.1	0	57.01	80.1	6137	-1548	-50	-505	-59	0
9-14-76	1430	129.1	129.1	0	57.01	80.1	6137	-1548	-50	-505	-59	0
9-18-76	1430	131.1	131.1	0	57.01	80.1	6137	-1548	-50	-505	-59	0
9-22-76	1430	133.1	133.1	0	57.01	80.1	6137	-1548	-50	-505	-59	0
9-26-76	1430	135.1	135.1	0	57.01	80.1	6137	-1548	-50	-505	-59	0
9-30-76	1430	137.1	137.1	0	57.01	80.1	6137	-1548	-50	-505	-59	0
10-4-76	1430	139.1	139.1	0	57.01	80.1	6137	-1548	-50	-505	-59	0
10-8-76	1430	141.1	141.1	0	57.01	80.1	6137	-1548	-50	-505	-59	0
10-12-76	1430	143.1	143.1	0	57.01	80.1	6137	-1548	-50	-505	-59	0
10-16-76	1430	145.1	145.1	0	57.01	80.1	6137	-1548	-50	-505	-59	0
10-20-76	1430	147.1	147.1	0	57.01	80.1	6137	-1548	-50	-505	-59	0
10-24-76	1430	149.1	149.1	0	57.01	80.1	6137	-1548	-50	-505	-59	0
10-28-76	1430	151.1	151.1	0	57.01	80.1	6137	-1548	-50	-505	-59	0
11-1-76	1430	153.1	153.1	0	57.01	80.1	6137	-1548	-50	-505	-59	0
11-5-76	1430	155.1	155.1	0	57.01	80.1	6137	-1548	-50	-505	-59	0
11-9-76	1430	157.1	157.1	0	57.01	80.1	6137	-1548	-50	-505	-59	0
11-13-76	1430	159.1	159.1	0	57.01	80.1	6137	-1548	-50	-505	-59	0
11-17-76	1430	161.1	161.1	0	57.01	80.1	6137	-1548	-50	-505	-59	0
11-21-76	1430	163.1	163.1	0	57.01	80.1	6137	-1548	-50	-505	-59	0
11-25-76	1430	165.1	165.1	0	57.01	80.1	6137	-1548	-50	-505	-59	0
11-29-76	1430	167.1	167.1	0	57.01	80.1	6137	-1548	-50	-505	-59	0
12-3-76	1430	169.1	169.1	0	57.01	80.1	6137	-1548	-50	-505	-59	0
12-7-76	1430	171.1	171.1	0	57.01	80.1	6137	-1548	-50	-505	-59	0
12-11-76	1430	173.1	173.1	0	57.01	80.1	6137	-1548	-50	-505	-59	0
12-15-76	1430	175.1	175.1	0	57.01	80.1	6137	-1548	-50	-505	-59	0
12-19-76	1430	177.1	177.1	0	57.01	80.1	6137	-1548	-50	-505	-59	0
12-23-76	1430	179.1	179.1	0	57.01	80.1	6137	-1548	-50	-505	-59	0
12-27-76	1430	181.1	181.1	0	57.01	80.1	6137	-1548	-50	-505	-59	0
1-1-77	1430	183.1	183.1	0	57.01	80.1	6137	-1548	-50	-505	-59	0
1-5-77	1430	185.1	185.1	0	57.01	80.1	6137	-1548	-50	-505	-59	0
1-9-77	1430	187.1										

TABLE 2B

ELASTIC AND CREEP STRAINS (NOT CORRECTED FOR AUTOGENOUS STRAINS)
 (SPECIMEN: SEALED A BY 16 IN. CONCRETE CYL.)

CALIBRATION CONSTANTS:
 METED RESISTANCE AT 0.0 DEGREES F. = 49.2 CHMS
 TEMP. CALIBRATION CONSTANT = 10.76 MICROVOLTS/VOLT/MICROSTRAIN
 STRAIN CALIBRATION CONSTANT = 9.09 MICROVOLTS/VOLT/MICROSTRAIN
 CALIBRATED RANGE = 11100 TO -10100 MICROVOLTS/VOLT
 WELDER COEFF. OF THERMAL EXPANSION = 6.7 MICROSTRAIN/DEGREE F.
 CONCRETE COEFF. OF THERMAL EXPANSION = 5.6 MICROSTRAIN/DEGREE F.
 STRAIN INCREMENT FACTOR = 0 PERCENT

NOTE: FOR MODE 4 OR 5 VOLTS, AND MODE 3 MICROVOLTS -- THE BRIDGE VOLTAGE WAS 2.0000 VOLTS.

DATE	* TIME	* AGE	* DAYS	* UNDER	* MOVS	* DAYS	* REPRST.	* TEMP.	* MODE 3	* CHANGE	* MICROSTRAIN	* TEMPERATURE	* CORRECTED	* MICROSTRAIN	* RELATIVE	* CREEP	* CREEP
2	4-76	1400	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
2	6-75	1100	1.2	0	0	0	0	0	0	0	0	0	0	0	0	0	0
2	12-74	1300	7.4	0	0	0	0	0	0	0	0	0	0	0	0	0	0
2	20-74	1204	15.0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
2	3-74	1204	26.0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	3-76	1205	26.0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	3-76	1205	26.0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	3-76	1433	27.0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	3-76	2110	27.3	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	4-76	1400	28.0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	5-76	1600	29.1	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	6-76	1410	30.0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	6-76	1230	31.1	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	6-76	1208	32.1	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	11-76	1615	38.1	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	12-76	1745	41.4	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	12-76	1745	41.4	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	12-76	1615	47.1	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	12-76	1615	47.1	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4	6-76	1050	61.0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4	6-76	1500	71.1	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4	70-76	1100	84.9	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5	12-76	1340	97.0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5	28-76	1416	105.0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6	10-76	1320	110.0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6	10-76	1150	125.9	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6	10-76	1210	126.0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7	14-76	1316	142.0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7	14-76	1316	142.0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7	14-76	1306	145.0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8	16-76	1410	163.0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8	16-76	1410	163.0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9	6-76	1415	176.0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9	14-76	1430	204.0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10	21-76	1430	233.0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10	21-76	1430	233.0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11	4-76	1500	272.0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11	10-76	1420	286.0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12	20-76	1445	319.0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12	20-76	1370	344.0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
1	20-77	1155	343.0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
1	20-77	1000	363.0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
2	5-77	905	365.0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
2	5-77	905	365.0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
2	5-77	406	365.0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
2	5-77	410	365.0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
2	5-77	415	365.0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
2	5-77	1005	365.0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
2	5-77	1057	365.0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
2	5-77	1214	365.0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
2	5-77	1327	365.0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	7-77	1077	387.0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	7-77	1077	387.0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	7-77	970	387.0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	7-77	1504	387.0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	10-77	1336	371.0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	10-77	1738	360.0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	10-77	1474	385.0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	12-77	1417	411.0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	5-77	900	401.0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	14-77	1405	405.0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	24-77	1131	412.0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
1	30-77	926	416.0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4	6-77	1500	424.0	0	0	0	0	0	0	0	0	0	0	0	0	0	0

MODULUS: LOADING E = 4.5 AT AGE 27 DAYS (STRESS LEVEL 0.10, 2100 PSI)
 NOTE: MINUS DAYS UNDER LCAC INDICATES SPECIMEN LOADING TIME PRIOR TO FULL LOAD

TABLE 3B

ELASTIC AND CREEP STRAINS (NOT CORRECTED FOR AUTIGENOUS STRAINS)
 (SPECIMEN: SEALED 6 BY 16 IN. CONCRETE CYL.)

DATE	TIME	AGE	DAYS	MODE	REGIST.	TEMP.	MOIST.	CHG.	FROM	TEMP.	CORRECTED
						DEGREE	%	PERCENT	PERCENT	PERCENT	
2	1400	0	0	0	0	0	0	0	0	0	0
2	1576	1000	17.8	0	0	0	0	0	0	0	0
2	2076	1000	16.0	0	0	0	0	0	0	0	0
3	576	1500	29.1	0	0	0	0	0	0	0	0
3	1076	1725	33.1	0	0	0	0	0	0	0	0
3	1176	1815	35.1	0	0	0	0	0	0	0	0
3	1276	1900	35.1	0	0	0	0	0	0	0	0
3	1376	1985	35.1	0	0	0	0	0	0	0	0
3	1476	2070	35.1	0	0	0	0	0	0	0	0
3	1576	2155	35.1	0	0	0	0	0	0	0	0
3	1676	2240	35.1	0	0	0	0	0	0	0	0
3	1776	2325	35.1	0	0	0	0	0	0	0	0
3	1876	2410	35.1	0	0	0	0	0	0	0	0
3	1976	2495	35.1	0	0	0	0	0	0	0	0
3	2076	2580	35.1	0	0	0	0	0	0	0	0
3	2176	2665	35.1	0	0	0	0	0	0	0	0
3	2276	2750	35.1	0	0	0	0	0	0	0	0
3	2376	2835	35.1	0	0	0	0	0	0	0	0
3	2476	2920	35.1	0	0	0	0	0	0	0	0
3	2576	3005	35.1	0	0	0	0	0	0	0	0
3	2676	3090	35.1	0	0	0	0	0	0	0	0
3	2776	3175	35.1	0	0	0	0	0	0	0	0
3	2876	3260	35.1	0	0	0	0	0	0	0	0
3	2976	3345	35.1	0	0	0	0	0	0	0	0
3	3076	3430	35.1	0	0	0	0	0	0	0	0
3	3176	3515	35.1	0	0	0	0	0	0	0	0
3	3276	3600	35.1	0	0	0	0	0	0	0	0
3	3376	3685	35.1	0	0	0	0	0	0	0	0
3	3476	3770	35.1	0	0	0	0	0	0	0	0
3	3576	3855	35.1	0	0	0	0	0	0	0	0
3	3676	3940	35.1	0	0	0	0	0	0	0	0
3	3776	4025	35.1	0	0	0	0	0	0	0	0
3	3876	4110	35.1	0	0	0	0	0	0	0	0
3	3976	4195	35.1	0	0	0	0	0	0	0	0
3	4076	4280	35.1	0	0	0	0	0	0	0	0
3	4176	4365	35.1	0	0	0	0	0	0	0	0
3	4276	4450	35.1	0	0	0	0	0	0	0	0
3	4376	4535	35.1	0	0	0	0	0	0	0	0
3	4476	4620	35.1	0	0	0	0	0	0	0	0
3	4576	4705	35.1	0	0	0	0	0	0	0	0
3	4676	4790	35.1	0	0	0	0	0	0	0	0
3	4776	4875	35.1	0	0	0	0	0	0	0	0
3	4876	4960	35.1	0	0	0	0	0	0	0	0
3	4976	5045	35.1	0	0	0	0	0	0	0	0
3	5076	5130	35.1	0	0	0	0	0	0	0	0
3	5176	5215	35.1	0	0	0	0	0	0	0	0
3	5276	5300	35.1	0	0	0	0	0	0	0	0
3	5376	5385	35.1	0	0	0	0	0	0	0	0
3	5476	5470	35.1	0	0	0	0	0	0	0	0
3	5576	5555	35.1	0	0	0	0	0	0	0	0
3	5676	5640	35.1	0	0	0	0	0	0	0	0
3	5776	5725	35.1	0	0	0	0	0	0	0	0
3	5876	5810	35.1	0	0	0	0	0	0	0	0
3	5976	5895	35.1	0	0	0	0	0	0	0	0
3	6076	5980	35.1	0	0	0	0	0	0	0	0
3	6176	6065	35.1	0	0	0	0	0	0	0	0
3	6276	6150	35.1	0	0	0	0	0	0	0	0
3	6376	6235	35.1	0	0	0	0	0	0	0	0
3	6476	6320	35.1	0	0	0	0	0	0	0	0
3	6576	6405	35.1	0	0	0	0	0	0	0	0
3	6676	6490	35.1	0	0	0	0	0	0	0	0
3	6776	6575	35.1	0	0	0	0	0	0	0	0
3	6876	6660	35.1	0	0	0	0	0	0	0	0
3	6976	6745	35.1	0	0	0	0	0	0	0	0
3	7076	6830	35.1	0	0	0	0	0	0	0	0
3	7176	6915	35.1	0	0	0	0	0	0	0	0
3	7276	7000	35.1	0	0	0	0	0	0	0	0
3	7376	7085	35.1	0	0	0	0	0	0	0	0
3	7476	7170	35.1	0	0	0	0	0	0	0	0
3	7576	7255	35.1	0	0	0	0	0	0	0	0
3	7676	7340	35.1	0	0	0	0	0	0	0	0
3	7776	7425	35.1	0	0	0	0	0	0	0	0
3	7876	7510	35.1	0	0	0	0	0	0	0	0
3	7976	7595	35.1	0	0	0	0	0	0	0	0
3	8076	7680	35.1	0	0	0	0	0	0	0	0
3	8176	7765	35.1	0	0	0	0	0	0	0	0
3	8276	7850	35.1	0	0	0	0	0	0	0	0
3	8376	7935	35.1	0	0	0	0	0	0	0	0
3	8476	8020	35.1	0	0	0	0	0	0	0	0
3	8576	8105	35.1	0	0	0	0	0	0	0	0
3	8676	8190	35.1	0	0	0	0	0	0	0	0
3	8776	8275	35.1	0	0	0	0	0	0	0	0
3	8876	8360	35.1	0	0	0	0	0	0	0	0
3	8976	8445	35.1	0	0	0	0	0	0	0	0
3	9076	8530	35.1	0	0	0	0	0	0	0	0
3	9176	8615	35.1	0	0	0	0	0	0	0	0
3	9276	8700	35.1	0	0	0	0	0	0	0	0
3	9376	8785	35.1	0	0	0	0	0	0	0	0
3	9476	8870	35.1	0	0	0	0	0	0	0	0
3	9576	8955	35.1	0	0	0	0	0	0	0	0
3	9676	9040	35.1	0	0	0	0	0	0	0	0
3	9776	9125	35.1	0	0	0	0	0	0	0	0
3	9876	9210	35.1	0	0	0	0	0	0	0	0
3	9976	9295	35.1	0	0	0	0	0	0	0	0
3	10076	9380	35.1	0	0	0	0	0	0	0	0
3	10176	9465	35.1	0	0	0	0	0	0	0	0
3	10276	9550	35.1	0	0	0	0	0	0	0	0
3	10376	9635	35.1	0	0	0	0	0	0	0	0
3	10476	9720	35.1	0	0	0	0	0	0	0	0
3	10576	9805	35.1	0	0	0	0	0	0	0	0
3	10676	9890	35.1	0	0	0	0	0	0	0	0
3	10776	9975	35.1	0	0	0	0	0	0	0	0
3	10876	10060	35.1	0	0	0	0	0	0	0	0
3	10976	10145	35.1	0	0	0	0	0	0	0	0
3	11076	10230	35.1	0	0	0	0	0	0	0	0
3	11176	10315	35.1	0	0	0	0	0	0	0	0
3	11276	10400	35.1	0	0	0	0	0	0	0	0
3	11376	10485	35.1	0	0	0	0	0	0	0	0
3	11476	10570	35.1	0	0	0	0	0	0	0	0
3	11576	10655	35.1	0	0	0	0	0	0	0	0
3	11676	10740	35.1	0	0	0	0	0	0	0	0
3	11776	10825	35.1	0	0	0	0	0	0	0	0
3	11876	10910	35.1	0	0	0	0	0	0	0	0
3	11976	10995	35.1	0	0	0	0	0	0	0	0
3	12076	11080	35.1	0	0	0	0	0	0	0	0
3	12176	11165	35.1	0	0	0	0	0	0	0	0
3	12276	11250	35.1	0	0	0	0	0	0	0	0
3	12376	11335	35.1	0	0	0	0	0	0	0	0
3	12476	11420	35.1	0	0	0	0	0	0	0	0
3	12576	11505	35.1	0	0	0	0	0	0	0	0

TABLE 4B

ELASTIC AND CREEP STRAINS (NOT CORRECTED FOR AUTOMORPHOUS STRAINS)
 (SPECIMEN: 24114 F BY 16 IN. CONCRETE CYL.)

CALIBRATION CONSTANT: 1.0
 SET-POINT RESISTANCE AT 0.0 DEGREES F. = 49.56 OHMS
 TEMPERATURE CALIBRATION CONSTANT = 10.75 F/VOHMS CHANGE IN RESIST.
 STRAIN CALIBRATION CONSTANT = 0.116 MICROVOLTS/VOLV/MICROSTRAIN
 CALIBRATED RANGE = 11.02 MICROSTRAIN/PERCENT STRAIN
 CONCRETE THERMAL EXPANSION = 0.000005 INCH/INCH/DEGREE F.
 STRAIN INCREMENT FACTOR = 0 PERCENT

NOTE: FOR MODE A OF 5 VOLTS, AND MODE B MICROVOLTS -- THE BRIDGE VOLTAGE WAS 2.00000 VOLTS.

DATE	TIME	AGE, DAYS	LOAD, POUNDS	STRESS, P.S.I.	STRAIN, MICROSTRAIN	PERCENT STRAIN	STRAIN RATE, MICROSTRAIN/HR.	PERCENT STRAIN RATE	AGE OF LEADING TEST TEMPERATURE, DEGREES F.	STRAIN RATE NO. 1 SER.	AGE OF LEADING TEST TEMPERATURE, DEGREES F.	STRAIN RATE NO. 2 SER.
2-1-76	1600	0	0	0	0	0	0	0	70.0	12014	0	0
2-1-76	1600	0	100	1000	1000	1000	1000	1000	1000	1000	1000	1000
2-1-76	1600	0	200	2000	2000	2000	2000	2000	2000	2000	2000	2000
2-1-76	1600	0	300	3000	3000	3000	3000	3000	3000	3000	3000	3000
2-1-76	1600	0	400	4000	4000	4000	4000	4000	4000	4000	4000	4000
2-1-76	1600	0	500	5000	5000	5000	5000	5000	5000	5000	5000	5000
2-1-76	1600	0	600	6000	6000	6000	6000	6000	6000	6000	6000	6000
2-1-76	1600	0	700	7000	7000	7000	7000	7000	7000	7000	7000	7000
2-1-76	1600	0	800	8000	8000	8000	8000	8000	8000	8000	8000	8000
2-1-76	1600	0	900	9000	9000	9000	9000	9000	9000	9000	9000	9000
2-1-76	1600	0	1000	10000	10000	10000	10000	10000	10000	10000	10000	10000
2-1-76	1600	0	1100	11000	11000	11000	11000	11000	11000	11000	11000	11000
2-1-76	1600	0	1200	12000	12000	12000	12000	12000	12000	12000	12000	12000
2-1-76	1600	0	1300	13000	13000	13000	13000	13000	13000	13000	13000	13000
2-1-76	1600	0	1400	14000	14000	14000	14000	14000	14000	14000	14000	14000
2-1-76	1600	0	1500	15000	15000	15000	15000	15000	15000	15000	15000	15000
2-1-76	1600	0	1600	16000	16000	16000	16000	16000	16000	16000	16000	16000
2-1-76	1600	0	1700	17000	17000	17000	17000	17000	17000	17000	17000	17000
2-1-76	1600	0	1800	18000	18000	18000	18000	18000	18000	18000	18000	18000
2-1-76	1600	0	1900	19000	19000	19000	19000	19000	19000	19000	19000	19000
2-1-76	1600	0	2000	20000	20000	20000	20000	20000	20000	20000	20000	20000
2-1-76	1600	0	2100	21000	21000	21000	21000	21000	21000	21000	21000	21000
2-1-76	1600	0	2200	22000	22000	22000	22000	22000	22000	22000	22000	22000
2-1-76	1600	0	2300	23000	23000	23000	23000	23000	23000	23000	23000	23000
2-1-76	1600	0	2400	24000	24000	24000	24000	24000	24000	24000	24000	24000
2-1-76	1600	0	2500	25000	25000	25000	25000	25000	25000	25000	25000	25000
2-1-76	1600	0	2600	26000	26000	26000	26000	26000	26000	26000	26000	26000
2-1-76	1600	0	2700	27000	27000	27000	27000	27000	27000	27000	27000	27000
2-1-76	1600	0	2800	28000	28000	28000	28000	28000	28000	28000	28000	28000
2-1-76	1600	0	2900	29000	29000	29000	29000	29000	29000	29000	29000	29000
2-1-76	1600	0	3000	30000	30000	30000	30000	30000	30000	30000	30000	30000
2-1-76	1600	0	3100	31000	31000	31000	31000	31000	31000	31000	31000	31000
2-1-76	1600	0	3200	32000	32000	32000	32000	32000	32000	32000	32000	32000
2-1-76	1600	0	3300	33000	33000	33000	33000	33000	33000	33000	33000	33000
2-1-76	1600	0	3400	34000	34000	34000	34000	34000	34000	34000	34000	34000
2-1-76	1600	0	3500	35000	35000	35000	35000	35000	35000	35000	35000	35000
2-1-76	1600	0	3600	36000	36000	36000	36000	36000	36000	36000	36000	36000
2-1-76	1600	0	3700	37000	37000	37000	37000	37000	37000	37000	37000	37000
2-1-76	1600	0	3800	38000	38000	38000	38000	38000	38000	38000	38000	38000
2-1-76	1600	0	3900	39000	39000	39000	39000	39000	39000	39000	39000	39000
2-1-76	1600	0	4000	40000	40000	40000	40000	40000	40000	40000	40000	40000
2-1-76	1600	0	4100	41000	41000	41000	41000	41000	41000	41000	41000	41000
2-1-76	1600	0	4200	42000	42000	42000	42000	42000	42000	42000	42000	42000
2-1-76	1600	0	4300	43000	43000	43000	43000	43000	43000	43000	43000	43000
2-1-76	1600	0	4400	44000	44000	44000	44000	44000	44000	44000	44000	44000
2-1-76	1600	0	4500	45000	45000	45000	45000	45000	45000	45000	45000	45000
2-1-76	1600	0	4600	46000	46000	46000	46000	46000	46000	46000	46000	46000
2-1-76	1600	0	4700	47000	47000	47000	47000	47000	47000	47000	47000	47000
2-1-76	1600	0	4800	48000	48000	48000	48000	48000	48000	48000	48000	48000
2-1-76	1600	0	4900	49000	49000	49000	49000	49000	49000	49000	49000	49000
2-1-76	1600	0	5000	50000	50000	50000	50000	50000	50000	50000	50000	50000
2-1-76	1600	0	5100	51000	51000	51000	51000	51000	51000	51000	51000	51000
2-1-76	1600	0	5200	52000	52000	52000	52000	52000	52000	52000	52000	52000
2-1-76	1600	0	5300	53000	53000	53000	53000	53000	53000	53000	53000	53000
2-1-76	1600	0	5400	54000	54000	54000	54000	54000	54000	54000	54000	54000
2-1-76	1600	0	5500	55000	55000	55000	55000	55000	55000	55000	55000	55000
2-1-76	1600	0	5600	56000	56000	56000	56000	56000	56000	56000	56000	56000
2-1-76	1600	0	5700	57000	57000	57000	57000	57000	57000	57000	57000	57000
2-1-76	1600	0	5800	58000	58000	58000	58000	58000	58000	58000	58000	58000
2-1-76	1600	0	5900	59000	59000	59000	59000	59000	59000	59000	59000	59000
2-1-76	1600	0	6000	60000	60000	60000	60000	60000	60000	60000	60000	60000
2-1-76	1600	0	6100	61000	61000	61000	61000	61000	61000	61000	61000	61000
2-1-76	1600	0	6200	62000	62000	62000	62000	62000	62000	62000	62000	62000
2-1-76	1600	0	6300	63000	63000	63000	63000	63000	63000	63000	63000	63000
2-1-76	1600	0	6400	64000	64000	64000	64000	64000	64000	64000	64000	64000
2-1-76	1600	0	6500	65000	65000	65000	65000	65000	65000	65000	65000	65000
2-1-76	1600	0	6600	66000	66000	66000	66000	66000	66000	66000	66000	66000
2-1-76	1600	0	6700	67000	67000	67000	67000	67000	67000	67000	67000	67000
2-1-76	1600	0	6800	68000	68000	68000	68000	68000	68000	68000	68000	68000
2-1-76	1600	0	6900	69000	69000	69000	69000	69000	69000	69000	69000	69000
2-1-76	1600	0	7000	70000	70000	70000	70000	70000	70000	70000	70000	70000
2-1-76	1600	0	7100	71000	71000	71000	71000	71000	71000	71000	71000	71000
2-1-76	1600	0	7200	72000	72000	72000	72000	72000	72000	72000	72000	72000
2-1-76	1600	0	7300	73000	73000	73000	73000	73000	73000	73000	73000	73000
2-1-76	1600	0	7400	74000	74000	74000	74000	74000	74000	74000	74000	74000
2-1-76	1600	0	7500	75000	75000	75000	75000	75000	75000	75000	75000	75000
2-1-76	1600	0	7600	76000	76000	76000	76000	76000	76000	76000	76000	76000
2-1-76	1600	0	7700	77000	77000	77000	77000	77000	77000	77000	77000	77000
2-1-76	1600	0	7800	78000	78000	78000	78000	78000	78000	78000	78000	78000
2-1-76	1600	0	7900	79000	79000	79000	79000	79000	79000	79000	79000	79000
2-1-76	1600	0	8000	80000	80000	80000	80000	80000	80000	80000	80000	80000
2-1-76	1600	0	8100	81000	81000	81000	81000	81000	81000	81000	81000	81000
2-1-76	1600	0	8200	82000	82000							

ELASTIC AND CREEP STRAINS (NOT CORRECTED FOR AUTOGENOUS STRAINS)
WOLF CREEK SECTION 1 CLASS 2-2-57
(SPECIMEN: SEALED 6 BY 16 IN. CONCRETE C.Y.)

CALIBRATION CONSTANTS:
TEMP. RESISTANCE AT 0.0 DEGREE F. = 44.11 CHMS
CALIBRATION CONSTANT = 10.0 PA F/1000 CHMS
STRAIN CALIBRATION CONSTANT = 9.16 MICROVOLTS/VOLTS/MICROSTRAIN
METER CALIBRATION RANGE = 11100 TO -10100 MICROVOLTS/VOLTS
CONCRETE COEFF. OF THERMAL EXPANSION = 6.7 MICROSTRAIN/DEGREE F.
STRAIN INCREMENT FACTOR = 0 PERCENT

NOTE: FOR MODE 4 OR 5 VOLTS, AND MODE 3 MICROVOLTS -- THE BRIDGE VOLTAGE WAS 2.00000 VOLTS.

Table with columns: DATE, TIME, AGE, DAYS, MODE, LOAD, VOLTS, CHMS, DEGREE, MICROSTRAIN, MICROSTRAIN, TEMPERATURE CORRECTED, FROM ELASTIC CREEP, ELECTRIC, STRAIN METER NO., AGE OF LOADING, TEST TEMPERATURE, U.L.T. STR., APPLIED TEST STRESS, PER. U.L.T. STR. APPLIC.

MODULUS: LOADING = 512 AT AGE 336 DAYS (STRESS LEVEL 0 TO 2100 PSI)
NOTE: MINUS DAYS UNDER LOAD INDICATES SPECIMEN LOADING TIME PRIOR TO FULL LOAD

TABLE 6A

ELASTIC AND CREEP STRAINS (NOT CORRECTED FOR AUTOGENOUS STRAINS)
 WOLFE CREEK OPTION 1 CLASS E-2 TEST 38A
 (SPECIMEN: SEALED 6 BY 16 IN. CONCRETE CYL.)

CALIBRATION CONSTANTS: 4 DEGREES F. = 48.56 OHMS
 WEEP RESISTANCE AT CONSTANT LOAD = 10.78 OHMS
 STRAIN CALIBRATION CONSTANT = 0.09 MICROVOLTS/VOLT/MICROSTRAIN
 CALIBRATED RANGE = 1100 TO -10100 MICROVOLTS/VOLT
 WEEP COEFF. OF THERMAL EXPANSION = 6.7 MICRONS/IN/DEGREE F.
 CONCRETE COEFF. OF THERMAL EXPANSION = 3.7 MICRONS/IN/DEGREE F.
 STRAIN INCREMENT FACTOR = 0 PERCENT

STRAIN METER NO.: 935
 AGE OF LOADING: 343 DAYS
 TEST TEMPERATURE: 110 DEG. F.
 U.L.T. STR.: 9550 PSI
 APPLIED TEST STRESS: 2100 PSI
 PER. LUT. STR. APPLIED: 21.0 PERCENT

NOTE: FOR MODE 4 DR 5 VOLTS AND MODE 3 MICROVOLTS -- THE BRIDGE VOLTAGE WAS 2.0000 VOLTS.

DATE	TIME	AGE	DAYS	MODE	RESIST.	TEMP.	CHARGE	MICROSTRAIN	TEMPERATURE	CORRECTED
*	*	*	*	*	* OHMS	* DEGREE F.	* VOLTS	* MICROSTRAIN	* DEGREE F.	* MICROSTRAIN
2	14:00	0	0	3	57.77	78.4	5700	0	0	0
2	16:15	19	19	3	55.46	75.4	5622	-128	-15	-15
2	12:16	1000	1000	3	56.67	75.4	5622	-1530	-45	-45
2	20:16	1300	1300	3	56.91	75.7	5622	-1530	-45	-45
2	16:16	1500	1500	3	56.66	75.7	5622	-1530	-45	-45
2	10:16	1615	1615	3	56.66	75.7	5622	-1530	-45	-45
2	11:16	1615	1615	3	56.66	75.7	5622	-1530	-45	-45
2	12:16	1700	1700	3	56.66	75.7	5622	-1530	-45	-45
2	14:16	1745	1745	3	56.66	75.7	5622	-1530	-45	-45
2	16:16	1800	1800	3	56.66	75.7	5622	-1530	-45	-45
2	18:16	1845	1845	3	56.66	75.7	5622	-1530	-45	-45
2	20:16	1900	1900	3	56.66	75.7	5622	-1530	-45	-45
2	22:16	1945	1945	3	56.66	75.7	5622	-1530	-45	-45
2	24:16	2000	2000	3	56.66	75.7	5622	-1530	-45	-45
2	26:16	2045	2045	3	56.66	75.7	5622	-1530	-45	-45
2	28:16	2100	2100	3	56.66	75.7	5622	-1530	-45	-45
2	30:16	2145	2145	3	56.66	75.7	5622	-1530	-45	-45
2	32:16	2200	2200	3	56.66	75.7	5622	-1530	-45	-45
2	34:16	2245	2245	3	56.66	75.7	5622	-1530	-45	-45
2	36:16	2300	2300	3	56.66	75.7	5622	-1530	-45	-45
2	38:16	2345	2345	3	56.66	75.7	5622	-1530	-45	-45
2	40:16	2400	2400	3	56.66	75.7	5622	-1530	-45	-45
2	42:16	2445	2445	3	56.66	75.7	5622	-1530	-45	-45
2	44:16	2500	2500	3	56.66	75.7	5622	-1530	-45	-45
2	46:16	2545	2545	3	56.66	75.7	5622	-1530	-45	-45
2	48:16	2600	2600	3	56.66	75.7	5622	-1530	-45	-45
2	50:16	2645	2645	3	56.66	75.7	5622	-1530	-45	-45
2	52:16	2700	2700	3	56.66	75.7	5622	-1530	-45	-45
2	54:16	2745	2745	3	56.66	75.7	5622	-1530	-45	-45
2	56:16	2800	2800	3	56.66	75.7	5622	-1530	-45	-45
2	58:16	2845	2845	3	56.66	75.7	5622	-1530	-45	-45
2	60:16	2900	2900	3	56.66	75.7	5622	-1530	-45	-45
2	62:16	2945	2945	3	56.66	75.7	5622	-1530	-45	-45
2	64:16	3000	3000	3	56.66	75.7	5622	-1530	-45	-45
2	66:16	3045	3045	3	56.66	75.7	5622	-1530	-45	-45
2	68:16	3100	3100	3	56.66	75.7	5622	-1530	-45	-45
2	70:16	3145	3145	3	56.66	75.7	5622	-1530	-45	-45
2	72:16	3200	3200	3	56.66	75.7	5622	-1530	-45	-45
2	74:16	3245	3245	3	56.66	75.7	5622	-1530	-45	-45
2	76:16	3300	3300	3	56.66	75.7	5622	-1530	-45	-45
2	78:16	3345	3345	3	56.66	75.7	5622	-1530	-45	-45
2	80:16	3400	3400	3	56.66	75.7	5622	-1530	-45	-45
2	82:16	3445	3445	3	56.66	75.7	5622	-1530	-45	-45
2	84:16	3500	3500	3	56.66	75.7	5622	-1530	-45	-45
2	86:16	3545	3545	3	56.66	75.7	5622	-1530	-45	-45
2	88:16	3600	3600	3	56.66	75.7	5622	-1530	-45	-45
2	90:16	3645	3645	3	56.66	75.7	5622	-1530	-45	-45
2	92:16	3700	3700	3	56.66	75.7	5622	-1530	-45	-45
2	94:16	3745	3745	3	56.66	75.7	5622	-1530	-45	-45
2	96:16	3800	3800	3	56.66	75.7	5622	-1530	-45	-45
2	98:16	3845	3845	3	56.66	75.7	5622	-1530	-45	-45
2	100:16	3900	3900	3	56.66	75.7	5622	-1530	-45	-45
2	102:16	3945	3945	3	56.66	75.7	5622	-1530	-45	-45
2	104:16	4000	4000	3	56.66	75.7	5622	-1530	-45	-45
2	106:16	4045	4045	3	56.66	75.7	5622	-1530	-45	-45
2	108:16	4100	4100	3	56.66	75.7	5622	-1530	-45	-45
2	110:16	4145	4145	3	56.66	75.7	5622	-1530	-45	-45
2	112:16	4200	4200	3	56.66	75.7	5622	-1530	-45	-45
2	114:16	4245	4245	3	56.66	75.7	5622	-1530	-45	-45
2	116:16	4300	4300	3	56.66	75.7	5622	-1530	-45	-45
2	118:16	4345	4345	3	56.66	75.7	5622	-1530	-45	-45
2	120:16	4400	4400	3	56.66	75.7	5622	-1530	-45	-45
2	122:16	4445	4445	3	56.66	75.7	5622	-1530	-45	-45
2	124:16	4500	4500	3	56.66	75.7	5622	-1530	-45	-45
2	126:16	4545	4545	3	56.66	75.7	5622	-1530	-45	-45
2	128:16	4600	4600	3	56.66	75.7	5622	-1530	-45	-45
2	130:16	4645	4645	3	56.66	75.7	5622	-1530	-45	-45
2	132:16	4700	4700	3	56.66	75.7	5622	-1530	-45	-45
2	134:16	4745	4745	3	56.66	75.7	5622	-1530	-45	-45
2	136:16	4800	4800	3	56.66	75.7	5622	-1530	-45	-45
2	138:16	4845	4845	3	56.66	75.7	5622	-1530	-45	-45
2	140:16	4900	4900	3	56.66	75.7	5622	-1530	-45	-45
2	142:16	4945	4945	3	56.66	75.7	5622	-1530	-45	-45
2	144:16	5000	5000	3	56.66	75.7	5622	-1530	-45	-45
2	146:16	5045	5045	3	56.66	75.7	5622	-1530	-45	-45
2	148:16	5100	5100	3	56.66	75.7	5622	-1530	-45	-45
2	150:16	5145	5145	3	56.66	75.7	5622	-1530	-45	-45

LOADING: SPECIMEN FULLY LOADED, APPLIED TEST STRESS 2100 PSI

NOTE: MINUS DAYS UNDER LOAD INDICATES SPECIMEN LOADING TIME PRIOR TO FULL LOAD

ELASTIC AND CREEP STRAINS (NOT CORRECTED FOR AUTOCGENOUS STRAINS)

WOLF CHECK BOTTOM 1 CLASS E-2 E5738A
(SPECIMEN: SEALED 6 BY 16 IN. CONCRETE CYL.)

CALIBRATION CONSTANTS:
 METER RESISTANCE AT 0.0 DEGREES F. = 48.32 OHMS STRAIN METER NO. : 531 73.12
 TEMP. CALIBRATION CONSTANT = 10.91 MICROVOLTS/VOLT/MICROSTRAIN AGE OF LOADING : 365 DAYS
 STRAIN CALIBRATION CONSTANT = 9.29 MICROVOLTS/VOLT/MICROSTRAIN TEST TEMPERATURE : 73 DEGC. F.
 CALIBRATED RANGE = 11100 TO -10100 MICROVOLTS/VOLT
 METER COEFF. OF THERMAL EXPANSION = 3.7 MICROCSTRAIN/DEGREE F. ULT. STR. : 8200. PSI
 CONCRETE COEFF. OF THERMAL EXPANSION = 6 PERCENT APPLIED TEST STRESS : 2100. PSI
 STRAIN INCREMENT FACTOR = 6 PERCENT PER. ULT. STR. APPLIED: 25.6 PERCENT

NOTE: FOR MODE 4 OR 5 VOLTS, AND MODE 3 MICROVOLTS -- THE BRIDGE VOLTAGE WAS 2.00000 VOLTS.

DATE	* TIME	* AGE,	* DAYS	* MODE	* RESIST.	* TEMP.	* CHARGE	* MICRO	* MICRO	* ELASTIC	* CREEP	* SPECIFIC
* 2	-4-76	1400	0	3	55.63	79.0	0	9709	0	0	0	0
2	-12-76	1000	1.9	3	55.38	76.3	-122	9587	-122	-14	-14	-14
2	-20-76	1300	7.9	3	54.89	71.1	-264	9445	-264	-37	-37	-37
3	-5-76	1600	15.0	3	54.80	70.0	-231	9478	-231	-39	-39	-39
3	-10-76	1545	14.1	3	54.81	70.2	-248	9461	-248	-39	-39	-39
3	-11-76	1515	13.1	3	54.82	70.3	-255	9454	-255	-39	-39	-39
3	-12-76	1370	11.8	3	54.83	70.4	-262	9447	-262	-39	-39	-39
3	-17-76	1745	41.2	3	54.95	71.6	-370	9370	-370	-39	-39	-39
3	-21-76	1615	47.1	3	54.88	70.9	-249	9420	-249	-39	-39	-39
4	-1-76	1810	54.8	3	54.83	70.4	-214	9495	-214	-36	-36	-36
4	-9-76	1050	63.9	3	54.95	70.6	-205	9504	-205	-34	-34	-34
4	-16-76	1600	71.1	3	54.80	71.1	-180	9510	-180	-34	-34	-34
4	-30-76	1100	84.9	3	54.84	70.5	-133	9575	-133	-32	-32	-32
5	-12-76	1140	87.0	3	54.95	71.6	-132	9557	-132	-30	-30	-30
5	-20-76	1415	105.0	3	54.82	71.3	-114	9595	-114	-29	-29	-29
6	-10-76	1150	125.9	3	54.89	71.0	-52	9687	-52	-27	-27	-27
6	-18-76	1370	138.0	3	54.98	72.0	-59	9610	-59	-26	-26	-26
6	-28-76	1430	145.0	3	55.16	73.9	-151	9648	-151	-23	-23	-23
6	-30-76	1315	145.0	3	54.93	71.5	-110	9599	-110	-22	-22	-22
7	-14-76	915	159.8	3	55.01	72.3	-49	9660	-49	-22	-22	-22
7	-20-76	1500	168.0	3	55.02	72.4	-85	9628	-85	-24	-24	-24
7	-26-76	1600	175.1	3	55.02	72.4	-17	9662	-17	-21	-21	-21
8	-2-76	1185	178.9	3	55.05	72.7	-10	9600	-10	-19	-19	-19
8	-6-76	1300	183.0	3	55.08	73.1	-49	9658	-49	-20	-20	-20
8	-16-76	1410	193.0	3	55.06	72.8	-41	9658	-41	-20	-20	-20
8	-23-76	1670	200.1	3	55.11	73.4	-71	9648	-71	-19	-19	-19
9	-6-76	1815	213.8	3	55.05	72.7	-10	9659	-10	-19	-19	-19
9	-16-76	1430	224.0	3	55.06	72.8	-14	9695	-14	-19	-19	-19
9	-21-76	1700	229.0	3	55.07	72.9	2	9711	2	-18	-18	-18
10	-1-76	1905	234.5	3	55.08	73.1	131	9840	131	-11	-11	-11
11	-4-76	1100	272.9	3	55.01	72.3	219	9907	219	-10	-10	-10
11	-19-76	1430	288.0	3	54.99	72.1	219	9928	219	-9	-9	-9
12	-20-76	1445	315.0	3	54.94	71.5	303	10017	303	-7	-7	-7
1	-14-77	1200	343.9	3	54.88	70.6	329	10038	329	-7	-7	-7
1	-16-77	1050	348.9	3	54.89	71.0	354	10067	354	-6	-6	-6
2	-3-77	945	363.8	3	54.92	71.4	354	10063	354	-5	-5	-5
2	-5-77	826	365.8	3	54.91	71.2	383	10074	383	-5	-5	-5
2	-5-77	920	365.8	3	54.92	71.4	383	10092	383	-3	-3	-3

TABLE 10A

ELASTIC AND CREEP STRAINS (NOT CORRECTED FOR AUTOCENTRUS STRAINS)

WOLF CHECK OPTION 1 CLASS E-2 E5739R
(SPECIMEN: SEALED 6 BY 16 IN. CONCRETE CVL.)

CALIBRATION CONSTANTS:

TEMP. RESISTANCE AT 0.0 DEGREES F. = 48.50 OHMS STRAIN METER NO. : 535 11 CA
 TEMP. CALIBRATION CONSTANT = 10.75 F/OHM CHANGE IN RESIST. AGE OF LOADING : 323 DAYS
 STRAIN CALIBRATION CONSTANT = 9.09 MICROVOLTS/VOLT/MICROSTRAIN TEST TEMPERATURE : 110 DEG. F.
 CALIBRATED RANGE = 1100 TO -10100 MICROVOLTS/VOLT
 METER COEFF. OF THERMAL EXPANSION = 6.87 MICROSTRAIN/DEGREE F. ULT. STR. : 0. PSI
 CONCRETE COEFF. OF THERMAL EXPANSION = 3.5 MICROSTRAIN/DEGREE F. APPLIED TEST STRESS : 2100. PSI
 STRAIN INCREMENT FACTOR = 0 PERCENT PER. ULT. STR. APPLIED: F PERCENT

NOTE: FOR MODE 4 OR 5 VOLTS, AND MODE 3 MICROVOLTS -- THE BRIDGE VOLTAGE WAS 2.00000 VOLTS.

DATE	* TIME	* AGE,	* DAYS	* MOLE	* RESIST.	* TEMP.	* MODE	* CHANGE	* MICROSTRAIN	* TEMPERATURE	* CORRECTED
		* DAYS	* UNDER	* 4 OR 5	* OHMS	* DEGREE	* F.	* VOLTS	* MICRO	* FROM	* ELASTIC
			* LOAD	* VOLTS				* VOLTS	* DAY ONE	* +CREEP	* CREEP
* 2	-4-75	1400	0		55.77	78.4		5790	0		
2	-6-76	1100	1.9		55.49	75.4		5672	-128		-15
2	-12-76	1000	7.9		56.81	89.7		4240	-1350		-49
3	-5-76	1600	29.1		56.66	109.7		3251	-2639		-42
3	-10-76	1545	34.1		57.92	101.7		3312	-1578		-36
3	-11-76	1615	35.1		56.51	108.0		3475	-2315		-35
3	-12-76	1710	45.1		56.45	109.6		3283	-2407		-35
3	-17-76	1745	41.2		56.75	110.5		3271	-2519		-38
3	-21-76	1615	47.1		56.71	110.5		3174	-2612		-44
3	-31-76	1410	54.4		56.74	110.5		3140	-2630		-45
4	-6-76	1950	67.9		56.77	110.9		3129	-2661		-45
4	-16-76	1600	71.1		56.53	108.2		3271	-2515		-45
4	-30-76	1100	84.9		56.64	109.5		3175	-2615		-47
5	-13-76	1360	97.0		56.84	111.5		3046	-2744		-47
5	-20-76	1415	105.0		56.85	111.7		3015	-2775		-48
5	-25-76	1320	110.0		56.80	111.8		2986	-2804		-50
5	-10-76	1150	134.9		56.89	121.1		2949	-2821		-50
6	-14-76	1330	138.0		56.68	108.9		3065	-2725		-51
6	-29-76	1435	144.0		56.42	106.1		3110	-2680		-51
6	-29-76	1430	145.0		56.67	109.7		3082	-2708		-51
7	-14-76	915	150.8		56.58	108.7		3101	-2689		-53
7	-20-76	1500	175.0		56.62	109.2		3058	-2652		-52
7	-29-76	1600	175.1		56.72	110.3		3076	-2714		-48
8	-2-76	1415	179.0		56.80	111.2		3032	-2758		-49
8	-6-76	1200	183.0		56.68	105.8		3194	-2546		-57
8	-16-76	1410	193.0		56.51	112.3		2850	-2570		-56
8	-23-76	1430	200.1		56.60	109.2		2959	-2631		-59
9	-6-76	815	213.8		56.76	110.7		2929	-2841		-56
9	-16-76	1430	224.0		56.67	109.7		2617	-2873		-50
9	-21-76	1330	223.0		56.61	104.1		2812	-2878		-52
10	-1-76	905	233.8		56.62	105.2		2856	-2934		-65
12	-20-76	1445	319.0		56.71	110.1		2554	-3236		-70
1	-14-77	1330	344.0		56.66	109.6		2417	-3373		-98
1	-20-77	1135	369.9		56.67	105.7		2384	-3406		-85
2	-3-77	1000	363.8		56.71	110.1		2311	-3479		-92
2	-5-77	951	365.8		56.70	110.1		2322	-3468		-92
2	-5-77	754	365.7		56.68	109.8		2326	-3461		-92
2	-5-77	955	365.4		56.70	110.1		2322	-3468		-92

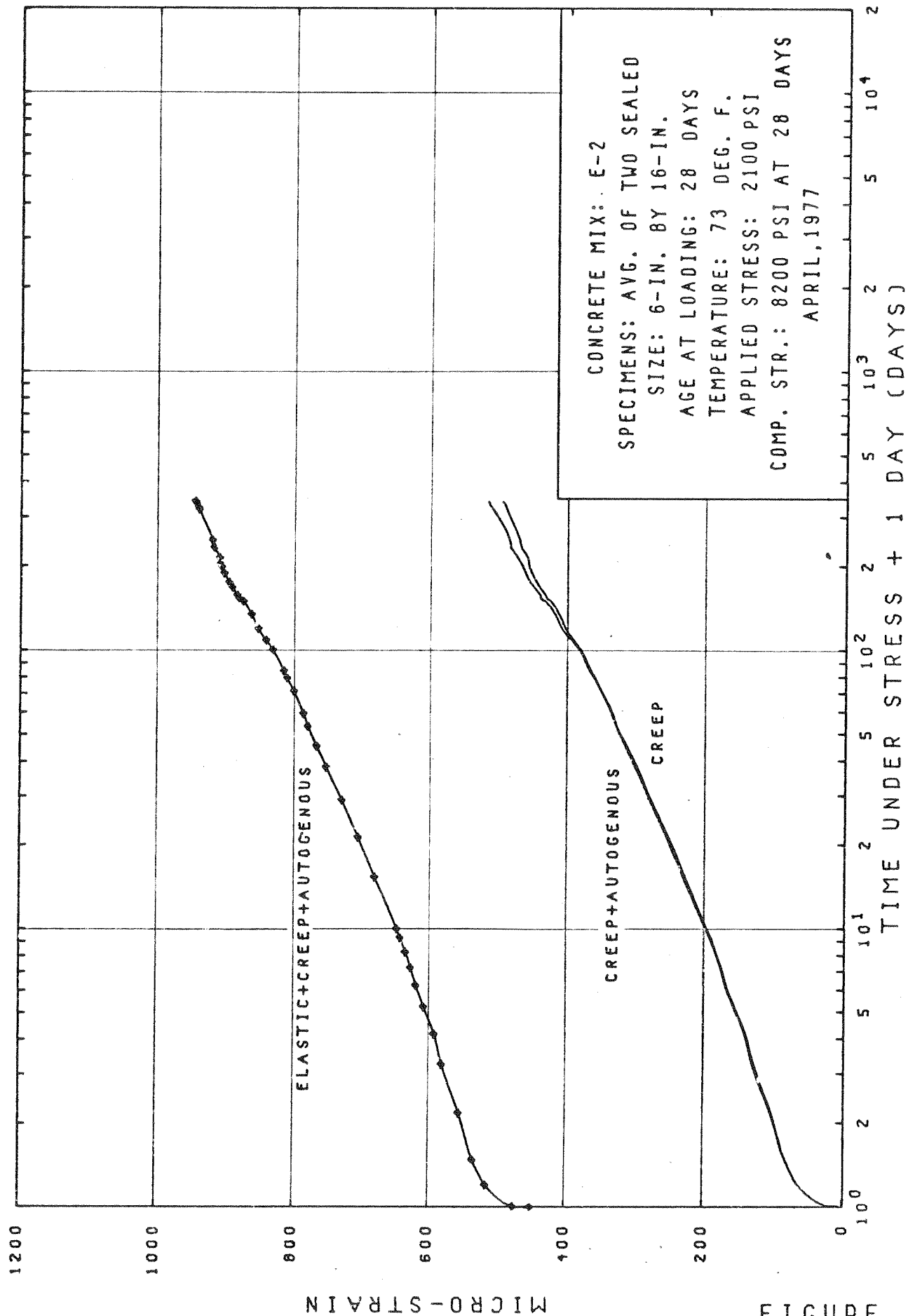
ELASTIC AND CREEP STRAINS (NOT CORRECTED FOR AUTOGENOUS STRAINS)
 WOLF CHECK OPTION 1 CLASS E-2 E57388
 (SPECIMEN: SEALED 6 HY 16 IN. CONCRETE CYL.)

CALIBRATION CONSTANTS:
 METER RESISTANCE AT 0.0 DEGREES F. = 49.51 OHMS
 TEMP. CALIBRATION CONSTANT = 10.70 MICROVOLTS/VOLTS/MICROSTRAIN
 STRAIN CALIBRATION CONSTANT = 0.19 MICROVOLTS/VOLTS/MICROSTRAIN
 CALIBRATED RANGE = 11100 TO -10100 MICROVOLTS/VOLTS
 METER COEFF. OF THERMAL EXPANSION = 6.7 MICROSTRAIN/DEGREE F.
 CONCRETE COEFF. OF THERMAL EXPANSION = 3.6 MICROSTRAIN/DEGREE F.
 STRAIN INCREMENT FACTOR = 0 PERCENT

NOTE: FOR MODE 4 OR 5 VOLTS, AND MODE 3 MICROVOLTS -- THE BRIDGE VOLTAGE WAS 2.00000 VOLTS.

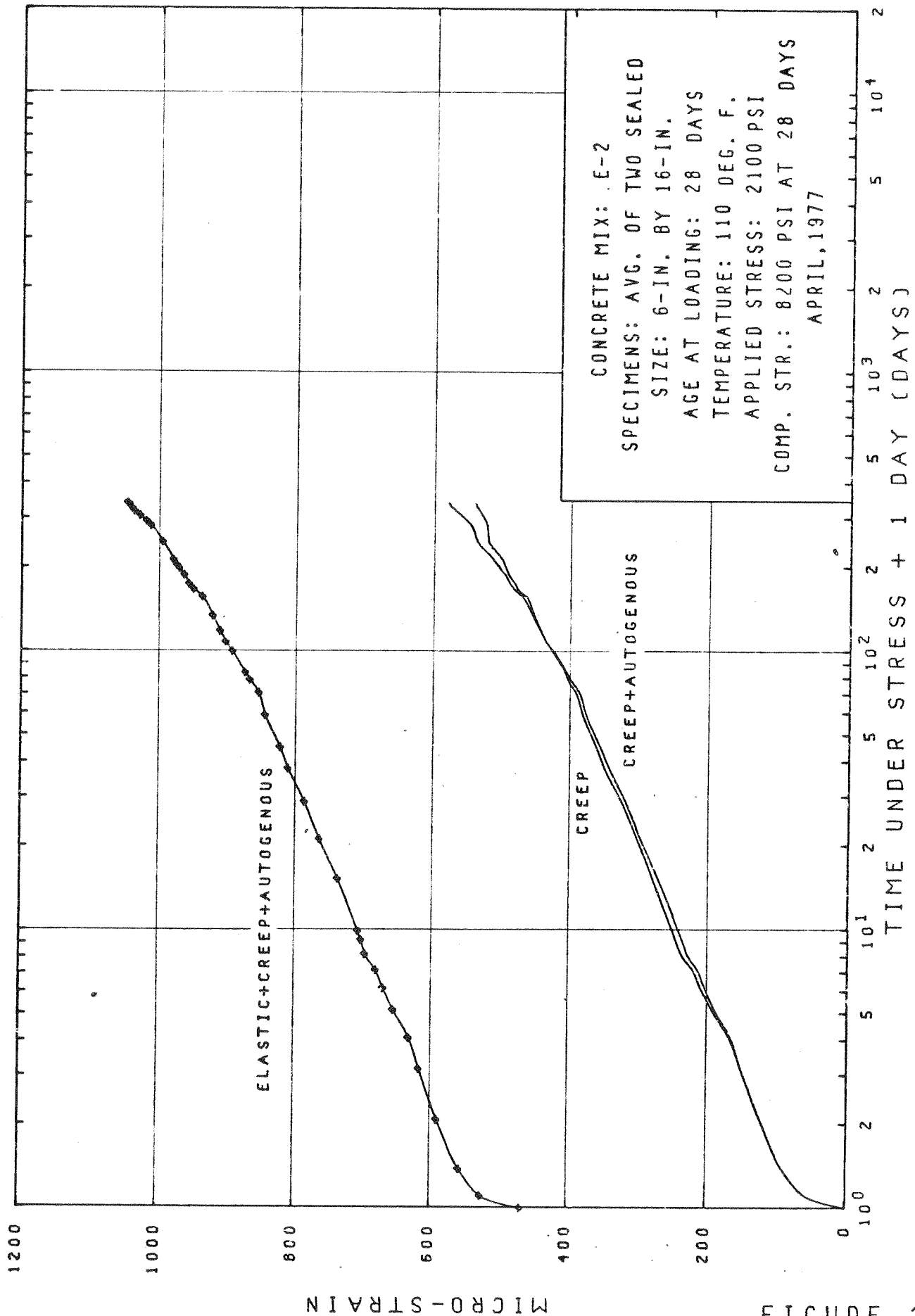
DATE	* TIME	* AGE,	* DAYS	* MORE	* RESIST.	* TEMP.	* MODE	* CHANGE	* MICROSTRAIN	* MICROSTRAIN	* TEMPERATURE	* CORRECTED
		* DAYS	* UNDER	* 4 OR 5	* OHMS	* DEGREE	* MICRO-	* FROM	* ELASTIC	* CREEP	* SPECIFIC	
			* LOAD	* VOLTS	* F.	* F.	* VOLTS	* DAY	* CREEP	* CREEP	* PERCENT	
				* SPECIMEN								
				CAST								
2	4-76	1400	0		56.15	77.9	11892	0				
2	4-76	1100	1.0	16256	56.45	70.0	11671	-221				
2	12-76	1000	7.4	16819	57.24	65.1	10255	-1637				
2	20-76	1300	15.0	135454	59.09	108.9	9245	-2647				
3	5-76	1600	29.1	134056	59.35	101.1	9871	-2021				
3	10-76	1545	34.1	134605	59.92	107.1	8561	-2331				
3	11-76	1615	35.1	134182	59.06	108.6	9477	-2415				
3	12-76	1930	35.8	134039	59.16	105.7	5439	-2453				
3	17-76	1745	41.2	134003	58.12	109.3	9462	-2430				
3	22-76	1415	47.1	134030	58.10	105.7	6476	-2417				
3	31-76	1410	54.8	134002	59.10	110.0	6492	-2400				
4	9-76	1650	61.9	133583	58.92	107.1	6643	-2249				
4	16-76	1600	71.1	134167	59.07	108.7	5543	-2748				
4	20-76	1100	84.9	134070	59.24	110.5	6422	-2470				
5	20-76	1415	87.0	133843	59.26	110.7	5365	-2497				
5	20-76	1415	105.0	133923	59.27	110.7	5360	-2132				
6	28-76	1320	125.9	133928	59.10	110.0	9744	-2544				
6	10-76	1150	125.9	133518	59.03	109.0	9420	-2472				
5	14-76	1330	134.0	134050	59.02	108.3	9448	-2444				
5	28-76	1435	145.0	134102	59.02	108.6	6436	-2456				
5	29-76	1430	145.0	134076	59.02	107.7	6445	-2447				
7	14-76	915	153.8	134144	59.02	108.2	9452	-2440				
7	20-76	1500	166.0	134109	59.11	109.2	5412	-2440				
7	29-76	1600	175.1	134078	59.16	109.7	9372	-2520				
9	2-76	1415	179.0	134003	59.70	104.8	5533	-2759				
9	6-76	1300	183.0	134268	59.10	111.1	8213	-2879				
9	17-76	1410	191.0	133702	59.00	108.0	9330	-2562				
8	23-76	1430	200.1	134122	59.11	109.1	5309	-2583				
9	5-76	915	211.8	134043	59.08	108.8	9265	-2627				
9	16-76	1430	224.0	134062	59.02	109.2	5276	-2613				
9	21-76	1370	229.0	134107	59.10	109.1	9178	-2714				
10	1-76	905	239.8	134047	59.15	109.5	8416	-2476				
12	20-76	1445	319.0	134014	59.10	109.0	8416	-2476				
1	14-77	1370	318.0	134014	59.10	109.0	8416	-2476				
1	20-77	1155	349.9	134050	59.14	105.4	8707	-1185				
2	3-77	1000	353.8	134020	59.15	109.5	8669	-1193				
2	5-77	1754	365.7	134034	59.15	109.5	8669	-1193				
2	5-77	951	365.8	134014	59.15	109.5	8669	-1193				
2	5-77	955	383.8	134014	59.15	109.5	8669	-1193				

TABLE 10B



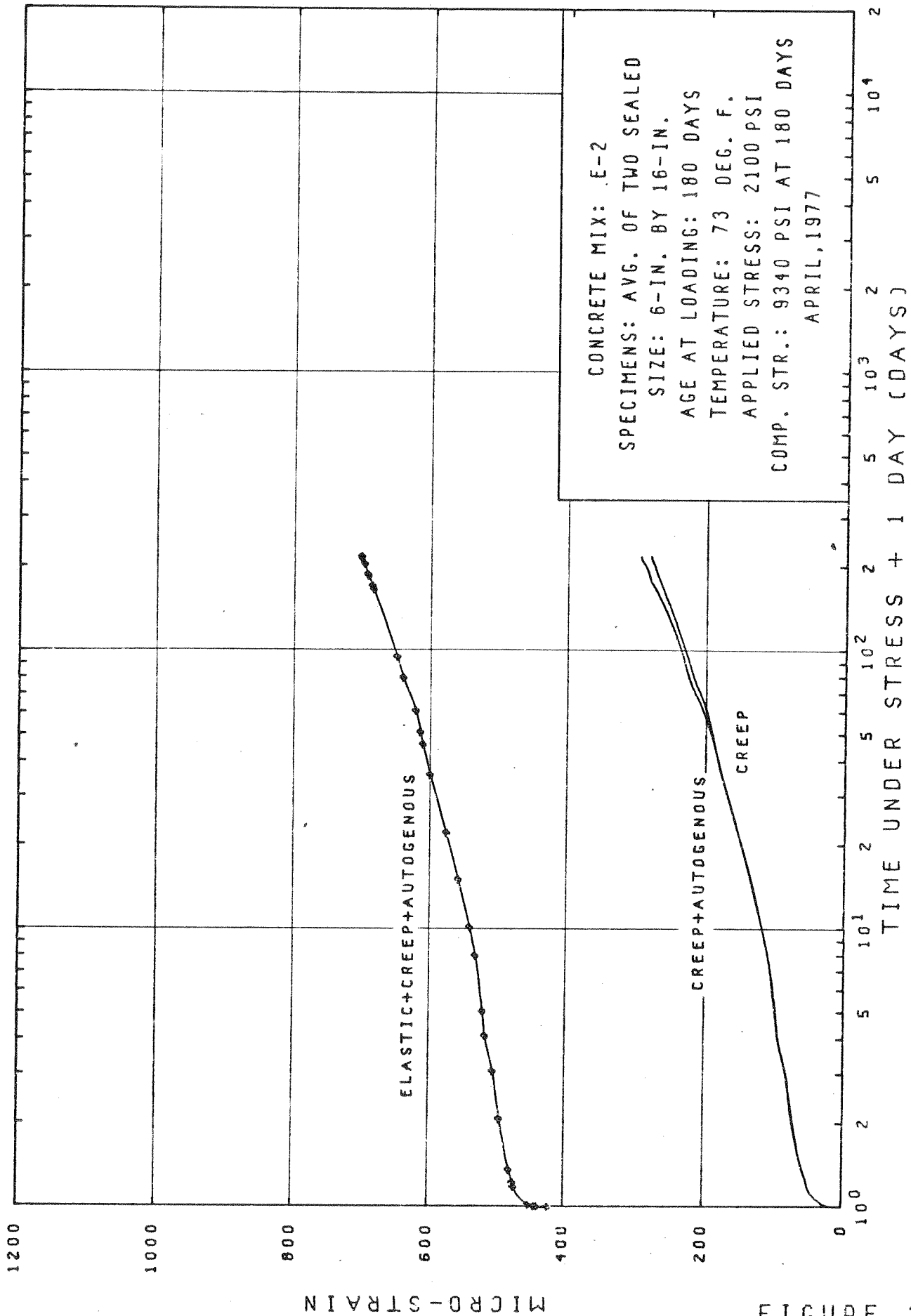
ELASTIC, CREEP AND AUTOGENOUS STRAINS
 WOLF CREEK POST TENSIONED REACTOR BUILDING

FIGURE 1



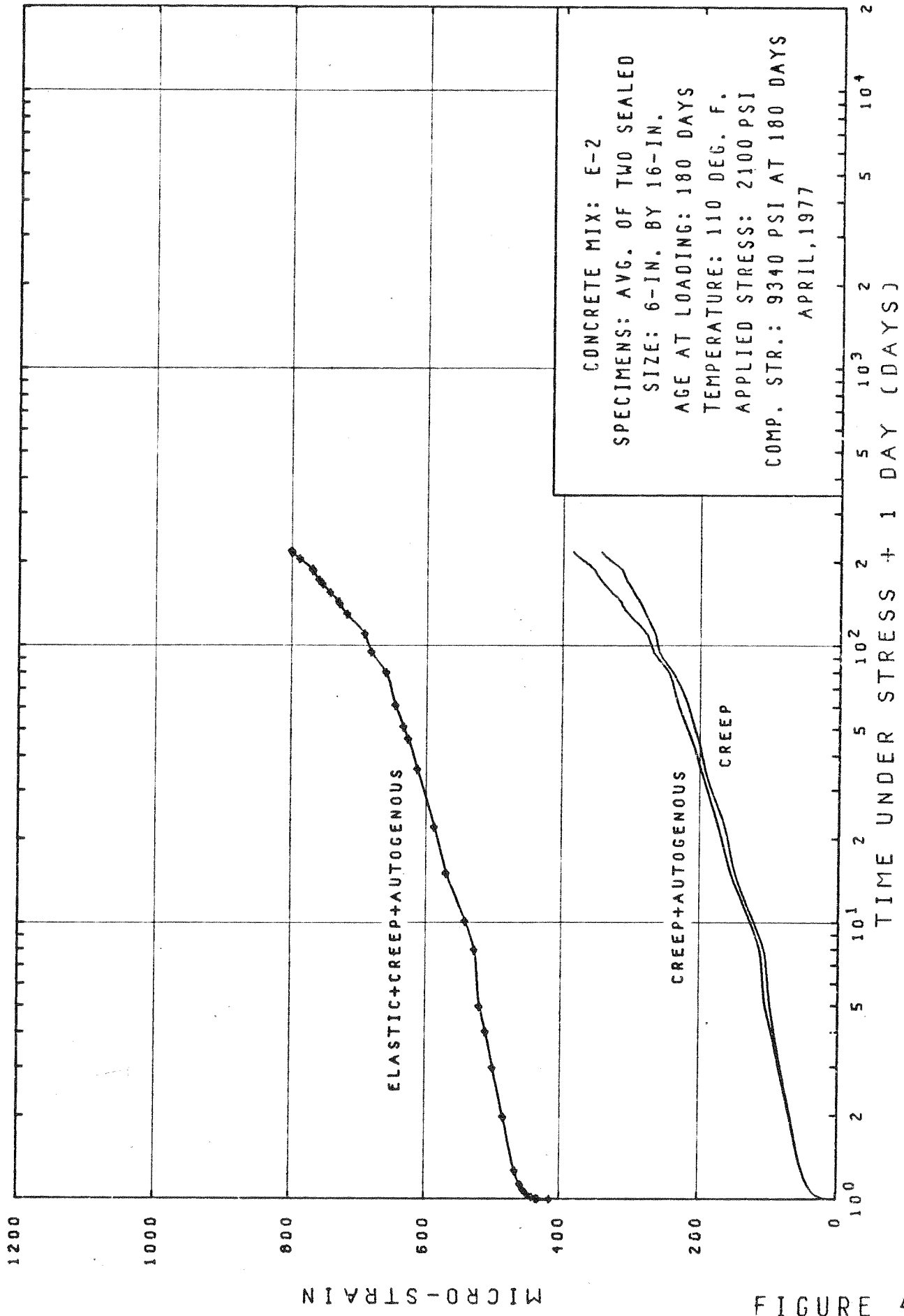
ELASTIC, CREEP AND AUTOGENOUS STRAINS
 WOLF CREEK POST TENSIONED REACTOR BUILDING

FIGURE 2



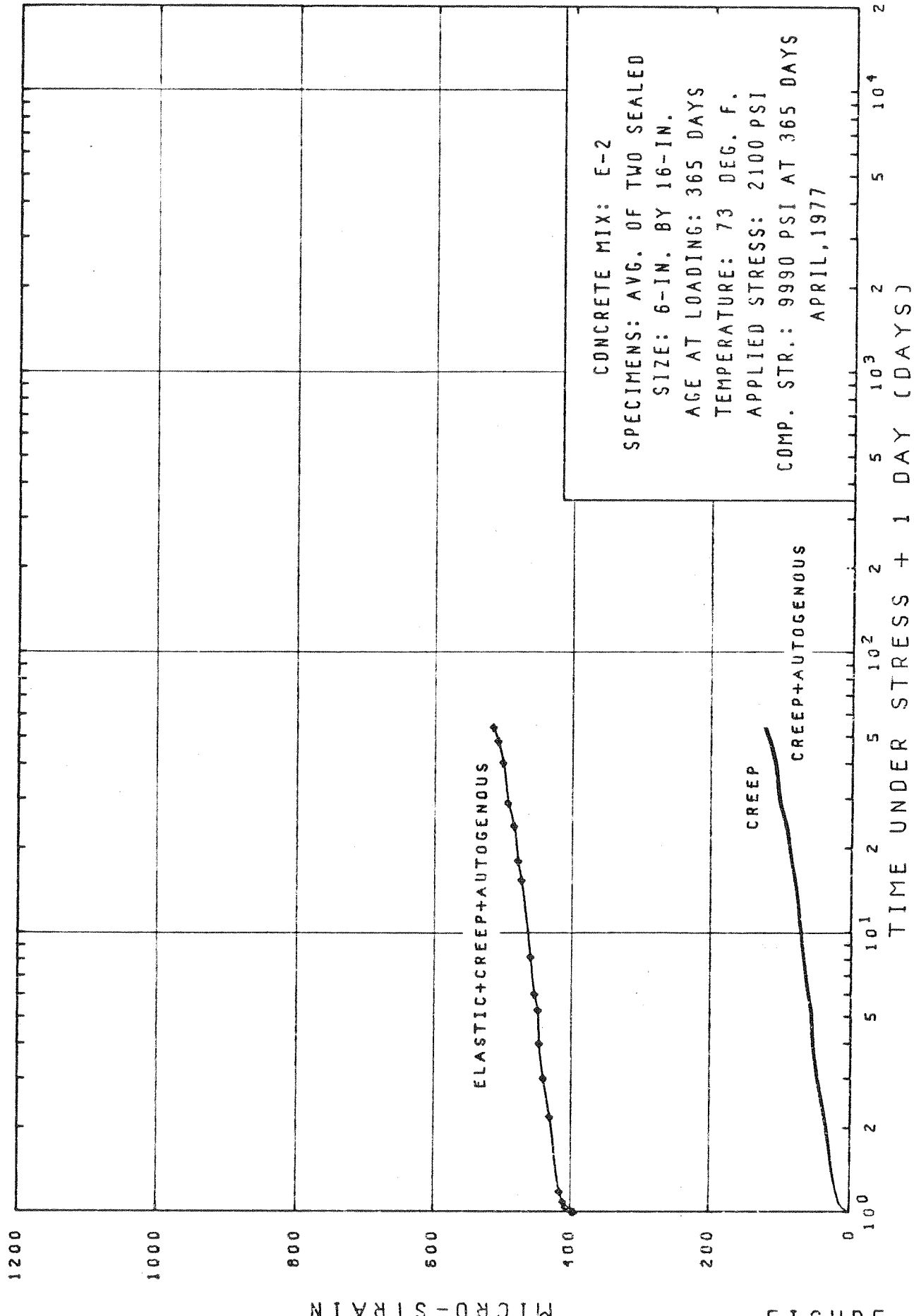
ELASTIC, CREEP AND AUTOGENOUS STRAINS
 WOLF CREEK POST TENSIONED REACTOR BUILDING

FIGURE 3



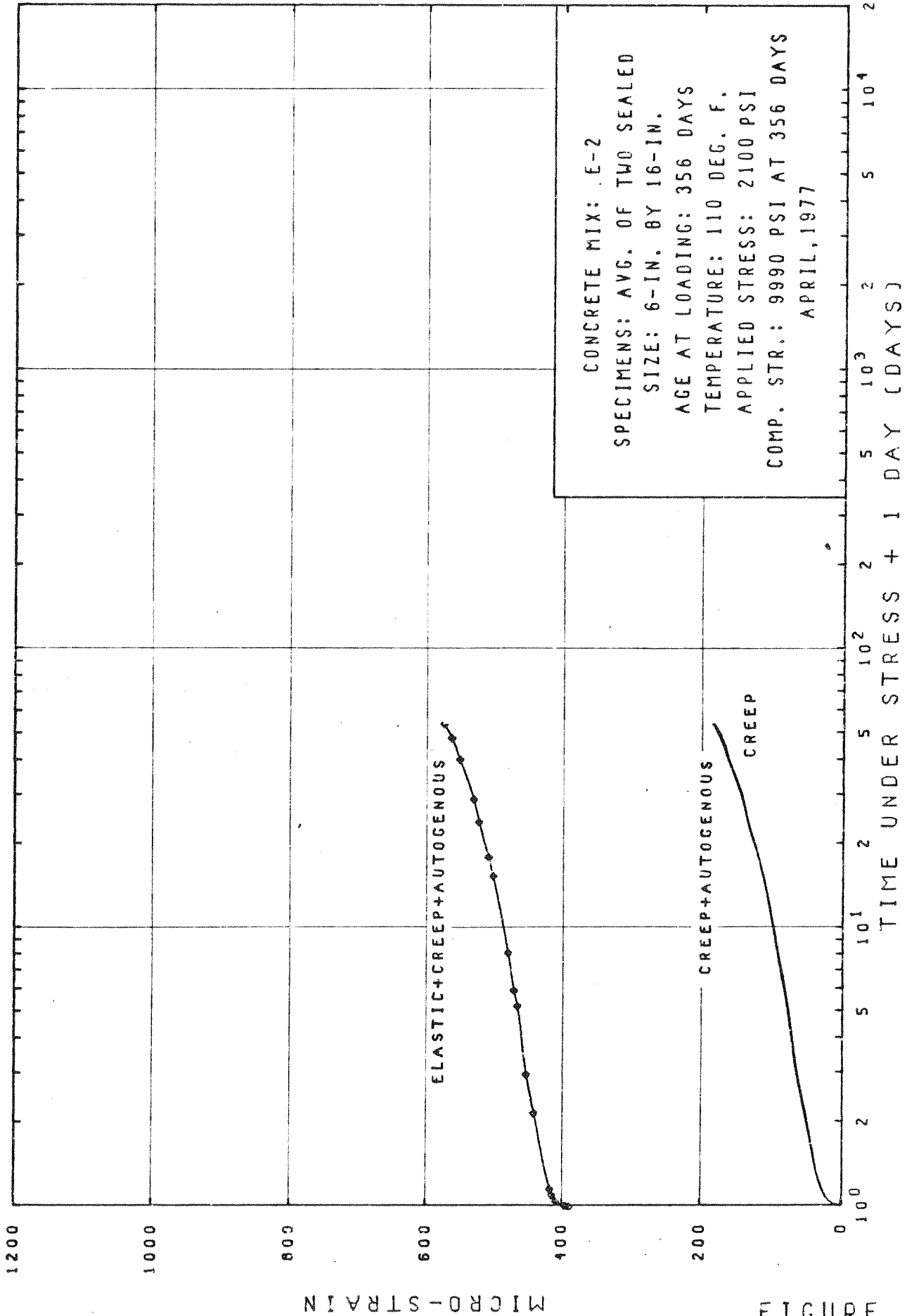
ELASTIC, CREEP AND AUTOGENOUS STRAINS
 WOLF CREEK POST TENSIONED REACTOR BUILDING

FIGURE 4



ELASTIC, CREEP AND AUTOGENOUS STRAINS
 WOLF CREEK POST TENSIONED REACTOR BUILDING

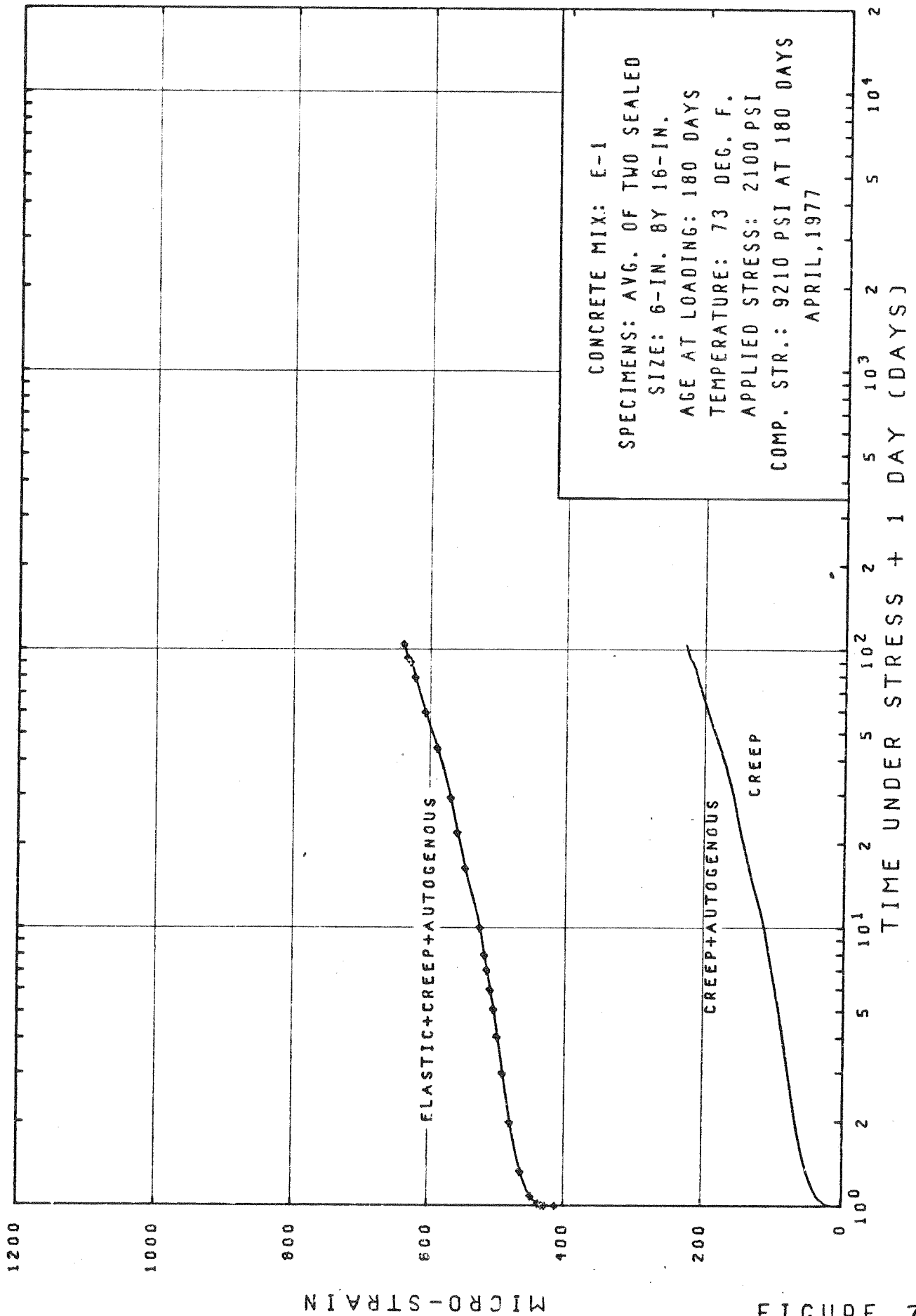
FIGURE 5



MICRO-STRAIN

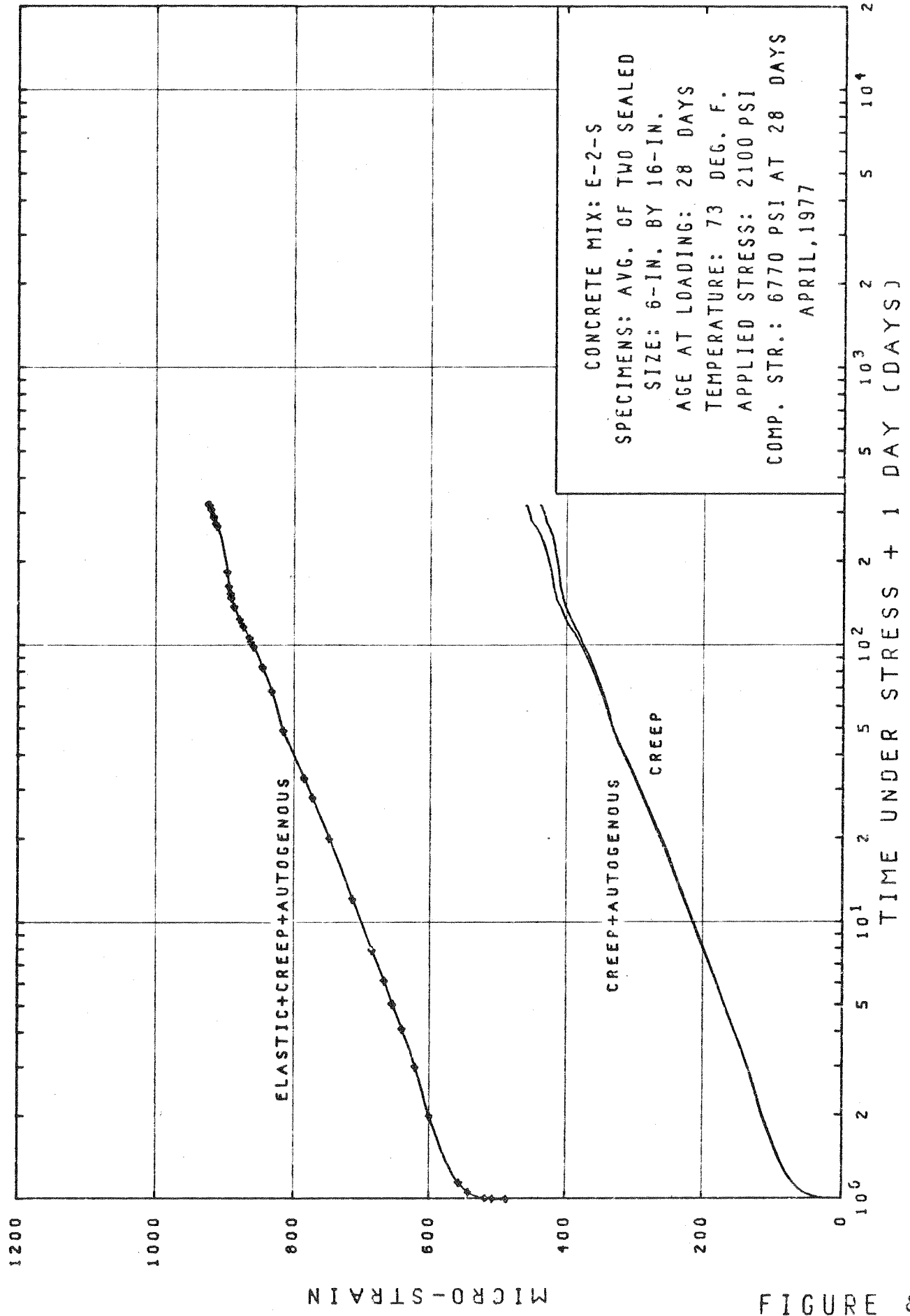
FIGURE 6

ELASTIC, CREEP AND AUTOGENOUS STRAINS
 WOLF CREEK POST TENSIONED REACTOR BUILDING



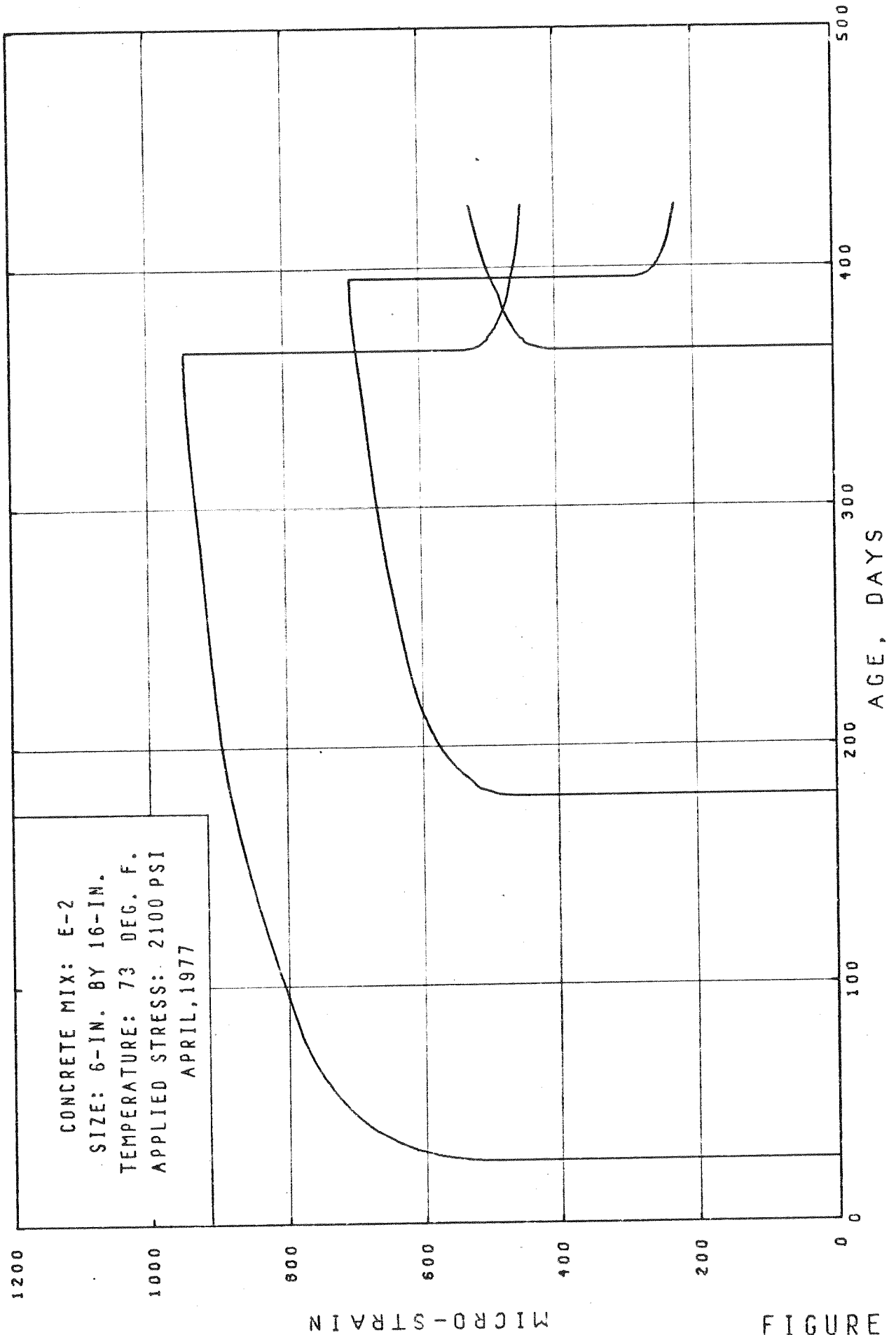
ELASTIC, CREEP AND AUTOGENOUS STRAINS
 WOLF CREEK POST TENSIONED REACTOR BUILDING

FIGURE 7



ELASTIC, CREEP AND AUTOGENOUS STRAINS
 WOLF CREEK POST TENSIONED REACTOR BUILDING

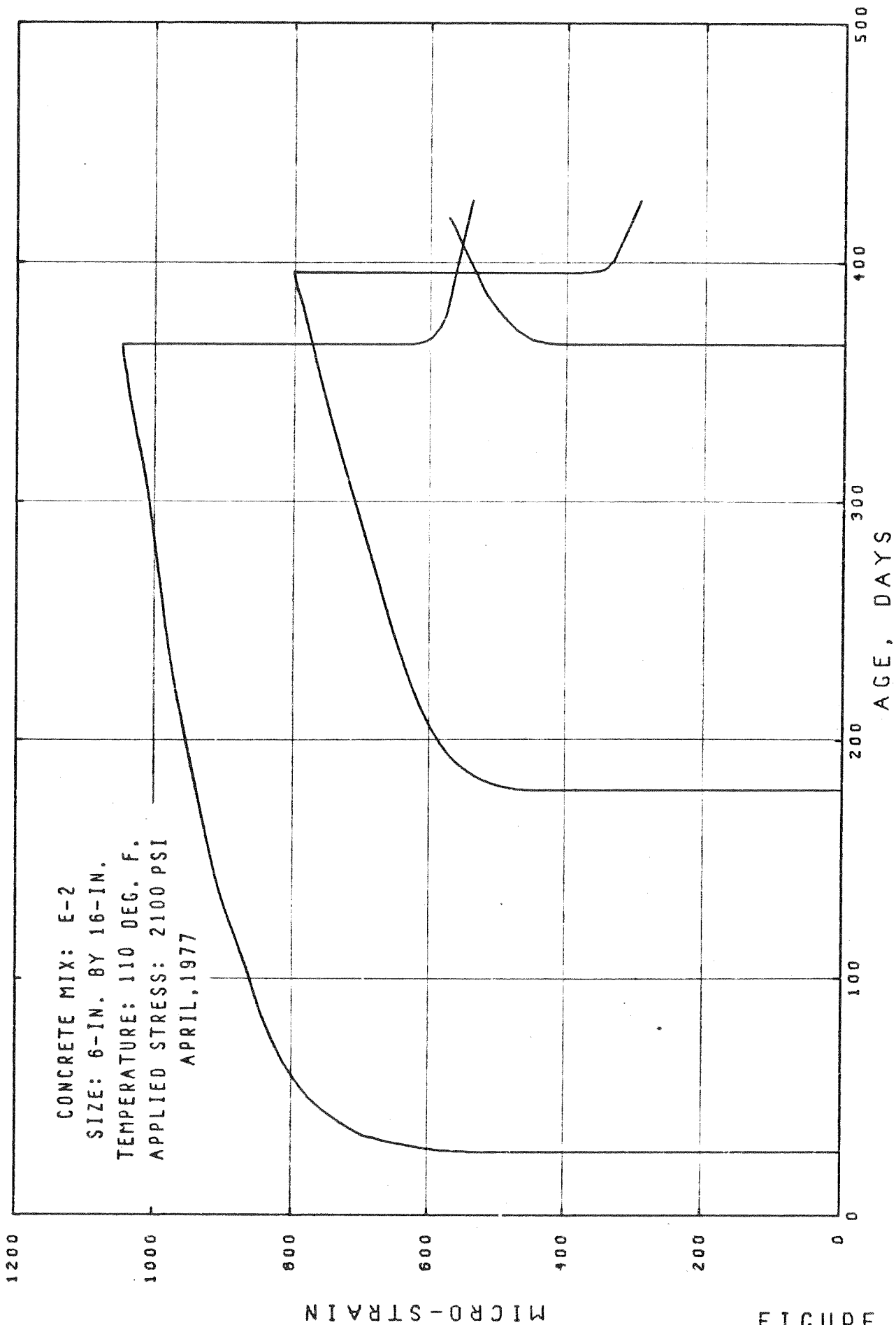
FIGURE 8



ELASTIC PLUS CREEP PLUS AUTOGENOUS STRAINS
 WOLF CREEK POST TENSIONED REACTOR BUILDING

MICRO-STRAIN

FIGURE 9



ELASTIC PLUS CREEP PLUS AUTOGENOUS STRAINS
 WOLF CREEK POST TENSIONED REACTOR BUILDING

FIGURE 10