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THE ULTRAVIOLET SPECTROSCOPY OF NITROUS OXIDE (N₂O): A TEMPERATURE-RESOLVED STUDY

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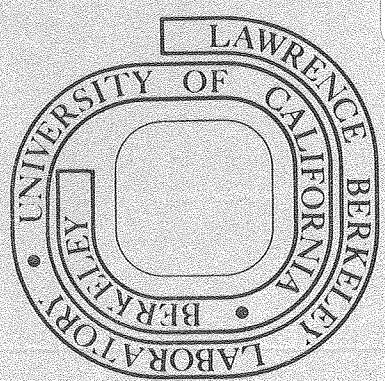
Gary Stewart Selwyn
(Ph. D. thesis)

March 1979

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THE ULTRAVIOLET SPECTROSCOPY OF NITROUS OXIDE (N_2O):
A TEMPERATURE-RESOLVED STUDY

by

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ABSTRACT

The absorption spectra of nitrous oxide and its ¹⁵N isotopes have been studied from 172 to 330 nm. The long wavelength absorption above 265 nm is shown to be almost entirely due to Rayleigh scattering, contrary to previous accounts. This correspondingly reduces the calculated rate of nitrous oxide photolysis in the troposphere to a very small value. The temperature dependence of the absorption from 173 to 240 nm has been measured for use in atmospheric modeling of the photolysis of nitrous oxide. At shorter wavelengths, previous investigators have noted the presence of very weak, diffuse banding of nitrous oxide superimposed on its continuous absorption. Spectra obtained in this study over the wavelength range 172 to 190 nm demonstrate that these diffuse bands are in fact a separate pronounced absorption of nitrous oxide which is strongly affected by temperature. This banding is the result of transitions to discrete vibronic levels in an upper electronic state. No rotational structure can be observed. From the temperature dependence of the observed structure it is shown that the transition results through vibronic coupling of the ν_2 bending mode. The energy spacing of the upper state is measured to be $\sim 480 \text{ cm}^{-1}$ and this with the available knowledge of the vibrational frequencies of the ground state, permits a partial assignment of the

spectrum. Using the large temperature effect observed, the spectra are deconvoluted into the individual absorption spectra of the (000) and (010) vibrational modes of the ground electronic state. This deconvolution reveals a (000) state absorption spectrum which is weakly structured on top of a continuum and a (010) state absorption spectrum which is strongly structured on top of an enhanced continuum. Using this deconvolution it is then shown that the pronounced structure at higher temperatures is primarily due to the presence of vibrationally "hot" molecules. Substitution of isotopically labeled nitrous oxide indicates a unique isotope shift for these vibronic features which increases in the order: $\text{NNO} - \text{N}^{15}\text{NO} - {}^{15}\text{NNO} - {}^{15}\text{N}^{15}\text{NO}$. The extent of the observed isotope shift is greatest at short wavelengths and has been observed to be as large as 130 cm^{-1} . Using the results of published theoretical studies of N_2O , it is deduced that the structure results from the transition ${}^1\Sigma^- \leftarrow X{}^1\Sigma^+$ while the continuous absorption results from the transition ${}^1\Delta \leftarrow X{}^1\Sigma^+$. Both of these are normally forbidden transitions but are allowed by bending. It is further proposed that in the bent equilibrium geometry, an avoided crossing results from the perturbation of the ${}^1A''$ components of ${}^1\Sigma^-$ and ${}^1\Delta$ in C_s symmetry. Evidence for this bent configuration of ${}^1\Sigma^-$ is offered and a mechanism of predissociation is proposed. Finally an anomalous result is briefly discussed. In one sample of isotopic nitrous oxide an extremely strong, sharp absorption ($\text{FWHM} = 0.2\text{\AA}$) is observed which is presumably due to an impurity. By IR, UV and mass spectrometry it was not possible to assign this absorption to any likely molecular or atomic species.

I. INTRODUCTION

This work covers two aspects of study on nitrous oxide: its role in atmospheric photochemistry and the basic ultraviolet spectroscopy of nitrous oxide which partially determines this photochemistry. This work began as a short study to evaluate the rate of tropospheric photolysis of nitrous oxide, but in the initial stages of this study inconsistencies in the near ultraviolet absorption spectrum of nitrous oxide became apparent. In the course of checking these inconsistencies other inconsistencies were noted between the literature and the new experimental evidence presented in this study. Eventually, a different absorption spectrum resulted along with a different theoretical interpretation of the ultraviolet absorption processes of nitrous oxide. The explanation of this absorption process offered here is consistent with all experimental evidence on nitrous oxide to date.

This section, I, covers the background of the two areas of study covered in this work. Sections II and III deal with the atmospheric photolysis of nitrous oxide and Section IV covers the basic spectroscopy of nitrous oxide.

A. History of Spectroscopic Studies of Nitrous Oxide in the Near and Middle Ultraviolet

Leifson¹ in 1926, was the first to study the ultraviolet absorption of nitrous oxide and reported a continuous absorption, from 200 to 168 nm, and a stronger continuum from 155 nm to shorter wavelengths. Dutta² in 1932, showed that the first absorption of nitrous oxide actually extended weakly to 275 nm and was unable to trace any banded absorption between 210 and 275 nm. In a broad range study of the nitrous oxide absorption spectrum from 220 to 85 nm, Duncan⁴ discovered

discrete structure near 155 nm with a vibrational spacing of 621 cm^{-1} but found only continuous absorption elsewhere.

NO was detected as a product of UV photolysis by Wulf and Melvin³ and Sen-Gupta⁵. Henry⁶ noted these findings and tried to associate them to dissociation products of N_2O .

In an effort to find the long wavelength limit of the dissociation of nitrous oxide, Sporer and Bonner⁷ in 1940 used a steel pipe 105 feet long as an absorption cell and filled it with nitrous oxide at pressures up to five atmospheres. At this pressure, the absorption extended weakly up to limit of observation, 306 nm, with two extremely weak continua noted above 275 nm.

In that same year, a study by Nicolle and Vodar⁸ reported on the difference in the absorption spectrum at 293 K and 183 K and found that at the lower temperature the absorption is uniformly decreased over the wavelength range studied, 215 to 235 nm.

Romand and Mayence⁹ in 1949, also noted banding in the second absorption at 145 nm, and reported a purely continuous absorption in the region about 184 nm. A more detailed study, using photomultipliers and with higher resolution, by Zelikoff, Watanabe and Inn¹⁰ in 1953, studied the absorption of N_2O from 210 nm to the LiF cutoff at 108 nm. Above 138 nm they found strong vibrational structure in the second absorption centered about 145 nm, as did Romand and Mayence, but unlike the previous studies, they noted very weak, diffuse bulges on the continuum centered at 180 nm. Because of the weak nature of these bulges, they could not be measured accurately or further analyzed. These bulges are a major concern of this work and are discussed in

Section IV. Extending to longer wavelengths than the Zelikoff, Watanabe and Inn study, the results of Thompson, Hartreck and Reeves¹¹ (1963) agreed quantitatively with Zelikoff and workers but found only a continuous absorption with no superimposed features between 150 and 239 nm.

In a study primarily concerning the atmospheric role of nitrous oxide, Bates and Hays¹² (1967) presented the N₂O absorption spectrum from 170 to 320 nm based upon unpublished sources. Their spectrum shows a second absorption above 260 nm. More will be said about this in Section II.

Studying the temperature dependence of the near UV absorption of nitrous oxide between 293 and 953 K, Holliday and Reuben¹³ reported in 1968 a very large temperature effect, primarily affecting the longer wavelengths although increasing temperature strengthened the absorption over the entire continuum above 200 nm. More will be said of this temperature dependence in Sections III and IV.

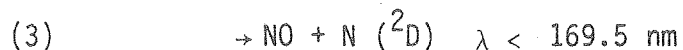
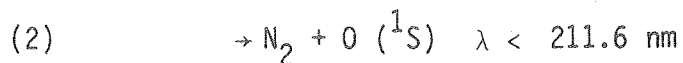
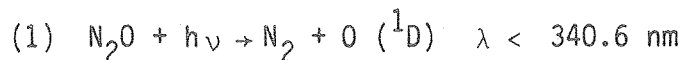
A comprehensive review article on the electronic spectroscopy of nitrous oxide and other molecules isoelectronic with it by Rabalais and coworkers¹⁴ presented new spectra of N₂O from 110 to 215 nm. Their spectrum of the first absorption of N₂O showed only a purely continuous absorption although they refer to the weak absorption bulges of Zelikoff et al. They also presented a review of the theoretical basis of this absorption of nitrous oxide and its related isoelectronic molecules.

Most recently, Monahan and Walker¹⁵ in 1975 compared the absorption of gaseous N₂O at 298 K with the absorption of a thin solid film of N₂O at 53 K. In the gas phase at 180 nm they also observed the very

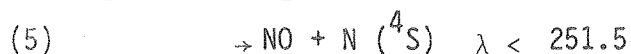
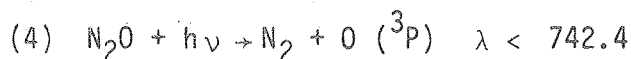
weak, diffuse bands superimposed on the continuous absorption, but like the Zelikoff study, were unable to analyze them or observe any detailed structuring.

B. Photochemical Processes of Nitrous Oxide

The following products of photolysis of N_2O are energetically possible in the near ultraviolet:

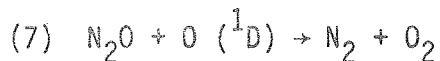
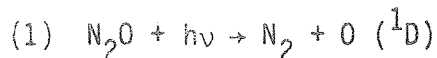


along with the spin-forbidden product of photolysis:



Originally, the NO produced in the early photochemical decomposition studies of N_2O in the near UV was thought to result from the direct photolysis into $NO + N$. Studies by Doering and Mahan¹⁶ indicated that channel (5) occurred in about 20% of the products, however more definitive studies have since indicated that production of $O(^1D)$ through (1) is the primary one reached.¹⁷⁻²¹

NO is produced indirectly through the reaction sequence for the photolysis of pure nitrous oxide:



Davidson²² has found that the rate constants for (7) and (8) can be fit by the equation:

$$(9) \quad \frac{k_7}{k_8} = (0.72 \pm 0.11) + \frac{21.6 \pm 7.0}{T}$$

$$170 < T < 434 \text{ K}$$

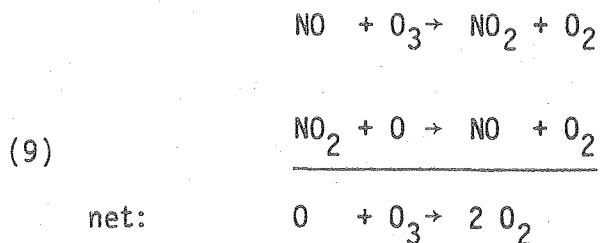
with other products constituting less than 4 per cent of the total yield.

C. Atmospheric Nitrous Oxide

Since nitrous oxide was discovered as a trace gas in the atmosphere by Adel²³ in 1938, its atmospheric concentration has been measured by ground based means²³⁻²⁹, and with air-borne methods to measure the variation in concentration with altitude^{30-35,41}. Current estimates indicate a concentration of about 0.32 ppmv in the troposphere³⁸⁻⁴⁰.

Atmospheric nitrous oxide is produced by bacterial action on nitrogenous compounds during the nitrogen cycle³⁶⁻³⁷, although a small contribution from combustion^{42,43} has also been proposed. The role of the ocean as a source or sink for nitrous oxide has also been debated⁴⁹⁻⁵², and fresh water bodies have also been proposed as a source of N₂O⁴⁴⁻⁴⁸.

While unreactive with atmospheric molecules in the lower atmosphere, in the stratosphere nitrous oxide is destroyed by photolysis, (1) or may react with O (¹D) through (7) and (8). The NO produced by (8) then influences stratospheric ozone⁵³⁻⁵⁵ by the NO_x catalytic oxidation cycle:



Recognizing that increased man-made fertilizer production may ultimately increase stratospheric nitrous oxide, Crutzen in 1974 estimated

a four percent decrease in stratospheric ozone resulting from a twenty percent increase in atmospheric N_2O concentration.⁵⁶

Estimates by other workers have since proposed both larger and smaller effects on stratospheric ozone.^{48,51,52,57-61} Complicating the situation further is evidence that bacterial action may also provide an additional significant sink for N_2O ⁶² and the possibility has also been raised that non-homogeneous chemistry may be important.⁶³

Free radicals other than NO_x vitally affect stratospheric ozone, such as ClO_x and HO_x .^{64,65} The degree and nature of the interactions between the NO_x , HO_x and ClO_x families of reactions are currently under investigation and thus it is difficult at this time to predict the effect of increasing N_2O on stratospheric ozone.

II. Long Wavelength Absorption of Nitrous Oxide⁶⁷

A. Introduction

1. The Bates and Hays Model

In an early review of atmospheric nitrous oxide, Bates and Hays¹² presented the photodissociation cross sections of nitrous oxide from 170 to 320 nm. They reported a moderately strong absorption with a maximum at about 180 nm, and a weak absorption at longer wavelengths with maxima at 280 and 295 nm. This weak absorption extended slightly beyond 320 nm, which is above the ozone cut-off of sunlight, and so this portion of the spectrum leads to a slow but significant rate of photolysis of nitrous oxide in the troposphere. On the basis of the observed mixing ratio of troposphere N₂O, the indicated absorption cross sections for dissociation, and an estimated constant vertical exchange coefficient (K_z) of $10^5 \text{ cm}^{-1} \text{ sec}^{-1}$ in the stratosphere. Bates and Hays¹² calculated the flux of nitrous oxide necessary to maintain the troposphere concentration and corresponding 70 year average atmospheric residence time. The error in this type of calculation is large, but should provide an approximate result ($\sim \pm 50\%$).

2. Experimental Indications

At the time of this experiment (1975), there were two arguments that pointed to the belief that the atmosphere residence time was much less than 70 years: (1) Schutz et al.⁶⁶ studied the seasonal, geographical and vertical variations in atmospheric nitrous oxide over a two year period and concluded on the basis of their experimental measurements that nitrous oxide is destroyed much faster than by the rate of photolysis as given by Bates and Hays¹²; (2) Junge and Hahn⁶⁸

and Hahn⁴⁹ estimated the source of nitrous oxide from bacterial reduction of nitrates and nitrites in the ocean and from soils; although there is a substantial uncertainty in extrapolating those observations to the entire globe, the results strongly implied a source strength such that the atmospheric residence time is about 12 years. Comparing this short residence with the calculated lifetime of 70 years based on the Bates and Hayes model of photolysis in the atmosphere, Junge and coworkers thus argued that there was a large unknown process that removes or destroys N_2O in the troposphere. By stretching every uncertainty to its utmost limit in the direction of minimizing the source's strength of nitrous oxide (i.e. increasing its residence time), it could be argued that such maximum "experimental" lifetimes might be balanced by the photolysis of nitrous oxide using the Bates and Hays cross sections in their model.

The purpose of this experiment was to study the near ultraviolet absorption of nitrous oxide at wavelengths above 260 nm in more depth, so that atmospheric models may more accurately assess the photolysis rate of atmospheric nitrous oxide. The results of this study indicate that this weak absorption does not exist, and so in its absence the rate of photolysis of tropospheric nitrous oxide is negligibly small and thus its atmospheric lifetime based upon photolysis and chemical reaction must be increased more than the 70 years postulated by Bates and Hays.

As stated in Section I, evidence compiled after the completion of this experimental section indicates that other processes, possibly

bacteriological in nature, may play an important role in the destruction rates of atmospheric nitrous oxide. This does not preclude the findings offered here of a large discrepancy between the chemical and photochemical rates of nitrous oxide destruction and the necessary rate to maintain steady state concentration, but instead these non-homogeneous mechanisms may help explain the difference.

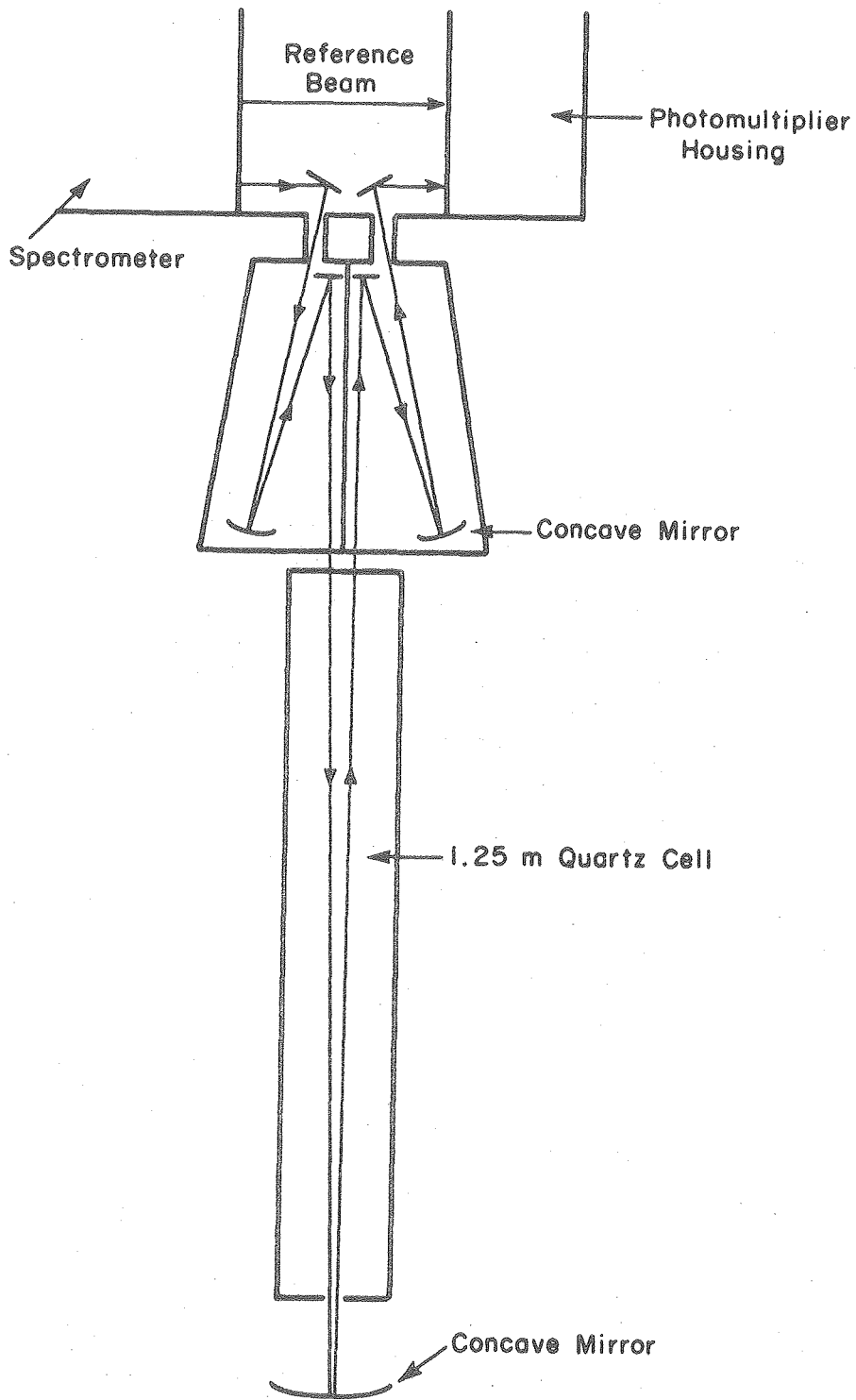
B. Experimental

1. The Cary 118C Spectrometer

The Cary 118C spectrometer is manufactured by Varian Associates and the model purchased is equipped with a photomultiplier suitable for use down to 165 nm. It has a double prism monochromator which provides greatest resolution at short wavelengths. A deuterium discharge lamp provides a continuous light supply free from strong emission lines from 480 to 160 nm. A tungsten lamp is also provided for wavelengths greater than 350 nm. The instrument may be operated in the single or double beam mode and provisions are made for purging all light paths. Since the light is dispersed by the monochromator before passage through the sample compartment, photolysis due to the beam is not usually a problem.

2. Optics and the Quartz Cell

The spectra taken in this section used an existing optical system and quartz cell built by my predecessors. The optical system, shown in figure 1, consisted of a plane mirror located within the Cary sample compartment which reflected the beam out through a tube into a double sided trapezoidal mirror housing. In the housing the beam was collected by a three inch concave mirror opposite the Cary and after reflection by a second plane mirror, was sent down the long cell passing through the two suprasil windows of the quartz cell. Beyond the cell, on an optical rail a large concave mirror collected the beam and reflected it back for a nearly identical return trip. Focal lengths of the concave mirrors and their placement were chosen so that the beam was focused at the end mirror.



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Figure 1

Only a very small percentage of the transmitted light was lost due to overfilling of mirrors or windows; typically the optical arrangement passed 15% of the light at 300 nm with the loss primarily due to inefficiency of the mirrors at each of the seven reflections. To minimize photometric errors arising from a "short-trip" of scattered light in the entrance section being picked up by the mirrors in the exit section, the mirror housing was painted black and the two sections were divided with a partition. This was checked by blocking the beam at any point past the housing; the transmitted light indicated was less than 0.02%.

The cell was constructed entirely of fused silica and had two fused suprasil windows (1/4" thick). With the double pass optics, a path length of 252 cm resulted. For all experiments it was necessary to blacken the length of the cell and darken the room to avoid light leakage into the spectrometer.

Initial experiments indicated that with the evacuated cell, the beam would be totally absorbed at wavelengths less than 260 nm. Upon tracing the beam path, I soon discovered that one front surface plane mirror had been mounted backwards by my predecessors so that the beam would pass through the pyrex backing before reflecting off the mirror thus resulting in total absorption at the shorter wavelengths. The problem was easily remedied and with proper alignment it was possible to work down to 205 nm with 1% of the transmitted light.

3. Procedures

In all experiments of this section, the spectrometer was used in the double beam mode with the reference path containing an unmodified 15 cm of air in the sample compartment. Due to distortions in

the cell when it was evacuated, there was a small systematic decrease in absorption when the evacuated cell was filled with helium or nitrogen. For this reason, the cell was filled with helium or nitrogen as a reference for N_2O , rather than the evacuated cell. This equal pressure background spectrum was repeated before and after each experiment and was subtracted from the observed spectra obtained with nitrous oxide. Reversing the procedure and measuring the nitrous oxide first and last and the reference spectrum second was occasionally tested and yielded identical results.

Since the object of this study was to measure extremely small absorptions, instrumental drift was an important factor. For this reason, three or four runs over the wavelength interval were repeated for both the reference and sample spectra to test for reproducibility. If a small variation was noted, more runs were repeated until reliability was insured. Occasionally a larger drift was found, and the entire measurement was discarded. The procedure reference-nitrous oxide-reference also served to check on instrumental drift.

Noise was another limiting problem. The most that could be done to improve signal/noise was using larger time constants and slower scan speeds. Most experimentation was done at night when the house current was cleaner. Especially bad results were had at 1-2 PM, 5 PM and 11 PM, the latter probably caused by switching of the compressors at Gaique Laboratory. During this time the Cary also suffered from an intermittent noise problem which was later traced to a faulty carbon resistor in the photomultiplier socket. A 15 amp Sorenson voltage regulator was used to drive the Cary when it was found that the house

current varied over the range 112 to 122 volts, a larger variation than was recommended for the Cary by the manufacturer.

4. Data Collection

Data for this section were collected on chart paper. At maximum sensitivity, the Cary gives a full scale chart reading for absorbance ($\log_{10} I_0/I$) of 0.02. Under the experimental conditions, the vibration and irreproducibility of the baseline was about 3 percent of full scale at this setting, limiting the sensitivity to about $2 \times 10^{-25} \text{ cm}^2$ for N_2O cross sections. Reproducibility from one day to the next was substantially less than this, indicating "low frequency" errors associated with the total method. At the longer wavelengths, the results sometimes indicated a negative absorption relative to the reference. These were calculated as negative cross sections and plotted with the other data to show the scatter of experimental data.

The nitrous oxide used was purified by vacuum distillation for some runs. In an effort to identify the impurity responsible for the long wavelength peak reported by Bates and Hays, we also used unpurified N_2O from the commercial cylinder (Matheson). No difference could be detected in the spectra between the purified and unpurified gas, and then most measurements (especially the long wavelength ones) were carried out with unpurified tank nitrous oxide. Most experiments were done at one atmosphere pressure and so the cell and vacuum lines were filled slightly over atmospheric pressure, then the line and cell were vented to the air and the atmospheric pressure was read off a mercury barometer in the next room. For measurements at less

than 1 atmosphere, a Wallace and Tierman dial pressure gauge was used to measure pressure, which was later calibrated against a Baracel electronic manometer. The resolution was about 1 nm and a scan speed of 0.2 and 0.05 nm sec⁻¹ was used with 1 or 5 second time constant.

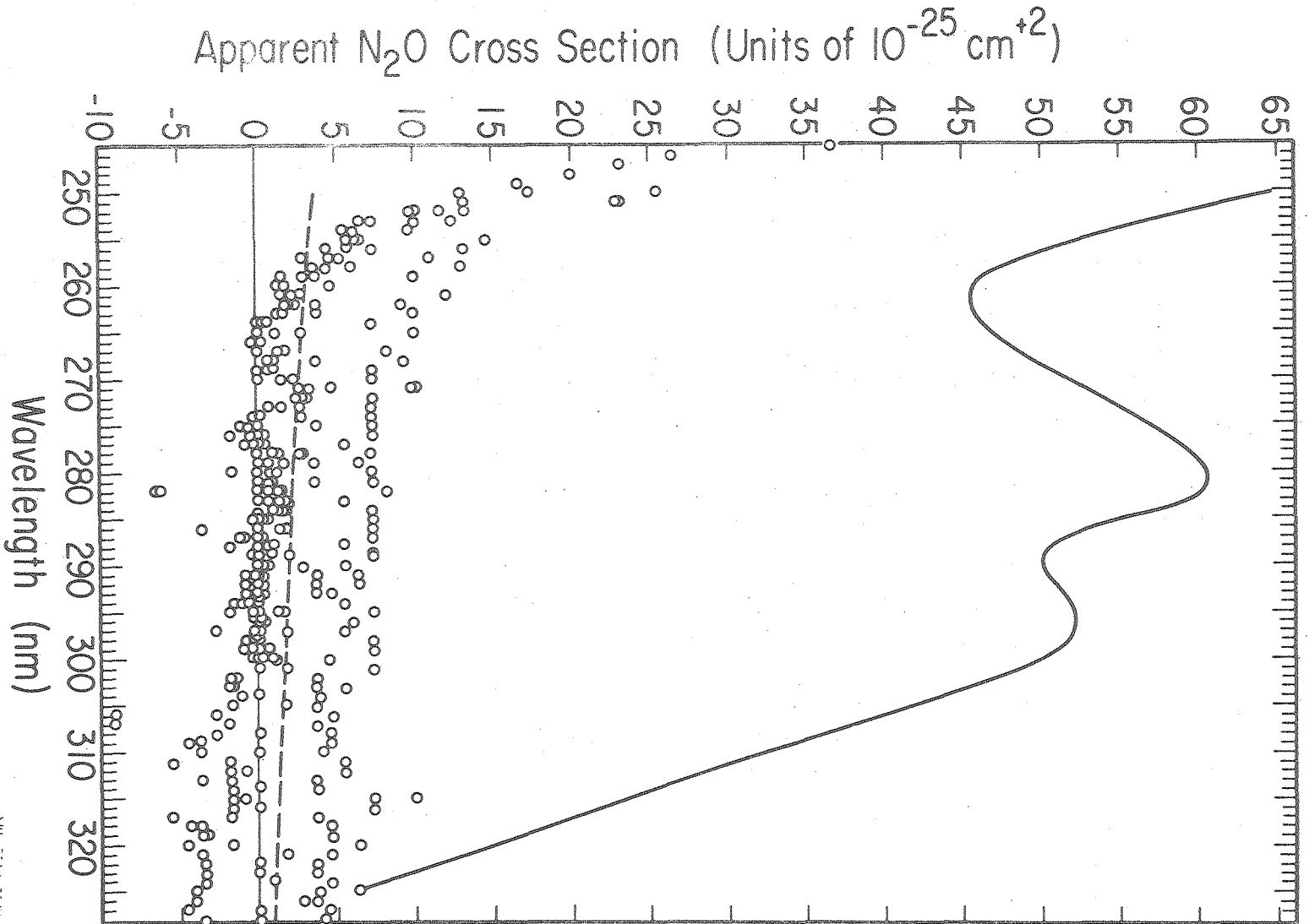
C. Results

1. Absorption Cross Sections, 240-330 nm

The apparent, observed N_2O cross sections ($\log_e I_0/I = \sigma NL$, cm^2 molecule⁻¹ where N is the number density and L is the path length in cm) are given in figure 2 for the wavelength range 245 to 328 nm at temperature $294 \pm 2K$. The solid curve represents the N_2O cross sections read from the first figure in the article by Bates and Hays. It can be seen that the wavelength cross sections reported by Bates and Hays are much higher than the results obtained here and are 10 times greater than the range of experimental error of these measurements. The dashed line of figure 2 is an estimate of the Rayleigh scattering cross section for nitrous oxide; the observed values for air (Leighton,⁶⁹ Forsythe⁷⁰) were scaled by the index of refraction function $(n-1)^2$ for air and N_2O . The results scatter more or less equally about the Rayleigh scattering line above 270 nm, and thus they indicate no significant absorption by nitrous oxide at room temperature in the troposphere.

Bates and Hays gave two references to the entire absorption spectrum reported, 170 to 320 nm. The references are not broken down with respect to wavelength and it is not stated whether these references were reviews of the literature or new data. One reference is to an unpublished British doctoral thesis and the other to a private communication. Because of this, the experimental basis for the long wavelength absorption is not clear. I have written to Bates and the stated addresses of the references and no further details could be obtained.

Using a 33 m stainless steel cell filled with 5 atmospheres of nitrous oxide, Spomer and Bonner⁷ did report a long wavelength absorp-



AM 7510-7579

Figure 2

Table 1. Long Wavelength Absorption of N₂O

| Wavelength, nm | Cross Section x 10 ²⁴ cm ⁻² |
|----------------|---|
| 330 | 0.1 ± .3 |
| 320 | 0.2 ± .3 |
| 310 | 0.2 ± .3 |
| 300 | 0.3 ± .3 |
| 290 | 0.4 ± .3 |
| 280 | 0.4 ± .3 |
| 270 | 0.5 ± .3 |
| 265 | 0.6 ± .3 |
| 260 | 0.7 ± .3 |
| 255 | 1.0 ± .3 |
| 250 | 1.9 ± .4 |
| 245 | 3.7 ± .4 |
| 240 | 9.6 ± .4 |

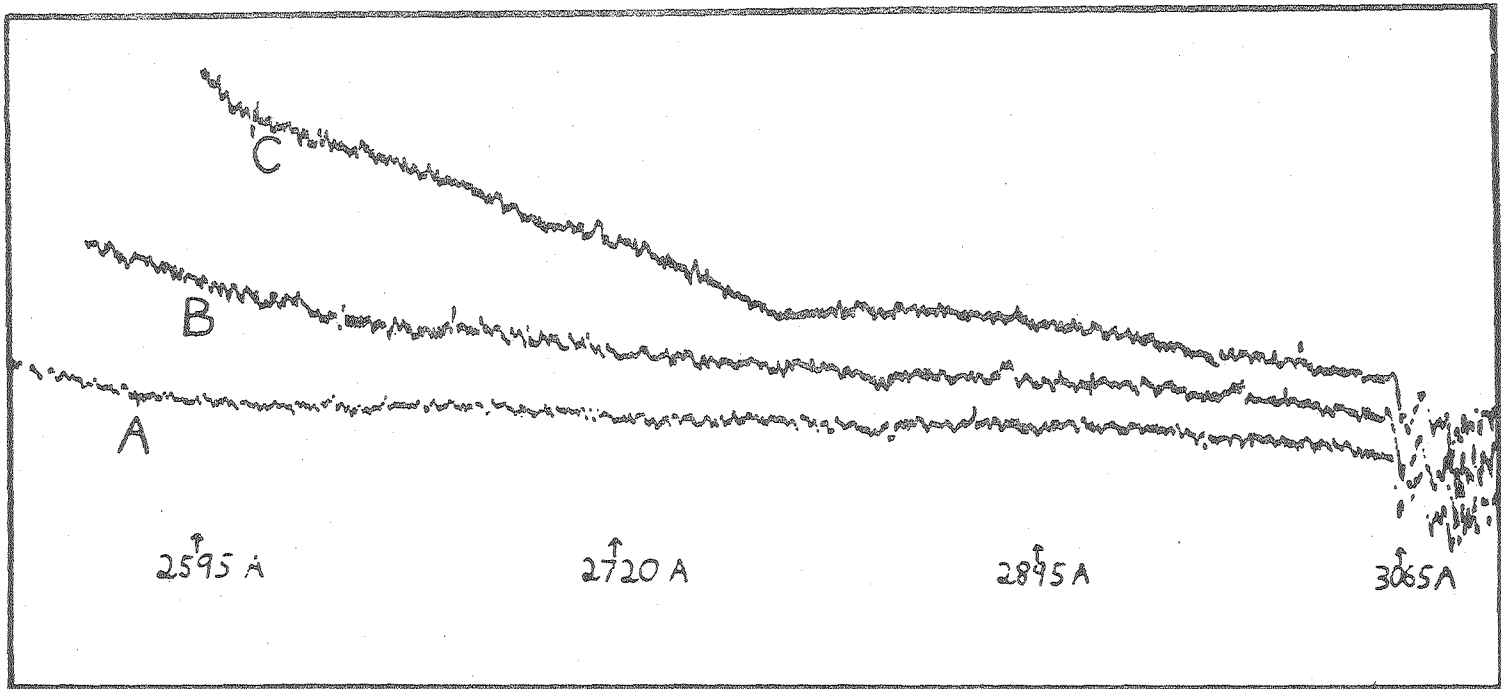
tion extending to 306 nm, but they used unpurified gas and stated that impurities could be the source of this absorption. Their findings, reproduced in figure 3, shows a microphotometer tracing of the absorption. The long wavelength absorbance of 5 atmospheres of N_2O , trace C, is clearly observed, but at 1.5 atmospheres, trace B, a proportional absorbance is not apparent relative to the vacuum trace A. The long wavelength absorption may also be due to the absorption of a dimer of nitrous oxide. This would exhibit a P^2 pressure dependence, possibly explaining the observation above. The nitrous oxide dimer produced in supersonic expansion has been observed,⁷¹ but its ultraviolet spectrum has not been studied.

Interestingly enough, for CO_2 a similar weak absorption at wavelengths longer than its first absorption feature at 147 nm, was noted⁷² only later to be proven incorrect.⁷³ At longer wavelengths the absorption approaches Rayleigh scattering, as was determined using a 250 m path length at one atmosphere pressure.⁷³

With purified nitrous oxide and pressures less than one atmosphere, the cross sections of N_2O are in reasonably good agreement with those reported by Bates and Hays below 230 nm as shown in figure 4. These results show that there is no major discrepancy with respect to the absorption of nitrous oxide between 235-210 nm.

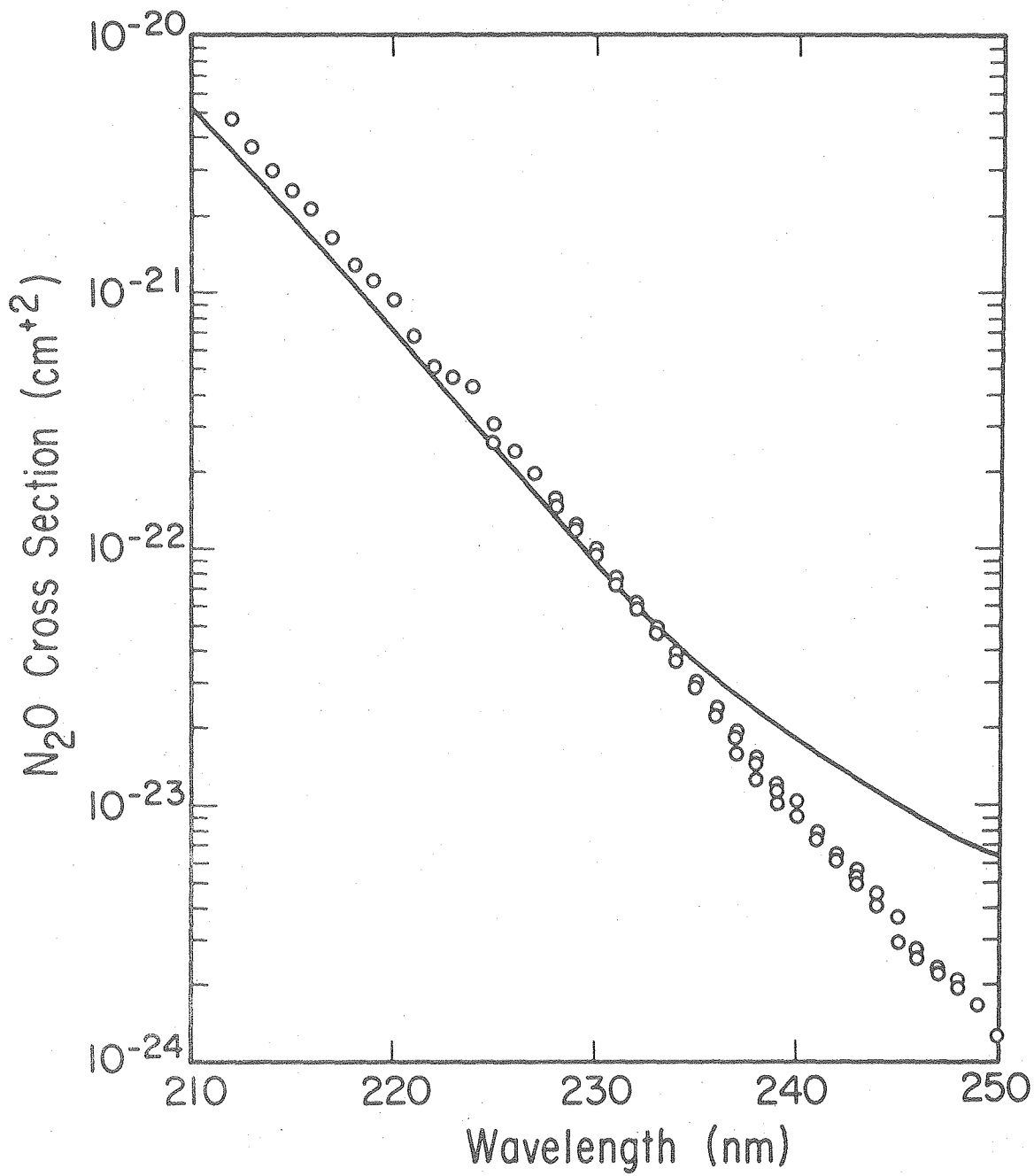
2. Atmospheric Implications

To estimate the atmospheric photochemical implications of these new cross sections of the near ultraviolet absorption of nitrous oxide, the program JVALVES was used. The program, developed by Whitten and Johnston, calculates the photolytic rate constant, j , using the same



XBL 7510-7530

Figure 3



XBL 7510-7528

Figure 4

relationship⁷⁴

$$j = \sum_i \sigma_i(\lambda_i) I(y, z, \lambda_i) \phi(\nu_i)$$

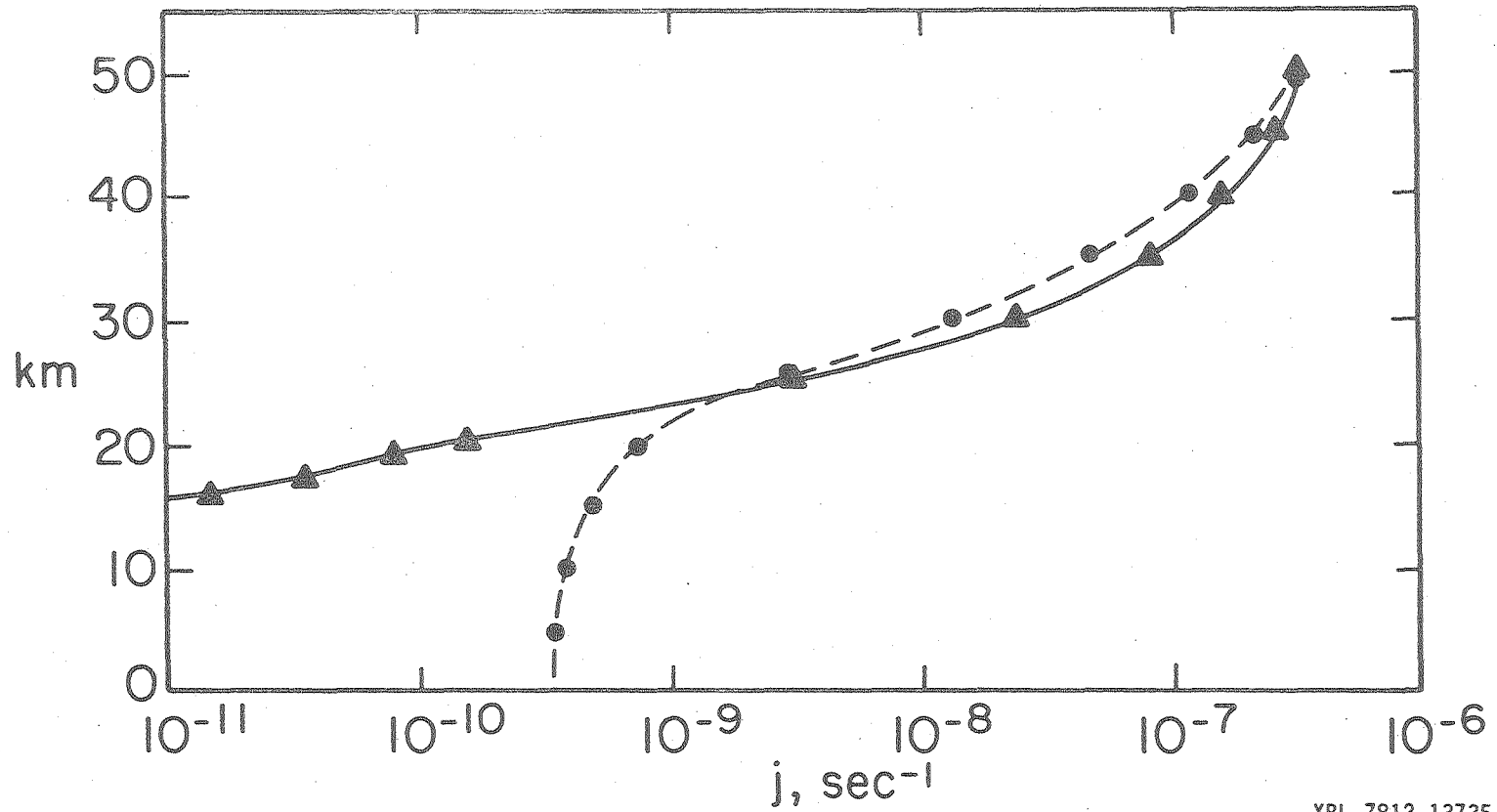
where the cross section σ is wavelength dependent. The attenuated light intensity, I , is input as a function of wavelength and solar zenith angle at the top of the stratosphere and is calculated below on the basis of the column density of absorbing molecules. The quantum yield of dissociation, ϕ , has been taken as 1.0 over all wavelengths. J is then calculated at each altitude up to 50 km in 1 km intervals and is a function of latitude in intervals of 10 degrees.

The rate constant of photolysis will also vary with season, but it is possible to make a temporal and latitudinal average. This average result for the altitude dependent j is shown as the solid line in figure 5. The dashed line in this figure is the temporal and latitudinal average value for j given by Bates and Hays.¹² Comparable values of j are obtained above 20 km since the bulk of photolysis at these altitudes is due to the larger absorbance between 200 and 235 nm, where our cross sections values agree with Bates and Hays. In the troposphere, a difference in the two models is clearly apparent. The Bates and Hays model predicts a small but finite j of 10^{-9} sec^{-1} whereas in the absence of the long wavelength absorbance, our model indicates a negligible rate of photolysis.

Multiplying the j value by the altitude dependent concentration of nitrous oxide (Ehhalt et al³¹) gives the instantaneous rate of photolysis, using the 12 hour average sun,

$$\frac{-d(\text{N}_2\text{O})}{dt} = j(\text{N}_2\text{O}) = \text{rate of destruction} = R.$$

Although the rate constant j is quite large at high altitudes,



XBL 7812-13735

Figure 5

very little N_2O is found at these altitudes and so R is small. At altitudes below 20 km, (N_2O) is much larger and j is small, but not negligible for the Bates and Hays model. Integrating the product $j(N_2O)$ over all altitudes and over the time period of a year gives a net photolytic dissociation quantity of 12.3 MT yr^{-1} for our model. Dividing the atmospheric inventory of N_2O , obtained by integrating the concentration of N_2O as a function of altitude over all altitudes and surface of the earth, by the amount of destruction by photolysis in one year gives 191 years as the lifetime of N_2O based on photolysis. The large difference of this, from the 70 years calculated by Bates and Hays, results from the lack of photolysis in the troposphere.

The importance of the other major pathway of destruction of nitrous oxide in the stratosphere, chemical reaction with $O(^1D)$, may be accessed by a similar method using the chemical rate constant (Davidson¹²⁶), the concentration of nitrous oxide, and the calculated $O(^1D)$ concentration primarily arising from O_3 photolysis. Adding the yearly destruction of nitrous oxide through chemical reaction, 1.6 MT yr^{-1} , to the 10.9 MT yr^{-1} calculated for photolysis alone, gives a corresponding lifetime of 160 years based upon these two known means of destruction. Clearly these results indicate a large discrepancy between the estimated atmospheric lifetime of 10 years and the known destruction pathways, too large to be accounted for by uncertainty in error.

In agreement with our prediction of a negligible rate of photolysis in the troposphere, Stedman⁷⁵ has experimentally demonstrated the lack of detectable photolysis in the troposphere, using a NO detector

sensitive enough to detect the NO produced by the Bates and Hays model and ambient sunlight.

III. Temperature Effect on The U.V. Absorption of N_2O

A. Introduction

The previous section showed that at shorter wavelengths, between 210 and 235 nm there was general agreement on the absorption cross section of nitrous oxide and so the atmospheric rate of photolysis was also agreed upon. These absorption measurements have been made at room temperature and thus do not necessarily reflect the properties of stratospheric nitrous oxide, where the temperatures range from 200 to 300 K.⁷⁸ For accurate modeling of the photolysis of nitrous oxide and temperature-dependent cross sections are required, assuming of course that a noticeable temperature dependence of absorption is noted within this temperature range.

Upon undertaking this project, there was substantial evidence of a noticeable temperature effect,^{8, 13} but the quantitative information was lacking. Nicolle and Vodar⁸ obtained a constant ratio of absorbance at 293 and 183 K at wavelengths above 200 nm, but did not display their data or other more quantitative results. Holliday and Reuben¹³ found the ultraviolet absorption to increase rapidly with increasing temperature from 293 to 953 K over the wavelength range 200 to 270 nm. The temperature effect was most pronounced at longer wavelengths; only a small temperature variation was noted at their shortest wavelength studied, 200 nm. Romand and Mayence⁹ reported on the quartz ultraviolet absorption as well as the more intense absorption centered at 145 nm and 291 K. Hudson presented a plot of absorption cross sections at 183, 293, and 373 K in the wavelength range 176 to 202 nm in a review article,⁷⁹ but the experimental basis for his

plot is unclear. He cites the Holliday and Reuben paper and the Romand and Mayence paper as sources, but the former only studied two of the temperatures plotted, and in fact did not study spectra at wavelengths below 200 nm. Romand and Mayence⁹ did study shorter wavelengths, but at 291 K only. Nicholle and Vodar did work at 183 K, but present no graph or tables and they worked at wavelengths greater than 200 nm. Other papers by these authors did not deal with temperature dependent measurements of nitrous oxide. Monahan and Walker¹⁵ have studied the absorption spectrum of N₂O gas at 293 K and of the solid film at 53 K over the wavelength range 100 to 200 nm.

The purpose of this study was to record the absorption spectrum of nitrous oxide at five temperatures spanning 194 to 302 K and over the wavelength range of 173 to 240 nm. These experimental conditions cover the range of temperatures and solar radiation encountered by N₂O in the stratosphere.

Previous studies have indicated that the spectrum of nitrous oxide in the region of 180 nm may have some weak structure superimposed on the continuum absorption. Zelikoff et al¹⁰ and Monahan and Walker¹⁵ have found evidence of very weak diffuse bands by optical methods. Lassetre et al⁸⁰ have observed diffuse banding by electron impact spectra. Chutjian and Segal¹⁰⁶ take note of this diffuse banding in their theoretical study in which they note an experimental band spacing of $488 \pm 30 \text{ cm}^{-1}$. Partly by accident, but mainly by pushing the instrumentation to its limits, we have found a pronounced, relatively strong, structured spectrum superimposed on the continuum in the wavelength range 173 to 187 nm.

B. Experimental

1. Quartz Cell Construction

Spectra were obtained with the Cary 118C spectrometer fitted with either one of two thermostated cells. A small quartz cell mounted in the nitrogen purged Cary sample compartment was used in the wavelength range 173 to 210 nm. The optical pathlength was 6.5 cm and each end was closed with a pair of suprasil windows (1/16" thick) with a vacuum between them for insulation. Because the inside diameter of the cell was smaller than the sample beam dimensions, it was necessary to block out the excess portion of the beam by placing two blackened washers with an inside diameter slightly less than the cell inside diameter, at both ends of the cell. This increases the background absorbance of the cell substantially but it was possible to subtract this background effect out and this process was necessary to insure accurate results.

The cell was enclosed in an insulating jacket constructed of 1/2" closed cell sponge rubber and was cooled by a stream of nitrogen boiled off from a liquid nitrogen dewar. An electric heater immersed in the liquid nitrogen regulated the nitrogen flow rate, thereby regulating the temperature in the cell. Temperature was measured by an iron-constant thermocouple located in the center of the cooling compartment of the cell. Voltage from the thermocouple was referenced to an ice-water bath, passed through a 1000x amplifier, and was measured with a digital voltmeter.

2. Long Pass Stainless Steel Cell Construction

A large stainless steel cell, used over the wavelength range 200 to 240 nm, had a double pass optical pathlength of 296 cm and

had a single optically flat, polished suprasil window (1/4" thick). The quartz was coated with 360 Å of MgF_2 on both sides to minimize reflective loss around 210 nm. The same optical arrangement used in Section II was employed here. In this cell, the mirror was mounted at the same location as the end mirror in Section II, and had the same focal length, but in this cell the mirror was contained internally. This was advantageous in that it resulted in a longer optical path length and it required one less window eliminating further the reflective losses.

All the mirrors, including the 3" diameter, 48" focal length concave mirror inside the cell were reconditioned by stripping down with acid, replating the front surface with aluminum and overcoating with MgF_2 . To enhance reflection around 210 nm, all mirrors were applied a rapid vacuum coating of aluminum followed by a 500 Å coating of MgF_2 on all mirrors except the two 45° incident mirrors in the sample compartment which had a 475 Å coating of MgF_2 on top of aluminum. A review of the relevant literature is provided by references 81-90. Greater reflectivity could be achieved by the use of a ThO or ThF_2 overcoating, but its radioactivity made this infeasible.⁹¹

The stainless steel cell, 3 1/2" diameter and 1/8" thick was welded to a second 5" diameter, 1/16" thick stainless steel tube which served as a cooling jacket. Between the two tubes, 22 feet of 3/8" copper tubing was wound into a spiral, encircling the narrower tube containing the gas. The copper spiral was suspended around the inner tube by a few hundred 3/8" rubber o-rings to damp the transfer of vibration from the cooling coils to the cell. A two stage Neslab model LT-9

refrigerating bath thermostated the cell by flowing cold methanol through the copper coils. This in turn cooled by conduction an ethanol bath in the space between the two tubes and thus cooled the cell uniformly as a unit. The cell had an end-to-end temperature differential of 0.5 K at 243 K and 1.5 K at 225 K.

Temperature was measured by placing two calibrated thermometers at either end in contact with the ethanol bath. With the ethanol bath drained, bake-out was possible up to 385 K by the use of electrical heating tape encircling the outer tube. Higher temperatures would damage the sponge rubber jacket and o-ring spacers. After bake-out, the cell could be pumped down to 2×10^{-5} torr with two small glass diffusion pumps.

To avoid some of the pressure deformation effects noted in Section II and to enable the use of the cell at pressures up to 170 psi, the rear mirror was mounted on a center flange with holes drilled in it to equalize pressure on both sides. Thus to adjust the rear mirror it was necessary to remove an end flange in order to have access to the adjusting screws. This was not inconvenient however, since no optical pressure effect was noted from 0 to 160 psi so the need for readjustment was infrequent. The front window flange was cut in the shape of two semicircles with an 1/8" metal strip between them to give added support to the window for use at higher pressures; this did not interfere with passage of the beam.

When the cell was cooled, a stream of dry nitrogen was passed across the window to prevent frost formation. At cooler temperatures, the flow was increased accordingly and, at temperatures below 245 K,

this was supplemented by placing a couple of trays containing P_2O_5 in the mirror housing below the path of the beam. To aid in this purging efficiency, the mirror housing was sealed and the cell was cemented to the mirror housing. Silicone cement worked best since the cell would contract about 0.5 mm when cooled to its lowest temperature. This purging procedure was efficient and the window could be kept completely free of frost for up to 48 hours. A schematic drawing of the cell is shown in figure 6.

Stainless Steel Cell Design

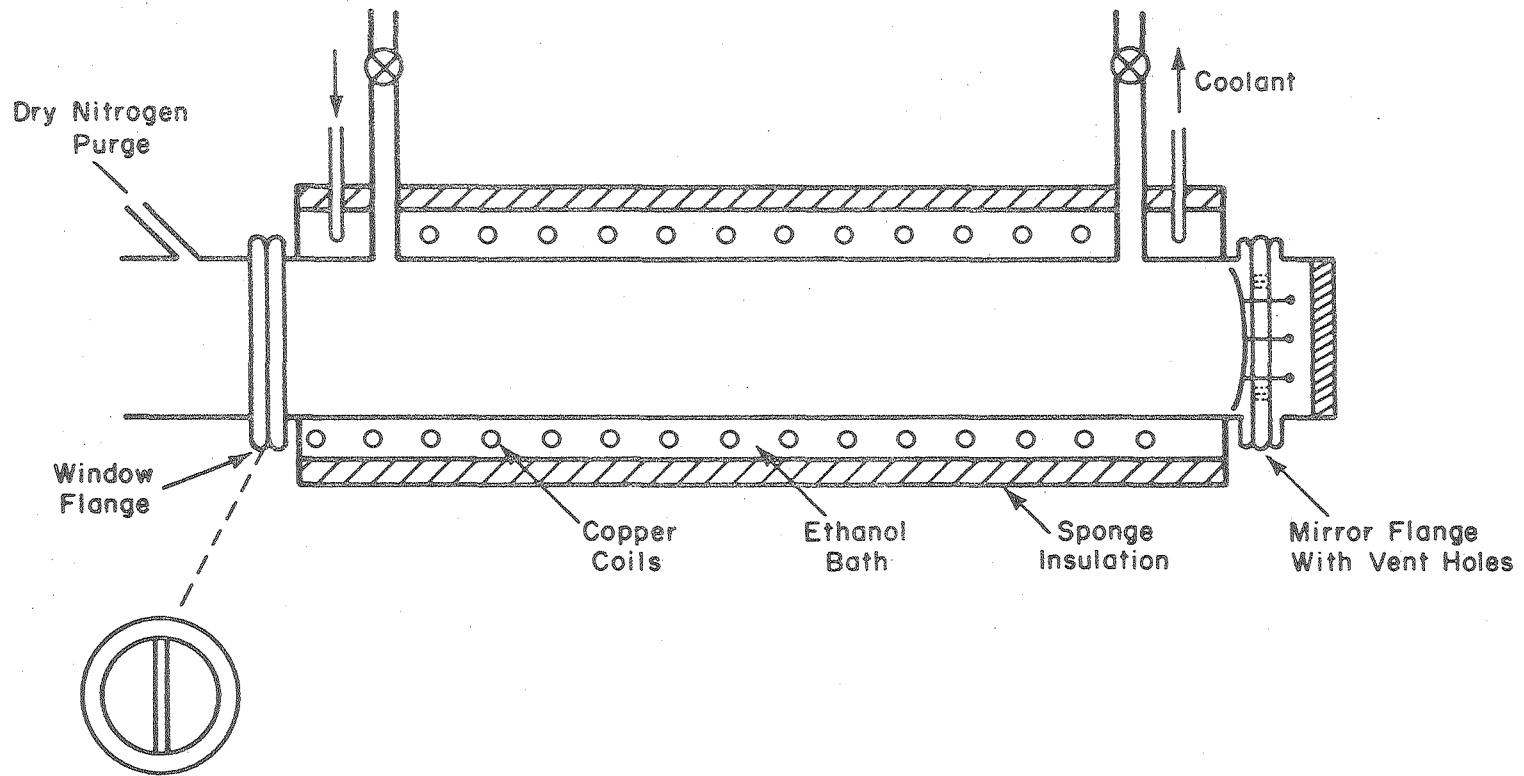


Figure 6

C. Experimental Procedures

1. Data Collection

The analog output of the spectrometer was collected and stored by a Fabritek 1074 data collector with a 12 bit A/D converter and 4000 words of storage. Data points were taken on a time basis, usually 1 point every 2 seconds and a scan was initiated by means of a Schmidt trigger located near the Cary. The Cary scan speed was 0.1 nm/sec so data points were recorded every 0.2 nm. Timing mismatch between the Cary and Fabritek did not prove to be a problem as evidenced by the reproducibility of spectral features and the results obtained with each run.

Data collected by the Fabritek could be arithmetically manipulated and was displayed on an oscilloscope screen. Through an interface to a PDP 8L minicomputer (DEC) further data reduction could be carried out using FOCAL programs. Control over the data collection and minicomputer was through a teletype and the final form results were stored on paper tape for further analysis. This method of data collection was superior to that used in Section II since signal averaging over several runs was possible.

All spectra were obtained in the double beam mode but were based on the ratio of I_0 through the evacuated cell and I through the same cell containing N_2O . For wavelengths greater than 187 nm, the resolution was 0.7 nm. Typically four scans of the sample and background (evacuated cell) were repeated. Each completed scan was checked for drift or error by comparison with other runs. The background scans were summed,

multiplied by 1/4 and subtracted from the result of the same procedure for the sample runs.

For all high resolution experiments in this section, the slits were set at 0.15 nm which gave an average resolution of 0.075 nm. The time constant was 25 seconds, the scan rate was $0.005 \text{ nm sec}^{-1}$ and data points were taken every 0.05 nm in this case. For these runs, signal averaging was also carried out for four runs, both for background and sample.

Nitrous oxide from a Matheson cylinder was purified by passing through a 3A molecular sieve (Linde) to remove water and then by four successive vacuum distillations with retention of the middle portion of each. Prior usage of a 4A molecular sieve indicated that the molecular sieve adsorbed nitrous oxide and quickly became saturated.

Gas purity was tested by a variety of techniques. By ultraviolet absorption studies, upper limits of NO and NO₂ impurity were set at < 1 ppm. By high resolution mass spectrometry, the upper limits of the following were set: N₂ < 0.1%, CO₂ < 0.01%, O₂ < 0.05%. Mass numbers from 12 to 800 were scanned and no other impurities were detected with a sensitivity of about 0.05%. The infrared spectrum from 500 to 5000 cm^{-1} was studied on a Nicolet 7199 Fourier Transform Spectrometer at 0.06 cm^{-1} resolution and did not reveal any other noticeable impurities.

Gas pressure for these experiments was measured with a factory calibrated Baracel electronic manometer.

Wavelength calibrations were made by filling a 10 cm cell with 7.5 torr NO and observing the NO absorption doublet at 226 nm (Herzberg⁹²) and by observing the rotational structuring of the Schumann-Runge

oxygen bands below 195 nm. (Knauss and Ballard⁹³, Ackerman et al⁹⁴). The nominal Cary wavelengths were accurate to 0.08 nm with a reproducibility better than 0.02 nm. The wavelengths reported here are believed to be accurate to 0.04 nm.

Since several scans in this section lasted four or five hours, it was necessary to check for photolysis by the sample beam. The absence of photolysis of N₂O in these conditions was established by the absence of any detectable NO produced during a special six hour run.

2. Nitrogen Purging

The Cary spectrometer cannot be evacuated, so nitrogen purging was required for wavelengths between 173 and 200 nm to reduce the effect of the Schumann-Runge absorption of atmospheric oxygen. The "house nitrogen" supply was used for purging. It is the boil-off of the large liquid nitrogen dewar supplying the college of chemistry, and so purity of the gas is good. Typically proper purging of the spectrometer required two days for the large monochromator chamber at 50 ft³ hr⁻¹ and the lamp, photomultiplier and sample compartments were flushed clean in 1 1/2 hours at 10 ft³ hr⁻¹. When N₂ was used to cool the cell, the cold gas was then warmed in a copper coil heat exchanger and used to purge the spectrometer.

The major problem encountered during the purging procedure was at the lamp assembly. The seal required for purging the light path was a flexible rubber gasket which would press against the flat face of the lamp. In time, the heat and UV radiation of the lamp would degrade the gasket, creating an air leak. This was further complicated

because the lamp was air cooled so the fan would blow air into the leak. This part required frequent replacement.

The efficiency of purging could be estimated by monitoring the relative transmittance of an evacuated cell in the single beam mode.

Generally, these procedures resulted in an oxygen free background spectrum; at worst a very small background absorbance at 183 nm was recorded, however this would appear in both background and sample spectra so that this was subtracted off during the data reduction phase at the Fabritek.

The rapidly decreasing transmittance of the light due to oxygen at wavelengths below 177 nm was reduced further by the decreased output of the lamp in this region, and was noticeable by the increased photomultiplier gain the Cary uses to compensate for less light. This of course, resulted in more noise and so data collection rapidly became more difficult at wavelengths below 177 nm.

D. Results

1. Reliability of Data

The absorption cross sections for nitrous oxide for radiation between 173 and 240 nm and at five temperatures between 194 and 302 K are entered in table 2. Data points were collected and analyzed at every 0.2 nm over this range, but for the rate of change noted, a data point presented for every 1 nm is sufficient. The estimated standard deviation of wavelength is ± 0.04 nm and cross section is 2%. Because only the quartz cell could be cooled to 194 K, cross sections for that temperature were only measured between 210 and 173 nm.

As stated in the introduction of this section, during the course of this study a pronounced structuring has been observed in the wavelength range 173 to 187 nm. The cross sections listed in table 2 have been averaged over this wavelength range by low resolution (0.7 nm) for the purpose of atmospheric modeling. Spectra obtained with the stainless steel cell used from 240 to 205 nm agreed with spectra obtained from the quartz cell, used from 173 to 210 nm, providing a check on systematic optical or temperature measurement errors. For the room temperature spectrum however, the stainless steel cell was at room temperature, 296 K, but inside the Cary sample compartment the "room temperature" measured was 302 K due to heat generated by the spectrometer. It proved infeasible to correct for this small temperature difference, and so two slightly different temperatures are indicated depending on the wavelength range.

Table 2. Ultraviolet absorption cross sections, $\sigma = (\ln I_0/I)(CL)^{-1}$ cm² for nitrous oxide as a function of temperature
 $3.83/24 = 3.83 \times 10^{-24}$

| Wave-length nm | 194 K | 225 K | 243 K | 263 K | 296 K | Wave-length nm | 194 K | 225 K | 243 K | 263 K | 302 K |
|-------------------|---------|---------|---------|---------|---------|-------------------|---------|---------|---------|---------|---------|
| 240 | | 3.83/24 | 4.80/24 | 5.00/24 | 1.01/23 | 209 | 5.23/21 | 5.95/21 | 6.27/21 | 7.15/21 | 9.80/21 |
| 239 | | 4.40/24 | 5.60/24 | 5.95/24 | 1.23/23 | 208 | 6.50/21 | 7.35/21 | 7.82/21 | 8.75/21 | 1.16/20 |
| 238 | | 5.30/24 | 6.70/24 | 7.35/24 | 1.52/23 | 207 | 7.87/21 | 8.95/21 | 9.52/21 | 1.07/20 | 1.38/20 |
| 237 | | 6.60/24 | 8.25/24 | 9.50/24 | 1.91/23 | 206 | 9.90/21 | 1.09/20 | 1.16/20 | 1.30/20 | 1.65/20 |
| 236 | | 7.70/24 | 9.90/24 | 1.19/23 | 2.40/23 | 205 | 1.19/20 | 1.33/20 | 1.40/20 | 1.57/20 | 1.95/20 |
| 235 | | 9.65/24 | 1.22/23 | 1.49/23 | 3.01/23 | 204 | 1.44/20 | 1.62/20 | 1.69/20 | 1.85/20 | 2.30/20 |
| 234 | | 1.21/23 | 1.54/23 | 1.93/23 | 3.60/23 | 203 | 1.69/20 | 1.90/20 | 2.00/20 | 2.20/20 | 2.67/20 |
| 233 | | 1.51/23 | 1.91/23 | 2.46/23 | 4.78/23 | 202 | 2.04/20 | 2.26/20 | 2.40/20 | 2.60/20 | 3.09/20 |
| 232 | | 1.92/23 | 2.43/23 | 3.13/23 | 6.05/23 | 201 | 2.40/20 | 2.67/20 | 2.81/20 | 3.01/20 | 3.58/20 |
| 231 | | 2.50/23 | 3.06/23 | 4.05/23 | 7.60/23 | 200 | 2.85/20 | 3.08/20 | 3.28/20 | 3.52/20 | 4.09/20 |
| 230 | | 3.20/23 | 3.91/23 | 5.05/23 | 9.55/23 | 199 | 3.36/20 | 3.64/20 | 3.86/20 | 4.06/20 | 4.70/20 |
| 229 | | 4.05/23 | 5.00/23 | 6.45/23 | 1.20/22 | 198 | 3.89/20 | 4.24/20 | 4.45/20 | 4.73/20 | 5.35/20 |
| 228 | | 5.25/23 | 6.40/23 | 8.35/23 | 1.51/22 | 197 | 4.55/20 | 4.88/20 | 5.10/20 | 5.42/20 | 6.10/20 |
| 227 | | 6.81/23 | 8.30/23 | 1.06/22 | 1.90/22 | 196 | 5.18/20 | 5.53/20 | 5.83/20 | 6.14/20 | 6.82/20 |
| 226 | | 9.85/23 | 1.07/22 | 1.36/22 | 2.39/22 | 195 | 5.80/20 | 6.20/20 | 6.42/20 | 6.85/20 | 7.57/20 |
| 225 | | 1.16/22 | 1.37/22 | 1.75/22 | 3.03/22 | 194 | 6.48/20 | 6.90/20 | 7.25/20 | 7.51/20 | 8.11/20 |
| 224 | | 1.45/22 | 1.81/22 | 2.34/22 | 3.75/22 | 193 | 7.20/20 | 7.64/20 | 7.95/20 | 8.32/20 | 8.95/20 |
| 223 | | 1.87/22 | 2.30/22 | 2.95/22 | 4.74/22 | 192 | 7.72/20 | 8.40/20 | 8.75/20 | 9.20/20 | 9.75/20 |
| 222 | | 2.39/22 | 2.93/22 | 3.76/22 | 5.88/22 | 191 | 8.59/20 | 9.02/20 | 9.36/20 | 9.81/20 | 1.04/19 |
| 221 | | 3.08/22 | 3.74/22 | 4.73/22 | 7.39/22 | 190 | 9.38/20 | 9.85/20 | 1.01/19 | 1.06/19 | 1.11/19 |
| 220 | | 3.98/22 | 4.82/22 | 6.01/22 | 9.22/22 | 189 | 9.97/20 | 1.05/19 | 1.07/19 | 1.12/19 | 1.17/19 |
| 219 | | 5.19/22 | 6.14/22 | 7.58/22 | 1.15/21 | 188 | 1.07/19 | 1.11/19 | 1.17/19 | 1.19/19 | 1.25/19 |
| 218 | | 6.68/22 | 7.85/22 | 9.68/22 | 1.42/21 | 187 | 1.12/19 | 1.17/19 | 1.19/19 | 1.23/19 | 1.31/19 |
| 217 | | 8.75/22 | 1.02/21 | 1.22/21 | 1.79/21 | 186 | 1.16/19 | 1.22/19 | 1.25/19 | 1.29/19 | 1.36/19 |
| 216 | | 1.13/21 | 1.29/21 | 1.54/21 | 2.23/21 | 185 | 1.22/19 | 1.27/19 | 1.31/19 | 1.35/19 | 1.43/19 |
| 215 | | 1.44/21 | 1.64/21 | 1.95/21 | 2.76/21 | 184 | 1.26/19 | 1.30/19 | 1.32/19 | 1.36/19 | 1.44/19 |
| 214 | | 1.87/21 | 2.08/21 | 2.45/21 | 3.42/21 | 183 | 1.28/19 | 1.33/19 | 1.35/19 | 1.39/19 | 1.46/19 |
| 213 | | 2.36/21 | 2.62/21 | 3.05/21 | 4.21/21 | 182 | 1.29/19 | 1.33/19 | 1.37/19 | 1.40/19 | 1.47/19 |
| 212 | | 3.00/21 | 3.31/21 | 3.80/21 | 5.18/21 | 181 | 1.32/19 | 1.34/19 | 1.36/19 | 1.39/19 | 1.46/19 |
| 211 | | 3.80/21 | 4.08/21 | 4.72/21 | 6.19/21 | 180 | 1.33/19 | 1.35/19 | 1.38/19 | 1.39/19 | 1.46/19 |
| 210 | 4.23/21 | 4.70/21 | 5.11/21 | 5.79/21 | 7.55/21 | 179 | 1.30/19 | 1.32/19 | 1.34/19 | 1.37/19 | 1.44/19 |
| | | | | | | 178 | 1.28/19 | 1.28/19 | 1.29/19 | 1.31/19 | 1.39/19 |
| | | | | | | 177 | 1.27/19 | 1.28/19 | 1.29/19 | 1.31/19 | 1.40/19 |
| | | | | | | 176 | 1.24/19 | 1.23/19 | 1.25/19 | 1.27/19 | 1.34/19 |
| | | | | | | 175 | 1.16/19 | 1.15/19 | 1.17/19 | 1.18/19 | 1.26/19 |
| | | | | | | 174 | 1.14/19 | 1.14/19 | 1.15/19 | 1.17/19 | 1.19/19 |
| | | | | | | 173 | 1.07/19 | 1.08/19 | 1.10/19 | 1.11/19 | 1.13/19 |

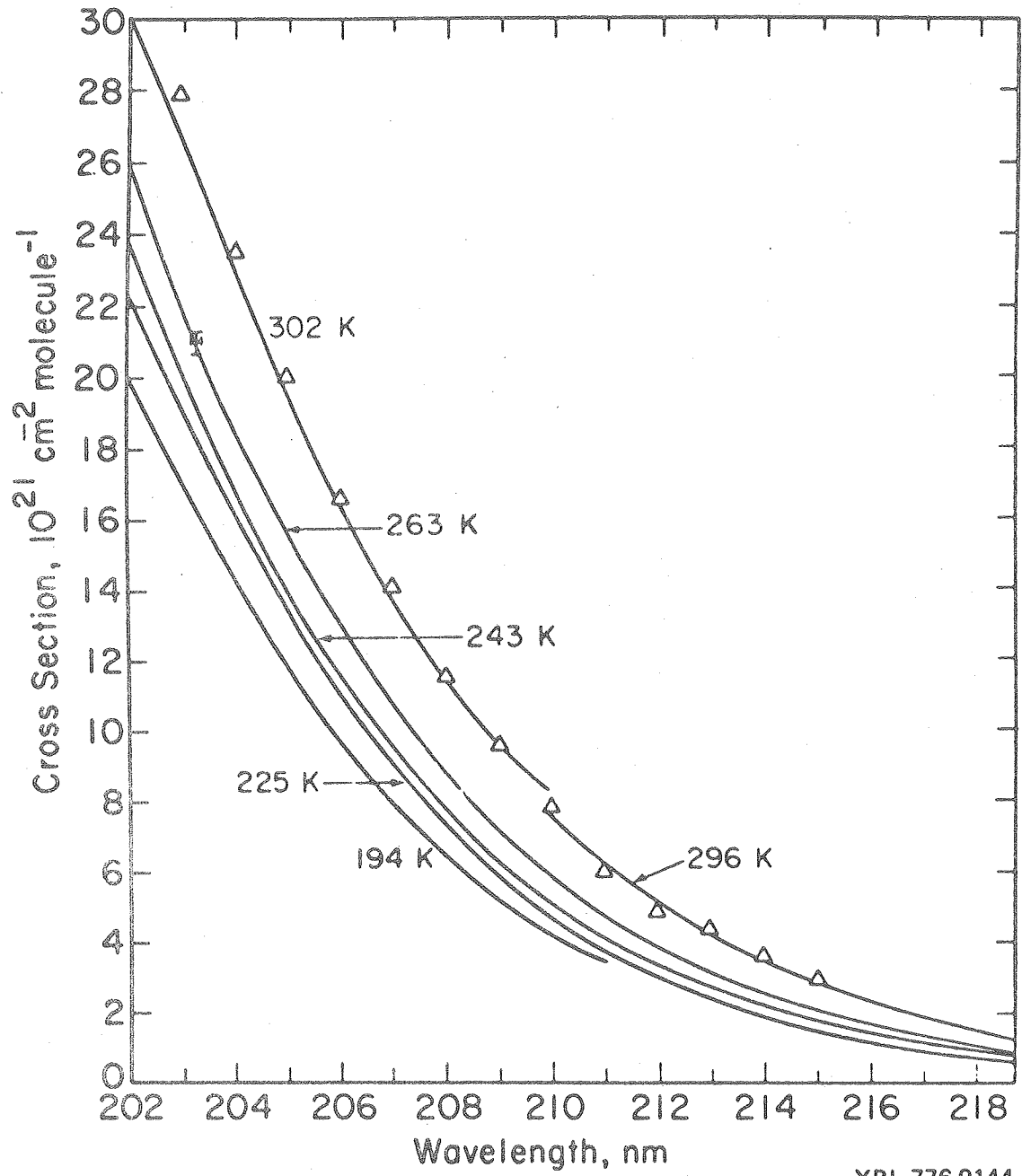
2. Continuous Absorption

The portion of the data centered at the stratospheric "window," the region between the decreasing absorbance of the Hartley O₃ band and the increasing absorbance of the Schumann-Runge bands of O₂, is shown in figure 7. The triangles are the data points of Zelikoff, Watanabe, and Inn. Excellent agreement between the room temperature values is noted. Agreement at room temperature with the values in Section II has also been noted. The region shown here, especially from 205 to 225 nm, is important in stratospheric photolysis of N₂O as a result of larger light flux in this "window" region. It is difficult to see in this figure that the percentage change of absorbance with temperature is greatest at longer wavelengths. The ratio of the cross sections between the room temperature value and the value obtained at 225 K is about 2.9 at 240 nm, about 1.6 at 210 nm and about 1.15 at 190 nm. This is in qualitative agreement with the findings of Holliday and Reuben at elevated temperatures.

Jim Podolske was able to fit the temperature dependence at each wavelength in the empirical formula:

$$\ln \sigma (\lambda, T) = A_1 + A_2 \lambda + A_3 \lambda^2 + A_4 \lambda^3 + A_5 \lambda^4 \\ + (T-300) \exp(B_1 + B_2 \lambda + B_3 \lambda^2 + B_4 \lambda^3)$$

The nine parameters were fit by a nonlinear, least-squares, minimization routine to give the coefficients for λ in nm,



XBL 776-9144

Figure 7

$$A_1 = 68.21023$$

$$B_1 = 123.4014$$

$$A_2 = -4.071805$$

$$B_2 = -2.116255$$

$$A_3 = 4.301146 \times 10^{-2}$$

$$B_3 = 1.111522 \times 10^{-2}$$

$$A_4 = -1.777846 \times 10^{-4}$$

$$B_4 = -1.881058 \times 10^{-5}$$

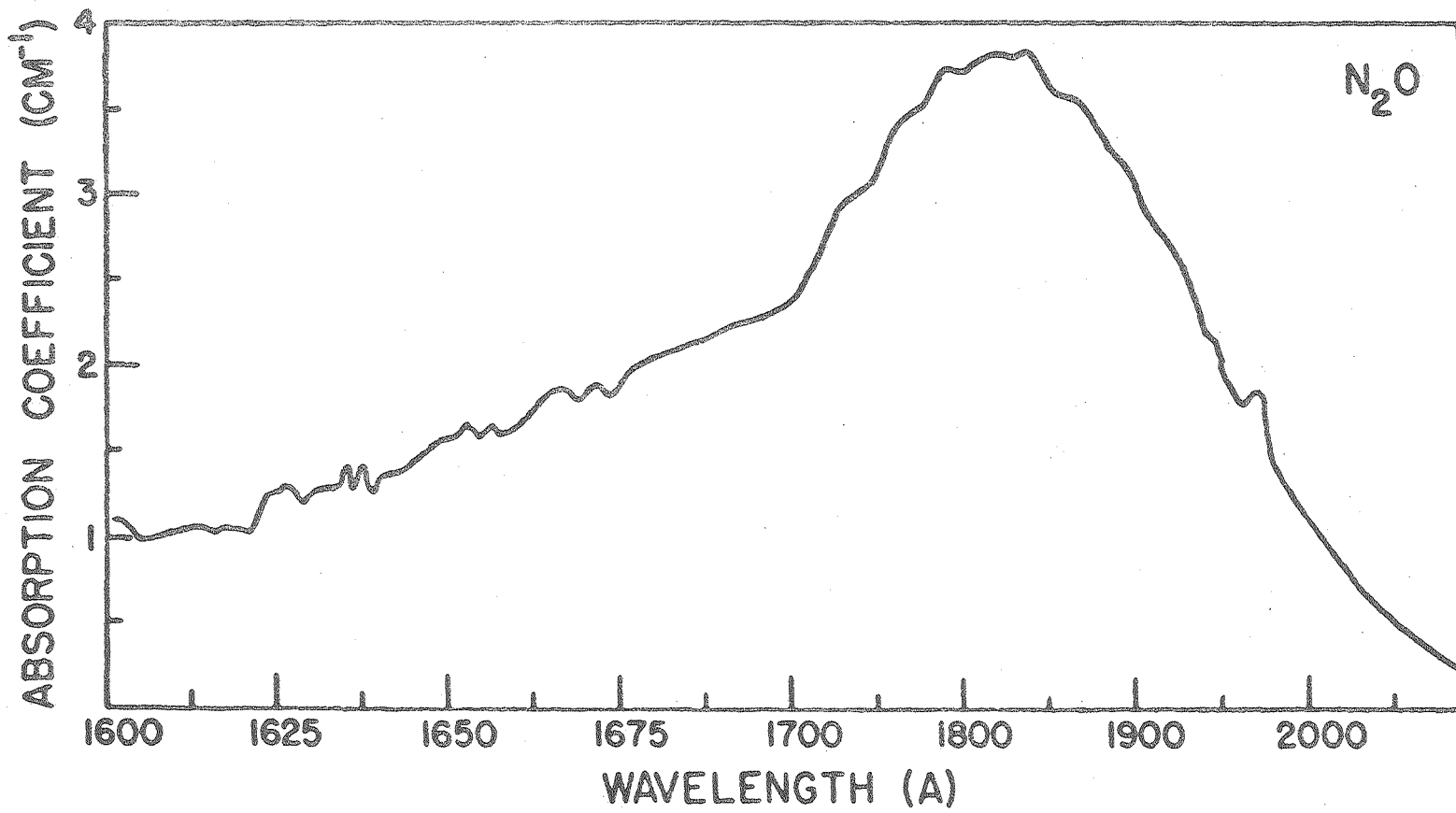
$$A_5 = 2.520672 \times 10^{-7}$$

with an estimated standard deviation of about 4 percent.

3. Structured Spectrum

While collecting low resolution data in the wavelength range 173 to 187 nm, it was noticed that small bulges in the continuum were consistently reproduced. This was not thought too unusual since a similar effect was noted by Zelikoff et al.¹⁰ A spectrum taken from their paper is shown as figure 8. However upon comparing spectra taken at different temperatures in this wavelength range, it was also noticed that the extent and intensity of the "bulges" varied strongly with temperature. A spectrum taken under conditions of higher resolution was remarkably different from that expected. Under the proper experimental conditions and with signal averaging, the spectrum shown in figure 9 was obtained.

The spectrum shows a number of vibrational envelopes of varying shapes and intensities; some have bandheads and others appear as superpositions of individual features. Generally, the structuring appears to decrease in intensity towards longer wavelengths. Very weak features can be observed up to 195 nm, but above 200 nm no hint of structuring at all is detected, only a purely continuous spectrum is observed. A similar spectrum taken at 195 K shows the structuring to be reduced substantially more than the underlying continuum was reduced.



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Figure 8

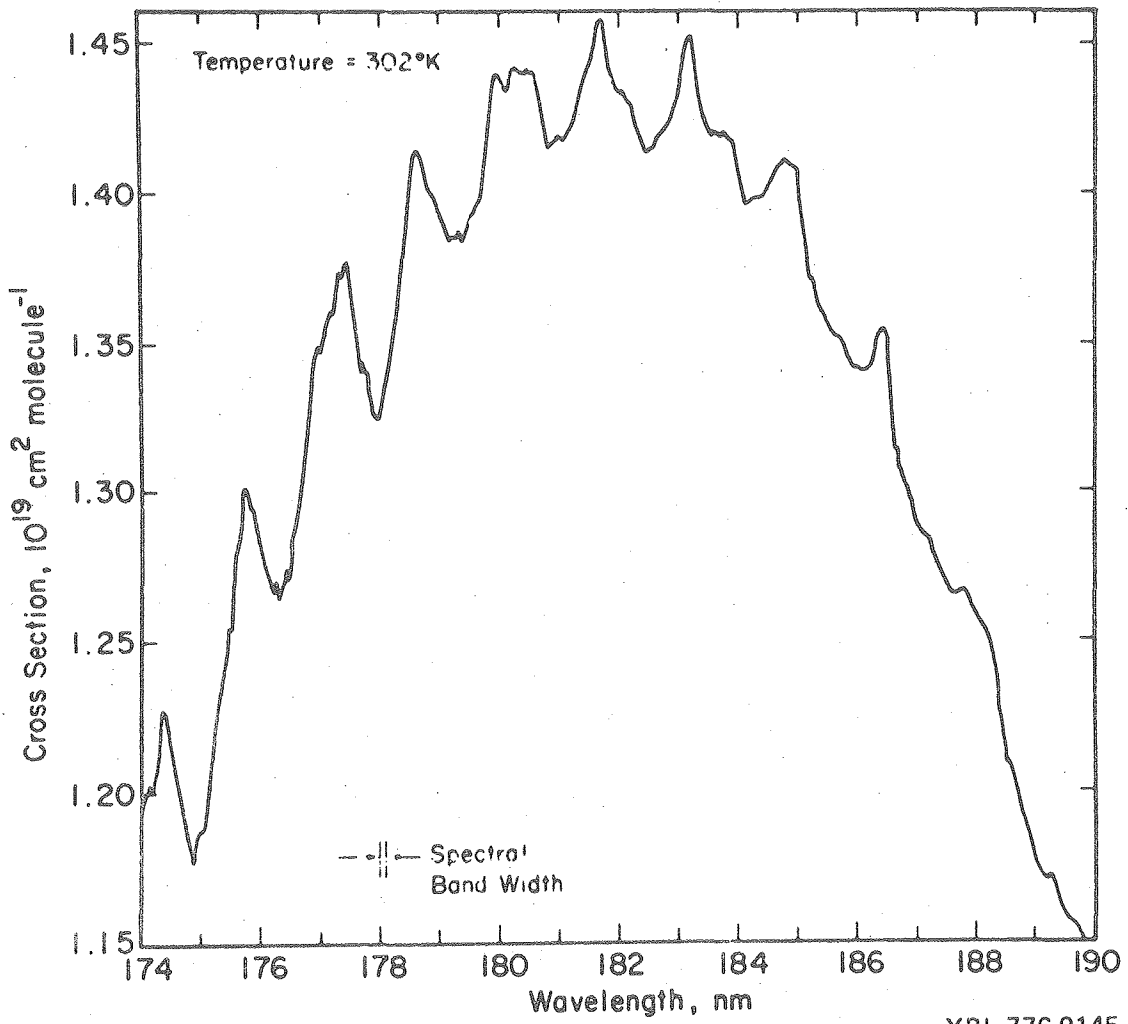


Figure 9

The possibility that the observed structuring was due to an impurity also received careful consideration. Confidence of the observed results was achieved only after the following considerations of purity:

1) UV spectroscopy, mass spectrometry and IR absorption did not reveal any observable impurities as mentioned previously in this section.

2) A search of the ultraviolet absorption literature did not reveal any spectra of other gases that closely fit the observed banding pattern.

3) The observed temperature effect was a function of temperature over a broad temperature range. For a condensing vapor of an impurity, one might expect a strong decrease in absorption only below a given temperature, and less effect at elevated temperatures. The temperature dependent survey is covered in Section IV.

4) The observed spectra of the four nitrogen isotopes $^{14}\text{N}^{14}\text{NO}$, $^{15}\text{N}^{14}\text{NO}$, $^{14}\text{N}^{15}\text{NO}$, and $^{15}\text{N}^{15}\text{NO}$ each show a similar spectrum but with a unique wavelength shift of the features. The remote possibility of a uniquely labeled impurity in each sample can be dismissed in conjunction with No. 1, 2 and 3 of the above for each isotope.

A more intensive survey of this structuring, its temperature dependence and theoretical basis is covered in the next section.

IV. Temperature Effect of Nitrous Oxide Vibronic Structuring at 6.8 eV

A. Introduction

1. Previous Studies

As mentioned in Section III, previous investigators have noted weak diffuse banding superimposed on the continuous absorption of N_2O . An example of this diffuse banding first observed by Zelikoff et al¹⁰ was shown as figure 8. Monahan and Walker¹⁵ also observed these bands, with somewhat more definition, but like previous studies were unable to analyze the banding or identify individual features.

Non-optical methods such as the high resolution electron energy loss spectra by Lassetree and coworkers⁸⁰ have also been successful in observing the diffuse banding of N_2O , although it was still too weak and diffuse for analysis by these methods.

At low resolution our spectra appeared similar to the previous studies, but at higher resolution a different spectrum resulted. Sufficient tests of purity as mentioned in Section III uphold its validity.

2. Definition of the Vibrational State Spectrum

It is the object of this study to quantify the effect of temperature on the resolved spectrum. With improved definition of the structured absorption and its temperature dependence, it should be possible to identify the active vibrations of N_2O responsible for the observed temperature effect and to analyze the energy spacing of the upper electronic state.

The initial assumption made in this study is that each vibrational mode of the lower electronic state will have a unique absorption spectrum and that the observed absorption spectrum results from the convolution of these vibrational state spectra which are individually weighted by their respective equilibrium populations at a given temperature. In other words, the observed ultraviolet spectrum, $Y(T, \lambda)$, can be expressed as the sum of individual state spectra,

$$Y(T, \lambda) = a(T)A(\lambda) + b(T)B(\lambda) + c(T)C(\lambda) + \dots$$

where a , b , and c reflect the equilibrium macroscopic populations of the pure A , B , and C vibrational state spectra. Implicit in this expansion, is the further assumption that the vibrational state spectra, A , B and C , are independent of temperature. In a rigorous definition, the ultraviolet spectrum of a pure vibrational mode will have a temperature dependence owing to the change in the thermal distribution of its rotational members. For an ultraviolet spectrum consisting only of discrete band spectra, a change in the distribution of J'' would be expected to alter the shape and intensity of the transition:

$$\nu'(K', J') + \nu''(J'')$$

due to the quantum selection rules for $J' - J''$. However, within the high temperature limit, the variation of the rotational distribution changes only by a small amount. This is illustrated in figure 10 which shows the normalized probability of the rotational distribution of N_2O as a function of J for three different temperatures. It is clear that between 300 and 500 K the change in the J distribution is minor and so the temperature variation of the vibrational state spectra will be small. At temperatures much below 300 K, as in the case at

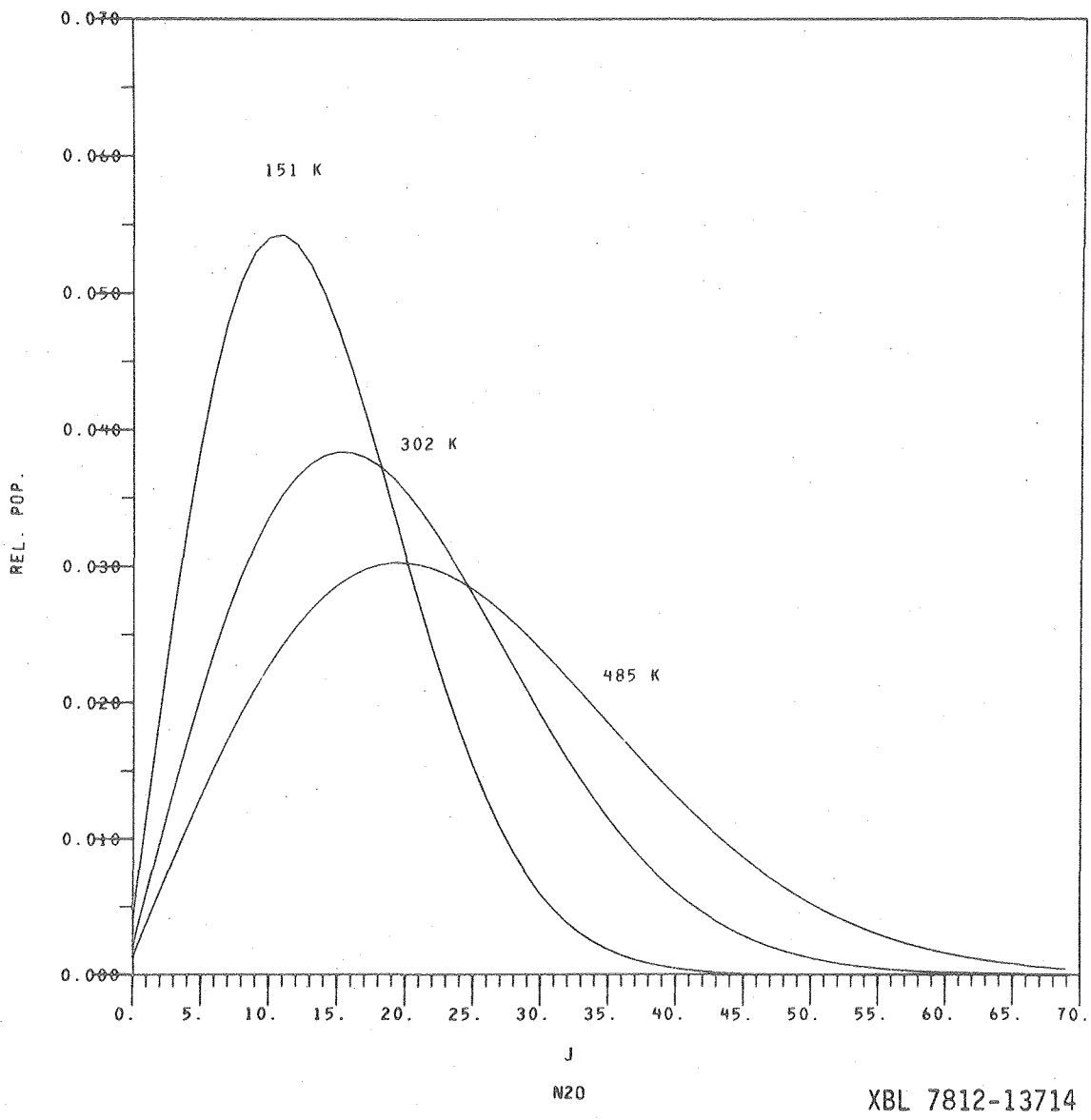


Figure 10

151 K, the rotational population is significantly altered. Fortunately, in the case of N_2O , at these temperatures a continuous spectrum is observed, and the discrete banding is very weak. The shape of a continuous absorption is determined by the electronic and vibrational wavefunctions of the two electronic states and the dependence on such rotational change should be minor term. For these reasons, the thermal independence of the vibrational state spectra, especially in the case of nitrous oxide, is considered valid to a first approximation.

The equilibrium populations of the vibrational modes, a,b,c ..., will be a strong function of temperature over the range 150 to 500 K, and will follow well known statistical relationships. These coefficients can be determined precisely over a wide temperature range.

3. Statistical Populations of Normal Vibrational Modes

For a one dimensional harmonic oscillator the vibrational partition function, q_v , is given by⁹⁵

$$q_v = \sum_{n=0}^{\infty} e^{-h\nu(n+1/2)/kT} = \frac{e^{-h\nu/2kT}}{1-e^{-h\nu/kT}}$$

where ν is the energy of the vibrational mode with quantum number n at temperature T .

Neglecting anharmonicity and coupling of vibrations for a polyatomic molecule,

$$q_v = \prod_{j=1}^{\alpha} \frac{e^{-h\nu_j/2kT}}{1-e^{-h\nu_j/kT}}$$

Here, the product of all independent normal vibration energies, ν_j , has been taken up to α , where $\alpha = 3n-5$ for a linear molecule. These normal vibrational frequencies of nitrous oxide reknown from infra-

red data:^{96a}

$$\nu_1 = 1284.7 \text{ cm}^{-1}$$

$$\nu_2 = 588.8 \text{ cm}^{-1} \text{ (doubly degenerate)}$$

$$\nu_3 = 2223.5 \text{ cm}^{-1}$$

The population of a given vibration irrespective of other normal vibrations is given by

$$f = \frac{\omega e^{-h\nu_j(n + 1/2)/kT}}{q_v}$$

where ω denotes the degeneracy of the n^{th} level of vibration ν_j .

For a triatomic of $C_{\infty v}$ symmetry, only the ν_2 vibration is degenerate and the degeneracy of the n^{th} level is $n+1$:^{96b}

$$\omega = (n + 1) \text{ for } \nu_2$$

To describe the population of the vibrational levels in terms of the four (two of which are degenerate) vibrations of nitrous oxide, the product of the individual populations is taken:

$$\frac{N_{\nu_{\ell mn}}}{N_T} = \frac{e^{-h\nu_i(\ell + 1/2)/kT} (n + 1) e^{-h\nu_j(n + 1/2)/kT} e^{-h\nu_k(m + 1/2)/kT}}{q_v}$$

Here, $\nu_{\ell mn}$ will also be written as (ℓnm) .

As indicated on page 49, q_v is given by

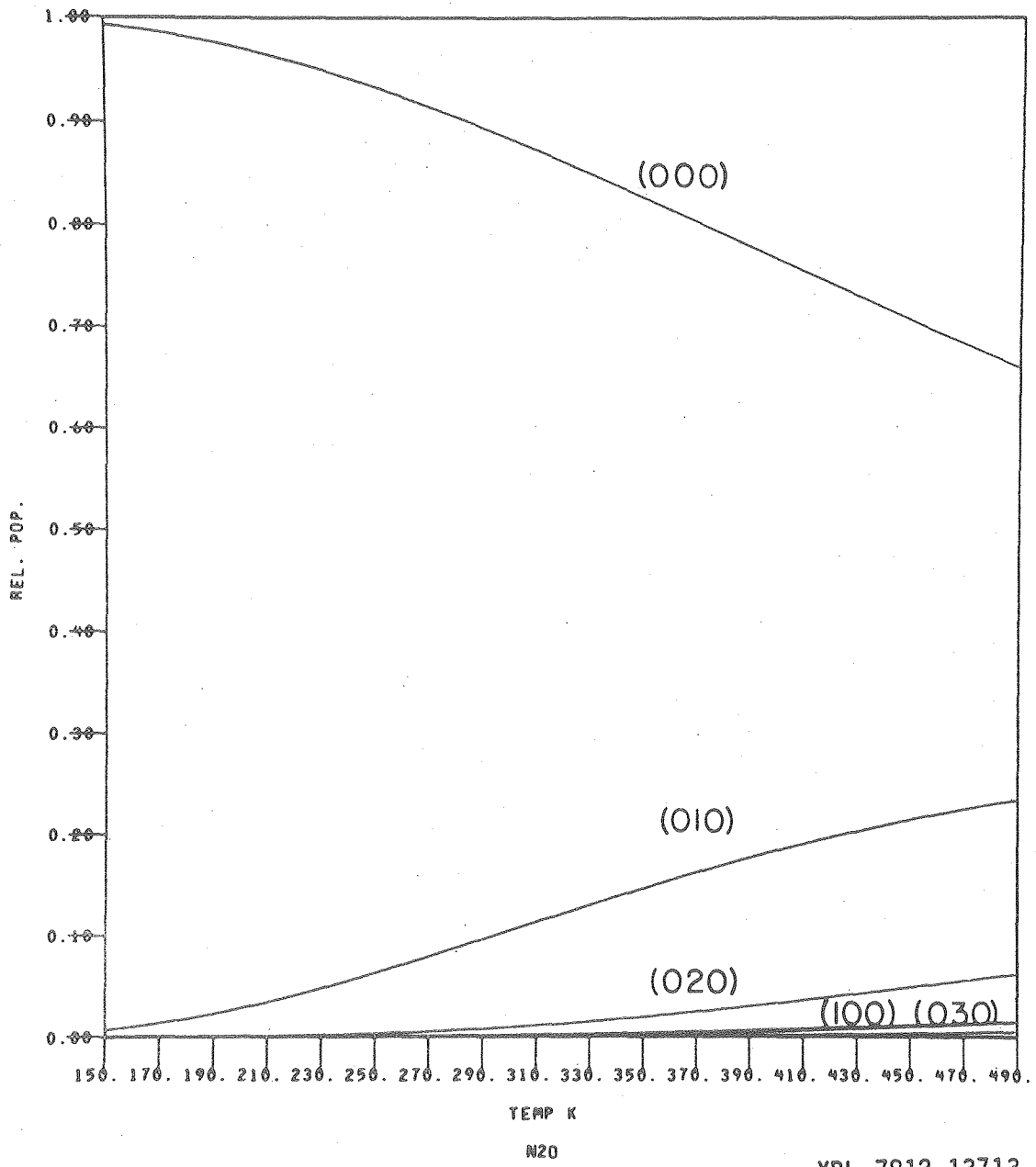
$$q_v = \left(\frac{e^{-h\nu_i/2kT}}{1 - e^{-h\nu_i/kT}} \right) \left(\frac{e^{-h\nu_j/2kT}}{1 - e^{-h\nu_j/kT}} \right)^2 \left(\frac{e^{-h\nu_k/2kT}}{1 - e^{-h\nu_k/kT}} \right)$$

The second factor is squared because it is doubly degenerate.

In this way, the populations of (000), (010), (006) or (113) may be determined as a function of temperature. In fact, over the

temperature range 150 to 485 K, only the populations of (000), (010), (020), (030), and (100) will be significant.

A plot of the populations of several vibrational modes as function of temperature is shown in figure 11. As in the case of the rotational populations, the sum of all vibrational populations at any temperature must equal 1. Also plotted in this figure, the sum of all vibrations shown, is superimposed on the top margin (1.0000), indicating this to be so.



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Figure 11

B. Theoretical Aspects of Electronic Spectrum of Polyatomic Molecules

1. Vibrational State Spectra

The observed spectrum, Y , has been described as the weighted sum of individual vibrational state spectra, $A, B, C \dots$, which have been assumed to be independent of temperature over the temperature range studied. If the state spectra of the different vibrational modes are not very much different, or if the populations of the excited vibrations are very small, then the observed spectrum does not vary much with temperature over this range. The magnitude of the difference in the absorption spectrum of the different vibrational modes will reflect the difference in the overlap of the differing Franck-Condon regions of the vibrational modes and the extent of vibronic interaction involved, if any.

If, for reasons of symmetry or vibrational coupling to be discussed later, the (010) state absorption is very much different than the absorption spectrum of the (000) state and the populations of other vibrations is negligible, the observed spectrum may be described simply by

$$Y(T, \lambda) = a(T)A(\lambda) + b(T)B(\lambda)$$

where, a designating the (000) population, will decrease with temperature, and b , designating the (010) population, will increase with temperature. At lower temperature, Y will most nearly resemble A and $Y \rightarrow A$ as $a \rightarrow 1.0$. At higher temperatures, the spectrum will involve increasingly more character of B . It is not possible to occupy only B and so this state spectrum cannot be directly observed in thermal equilibrium with its surroundings. In such a case, if it is the change

in $b(T)$ which is primarily responsible for a large temperature effect in $Y(T)$ over a given temperature range, then it is convenient to describe B as the "active vibration" responsible for the observed temperature dependence.

The populations of all the vibrational modes will follow the statistical relations outlined previously and so it is possible to deconvolute a series of temperature dependent absorption measurements into the component state spectra. The reliability of this calculation is greatly enhanced if the vibrational energies ν_i , ν_j , and ν_k are well separated from each other and their combinations, and if there is a reasonably large temperature effect on the observed absorption spectrum.

For "allowed" electronic transitions there will often be an observable difference in the vibrational state spectra due to differing regions of Franck-Condon overlap. For "forbidden" transitions, the vibrational state spectra may be even more markedly different if the transition occurs through vibronic interaction.

2. Allowed Electronic Transitions^{97a}

An electronic transition is designated as an "allowed" transition if the transition moment, R , is different from zero,

$$(1) R_{e'e''} = \int \psi'^*_{e'} M \psi''_{e''} d\tau_e \neq 0$$

here $R_{e'e''}$ is the electronic transition moment of the lower electronic state, $\psi''_{e''}$, and the complex conjugate of the upper electronic state, $\psi'^*_{e'}$, and M is the electronic dipole operator with the components

$$\sum_i e_i x_i, \quad \sum_i e_i y_i, \quad \sum_i e_i z_i$$

where e_i are the charges or the on particles with coordinates x_i , y_i , and z_i . The integral will be unequal to zero only if the product

$$(2) \psi'^*_{e'} M \psi''_{e''}$$

has a totally symmetric character class for the symmetry of the involved species. In Group Theory notation,

$$\Gamma(\psi'_{e'}) \times \Gamma(\psi''_{e''}) \times \Gamma(M) = \text{totally symmetric}$$

Implicit in this selection rule is the use of the Born-Oppenheimer approximation, separating the wavefunctions of nuclear and electronic motion:

$$(3) \psi_{ev} = \psi_e(q, Q) \psi_v(Q)$$

A more rigorous definition of the transition moment would be

$$(4) R_{e'v'e''v''} = \int \psi_{e'v'}^* M \psi_{e''v''} d\tau_{ev} \neq 0$$

Neglecting for a moment the more rigorous definition of (4) and continuing with (1) and assuming the Born-Oppenheimer approximation holds, a similar resolution may be made for the electric dipole moment into electronic and nuclear motion:

$$(5) \quad M = M_e + M_n$$

then

$$(6) \quad R_{e'v'e''v''} = \int \psi_{ev'}^* M \psi_{ev''} d\tau_{ev} \\ = \int \psi_v^* \psi_v'' d\tau_v \int \psi_e^* M \psi_e d\tau_e + \\ \int \psi_v^* M_n \psi_v'' d\tau_v \int \psi_e^* \psi_e d\tau_e$$

Standard analysis then assumes that for a valid Born-Oppenheimer approximation the electronic components of the wavefunctions are orthogonal, so that (6) reduces to

$$(7) \quad R_{e'v'e''v''} = \int \psi_v^* \psi_v'' d\tau_v \int \psi_e^* M \psi_e d\tau_e$$

where the second integral has been defined in equation (1),

$$(8) \quad R_{e'v'e''v''} = R_{e'e''} (Q) \int \psi_v^* \psi_v'' d\tau_v$$

The transition moment is equal to the product of the electronic transition moment and the vibrational overlap integral.

$R_{e'e''}$ is different from zero and applies to all transitions between the two electronic states. It is the second factor which is responsible for the intensity structure (vibrational features) of the transition. The overlap integral is the quantum mechanical interpretation of the Franck-Condon principle.

Applying a similar argument for electron spin it may be shown that, as for diatomics,

$$\Delta S = 0$$

where S is the net electron spin of the wavefunction. Only states of the same multiplicity may combine with each other. This rule applies primarily to light molecules and tends to break down increasingly with heavier molecular weights.

3. Forbidden Transitions^{97b}

Unlike diatomics, in which forbidden transitions are not usually seen optically, in polyatomics, these transitions often occur weakly. For a "forbidden" transition:

$$(1) R_{e'e''} = \int \psi_{e'}^* M \psi_{e''} d\tau_e = 0$$

However, if the more rigorous form is not equal to zero,

$$(4) R_{e'v'e''v''} = \int \psi_{ev'}^* M \psi_{ev''} d\tau_{ev} \neq 0$$

then the transition will occur.

Even if (4) equals zero, the transition may still occur if substitution of the magnetic dipole operator or electric quadrupole operator in (1) gives a nonvanishing result, although these transitions are much weaker than allowed electron dipole transitions, typically 10^{-5} and 10^{-8} respectively of an allowed electric dipole transition.^{97g}

One way in which the transition is allowed in (4) and not in (1) is through vibronic interaction. This implies that the separability of the wavefunction as expressed in equation (6) is not valid and correspondingly, (8) is also invalid.

A first approximation to the vibronic wavefunction, is obtained from the direct product multiplication

$$(9) \psi_{ev} = \psi_e \times \psi_v$$

and so it is immediately seen that if ψ_v is the totally symmetric species, (4) will give the same result as (1) and thus vibronic interaction cannot be responsible for the transition. However if ψ_v is an antisymmetric or degenerate vibration, then ψ_{ev} may have a different symmetry than

ψ_e and $R_{e',v',e''v''}$ may be unequal to zero when equation (4) is applied.

An example may be the ${}^1\Sigma_g^+ \rightarrow {}^1\Sigma_g^+$ transition for $D_{\infty h}$ symmetry. This transition is allowed only through the electronic quadrupole operator and thus is extremely weak. However coupling of ${}^1\Sigma_g^+$ with a Σ_u^+ or a π_u vibration would not result in $R_{e',v',e''v''} = 0$, and so electronic transitions due to vibronic interaction are specific for the vibration involved. The degree of intensity of a vibronically allowed transition depends on the strength of the vibronic interaction and is directly proportional to $(R_{e',v',e''v''})^2$.

Figure 12 shows a relevant possibility of vibronic interaction for the ${}^1\Sigma^+$ and ${}^1\Sigma^-$ electronic states of N_2O . (In this discussion, + and - of ${}^1\Sigma^-$ and ${}^1\Sigma^+$ refer to the symmetry or asymmetry of the electronic wavefunction when reflected by the vertical plane of symmetry.) The case without vibronic interaction has no transitions because of the $+ \nrightarrow -$ selection rule of electronic transitions. With vibronic interaction, the $- \rightarrow -$ and $+ \rightarrow +$ selection rule is still maintained, as is the angular momentum selection rule, $\Delta\lambda = 0, \pm 1$, except that with vibronic mixing a number of transitions are now possible. Note especially that the $v_2 = 1$, or 2 levels each have at least one transition to each v_2 vibrational level of the upper state. In contrast, the $v_2 = 0$ level has a transition only to the π vibronic levels of the upper state. Since the $v_2 = 0$ vibronic wavefunction has the same symmetry as the totally symmetric electronic state, this transition can be attributed to the bending interaction of the upper state.

Figure 12 is useful for demonstrating the effect of vibronic interaction on observed transitions but for studies here, it is more

| Electronic Species | ν_2 | Quantum No. | Vibrational Species | No Vibronic Mixing | With Vibronic Mixing | Vibronic Species | |
|---------------------------------------|---------|--|--|--------------------|----------------------|--|--|
| Σ^- | 2 | $\begin{Bmatrix} 2 \\ 0 \end{Bmatrix}$ | $\begin{matrix} \Delta \\ \Sigma^+ \end{matrix}$ | | | $\begin{matrix} \Delta \\ \Sigma^- \end{matrix}$ | |
| | 1 | 1 | π | | | π | |
| | 0 | 0 | Σ^+ | | | Σ^- | |
| (all $- \leftrightarrow +$ forbidden) | | | | | | | |
| Σ^+ | 2 | $\begin{Bmatrix} 2 \\ 0 \end{Bmatrix}$ | $\begin{matrix} \Delta \\ \Sigma^+ \end{matrix}$ | | | $\begin{matrix} \Delta \\ \Sigma^+ \end{matrix}$ | $\begin{matrix} (02^20) \\ (02^00) \end{matrix}$ |
| | 1 | 1 | π | | | π | (010) |
| | 0 | 0 | Σ^+ | | | Σ^+ | (000) |

Figure 12

useful to compare just the differences of the $\nu_2 = 0$ and $\nu_2 = 1$ vibronic levels of the ground electronic state with higher vibrational levels of an upper ${}^1\Sigma^-$ electronic state. Figure 13 shows the vibronic species of the upper levels of the ν_2 vibrational mode of ${}^1\Sigma^-$. The quantum numbers 12, 13, 14 and 15 have been chosen arbitrarily only to demonstrate that from $\nu_2'' = 0$ the spectrum should show an energy spacing of $2\nu_2'$ whereas transitions originating from the vibrationally hot $\nu_2'' = 1$ level should show a consecutive spacing of ν_2' . This means that at low temperatures when only the $\nu_2'' = 0$ state is occupied, any observed band spectra should have a spacing which is twice as large as the spacing of hot bands originating from higher temperatures.

4. Rotational Structuring^{97c}

The only discussion of rotational levels thus far has been the population of the different J quantum numbers as a function of temperature. For a linear triatomic of $C_{\infty v}$ symmetry, J is the only quantum number applicable to rotational structuring, and for this linear-linear transition,

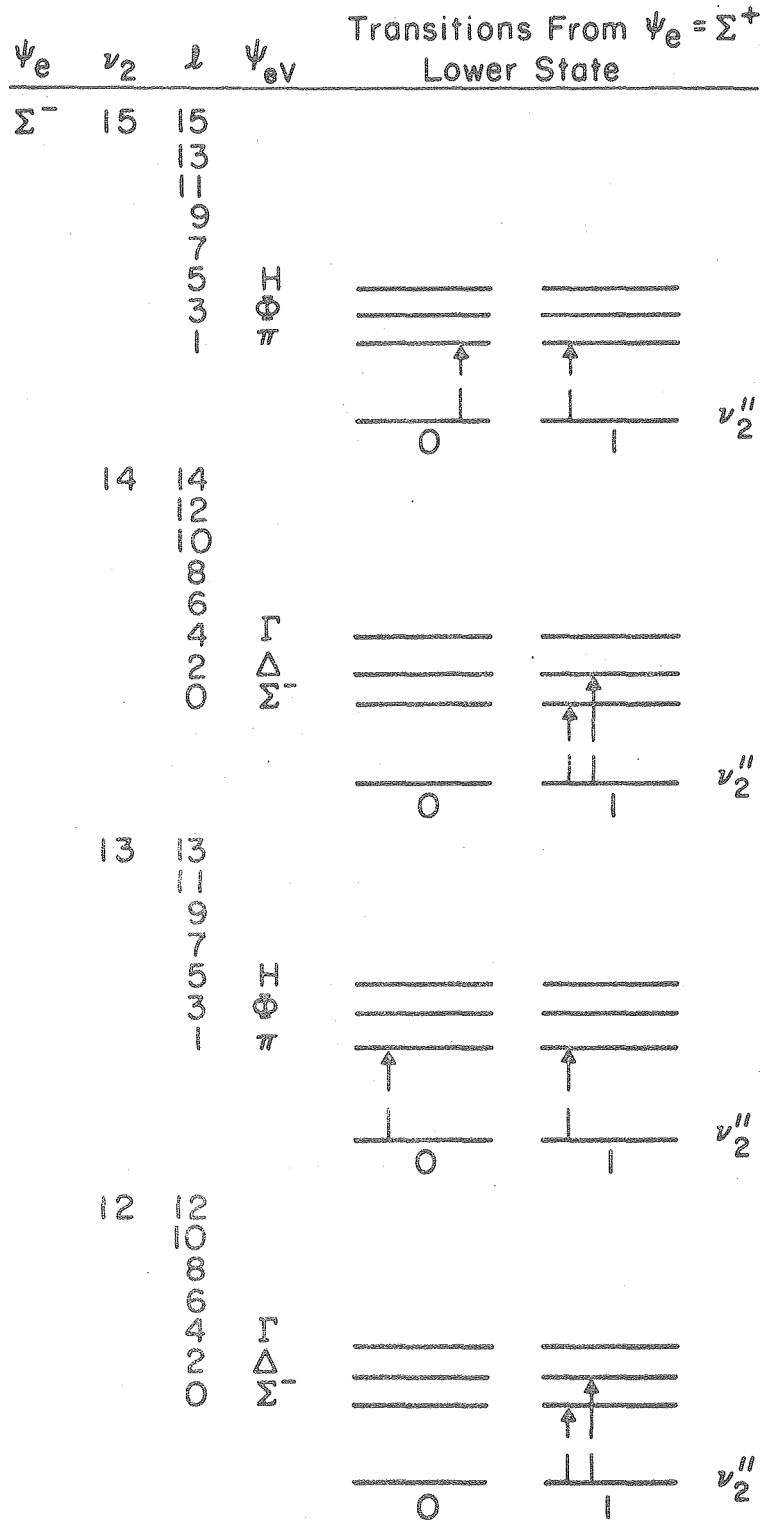
$$\Delta J = 0, \pm 1 \quad (J = 0 \nleftrightarrow J = 0)$$

with the usual selection rules for rotational symmetry,^{97c}

$$\begin{array}{ccc} + \leftrightarrow - & + \nleftrightarrow + & - \nleftrightarrow - \\ s \leftrightarrow s & a \leftrightarrow a & s \nleftrightarrow a \end{array}$$

here the + and - refer to the symmetry of the rotational level (to be distinguished from $^+$). These selection rules lead to

$$\begin{array}{ll} {}^1\Sigma^- - {}^1\Sigma^-, & \text{no Q, only P and R branch} \\ {}^1\Pi - {}^1\Pi, {}^1\Delta - {}^1\Delta, \dots, & \text{weak Q, P and R branch} \\ {}^1\Sigma^- - {}^1\Pi, {}^1\Delta - {}^1\Pi, \dots, & \text{strong Q, P and R branch} \end{array}$$



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Figure 13

Upon bending the molecule a second rotational quantum number arises, K, which is strictly defined only for a symmetric top. For nitrous oxide, as it is bent increasingly, the molecule less and less resembles a prolate symmetric top and becomes an asymmetric top molecule. Table 3 shows the three rotational constants, A, B, and C, for ground state N₂O for several bond angles. Kappa would be 1.0000 for a prolate symmetric top.

The rotational structure of an electronic transition between an upper electronic state which is bent in its equilibrium geometry and a lower electronic state which is linear, is determined by the selection rules for both the J and K quantum numbers. For the linear case, K represents the contribution of electronic and vibrational angular momentum,

$$K = |\Lambda + l|$$

where Λ is the electronic angular momentum and l is the vibrational angular momentum. For the ground electronic state of N₂O, $X^1 \Sigma^+$, $\Lambda = 0$ and so $K'' = |l|$. For the case of an electronic state which is slightly bent in its equilibrium geometry, K, the component of angular momentum about the top axis (i.e., the A axis for a prolate symmetric top), may also arise from the pure rotation of the molecule about its top axis. In this case, for each value of K there are a series of rotational levels with $J = K, K + 1, K + 2, \dots$

With K defined, the additional rotational selection rules for a bent-linear electronic transition are:

$$\Delta K = K' - K'' = 0 \text{ for } M_z \text{ (|| band)}$$

$$\Delta K = K' - K'' = \pm 1 \text{ for } M_x, M_y \text{ (⊥ band)}$$

plus the usual selection rules for J.

Under the instrumental conditions in this study, the resolution to reveal individual rotational features is not available. It is also likely that the structuring observed is predissociated, so that the fine structure may be smeared out and may not be observed, even with much higher resolution.

These selection rules state that from $v_2'' = 0$, only $K = 0$ for a \parallel transition or $K = 1$ for a \perp transition will be reached. That is, from the (000) level, the fine structure will appear the same as a linear-linear transition with only apparent selection from the J selection rules.

From $v_2'' = 1$, for a \parallel transition $K = 1$ will be reached in the upper state with fine structure arising from the J selection rules. A \perp transition of this hot band will have two sub-bands, the $K = 0, 2$ which will be separated by $4(A' - B')$. As seen in table 3 for a small bond angle, $A' - B'$ is quite large and this separation may be substantial. By observing this "coarse" structuring of the rotational features it may be possible to determine whether the transition moment is \parallel or \perp .

It should also be noted that for C_s symmetry a hybrid of \parallel and \perp transitions are possible. In this case, the rotational structuring would be the superposition of the two individual transitions with the relative intensities of each component depending on the projection of the transition moment on the principle axes. In this case, a more complicated spectrum results.

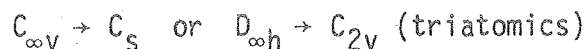
Table 3. N_2O Bond Angles and Calculated Rotational Constants, cm^{-1}
for N-N 1.185 Å and N-O 1.125 Å.

| NNO Bond Angle, deg. | Rotational Constants, cm^{-1} | | | |
|----------------------------|---------------------------------|--------|--------|--------|
| | A | B | C | Kappa |
| 180 | * | 0.4207 | * | * |
| 175 | 696.2 | 0.4215 | 0.4212 | 1.0000 |
| 170 | 174.4 | 0.4239 | 0.4229 | 0.9999 |
| 165 | 77.75 | 0.4280 | 0.4256 | 0.9999 |
| 160 | 43.93 | 0.4337 | 0.4295 | 0.9998 |
| 155 | 28.27 | 0.4413 | 0.4345 | 0.9995 |
| 150 | 19.78 | 0.4508 | 0.4407 | 0.9989 |
| 145 | 14.65 | 0.4624 | 0.4482 | 0.9980 |
| 140 | 11.33 | 0.4762 | 0.4570 | 0.9965 |
| 135 | 9.049 | 0.4926 | 0.4672 | 0.9941 |
| 130 | 7.421 | 0.5118 | 0.4788 | 0.9905 |
| 125 | 6.218 | 0.5342 | 0.4919 | 0.9852 |
| 120 | 5.304 | 0.5603 | 0.5068 | 0.9777 |
| 115 | 4.594 | 0.5906 | 0.5233 | 0.9669 |
| 110 | 4.033 | 0.6259 | 0.5418 | 0.9518 |
| 105 | 3.582 | 0.6670 | 0.5623 | 0.9306 |
| 100 | 3.214 | 0.7150 | 0.5849 | 0.9010 |
| 95 | 2.912 | 0.7714 | 0.6098 | 0.8596 |
| 90 | 2.660 | 0.8378 | 0.6372 | 0.8016 |

Kappa indicates how closely the molecule approaches a prolate symmetric top.

5. Change of Symmetry during Transition⁹⁸

Implicit in the foregoing discussion was the assumption that in both upper and lower electronic states the symmetry class remains the same. For linear triatomics especially, this is often not the case. CO_2 , HCN , CS_2 , and OCS are all believed to change to bent symmetry in their excited electronic states,⁹⁷ and the evidence is quite strong for a similar change of symmetry for N_2O . For a change of bond angle, the resulting symmetry class is



Evidence for such a symmetry change can be unambiguously obtained from the rotational structuring of the transition. In the absence of such rotational information, the vibrational progression pattern may also provide evidence for such a symmetry change. If the allowed electronic transition is between two different symmetry positions, the vibrational selection rules are determined by the symmetry elements common to both equilibrium positions. Thus, for an allowed $C_{\infty v} - C_s$ symmetry change the resulting vibrational selection rules are less restrictive than in the linear to linear case, and the bending vibration, asymmetric for a linear molecule, is considered now a symmetric vibration in the common symmetry class.

Consider then the vibrational selection rules for a progression in the bending mode of a triatomic^{97h}, ν_2 : if the transition is between two linear species, the selection rule for such as asymmetric vibration predicts $\Delta \nu_2 = 0, 2, 4 \dots$ with the $\Delta \nu_2 = 0$ transition the most intense. For a bent-linear transition, the selection rule for the symmetric bending vibration predicts a consecutive progression, or

$\Delta v_2 = 0, 1, 2, 3 \dots$. For such a transition, the most intense peak will not necessarily be $\Delta v = 0$ (see below).

Note that in the case of the vibronically induced transition as in the previous example of $1\Sigma^- \rightarrow 1\Sigma^+$, a consecutive progression in v_2' originating from $v_2'' = 1$ or $v_2'' = 2$ results, but from $v_2'' = 0$ (or from (000)), the selection rule^{97d} is $\Delta v_2 (v_2'' = 0 \text{ only}) = 1, 3, 5 \dots$. Thus, the presence of a consecutive progression of v_2' in the hot bands ($v_2'' = 1, 2 \dots$) is predicted for both the case of a bent-linear change of a symmetry, and for the case of the vibronically induced transition, and on this basis alone it is not possible to distinguish the two mechanisms unambiguously. However the progressions originating from $v_2'' = 0$ (or (000)) in the vibronically induced case, predict a spacing of $2v_2'$, whereas for the case of a change of symmetry, the symmetric v_2 mode of the upper state would show a consecutive spacing of v_2' , as would the hot bands. Other symmetric vibrations for the bent-linear transition will also of course show a consecutive spacing in v' .

The above discussion has dealt with the consideration of an allowed bent-linear transition and of a vibronically induced transition with no explicit mention of symmetry change. For the additional case of a bent-linear transition which is only allowed in the bent case, a slightly different situation arises. In this last case, although the product resolution of R into $R_{e'e''v'v''}$ is not strictly valid, it is useful to a first approximation provided that $R_{e'e''}$ is also considered a function of nuclear coordinates. The usual interpretation of the Franck-Condon principle in such a case would predict that the

vertical transition to the central maximum of the upper state bending potential would have the strongest intensity. For this resulting upper state configuration of 180 degrees, the $R_{e'e''}(q,Q)$ is small, and so this vertical transition is actually weak[†]. Instead, $R_{e'e''}(q,Q)$ will be large for a significant change in bond angle, or a non-vertical transition for which $R_{v'v''}(q)$ will be small. Clearly, the maximum of intensity of such a transition occurs at some point between the high energy limit (vertical) and low energy limit (non vertical) since for $R_{e'e''} \times R_{v'v''}$ the first product increases with bending angle whereas the second product decreases^{97d}. Note however, that in a plot of potential surfaces of another vibrational mode, as in the ν_1 stretch, the usual principle of vertical transitions would still apply for that dimension.

[†]See figure 68 of Herzberg, Vol. III (Ref. 97)

6. Intensities of Continuous Absorptions^{97e,92b}

For continuous transitions between two electronic states, the wavelength dependent intensity is given by

$$I_{\text{abs}}(\lambda) \propto \nu \left[\int \psi_V' * \psi_V'' d\tau_V \right]^2$$

where ν , the energy, is derived from the energy dependence of the Einstein coefficient, B , and weights the overlap integral. For a polyatomic molecule, the vibrational eigen functions of the upper and lower electronic states, are a function of all $3n-6(5)$ normal coordinates. If ψ_V'' is a low energy vibration such a (000) or (010) the wavefunction of these vibrations is easily obtained. For high energy vibrations in ψ_V' however, a much more complicated expression results and a delta function may be used to represent ψ_V' which is different from zero only at the classical turning point. With this approximation,

$$I_{\text{abs}}(\lambda) \propto \nu (\psi_V'')^2$$

This result predicts an intensity distribution of a continuous absorption from $\nu = 0$ which appears as an energy weighted probability distribution of the $\nu = 0$ vibrational level.

For ψ_V'' being the (000) state, this gives an energy weighted Gaussian type curve for the continuum intensity distribution.

7. Intersection of Potential Curves^{97f}

For diatomics the "non-crossing rule" in which potential curves of the same electronic species cannot cross, is well known and its proof readily available¹²⁷. In polyatomic molecules with additional degrees of freedom, however, energy surfaces can intersect even if they have the same symmetry and spin multiplicity. Herzberg and Longuet-Higgins⁹⁹ have studied this question for triatomics and have provided an example of the resulting conical intersection of HNO potential curves.

In the example of HNO, a repulsive $^1\pi$ state is formed from the $H(^2S)$ and $NO(^2\pi)$ components which may cross the bound $^1\Delta$ state formed from $H(^2S)$ and $NO(^2\Delta)$. Both these states are bent and since they are degenerate in the linear case, they will both split into $^1A'$ and $^1A''$ components in C_s symmetry. Crossing of the two states must occur because $NO(^2\Delta)$ is higher in energy than $NO(^2\pi)$, yet the HNO $^2\Delta$ state has a minimum below the $^2\pi$ state of HNO. This crossing can only take place at the point of intersection of the linear species. Once bent, the $^1A'$ components of the two species mix and the $^1A''$ components may also mix.

It is for this reason that HNO may be formed adiabatically from ground state $NO(^2\pi)$ and H in all orientations except the linear approach. In summary, for triatomics, intersection of two states of the same symmetry may occur at a point, the vertex of the resulting double conical intersection, but may not occur along a line.

A variation of this principle which is applicable to nitrous oxide will be presented in a later section.

C. Experimental

1. Instrumental Procedures

As before, spectra were obtained with the UV extended Cary 118C spectrophotometer. To overcome some of the purging problems noted in the previous section, it was necessary to design purging modifications and construct a different quartz cell. The deuterium lamp was rigidly mounted to the spectrometer and sealed with an o-ring to prevent purge leakage. This avoided the major source of leakage in Section III and was not prone to rapid deterioration. The main chamber of the monochromator was resealed by replacing the gasket material at the metal joints and by taping over the seals with 2" black photographic tape. Instead of purging the entire sample compartment, as was done in Section III, nylon tubes with sponge rubber gaskets connected the cell to the spectrometer and provided a small, tight purge connection for the light path. As before, complete purging required two days prior initiation, but improvements from these modifications reduced the level of noise significantly and permitted operation down to 171 nm.

Several different instrumental parameters were tested; the best results were obtained with a scan speed of 0.01 nm sec^{-1} and with the slits set at 0.06 mm to give an average spectral band width of 0.05 nm. Data points were taken every 0.02 nm over the range 190 to 172 nm. All data in this section was collected using a time constant of 5 seconds and was stored on both chart paper and in the Fabritek. Signal averaging was carried out over four runs for both background and sample spectra for each temperature.

2. Quartz Cell Design

A single quartz cell was used for the spectra obtained in this section and it is shown schematically in figure 14. The cell consisted of a 2.2 x 10 cm quartz cylinder with fused suprasil windows (1/16" thick) which contained the gas. The cell could be used in a flow or static manner but all spectra were collected in the static mode. A quartz jacket fused to the inner cell was used for temperature control and a second quartz jacket surrounding the entire assembly also with 1/16" thick suprasil windows was evacuated to 5×10^{-6} torr, sealed in vacuum, and provided thermal insulation.

Platinum wire was spiraled about the inner cell and was fed up the quartz tubing connected to the cooling jacket, past the quartz-pyrex graded seal and was welded to two tungsten electrodes. These electrodes, fused through the pyrex section with uranium seals, provided electrical connection to the wires, which served as built-in heaters. This was convenient for vacuum bake-out and for recording spectra at elevated temperatures. Platinum was necessary to withstand the heat generated in working the quartz. A wire thickness of 0.01 inches was chosen to increase the resistivity of the heaters, smaller diameter proved impractical for glass blowing. The resistance of the built-in heater was about 10 ohms and by simply using an ac rheostat it was possible to control the temperature of the cell. The maximum possible bake-temperature without damage to the cell or heaters was about 660 K. The maximum practical temperature for recording spectra was lower, about 520 K, owing to interference from black body radiation generated by the wires.

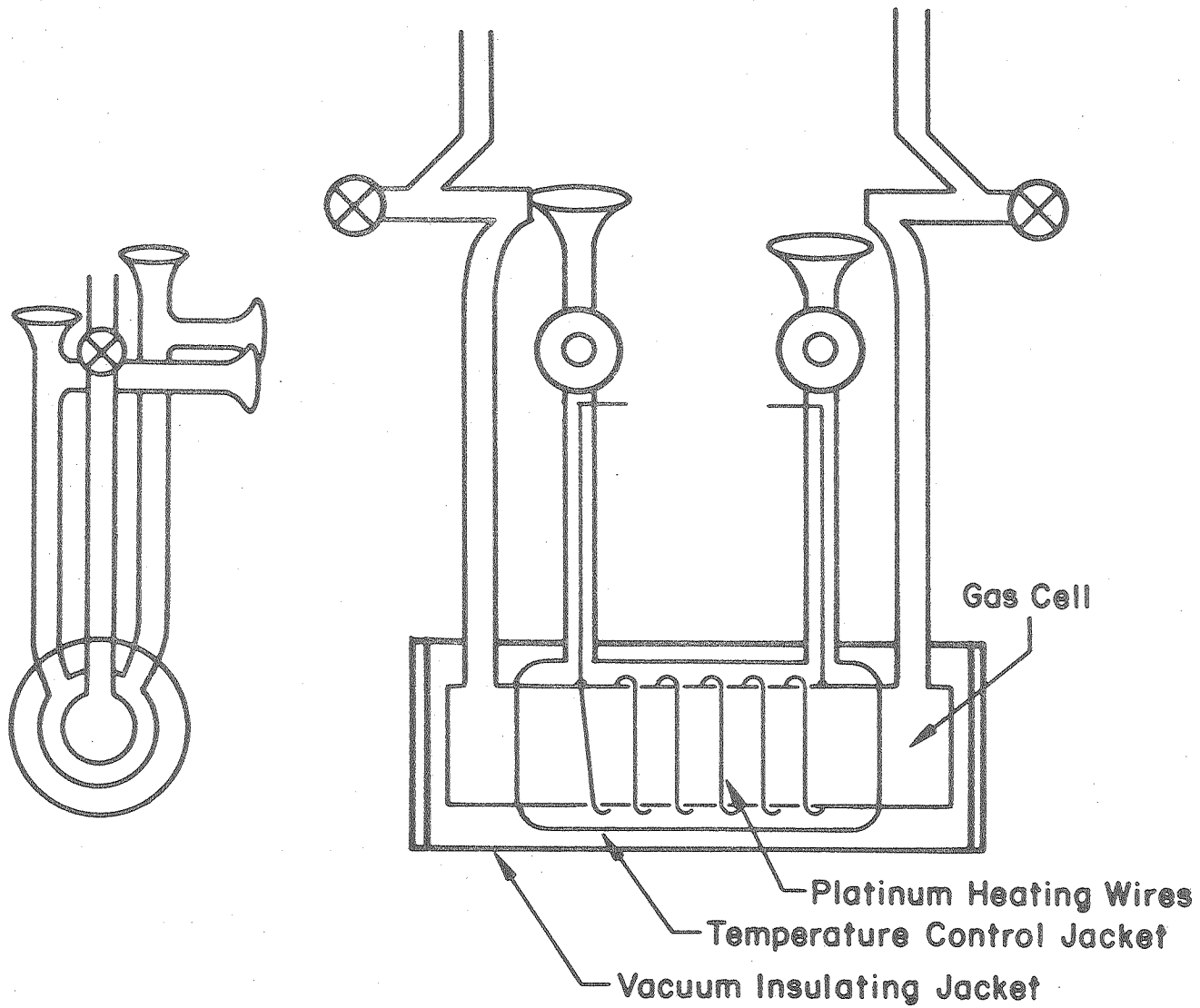


Figure 14

XBL 792-8344

Fluid was contained in the inner jacket for temperature control. For temperatures above 373 K, Dow Corning Silicone Oil was used and was heated by the Pt wires. This provided more uniform temperature control than heating an air space. For temperatures between 373 and 243 K, a Neslab model RTE - 9 thermostated circulating bath was used to flow water or methanol through the jacket. For temperatures between 243 and 200 K a Neslab double stage refrigerating bath, model LT - 9, was used to circulate methanol through the jacket. For temperatures below 200 K, a stream of cold nitrogen gas from a liquid nitrogen dewar was used to cool the cell, as in Section III. The lowest practical temperature to record spectra of nitrous oxide was determined from its equilibrium vapor pressure. To ensure enough optical density for accurate measurements, this was at about 151 K which has a vapor pressure of 28 torr.¹⁰⁰

3. Temperature, Pressure and Wavelength Measurement

Pressure was measured by a 100 torr factory calibrated MKS Baraton capacitance manometer with a stated accuracy of 0.05%. Pressures used varied from 5 to 45 torr at the temperatures studied. Before recording pressure of the gas, several minutes were allowed for temperature and pressure equilibrium to be reached. The nitrous oxide was purified in the manner described in Section III and the tests of purity performed in that section did not reveal any impurity in this case as well.

Temperature was measured by two calibrated iron-constantan thermocouples in contact with the inner cell. The thermocouples were fed through the same tubing as the Pt wires and so it was necessary to

insulate the Pt wires with a length of quartz capillary tubing. A 1000x amplifier with a digital voltmeter was used to measure the thermocouple output which was referenced to an ice-water bath. No significant deviation from standard tables of thermocouple emf¹⁰¹ was noted over the temperature range 78 to 490 K. Equilibrium vapor pressures of nitrous oxide at temperatures below 183 K provided a convenient check on both thermocouple and pressure measurement.

The use of two thermocouples, one at the fluid entrance and one at the fluid exit in the temperature control jacket, provided an estimate of the temperature differential in the cell. The observed temperature differential varied with the means of temperature control. When liquid nitrogen was used, an average temperature differential of 5 K resulted. The two thermostated circulating baths provided the best results with a differential of less than 0.5 K. Heating the silicone oil resulted in a higher temperature differential of about 10 K.

As in Section III, wavelength calibrations were checked by adding O₂ to the cell and observing the rotational structure of the Schumann-Runge oxygen bands.⁹⁴ Wavelength accuracy in this section is believed to be 0.05 nm.

The data stored in the PDP 8L was output in the form of paper tape and transferred to the Lawrence Berkeley Laboratory CDC-7600 computer. The most reliable means of transferring the data was by running the paper tape through a hard wired teletype located in the Vista Room. In this manner the data was converted into punch cards and further processing, graphics and corrections were possible.

4. Meter Vacuum Spectrometer

To check for the effect of lower pressures and higher resolution, the main chamber of a 3 m MacPherson monochromator, model 241, was evacuated and filled with 50 - 250 microns of nitrous oxide.

The spectrometer was an Ebert mount type with an aluminum, 1200 lines mm^{-1} concave grating, which was used in the first order to give a dispersion of $2.7 \text{ \AA} \text{ mm}^{-1}$. The highest resolution used in these experiments was 0.03 \AA , or about 1 cm^{-1} at 180 nm.

An air cooled deuterium discharge lamp provided a uniform continuous light source at wavelengths above 150 nm, below this, intense line spectra from the source made data collection impossible.

Plate exposures using Kodak SWR film were taken at intervals of up to eight hours. Since this was a vacuum spectrograph, it was possible to seal in the gas; only on one occasion was leakage a problem as evidenced by the presence of the sharp Schumann-Runge lines of oxygen. Densitometer tracings of the plates also revealed N_2O banding, but did not show noticeably more detail than the room temperature results obtained with the Cary, this was probably because noise reduction was not possible on the MacPherson spectrograph and the plates are inherently less sensitive than a photomultiplier.

D. Data Processing and Graphics

1. Techniques

The data collected on a time basis by the Fabritek corresponded to a linear wavelength scale on the Cary, and was converted to a wavenumber basis by use of the formula,¹⁰²

$$\nu = 10^7 (\eta\lambda)^{-1}$$

Here, the index of refraction of nitrogen, η , was taken to be 1.00035, and λ is the wavelength in nanometers.

Gas concentration was calculated by using the ideal gas equation. To avoid error in using this equation, experimental conditions near critical points were not used.

After signal averaging was completed for both the sample and background spectra, and the normalized background spectrum was subtracted from the normalized sample spectrum, a three point digital smooth of the type

$$\sum_I Y(I) + Y(I-1)/4 + Y(I)/2 + Y(I+1)/4$$

was applied to the final result. Since the three data points covered 0.06 nm and the resolution was 0.05 nm, it was not felt that information would be lost in this smoothing process. Comparison of the spectrum before and after smoothing did not reveal any noticeable differences except for reduction in the high frequency noise background.

2. Graphics

The quantitative data set at eleven different temperatures served as the experimental basis for the analysis to be discussed in the next subsection. In doing this programming analysis, it was of invaluable aid to have a graphical display of the calculation results. This

was made possible by the use of the graphics package available at LBL. The graphics routine IDDS was used for drawing the figures and slides along with on-line display units such as the Tektronics 4014 CRT display and with either calcomp or microfilm hard copy units.

The graphics program allows for variable scaling and size of output, and either plots points using two dimensional variable arrays or connects the points to give lines. Because the data points are close the plots appear smooth. For most spectra shown in this section, computer-generated 35 mm frames were photographically enlarged to give the figures, labels and plots.

All programming was done in Fortran IV with most programs run as batch jobs, although for some uses interactive programming was found to be more useful. In the appendix, two programs are listed.

3. Scale of Figures

It was found to be convenient to express the data in linear multiples of 10^{-19} cm^2 cross section. For this reason, all spectra in this section express the cross section (CSN) in units of 10^{19} cm^2 in the ordinate axis, and the abscissa axes of all figures have the same linear range of wavenumbers, cm^{-1} , corrected for vacuum. Care is necessary in the examination of these figures since the scaling of the ordinate axis varies from 0 to $5 \times 10^{-19} \text{ cm}^2$ in one case to 0 to 0.3 or 0.8 to $1.2 \times 10^{-19} \text{ cm}^2$ in other cases, as is needed to show the necessary detail.

The intensities of all data presented are quantitatively accurate to about 4% in absolute absorption cross sections, and the relative error of peak intensity is about 1%. For quantitative comparison

of the difference spectra only the relative intensity of peak-trough may be used.

It may be useful to compare the intensities given here with the approximate spectral intensities of other molecular absorptions:^{78a}

| | |
|---|---|
| O ₂ : maximum of Schumann-Runge continuum, | 1.3 x 10 ⁻¹⁷ cm ² |
| Herzberg continuum at 230 nm, | 2.3 x 10 ⁻²⁴ |
| SchumannRunge band structure, max. | 1 x 10 ⁻¹⁹ |
| O ₃ : maximum of Hartley band, | 1.1 x 10 ⁻¹⁷ |
| maximum of Chappuis band, | 5 x 10 ⁻²¹ |
| H ₂ : Lyman , | 4 x 10 ⁻¹⁶ |
| SO ₂ : maximum at 285 nm, | 1.0 x 10 ⁻¹⁸ |
| CO ₂ : maximum at 147 nm, | 7 x 10 ⁻¹⁹ |
| CCS: maximum at 223 nm (room temp), | 3 x 10 ⁻¹⁹ |
| N ₂ : rayleigh scattering at 300 nm, | 2 x 10 ⁻²⁵ |

To convert from absorbance coefficient, cm⁻¹ to cross section, cm², divide by 2.5 x 10¹⁹.

E. Results

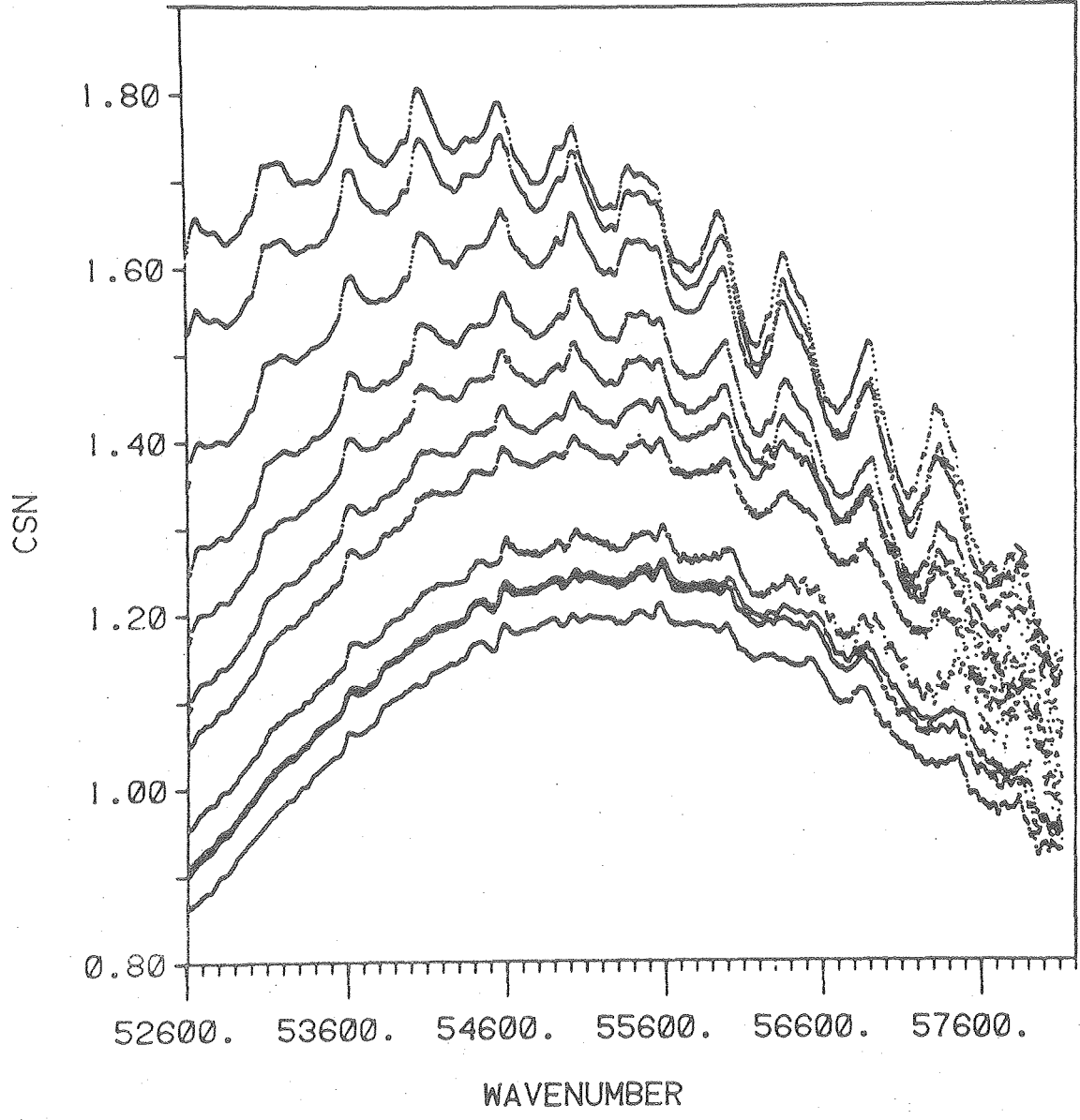
1. Temperature Effect on the Structured and Continuous Absorption

The composite profile of the absorption spectrum at eleven different temperatures from 151 to 485 K is shown as figure 15. The cross sections are believed accurate to 4%. At all temperatures a banding progression is seen superimposed on a continuous background, although at higher temperatures the banding is most pronounced. The increase in absorption in intensity and to longer wavelengths with increasing temperature has been observed by Holliday and Reuben¹³.

The temperature profile shows that many of the observed broad peaks and shoulders are really composites of overlapping peaks which are resolved at lower temperatures. The effect of temperature is seen to be most pronounced on the peak structuring. The rate of temperature dependent increase varies among different members of the banding. The feature at 53200 cm^{-1} at 485 K is seen to be composed of three different peaks; at 151 K the high energy member is most intense, but at increasing temperatures, the low energy member increases rapidly and becomes predominant. The effect of temperature on the apparent underlying continuum is most noticeable at longer wavelengths.

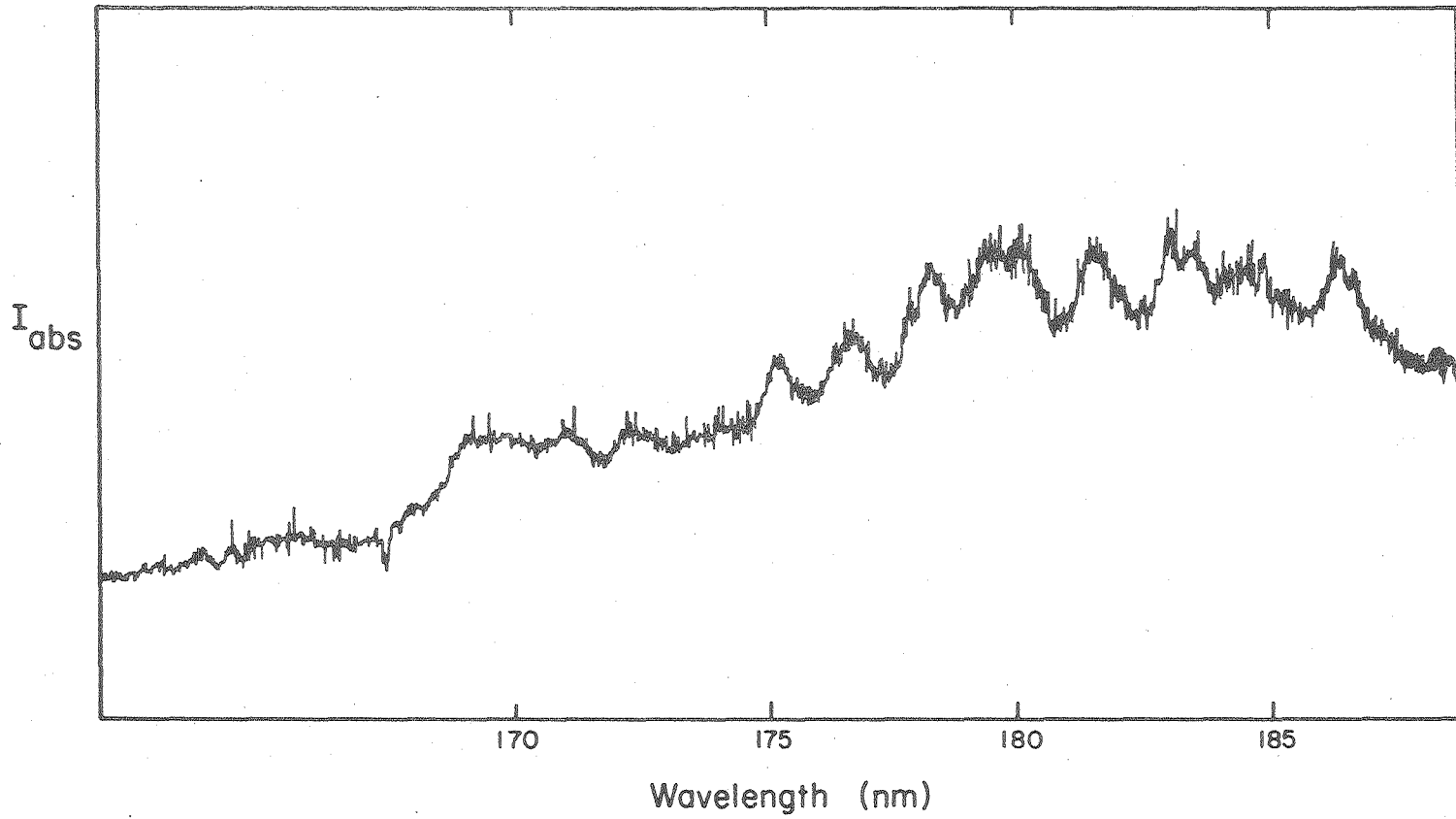
2. Three Meter Spectrograph

The room temperature spectrum taken on the 3 m vacuum spectrograph is shown in figure 16. It is clear from this figure that the structuring continues at wavelengths below the limit of the Cary spectrometer. Since plates were used, only approximate relative intensities can be estimated.



XBL 792-8250

Figure 15



XBL 792-8574

Figure 16

F. Discussion

1. Contribution of Cold and Hot Bands of $X^1\gamma^+$

Using the fundamental vibrational frequencies of nitrous oxide (1285, 589, 2224 cm^{-1}), it is possible to calculate the fractional population of vibrational states in the ground electronic state for any given temperature⁹⁵. Since at the lowest temperature studied, 151 K, only 0.7% of the molecules are in the (010) state, this spectrum provides a good approximation to the spectrum of the "pure" (000) state. Weighting this spectrum by the fractional (000) population for each of the five highest temperatures studied, and subtracting the resultant spectral contribution of the (000) molecules from each of these five highest temperatures, the difference spectra obtained represent the spectral contributions of all the vibrationally "hot" molecules at these temperatures. It is possible to identify which active vibration or vibrations are responsible for these difference spectra by dividing the difference spectra by the fractional equilibrium populations of (010), (020), (100), (110), (001) and so on. Only for the (010) state with its activation energy of 589 cm^{-1} are the normalized "hot" spectra consistent and in agreement for all five highest temperatures. Applying the same procedure but using an activation energy of $2\nu_2$ or ν_1 yields widely varying normalized results for each of the five highest temperatures indicating these modes could not be primarily responsible for the observed temperature effect. Use of colder spectra for the derivation of the hot bands is less reliable due to the large error incurred by dividing a smaller temperature effect by a very small number.

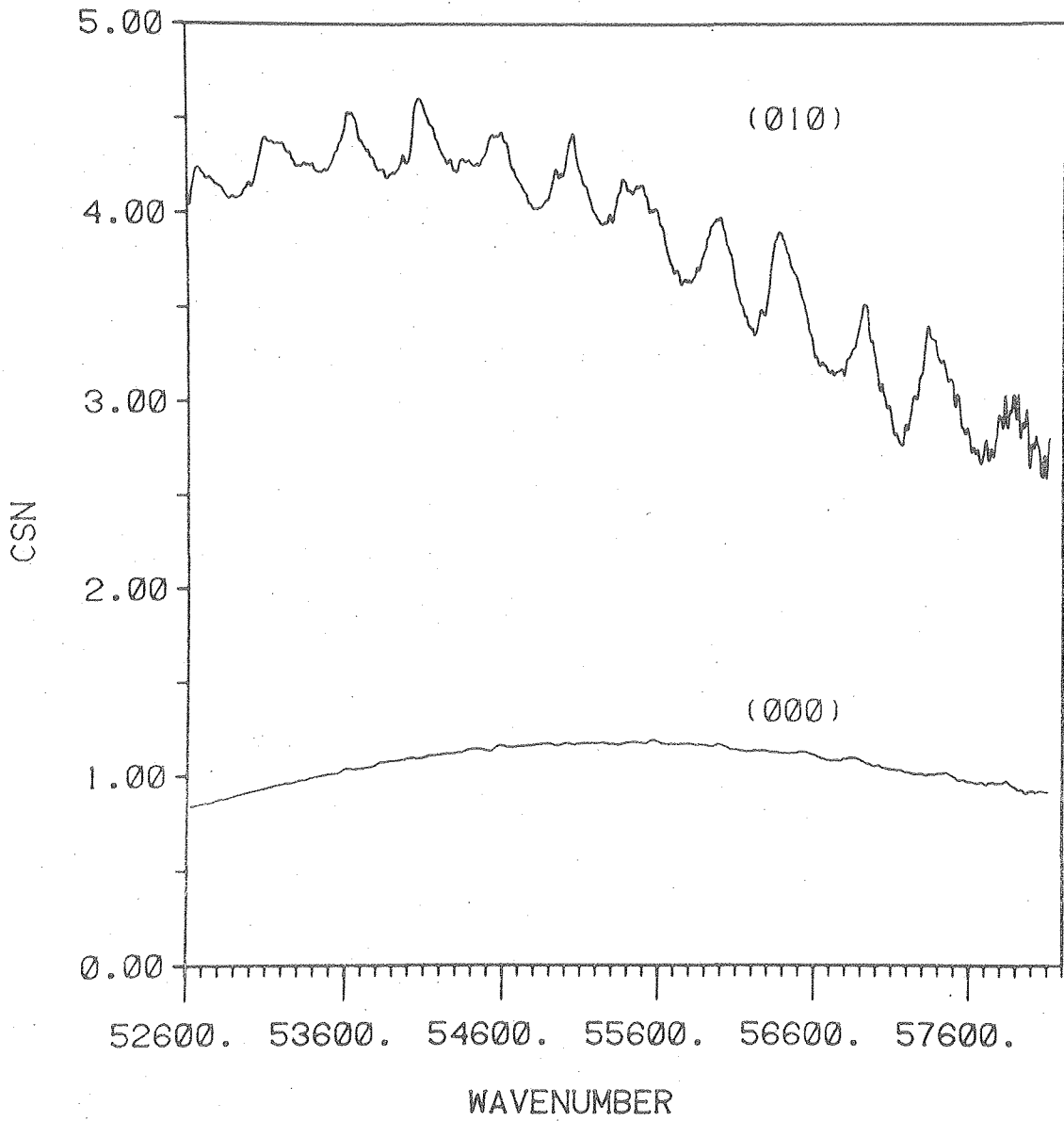
The process may be summarized by use of the simple formula:

$$B(\lambda) = \frac{Y(\lambda, T) - a(T)A(\lambda)}{b(T)}$$

where A and B are the spectra of the (000) and (010) states respectively for 100% occupancy, Y is the observed spectrum at temperature T, and a and b are the fractional equilibrium populations of (000) and (010) at T. The first iteration provides an approximation to the (010) state spectrum, which is then used to correct the 151 K spectrum for the spectral contribution of the 0.7 per cent of (010) molecules present. The process is then repeated through an iterative procedure and convergence occurs quickly with the final result shown in figure 17.

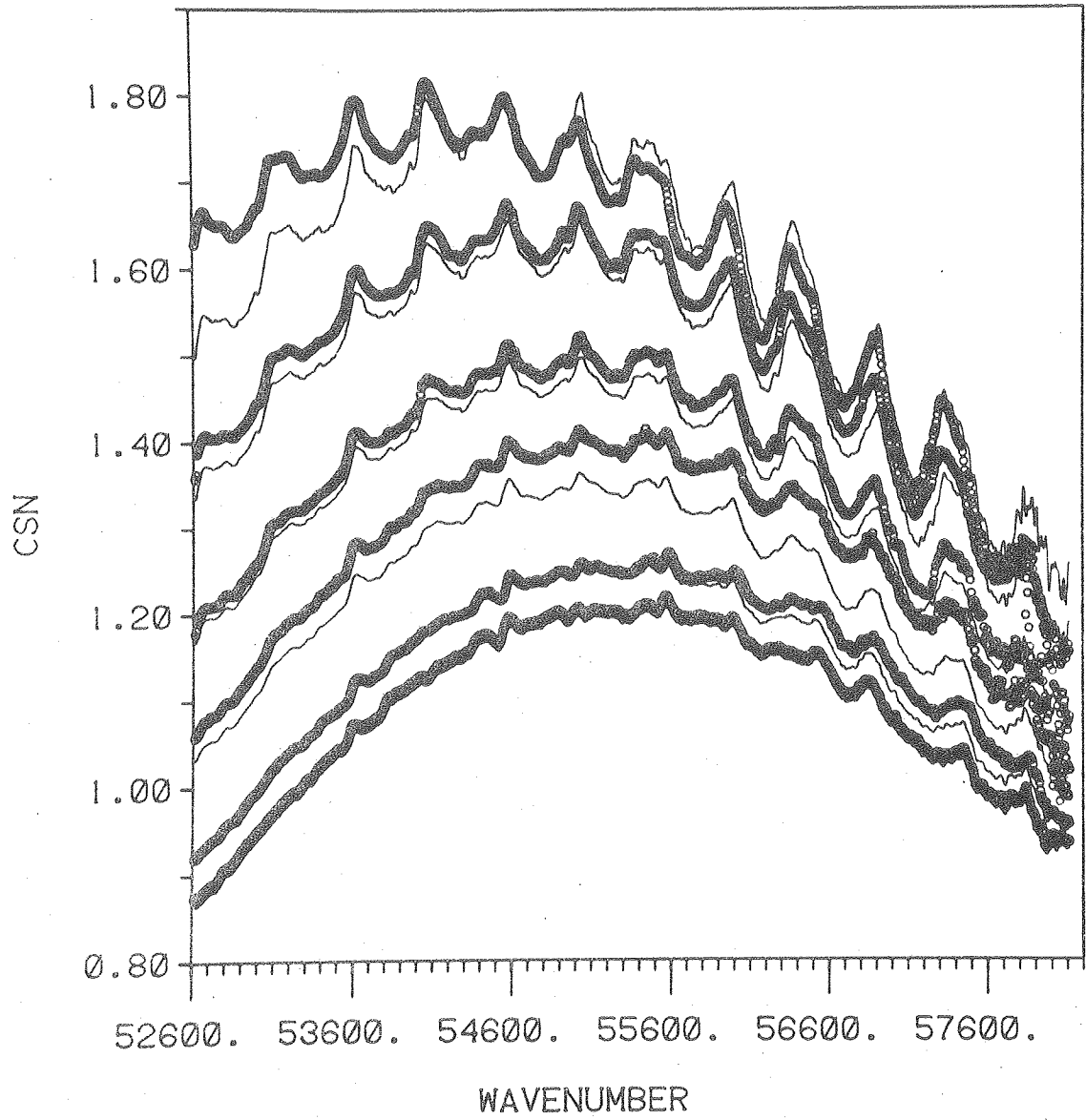
The large affect of the bending vibration is very apparent in figure 17. Most of the structuring is seen to result from the excitation of the bending vibration although a small amount of structuring is seen in the pure (000) spectrum. The observed continuum is also enhanced and is red-shifted somewhat from the maximum of the (000) spectrum. The presence of a vibrational progression is noted in the (010) state spectrum, but this will be addressed later.

The reverse procedure of weighting each state spectrum by the fractional population of (000) and (010) for a given temperature and convoluting, allows a comparison of this composite spectrum with the observed spectrum over a wide temperature range. For clarity, in figure 18, the composite spectrum (solid lines) is compared with the observed spectrum (data points shown) for every other temperature studied. Figure 18 shows good agreement at some temperatures and fair agreement at other temperatures. Of the eleven temperatures studied, two were used to derive the state spectra and therefore are not independent



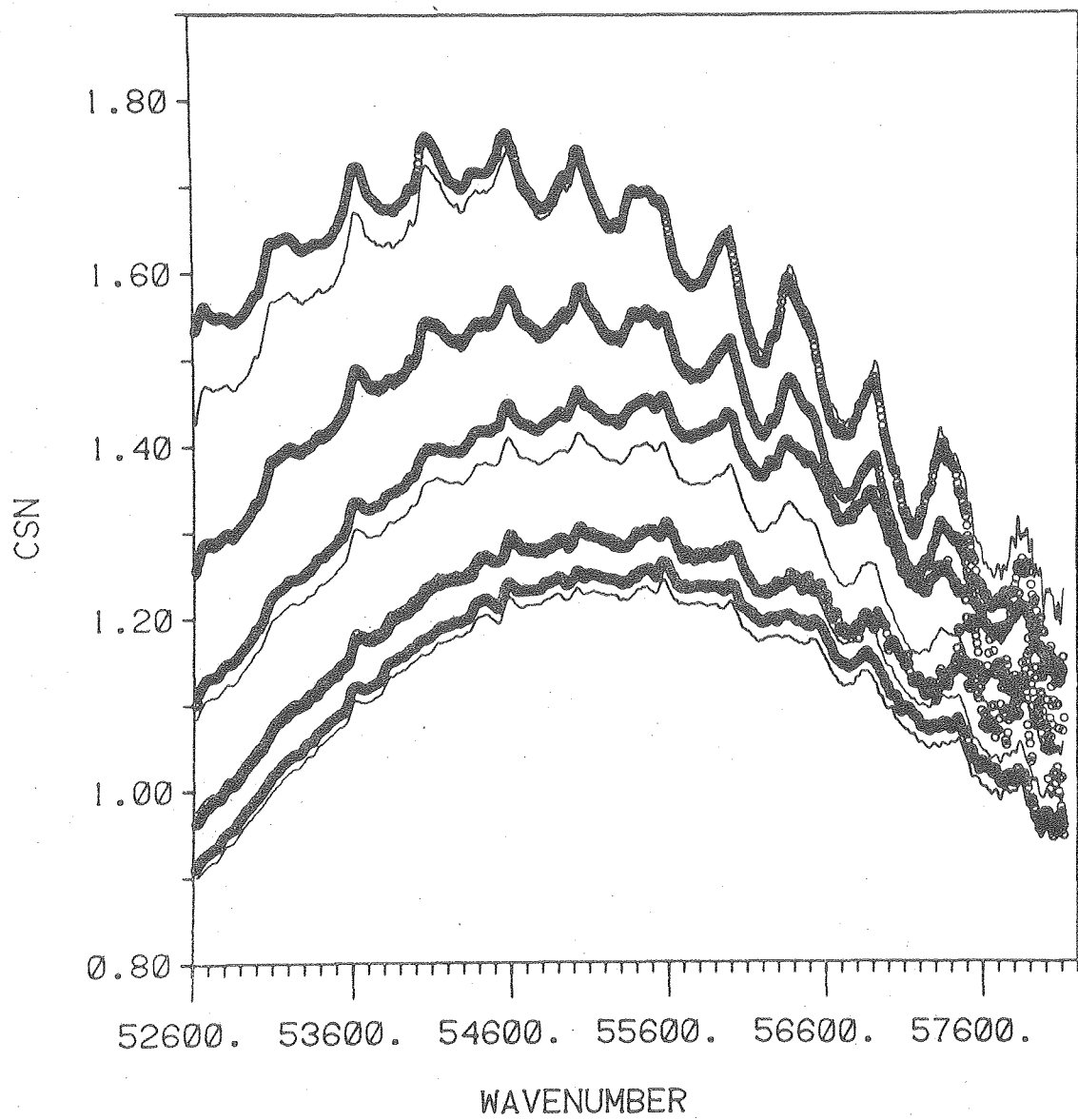
XBL 792-8249

Figure 17



XBL 792 8246

Figure 18a



XBL 792-8247

Figure 18b

comparisons by this method. Table 4 lists for every temperature studied the correlation coefficients,¹¹⁶ which measure shape similarity but are insensitive to a constant displacement. In this table, the two temperatures used in the derivation of the two state spectra will necessarily yield a correlation coefficient of 1.0000, but the correlation coefficients of the other nine temperatures demonstrate that the convoluted spectrum closely approaches the actual absorption spectrum.

From figure 18, we see that this method tends to underestimate the absorption at the highest temperature, 485 K, because at this temperature this method ignores the increasingly substantial population and spectral contribution of higher vibrational species. Similarly, in the derivation of the (010) state spectrum, this method unavoidably includes the interfering contribution of the (020) state spectrum present from the small equilibrium population of (020) at this temperature, and so at lower temperatures where there is essentially no (020) population, this convolution tends slightly to overestimate the absorption.

The overall conclusion from the agreement shown in figure 18 and table 4 is to confirm the assignment of ν_2 , the bending vibration, as the "active" vibration which is responsible for the bulk of the observed temperature dependence in figure 15. Had it been the small population of another vibration, say (100) or (001) and their respective energies of activation governing the rate of temperature dependent increase of the spectrum, then this process would not converge for this noticeably different activation energy of the vibrational mode. The further result that the two state spectra and their respective activation energies may be used to predict the spectra at temperatures

other than was used in their derivation, supports the assignment of these state spectra and their shape and intensities.

2. Second Order Approximation to the Hot Bands

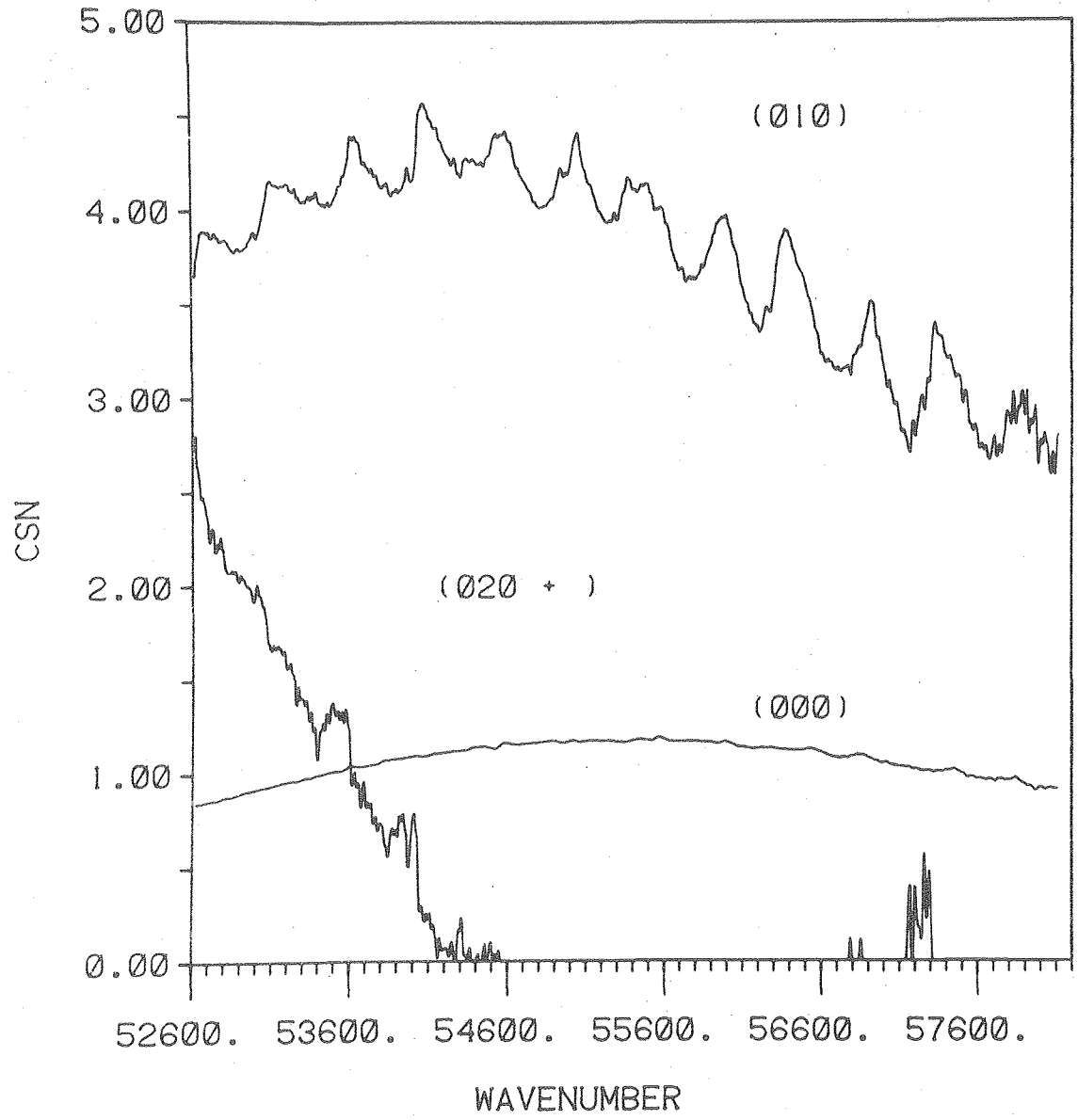
In the derivation of the (010) state spectrum it was assumed that only two primary absorbing species were involved in the absorption spectrum: the (000) vibrational mode and a single hot band. This hot band was identified as the (010) vibrational mode because only for this respective activation energy was convergence of the normalized state spectrum achieved for several temperatures. It was also noted in the preceding discussion that the derived (010) spectrum was likely to contain some character of (020) because the iterative method used could not separate three contributing species. The (020) interference is probably not too great because the (020) population is about 1.5 percent compared to the 13.3 per cent population of (010) at 333 K. Unlike (010), the (020) state will be split into one component with two quanta of angular momentum, (02^2_0), and one without net angular momentum, (02^0_0). The ψ_{ev} of the (02^0_0) state is $^1\Sigma^+$, and since it has not net angular momentum, it is likely that the spectrum of this state will be weak, perhaps weaker than the (000) state spectrum. This is because its probability amplitude is shaped more sharply about 180° than (000) and so for a bent-linear transition, the $R_{e'e''}(q,Q)$ factor of the transition moment will be smaller. (This is assuming that the transition is forbidden in linear case, but is allowed in a bent configuration. More evidence for this will be presented.)

The (02^2_0) state with an ψ_{ev} of $^1\Delta$, has a net quantum of angular momentum. It is then likely to resemble the (010) state spectrum in intensity and may in fact be stronger due to its greater equilibrium bond angle. The population of (02^2_0) at 333 K is about 1 per cent

which makes for an expected relative error of about 7 - 20% in the derived (010) spectrum depending on the extent of the (02⁰0) contribution and the wavelength examined.

By supplementing the previous method with an additional tier, it is possible to partially correct the (010) state spectrum for the interference of these higher order vibrations, particularly the bending vibrations. The disadvantage of this second order approach is that in solving for higher order vibrations which have very small populations and similar spectra, as in the case of (020) and (030), the final, normalized result of these spectra becomes increasingly unreliable and noisier. Specifically, in this case we are solving for 3% of the molecules at 485 K, so the degree of instrumental noise and the accuracy of data becomes extremely critical to the final result. It is unreasonable to expect then that the resulting normalized (020) and (030) state spectrum to accurately reflect the actual spectra of these higher order vibrations, but the use of this result in partially correcting the (010) state spectrum for higher order contributions is more reasonable. This is because the (010) spectrum derived previously contains only a 1% contribution of the normalized state spectra of these higher order vibrations.

Figure 19 shows the result of this second order iterative procedure. In deriving this result, three temperatures were used, 151, 333, and 485 K, to derive the (000), (010) and ((020) + (030)) state spectra. It is seen that the contribution of the higher order vibrations is most noticeable at longer wavelengths. It is not known whether the contribution of these higher order vibrations is negligible at short



XBL 792-8251

Figure 19

wavelengths, as this result appears to show, or whether this result indicates an intrinsic failure of the method. Only a small portion of the higher vibrational spectrum is seen; this may indicate a maximum at much longer wavelengths (as demonstrated in Section II, the absorption of nitrous oxide extends to about 260 nm) although this is not possible to tell with the limited data base of this section. As expected, the (000) state spectrum is unchanged by this second order approach; the population of (020) at 151 K is about 4×10^{-3} per cent. The (010) state spectrum is unchanged at the short wavelengths, but at longer wavelengths the overall absorption is noticeably reduced, resulting in a sharper maximum than the overall appearance of the result which indicated a slightly sloping, flat maximum. Convolution of the three state spectra to give a composite spectrum gives an improved fit to the observed spectra, as indicated in figure 20 and table 4. Again, since three temperatures in this case were used to derive the state spectra, these are not independent measurements, but comparing the correlation coefficients in table 4, the improved fit of the second order approach can be seen for the other eight temperatures.

The logical process used to derive the three state spectra is outlined on the following page.

Use of higher temperatures than 485 K to derive the state spectra of higher order vibrations, was considered but rejected because the (100) state would also become occupied at nearly the same rate, as would (030) and so higher temperatures would only complicate the result increasingly. A more reasonable approach might be to cross the gas sample with a tuned, high power IR laser to selectively excite normal

Table 4. Comparison of the Correlation Coefficients of Convolutated and Observed Spectra for Each Temperature.^{38a}

| Temp., K | First Order | Second Order |
|--------------------------|------------------|------------------|
| | <u>Iteration</u> | <u>Iteration</u> |
| Correlation Coefficients | | |
| 151 | 1.0000 | 1.0000 |
| 182 | 0.9991 | 0.9992 |
| 196 | 0.9926 | 0.9935 |
| 223 | 0.9571 | 0.9619 |
| 247 | 0.9954 | 0.9963 |
| 268 | 0.9797 | 0.9812 |
| 301 | 0.9911 | 0.9908 |
| 333 | 1.0000 | 1.0000 |
| 372 | 0.9963 | 0.9968 |
| 423 | 0.9773 | 0.9935 |
| 485 | 0.9593 | 0.9902 |

First Order Iteration Sequence:

$$Y(T) = a(T)A + b(T)B + c(T)C$$

$$\text{assumes } a = 1.000, b = 0, c = 0$$

$$T = 151 \text{ K}$$

$$A' = Y(T)$$

$$B'(\lambda) = \frac{Y(T) - a(T)A'}{b(T)}$$

$$T = 333 \text{ K}$$

$$A''(\lambda) = \frac{Y(T) - b(T)B'}{a(T)}$$

$$T = 151 \text{ K}$$

$$B''(\lambda) = \frac{Y(T) - a(T)A''}{b(T)}$$

$$T = 333 \text{ K}$$

repeat sequence until convergence for B and A

Second Order Iteration Sequence:

$$C'(\lambda) = \frac{Y(T) - a(T)A'' - b(T)B''}{c(T)}$$

$$T = 485 \text{ K}$$

$$B'''(\lambda) = \frac{Y(T) - a(T)A'' - c(T)C'}{b(T)}$$

$$T = 333 \text{ K}$$

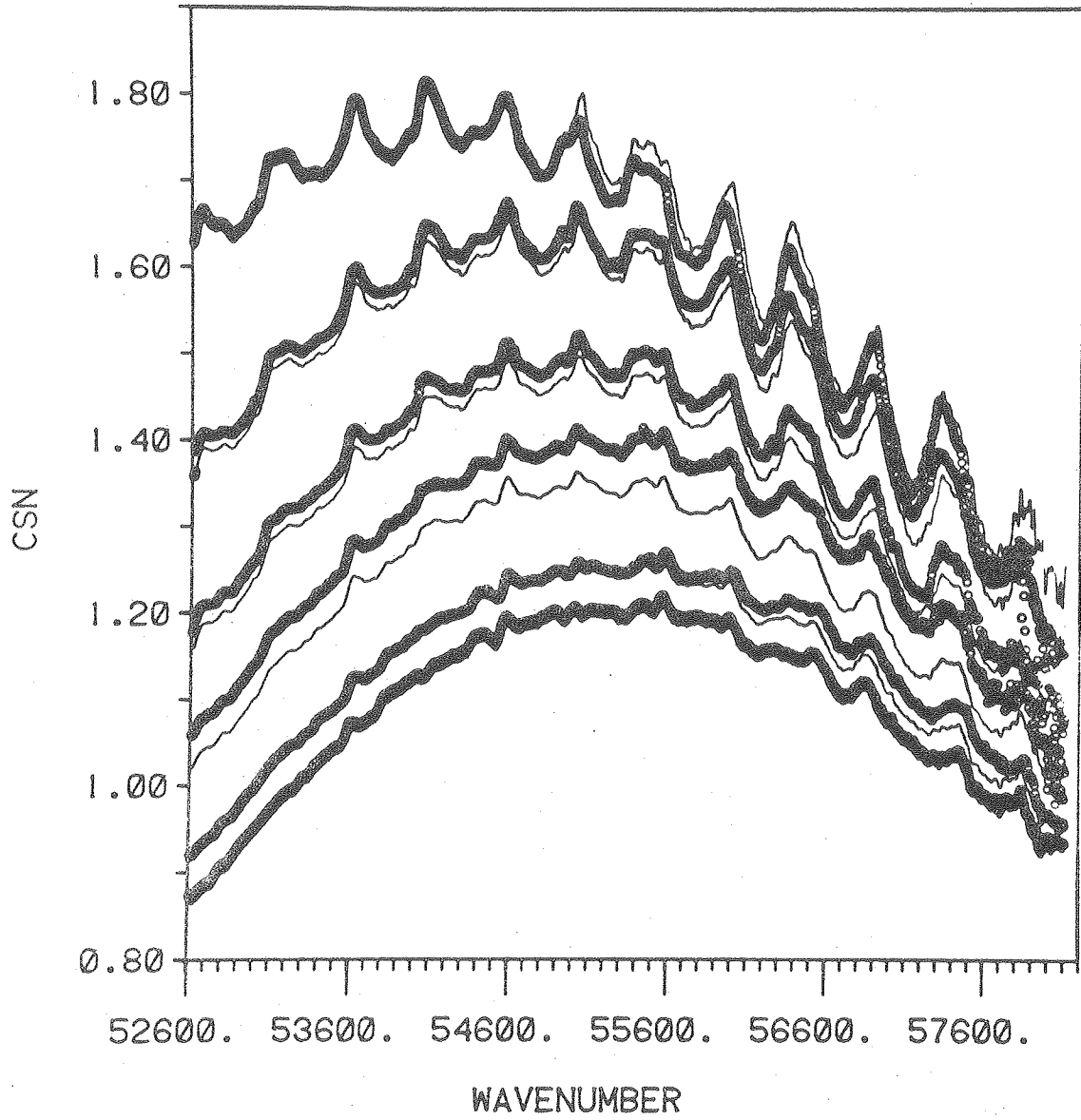
$$A'''(\lambda) = \frac{Y(T) - b(T)B''' - c(T)C'}{a(T)}$$

$$T = 151 \text{ K}$$

$$C''(\lambda) = \frac{Y(T) - a(T)A''' - b(T)B'''}{c(T)}$$

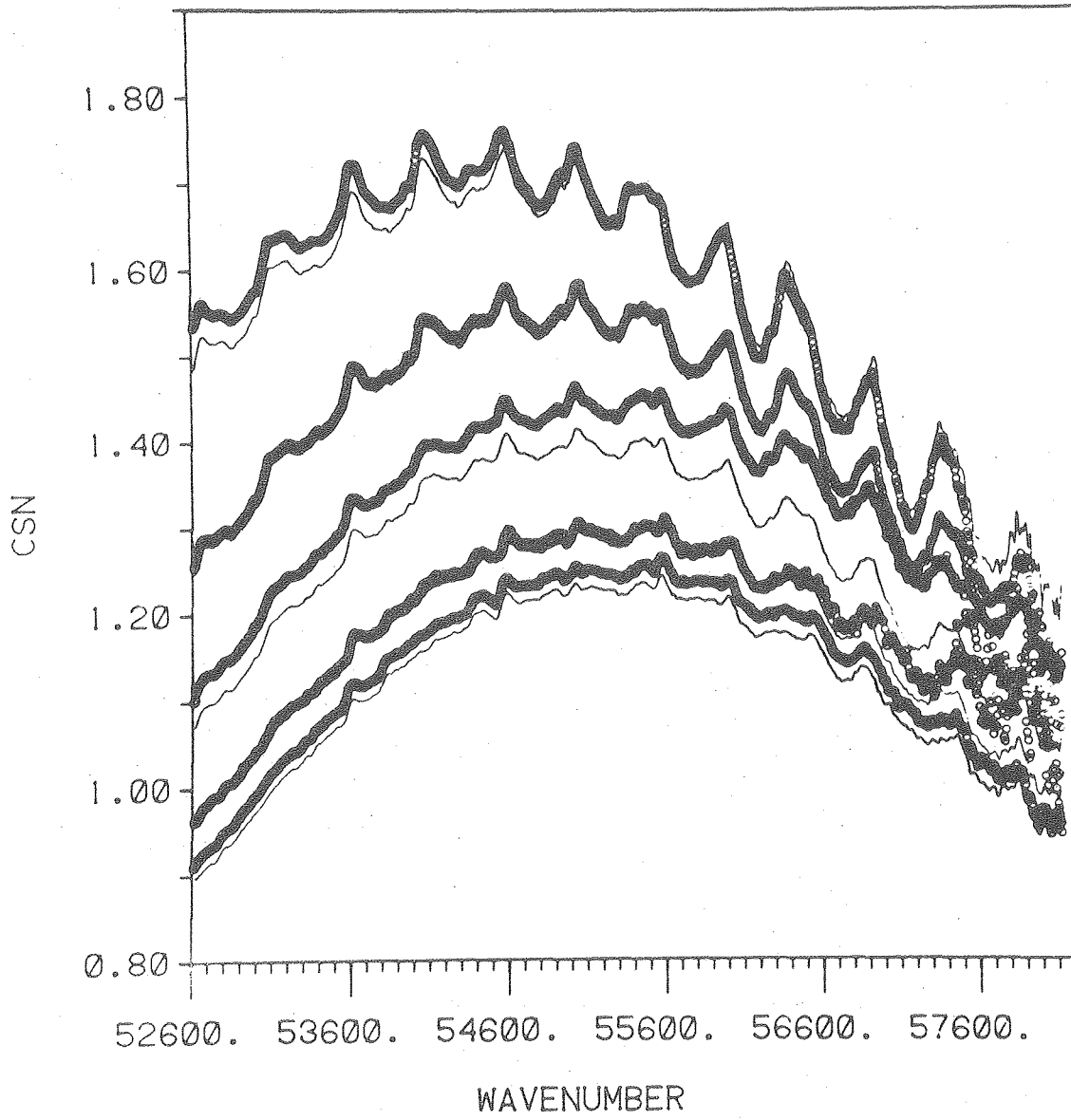
$$T = 485 \text{ K}$$

repeat sequences until convergence for A, B and C



XBL 792-8245

Figure 20a



XBL 792-8253

Figure 20b

vibrations and calculate the excited species population knowing the absorbed IR power, the quenching rate, and the temperature. Most likely this would involve excitation of selective rotational quanta and then forming a Maxwell-Boltzman average to simulate temperature equilibrium.

3. Energy Levels of the Upper Electronic State

In the preceding subsection, the observed spectra of N_2O were separated into the (000) and (010) state spectra. In figure 17, the (010) is seen to be strongly structured and more intense than the (000) state spectrum. Also a progression is apparent, indicating transition to discrete vibrational levels of the upper state. On the scale of figure 17, however, it is not apparent that very weak structuring can be observed in the (000) spectrum.

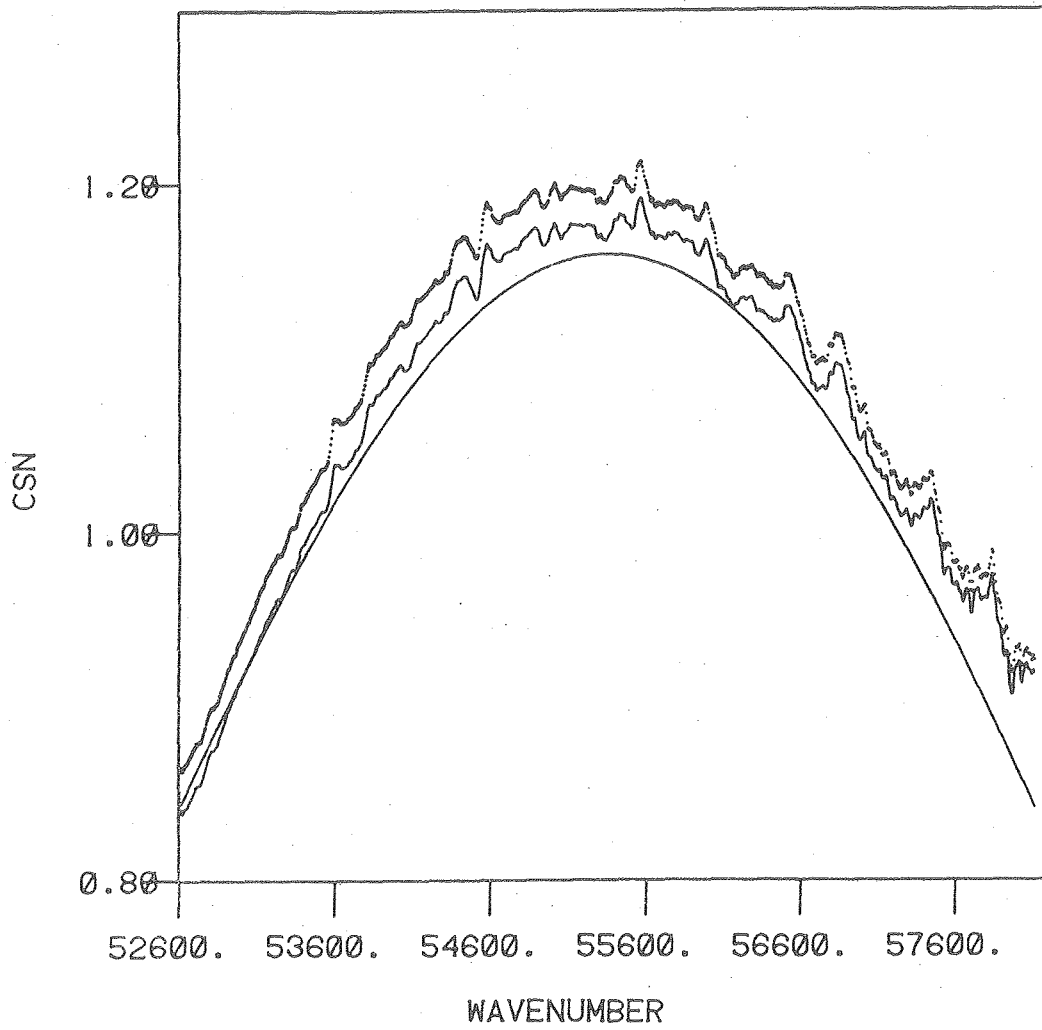
Figure 21 shows the (000) state spectrum on a different scale plotted as solid lines, along with the 151 K spectrum shown as individual data points. This shows that the effect of correcting the 151 K spectrum for the 0.7% of hot molecules is primarily to reduce the intensity of the 151 K spectrum by a small amount and that the observed structuring does not arise from this small fraction of hot molecules at that temperature. A weak progression is now observable at this temperature.

Figure 21 also shows an energy weighted Gaussian superimposed on the (000) state spectrum. The function shown is of the type:

$$I_{\text{abs}}(\lambda) = \nu N \exp(-D(\nu - \nu_0)^2)$$

where D , N , and ν_0 are constants. This is the equation of an energy weighted Gaussian which is seen to agree with the expected intensity distribution, as outlined in previous sections, by reaching the minima between the peak features.

It is possible the observed spectrum results from a continuous absorption, as the Gaussian curve shown in figure 21, superimposed on a separate second transition to give discrete spectra, represented by the difference between the (000) spectrum and the Gaussian curve.



N20

XBL 7812-13730

Figure 21

It is also possible that the intensity of the conjugate continuum absorption results from a single, pressure dependent broadening of the banding. The measurements using the 3 m monochromator as a long path cell at pressures between 50 - 200 millitorr would appear to support the former contention. Of course, any intermediate interpretation of the two theories is also reasonable. Interestingly, in the analogous absorption of carbonyl sulfide, Price and Simpson¹⁰³ reported that at pressures less than 10 m, the continuous absorption of OCS with superimposed diffuse bands, breaks down into a series of three broad band structured features without a superimposed continuum.

In view of this unconfirmed result and the similar possibility that at lower pressures the continuum may be reduced with a subsequent increase in the apparent banding intensity, the Gaussian curve in figure 21 has been only used as a means of removing the "background" absorption of nitrous oxide.

By fitting a similar curve to the (010) state spectrum, it is possible to remove the background absorption by subtracting a temperature weighted composite of the two Gaussian curves based upon the fractional (000) and (010) populations from the observed spectra. In the resulting difference spectrum the structured spectrum may be studied without the effect of superposition on a slope which tends to change the shape and wavelength maximum of the peaks. Figure 22a shows this result at 151 K. The structuring is quite weak although the progression noted previously for this temperature is now more clearly seen with a spacing of 970 cm^{-1} and is noted by downward arrows. The peak positions of the progression and their separations are noted in table 5. At

Table 5. Vibrational Progression Members at 151 K

| Peak No. | ν^{-1} , cm^{-1} | $\Delta \nu^{-1}$, cm^{-1} |
|----------|-------------------------------|--------------------------------------|
| 1 | 53 595 | |
| 2 | 54 578 | 983 |
| 3 | 55 567 | 989 |
| 4 | 56 534 | 96 |
| 5 | 57 450 | 916 (962)* |
| | average spacing: | 964 |

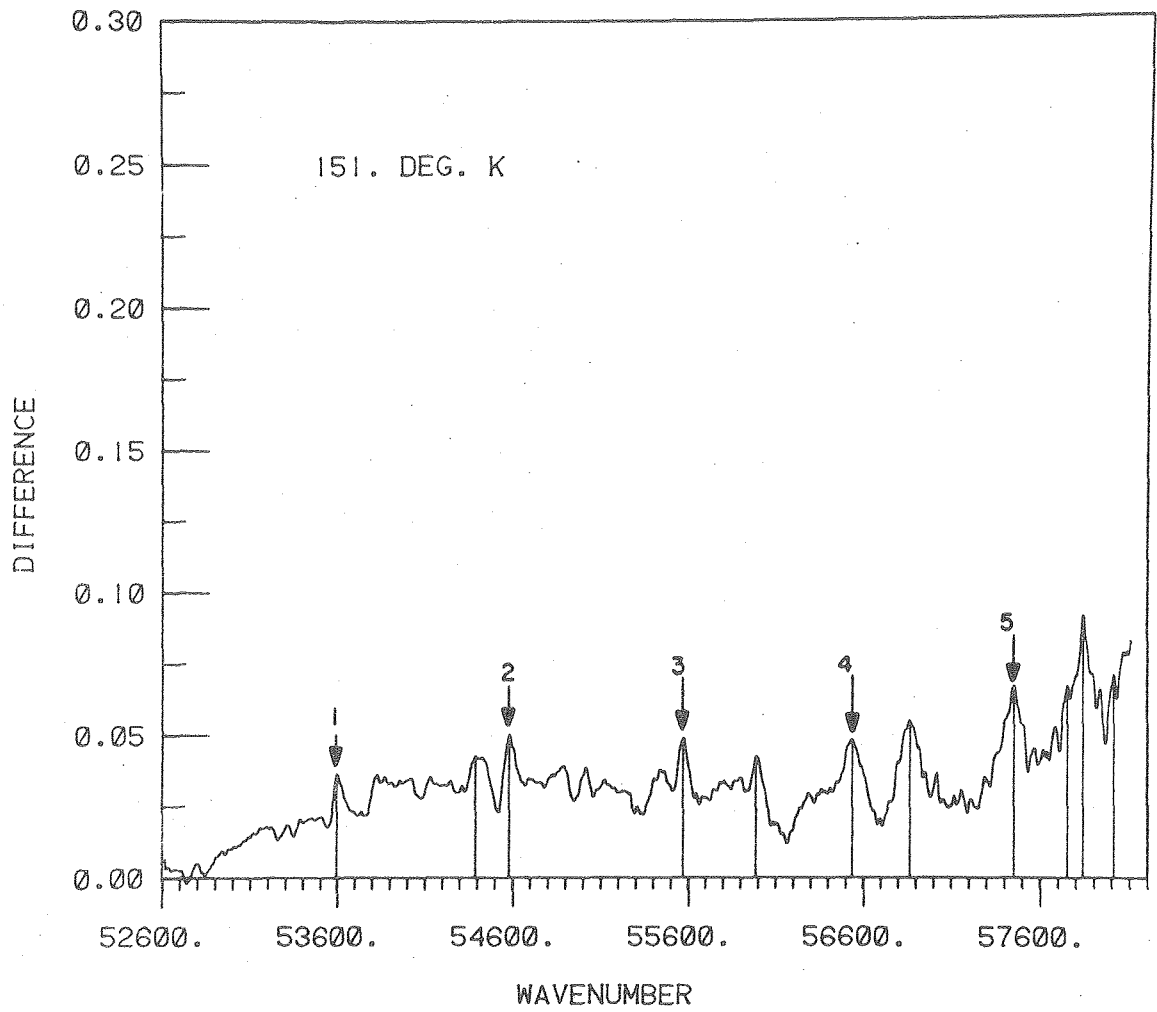
*second figure from the 182 K difference spectrum

this temperature the spectrum is least complicated by hot bands, but the weak intensity of structuring makes analysis difficult. Besides the features fit to the 970 cm^{-1} progression, there are a few other features noted which do not appear to fit another progression.

Figures 22a to 22k show the result of this correction process at each temperature between 151 K and 485 K. With increasing temperature, the structuring increases in intensity and the presence of a second, more intense progression with a spacing of about 480 cm^{-1} is becoming increasingly dominant with temperature. At 485 K only this dominant progression is seen as major peak features, although another minor progression is also seen as shoulders on the stronger peaks. The wavenumbers and energy separations of the major features in figure 22k are given in table 6. The slope of the difference spectra at the higher temperatures arises from the contribution of higher-order vibrations (note this is most pronounced at the longer wavelengths.)

It is useful to interpret the relative energy separations of the peak features in these figures in relation to absolute energy levels of the upper electronic state and to see if similar results are present in the less obvious progressions at lower temperatures.

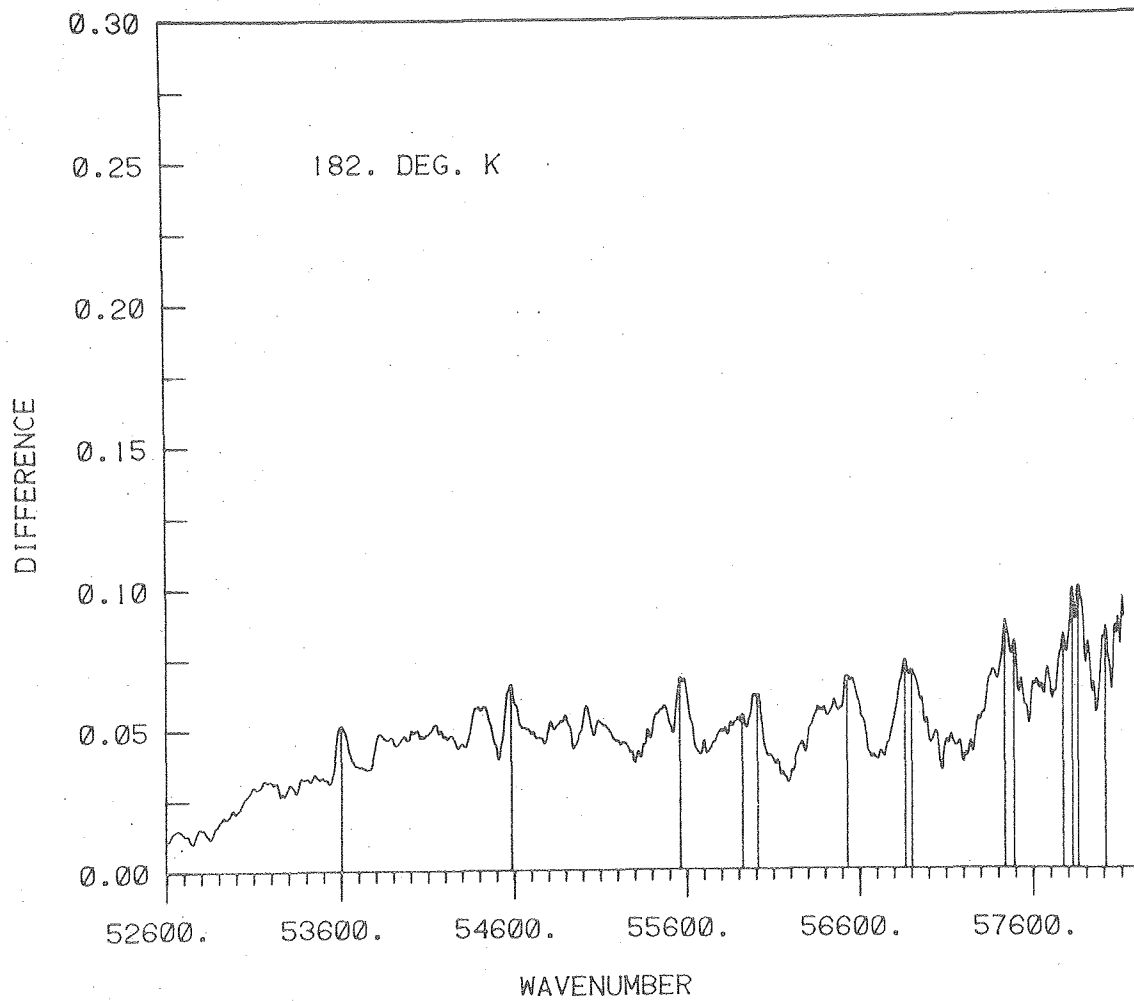
To do this, a program was developed to select the major peak features using the same selection criteria for all temperatures studied. To deal with the very weak, diffuse banding as in the colder temperatures in the same objective way as the greater intensities as in figure 22k it was necessary in the peak selection process to utilize width and height criteria as well as an inflection in the first derivative of the plot. Without such width and height criteria, a simple inflection



N2O

XBL 792-8397

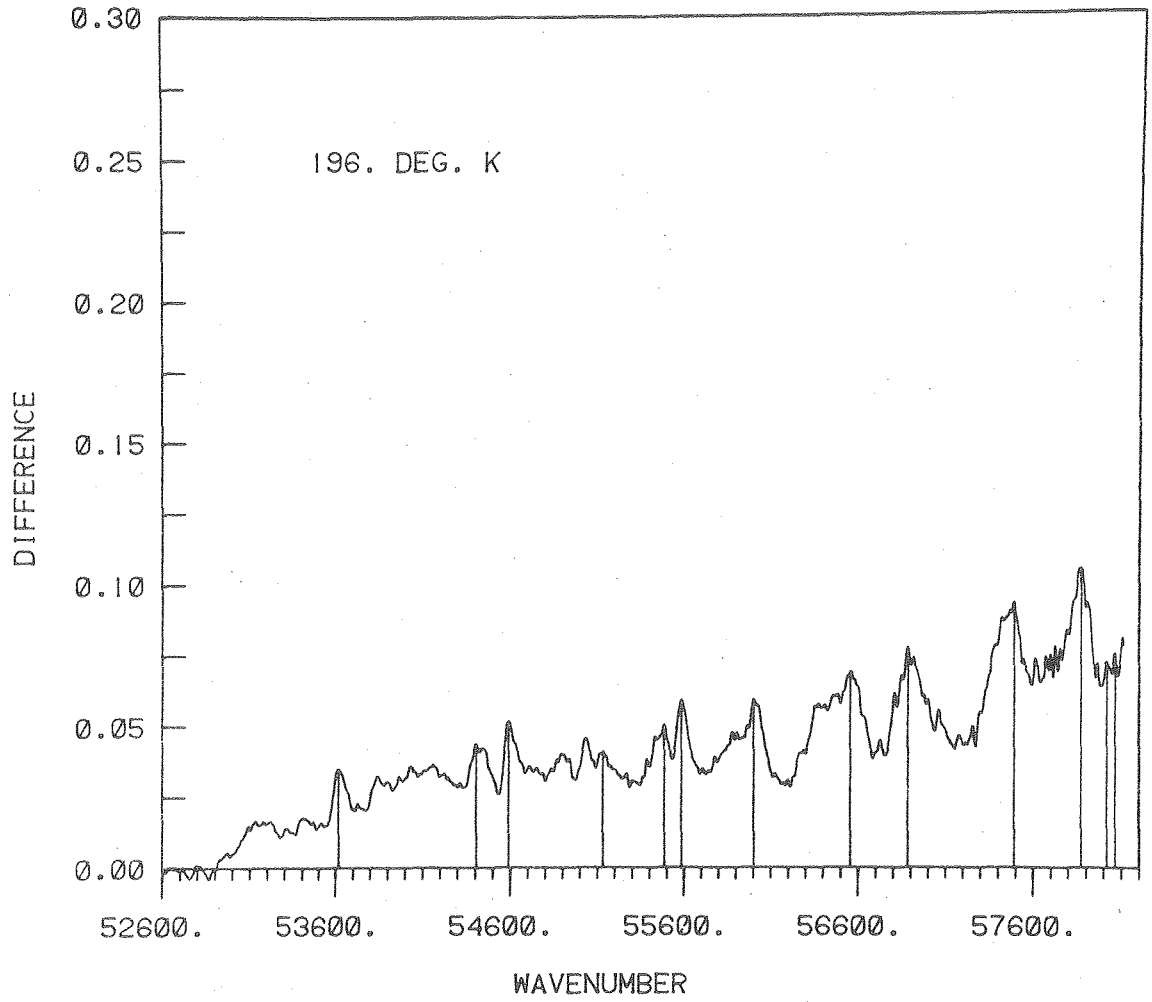
Figure 22a



N20

XBL 7812-13973

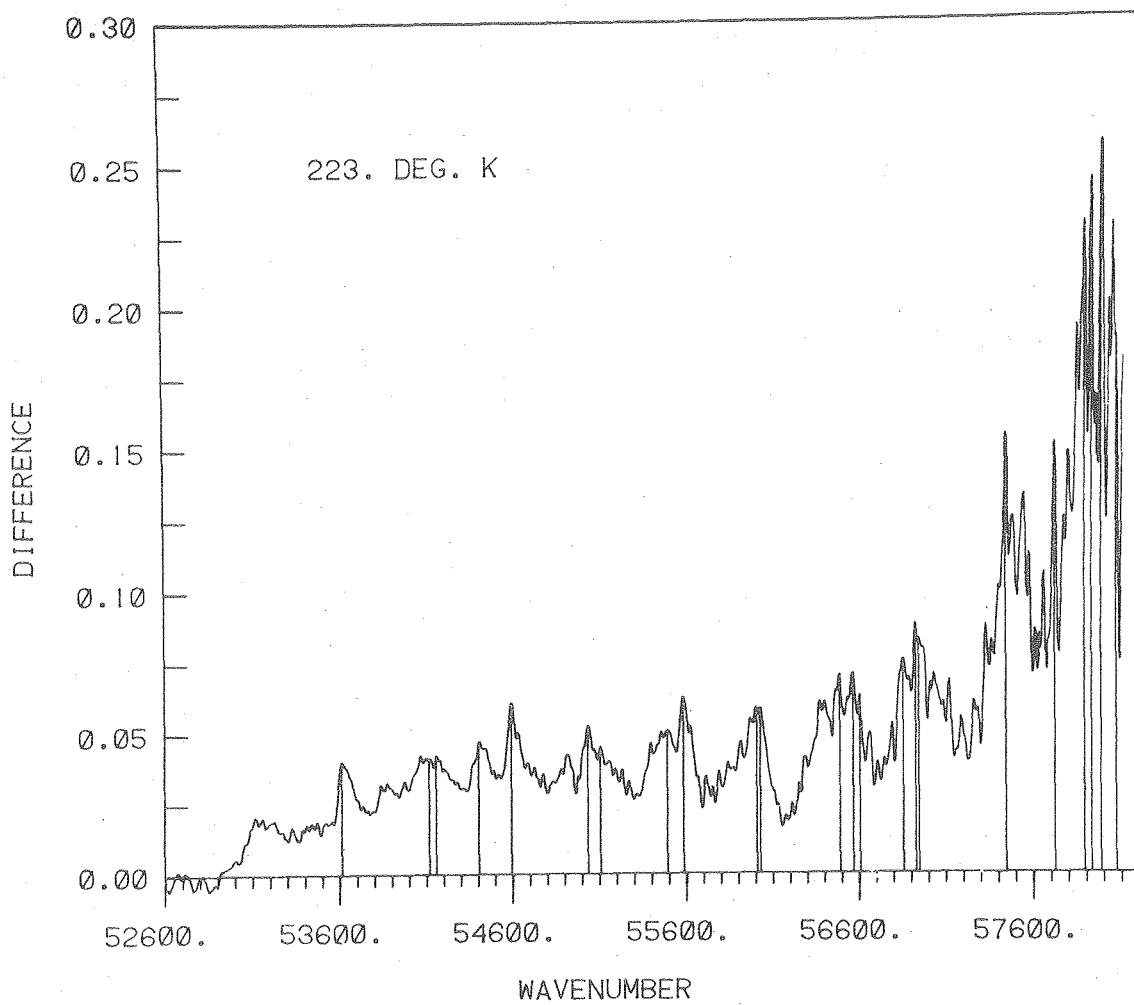
Figure 22b



N2O

XBL 7812-13972

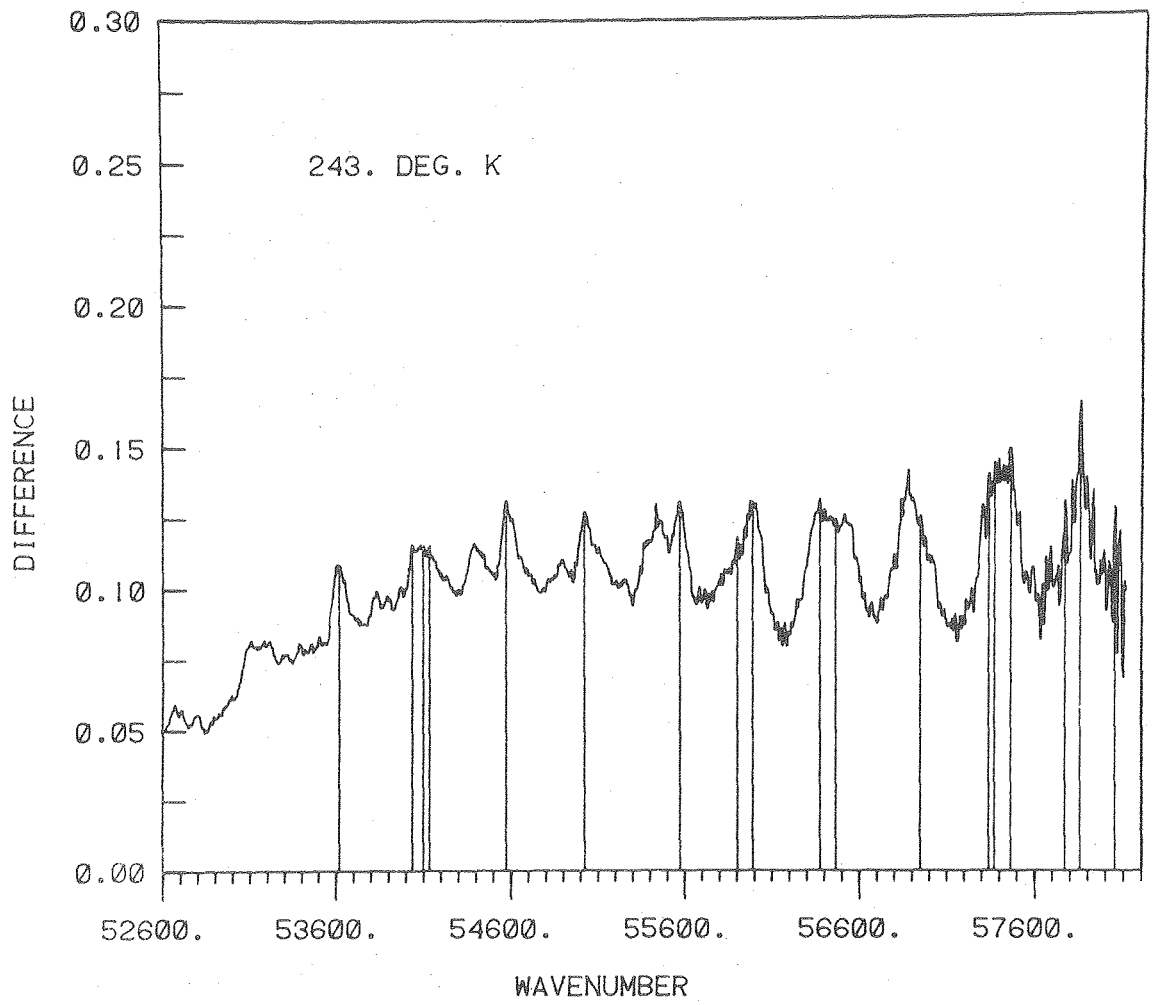
Figure 22c



N20

XBL 7812-13971

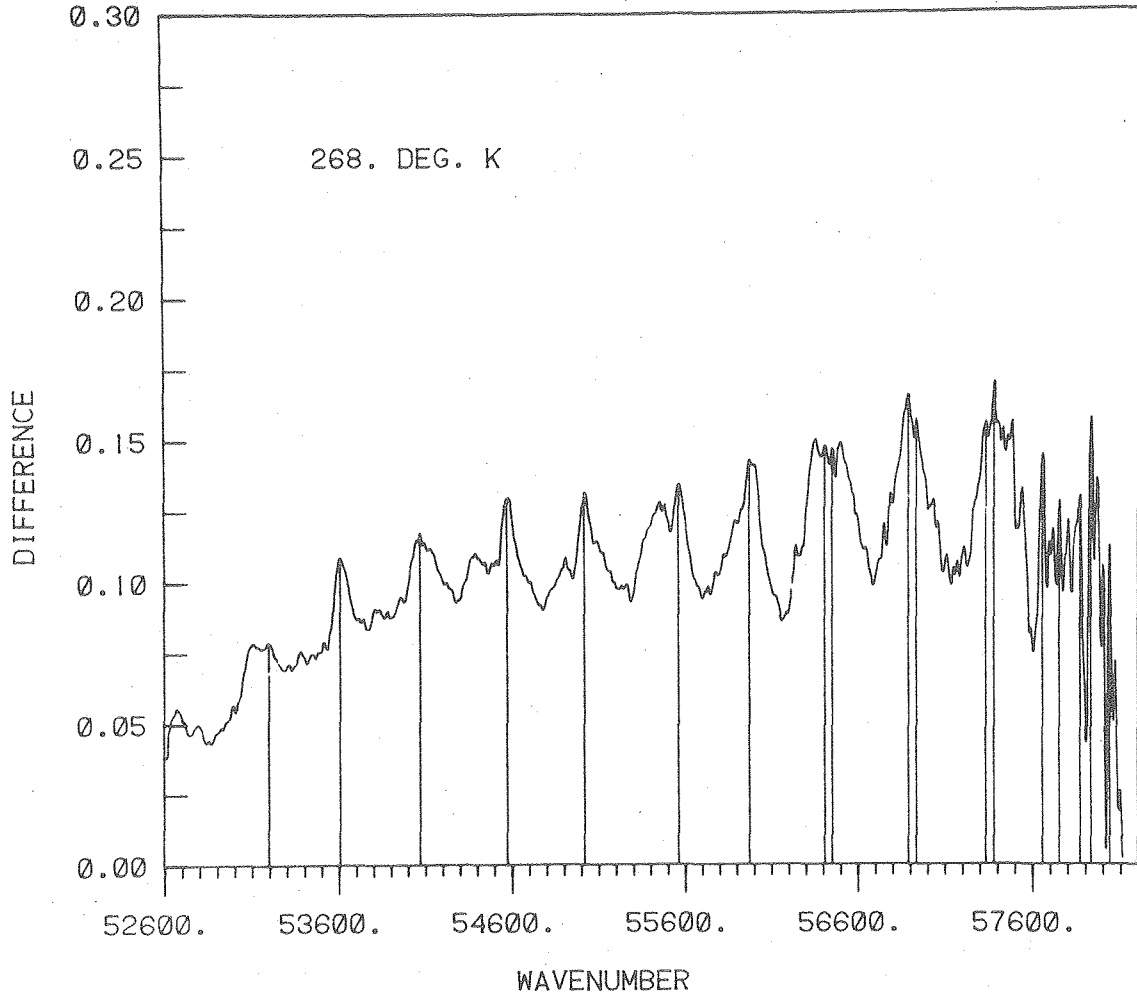
Figure 22d



N2O

XBL 7812-13976

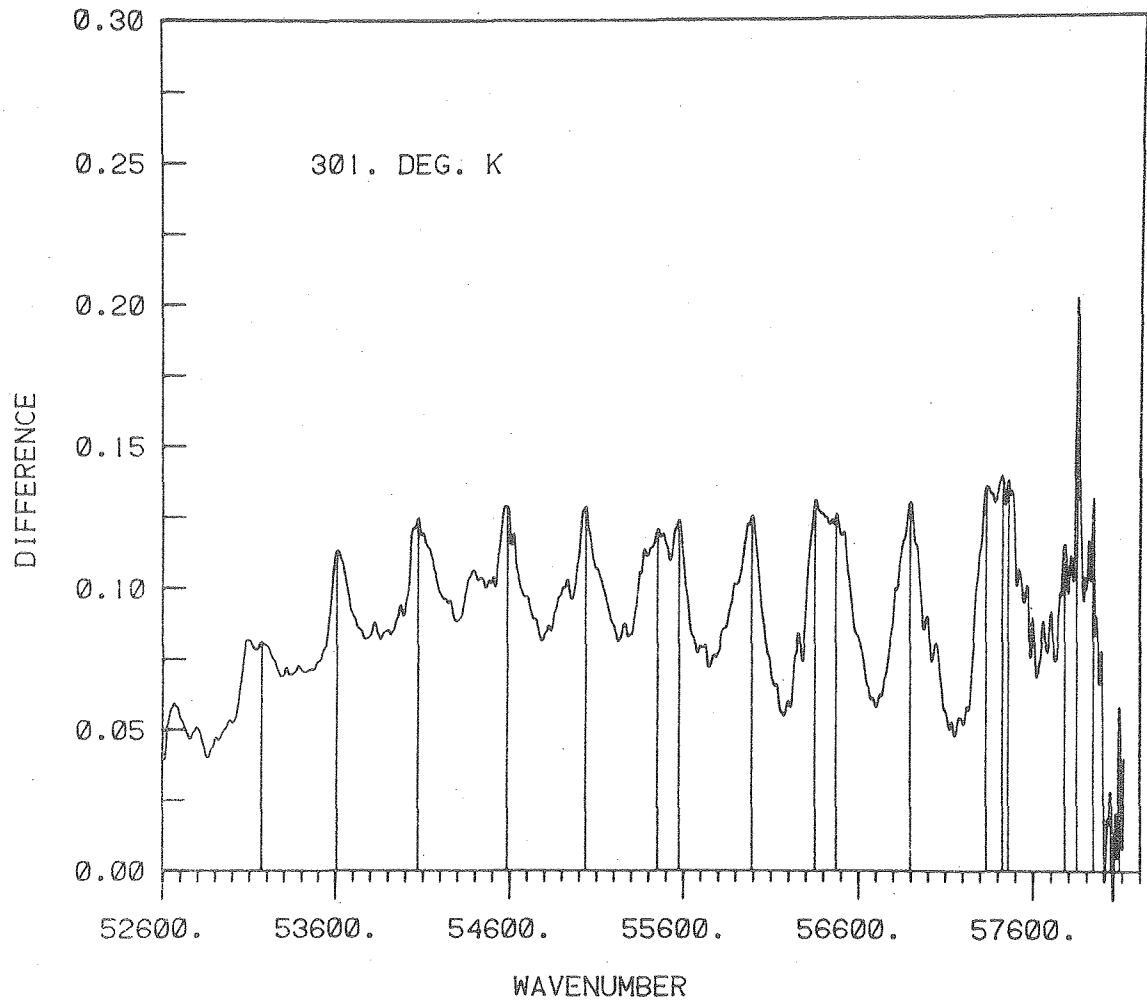
Figure 22e



N2O

XBL 7812-13977

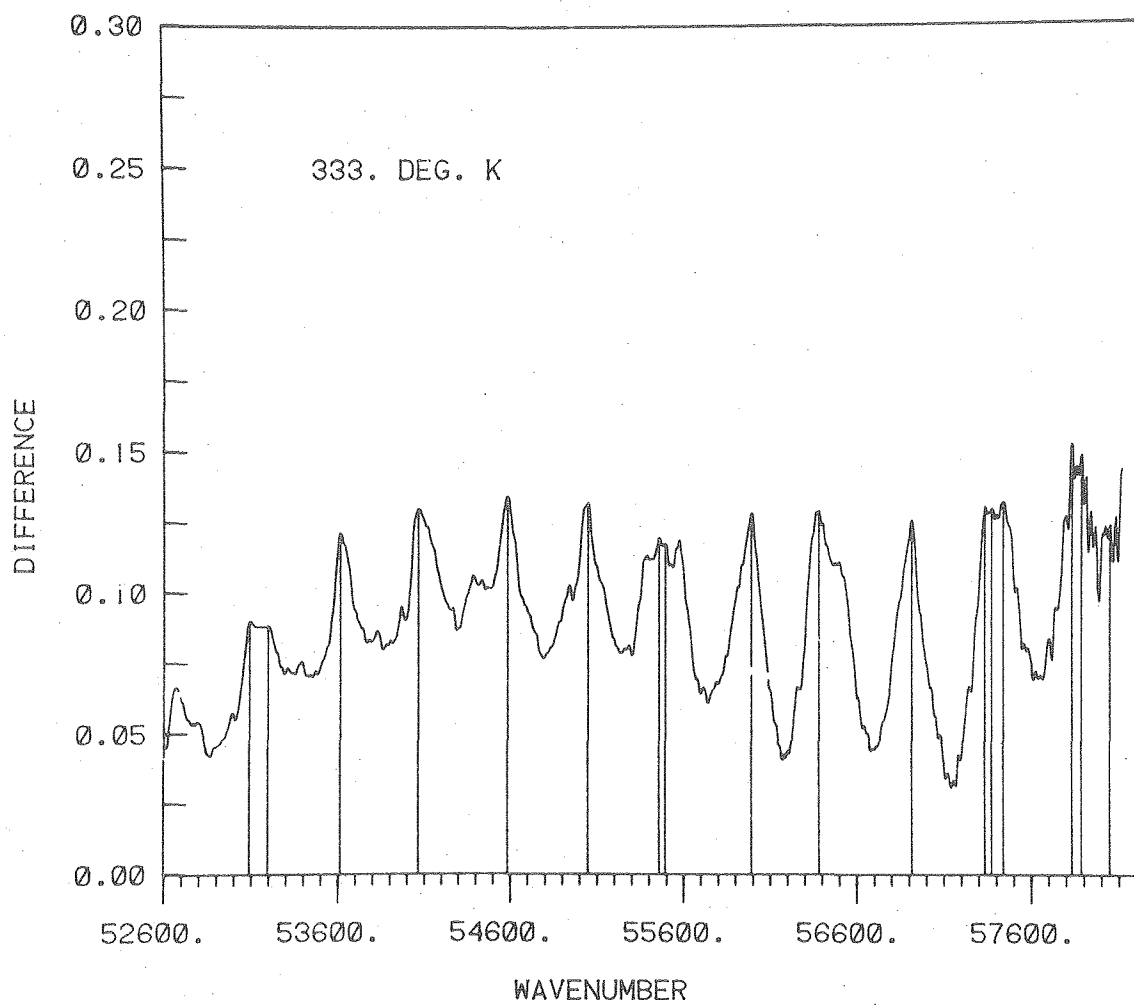
Figure 22f



N2O

XBL 7812-13975

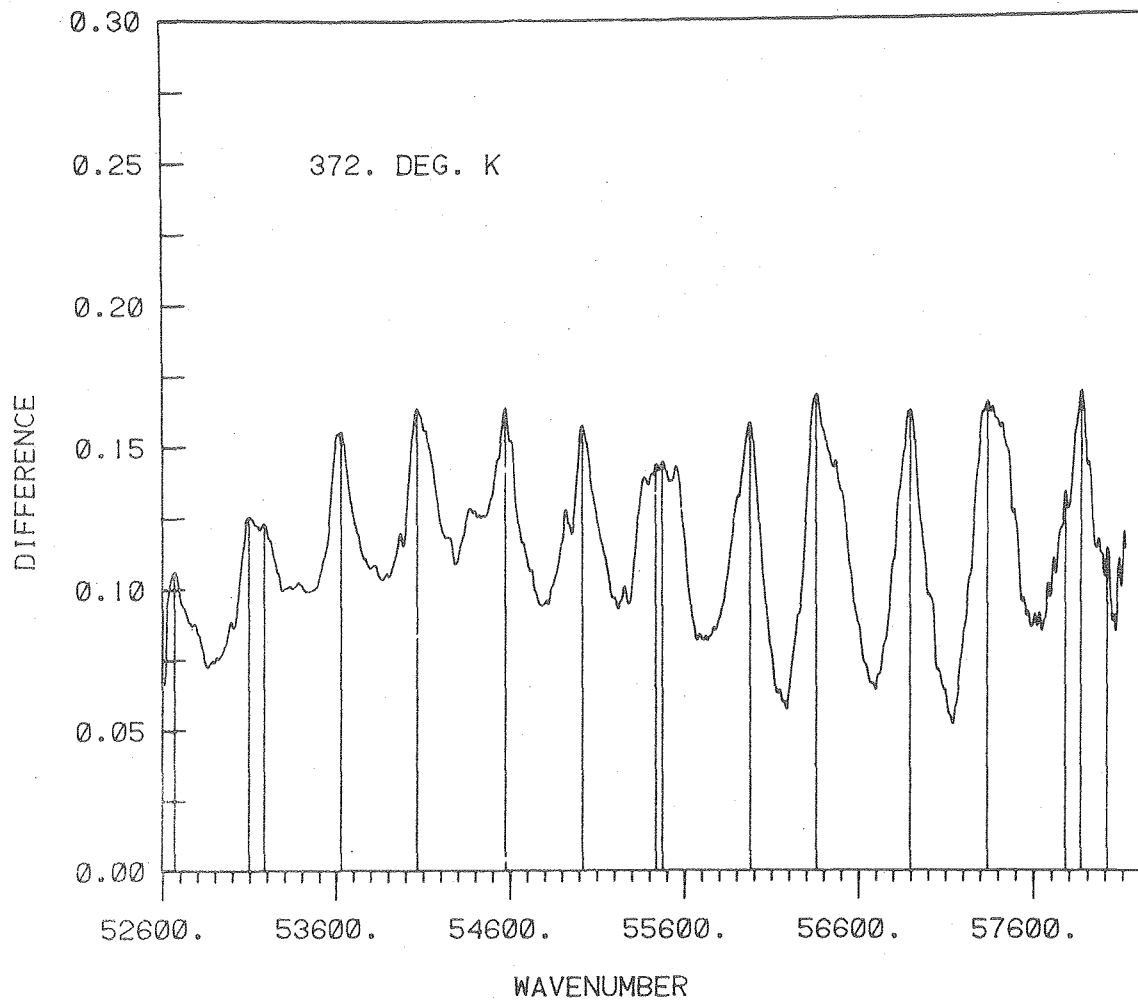
Figure 22g



N2O

XBL 7812-13978

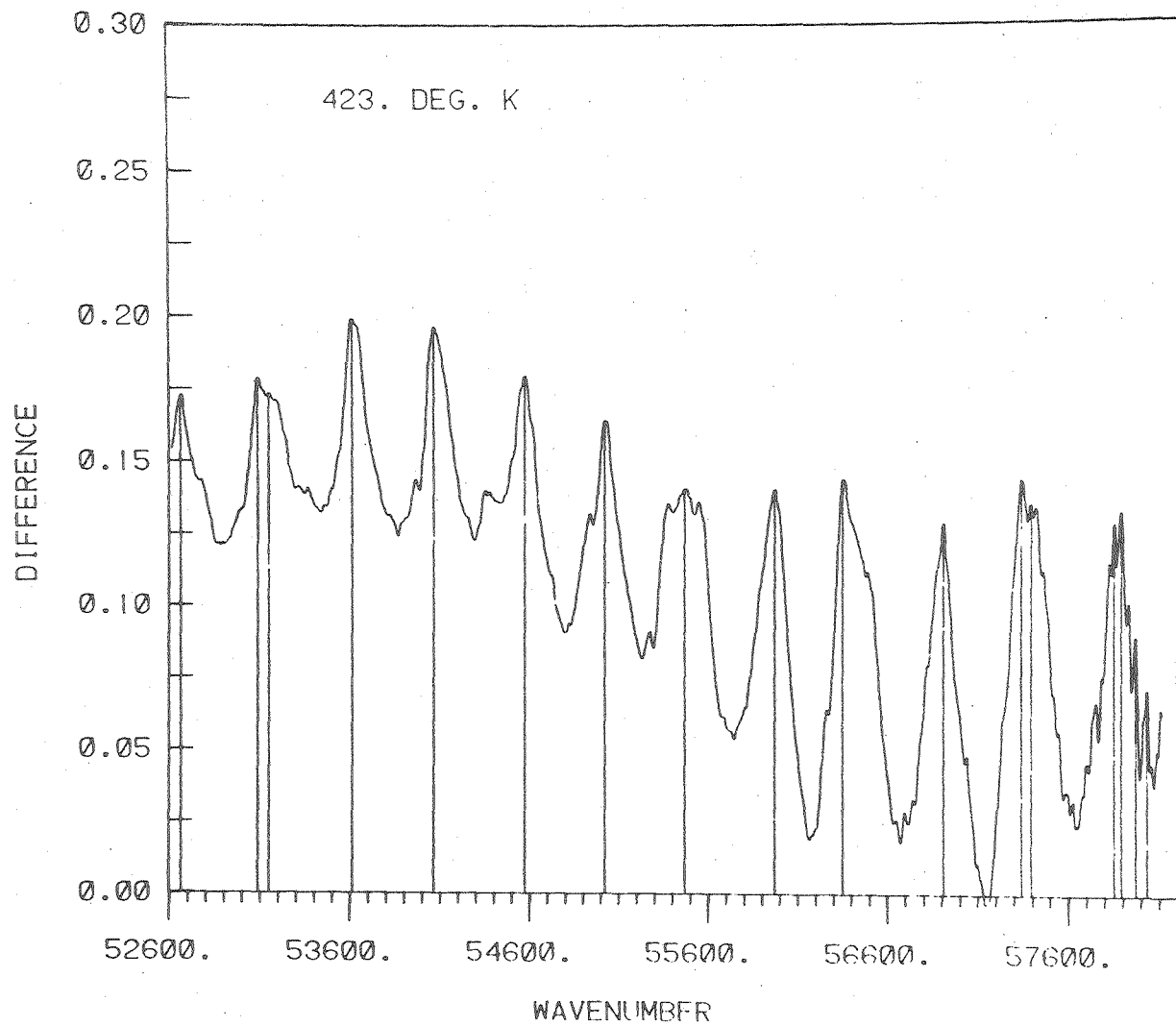
Figure 22h



N2O

XBL 7812-13979

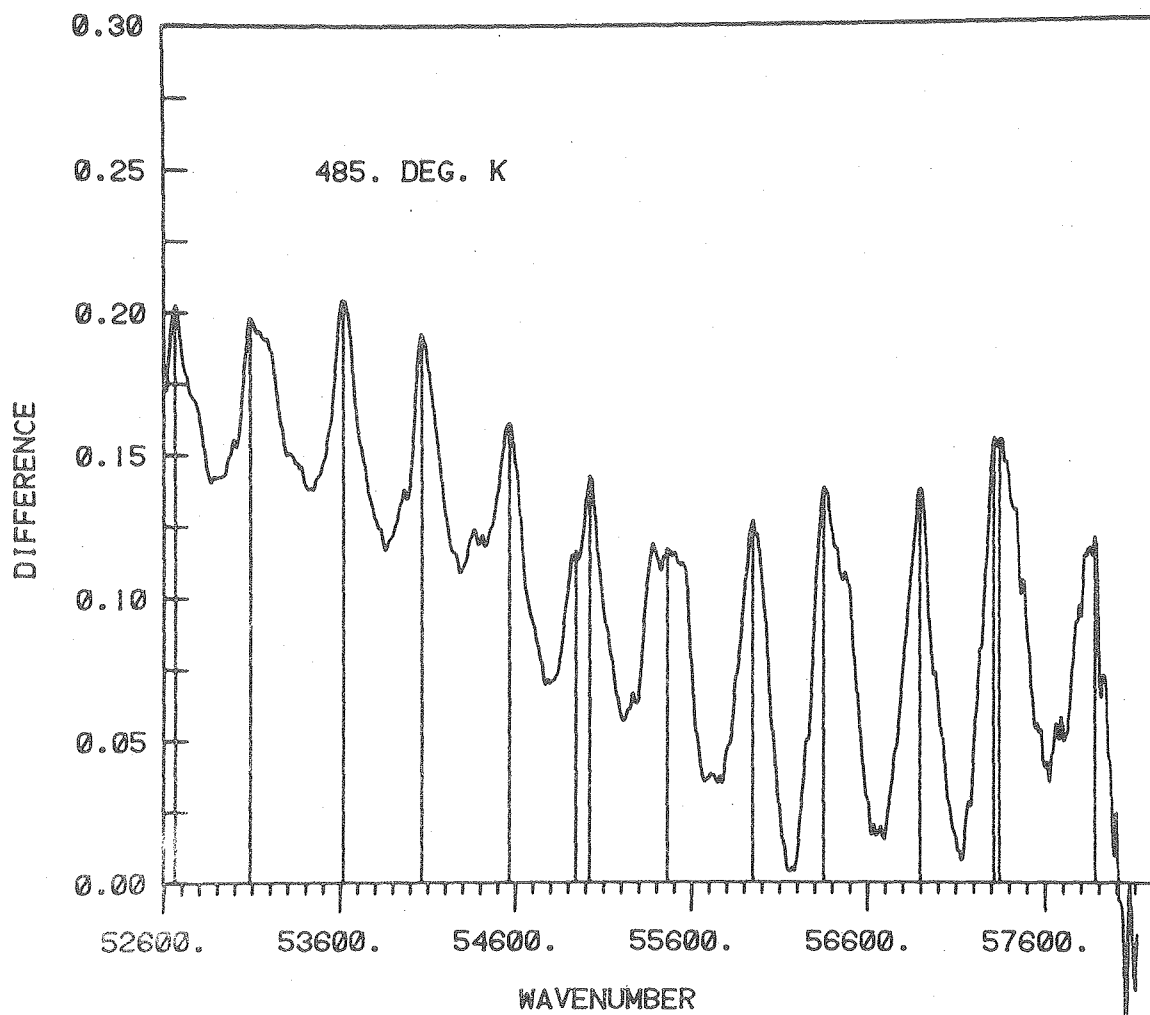
Figure 22i



N2O

Figure 22j

XBL 7812-13980



N2O

XBL 7812-13986

Figure 22k

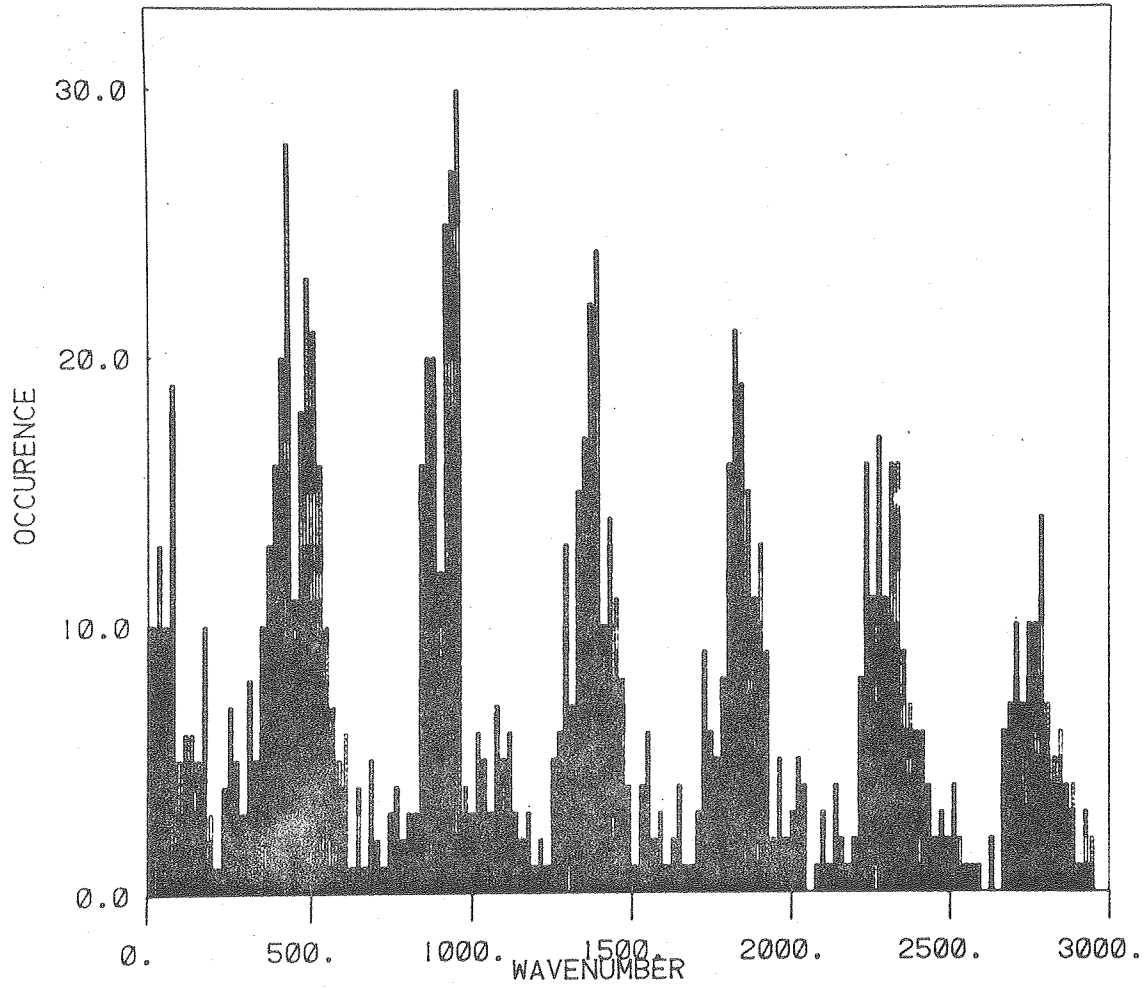
Table 6. Selected Vibrational Progression Members at 485 K

| Peak Number | Energy, cm^{-1} | Spacing, cm^{-1} |
|-------------|--------------------------|---------------------------|
| 1 | 52 662 | 425 |
| 2 | 53 087 | 529 |
| 3 | 53 616 | 446 |
| 4 | 54 062 | 501 |
| 5 | 54 563 | 456 |
| 7 | 55 019 | 439 |
| 8 | 55 458 | 484 |
| 9 | 55 942 | 403 |
| 11 | 56 890 | 450 |
| 13 | 57 340 | 531 |
| 14 | 57 871 | |

in slope would have indicated hundreds of peaks at the low temperatures as in figure 22a and thereby emphasize the weak low temperature spectra much more than the stronger high temperature results. The width and height criteria were both logical decisions using the Fortran .OR. command and could be met by either large broad peaks or by smaller but sharper features. (For details see Subroutine CHECK in Program FINAL in the appendix.) Unavoidably, the program would occasionally identify two nearby peaks on a feature with a slight double maximum which a more subjective observer would place one peak, or a smaller feature appearing on the shoulder of a more intense peak might be missed. The features at each temperature which are selected as peaks by the program are indicated as solid lines in figures 22a to 22k.

The permutation of all energy separations between the selected peaks for each temperature were measured and counted in bins of 20 cm^{-1} . The grand summation of this energy separation count for all temperatures is shown in figure 23 as a histogram of frequency of occurrence in energy spacing between peaks vs. relative energy separation in cm^{-1} . The different shadings of the individual bars in the histogram represent the portion contributed by each temperature. Use of a permutation in counting all possible energy separations at a given temperature avoids overcounting the same energy separation between two peaks, although it tends to emphasize the smaller energy separations. This is seen by the decreasing intensity of the vibrational features in the histogram with increasing energy of separation.

To check the effect of the peak selection parameters on the final histogram result, the parameters were varied for ten different cases



XBL 7812-13970

Figure 23

varying from very restrictive criteria, yielding very few peaks, to a much less restrictive criteria, yielding many more peaks, especially at the lower temperatures. The final histogram derived from each case varied in the relative height (or signal/noise ratio) of the features seen in figure 23, but did not change the overall appearance of the histogram or the energy spacing of the features in figure 23. The sharp features of figure 23 indicate the approximate active vibrational energy levels of the upper electronic state relative to a minimum of potential energy.

The vibrational energy levels of figure 23 are listed in table 7.

Table 7. Histogram Vibrational Features and Energy Levels

| Vibrational Level, n | Energy, cm^{-1} | E/n, cm^{-1} |
|----------------------|--------------------------|-----------------------|
| 1 | 500 | 500 |
| 2 | 980 | 490 |
| 3 | 1420 | 473 |
| 4 | 1880 | 470 |
| 5 | 2340 | 468 |
| 6 | 2840 | 473 |

4. Vibrational Selection Pattern

From the progressions in figures 22a to 22k, and from the energy separations indicated in the histogram, it is seen that $\nu_2' \approx 480 \text{ cm}^{-1}$. Yet in the (000) state spectrum, the spacing of the progression noted previously is 970 cm^{-1} . Since this value is very close to $2\nu_2'$, it appears that the (000) state follows the vibrational selection pattern:

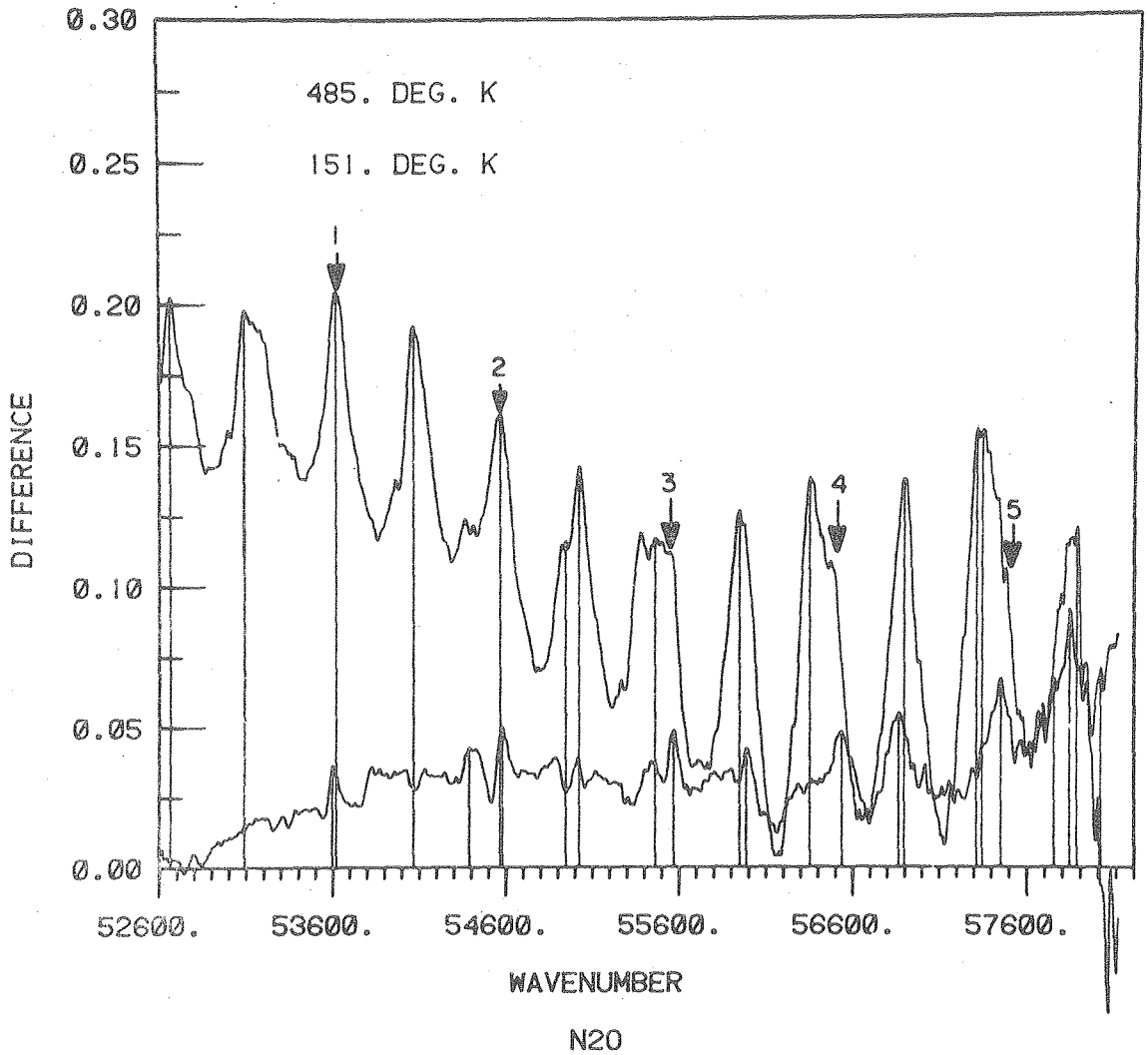
$$\Delta\nu_2 (\nu_2'' = 0) = 1, 3, 5, 7 \dots$$

whereas the "hot" spectra and the spectrum of the (010) state indicate that from $\nu_2'' = 1$ or 2 consecutive values of ν_2' are selected. This pattern becomes more evident when the weak structuring of the (000) state spectrum is superimposed on the spectrum taken at 485 K. In figure 24, the two spectra have had the underlying absorbance subtracted out and they have been superimposed on the same scale. The advantage of this method of forming difference spectra to study the energy positions of the structuring is evident by allowing such a comparison. Each of the five members of the progression in the (000) state spectrum agrees well with an alternate feature of the high temperature spectrum.

As outlined in previous parts of this section, this vibrational selection pattern is symptomatic of only a vibronically allowed transition. This is to be differentiated from the case of a bent-linear transition which would be rigorously forbidden in the linear-linear configuration. For such a case, as outlined previously, transitions from $\nu_2'' = 0$ (i.e. the (000) state), as well as the hot bending vibrations, would show consecutive values of ν_2' . Since the bending vibration

would show consecutive values of ν_2' since the bending vibration is a symmetric motion in Cs symmetry and the selection rules for symmetric vibrations predict^{97h} a conservative sequence in ν_2' . Yet the alternate peaks at 53 100, 54 050 and 55 000 cm^{-1} are noticeably absent from the (000) state spectrum whereas they are strong in the 485 K spectrum (and the (010) state spectrum).

It is also noted in the 151 K spectrum that weak, vibrational peaks are observed at 55 950 and 56 850 cm^{-1} , which according to the theory outlined previously, would be expected to be absent. Two possible explanations are offered here for the occurrence of these additional features. The two unexplained peaks may be members of a different vibrational progression other than the ν_2 bending mode. The other members of this second (or third) progression may be obscured by their weak intensity in comparison with the observed ν_2 progression features. Secondly, the intensity of these two features is seen from figure 24 to be about $3 \times 10^{-21} \text{ cm}^2$ (peak to trough). Accordingly, the intensities of the two features are about 10^{-5} of a fully allowed electric dipole transition. As stated previously, the intensity of an allowed magnetic dipole transition is about 10^{-5} of an allowed electric dipole transition.^{97g} The $\sum^- - \sum^+$ transition is allowed by the magnetic dipole operator,^{97g} so it is reasonable to believe that there may be a magnetic dipole contribution to the vibronic structure since the intensities observed are on the order of magnitude of a magnetic dipole transition. For an allowed magnetic dipole transition such as this (and for most allowed electric dipole transitions as well), the greatest intensity is expected for one or two progression



XBL 7812-13985

Figure 24

members with optimal Franck-Condon overlap (vertical transitions) and with the other members of the progression rapidly decreasing in intensity (nonvertical transitions). The two unexplained features at 151 K may then arise from the contribution of a magnetic dipole transition, which is non-negligible only in this limited short wavelength range corresponding to a vertical transition.

In view of this discussion, it is seen that the repeated absence of vibrational features at 53 100, 54 050 and 55 000 cm^{-1} is more informative than the occasional presence of an unexplained feature in one region of the spectrum since these may be complications due to additional progressions or may be bands due to magnetic dipole transitions.

Armed with this insight, it is possible to partially assign the features in the observed spectrum. Each of the five members of the progression in the (000) state represent the transitions:

$$\begin{aligned} \omega \nu_2' \\ \omega \nu_2' + 2 \\ \omega \nu_2' + 4 \leftarrow \nu_2''(0) \\ \omega \nu_2' + 6 \\ \omega \nu_2' + 8 \end{aligned}$$

where ω has been shown to be an odd integral quantum number.

The energy of ν_2' is approximately 480 cm^{-1} , which is 100 cm^{-1} less than the ν_2'' of 589 cm^{-1} in the ground electronic state. Thereby the transitions:

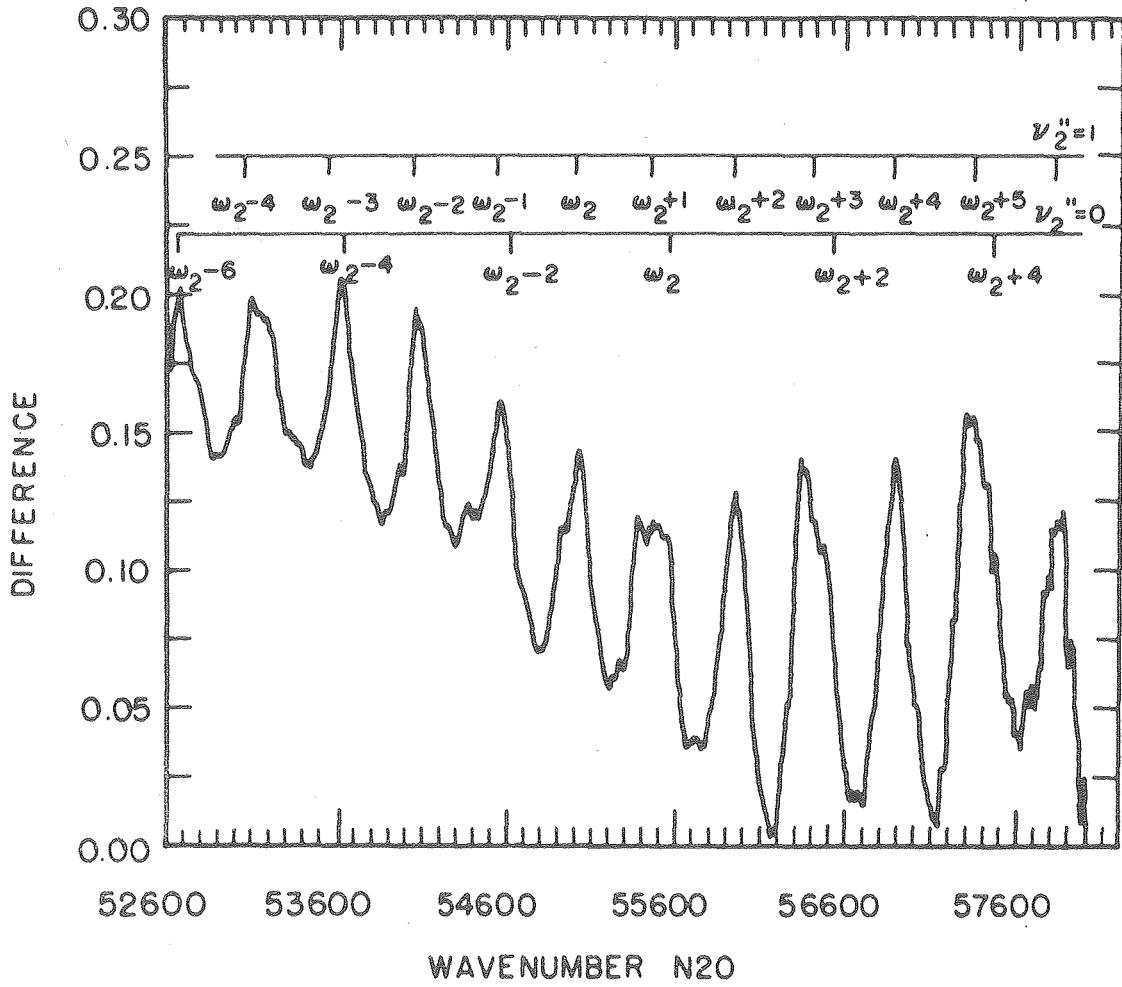
$$\begin{aligned} \omega\nu_2' - 1 \\ \omega\nu_2' + 1 \\ \omega\nu_2' + 3 \quad \leftarrow \nu_2''(1) \\ \omega\nu_2' + 5 \\ \omega\nu_2' + 7 \end{aligned}$$

where ω is the same odd quantum number, will be located 100 cm^{-1} below the peak positions of $\nu_2'' = 0$. Midpoint between these hot bands will be the remaining transitions of the type $\omega\nu_2' + (2, 4, 6, 8\dots) \leftarrow \nu_2''(1)$.

Similarly, hot band originating from $\nu_2''(2)$ would be expected to be 95 cm^{-1} below the $\nu_2''(1)$ levels and thus form a sequence in ν_2 .

The resulting sequences in ν_2 and its peak positions is shown superimposed on the composite difference spectrum of figure 22K in the next figure.

The assigned peak positions fit the observed spectrum and this interpretation explains the different rates of activation energies of the spectra. For example, the feature at $55\,500 \text{ cm}^{-1}$ at low temperatures has a predominate feature at its short wavelength end. At higher temperatures, the absorption assigned to $\nu_2''(1)$, located 100 cm^{-1} below the $\nu_2''(0)$ assignment rapidly increases and becomes more intense. The lowest energy peak of this triplet structure may be the hot band from $\nu_2''(2)$, but there is no conclusive proof for this. Similarly, the feature at $56\,400 \text{ cm}^{-1}$ at low temperatures the short wavelength absorption assigned to $\nu_2''(0)$ is seen as predominant.



XBL 792-8573

Figure 25

At 485 K, the same feature is only seen as a sloping shoulder on top of the more intense hot bands located 100 cm^{-1} below the $\nu_2''(0)$ assignment.

Although the vibrational pattern appears to support the contention of transition through vibronic interaction, there is evidence also for a change of symmetry between the two electronic states. For a linear-linear transition, the intensity of the observed peaks are typically most intense in one or two peaks with subsequent members of that progression rapidly decreasing in intensity due to poor Franck-Condon overlap. If there is a change of symmetry during transition, and if the transition is forbidden in the linear-linear configuration, then as previously demonstrated, there is a slow variation in the intensity of the progression members, with a maximum located somewhere between the $\Delta v = 0$ and the high energy limit of the bands. This is clearly the case of the observed structuring, so this may indicate that the upper state is bent, as it has been calculated to be (references 14, 124, 106) with a bond angle of 130 degrees¹⁰⁴.

G. Photodynamics

1. Continuous Absorption

Rabalais et al¹⁴ and Fortune and coworkers^{104a,b} have assigned the continuous absorption at 6.8 eV to the $^1\Delta$ state correlating with N_2 ($^1\Sigma_g^+$) and O (1D_2). This could explain the weak nature of the absorbance ($f \sim 1.5 \times 10^{-2}$) since the transition $^1\Delta \leftarrow ^1\Sigma^+$ is angular-momentum forbidden. Chutjian and Segal¹⁰⁶, however assign the same absorption to the $^1\pi$ state correlating to the same asymptote as the $^1\Delta$ state. A more definitive theoretical result is required here to resolve this discrepancy.

Interestingly, in a recent electron impact study of the analogous absorption of OCS, the assignment of $^1\Delta$ to the observed continuous absorption was determined by measuring the angular dependence of the electron scattering.¹⁰⁵ A similar experimental study of this type would be useful in confirming the calculations of Fortune and coworkers and the Rabalais study.

I shall adopt here the $^1\Delta$ assignment on the basis of these more recent calculations and since the $^1\pi$ assignment would be expected to be more intense than the absorption is actually observed to be.

2. Structured Absorption

The Chutjian and Segal study¹⁰⁶ has offered the most detailed explanation of the vibronic banding of nitrous oxide in this energy range. They suggest that the banding results from vibrational resonance between the strongly bound $1\Sigma^-$ state (the only state calculated to be bound in this energy region -- agreed upon by all the theoretical studies) and the repulsive 1Δ state. Mixing of the two eigenfunctions may occur by vibronic coupling, even though the two states are separated by 2.8 eV in the Franck-Condon region. They further explain "at certain energies a band width of continuum levels (of 1π) will be in resonance with a vibrational level of the $1\Sigma^-$ state, and electronic mixing via the A" components of the two states will take place upon bending. The resonances will occur at spacings corresponding to spacings of either the ν_2 bending vibrations of the $1\Sigma^-$ state or to the very anharmonic ν_3 vibrations near the top of the $1\Sigma^-$ well."

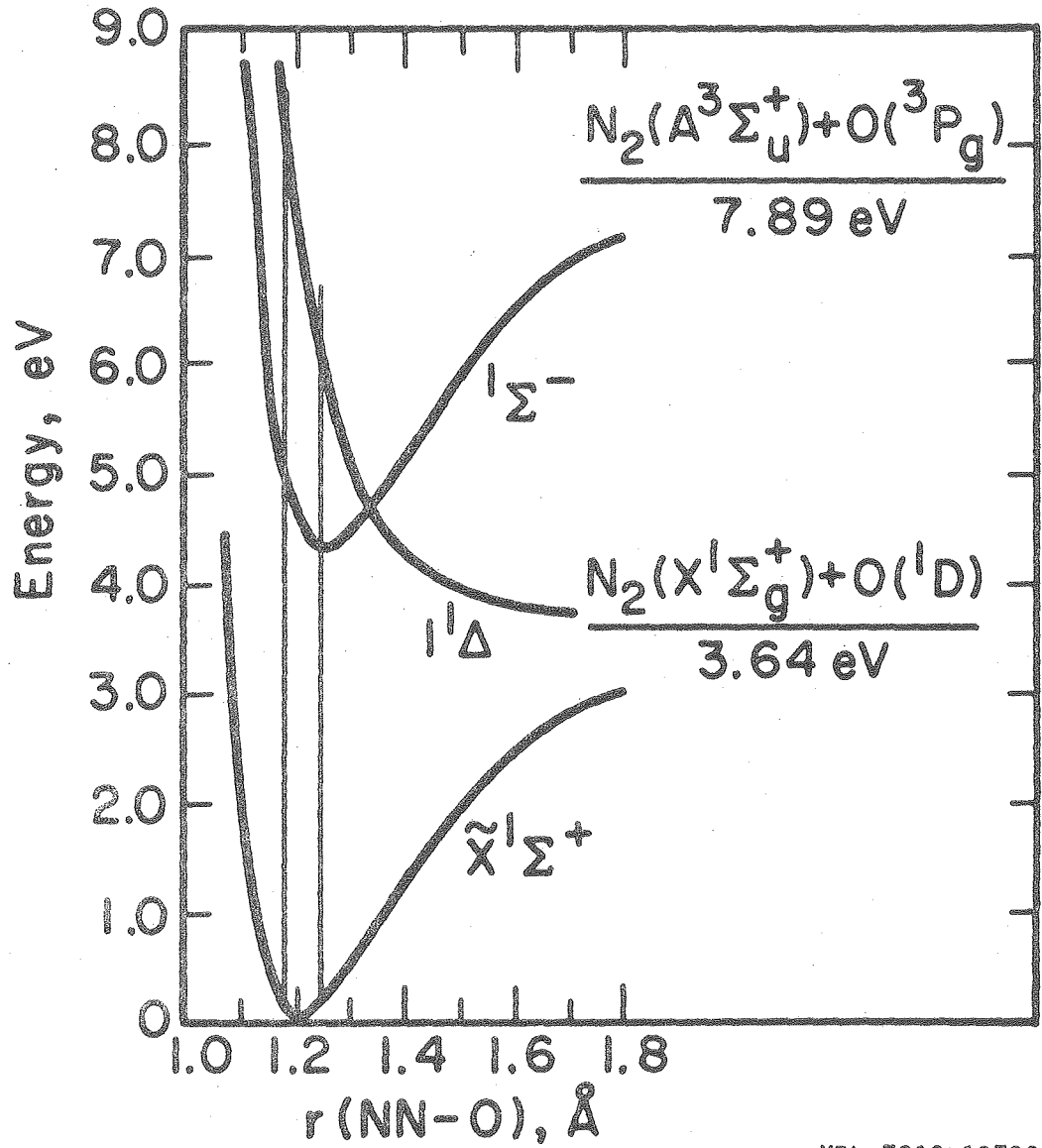
The authors state that ordinarily such vibronic coupling would be unlikely due to poor vibrational overlap, however because the minimum of the $1\Sigma^-$ state "accidentally" (their words) is near the 1π repulsive asymptote, therefore the "kinetic energy of translation in the 1π state and of vibrational motion in the $1\Sigma^-$ state will be very nearly the [same so that] the wavelengths of the vibrational wavefunctions of both states will not be very different."

In fact however, they calculate the minimum of the $1\Sigma^-$ state as 4.23 eV and the minimum of the 1π and 1Δ repulsive states is 3.64 eV. The Chutjian and Segal study can not explain the temperature

dependence noted by Holliday and Reuben, nor much of the new experimental evidence offered in this study.

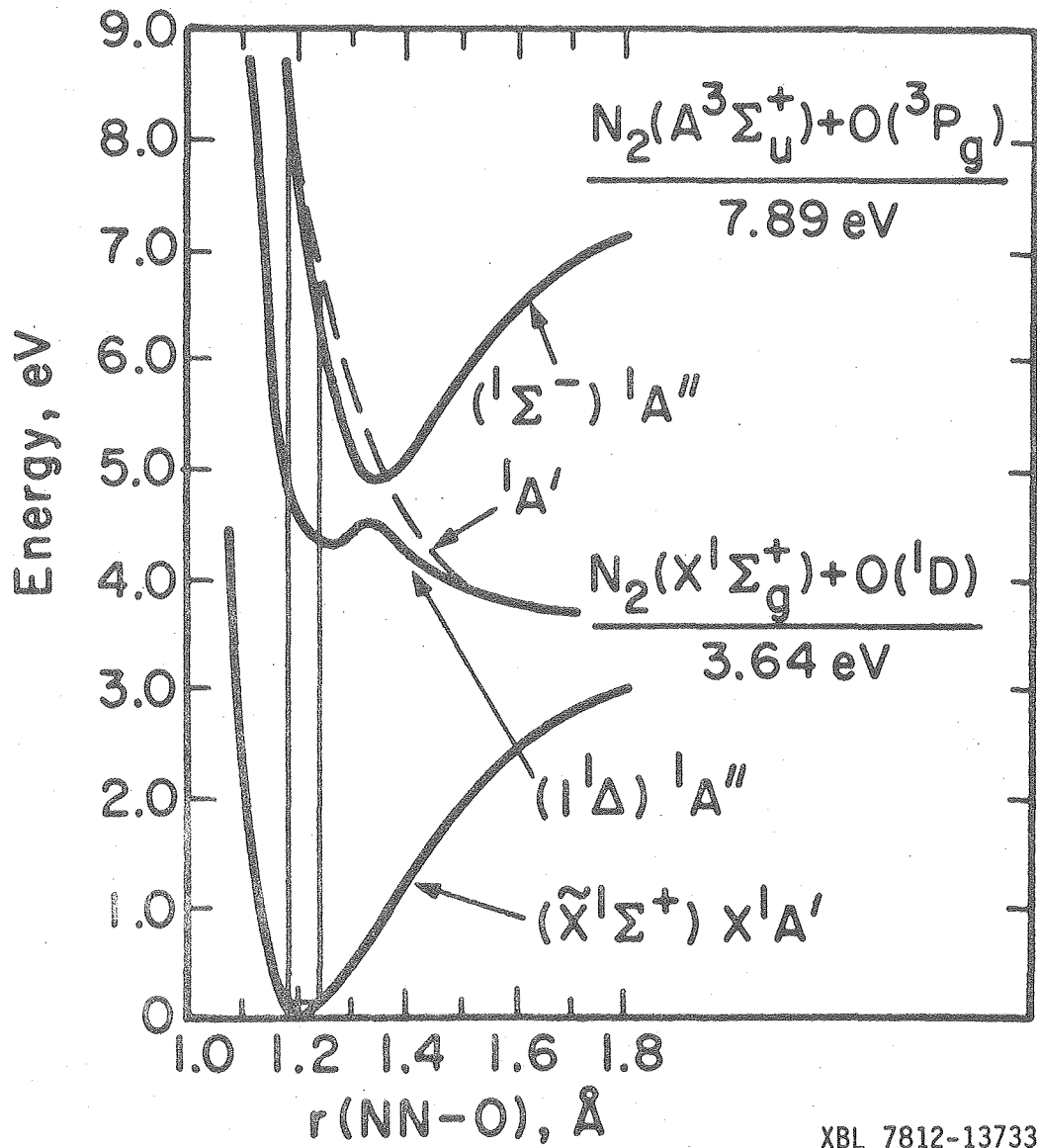
By carrying the original hypothesis of Chutjian and Segal one step further, and discarding their theory of vibrational resonance, another interpretation of the photodynamics arises, which is compatible with the new experimental evidence of this study. In lieu of further, more definitive assignments, I have tentatively adopted the ${}^1\Delta$ state assignment as the repulsive curve which was designated as ${}^1\pi$ by Chutjian and Segal. It should be carefully noted that since both the ${}^1\pi$ and ${}^1\Delta$ states are degenerate, what I apply to one may also apply to the other; this interpretation does not critically depend on the species assignment of the degenerate, repulsive potential curve. The Chutjian and Segal interpretation of vibrational resonance does critically depend on the state assignment of the repulsive curve because a ${}^1\Delta$ state could not directly perturb a ${}^1\Sigma^-$ state since it violates the perturbation selection rules with $\Delta\Lambda = 2$.^{92c}

Both the ${}^1\Sigma^-$ and the ${}^1\Delta$ states are calculated to be bent in Fortunes study, so that ${}^1\Sigma^-$ becomes ${}^1A''$ in C_s symmetry and ${}^1\Delta$ as well as ${}^1\pi$ will lose their degeneracy and will both split into ${}^1A'$ and ${}^1A''$ components in C_s symmetry. Figure 26 was taken from the Chutjian and Segal study except that the repulsive state has been tentatively relabeled ${}^1\Delta$. It is clear from this figure that the Franck-Condon region, indicated by the two vertical lines, does not intersect a turning point of the ${}^1\Sigma^-$ state near the 6.8 eV energy at which structuring is observed. Let us then assume that due to the bent geometry of both electronic states, the potential curves of figure 26 interact to yield an avoided



XBL 7812-13732

Figure 26



XBL 7812-13733

Figure 27

crossing as indicated in figure 27. This is the hyper conical intersection discussed by Herzberg⁴⁹ which results in an avoided crossing at all points except the point of linear intersection, which is allowed to cross. Therefore, in a strict linear geometry of the upper states no mixing can occur, and the interpretation of figure 26 is the correct one. Only the $^1A''$ components interact, and the Franck-Condon region now sees a turning point which would have vibrational overlap and thus give rise to a structured spectrum. Unlike the HNO study of Herzberg, the $^1A'$ component originating from $^1\Delta$ in this case, could only remain unperturbed and give rise to a continuous absorption. The resultant spectrum would consist of vibrational bands superimposed on a continuous background, as is observed.

3. Vibronic Enhancement of Transition

Account must also be taken of the large, fundamental differences of the derived (000) and (010) state spectra, as shown in figure 17. By thermal excitation of the ν_2 mode in the ground electronic state, the resulting ψ_{ev} is then ${}^1\pi$. In $C_{\infty v}$ symmetry all transitions are allowed, however it is only through the excitation of the bending mode that the molecule may be considered to some degree in C_s symmetry. Thus by excitation of the bending mode, the transition moments to the continuous state as well as to the bound state are both enhanced, as has been observed for the (010) state spectrum.

In the cold, vibrationless state, (000), there cannot be vibrational interaction in the ground electronic state and so even though mixing of the ${}^1\Sigma^-$ and ${}^1\Delta$ eigenfunctions in the upper electronic states occur through their ${}^1A''$ components, in no manner may the $X{}^1\Sigma^+$ ground state be considered in C_s symmetry. The transition moment for ${}^1\Sigma^- \leftarrow X{}^1\Sigma^+$ then remains strongly parity forbidden and ${}^1\Delta \leftarrow X{}^1\Sigma^+$ remains angular momentum forbidden and very little structuring is observed on a weaker continuum. Yet, a weak progression is noted with a spacing of 970 cm^{-1} which is very close to $2\nu_2'$ for $\nu_2' = 480 \text{ cm}^{-1}$. Figure 13 demonstrates that for alternate, odd ν_2' levels in ${}^1\Sigma^-$, the vibronic transition ${}^1\pi \leftarrow X{}^1\Sigma^+$ is allowed. This is interpreted as due to bending interaction of the upper state and should have a spacing observed at low temperatures of $2\nu_2'$, as is observed. This proof of a vibronically-induced transition-- consecutive values of ν_2' in the hot bands and alternate values of $\nu_2'' = 0$ -- confirms the same conclusion reached by Innes,¹⁰⁷ using conventional Herzberg-Teller theory of vibronically induced transitions.¹⁰³⁻¹¹²

Lastly, the observed decrease in the fundamental frequency of ν_2 in the upper electronic state relative to the ground electronic state is reasonable since the transition involved has been interpreted as $n \rightarrow \pi^*$ ¹⁴, and in this context the presence of a π^* electron would lessen the bond order, which will increase the internuclear separation and cause a reduced fundamental frequency.

A further theoretical discussion of vibronically induced transitions is provided by references 117 to 125.

H. Conclusions

1. Experimentally Deduced Conclusions

A series of measurements of the absorption spectrum of nitrous oxide at 11 different temperatures indicates a pronounced effect of temperature on the spectrum. The active vibration responsible for this temperature effect has been shown to be ν_2 and using its infra-red fundamental frequency, it is possible to deconvolute the spectrum of nitrous oxide into the normalized contributions of two vibrational modes of the ground electronic state. These may be used to predict the spectrum over a wide temperature range, and their comparison points to the role of vibronic interaction of the ground electronic state and its bending vibration. In the (010) state spectrum both the continuous and the structured absorption are seen to be markedly enhanced relative to the spectrum of the (000) vibrational state.

Analysis of the observed banding indicates that ν_2' levels are selected by the (000) state, this supports the theory of vibronically induced transition along with the comparison of the (010) and (000) state spectra. The peaks have been tentatively assigned; although the exact quantum numbers of the upper state bending mode are not known, from the presented theory of vibronically induced transitions, the assignment of the alternate ν_2' levels selected by the (000) state should be to an odd quantum number. On the basis of the large difference between the region of structuring and the calculated minimum of the ${}^1\Sigma^-$ potential well, it is expected that these are transitions to high vibrational quantum numbers of ${}^1\Sigma^-$.

Fortunately, on the basis of theoretical calculations, the only bound singlet state in this region is the $^1\Sigma^-$. Triplet states also exist; however, transitions to these states would require overcoming an additional degree of a forbidden nature. Chutjian and Segal have attempted to explain the transition to the $^1\Sigma^-$ through vibrational resonance since the Franck-Condon overlap with this state is well separated from a classical turning point of the potential curve and is then expected to be quite poor. However, if the state is bent in its equilibrium configuration, it has been suggested that the resulting double conical intersection of the $^1\Sigma^-$ with a repulsive, degenerate state may occur through their $^1A''$ components in C_s symmetry. This would be expected to yield an avoided crossing in all orientations except the colinear one, and the new resulting potential well would then have a classical turning point within the Franck-Condon region at 6.8 eV.

No rotational structuring can be definitely determined, even with the high resolution of a three meter vacuum spectrometer. However, from the intensity pattern of the observed vibrational features, there is evidence that the upper electronic state is bent to a large extent. This is in agreement with theoretical calculations and the model provided by Walsh diagrams.^{14,113}

2. A Proposed Mechanism of Predissociation

The lack of rotational structuring, even the coarse rotational structuring arising from the K selection rules may be due to predissociation of the molecule. The short lifetime of a predissociated state would smear out fine structure due to uncertainty broadening. A mechanism of predissociation may be proposed using the theory developed in this study:

The double conical intersection of $1\Sigma^-$ and 1Δ would break down in the linear configuration. If then, during the bending motion of the excited states, the molecule passes through the linear configuration and simultaneously the ν_1 vibration is at its left hand turning point as indicated in figure 26, then the molecule would be expected to fly apart into the fragments N_2 (X^1+) and O ($1D$) when these two combinations are simultaneously met. This is because in the linear configuration the avoided crossing would not occur and the left hand turning point of ν_1 would be the repulsive 1Δ state correlating with N_2 ($1\Sigma^+g$) and O ($1D$). In fact, it is interesting that the photochemical studies of Bradley et al¹¹⁴ point to an excited state of N_2O with an estimated lifetime of 10^{-8} second, although this unconfirmed lifetime may also result from other physical processes such as quenching or fluorescence.

Acknowledgments

To Professor Harold S. Johnston I wish to express my unequivocal appreciation for his role in my scientific education. As an educator he has helped guide my passage through graduate school at the necessary moments while understanding my preference for self-education. As a researcher his experience and insight has been of invaluable aid to this work: many of the ideas presented here have been refined under the scrupulous examination of Professor Johnston while his philosophy of research has allowed me the opportunity to carry on my own independent work.

I also wish to thank John Conway and George Shalimoff of the Lawrence Berkeley Laboratory who have provided an additional sounding board for my ideas as well as occasionally providing equipment and laboratory space. Special thanks are also due to Professor Andrew Yenchu of SUNY Albany who has provided guidance and direction from the beginning of my undergraduate studies.

I also wish to express my appreciation to the personnel of the support facilities of the Department of Chemistry and of Lawrence Berkeley Laboratory. I especially thank Mr. Locke Yow of the Chemistry Glass Shop for the competence and patience he has shown in his work.

Support of an entirely different nature was contributed by Ms. Sharon Altman. To her I express my sincerest appreciation for her emotional aid and her understanding. In most every sense she was involved in this work.

Finally, I wish to thank the University of California and the U.S. Department of Energy for the financial aid provided during my

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Appendices

A. Results of ^{15}N Substitution

1. Temperature Effect--Raw Data

To prove the reproducibility of the previous results and to demonstrate the extent of the observed isotope shift on the structured absorption, the ^{15}N isotopes of nitrous oxide, N^{15}NO , ^{15}NNO , $^{15}\text{N}^{15}\text{NO}$ were purchased from Prochem (British Oxygen Co.) with a stated isotopic purity of better than 99.0%.

Gas purity and isotopic labeling purity were further checked by measuring the infrared frequencies of the various isotopes with a Nicolet 7199 Fourier-Transform Spectrometer and comparing this result with literature values^{128, 129}. All experimental procedures used were identical to the previous section, however a longer wavelength range was covered, 197 to 172 nm for six temperatures using 1250 data points for each spectrum.

Signal averaging was carried out for two runs on both background and sample spectra at slightly less resolution, to improve the signal/noise ratio (0.7A). For optimal comparison with the unlabeled isotope, regular N_2O (Matheson) was also run in the same manner.

The result of the temperature dependent absorption of each isotope is shown in figures 28 a-d for six temperatures from 197 to 172 nm. As expected, isotopic substitution does not significantly alter the intensity of absorption at a given temperature. It is also clear from these figures that even at high temperatures the observed structuring is quite weak at longer wavelengths.

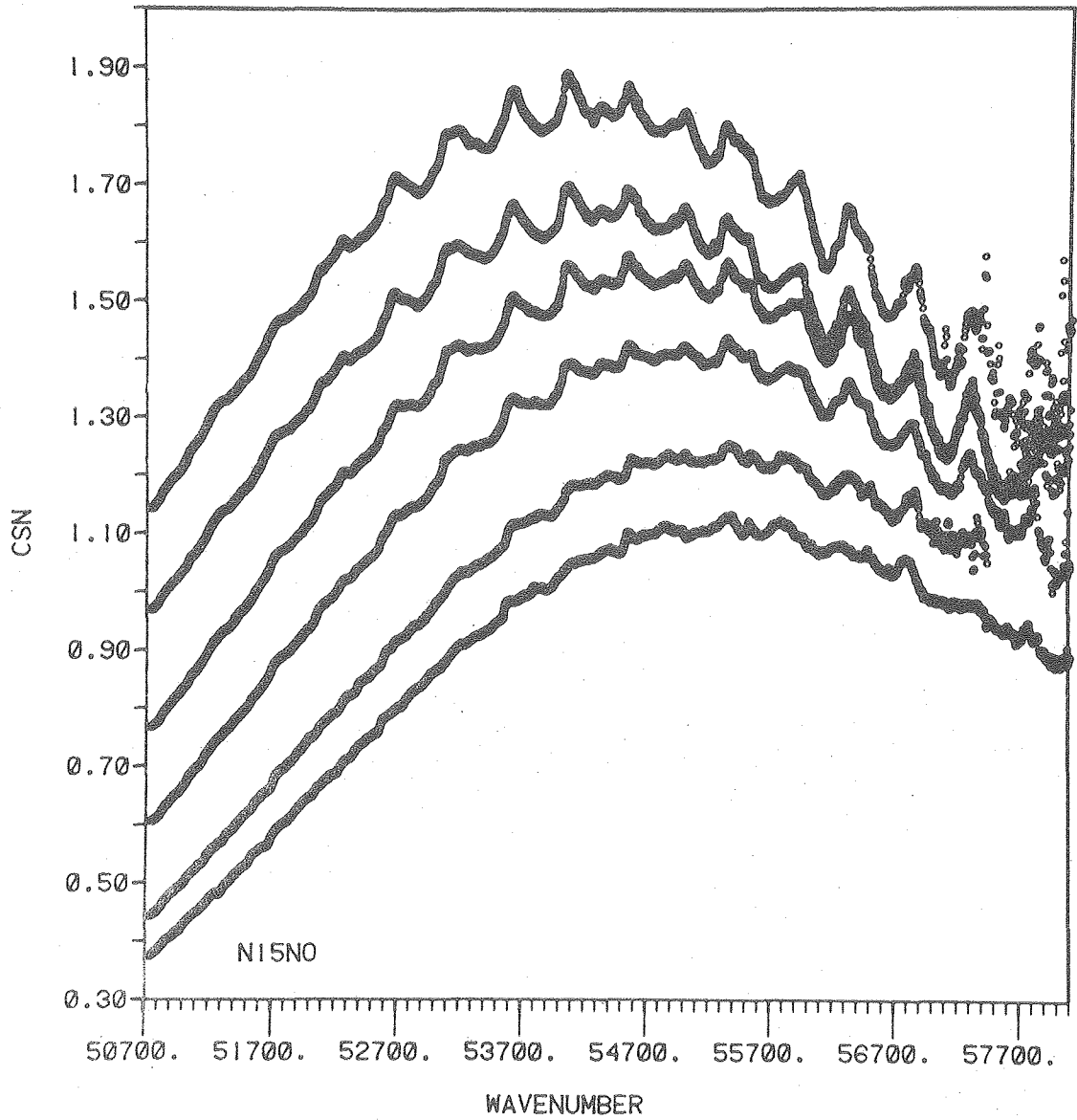


Figure 28a

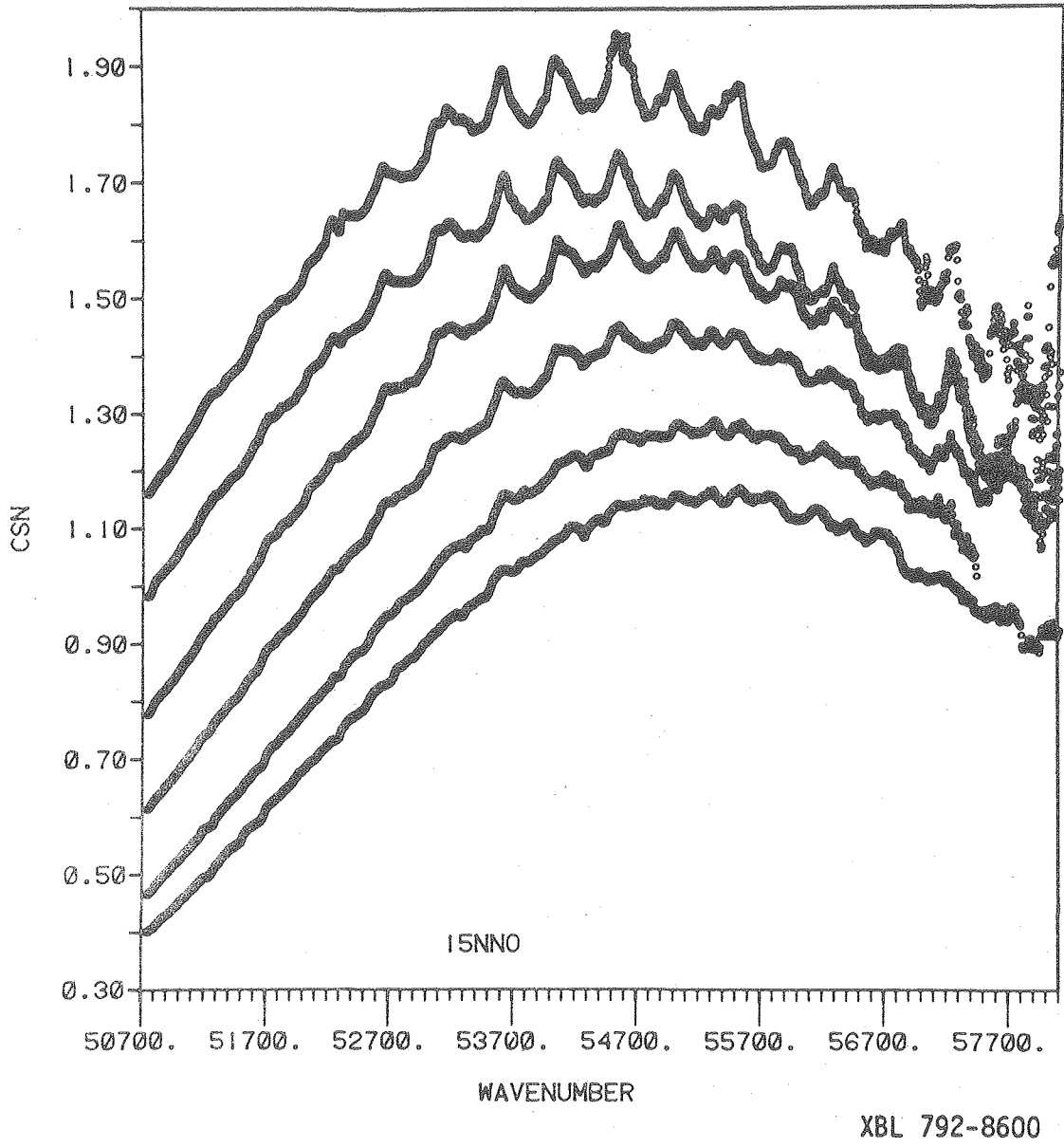
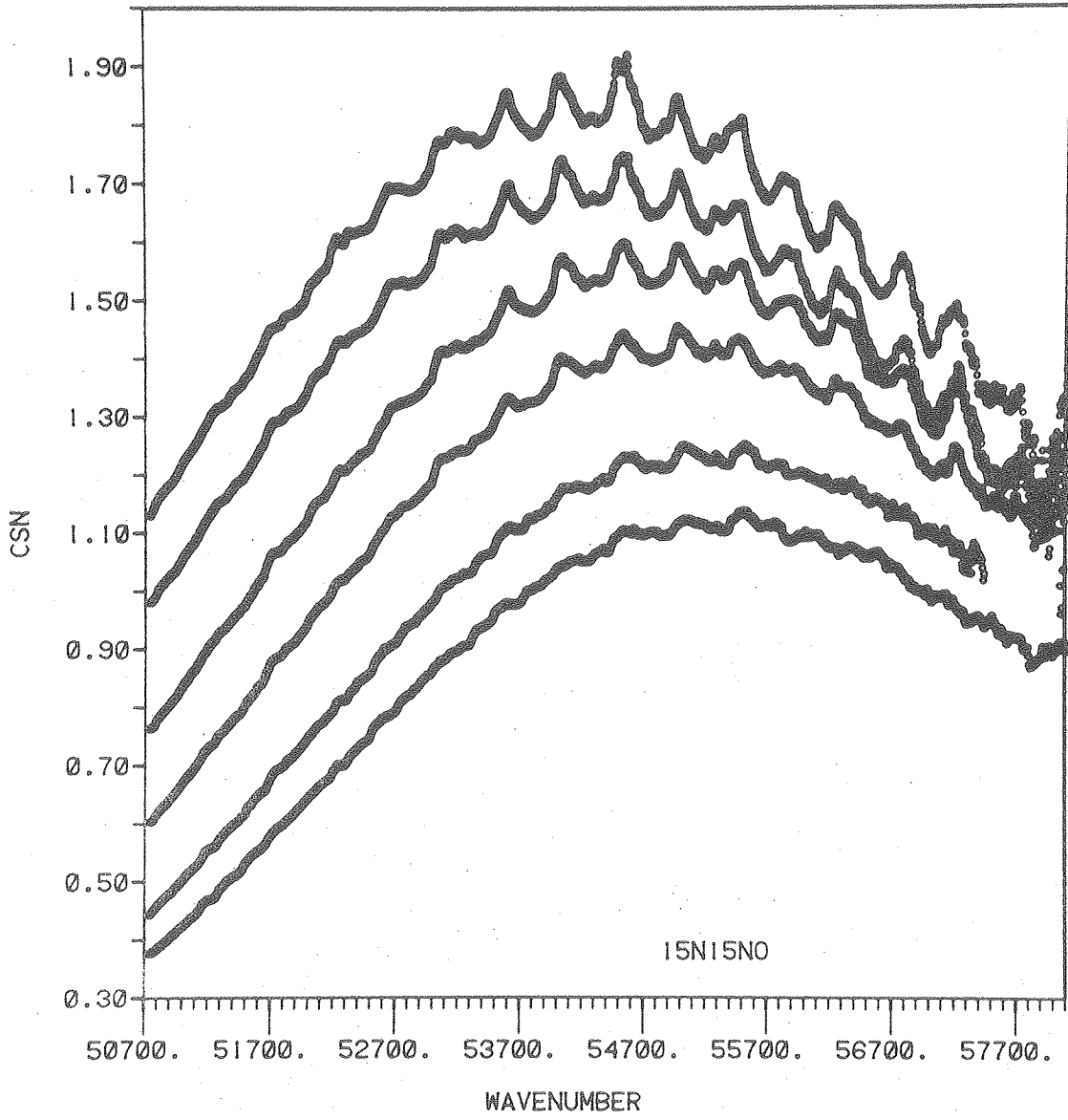
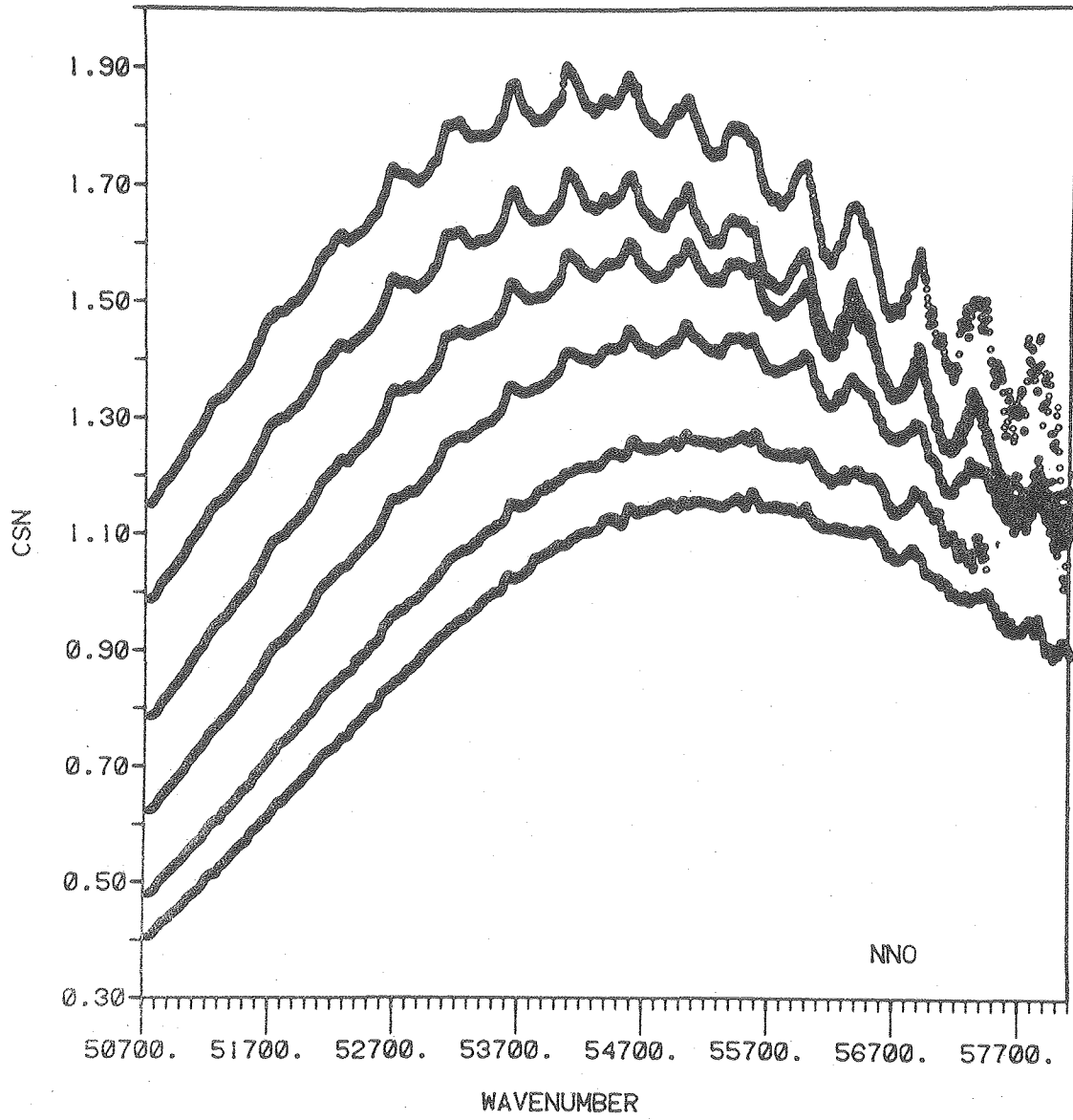


Figure 28b



XBL 792-8588

Figure 28c



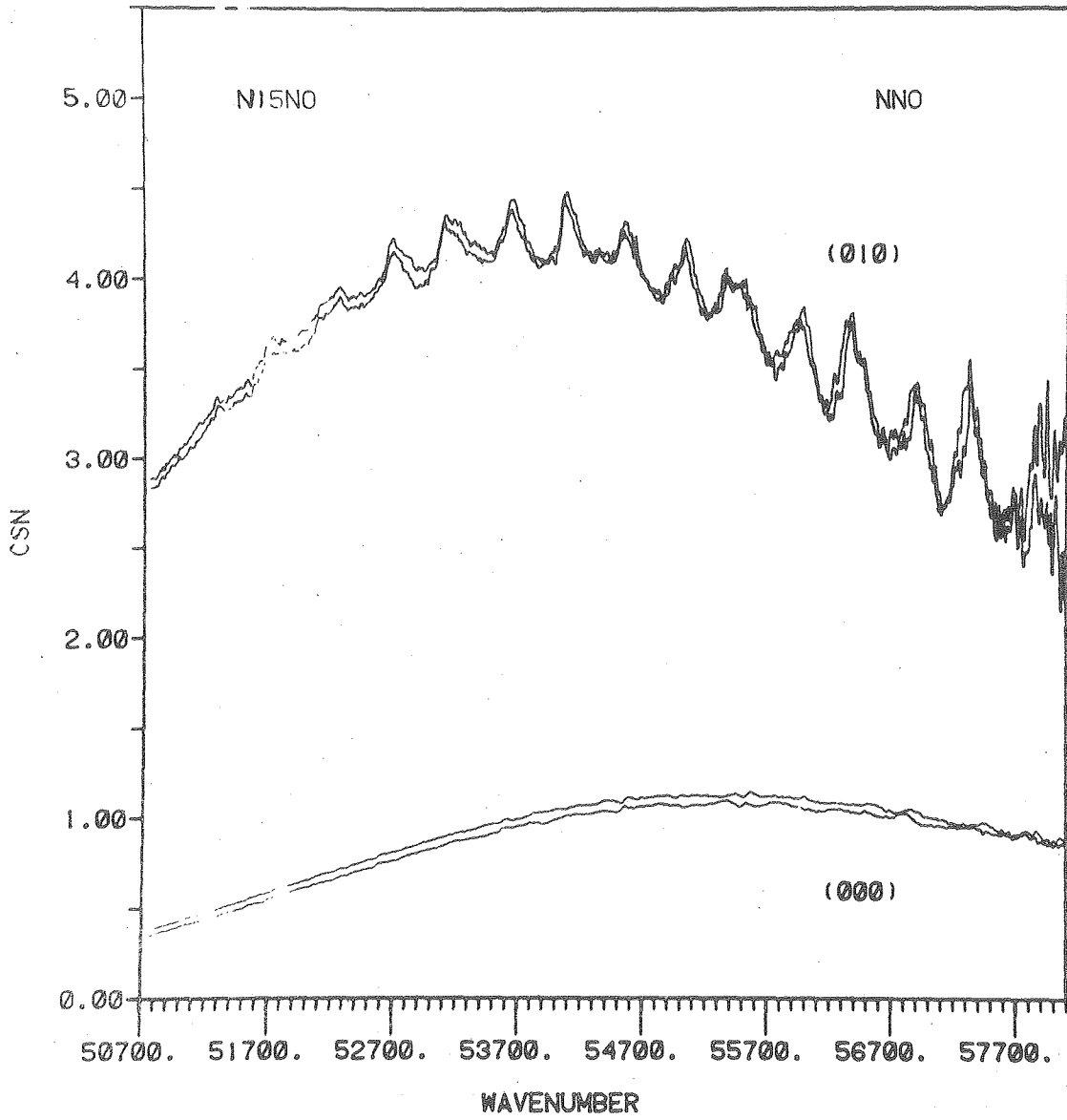
XBL 792-8580

Figure 28d

2. Deconvolution and Isotope Shift

Using the unique infrared frequencies of each nitrous oxide isotope, it is possible to deconvolute the raw data presented in figures 28 a-d using the first order or second order iterative procedures outlined in the last section. Figures 29 a-f show the result of a first order deconvolution into the (000) and (010) state spectra. To demonstrate the observed isotope shift, figures 29 a-f are shown superimposed, as a permutation of all possible isotope comparisons. In each case, the extent of the isotope shift, as indicated by the displacement of the structured spectra, is seen to increase at the shorter wavelengths. At longer wavelengths, the isotope shift is minimal and the peaks most nearly coincide. This is to be expected, since the extent of isotope shift would be greatest for high quantum vibrations, corresponding to the short wavelength transitions. It is also seen that the extent of isotope shift is greatest for the most dissimilar isotopes, such as NNO and $^{15}\text{N}^{15}\text{NO}$ whereas the isotope shift between more nearly similar species, such as $^{15}\text{N}^{15}\text{NO}$ and ^{15}NNO , show the least displacement. It is also seen that the observed isotope shift can be so large as 125 cm^{-1} at the short wavelength end of the spectrum. In comparison with the isotope shift of less than 15 cm^{-1} for $\nu_2'' = 1$ in the ground electronic state, this large isotope shift appears to indicate transition to high quantum vibrations in the upper electronic state, in agreement with the theory discussed previously.

Using the second order deconvolution procedure to solve for the (000), (010) and (020) state spectra is also revealing. With the larger wavelength range of this study, the (020) state spectrum is



XBL 792-8607

Figure 29a

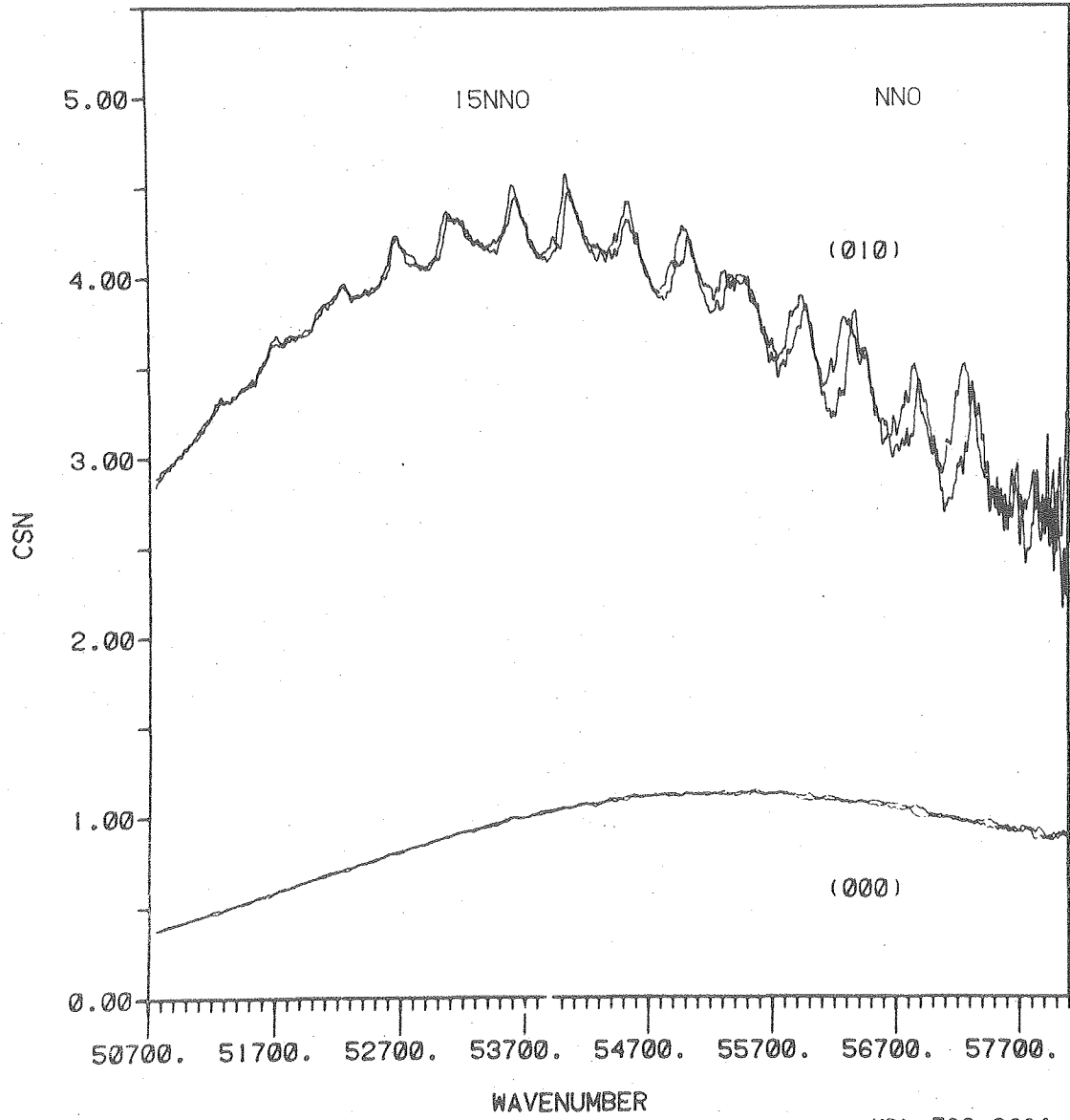
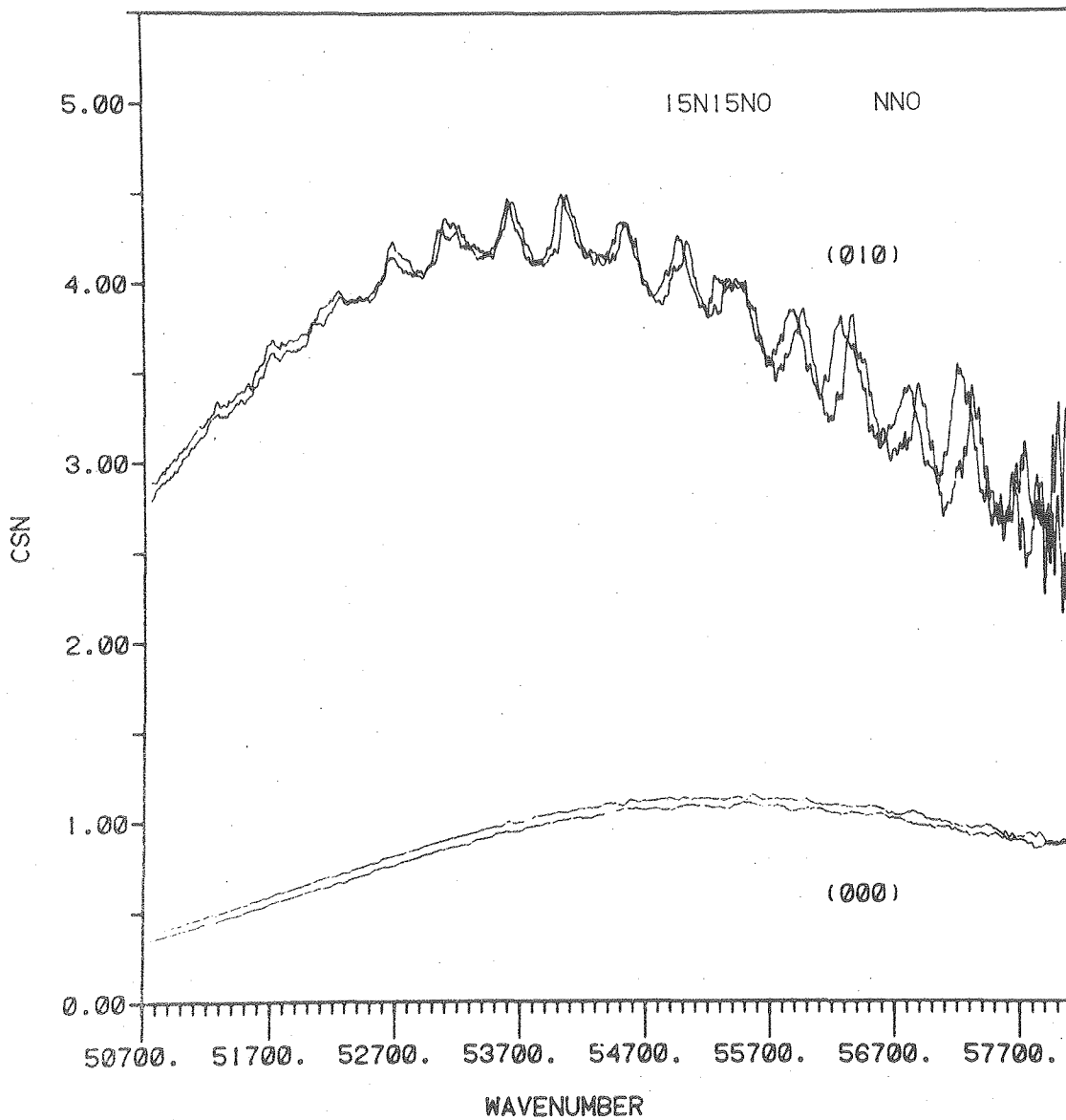
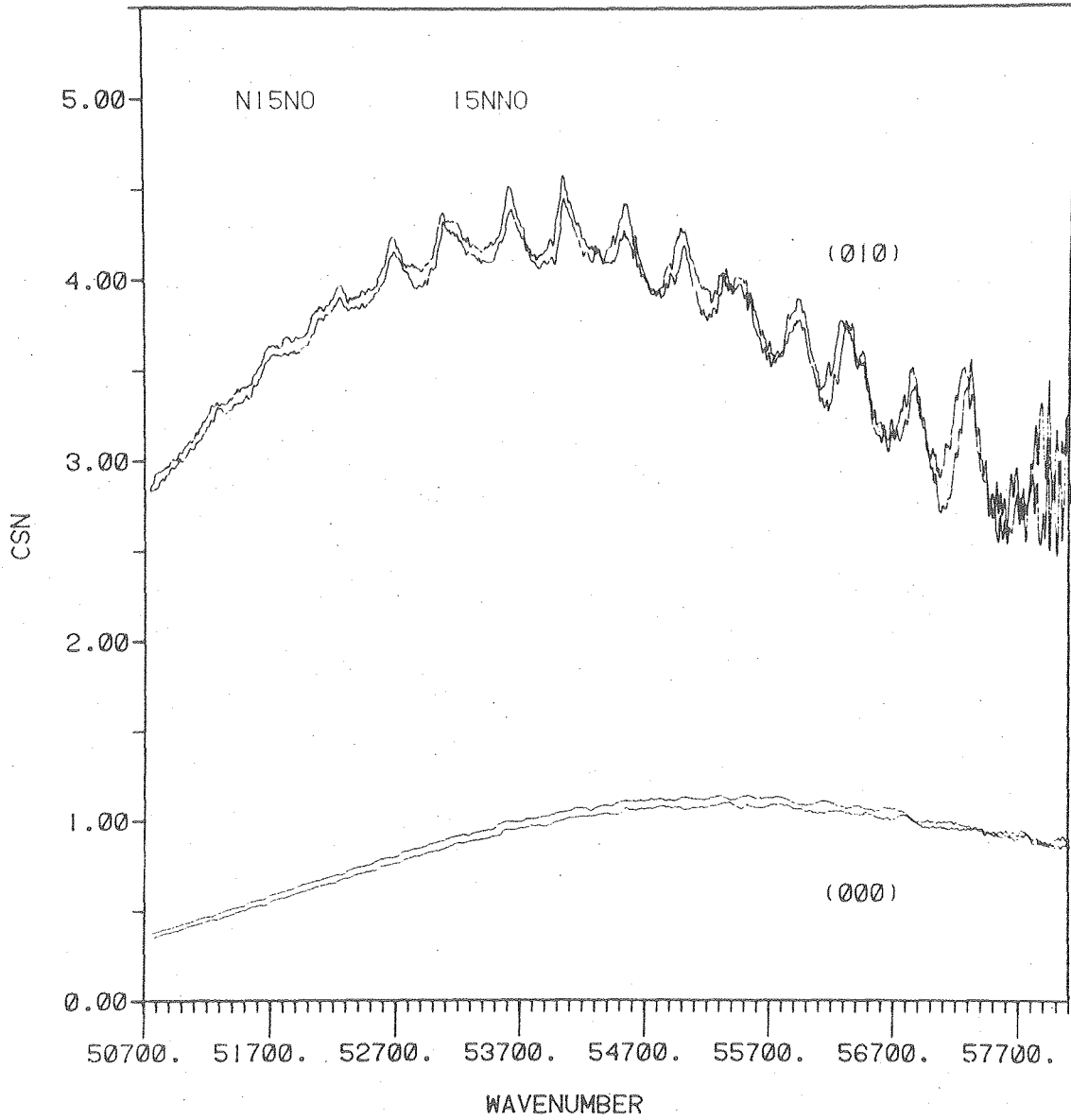


Figure 29b



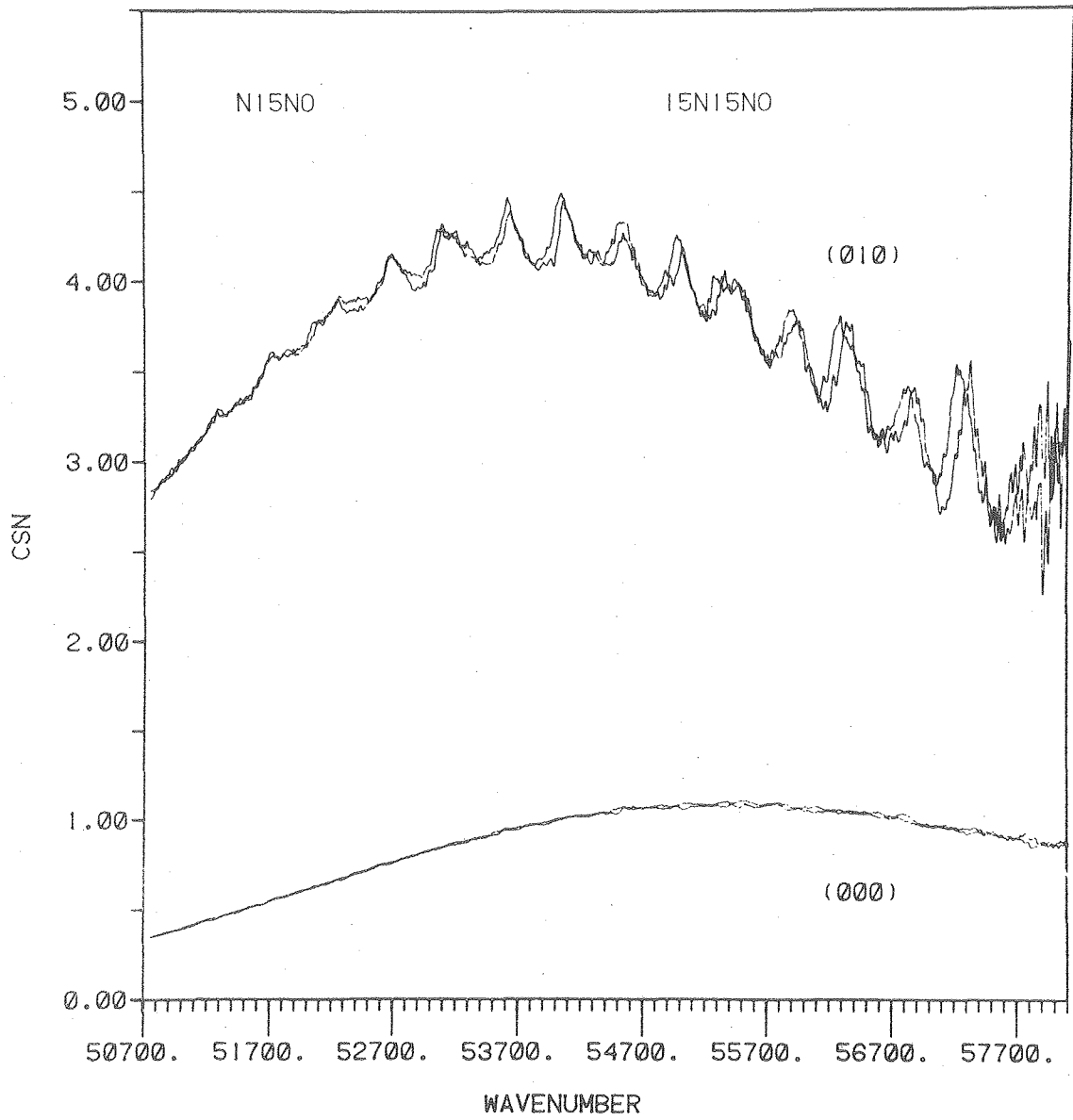
XBL 792-8605

Figure 29c



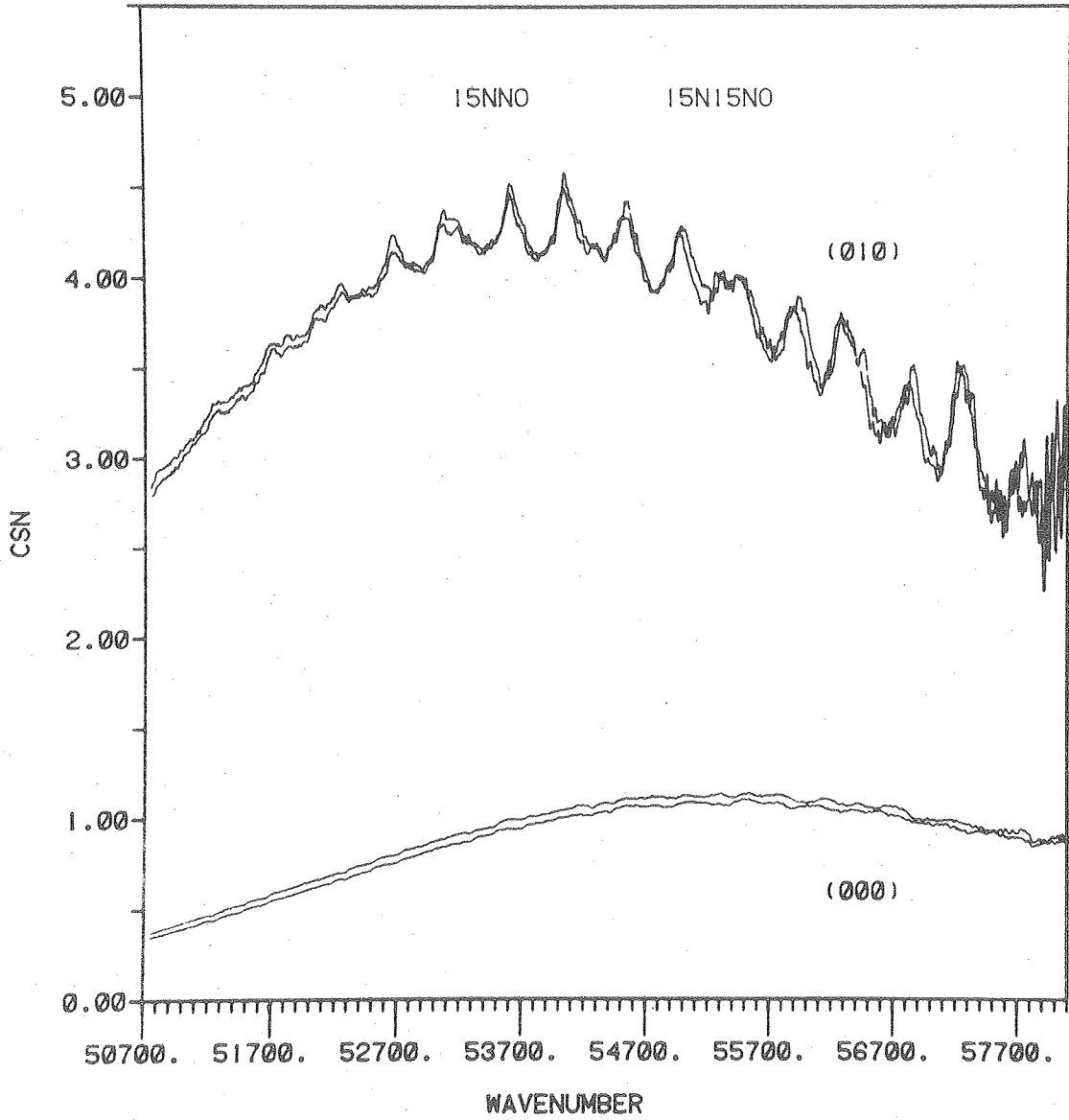
XBL 793-8693

Figure 29d



XBL 793-8694

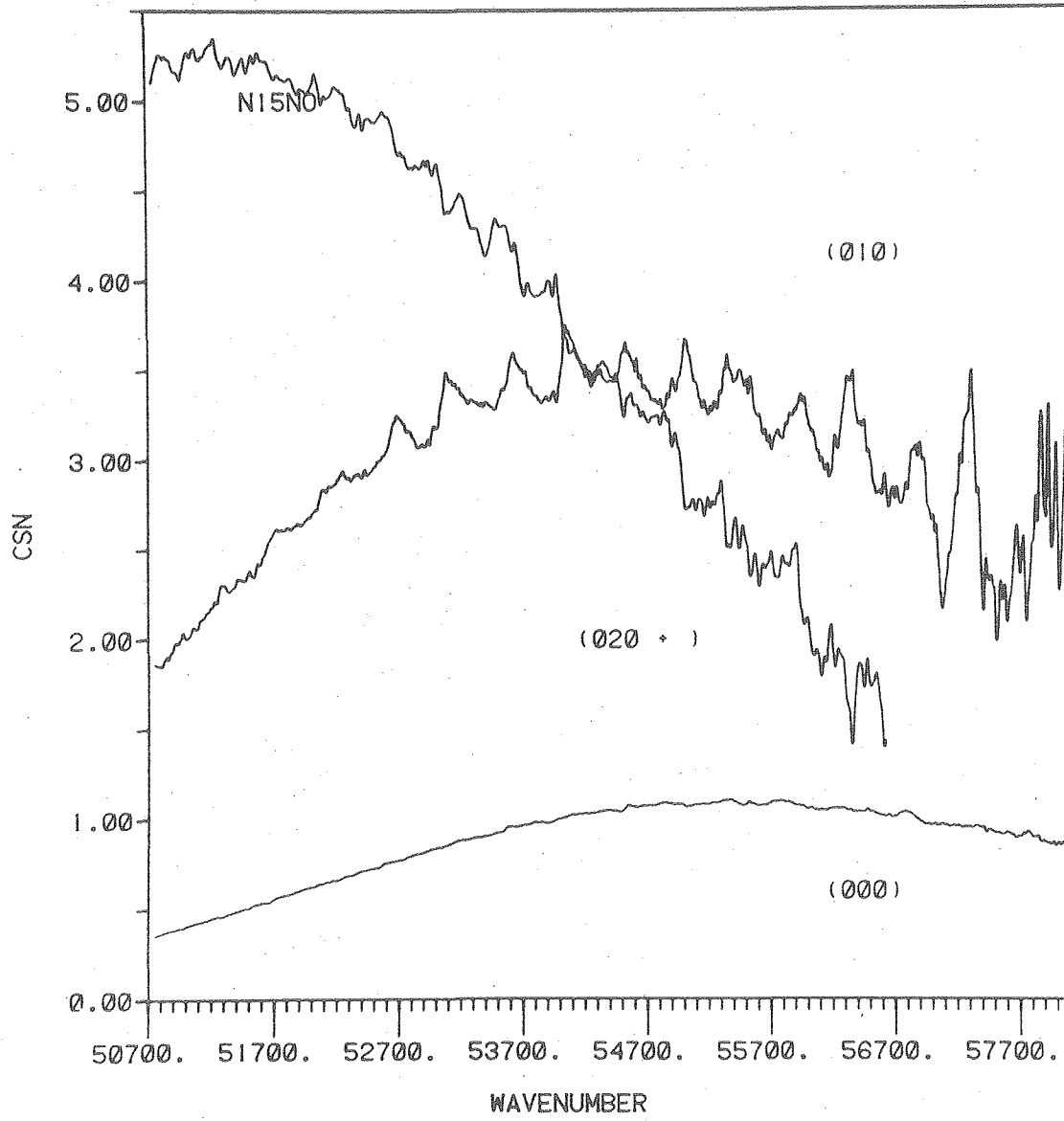
Figure 29e



XBL 792-8603

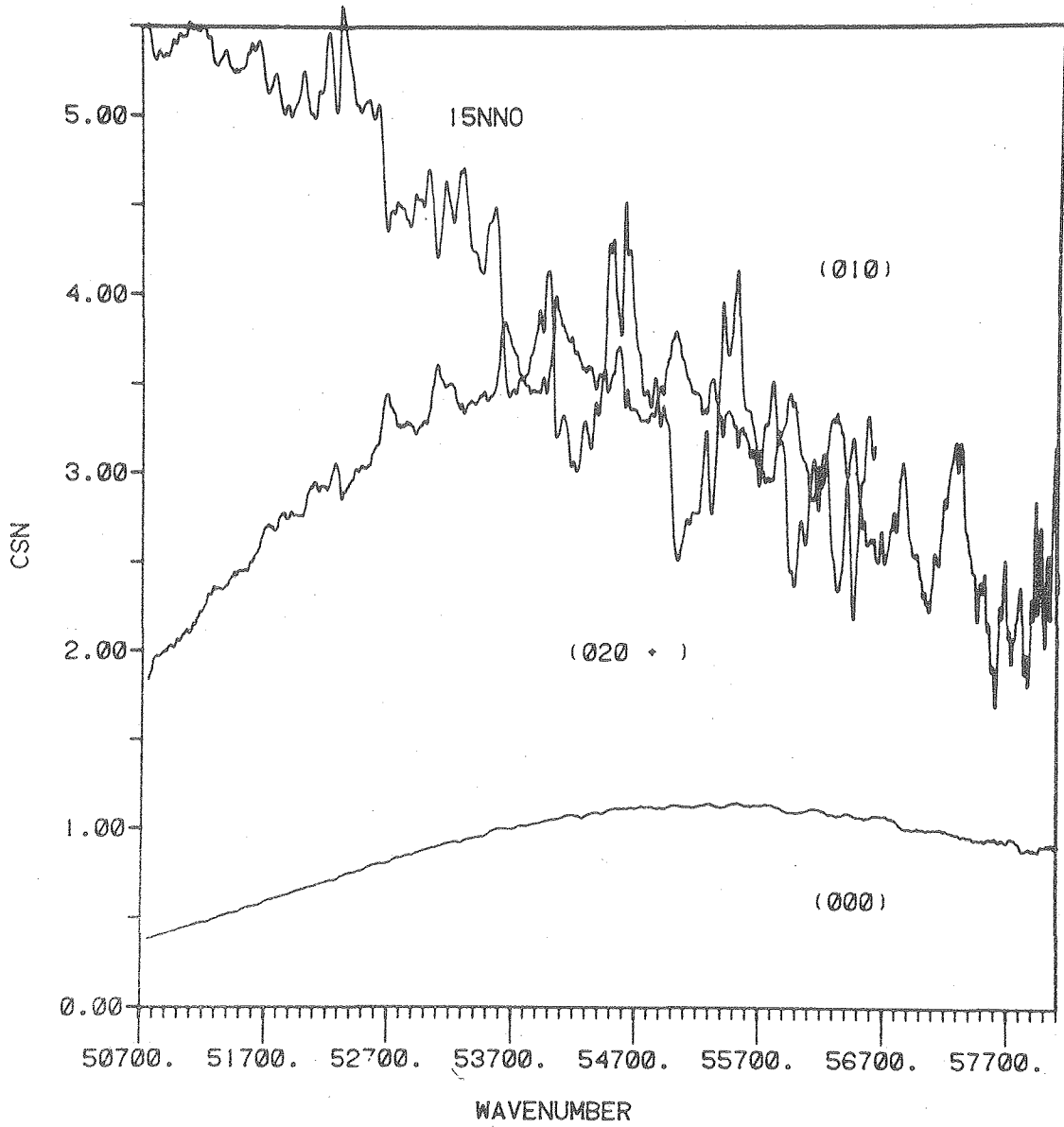
Figure 29f

is now more clearly defined. As seen in figures 30 a-d, the (020) state spectrum is slightly more intense than the (010) state spectrum and is noticeably red-shifted. Unlike the result in the previous section, here the (020) state spectrum extends weakly to shorter wavelengths, although to avoid the very large noise resulting from small equilibrium populations of (020) and their minimal contribution at short wavelengths it was necessary here to use a seven point digital smooth and display only the portion of the (020) state spectrum above 175 nm.



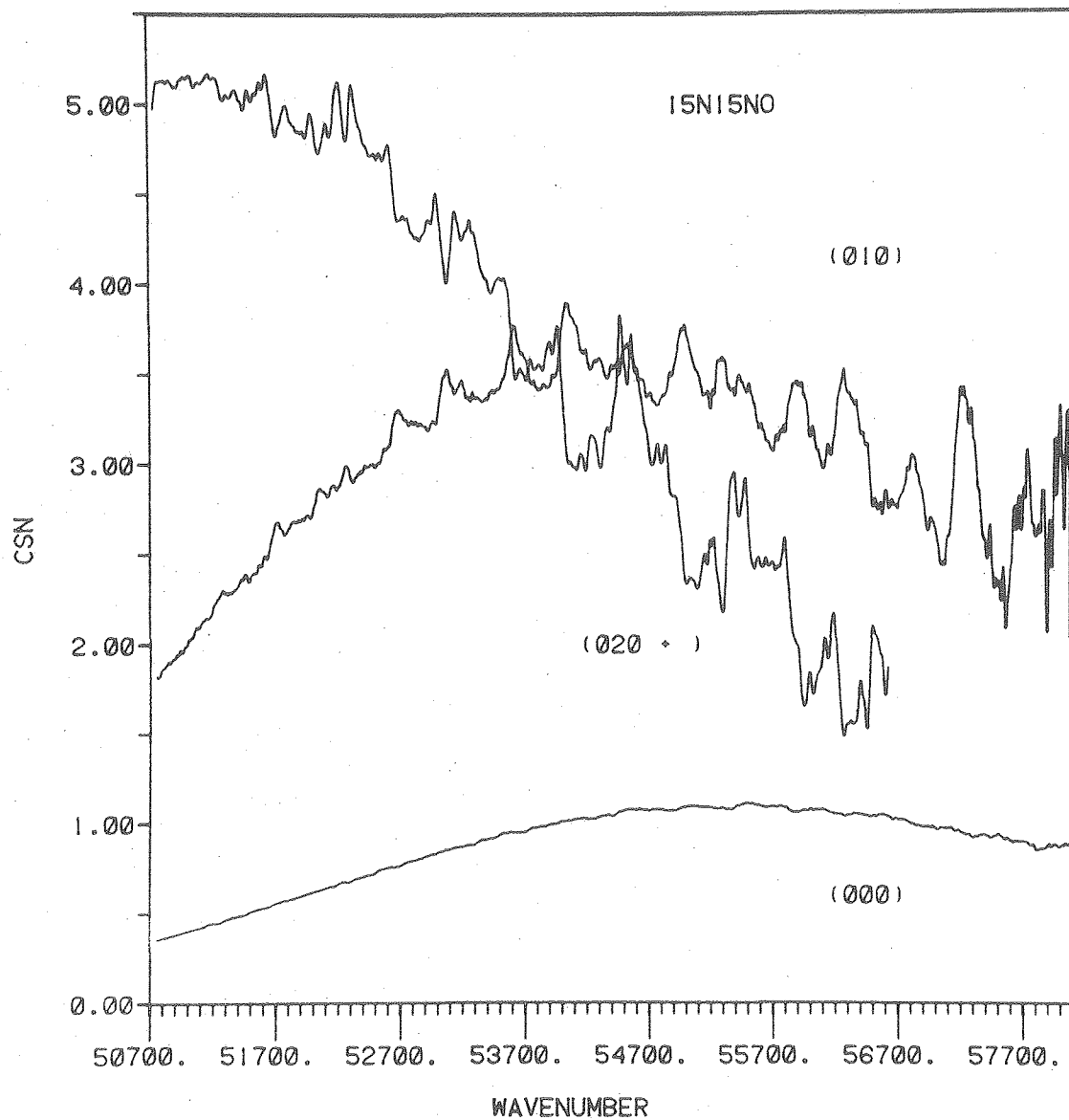
XBL 792-8596

Figure 30a



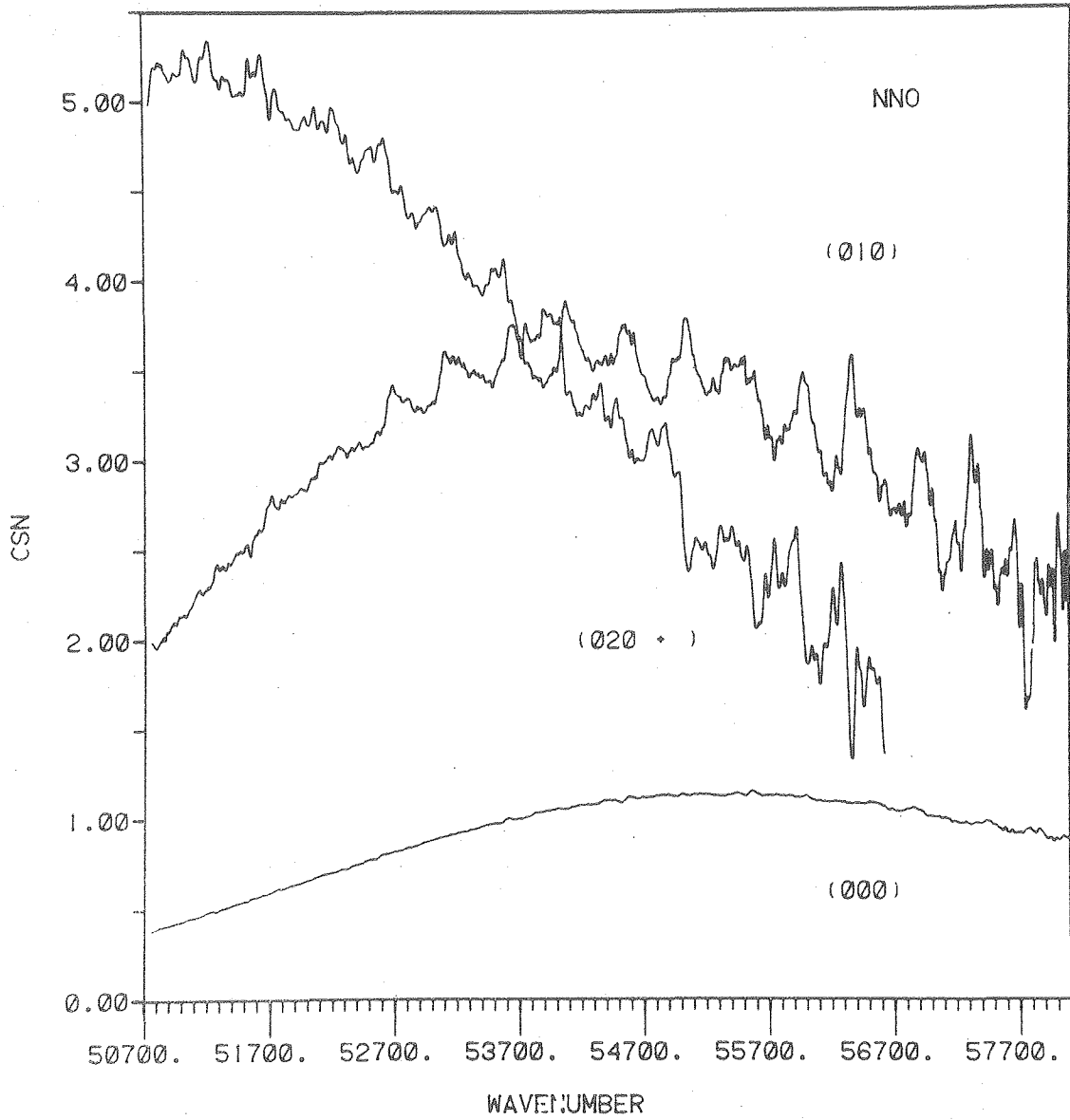
XBL 792-8589

Figure 30b



XBL 792-8584

Figure 30c



XBL 792-8576

Figure 30d

Appendix B: An Anomalous Result

In one sample of isotopic nitrous oxide, ^{15}NNO purchased from Prochem, an intensely strong and sharp absorption was noted. The sample, batch number 19X95 was found to contain a large amount of noncondensables in liquid nitrogen even though the flask was received in good condition with the seal unbroken. The noncondensables were pumped off and the remaining gas was purified by vacuum distillation. A mass spectrum of the purified gas indicated 95% atom purity of ^{15}NNO , in agreement with the manufacturers specifications, without other noticeable impurities.

Unlike the other samples of isotopic nitrous oxide, including a sample of 99% atom purity ^{15}NNO , the sample alone indicated a series of sharp, featureless absorptions following an apparent progression. Absorption spikes were noted at 201, 197, 183 and 179 nm in the intensity pattern 3:1:3:1. By comparison with the second sample of ^{15}NNO it was concluded that these absorptions were the result of an impurity present in the 95% sample of ^{15}NNO since this other sample of the same isotope did not show these features.

Spectra of this anomalous absorption were also recorded on the 3 m vacuum spectrograph. At 0.03 Å resolution it was possible to measure the sharpness of these features: the 201 nm absorption had a full-width-half-maximum band width of 0.20 Å while the 197 nm absorption had a FWHM of 0.39 Å. Neither absorption exhibited any additional fine structure at this resolution.

Repeated exposure of the same sample to ultraviolet light weakened the intensity of these absorptions, indicating that dissociative

photolysis was resulting. This eliminated the possibility that the absorptions were atomic in nature. Additionally, the wavelengths noted did not match the absorption lines of any likely atomic species.

The temperature dependence of this unexplained absorption was also measured. From room temperature down to 200 K no significant change in absorption was noted. At temperatures below 200 K the impurity froze out. At 150 K only a very weak absorption could be noted. The 201 nm and 197 nm absorption exhibited a uniformity in their temperature dependence as described above.

In a further effort to identify the impurity responsible for these sharp absorptions, the infrared spectrum of the contaminated sample of ^{15}NNO was recorded on a Nicolet 7199 Fourier Transform Spectrometer. Signal averaging was carried out for 2000 scans of sample and background at 0.06 cm^{-1} resolution. No impurities were identified by these techniques, although the sensitivity of results was enough to detect the "hot" $(001) \leftarrow (100)$ transition of ^{15}NNO in a 10 cm cell. At room temperature 0.2% of nitrous oxide molecules are in the (100) vibrational mode. It is possible that the impurity is not infrared active.

The impurity should not be a trace impurity because of the extremely intense absorption noted in the U.V. Knowing the total pressure of a gas sample and the absorption of these "spikes" in that sample, it is possible to estimate the concentration of the gas impurity as $> 0.1\%$ since a smaller concentration would result in an absorption cross section of greater than 10^{-16} cm^2 .

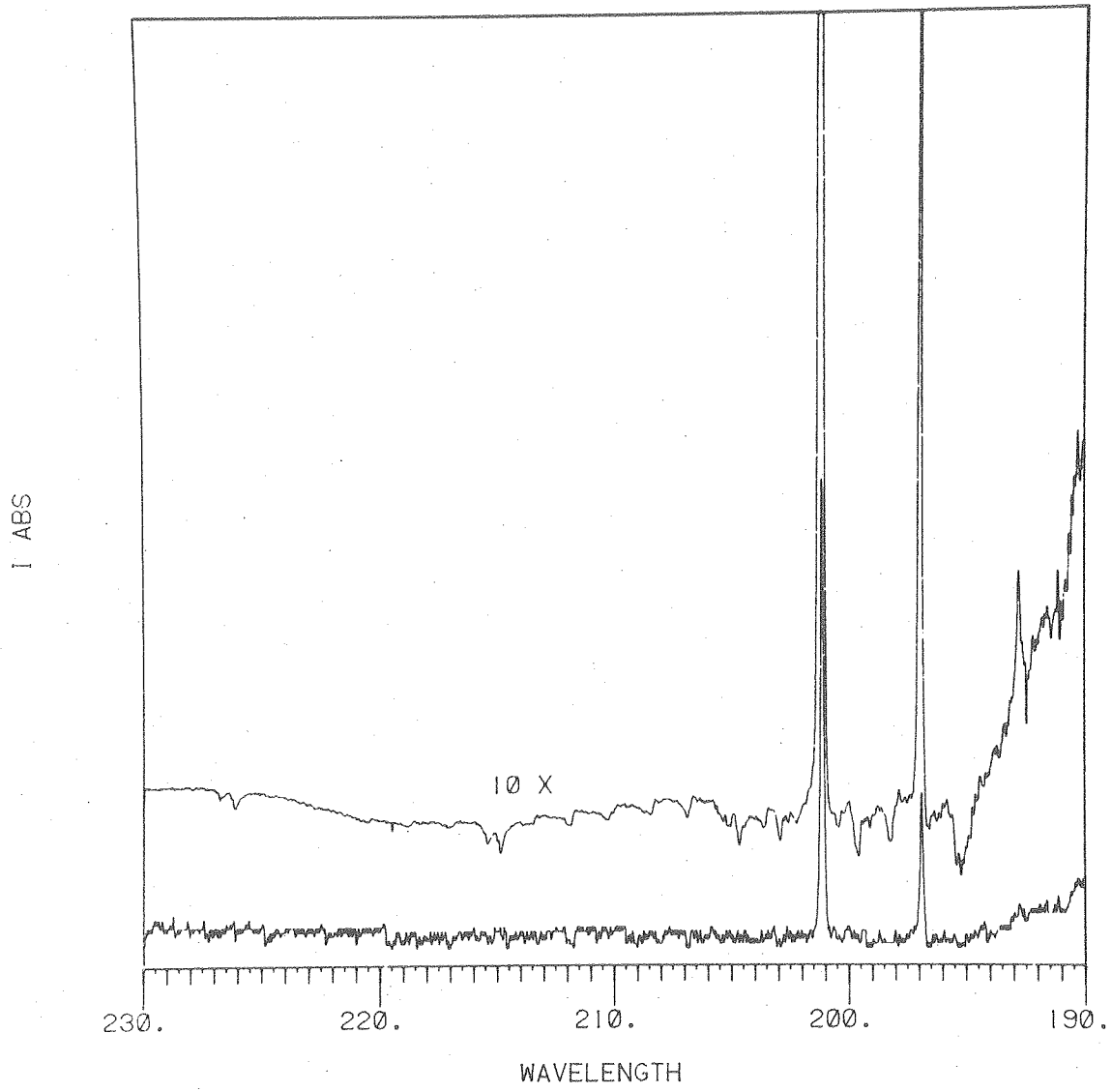
A mass spectrum of the contaminated sample of ^{15}NNO indicated the results shown in Table 8. Trichloroethylene was identified as

Table 8. Mass Spectrum Results for ¹⁵NNO Sample

| Peak No. | Mass | % Rel. Area |
|----------|------|-------------|
| 2 | 16 | 1.78 |
| 6 | 28 | 2.56 |
| 7 | 29 | 2.69 |
| 8 | 30 | 12.17 |
| 9 | 31 | 1.11 |
| 10 | 44 | 3.22 |
| 11 | 45 | 100.00 |

an impurity by this method, but this could not be responsible for the observed spectrum in the U.V.

Further spectra were obtained in the U.V. using a double beam technique in which the sample of 99% ^{15}NNO not exhibiting the spikes was placed in the reference beam of the Cary spectrometer. Using equal measures of the two samples, one in the reference beam and one in the sample beam results in subtracting out the common absorption of nitrous oxide, and leaving the spectrum of the impurities only. The result of this technique is shown in figure 31 at a SBW of 0.3 . Here, two of the spikes are noted at 201 and 197 nm and an additional weak feature is found at 193 nm. It is also seen that the spikes are not features superimposed on a weak absorption but instead the background is flat. The increasing slope below 195 nm is due to oxygen in the spectrometer (not purged for this run). The presence of some weak "negative" absorptions at longer wavelengths in the 10X curve is due to trace impurity of NO in the reference sample. In conclusion, this spectrum is inexplicable since the absorption spikes do not fit the absorption spectra of any likely molecular or atomic species.



XBL 793-8696

Figure 31

C. Computer Programs

1. Deconvolution and Comparison of Observed and Predicted Spectra

PROGRAM FIND 7600-7600 OPT=1 FTN 4.6+452/034 06 FEB 79 22.56.51 8KV PAGE 1

```
1 PROGRAM FIND(INPUT,OUTPUT,FILM,ASPEC,BSPEC,TAPE6=OUTPUT,
A TAPE7=ASPEC,TAPE8=BSPEC)
COMMON/RACY/TEMP(11),QTEMP(11),POPB(11),POPC(11)
COMMON/IGSZZ/Z(200)/NND/SPECT(900),X(900)
5 COMMON/FIT/Y(11,900),Y000(900),Y010(900),YGS(900),GAUSA(900)
DIMENSION Y020(900)
EXTERNAL FONT2
DATA (TEMP(I),I=1,11)/151.,162.,196.,223.,247.,266.,301.,
* 333.,372.,425.,485./
10 DO 12 I=1,900
X(I)=1/((1.00035*(190.02-1/50.))*1E-7)
Y020(I)=0.
12 CONTINUE
15
C ***** GRAPHICS PARAMETERS *****
20 CALL MODESG(Z,6,4MTEST)
CALL VECIG(Z,FONT2,0)
CALL SETSMG(Z,51,1.)
CALL SETSMG(Z,93,000)
CALL SETSMG(Z,103,-1.0)
25 CALL SETSMG(Z,102,-3.)
CALL SETSMG(Z,45,2.25)
C ***** USED TO DRAW CIRCLES FOR DATA POINTS*****
CALL SETSMG(Z,84,3#52)
30 CALL OBJCTG(Z,15.,15.,90.,95.)
C *** 900 DATA POINTS ***
III=900
CALL SUBJEG(Z,52600.,.8,58200.,1.9)
CALL PICTUR(1)
35 DO 15 NN=1,11
DO 16 J=1,900,10
IK=J+9
40 READ 100,(Y(NN,K),K=J,IK)
100 FORMAT(10F 7.4)
16 CONTINUE
45 DO 9 I=1,900
SPECT(I)=Y(NN,I)
9 CONTINUE
50 C ***** PLOTS RAW SPECTRAL DATA *****
C ***** CALCULATES (000), (010), (020 + 030)
C ***** EQUILIBRIUM POPULATIONS FOR EACH TEMPERATURE ***
55 CALL SETSMG(Z,45,7)
CALL POINTG(Z,111,X,SPECT)
CALL SETSMG(Z,45,2.35)
CALL BTEMP(NN)
```

```
15 CONTINUE
60 C INITIALIZE CALCULATION
    CALL SETSMG(2,84,3H$SK)
    DO 7 I=1,900
65 Y000(I)=Y(1,I)
    YG5(I)=Y(1,I)
    7 CONTINUE
70 C ***** NJJ IS COUNTER FOR Y020 ITERATION*****
    NJJ=0
    51 CONTINUE
75 C ***** JJJ IS COUNTER FOR Y010 SUB- ITERATION *****
    JJJ=0
    50 CONTINUE
    DO 5 I=1,900
80 Y010(I)=0.
    5 CONTINUE
    NN=8
C ***** CALCULATES (010) STATE SPECTRUM *****
C ***** FOR FIRST-ORDER CALCULATION (020) IS SET TO 0 *****
85 DO 20 I = 1,900
    Y010(I)=(Y(NN,I)-Y000(I)*QTEMP(NN)-Y020(I)*POPB(NN))/(POPB(NN))
    20 CONTINUE
    DO 23 NN = 1,11
90 DO 21 I = 1,900
    SPECT(I)=Y000(I)*QTEMP(NN)+Y010(I)*POPB(NN)+Y020(I)*POPC(NN)
    21 CONTINUE
C ***** CALCULATES CORRELATION COEFFICIENT *****
95 A=0. S C=0. SAA=0. S CC=0. SAC=0.
    R=0.
    DO 30 I=1,900
100 A=A+Y(NN,I)
    AA=AA+Y(NN,I)**2
    CC=CC+SPECT(I)**2
    C=C+SPECT(I)
    AC=AC+Y(NN,I)*SPECT(I)
105 30 CONTINUE
    R=((III*AC)-A*C)/(SQRT(III*AA-A*A)*SQRT(III*CC-C*C))
    WRITE (6,200) JJJ,TEMP(NN),R
200 FORMAT (1X,ITER. NO. *12,* TEMP K *F 6.1* COR. COEFF. *F9.6)
23 CONTINUE
110 C ***** CORRECT 151 K SPECTRA FOR HOT CONTRIBUTION **
    DO 25 I = 1,900
```

```
115      Y000(I)=(V(I,I)-V010(I)*POP(B(I))-Y020(I)*POPC(I))/QTEMP(I)
25      CONTINUE
26      CONTINUE

      JJJ=JJJ+1
120      C      IF (JJJ .LE. 5) GO TO 50
      *** FIRST-ORDER RESULT OBTAINED FROM NJJ=0 ***

      IF (NJJ .EQ. 0) GO TO 14
      NN=11

125      C      **** USE 423 K SPECTRA TO CALCULATE (020) ****
      C      NN = 10 IS THE 423 K DATA

      DO 77 I=1,900
130      Y020(I)=(V(NN,I)-V010(I)*POP(B(NN))-Y000(I)*QTEMP(NN))/(POPC(NN))
      YPOINT=Y020(I)
      IF (YPOINT .LE. 0.) Y020(I)=0.
77      CONTINUE

135      C      NJJ=NJJ+1
      C      ***** CONVERGENCE IS REACHED BY 8 ITERATIONS ***
      IF (NJJ .LE. 8) GO TO 51

140      14 CONTINUE
      NCONT=1
      CALL SUBJEG(Z,52600.,0.,58200.,5.0)
      CALL PIKTUR(0)

145      C      **** DRAW SPECTRA OF (000), (010) AND (020) ****

      CALL LINESG(Z,III,X,Y000)
      CALL LINESG(Z,III,X,Y010)
      CALL LINESG(Z,III,X,Y020)
150      IF (NJJ .EQ. 0) GO TO 8

      CALL LEGNDG(Z,54200.,2.0,0,0,0H(020 * ))
      WRITE (8,100) Y000
155      WRITE (8,105)
      WRITE (8,100) Y010
      WRITE (8,106)
      WRITE (8,100) Y020
      8 CONTINUE

160      IF (NJJ .EQ. 0) WRITE (7,100) Y000
      IF (NJJ .EQ. 0) WRITE (7,105)
      IF (NJJ .EQ. 0) WRITE (7,100) Y010
105      FORMAT ( *THIS IS (010) SPECTRUM* )
165      106      FORMAT ( *THIS IS (020) SPECTRUM* )
      CALL LEGNDG(Z,56200.,4.5,5,5H(010))
      CALL LEGNDG(Z,56200.,1.35,5,5H(000))

170      CALL SUBJEG(Z,52600.,0,58200.,1.3)
      CALL PIKTUR(1)
      CALL LINESG(Z,III,X,Y000)
```

PROGRAM FIND T600-T600 OPT=1 FTN 4.6-452/034 06 FEB 79 22.56.51 BKV PAGE 4

```

CALL POINTG(Z,III,X,YGS)
175      13 CALL SUBJEG(Z,52600.,.8,58200.,1.9)
        CONTINUE
C ***** CALCULATE CONVOLUTED SPECTRUM *****
180      CALL PIKTUR(I)
        DO 55 NN=NCONT,11,2
        DO 60 I=1,900

185      SPECT(I)=Y000(I)*QTEMP(NN)+Y010(I)*POPB(NN)+Y020(I)*POPC(NN)
        GAUSA(I)=Y(NN,I)
        60 CONTINUE
C ***** PLOT CONVOLUTED AND OBSERVED SPECTRA *****
190      CALL LINESG(Z,III,X,SPECT)
        CALL POINTG(Z,III,X,GAUSA)
        55 CONTINUE
195      NCONT=NCONT+1
        NJJ =NJJ +1
        IF (NCONT .EQ. 2) GO TO 13
        IF (NJJ .EQ. 2) GO TO 51
        CALL EXITG(Z)
        END
    
```

SYMBOLIC REFERENCE MAP (R=1)

ENTRY POINTS
5257 FIND

| VARIABLES | SN | TYPE | RELOCATION | | | | | |
|-----------|--------|---------|--------------|-------|-------|---------|-------|------|
| 6262 | A | REAL | | 6264 | AA | REAL | | |
| 6266 | AC | REAL | | 6263 | C | REAL | | |
| 6265 | CC | REAL | | 30470 | GAUSA | REAL | ARRAY | FIT |
| 6252 | I | INTEGER | | 6253 | III | INTEGER | | |
| 6256 | JK | INTEGER | | 6255 | J | INTEGER | | |
| 6261 | JJJ | INTEGER | | 6257 | K | INTEGER | | |
| 6271 | NCONT | INTEGER | | 6260 | NJJ | INTEGER | | |
| 6254 | NN | INTEGER | | 26 | POPB | REAL | ARRAY | RACY |
| 41 | POPC | REAL | ARRAY RACY | 13 | QTEMP | REAL | ARRAY | RACY |
| 6267 | R | REAL | | 0 | SPECT | REAL | ARRAY | NNO |
| 0 | TEMP | REAL | ARRAY RACY | 1604 | X | REAL | ARRAY | NNO |
| 0 | Y | REAL | ARRAY FIT | 26664 | YGS | REAL | ARRAY | FIT |
| 6270 | YPOINT | REAL | | 23254 | Y000 | REAL | ARRAY | FIT |
| 25060 | Y010 | REAL | ARRAY FIT | 6272 | Y020 | REAL | ARRAY | |
| 0 | Z | REAL | ARRAY IGSZZZ | | | | | |

```

PROGRAM FIND      7600-7600 OPT=1          FTN 4.6+452/034    06 FEB 79 22.56.51  BKJ PAGE 5

FILE NAMES      MODE
3143 ASPEC      4204 BSPEC      2102 FILM      0 INPUT      FMT
1041 OUTPUT     1041 TAPE6      FMT        3143 TAPE7      FMT        4204 TAPE8      FMT

EXTERNALS      TYPE  ARGS
BTEMP          1          EXITG          1
FONT2          0          LEGNDG         5
LINESG         4          MODESG         3
OBJCTG         5          PIKTUR         1
POINTG         4          SETSMG         3
SORT           1 LIBRARY  SUBJEG         5
VECIG          3

STATEMENT LABELS
0 5             0 7             5621 8
0 9             0 12            5650 13
5571 14         0 15            0 16
0 20            0 21            0 23
0 25            0 26            INACTIVE      0 30
5404 50         5403 51          0 55
0 60            0 77            6121 100      FMT
6175 105       FMT        6201 106       FMT        6131 200      FMT

LOOPS LABEL     INDEX     FROM-TO     LENGTH     PROPERTIES
5263 12         I         11 14      10B      INSTACK
5323 15         * NN      36 58      46B
5324 16         * J       37 42      23B      EXT REFS NOT INNER
5332           * K       40 40      11B      EXT REFS
5353 9          I         44 47      3B       INSTACK
5376 7          I         64 67      3B       INSTACK
5407 5          I         78 80      2B       INSTACK
5424 20         I         86 88      7B       INSTACK
5435 23         * NN      89 110     66B      EXT REFS NOT INNER
5444 21         I         90 92      7B       INSTACK
5464 30         I         98 104     13B      OPT
5526 25         I         114 116    7B       INSTACK
5554 77         I         129 133    11B      INSTACK
5654 55         * NN      180 192    31B      EXT REFS NOT INNER
5665 60         I         181 186    10B      INSTACK

COMMON BLOCKS  LENGTH
RACY           44
IGSZZZ        200
NNO           1800
FIT           13500

STATISTICS
PROGRAM LENGTH      2645B  1445
BUFFER LENGTH      5245B  2725
SCM LABELED COMMON LENGTH  36270B  15544
    
```


SUBROUTINE PIKTUR 7600-7600 OPT=1

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```

1      SUBROUTINE PIKTUR(W)
      COMMON/ IGSZZZ/ Z (200)
      INTEGER W
      CALL PAGEG(Z,0,1,1)
5      CALL GRID G (Z,0,0,0,0)
      FMT = 6.0
      CALL LABEL G (Z,0,1000.,0,FMT)
      CALL SETSMG(Z,102,-1.0)
10     CALL LABELG(Z,0,100.,1,1H )
      CALL SETSMG(Z,102,-3.0)
      FMT = 4.2
      IF (W .EQ. 1) GO TO 50
      CALL LABELG(Z,1,1.,0,FMT)
      CALL SETSMG(Z,178,1.)
15     CALL LABELG(Z,1,0.5,1,1H )
      CALL SETSMG(Z,178,0.)
      GO TO 70
50    CONTINUE
      CALL LABELG(Z,1,2.0,FMT)
      CALL SETSMG(Z,178,1.)
      CALL LABELG(Z,1,1,1,1H )
      CALL SETSMG(Z,178,0.)
20     CALL SETSMG(Z,103,-1.0)
70    CONTINUE
      CALL TITLE G (Z,10,10HWAVENUMBER,3,3HCSN,3,3HN20)
      RETURN
      END

```

SYMBOLIC REFERENCE MAP (R=1)

ENTRY POINTS
3 PIKTUR

| VARIABLES | SN | TYPE | RELOCATION | O | W | INTEGER | F.P. |
|-----------|----|------|--------------|---|---|---------|------|
| 210 FMT | | REAL | | | | | |
| 0 Z | | REAL | ARRAY IGSZZZ | | | | |

| EXTERNALS | TYPE | ARGS | | | |
|-----------|------|------|--|--------|---|
| GRIDG | | 5 | | LABELG | 5 |
| PAGEG | | 4 | | SETSMG | 3 |
| TITLEG | | 7 | | | |

STATEMENT LABELS
36 50 50 70

COMMON BLOCKS LENGTH
IGSZZZ 200

| STATISTICS | | | |
|---------------------------|------|-----|--|
| PROGRAM LENGTH | 225B | 149 | |
| SCM LABELED COMMON LENGTH | 310B | 200 | |

SUBROUTINE BTEMP 7600-7600 OPT=1

FTN 4.6-452/034

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1

```

1      SUBROUTINE BTEMP(NN)
      COMMON/RACY/TEMP(11),QTEMP(11),POPB(11),POPC(11)
      BB=(1-EXP(-589./(TEMP(NN)*.6952)))**2
5      BC=(1-EXP(-1284./(TEMP(NN)*.6952)))
      BD=(1-EXP(-2223./(TEMP(NN)*.6952)))
      QTEMP(NN)=BB*BC*BD
      POPB(NN)=2*(EXP(-589./(TEMP(NN)*.6952))*QTEMP(NN)
10     POPC(NN)=3*(EXP(-2.*585./(TEMP(NN)*.6952))*QTEMP(NN)
      A = 4.*(EXP(-3.*582./(TEMP(NN)*.6952))*QTEMP(NN)
      RETURN
      END

```

SYMBOLIC REFERENCE MAP (R=1)

ENTRY POINTS
3 BTEMP

| VARIABLES | SN | TYPE | RELOCATION | 71 | BC | REAL | F.P. |
|-----------|-------|------|------------|----|------|---------|------------|
| 70 | BB | REAL | | 0 | NN | INTEGER | |
| 72 | BD | REAL | | 41 | POPC | REAL | RACY |
| 26 | POPB | REAL | ARRAY RACY | 0 | TEMP | REAL | ARRAY RACY |
| 13 | QTEMP | REAL | ARRAY RACY | | | | |

EXTERNALS
EXP REAL ARGS
1 LIBRARY

COMMON BLOCKS
RACY LENGTH
44

STATISTICS

| | | |
|---------------------------|-----|----|
| PROGRAM LENGTH | 738 | 59 |
| SCM LABELED COMMON LENGTH | 548 | 44 |

2. Computation of Difference Spectra and Energy Levels in the Upper Electronic State

```

1
C ***** MAIN PROGRAM INSIGHT *****
5 PROGRAM INSIGHT(INPUT,OUTPUT,FILM,TAPE6=OUTPUT)
  COMMON/RACY/TEMP(11)/I65ZZZ/Z(200)
  COMMON/PICKER/PEAK(200)/EASY/ISUBRT(20)
  COMMON/GRAPH/A(11,150)
10 DIMENSION X(900),Y(900),GAUST(900),DIF(900)
  INTEGER M
  EXTERNAL FONTZ

C **** TEMPERATURES OF SPECTRA IN DEGREES K ****
15 DATA (TEMP(I) I=1,11)/151.,182.,196.,223.,243.,260.,301.,
  * 333.,372.,423.,483./

C **** INITIALIZE ARRAY ****

20 DO 7 A=1,11
  DO 0 J=1,150
  M(A,J)=0.
  0 CONTINUE
  7 CONTINUE

C **** CONVERT X-AXIS IN WAVELENGTH SCALE TO WAVENUMBER SCALE ****
25 DO 12 I=1,900
  X(I)=1/((1.00035*(190.02-1/50.))*1E-7)
  12 CONTINUE
  III=900

C ***** GRAPHICS PARAMETERS *****
30 CALL MODESG(Z,6,9MTEST)
  CALL OBJECTG(Z,15.,22.,99.,95.)
  CALL VECIG(Z,FONTZ,0)
  CALL SETSG(Z,51,1.)
35 CALL SETSG(Z,45,2.0)
  CALL SETSG(Z,102,-2.5)
  CALL SUBJEG(Z,52600.,0.,50200.,.3)
  CALL SETSG(Z,93,000)
  CALL SETSG(Z,103,9.)
40 DO 03 MM=1,11
  CALL GRIDG(Z,0,0,0,0)
  FMT=6.0
  CALL LABELG(Z,0,1000.,0,FMT)
  FMT=4.2
45 CALL LABELG(Z,1,0.05,0,FMT)
  CALL SETSG(Z,102,-1.)
  CALL SETSG(Z,170,1.)
  CALL LABELG(Z,0,100.,1,IN)
  CALL SETSG(Z,103,2.)
50 CALL LABELG(Z,1,0.025,1,IN)
  CALL TITLEG(Z,10,10*WAVENUMBER,10,10*DIFFERENCE,3,3MMZ0)

C **** BTEMP CALCULATES STATISTICAL POP. ****
55 CALL BTEMP(MM,BTEMP,POPB)
  CALL SETSG(Z,102,-2.5)
  CALL SETSG(Z,170,0.)

```

```

C ***READ RAW DATA***
60      READ 100,Y
      100 FORMAT(10F7.4)
C ***** FORM COMPOSITE GAUSSIAN CURVE FOR 000 AND 010 STATES *****
65      DO 67 I=1,900
      B=1.21
      D=4.2E-8
      XC=55140.
      GAUSA =X(I)*(B/90140.)*(EXP(-D*(X(I)-XC)*(X(I)-XC))) *GTEMP
70      B=4.1
      D=2.3E-8
      XC=53100.
      GAUSB =X(I)*(B/90140.)*(EXP(-D*(X(I)-XC)*(X(I)-XC))) *POPB
      GAUST(I)=GAUSA+GAUSB
75      C ***** FORM DIFFERENCE SPECTRUM *****
      DIF(I)=Y(I)-GAUST(I)
80      67 CONTINUE
      PRINT 121,TEMP(MN),GTEMP,POPB
      121 FORMAT(1H1,10E,TEMP IS *F5.0,* PAR FUNCT IS*F5.4,*010 IS*F5.4)
C ***** PLOT DIFFERENCE SPECTRUM *****
85      CALL LINES6(Z,111,X,DIF)
      FMT=4.0
      CALL NUM66(Z,53500.,.25,FMT,TEMP(MN))
      CALL LEG66(Z,54000.,.25,6,64DEG,K)
90      C ***** IDENTIFY PEAK POSITIONS*****
      CALL CHECK (X,111,DIF,W,PEAK)
95      C ***** PRINTOUT OF PEAK SEPARATION PERMUTATIONS *****
      PRINT 137,W
      137 FORMAT(30X,*TOTAL NUMBER OF PEAKS IS *I4)
      WRITE (6,139)
      139 FORMAT(6X,*ENERGY SPACING BTW PEAKS IN WAVENUMBERS*)
100     CALL PRINTER (W,MN)
C ***** ADVANCE PAGE ***
      CALL PAGE6(Z,0,1,1)
105     83 CONTINUE
C ***** MAKES BAR GRAPH-- HISTOGRAM *****
C ***** NUMBER SEGMENTS NB=NUMBER OF ENERGY BINS ***
110     NS=11 0 NB=150
      CALL OBJCT6(Z,12.,19.,95.,95.)
      CALL SUBJ6(Z,0.,0.,3000.,5.)
      FMT=6.0
      CALL LABEL6(Z,0,500.,0,FMT)

```

115

```
CALL OBJCTG(Z,7,14,100,100.)
CALL SETSMG(Z,117,1,0)
CALL KWKBORG(Z,A,NS,NB,10,10HWAVERNBER,9,9HOCURENCE,1,1H)
CALL EXITG(Z)
END
```

SYMBOLIC REFERENCE MAP (R=1)

ENTRY POINTS
3151 INSIGHT

| VARIABLES | SN | TYPE | RELOCATION | | | | | |
|------------|----|---------|------------|--------|------------|---------|-------|------|
| 0 A | | REAL | ARRAY | GRAPH | 4010 B | REAL | | |
| 4011 D | | REAL | | | 11233 DIF | REAL | ARRAY | |
| 4005 FMT | | REAL | | | 4013 GAUSA | REAL | | |
| 4014 GAUSB | | REAL | | | 7427 GAUST | REAL | ARRAY | |
| 4002 I | | INTEGER | | | 4003 III | INTEGER | | |
| 0 ISUBRT | | INTEGER | ARRAY | EASY | 4001 J | INTEGER | | |
| 4000 M | | INTEGER | | | 4016 NB | INTEGER | | |
| 4004 NN | | INTEGER | | | 4015 NS | INTEGER | | |
| 0 PEAK | | REAL | ARRAY | PICKER | 4007 POPB | REAL | | |
| 4006 BTEMP | | REAL | | | 0 TEMP | REAL | ARRAY | RACY |
| 3777 W | | INTEGER | | | 4017 X | REAL | ARRAY | |
| 4012 XC | | REAL | | | 5623 Y | REAL | ARRAY | |
| 0 Z | | REAL | ARRAY | 16SZZZ | | | | |

| FILE NAMES | MODE | 0 | INPUT | FMT | 1041 | OUTPUT | FMT | 1041 | TAPE6 | FMT |
|------------|------|---|-------|-----|------|--------|-----|------|-------|-----|
| 2102 FILM | | | | | | | | | | |

| EXTERNALS | TYPE | ARGS | | | | |
|-----------|------|------|--|--------|------|-----------|
| BTEMP | | 3 | | CHECK | | 5 |
| EXITG | | 1 | | EXP | REAL | 1 LIBRARY |
| FONT2 | | 0 | | GRIDG | | 5 |
| KWKBORG | | 10 | | LABELG | | 5 |
| LEGMDG | | 5 | | LINESG | | 4 |
| MODESG | | 3 | | NUMBRG | | 5 |
| OBJCTG | | 5 | | PAGEG | | 4 |
| PRINTER | | 2 | | SETSMG | | 3 |
| SUBJEG | | 5 | | TITLEG | | 7 |
| VECTG | | 3 | | | | |

STATEMENT LABELS

| | | | | | | |
|----------|-----|--|----------|-----|--|----------|
| 0 7 | | | 0 8 | | | 0 12 |
| 0 67 | | | 0 83 | | | 3646 100 |
| 3656 121 | FMT | | 3672 137 | FMT | | 3702 139 |

PROGRAM INSIGHT 7600-7600 OPT=1

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4

| LOOPS | LABEL | INDEX | FROM-TO | LENGTH | PROPERTIES |
|-------|-------|-------|---------|--------|--------------------|
| 3153 | 7 | * M | 18 22 | 13B | NOT INNER |
| 3160 | 8 | J | 19 21 | 2B | INSTACK |
| 3170 | 12 | I | 24 26 | 7B | INSTACK |
| 3224 | 83 | * NN | 40 105 | 122B | EXT REFS NOT INNER |
| 3261 | 67 | * I | 65 79 | 32B | EXT REFS |

| COMMON BLOCKS | LENGTH |
|---------------|--------|
| RACY | 11 |
| IGSZZZ | 200 |
| PICKER | 200 |
| EASY | 20 |
| GRAPH | 1650 |

| STATISTICS | | |
|---------------------------|-------|------|
| PROGRAM LENGTH | 7720B | 4048 |
| BUFFER LENGTH | 3143B | 1635 |
| SCM LABELED COMMON LENGTH | 4041B | 2081 |

```

1
      SUBROUTINE BTEMP (NN,QTEMP,POPB)
5      C **** CALCULATES VIBRATIONAL POPULATIONS ****
      COMMON/RACY/TEMP(11)
      T=TEMP(NN)
      BB=(1-EXP(-589./(T*.6952)))
10     QTEMP=BB*BB
      C ***** QTEMP IS (000)POPULATION *****
      C ***** POPB IS (010) POPULATION *****
15     POPB=2*(EXP(-589./(T*.6952)))*QTEMP
      RETURN
      END
    
```

SYMBOLIC REFERENCE MAP (R=1)

ENTRY POINTS
3 BTEMP

| VARIABLES | SN | TYPE | RELOCATION | | | | |
|-----------|----|------|------------|---|-------|---------|------------|
| 27 BB | | REAL | | 0 | NN | INTEGER | F.P. |
| 0 POPB | | REAL | F.P. | 0 | QTEMP | REAL | F.P. |
| 26 T | | REAL | | 0 | TEMP | REAL | ARRAY RACY |

EXTERNALS
EXP REAL 1 LIBRARY

COMMON BLOCKS
RACY 11

STATISTICS
PROGRAM LENGTH 308 24
SCA LABELED COMMON LENGTH 138 11

SUBROUTINE BAR 7600-7600 OPT=1

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```
1
SUBROUTINE BAR(NN,JSUBRT)
5 C **** GROUPS ENERGY SEPARATIONS INTO BINS OF 20 CM-1 ****
COMMON/GRAPH/A(11,150)
KSUBRT=JSUBRT/20
10 C ***** FORMS BAR GRAPH ARRAYS *****
A(NN,KSUBRT)=A(NN,KSUBRT)+1.
RETURN SEND
```

SYMBOLIC REFERENCE MAP (R=1)

ENTRY POINTS
3 BAR

| VARIABLES | SN | TYPE | RELOCATION | | | | |
|-----------|----|---------|------------|-------|----------|---------|------|
| 0 A | | REAL | ARRAY | GRAPH | 0 JSUBRT | INTEGER | F.P. |
| 15 KSUBRT | | INTEGER | | | 0 NN | INTEGER | F.P. |

| COMMON BLOCKS | LENGTH |
|---------------|--------|
| GRAPH | 1650 |

| STATISTICS | | | |
|---------------------------|-------|------|--|
| PROGRAM LENGTH | 168 | 14 | |
| SCM LABELED COMMON LENGTH | 31628 | 1650 | |

```

1
      SUBROUTINE CHECK(X,III, TOP,D,PEAK)
5      C ***** SELECTS PEAKS *****
      COMMON/IGSZZZ/Z(200)
      DIMENSION TOP(III),X(900) PEAK(200)
10     LOGICAL POINT, CHECKA, CHECKB, CHECKC, CHECKD, POP
      INTEGER D
      POP=.TRUE.
      I=5 & D=0
      C *** SLOPE CRITERIA ***
15     10 POINT=((TOP(I) .GT. TOP (I-1)) .AND. (TOP(I) .GE. TOP(I+1)))
      CHECKB=(TOP(I+1) .GE. TOP(I+2))
      CHECKC=((TOP(I) .GT. TOP(I-4)) .AND. (TOP(I) .GT. TOP(I+4)))
      CHECKA=((POINT .AND. CHECKB) .AND. CHECKC)
20     CHECKD=((TOP(I) .GT. TOP(I-10)) .OR. ((TOP(I) .GT. TOP(I+10))))
      POINT=((CHECKD .AND. CHECKA) .AND. POP)
      C *** WIDTH CRITERIA ***
25     WM=TOP(I-25) & WP=TOP(I+25)
      CHECKA=((TOP(I)-WM .GE. 0.008) .AND. ((TOP(I)-WP) .GE. 0.008))
      C ***** APPLICABLE TO FIRST OR LAST 25 DATA POINTS ONLY *****
      IF (I .LE. 25) CHECKA=((TOP(I)-WM) .GT. 0.015) .OR.
      * ((TOP(I)-WP) .GT. 0.015)
30     IF (I .GE. (III-25)) CHECKA=((TOP(I)-WM) .GT. 0.024) .OR.
      * ((TOP(I)-WP) .GT. 0.024)
      IF (POINT .AND. CHECKA) GO TO 50
      WM=TOP(I-10) & WP=TOP(I+10)
      CHECKA=((TOP(I)-WM .GE. 0.012) .AND.
35     @ (TOP(I)-WP .GE. 0.012))
      IF (POINT .AND. CHECKA) GO TO 50
      I=I+1
      IF (I .LE. III-4) GO TO 10
      RETURN
40     50 CONTINUE
      XI=X(I)
      YI=0. & Y2=TOP(I)
45     C ***** DRAWS VERTICAL LINES FOR PEAKS POSITION *****
      CALL SEGMT6(Z,I,XI,YI,XI,Y2)
      IFMT=1
      D=D+1
50     PEAK(D)=X(I)
      I=I+2
      IF (I .LE. III-4) GO TO 10
      RETURN & END

```

SUBROUTINE CHECK 7600-7600 OPT=1

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SYMBOLIC REFERENCE MAP (R=1)

ENTRY POINTS
3 CHECK

| VARIABLES | SN | TYPE | RELOCATION | | | | |
|-----------|--------|---------|--------------|-----|--------|---------|------------|
| 134 | CHECKA | LOGICAL | | 135 | CHECKB | LOGICAL | |
| 136 | CHECKC | LOGICAL | | 137 | CHECKD | LOGICAL | |
| 0 | 0 | INTEGER | F.P. | 141 | I | INTEGER | |
| 147 | IFMT | INTEGER | | 0 | III | INTEGER | F.P. |
| 0 | PEAK | REAL | ARRAY F.P. | 133 | POINT | LOGICAL | |
| 140 | POP | LOGICAL | | 0 | TOP | REAL | ARRAY F.P. |
| 142 | WP | REAL | | 143 | WP | REAL | |
| 0 | X | REAL | ARRAY F.P. | 144 | X1 | REAL | |
| 145 | Y1 | REAL | | 146 | Y2 | REAL | |
| 0 | Z | REAL | ARRAY 16SZZZ | | | | |

EXTERNALS
SEGMT6 TYPE ARGS
6

STATEMENT LABELS
10 10 76 50

COMMON BLOCKS LENGTH
16SZZZ 200

STATISTICS
PROGRAM LENGTH 1508 104
SCM LABELED COMMON LENGTH 3108 200

```

1
SUBROUTINE PRINTER (M,NN)
C ***** PRINTOUT PROGRAM *****
5 COMMON/GRAPH/A(1) 150)
COMMON/PICKER/PEAK(200)
COMMON/EASY/ISUBRT(20)
INTEGER W
INTEGER R
10 DO 39 I=1,W

C ***** MAKES AND LABELS COLUMNS FROM START TO START+ 20 *****

15 J=I+19
N=0
DO 29 K=I,J
N=N+1
ISUBRT(N)=K
29 CONTINUE
PRINT 119, ISUBRT
20 119 FORMAT(10X,2016)
DO 40 K=I,W,20
KK=K+19
IF (KK .GT. W) KK=W
25 N=0
DO 45 JK =1,20
ISUBRT(JK)=0
45 CONTINUE
DO 41 J=K,KK
N=N+1
30 C *** TRUNCATES REMAINDER ***
ISUBRT(N)=INT(ABS(PEAK(I)-PEAK(J) *.0000001))
JSUBRT=ISUBRT(N)
IF ((JSUBRT.GE.20).AND.(JSUBRT.LE.3019)) CALL BAR(NN,JSUBRT)
35 41 CONTINUE
PRINT 142 (ISUBRT(IN),IN=1,20)
142 FORMAT(10X,2016)
40 CONTINUE
PRINT 143
40 143 FORMAT(1X,/)
39 CONTINUE
RETURN SEND

```

SYMBOLIC REFERENCE MAP (R=1)

ENTRY POINTS
3 PRINTER

| VARIABLES | SM | TYPE | RELOCATION | | | | | |
|-----------|--------|---------|------------|-------|-----|--------|---------|------------|
| 0 | A | REAL | ARRAY | GRAPH | 130 | I | INTEGER | |
| 137 | IN | INTEGER | | | 0 | ISUBRT | INTEGER | ARRAY EASY |
| 131 | J | INTEGER | | | 135 | JK | INTEGER | |
| 136 | JSUBRT | INTEGER | | | 133 | K | INTEGER | |

SUBROUTINE PRINTER 7600-7600 OPT=1

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| VARIABLES | SN | TYPE | RELOCATION | | | | |
|-----------|----|---------|------------|-----|------|---------|--------------|
| 134 | KK | INTEGER | | 132 | N | INTEGER | |
| 0 | NN | INTEGER | F.P. | 0 | PEAK | REAL | ARRAY PICKER |
| 127 | R | INTEGER | *UNDEF | 0 | W | INTEGER | F.P. |

| FILE NAMES | MODE |
|------------|------|
| OUTPUT | FMT |

| EXTERNALS | TYPE | ARGS |
|-----------|------|------|
| BAR | | 2 |

| INLINE FUNCTIONS | TYPE | ARGS | | | | |
|------------------|------|------|--------|-----|---------|----------|
| ABS | REAL | 1 | INTRIN | INT | INTEGER | 1 INTRIN |

| STATEMENT LABELS | | | | | |
|------------------|-----|-----|-----|-----|-------------|
| 0 | 29 | | 0 | 39 | |
| 0 | 41 | | 0 | 45 | 0 40 |
| 117 | 142 | FMT | 124 | 143 | 111 119 FMT |

| LOOPS | LABEL | INDEX | FROM-TO | LENGTH | PROPERTIES | | |
|-------|-------|-------|---------|--------|------------|----------|-----------|
| 17 | 39 | * I | 10 41 | 63B | INSTACK | EXT REFS | NOT INNER |
| 26 | 29 | * K | 16 19 | 2B | INSTACK | EXT REFS | NOT INNER |
| 35 | 40 | * K | 22 36 | 41B | INSTACK | EXT REFS | NOT INNER |
| 45 | 45 | * JK | 26 28 | 2B | INSTACK | EXT REFS | |
| 52 | 41 | * J | 29 35 | 20B | INSTACK | EXT REFS | |

| COMMON BLOCKS | LENGTH |
|---------------|--------|
| GRAPH | 1650 |
| PICKER | 200 |
| EASY | 20 |

| STATISTICS | | |
|---------------------------|-------|------|
| PROGRAM LENGTH | 146B | 102 |
| SCM LABELED COMMON LENGTH | 3516B | 1670 |

D. Listing of Data

1. Cross Sections from 190-172 nm for Eleven Temperatures

| WAVENUMBER CM-1 | WAVELENGTH NM | CROSS SECTION X E19 CM-2, TEMPERATURE DEG. K | | | | | | | | | | |
|--------------------|------------------|--|-------|-------|--------|--------|--------|--------|--------|--------|--------|--------|
| | | 151. | 182. | 196. | 223. | 247. | 268. | 301. | 333. | 372. | 423. | 485. |
| 52613. | 190.00 | .8640 | .9010 | .9101 | .9540 | 1.0500 | 1.0925 | 1.1700 | 1.2475 | 1.3500 | 1.5253 | 1.6200 |
| 52619. | 189.98 | .8657 | .9028 | .9108 | .9543 | 1.0511 | 1.0950 | 1.1750 | 1.2500 | 1.3550 | 1.5280 | 1.6263 |
| 52624. | 189.96 | .8634 | .9047 | .9112 | .9545 | 1.0531 | 1.1039 | 1.1835 | 1.2561 | 1.3789 | 1.5308 | 1.6318 |
| 52630. | 189.94 | .8648 | .9065 | .9130 | .9565 | 1.0546 | 1.1062 | 1.1859 | 1.2598 | 1.3829 | 1.5348 | 1.6373 |
| 52635. | 189.92 | .8659 | .9082 | .9144 | .9585 | 1.0561 | 1.1090 | 1.1889 | 1.2641 | 1.3861 | 1.5382 | 1.6425 |
| 52641. | 189.90 | .8673 | .9095 | .9157 | .9600 | 1.0592 | 1.1118 | 1.1918 | 1.2682 | 1.3896 | 1.5419 | 1.6472 |
| 52646. | 189.88 | .8677 | .9109 | .9169 | .9620 | 1.0612 | 1.1138 | 1.1942 | 1.2718 | 1.3926 | 1.5455 | 1.6510 |
| 52652. | 189.86 | .8679 | .9121 | .9182 | .9643 | 1.0632 | 1.1153 | 1.1956 | 1.2750 | 1.3950 | 1.5487 | 1.6540 |
| 52658. | 189.84 | .8691 | .9135 | .9191 | .9663 | 1.0652 | 1.1168 | 1.1975 | 1.2769 | 1.3974 | 1.5513 | 1.6567 |
| 52663. | 189.82 | .8707 | .9149 | .9198 | .9682 | 1.0663 | 1.1191 | 1.1994 | 1.2786 | 1.3987 | 1.5534 | 1.6587 |
| 52669. | 189.80 | .8716 | .9158 | .9209 | .9700 | 1.0693 | 1.1209 | 1.1999 | 1.2798 | 1.4001 | 1.5542 | 1.6589 |
| 52674. | 189.78 | .8727 | .9165 | .9223 | .9712 | 1.0688 | 1.1214 | 1.2004 | 1.2803 | 1.4009 | 1.5532 | 1.6584 |
| 52680. | 189.76 | .8738 | .9171 | .9232 | .9717 | 1.0688 | 1.1219 | 1.2012 | 1.2805 | 1.4009 | 1.5508 | 1.6567 |
| 52685. | 189.74 | .8748 | .9184 | .9238 | .9721 | 1.0688 | 1.1226 | 1.2018 | 1.2805 | 1.4001 | 1.5487 | 1.6543 |
| 52691. | 189.72 | .8759 | .9191 | .9245 | .9721 | 1.0688 | 1.1232 | 1.2015 | 1.2803 | 1.3993 | 1.5469 | 1.6521 |
| 52696. | 189.70 | .8768 | .9197 | .9261 | .9731 | 1.0718 | 1.1229 | 1.2010 | 1.2800 | 1.3979 | 1.5461 | 1.6496 |
| 52702. | 189.68 | .8775 | .9207 | .9277 | .9753 | 1.0728 | 1.1226 | 1.2010 | 1.2808 | 1.3966 | 1.5448 | 1.6472 |
| 52707. | 189.66 | .8786 | .9211 | .9281 | .9769 | 1.0749 | 1.1237 | 1.2015 | 1.2812 | 1.3958 | 1.5434 | 1.6455 |
| 52713. | 189.64 | .8800 | .9223 | .9295 | .9785 | 1.0738 | 1.1247 | 1.2021 | 1.2803 | 1.3961 | 1.5424 | 1.6450 |
| 52719. | 189.62 | .8802 | .9235 | .9304 | .9790 | 1.0743 | 1.1247 | 1.2021 | 1.2795 | 1.3966 | 1.5419 | 1.6444 |
| 52724. | 189.60 | .8800 | .9244 | .9308 | .9793 | 1.0738 | 1.1242 | 1.2018 | 1.2793 | 1.3966 | 1.5416 | 1.6444 |
| 52730. | 189.58 | .8802 | .9246 | .9315 | .9807 | 1.0743 | 1.1239 | 1.2021 | 1.2795 | 1.3966 | 1.5416 | 1.6441 |
| 52735. | 189.56 | .8804 | .9248 | .9320 | .9815 | 1.0749 | 1.1242 | 1.2026 | 1.2803 | 1.3966 | 1.5406 | 1.6428 |
| 52741. | 189.54 | .8804 | .9253 | .9322 | .9815 | 1.0754 | 1.1249 | 1.2026 | 1.2812 | 1.3966 | 1.5395 | 1.6417 |
| 52746. | 189.52 | .8816 | .9260 | .9331 | .9815 | 1.0754 | 1.1262 | 1.2029 | 1.2815 | 1.3963 | 1.5392 | 1.6411 |
| 52752. | 189.50 | .8834 | .9267 | .9338 | .9814 | 1.0779 | 1.1270 | 1.2031 | 1.2817 | 1.3966 | 1.5398 | 1.6417 |
| 52758. | 189.48 | .8852 | .9281 | .9342 | .9813 | 1.0789 | 1.1282 | 1.2042 | 1.2824 | 1.3977 | 1.5400 | 1.6420 |
| 52763. | 189.46 | .8873 | .9304 | .9356 | .9815 | 1.0794 | 1.1297 | 1.2058 | 1.2844 | 1.3977 | 1.5408 | 1.6425 |
| 52769. | 189.44 | .8888 | .9327 | .9374 | .9826 | 1.0814 | 1.1318 | 1.2080 | 1.2849 | 1.3985 | 1.5419 | 1.6430 |
| 52774. | 189.42 | .8911 | .9348 | .9389 | .9841 | 1.0835 | 1.1335 | 1.2096 | 1.2853 | 1.3998 | 1.5432 | 1.6436 |
| 52780. | 189.40 | .8932 | .9364 | .9407 | .9858 | 1.0855 | 1.1348 | 1.2109 | 1.2870 | 1.4014 | 1.5432 | 1.6436 |
| 52785. | 189.38 | .8950 | .9383 | .9430 | .9862 | 1.0870 | 1.1363 | 1.2126 | 1.2887 | 1.4022 | 1.5429 | 1.6433 |
| 52791. | 189.36 | .8968 | .9394 | .9453 | .9905 | 1.0880 | 1.1376 | 1.2142 | 1.2894 | 1.4020 | 1.5424 | 1.6430 |
| 52797. | 189.34 | .8979 | .9404 | .9464 | .9922 | 1.0895 | 1.1386 | 1.2152 | 1.2902 | 1.4014 | 1.5421 | 1.6417 |
| 52802. | 189.32 | .8991 | .9411 | .9473 | .9937 | 1.0905 | 1.1391 | 1.2158 | 1.2911 | 1.4014 | 1.5421 | 1.6403 |
| 52808. | 189.30 | .9000 | .9425 | .9482 | .9949 | 1.0911 | 1.1396 | 1.2163 | 1.2916 | 1.4022 | 1.5411 | 1.6392 |
| 52813. | 189.28 | .9002 | .9434 | .9493 | .9960 | 1.0911 | 1.1401 | 1.2163 | 1.2911 | 1.4020 | 1.5400 | 1.6381 |
| 52819. | 189.26 | .8997 | .9436 | .9502 | .9967 | 1.0900 | 1.1396 | 1.2161 | 1.2899 | 1.4009 | 1.5392 | 1.6359 |
| 52824. | 189.24 | .9000 | .9441 | .9504 | .9970 | 1.0900 | 1.1389 | 1.2155 | 1.2894 | 1.4009 | 1.5387 | 1.6346 |
| 52830. | 189.22 | .9013 | .9448 | .9511 | .9976 | 1.0911 | 1.1389 | 1.2152 | 1.2892 | 1.4006 | 1.5382 | 1.6332 |
| 52836. | 189.20 | .9022 | .9452 | .9518 | .9977 | 1.0916 | 1.1394 | 1.2155 | 1.2885 | 1.3998 | 1.5366 | 1.6313 |
| 52841. | 189.18 | .9022 | .9462 | .9525 | .9971 | 1.0911 | 1.1401 | 1.2150 | 1.2877 | 1.3985 | 1.5350 | 1.6299 |
| 52847. | 189.16 | .9034 | .9464 | .9527 | .9973 | 1.0931 | 1.1417 | 1.2142 | 1.2877 | 1.3985 | 1.5340 | 1.6294 |
| 52852. | 189.14 | .9050 | .9471 | .9534 | .9977 | 1.0936 | 1.1432 | 1.2147 | 1.2887 | 1.3987 | 1.5340 | 1.6291 |
| 52858. | 189.12 | .9068 | .9487 | .9540 | .9987 | 1.0946 | 1.1439 | 1.2155 | 1.2892 | 1.3990 | 1.5345 | 1.6288 |
| 52864. | 189.10 | .9082 | .9506 | .9540 | 1.0007 | 1.0971 | 1.1442 | 1.2169 | 1.2899 | 1.4006 | 1.5356 | 1.6285 |
| 52869. | 189.08 | .9097 | .9524 | .9549 | 1.0017 | 1.0991 | 1.1450 | 1.2193 | 1.2911 | 1.4022 | 1.5371 | 1.6299 |
| 52875. | 189.06 | .9111 | .9545 | .9570 | 1.0030 | 1.1012 | 1.1467 | 1.2214 | 1.2933 | 1.4036 | 1.5377 | 1.6318 |
| 52880. | 189.04 | .9131 | .9566 | .9592 | 1.0050 | 1.1012 | 1.1485 | 1.2228 | 1.2957 | 1.4049 | 1.5377 | 1.6335 |
| 52886. | 189.02 | .9143 | .9575 | .9608 | 1.0063 | 1.1022 | 1.1505 | 1.2241 | 1.2972 | 1.4063 | 1.5390 | 1.6343 |
| 52892. | 189.00 | .9156 | .9587 | .9622 | 1.0068 | 1.1062 | 1.1526 | 1.2260 | 1.2981 | 1.4065 | 1.5406 | 1.6346 |

| WAVENUMBER (CM-1) | WAVELENGTH NM | CROSS SECTION X E19 | | | CM-2 223. | TEMPERATURE DEG. K | | | 301. | 333. | 372. | 423. | 485. |
|----------------------|------------------|---------------------|--------|--------|--------------|--------------------|--------|--------|--------|--------|--------|--------|------|
| | | 151. | 182. | 196. | | 247. | 268. | | | | | | |
| 52892. | 189.00 | .9156 | .9587 | .9622 | 1.0068 | 1.1062 | 1.1526 | 1.2260 | 1.2981 | 1.4065 | 1.5406 | 1.6346 | |
| 52897. | 188.98 | .9177 | .9605 | .9635 | 1.0076 | 1.1062 | 1.1538 | 1.2290 | 1.2991 | 1.4073 | 1.5413 | 1.6354 | |
| 52903. | 188.96 | .9200 | .9624 | .9649 | 1.0091 | 1.1078 | 1.1548 | 1.2306 | 1.3003 | 1.4092 | 1.5416 | 1.6367 | |
| 52908. | 188.94 | .9213 | .9638 | .9658 | 1.0119 | 1.1083 | 1.1561 | 1.2311 | 1.3017 | 1.4114 | 1.5429 | 1.6376 | |
| 52914. | 188.92 | .9225 | .9649 | .9682 | 1.0152 | 1.1093 | 1.1574 | 1.2317 | 1.3029 | 1.4119 | 1.5442 | 1.6381 | |
| 52920. | 188.90 | .9236 | .9668 | .9707 | 1.0170 | 1.1123 | 1.1591 | 1.2325 | 1.3039 | 1.4122 | 1.5455 | 1.6392 | |
| 52925. | 188.88 | .9252 | .9684 | .9721 | 1.0176 | 1.1128 | 1.1607 | 1.2338 | 1.3056 | 1.4138 | 1.5471 | 1.6403 | |
| 52931. | 188.86 | .9266 | .9693 | .9732 | 1.0187 | 1.1138 | 1.1614 | 1.2354 | 1.3073 | 1.4154 | 1.5482 | 1.6414 | |
| 52936. | 188.84 | .9284 | .9696 | .9741 | 1.0203 | 1.1143 | 1.1619 | 1.2373 | 1.3087 | 1.4165 | 1.5492 | 1.6420 | |
| 52942. | 188.82 | .9293 | .9707 | .9757 | 1.0214 | 1.1179 | 1.1640 | 1.2389 | 1.3099 | 1.4181 | 1.5519 | 1.6430 | |
| 52948. | 188.80 | .9302 | .9719 | .9770 | 1.0225 | 1.1184 | 1.1662 | 1.2406 | 1.3114 | 1.4202 | 1.5540 | 1.6452 | |
| 52953. | 188.78 | .9302 | .9733 | .9786 | 1.0237 | 1.1209 | 1.1678 | 1.2422 | 1.3136 | 1.4224 | 1.5555 | 1.6488 | |
| 52959. | 188.76 | .9311 | .9744 | .9797 | 1.0251 | 1.1214 | 1.1688 | 1.2430 | 1.3157 | 1.4237 | 1.5574 | 1.6515 | |
| 52964. | 188.74 | .9331 | .9761 | .9813 | 1.0263 | 1.1229 | 1.1700 | 1.2449 | 1.3177 | 1.4256 | 1.5595 | 1.6532 | |
| 52970. | 188.72 | .9350 | .9781 | .9827 | 1.0273 | 1.1245 | 1.1718 | 1.2467 | 1.3198 | 1.4288 | 1.5613 | 1.6545 | |
| 52976. | 188.70 | .9363 | .9800 | .9836 | 1.0285 | 1.1270 | 1.1741 | 1.2486 | 1.3220 | 1.4310 | 1.5631 | 1.6565 | |
| 52981. | 188.68 | .9372 | .9812 | .9838 | 1.0299 | 1.1280 | 1.1771 | 1.2500 | 1.3244 | 1.4339 | 1.5647 | 1.6589 | |
| 52987. | 188.66 | .9381 | .9814 | .9843 | 1.0318 | 1.1290 | 1.1794 | 1.2511 | 1.3263 | 1.4366 | 1.5671 | 1.6611 | |
| 52992. | 188.64 | .9390 | .9819 | .9854 | 1.0334 | 1.1315 | 1.1802 | 1.2516 | 1.3273 | 1.4377 | 1.5679 | 1.6633 | |
| 52998. | 188.62 | .9406 | .9826 | .9872 | 1.0347 | 1.1310 | 1.1799 | 1.2519 | 1.3268 | 1.4371 | 1.5673 | 1.6630 | |
| 53004. | 188.60 | .9422 | .9844 | .9885 | 1.0360 | 1.1320 | 1.1797 | 1.2532 | 1.3266 | 1.4371 | 1.5676 | 1.6625 | |
| 53009. | 188.58 | .9431 | .9858 | .9894 | 1.0366 | 1.1331 | 1.1817 | 1.2546 | 1.3278 | 1.4382 | 1.5684 | 1.6628 | |
| 53015. | 188.56 | .9436 | .9870 | .9908 | 1.0370 | 1.1351 | 1.1850 | 1.2564 | 1.3302 | 1.4401 | 1.5705 | 1.6652 | |
| 53021. | 188.54 | .9450 | .9881 | .9926 | 1.0378 | 1.1361 | 1.1870 | 1.2583 | 1.3326 | 1.4433 | 1.5750 | 1.6682 | |
| 53026. | 188.52 | .9463 | .9902 | .9944 | 1.0390 | 1.1396 | 1.1883 | 1.2615 | 1.3358 | 1.4473 | 1.5802 | 1.6726 | |
| 53032. | 188.50 | .9477 | .9921 | .9960 | 1.0408 | 1.1412 | 1.1903 | 1.2648 | 1.3396 | 1.4508 | 1.5841 | 1.6773 | |
| 53037. | 188.48 | .9486 | .9939 | .9971 | 1.0428 | 1.1442 | 1.1934 | 1.2685 | 1.3432 | 1.4546 | 1.5876 | 1.6819 | |
| 53043. | 188.46 | .9495 | .9953 | .9989 | 1.0451 | 1.1452 | 1.1972 | 1.2720 | 1.3466 | 1.4597 | 1.5923 | 1.6866 | |
| 53049. | 188.44 | .9513 | .9972 | 1.0012 | 1.0480 | 1.1477 | 1.2007 | 1.2753 | 1.3507 | 1.4648 | 1.5973 | 1.6926 | |
| 53054. | 188.42 | .9529 | .9983 | 1.0023 | 1.0503 | 1.1513 | 1.2030 | 1.2790 | 1.3551 | 1.4691 | 1.6025 | 1.6978 | |
| 53060. | 188.40 | .9543 | .9997 | 1.0036 | 1.0516 | 1.1533 | 1.2050 | 1.2834 | 1.3592 | 1.4731 | 1.6073 | 1.7025 | |
| 53066. | 188.38 | .9552 | 1.0011 | 1.0057 | 1.0525 | 1.1563 | 1.2083 | 1.2869 | 1.3625 | 1.4763 | 1.6112 | 1.7060 | |
| 53071. | 188.36 | .9561 | 1.0025 | 1.0070 | 1.0540 | 1.1604 | 1.2114 | 1.2909 | 1.3669 | 1.4806 | 1.6159 | 1.7101 | |
| 53077. | 188.34 | .9575 | 1.0041 | 1.0084 | 1.0560 | 1.1624 | 1.2139 | 1.2939 | 1.3710 | 1.4852 | 1.6212 | 1.7148 | |
| 53083. | 188.32 | .9595 | 1.0055 | 1.0104 | 1.0587 | 1.1639 | 1.2159 | 1.2955 | 1.3739 | 1.4881 | 1.6251 | 1.7184 | |
| 53088. | 188.30 | .9606 | 1.0074 | 1.0127 | 1.0617 | 1.1649 | 1.2174 | 1.2963 | 1.3756 | 1.4892 | 1.6275 | 1.7192 | |
| 53094. | 188.28 | .9615 | 1.0092 | 1.0140 | 1.0631 | 1.1670 | 1.2185 | 1.2974 | 1.3763 | 1.4906 | 1.6283 | 1.7194 | |
| 53099. | 188.26 | .9622 | 1.0104 | 1.0138 | 1.0642 | 1.1690 | 1.2202 | 1.2982 | 1.3768 | 1.4914 | 1.6280 | 1.7194 | |
| 53105. | 188.24 | .9643 | 1.0108 | 1.0142 | 1.0666 | 1.1705 | 1.2215 | 1.2990 | 1.3772 | 1.4919 | 1.6272 | 1.7194 | |
| 53111. | 188.22 | .9659 | 1.0115 | 1.0158 | 1.0691 | 1.1695 | 1.2225 | 1.2995 | 1.3777 | 1.4924 | 1.6272 | 1.7194 | |
| 53116. | 188.20 | .9670 | 1.0122 | 1.0181 | 1.0705 | 1.1700 | 1.2228 | 1.2990 | 1.3782 | 1.4932 | 1.6277 | 1.7189 | |
| 53122. | 188.18 | .9679 | 1.0134 | 1.0196 | 1.0712 | 1.1710 | 1.2233 | 1.2990 | 1.3789 | 1.4930 | 1.6280 | 1.7186 | |
| 53128. | 188.16 | .9686 | 1.0145 | 1.0208 | 1.0713 | 1.1720 | 1.2238 | 1.3000 | 1.3797 | 1.4932 | 1.6277 | 1.7197 | |
| 53133. | 188.14 | .9695 | 1.0155 | 1.0226 | 1.0708 | 1.1730 | 1.2251 | 1.3003 | 1.3806 | 1.4935 | 1.6280 | 1.7211 | |
| 53139. | 188.12 | .9709 | 1.0169 | 1.0235 | 1.0718 | 1.1725 | 1.2258 | 1.3014 | 1.3814 | 1.4946 | 1.6290 | 1.7216 | |
| 53145. | 188.10 | .9731 | 1.0185 | 1.0233 | 1.0736 | 1.1751 | 1.2261 | 1.3025 | 1.3826 | 1.4951 | 1.6304 | 1.7216 | |
| 53150. | 188.08 | .9747 | 1.0206 | 1.0239 | 1.0752 | 1.1751 | 1.2268 | 1.3041 | 1.3835 | 1.4949 | 1.6314 | 1.7211 | |
| 53156. | 188.06 | .9756 | 1.0222 | 1.0248 | 1.0769 | 1.1761 | 1.2278 | 1.3060 | 1.3840 | 1.4951 | 1.6319 | 1.7216 | |
| 53162. | 188.04 | .9763 | 1.0231 | 1.0260 | 1.0776 | 1.1776 | 1.2291 | 1.3073 | 1.3850 | 1.4965 | 1.6319 | 1.7216 | |
| 53167. | 188.02 | .9770 | 1.0240 | 1.0271 | 1.0770 | 1.1794 | 1.2299 | 1.3087 | 1.3859 | 1.4983 | 1.6319 | 1.7222 | |
| 53173. | 188.00 | .9781 | 1.0245 | 1.0284 | 1.0764 | 1.1806 | 1.2309 | 1.3095 | 1.3869 | 1.4994 | 1.6322 | 1.7233 | |

| WAVENUMBER CM-1 | WAVELENGTH NM | CROSS SECTION X E19 | | | CM-2 | | TEMPERATURE DEG. K | | | | | |
|--------------------|------------------|---------------------|--------|--------|--------|--------|--------------------|--------|--------|--------|--------|--------|
| | | 151. | 182. | 196. | 223. | 247. | 268. | 301. | 333. | 372. | 423. | 485. |
| 53173. | 188.00 | .9701 | 1.0245 | 1.0284 | 1.0764 | 1.1806 | 1.2309 | 1.3095 | 1.3869 | 1.4994 | 1.6322 | 1.7233 |
| 53179. | 187.98 | .9793 | 1.0252 | 1.0302 | 1.0774 | 1.1827 | 1.2324 | 1.3095 | 1.3876 | 1.5005 | 1.6330 | 1.7244 |
| 53184. | 187.96 | .9806 | 1.0268 | 1.0309 | 1.0789 | 1.1816 | 1.2344 | 1.3103 | 1.3886 | 1.5018 | 1.6340 | 1.7241 |
| 53190. | 187.94 | .9818 | 1.0277 | 1.0311 | 1.0804 | 1.1822 | 1.2357 | 1.3114 | 1.3898 | 1.5021 | 1.6346 | 1.7230 |
| 53196. | 187.92 | .9827 | 1.0284 | 1.0318 | 1.0817 | 1.1837 | 1.2367 | 1.3116 | 1.3908 | 1.5013 | 1.6348 | 1.7227 |
| 53201. | 187.90 | .9833 | 1.0294 | 1.0332 | 1.0828 | 1.1852 | 1.2370 | 1.3122 | 1.3912 | 1.5000 | 1.6346 | 1.7230 |
| 53207. | 187.88 | .9838 | 1.0298 | 1.0343 | 1.0841 | 1.1867 | 1.2375 | 1.3124 | 1.3915 | 1.4997 | 1.6343 | 1.7233 |
| 53213. | 187.86 | .9854 | 1.0301 | 1.0357 | 1.0850 | 1.1882 | 1.2377 | 1.3127 | 1.3915 | 1.5002 | 1.6335 | 1.7222 |
| 53218. | 187.84 | .9865 | 1.0315 | 1.0368 | 1.0862 | 1.1877 | 1.2375 | 1.3124 | 1.3903 | 1.5008 | 1.6325 | 1.7200 |
| 53224. | 187.82 | .9872 | 1.0331 | 1.0377 | 1.0875 | 1.1877 | 1.2367 | 1.3124 | 1.3898 | 1.5005 | 1.6309 | 1.7173 |
| 53230. | 187.80 | .9877 | 1.0340 | 1.0379 | 1.0875 | 1.1887 | 1.2370 | 1.3124 | 1.3893 | 1.4989 | 1.6293 | 1.7148 |
| 53235. | 187.78 | .9877 | 1.0342 | 1.0386 | 1.0875 | 1.1867 | 1.2377 | 1.3130 | 1.3886 | 1.4978 | 1.6290 | 1.7131 |
| 53241. | 187.76 | .9874 | 1.0340 | 1.0393 | 1.0877 | 1.1877 | 1.2377 | 1.3135 | 1.3881 | 1.4975 | 1.6288 | 1.7115 |
| 53247. | 187.74 | .9874 | 1.0331 | 1.0384 | 1.0875 | 1.1872 | 1.2380 | 1.3135 | 1.3891 | 1.4973 | 1.6267 | 1.7093 |
| 53252. | 187.72 | .9877 | 1.0328 | 1.0388 | 1.0881 | 1.1877 | 1.2380 | 1.3130 | 1.3888 | 1.4959 | 1.6241 | 1.7060 |
| 53258. | 187.70 | .9888 | 1.0342 | 1.0397 | 1.0891 | 1.1877 | 1.2387 | 1.3130 | 1.3874 | 1.4951 | 1.6220 | 1.7040 |
| 53264. | 187.68 | .9904 | 1.0359 | 1.0397 | 1.0898 | 1.1882 | 1.2390 | 1.3132 | 1.3864 | 1.4957 | 1.6212 | 1.7041 |
| 53269. | 187.66 | .9918 | 1.0361 | 1.0397 | 1.0911 | 1.1897 | 1.2392 | 1.3132 | 1.3874 | 1.4954 | 1.6212 | 1.7036 |
| 53275. | 187.64 | .9931 | 1.0368 | 1.0406 | 1.0919 | 1.1908 | 1.2398 | 1.3132 | 1.3879 | 1.4935 | 1.6204 | 1.7011 |
| 53281. | 187.62 | .9949 | 1.0384 | 1.0417 | 1.0917 | 1.1933 | 1.2403 | 1.3143 | 1.3871 | 1.4922 | 1.6191 | 1.6986 |
| 53286. | 187.60 | .9963 | 1.0403 | 1.0431 | 1.0914 | 1.1953 | 1.2413 | 1.3149 | 1.3871 | 1.4927 | 1.6178 | 1.6973 |
| 53292. | 187.58 | .9981 | 1.0421 | 1.0442 | 1.0921 | 1.1948 | 1.2425 | 1.3159 | 1.3881 | 1.4938 | 1.6178 | 1.6975 |
| 53298. | 187.56 | .9999 | 1.0437 | 1.0462 | 1.0929 | 1.1968 | 1.2443 | 1.3175 | 1.3888 | 1.4951 | 1.6188 | 1.6989 |
| 53303. | 187.54 | 1.0015 | 1.0456 | 1.0483 | 1.0930 | 1.1978 | 1.2458 | 1.3200 | 1.3917 | 1.4962 | 1.6201 | 1.7000 |
| 53309. | 187.52 | 1.0024 | 1.0465 | 1.0494 | 1.0942 | 1.1989 | 1.2471 | 1.3216 | 1.3927 | 1.4970 | 1.6212 | 1.7003 |
| 53315. | 187.50 | 1.0033 | 1.0470 | 1.0501 | 1.0969 | 1.1999 | 1.2479 | 1.3216 | 1.3927 | 1.4978 | 1.6217 | 1.7008 |
| 53320. | 187.48 | 1.0036 | 1.0474 | 1.0512 | 1.1001 | 1.1994 | 1.2471 | 1.3210 | 1.3929 | 1.4986 | 1.6217 | 1.7011 |
| 53326. | 187.46 | 1.0033 | 1.0479 | 1.0517 | 1.1016 | 1.1994 | 1.2474 | 1.3213 | 1.3934 | 1.5000 | 1.6222 | 1.7011 |
| 53332. | 187.44 | 1.0031 | 1.0484 | 1.0519 | 1.1017 | 1.2009 | 1.2491 | 1.3224 | 1.3941 | 1.5008 | 1.6222 | 1.7008 |
| 53337. | 187.42 | 1.0033 | 1.0481 | 1.0526 | 1.1016 | 1.2014 | 1.2507 | 1.3235 | 1.3951 | 1.5010 | 1.6225 | 1.7003 |
| 53343. | 187.40 | 1.0038 | 1.0488 | 1.0537 | 1.1019 | 1.2009 | 1.2517 | 1.3240 | 1.3958 | 1.5016 | 1.6235 | 1.7011 |
| 53349. | 187.38 | 1.0056 | 1.0505 | 1.0544 | 1.1018 | 1.2029 | 1.2529 | 1.3254 | 1.3961 | 1.5021 | 1.6241 | 1.7022 |
| 53355. | 187.36 | 1.0077 | 1.0530 | 1.0550 | 1.1015 | 1.2044 | 1.2542 | 1.3264 | 1.3970 | 1.5032 | 1.6254 | 1.7022 |
| 53360. | 187.34 | 1.0095 | 1.0553 | 1.0555 | 1.1024 | 1.2059 | 1.2567 | 1.3275 | 1.3994 | 1.5045 | 1.6269 | 1.7014 |
| 53366. | 187.32 | 1.0113 | 1.0576 | 1.0564 | 1.1033 | 1.2075 | 1.2593 | 1.3291 | 1.4014 | 1.5056 | 1.6277 | 1.7022 |
| 53372. | 187.30 | 1.0138 | 1.0588 | 1.0582 | 1.1037 | 1.2095 | 1.2608 | 1.3307 | 1.4028 | 1.5069 | 1.6275 | 1.7036 |
| 53377. | 187.28 | 1.0158 | 1.0593 | 1.0609 | 1.1061 | 1.2105 | 1.2621 | 1.3324 | 1.4038 | 1.5083 | 1.6272 | 1.7036 |
| 53383. | 187.26 | 1.0165 | 1.0600 | 1.0632 | 1.1095 | 1.2145 | 1.2626 | 1.3326 | 1.4050 | 1.5091 | 1.6269 | 1.7022 |
| 53389. | 187.24 | 1.0170 | 1.0609 | 1.0650 | 1.1109 | 1.2145 | 1.2623 | 1.3329 | 1.4064 | 1.5091 | 1.6272 | 1.7008 |
| 53394. | 187.22 | 1.0172 | 1.0620 | 1.0663 | 1.1107 | 1.2156 | 1.2628 | 1.3334 | 1.4067 | 1.5096 | 1.6269 | 1.6997 |
| 53400. | 187.20 | 1.0179 | 1.0632 | 1.0674 | 1.1122 | 1.2156 | 1.2631 | 1.3337 | 1.4055 | 1.5102 | 1.6264 | 1.6992 |
| 53406. | 187.18 | 1.0195 | 1.0641 | 1.0688 | 1.1144 | 1.2140 | 1.2626 | 1.3342 | 1.4045 | 1.5102 | 1.6264 | 1.6995 |
| 53412. | 187.16 | 1.0206 | 1.0646 | 1.0692 | 1.1160 | 1.2145 | 1.2626 | 1.3348 | 1.4045 | 1.5102 | 1.6269 | 1.6997 |
| 53417. | 187.14 | 1.0215 | 1.0648 | 1.0699 | 1.1159 | 1.2176 | 1.2638 | 1.3356 | 1.4052 | 1.5104 | 1.6272 | 1.7006 |
| 53423. | 187.12 | 1.0229 | 1.0655 | 1.0713 | 1.1157 | 1.2181 | 1.2659 | 1.3367 | 1.4062 | 1.5110 | 1.6275 | 1.7014 |
| 53429. | 187.10 | 1.0240 | 1.0671 | 1.0717 | 1.1172 | 1.2181 | 1.2674 | 1.3377 | 1.4062 | 1.5120 | 1.6277 | 1.7019 |
| 53434. | 187.08 | 1.0249 | 1.0688 | 1.0722 | 1.1196 | 1.2191 | 1.2692 | 1.3385 | 1.4076 | 1.5126 | 1.6277 | 1.7022 |
| 53440. | 187.06 | 1.0261 | 1.0704 | 1.0731 | 1.1208 | 1.2196 | 1.2702 | 1.3399 | 1.4086 | 1.5134 | 1.6283 | 1.7025 |
| 53446. | 187.04 | 1.0272 | 1.0720 | 1.0735 | 1.1209 | 1.2209 | 1.2712 | 1.3404 | 1.4091 | 1.5142 | 1.6298 | 1.7044 |
| 53452. | 187.02 | 1.0277 | 1.0725 | 1.0735 | 1.1208 | 1.2242 | 1.2719 | 1.3412 | 1.4093 | 1.5150 | 1.6319 | 1.7066 |
| 53457. | 187.00 | 1.0281 | 1.0727 | 1.0744 | 1.1214 | 1.2257 | 1.2722 | 1.3424 | 1.4108 | 1.5161 | 1.6332 | 1.7082 |

| WAVENUMBER CM-1 | WAVELENGTH NM | CROSS SECTION X E19 | | | CM-2, TEMPERATURE DEG. K | | | | | | | |
|--------------------|------------------|---------------------|--------|--------|--------------------------|--------|--------|--------|--------|--------|--------|--------|
| | | 151. | 182. | 196. | 223. | 247. | 268. | 301. | 333. | 372. | 423. | 485. |
| 53457. | 187.00 | 1.0281 | 1.0727 | 1.0744 | 1.1214 | 1.2257 | 1.2722 | 1.3426 | 1.4108 | 1.5161 | 1.6332 | 1.7082 |
| 53463. | 186.98 | 1.0290 | 1.0732 | 1.0758 | 1.1234 | 1.2257 | 1.2719 | 1.3431 | 1.4125 | 1.5169 | 1.6335 | 1.7093 |
| 53469. | 186.96 | 1.0299 | 1.0741 | 1.0771 | 1.1258 | 1.2237 | 1.2737 | 1.3437 | 1.4139 | 1.5174 | 1.6338 | 1.7104 |
| 53474. | 186.94 | 1.0313 | 1.0743 | 1.0774 | 1.1261 | 1.2257 | 1.2757 | 1.3445 | 1.4139 | 1.5188 | 1.6348 | 1.7115 |
| 53480. | 186.92 | 1.0322 | 1.0753 | 1.0774 | 1.1253 | 1.2267 | 1.2768 | 1.3466 | 1.4139 | 1.5198 | 1.6364 | 1.7126 |
| 53486. | 186.90 | 1.0333 | 1.0769 | 1.0771 | 1.1244 | 1.2287 | 1.2775 | 1.3485 | 1.4154 | 1.5209 | 1.6398 | 1.7148 |
| 53492. | 186.88 | 1.0345 | 1.0778 | 1.0776 | 1.1242 | 1.2292 | 1.2783 | 1.3496 | 1.4171 | 1.5228 | 1.6424 | 1.7173 |
| 53497. | 186.86 | 1.0354 | 1.0780 | 1.0792 | 1.1260 | 1.2328 | 1.2793 | 1.3509 | 1.4192 | 1.5252 | 1.6437 | 1.7189 |
| 53503. | 186.84 | 1.0363 | 1.0785 | 1.0805 | 1.1290 | 1.2348 | 1.2813 | 1.3517 | 1.4209 | 1.5276 | 1.6440 | 1.7203 |
| 53509. | 186.82 | 1.0372 | 1.0797 | 1.0819 | 1.1308 | 1.2343 | 1.2844 | 1.3525 | 1.4228 | 1.5290 | 1.6461 | 1.7219 |
| 53514. | 186.80 | 1.0367 | 1.0806 | 1.0834 | 1.1321 | 1.2333 | 1.2854 | 1.3544 | 1.4238 | 1.5314 | 1.6487 | 1.7249 |
| 53520. | 186.78 | 1.0367 | 1.0810 | 1.0846 | 1.1332 | 1.2338 | 1.2851 | 1.3568 | 1.4255 | 1.5341 | 1.6519 | 1.7285 |
| 53526. | 186.76 | 1.0372 | 1.0810 | 1.0850 | 1.1336 | 1.2358 | 1.2849 | 1.3585 | 1.4274 | 1.5359 | 1.6553 | 1.7315 |
| 53532. | 186.74 | 1.0374 | 1.0815 | 1.0850 | 1.1339 | 1.2368 | 1.2849 | 1.3601 | 1.4301 | 1.5375 | 1.6579 | 1.7340 |
| 53537. | 186.72 | 1.0381 | 1.0827 | 1.0857 | 1.1350 | 1.2373 | 1.2877 | 1.3612 | 1.4315 | 1.5400 | 1.6598 | 1.7359 |
| 53543. | 186.70 | 1.0390 | 1.0845 | 1.0870 | 1.1360 | 1.2373 | 1.2917 | 1.3625 | 1.4327 | 1.5421 | 1.6616 | 1.7383 |
| 53549. | 186.68 | 1.0406 | 1.0871 | 1.0877 | 1.1371 | 1.2393 | 1.2942 | 1.3649 | 1.4349 | 1.5448 | 1.6650 | 1.7419 |
| 53555. | 186.66 | 1.0420 | 1.0894 | 1.0886 | 1.1386 | 1.2414 | 1.2960 | 1.3690 | 1.4390 | 1.5488 | 1.6695 | 1.7463 |
| 53560. | 186.64 | 1.0445 | 1.0922 | 1.0907 | 1.1392 | 1.2459 | 1.2993 | 1.3733 | 1.4434 | 1.5545 | 1.6745 | 1.7509 |
| 53566. | 186.62 | 1.0476 | 1.0961 | 1.0925 | 1.1390 | 1.2510 | 1.3049 | 1.3773 | 1.4467 | 1.5598 | 1.6797 | 1.7556 |
| 53572. | 186.60 | 1.0515 | 1.1007 | 1.0952 | 1.1407 | 1.2550 | 1.3107 | 1.3816 | 1.4503 | 1.5655 | 1.6842 | 1.7608 |
| 53578. | 186.58 | 1.0551 | 1.1056 | 1.0985 | 1.1443 | 1.2576 | 1.3153 | 1.3870 | 1.4554 | 1.5708 | 1.6900 | 1.7663 |
| 53583. | 186.56 | 1.0597 | 1.1084 | 1.1022 | 1.1486 | 1.2626 | 1.3188 | 1.3924 | 1.4619 | 1.5759 | 1.6963 | 1.7715 |
| 53589. | 186.54 | 1.0629 | 1.1098 | 1.1055 | 1.1534 | 1.2682 | 1.3216 | 1.3967 | 1.4668 | 1.5805 | 1.7023 | 1.7761 |
| 53595. | 186.52 | 1.0654 | 1.1114 | 1.1096 | 1.1583 | 1.2697 | 1.3244 | 1.4002 | 1.4709 | 1.5848 | 1.7073 | 1.7805 |
| 53601. | 186.50 | 1.0658 | 1.1126 | 1.1127 | 1.1626 | 1.2733 | 1.3269 | 1.4029 | 1.4757 | 1.5878 | 1.7112 | 1.7838 |
| 53606. | 186.48 | 1.0654 | 1.1130 | 1.1152 | 1.1657 | 1.2748 | 1.3277 | 1.4042 | 1.4798 | 1.5894 | 1.7139 | 1.7860 |
| 53612. | 186.46 | 1.0649 | 1.1130 | 1.1168 | 1.1678 | 1.2748 | 1.3277 | 1.4048 | 1.4815 | 1.5896 | 1.7146 | 1.7868 |
| 53618. | 186.44 | 1.0651 | 1.1133 | 1.1177 | 1.1685 | 1.2763 | 1.3277 | 1.4053 | 1.4817 | 1.5904 | 1.7152 | 1.7876 |
| 53624. | 186.42 | 1.0656 | 1.1135 | 1.1179 | 1.1683 | 1.2768 | 1.3272 | 1.4045 | 1.4810 | 1.5921 | 1.7146 | 1.7879 |
| 53629. | 186.40 | 1.0649 | 1.1133 | 1.1182 | 1.1687 | 1.2753 | 1.3272 | 1.4040 | 1.4800 | 1.5929 | 1.7146 | 1.7874 |
| 53635. | 186.38 | 1.0635 | 1.1123 | 1.1184 | 1.1689 | 1.2743 | 1.3269 | 1.4042 | 1.4800 | 1.5923 | 1.7149 | 1.7860 |
| 53641. | 186.36 | 1.0631 | 1.1107 | 1.1184 | 1.1693 | 1.2733 | 1.3259 | 1.4034 | 1.4800 | 1.5910 | 1.7149 | 1.7852 |
| 53647. | 186.34 | 1.0631 | 1.1100 | 1.1179 | 1.1694 | 1.2753 | 1.3249 | 1.4021 | 1.4786 | 1.5891 | 1.7136 | 1.7838 |
| 53652. | 186.32 | 1.0635 | 1.1098 | 1.1173 | 1.1689 | 1.2728 | 1.3237 | 1.4013 | 1.4774 | 1.5861 | 1.7115 | 1.7813 |
| 53658. | 186.30 | 1.0635 | 1.1096 | 1.1166 | 1.1687 | 1.2712 | 1.3219 | 1.3999 | 1.4762 | 1.5835 | 1.7083 | 1.7778 |
| 53664. | 186.28 | 1.0635 | 1.1091 | 1.1166 | 1.1690 | 1.2697 | 1.3206 | 1.3986 | 1.4752 | 1.5816 | 1.7044 | 1.7728 |
| 53670. | 186.26 | 1.0635 | 1.1091 | 1.1170 | 1.1689 | 1.2702 | 1.3198 | 1.3975 | 1.4730 | 1.5789 | 1.7005 | 1.7674 |
| 53675. | 186.24 | 1.0640 | 1.1093 | 1.1170 | 1.1679 | 1.2672 | 1.3193 | 1.3964 | 1.4696 | 1.5767 | 1.6970 | 1.7630 |
| 53681. | 186.22 | 1.0645 | 1.1098 | 1.1161 | 1.1666 | 1.2677 | 1.3186 | 1.3943 | 1.4665 | 1.5751 | 1.6928 | 1.7597 |
| 53687. | 186.20 | 1.0658 | 1.1105 | 1.1150 | 1.1658 | 1.2682 | 1.3183 | 1.3932 | 1.4643 | 1.5738 | 1.6892 | 1.7561 |
| 53693. | 186.18 | 1.0663 | 1.1112 | 1.1143 | 1.1656 | 1.2687 | 1.3183 | 1.3935 | 1.4636 | 1.5725 | 1.6863 | 1.7523 |
| 53698. | 186.16 | 1.0663 | 1.1119 | 1.1148 | 1.1661 | 1.2697 | 1.3181 | 1.3932 | 1.4641 | 1.5708 | 1.6844 | 1.7498 |
| 53704. | 186.14 | 1.0667 | 1.1126 | 1.1159 | 1.1669 | 1.2692 | 1.3186 | 1.3929 | 1.4634 | 1.5698 | 1.6831 | 1.7474 |
| 53710. | 186.12 | 1.0674 | 1.1135 | 1.1159 | 1.1665 | 1.2697 | 1.3201 | 1.3955 | 1.4622 | 1.5684 | 1.6813 | 1.7460 |
| 53716. | 186.10 | 1.0685 | 1.1144 | 1.1168 | 1.1653 | 1.2697 | 1.3209 | 1.3927 | 1.4622 | 1.5668 | 1.6800 | 1.7446 |
| 53722. | 186.08 | 1.0692 | 1.1147 | 1.1191 | 1.1657 | 1.2717 | 1.3204 | 1.3921 | 1.4622 | 1.5671 | 1.6792 | 1.7433 |
| 53727. | 186.06 | 1.0708 | 1.1154 | 1.1211 | 1.1677 | 1.2722 | 1.3204 | 1.3921 | 1.4619 | 1.5668 | 1.6784 | 1.7414 |
| 53733. | 186.04 | 1.0722 | 1.1163 | 1.1211 | 1.1689 | 1.2702 | 1.3216 | 1.3927 | 1.4617 | 1.5652 | 1.6771 | 1.7408 |
| 53739. | 186.02 | 1.0722 | 1.1165 | 1.1211 | 1.1687 | 1.2728 | 1.3234 | 1.3929 | 1.4624 | 1.5636 | 1.6758 | 1.7403 |
| 53745. | 186.00 | 1.0722 | 1.1172 | 1.1215 | 1.1683 | 1.2728 | 1.3242 | 1.3935 | 1.4629 | 1.5631 | 1.6753 | 1.7381 |

| WAVENUMBER CM-1 | WAVELENGTH MM | CROSS SECTION X E19 | | | CM-2 | | | TEMPERATURE DEG. K | | | | |
|--------------------|------------------|---------------------|--------|--------|--------|--------|--------|--------------------|--------|--------|--------|--------|
| | | 151. | 182. | 196. | 223. | 247. | 268. | 301. | 333. | 372. | 423. | 485. |
| 53745. | 186.00 | 1.0722 | 1.1172 | 1.1215 | 1.1683 | 1.2728 | 1.3242 | 1.3935 | 1.4629 | 1.5631 | 1.6753 | 1.7381 |
| 53750. | 185.98 | 1.0729 | 1.1181 | 1.1222 | 1.1687 | 1.2728 | 1.3229 | 1.3937 | 1.4617 | 1.5625 | 1.6745 | 1.7351 |
| 53758. | 185.96 | 1.0740 | 1.1188 | 1.1231 | 1.1703 | 1.2738 | 1.3221 | 1.3929 | 1.4602 | 1.5620 | 1.6734 | 1.7323 |
| 53762. | 185.94 | 1.0749 | 1.1195 | 1.1236 | 1.1710 | 1.2748 | 1.3226 | 1.3927 | 1.4598 | 1.5622 | 1.6713 | 1.7318 |
| 53768. | 185.92 | 1.0754 | 1.1207 | 1.1240 | 1.1704 | 1.2748 | 1.3231 | 1.3929 | 1.4605 | 1.5631 | 1.6695 | 1.7312 |
| 53774. | 185.90 | 1.0772 | 1.1225 | 1.1247 | 1.1708 | 1.2750 | 1.3239 | 1.3937 | 1.4619 | 1.5625 | 1.6684 | 1.7301 |
| 53779. | 185.88 | 1.0799 | 1.1246 | 1.1254 | 1.1721 | 1.2763 | 1.3254 | 1.3945 | 1.4629 | 1.5622 | 1.6674 | 1.7296 |
| 53785. | 185.86 | 1.0826 | 1.1269 | 1.1267 | 1.1735 | 1.2793 | 1.3277 | 1.3953 | 1.4629 | 1.5620 | 1.6669 | 1.7288 |
| 53791. | 185.84 | 1.0851 | 1.1297 | 1.1283 | 1.1744 | 1.2814 | 1.3297 | 1.3964 | 1.4631 | 1.5620 | 1.6666 | 1.7274 |
| 53797. | 185.82 | 1.0881 | 1.1323 | 1.1306 | 1.1759 | 1.2814 | 1.3325 | 1.3972 | 1.4641 | 1.5622 | 1.6661 | 1.7263 |
| 53802. | 185.80 | 1.0906 | 1.1350 | 1.1337 | 1.1755 | 1.2849 | 1.3348 | 1.3986 | 1.4651 | 1.5633 | 1.6658 | 1.7257 |
| 53808. | 185.78 | 1.0931 | 1.1371 | 1.1364 | 1.1768 | 1.2884 | 1.3353 | 1.4005 | 1.4663 | 1.5644 | 1.6658 | 1.7252 |
| 53814. | 185.76 | 1.0949 | 1.1390 | 1.1382 | 1.1795 | 1.2905 | 1.3351 | 1.4032 | 1.4680 | 1.5652 | 1.6663 | 1.7244 |
| 53820. | 185.74 | 1.0965 | 1.1401 | 1.1396 | 1.1824 | 1.2910 | 1.3358 | 1.4048 | 1.4701 | 1.5657 | 1.6674 | 1.7249 |
| 53826. | 185.72 | 1.0976 | 1.1406 | 1.1414 | 1.1844 | 1.2920 | 1.3371 | 1.4053 | 1.4709 | 1.5663 | 1.6674 | 1.7252 |
| 53831. | 185.70 | 1.0976 | 1.1411 | 1.1434 | 1.1871 | 1.2950 | 1.3381 | 1.4045 | 1.4709 | 1.5663 | 1.6671 | 1.7244 |
| 53837. | 185.68 | 1.0969 | 1.1415 | 1.1450 | 1.1896 | 1.2945 | 1.3381 | 1.4032 | 1.4709 | 1.5652 | 1.6669 | 1.7230 |
| 53843. | 185.66 | 1.0969 | 1.1418 | 1.1459 | 1.1898 | 1.2935 | 1.3381 | 1.4029 | 1.4699 | 1.5644 | 1.6666 | 1.7214 |
| 53849. | 185.64 | 1.0978 | 1.1420 | 1.1463 | 1.1891 | 1.2935 | 1.3384 | 1.4032 | 1.4684 | 1.5644 | 1.6663 | 1.7203 |
| 53855. | 185.62 | 1.0990 | 1.1425 | 1.1461 | 1.1895 | 1.2915 | 1.3384 | 1.4026 | 1.4672 | 1.5644 | 1.6650 | 1.7194 |
| 53860. | 185.60 | 1.1003 | 1.1432 | 1.1461 | 1.1905 | 1.2935 | 1.3384 | 1.4034 | 1.4677 | 1.5647 | 1.6637 | 1.7203 |
| 53866. | 185.58 | 1.1022 | 1.1436 | 1.1461 | 1.1924 | 1.2930 | 1.3389 | 1.4053 | 1.4689 | 1.5652 | 1.6637 | 1.7219 |
| 53872. | 185.56 | 1.1028 | 1.1446 | 1.1466 | 1.1946 | 1.2945 | 1.3406 | 1.4069 | 1.4704 | 1.5660 | 1.6661 | 1.7238 |
| 53878. | 185.54 | 1.1024 | 1.1457 | 1.1470 | 1.1949 | 1.2965 | 1.3429 | 1.4077 | 1.4716 | 1.5671 | 1.6687 | 1.7249 |
| 53884. | 185.52 | 1.1022 | 1.1469 | 1.1479 | 1.1946 | 1.2976 | 1.3432 | 1.4085 | 1.4718 | 1.5684 | 1.6700 | 1.7257 |
| 53889. | 185.50 | 1.1028 | 1.1476 | 1.1495 | 1.1949 | 1.3001 | 1.3422 | 1.4091 | 1.4721 | 1.5695 | 1.6708 | 1.7266 |
| 53895. | 185.48 | 1.1038 | 1.1480 | 1.1504 | 1.1954 | 1.3006 | 1.3422 | 1.4102 | 1.4737 | 1.5698 | 1.6713 | 1.7274 |
| 53901. | 185.46 | 1.1044 | 1.1478 | 1.1513 | 1.1958 | 1.2996 | 1.3432 | 1.4110 | 1.4752 | 1.5695 | 1.6724 | 1.7290 |
| 53907. | 185.44 | 1.1056 | 1.1471 | 1.1515 | 1.1956 | 1.3011 | 1.3447 | 1.4107 | 1.4754 | 1.5700 | 1.6737 | 1.7312 |
| 53913. | 185.42 | 1.1060 | 1.1476 | 1.1517 | 1.1955 | 1.3006 | 1.3444 | 1.4104 | 1.4752 | 1.5716 | 1.6739 | 1.7329 |
| 53919. | 185.40 | 1.1058 | 1.1483 | 1.1515 | 1.1962 | 1.2986 | 1.3457 | 1.4118 | 1.4759 | 1.5733 | 1.6747 | 1.7340 |
| 53924. | 185.38 | 1.1060 | 1.1494 | 1.1511 | 1.1973 | 1.2996 | 1.3475 | 1.4128 | 1.4774 | 1.5751 | 1.6758 | 1.7356 |
| 53930. | 185.36 | 1.1072 | 1.1503 | 1.1515 | 1.1980 | 1.2996 | 1.3495 | 1.4137 | 1.4786 | 1.5770 | 1.6774 | 1.7381 |
| 53936. | 185.34 | 1.1076 | 1.1517 | 1.1529 | 1.1976 | 1.3011 | 1.3513 | 1.4155 | 1.4798 | 1.5786 | 1.6792 | 1.7403 |
| 53942. | 185.32 | 1.1088 | 1.1529 | 1.1542 | 1.1977 | 1.3031 | 1.3528 | 1.4180 | 1.4822 | 1.5802 | 1.6821 | 1.7419 |
| 53948. | 185.30 | 1.1103 | 1.1543 | 1.1554 | 1.1996 | 1.3051 | 1.3546 | 1.4196 | 1.4848 | 1.5829 | 1.6855 | 1.7433 |
| 53953. | 185.28 | 1.1122 | 1.1554 | 1.1569 | 1.2019 | 1.3062 | 1.3561 | 1.4209 | 1.4877 | 1.5856 | 1.6886 | 1.7457 |
| 53959. | 185.26 | 1.1126 | 1.1566 | 1.1592 | 1.2030 | 1.3097 | 1.3566 | 1.4231 | 1.4909 | 1.5883 | 1.6907 | 1.7482 |
| 53965. | 185.24 | 1.1124 | 1.1575 | 1.1610 | 1.2041 | 1.3117 | 1.3566 | 1.4260 | 1.4935 | 1.5904 | 1.6913 | 1.7482 |
| 53971. | 185.22 | 1.1131 | 1.1575 | 1.1608 | 1.2061 | 1.3127 | 1.3563 | 1.4268 | 1.4933 | 1.5902 | 1.6907 | 1.7468 |
| 53977. | 185.20 | 1.1140 | 1.1575 | 1.1608 | 1.2075 | 1.3122 | 1.3566 | 1.4258 | 1.4914 | 1.5883 | 1.6894 | 1.7457 |
| 53983. | 185.18 | 1.1151 | 1.1580 | 1.1614 | 1.2067 | 1.3102 | 1.3579 | 1.4242 | 1.4902 | 1.5872 | 1.6886 | 1.7463 |
| 53989. | 185.16 | 1.1163 | 1.1589 | 1.1617 | 1.2058 | 1.3112 | 1.3604 | 1.4247 | 1.4904 | 1.5888 | 1.6892 | 1.7482 |
| 53994. | 185.14 | 1.1167 | 1.1596 | 1.1630 | 1.2062 | 1.3148 | 1.3632 | 1.4268 | 1.4914 | 1.5923 | 1.6931 | 1.7515 |
| 54000. | 185.12 | 1.1176 | 1.1622 | 1.1644 | 1.2069 | 1.3148 | 1.3652 | 1.4303 | 1.4935 | 1.5972 | 1.6984 | 1.7556 |
| 54006. | 185.10 | 1.1188 | 1.1643 | 1.1653 | 1.2085 | 1.3168 | 1.3680 | 1.4333 | 1.4942 | 1.6031 | 1.7028 | 1.7602 |
| 54012. | 185.08 | 1.1197 | 1.1645 | 1.1657 | 1.2104 | 1.3213 | 1.3723 | 1.4344 | 1.5010 | 1.6092 | 1.7060 | 1.7652 |
| 54018. | 185.06 | 1.1203 | 1.1645 | 1.1682 | 1.2126 | 1.3244 | 1.3754 | 1.4384 | 1.5061 | 1.6146 | 1.7112 | 1.7720 |
| 54023. | 185.04 | 1.1212 | 1.1656 | 1.1709 | 1.2145 | 1.3249 | 1.3766 | 1.4478 | 1.5116 | 1.6205 | 1.7202 | 1.7800 |
| 54029. | 185.02 | 1.1210 | 1.1666 | 1.1720 | 1.2156 | 1.3310 | 1.3784 | 1.4570 | 1.5191 | 1.6267 | 1.7291 | 1.7871 |
| 54035. | 185.00 | 1.1199 | 1.1675 | 1.1725 | 1.2165 | 1.3345 | 1.3812 | 1.4600 | 1.5263 | 1.6294 | 1.7362 | 1.7931 |

| WAVENUMBER CM-1 | WAVELENGTH NM | CROSS SECTION X E19 | | | CM-2 , TEMPERATURE DEG. K | | | | | | | |
|--------------------|------------------|---------------------|--------|--------|---------------------------|--------|--------|--------|--------|--------|--------|--------|
| | | 151. | 182. | 196. | 223. | 247. | 268. | 301. | 333. | 372. | 423. | 485. |
| 54035. | 185.00 | 1.1199 | 1.1675 | 1.1725 | 1.2165 | 1.3345 | 1.3812 | 1.4600 | 1.5263 | 1.6294 | 1.7362 | 1.7931 |
| 54041. | 184.98 | 1.1185 | 1.1684 | 1.1727 | 1.2176 | 1.3340 | 1.3837 | 1.4605 | 1.5307 | 1.6315 | 1.7412 | 1.7986 |
| 54047. | 184.96 | 1.1183 | 1.1680 | 1.1720 | 1.2192 | 1.3335 | 1.3855 | 1.4613 | 1.5326 | 1.6353 | 1.7440 | 1.8032 |
| 54053. | 184.94 | 1.1188 | 1.1670 | 1.1723 | 1.2208 | 1.3340 | 1.3865 | 1.4618 | 1.5343 | 1.6393 | 1.7461 | 1.8063 |
| 54059. | 184.92 | 1.1192 | 1.1675 | 1.1732 | 1.2231 | 1.3345 | 1.3865 | 1.4637 | 1.5360 | 1.6417 | 1.7485 | 1.8082 |
| 54064. | 184.90 | 1.1192 | 1.1691 | 1.1732 | 1.2260 | 1.3355 | 1.3885 | 1.4661 | 1.5370 | 1.6425 | 1.7506 | 1.8087 |
| 54070. | 184.88 | 1.1199 | 1.1696 | 1.1725 | 1.2268 | 1.3370 | 1.3908 | 1.4670 | 1.5374 | 1.6423 | 1.7506 | 1.8071 |
| 54076. | 184.86 | 1.1203 | 1.1693 | 1.1734 | 1.2257 | 1.3375 | 1.3893 | 1.4645 | 1.5372 | 1.6415 | 1.7496 | 1.8063 |
| 54082. | 184.84 | 1.1210 | 1.1705 | 1.1750 | 1.2254 | 1.3391 | 1.3875 | 1.4624 | 1.5365 | 1.6415 | 1.7490 | 1.8063 |
| 54088. | 184.82 | 1.1222 | 1.1719 | 1.1756 | 1.2265 | 1.3385 | 1.3885 | 1.4624 | 1.5362 | 1.6412 | 1.7485 | 1.8049 |
| 54094. | 184.80 | 1.1235 | 1.1726 | 1.1759 | 1.2283 | 1.3391 | 1.3896 | 1.4635 | 1.5360 | 1.6398 | 1.7464 | 1.8019 |
| 54099. | 184.78 | 1.1256 | 1.1731 | 1.1774 | 1.2288 | 1.3406 | 1.3896 | 1.4643 | 1.5353 | 1.6382 | 1.7451 | 1.7997 |
| 54105. | 184.76 | 1.1278 | 1.1742 | 1.1788 | 1.2289 | 1.3401 | 1.3885 | 1.4632 | 1.5345 | 1.6374 | 1.7435 | 1.7972 |
| 54111. | 184.74 | 1.1294 | 1.1754 | 1.1795 | 1.2299 | 1.3385 | 1.3883 | 1.4616 | 1.5345 | 1.6382 | 1.7417 | 1.7942 |
| 54117. | 184.72 | 1.1308 | 1.1763 | 1.1797 | 1.2308 | 1.3385 | 1.3890 | 1.4616 | 1.5350 | 1.6382 | 1.7396 | 1.7917 |
| 54123. | 184.70 | 1.1324 | 1.1775 | 1.1804 | 1.2310 | 1.3396 | 1.3903 | 1.4613 | 1.5348 | 1.6361 | 1.7377 | 1.7898 |
| 54129. | 184.68 | 1.1337 | 1.1789 | 1.1815 | 1.2311 | 1.3426 | 1.3908 | 1.4616 | 1.5331 | 1.6339 | 1.7356 | 1.7868 |
| 54135. | 184.66 | 1.1340 | 1.1802 | 1.1829 | 1.2305 | 1.3441 | 1.3908 | 1.4616 | 1.5319 | 1.6329 | 1.7341 | 1.7838 |
| 54140. | 184.64 | 1.1333 | 1.1812 | 1.1835 | 1.2299 | 1.3411 | 1.3906 | 1.4610 | 1.5309 | 1.6318 | 1.7314 | 1.7808 |
| 54146. | 184.62 | 1.1333 | 1.1821 | 1.1842 | 1.2304 | 1.3411 | 1.3906 | 1.4600 | 1.5302 | 1.6299 | 1.7283 | 1.7786 |
| 54152. | 184.60 | 1.1337 | 1.1823 | 1.1851 | 1.2331 | 1.3421 | 1.3903 | 1.4591 | 1.5302 | 1.6286 | 1.7246 | 1.7759 |
| 54158. | 184.58 | 1.1344 | 1.1812 | 1.1865 | 1.2359 | 1.3411 | 1.3893 | 1.4575 | 1.5297 | 1.6267 | 1.7209 | 1.7720 |
| 54164. | 184.56 | 1.1351 | 1.1805 | 1.1865 | 1.2357 | 1.3416 | 1.3880 | 1.4565 | 1.5273 | 1.6237 | 1.7186 | 1.7696 |
| 54170. | 184.54 | 1.1356 | 1.1814 | 1.1865 | 1.2350 | 1.3421 | 1.3870 | 1.4554 | 1.5246 | 1.6213 | 1.7167 | 1.7668 |
| 54176. | 184.52 | 1.1358 | 1.1830 | 1.1871 | 1.2360 | 1.3401 | 1.3868 | 1.4540 | 1.5237 | 1.6194 | 1.7144 | 1.7635 |
| 54182. | 184.50 | 1.1365 | 1.1830 | 1.1874 | 1.2366 | 1.3396 | 1.3868 | 1.4530 | 1.5230 | 1.6178 | 1.7112 | 1.7602 |
| 54187. | 184.48 | 1.1367 | 1.1823 | 1.1865 | 1.2353 | 1.3406 | 1.3868 | 1.4519 | 1.5215 | 1.6157 | 1.7091 | 1.7570 |
| 54193. | 184.46 | 1.1376 | 1.1821 | 1.1856 | 1.2337 | 1.3391 | 1.3860 | 1.4513 | 1.5201 | 1.6130 | 1.7078 | 1.7542 |
| 54199. | 184.44 | 1.1383 | 1.1835 | 1.1862 | 1.2343 | 1.3406 | 1.3852 | 1.4511 | 1.5191 | 1.6103 | 1.7057 | 1.7520 |
| 54205. | 184.42 | 1.1390 | 1.1837 | 1.1874 | 1.2359 | 1.3385 | 1.3850 | 1.4508 | 1.5184 | 1.6090 | 1.7028 | 1.7501 |
| 54211. | 184.40 | 1.1397 | 1.1833 | 1.1880 | 1.2358 | 1.3401 | 1.3852 | 1.4508 | 1.5174 | 1.6084 | 1.6999 | 1.7479 |
| 54217. | 184.38 | 1.1399 | 1.1840 | 1.1887 | 1.2358 | 1.3406 | 1.3863 | 1.4508 | 1.5167 | 1.6082 | 1.6989 | 1.7460 |
| 54223. | 184.36 | 1.1406 | 1.1853 | 1.1898 | 1.2363 | 1.3401 | 1.3870 | 1.4513 | 1.5160 | 1.6076 | 1.6984 | 1.7438 |
| 54229. | 184.34 | 1.1412 | 1.1863 | 1.1898 | 1.2358 | 1.3426 | 1.3865 | 1.4519 | 1.5160 | 1.6079 | 1.6973 | 1.7419 |
| 54234. | 184.32 | 1.1426 | 1.1872 | 1.1889 | 1.2350 | 1.3421 | 1.3860 | 1.4513 | 1.5157 | 1.6084 | 1.6963 | 1.7405 |
| 54240. | 184.30 | 1.1440 | 1.1874 | 1.1894 | 1.2351 | 1.3421 | 1.3863 | 1.4511 | 1.5150 | 1.6084 | 1.6957 | 1.7403 |
| 54246. | 184.28 | 1.1449 | 1.1877 | 1.1907 | 1.2356 | 1.3411 | 1.3865 | 1.4516 | 1.5148 | 1.6090 | 1.6957 | 1.7403 |
| 54252. | 184.26 | 1.1444 | 1.1874 | 1.1903 | 1.2362 | 1.3401 | 1.3870 | 1.4530 | 1.5150 | 1.6092 | 1.6957 | 1.7403 |
| 54258. | 184.24 | 1.1435 | 1.1874 | 1.1901 | 1.2366 | 1.3411 | 1.3868 | 1.4532 | 1.5155 | 1.6087 | 1.6955 | 1.7397 |
| 54264. | 184.22 | 1.1431 | 1.1870 | 1.1905 | 1.2359 | 1.3406 | 1.3850 | 1.4519 | 1.5167 | 1.6074 | 1.6942 | 1.7389 |
| 54270. | 184.20 | 1.1431 | 1.1863 | 1.1910 | 1.2360 | 1.3401 | 1.3840 | 1.4497 | 1.5162 | 1.6049 | 1.6923 | 1.7372 |
| 54276. | 184.18 | 1.1435 | 1.1863 | 1.1907 | 1.2376 | 1.3411 | 1.3842 | 1.4486 | 1.5136 | 1.6023 | 1.6905 | 1.7351 |
| 54282. | 184.16 | 1.1440 | 1.1872 | 1.1912 | 1.2381 | 1.3406 | 1.3850 | 1.4484 | 1.5104 | 1.6015 | 1.6894 | 1.7342 |
| 54288. | 184.14 | 1.1446 | 1.1886 | 1.1919 | 1.2378 | 1.3401 | 1.3860 | 1.4481 | 1.5099 | 1.6020 | 1.6892 | 1.7345 |
| 54293. | 184.12 | 1.1453 | 1.1895 | 1.1923 | 1.2370 | 1.3426 | 1.3870 | 1.4484 | 1.5111 | 1.6028 | 1.6892 | 1.7356 |
| 54299. | 184.10 | 1.1462 | 1.1902 | 1.1919 | 1.2368 | 1.3436 | 1.3870 | 1.4492 | 1.5116 | 1.6044 | 1.6907 | 1.7364 |
| 54305. | 184.08 | 1.1483 | 1.1904 | 1.1928 | 1.2378 | 1.3436 | 1.3888 | 1.4500 | 1.5119 | 1.6071 | 1.6926 | 1.7378 |
| 54311. | 184.06 | 1.1494 | 1.1904 | 1.1948 | 1.2385 | 1.3426 | 1.3916 | 1.4508 | 1.5136 | 1.6095 | 1.6944 | 1.7386 |
| 54317. | 184.04 | 1.1490 | 1.1907 | 1.1948 | 1.2386 | 1.3436 | 1.3936 | 1.4516 | 1.5164 | 1.6111 | 1.6955 | 1.7397 |
| 54323. | 184.02 | 1.1483 | 1.1911 | 1.1941 | 1.2393 | 1.3472 | 1.3946 | 1.4532 | 1.5189 | 1.6125 | 1.6965 | 1.7416 |
| 54329. | 184.00 | 1.1487 | 1.1930 | 1.1946 | 1.2392 | 1.3477 | 1.3959 | 1.4559 | 1.5205 | 1.6138 | 1.6989 | 1.7438 |

| WAVENUMBER (CM-1) | WAVELENGTH NM | CROSS SECTION X E19 | | | CM-2 | | TEMPERATURE DEG. K | | | | | | | |
|----------------------|------------------|---------------------|--------|--------|--------|--------|--------------------|--------|--------|--------|--------|--------|--|--|
| | | 151. | 182. | 196. | 223. | 247. | 268. | 301. | 333. | 372. | 423. | 485. | | |
| 54129. | 184.00 | 1.1487 | 1.1930 | 1.1946 | 1.2392 | 1.3477 | 1.3959 | 1.4559 | 1.5205 | 1.6138 | 1.6989 | 1.7438 | | |
| 54335. | 183.98 | 1.1499 | 1.1948 | 1.1950 | 1.2391 | 1.3492 | 1.3967 | 1.4586 | 1.5222 | 1.6157 | 1.7028 | 1.7457 | | |
| 54341. | 183.96 | 1.1519 | 1.1965 | 1.1955 | 1.2400 | 1.3517 | 1.3982 | 1.4613 | 1.5244 | 1.6181 | 1.7060 | 1.7477 | | |
| 54347. | 183.94 | 1.1542 | 1.1986 | 1.1964 | 1.2413 | 1.3532 | 1.4007 | 1.4635 | 1.5261 | 1.6202 | 1.7083 | 1.7482 | | |
| 54352. | 183.92 | 1.1565 | 1.2016 | 1.1980 | 1.2428 | 1.3552 | 1.4035 | 1.4661 | 1.5271 | 1.6219 | 1.7094 | 1.7496 | | |
| 54358. | 183.90 | 1.1594 | 1.2041 | 1.2002 | 1.2461 | 1.3568 | 1.4055 | 1.4678 | 1.5288 | 1.6240 | 1.7086 | 1.7515 | | |
| 54364. | 183.88 | 1.1619 | 1.2067 | 1.2038 | 1.2504 | 1.3603 | 1.4065 | 1.4688 | 1.5304 | 1.6253 | 1.7078 | 1.7518 | | |
| 54370. | 183.86 | 1.1631 | 1.2087 | 1.2063 | 1.2522 | 1.3623 | 1.4073 | 1.4696 | 1.5319 | 1.6259 | 1.7089 | 1.7512 | | |
| 54376. | 183.84 | 1.1640 | 1.2099 | 1.2077 | 1.2523 | 1.3639 | 1.4078 | 1.4710 | 1.5333 | 1.6259 | 1.7097 | 1.7498 | | |
| 54382. | 183.82 | 1.1656 | 1.2101 | 1.2090 | 1.2538 | 1.3649 | 1.4091 | 1.4723 | 1.5353 | 1.6253 | 1.7091 | 1.7479 | | |
| 54388. | 183.80 | 1.1669 | 1.2108 | 1.2110 | 1.2550 | 1.3669 | 1.4103 | 1.4729 | 1.5353 | 1.6248 | 1.7083 | 1.7468 | | |
| 54394. | 183.78 | 1.1669 | 1.2118 | 1.2131 | 1.2561 | 1.3669 | 1.4103 | 1.4729 | 1.5348 | 1.6259 | 1.7083 | 1.7474 | | |
| 54400. | 183.76 | 1.1669 | 1.2115 | 1.2153 | 1.2592 | 1.3664 | 1.4093 | 1.4723 | 1.5338 | 1.6264 | 1.7081 | 1.7485 | | |
| 54406. | 183.74 | 1.1674 | 1.2113 | 1.2167 | 1.2626 | 1.3654 | 1.4093 | 1.4713 | 1.5333 | 1.6253 | 1.7073 | 1.7504 | | |
| 54412. | 183.72 | 1.1678 | 1.2120 | 1.2164 | 1.2629 | 1.3664 | 1.4101 | 1.4707 | 1.5333 | 1.6245 | 1.7076 | 1.7509 | | |
| 54418. | 183.70 | 1.1685 | 1.2134 | 1.2149 | 1.2618 | 1.3659 | 1.4098 | 1.4713 | 1.5338 | 1.6253 | 1.7078 | 1.7490 | | |
| 54423. | 183.68 | 1.1694 | 1.2143 | 1.2149 | 1.2614 | 1.3654 | 1.4096 | 1.4723 | 1.5345 | 1.6259 | 1.7078 | 1.7471 | | |
| 54429. | 183.66 | 1.1696 | 1.2148 | 1.2160 | 1.2617 | 1.3669 | 1.4093 | 1.4726 | 1.5360 | 1.6253 | 1.7073 | 1.7471 | | |
| 54435. | 183.64 | 1.1692 | 1.2150 | 1.2176 | 1.2621 | 1.3649 | 1.4093 | 1.4729 | 1.5365 | 1.6251 | 1.7076 | 1.7479 | | |
| 54441. | 183.62 | 1.1694 | 1.2145 | 1.2178 | 1.2628 | 1.3659 | 1.4106 | 1.4729 | 1.5357 | 1.6262 | 1.7078 | 1.7493 | | |
| 54447. | 183.60 | 1.1694 | 1.2134 | 1.2180 | 1.2632 | 1.3674 | 1.4108 | 1.4721 | 1.5343 | 1.6267 | 1.7081 | 1.7518 | | |
| 54453. | 183.58 | 1.1683 | 1.2122 | 1.2187 | 1.2622 | 1.3633 | 1.4093 | 1.4707 | 1.5338 | 1.6264 | 1.7089 | 1.7537 | | |
| 54459. | 183.56 | 1.1665 | 1.2115 | 1.2185 | 1.2607 | 1.3628 | 1.4078 | 1.4707 | 1.5343 | 1.6264 | 1.7104 | 1.7542 | | |
| 54465. | 183.54 | 1.1656 | 1.2113 | 1.2164 | 1.2599 | 1.3639 | 1.4078 | 1.4721 | 1.5353 | 1.6272 | 1.7115 | 1.7548 | | |
| 54471. | 183.52 | 1.1646 | 1.2104 | 1.2140 | 1.2593 | 1.3644 | 1.4091 | 1.4731 | 1.5353 | 1.6283 | 1.7123 | 1.7561 | | |
| 54477. | 183.50 | 1.1635 | 1.2087 | 1.2133 | 1.2578 | 1.3633 | 1.4111 | 1.4745 | 1.5355 | 1.6299 | 1.7141 | 1.7581 | | |
| 54483. | 183.48 | 1.1628 | 1.2069 | 1.2128 | 1.2566 | 1.3633 | 1.4129 | 1.4740 | 1.5357 | 1.6323 | 1.7165 | 1.7602 | | |
| 54489. | 183.46 | 1.1619 | 1.2062 | 1.2126 | 1.2577 | 1.3639 | 1.4131 | 1.4740 | 1.5360 | 1.6339 | 1.7194 | 1.7633 | | |
| 54495. | 183.44 | 1.1606 | 1.2064 | 1.2124 | 1.2589 | 1.3628 | 1.4126 | 1.4756 | 1.5367 | 1.6347 | 1.7223 | 1.7660 | | |
| 54501. | 183.42 | 1.1587 | 1.2053 | 1.2117 | 1.2576 | 1.3639 | 1.4131 | 1.4769 | 1.5382 | 1.6364 | 1.7241 | 1.7679 | | |
| 54507. | 183.40 | 1.1578 | 1.2034 | 1.2113 | 1.2565 | 1.3644 | 1.4149 | 1.4753 | 1.5403 | 1.6396 | 1.7251 | 1.7704 | | |
| 54512. | 183.38 | 1.1574 | 1.2023 | 1.2108 | 1.2577 | 1.3623 | 1.4157 | 1.4737 | 1.5420 | 1.6431 | 1.7257 | 1.7739 | | |
| 54518. | 183.36 | 1.1578 | 1.2041 | 1.2092 | 1.2590 | 1.3639 | 1.4146 | 1.4756 | 1.5437 | 1.6466 | 1.7288 | 1.7780 | | |
| 54524. | 183.34 | 1.1594 | 1.2074 | 1.2081 | 1.2593 | 1.3684 | 1.4144 | 1.4812 | 1.5461 | 1.6490 | 1.7338 | 1.7808 | | |
| 54530. | 183.32 | 1.1628 | 1.2097 | 1.2081 | 1.2589 | 1.3684 | 1.4172 | 1.4861 | 1.5500 | 1.6492 | 1.7388 | 1.7830 | | |
| 54536. | 183.30 | 1.1676 | 1.2120 | 1.2088 | 1.2586 | 1.3709 | 1.4233 | 1.4888 | 1.5534 | 1.6500 | 1.7430 | 1.7860 | | |
| 54542. | 183.28 | 1.1724 | 1.2157 | 1.2106 | 1.2596 | 1.3765 | 1.4286 | 1.4920 | 1.5563 | 1.6538 | 1.7469 | 1.7890 | | |
| 54548. | 183.26 | 1.1762 | 1.2210 | 1.2135 | 1.2617 | 1.3806 | 1.4319 | 1.4963 | 1.5594 | 1.6584 | 1.7493 | 1.7904 | | |
| 54554. | 183.24 | 1.1794 | 1.2261 | 1.2173 | 1.2634 | 1.3851 | 1.4342 | 1.5008 | 1.5632 | 1.6611 | 1.7501 | 1.7909 | | |
| 54560. | 183.22 | 1.1828 | 1.2294 | 1.2221 | 1.2665 | 1.3871 | 1.4375 | 1.5036 | 1.5661 | 1.6643 | 1.7511 | 1.7915 | | |
| 54566. | 183.20 | 1.1855 | 1.2305 | 1.2270 | 1.2716 | 1.3912 | 1.4400 | 1.5049 | 1.5678 | 1.6672 | 1.7532 | 1.7917 | | |
| 54572. | 183.18 | 1.1878 | 1.2317 | 1.2311 | 1.2761 | 1.3942 | 1.4410 | 1.5049 | 1.5700 | 1.6686 | 1.7543 | 1.7909 | | |
| 54578. | 183.16 | 1.1894 | 1.2335 | 1.2349 | 1.2793 | 1.3937 | 1.4413 | 1.5052 | 1.5719 | 1.6670 | 1.7540 | 1.7887 | | |
| 54584. | 183.14 | 1.1885 | 1.2340 | 1.2374 | 1.2827 | 1.3917 | 1.4410 | 1.5055 | 1.5727 | 1.6637 | 1.7522 | 1.7854 | | |
| 54590. | 183.12 | 1.1867 | 1.2322 | 1.2383 | 1.2868 | 1.3897 | 1.4402 | 1.5038 | 1.5722 | 1.6603 | 1.7493 | 1.7813 | | |
| 54596. | 183.10 | 1.1862 | 1.2301 | 1.2381 | 1.2894 | 1.3881 | 1.4380 | 1.4982 | 1.5698 | 1.6578 | 1.7448 | 1.7780 | | |
| 54602. | 183.08 | 1.1852 | 1.2287 | 1.2367 | 1.2889 | 1.3897 | 1.4349 | 1.4928 | 1.5669 | 1.6573 | 1.7412 | 1.7767 | | |
| 54608. | 183.06 | 1.1849 | 1.2284 | 1.2354 | 1.2863 | 1.3897 | 1.4309 | 1.4928 | 1.5637 | 1.6578 | 1.7391 | 1.7750 | | |
| 54614. | 183.04 | 1.1821 | 1.2287 | 1.2340 | 1.2820 | 1.3876 | 1.4288 | 1.4968 | 1.5608 | 1.6557 | 1.7383 | 1.7696 | | |
| 54620. | 183.02 | 1.1805 | 1.2278 | 1.2324 | 1.2781 | 1.3861 | 1.4274 | 1.4974 | 1.5596 | 1.6495 | 1.7359 | 1.7630 | | |
| 54626. | 183.00 | 1.1801 | 1.2252 | 1.2327 | 1.2783 | 1.3836 | 1.4261 | 1.4928 | 1.5584 | 1.6425 | 1.7314 | 1.7594 | | |

| WAVENUMBER CM-1 | WAVELENGTH NM | CROSS SECTION X E19 | | | CM-2 | | | TEMPERATURE DEG. K | | | | |
|--------------------|------------------|---------------------|--------|--------|--------|--------|--------|--------------------|--------|--------|--------|--------|
| | | 151. | 182. | 196. | 223. | 247. | 268. | 301. | 333. | 372. | 423. | 485. |
| 54626. | 183.00 | 1.1801 | 1.2252 | 1.2327 | 1.2783 | 1.3836 | 1.4261 | 1.4928 | 1.5584 | 1.6425 | 1.7314 | 1.7594 |
| 54632. | 182.98 | 1.1794 | 1.2233 | 1.2327 | 1.2809 | 1.3821 | 1.4238 | 1.4874 | 1.5555 | 1.6369 | 1.7254 | 1.7561 |
| 54638. | 182.96 | 1.1790 | 1.2229 | 1.2311 | 1.2807 | 1.3795 | 1.4225 | 1.4853 | 1.5509 | 1.6342 | 1.7186 | 1.7498 |
| 54644. | 182.94 | 1.1778 | 1.2227 | 1.2288 | 1.2777 | 1.3775 | 1.4215 | 1.4842 | 1.5459 | 1.6315 | 1.7133 | 1.7430 |
| 54650. | 182.92 | 1.1776 | 1.2227 | 1.2277 | 1.2754 | 1.3780 | 1.4205 | 1.4820 | 1.5423 | 1.6294 | 1.7097 | 1.7389 |
| 54656. | 182.90 | 1.1780 | 1.2236 | 1.2275 | 1.2742 | 1.3790 | 1.4200 | 1.4801 | 1.5403 | 1.6270 | 1.7068 | 1.7351 |
| 54662. | 182.88 | 1.1780 | 1.2238 | 1.2279 | 1.2727 | 1.3785 | 1.4187 | 1.4793 | 1.5391 | 1.6245 | 1.7044 | 1.7318 |
| 54668. | 182.86 | 1.1774 | 1.2238 | 1.2275 | 1.2709 | 1.3775 | 1.4177 | 1.4780 | 1.5394 | 1.6229 | 1.7015 | 1.7301 |
| 54673. | 182.84 | 1.1778 | 1.2238 | 1.2266 | 1.2704 | 1.3760 | 1.4182 | 1.4777 | 1.5382 | 1.6232 | 1.6991 | 1.7282 |
| 54679. | 182.82 | 1.1799 | 1.2245 | 1.2250 | 1.2718 | 1.3740 | 1.4184 | 1.4775 | 1.5367 | 1.6229 | 1.6968 | 1.7260 |
| 54685. | 182.80 | 1.1812 | 1.2247 | 1.2257 | 1.2730 | 1.3765 | 1.4177 | 1.4775 | 1.5367 | 1.6211 | 1.6949 | 1.7247 |
| 54691. | 182.78 | 1.1815 | 1.2240 | 1.2270 | 1.2731 | 1.3765 | 1.4167 | 1.4777 | 1.5365 | 1.6192 | 1.6931 | 1.7233 |
| 54697. | 182.76 | 1.1817 | 1.2236 | 1.2277 | 1.2720 | 1.3740 | 1.4164 | 1.4780 | 1.5350 | 1.6176 | 1.6913 | 1.7219 |
| 54703. | 182.74 | 1.1819 | 1.2240 | 1.2291 | 1.2701 | 1.3750 | 1.4172 | 1.4777 | 1.5343 | 1.6162 | 1.6894 | 1.7208 |
| 54709. | 182.72 | 1.1824 | 1.2252 | 1.2293 | 1.2694 | 1.3750 | 1.4172 | 1.4756 | 1.5341 | 1.6143 | 1.6879 | 1.7189 |
| 54715. | 182.70 | 1.1824 | 1.2254 | 1.2291 | 1.2707 | 1.3755 | 1.4152 | 1.4740 | 1.5331 | 1.6135 | 1.6865 | 1.7162 |
| 54721. | 182.68 | 1.1821 | 1.2243 | 1.2284 | 1.2722 | 1.3730 | 1.4141 | 1.4731 | 1.5312 | 1.6141 | 1.6868 | 1.7145 |
| 54727. | 182.66 | 1.1824 | 1.2240 | 1.2282 | 1.2736 | 1.3725 | 1.4136 | 1.4721 | 1.5300 | 1.6141 | 1.6858 | 1.7131 |
| 54733. | 182.64 | 1.1824 | 1.2240 | 1.2286 | 1.2729 | 1.3745 | 1.4129 | 1.4710 | 1.5290 | 1.6117 | 1.6831 | 1.7115 |
| 54739. | 182.62 | 1.1830 | 1.2245 | 1.2295 | 1.2705 | 1.3725 | 1.4119 | 1.4713 | 1.5283 | 1.6084 | 1.6797 | 1.7093 |
| 54745. | 182.60 | 1.1833 | 1.2250 | 1.2304 | 1.2703 | 1.3725 | 1.4114 | 1.4718 | 1.5280 | 1.6068 | 1.6760 | 1.7074 |
| 54751. | 182.58 | 1.1835 | 1.2250 | 1.2311 | 1.2705 | 1.3709 | 1.4108 | 1.4715 | 1.5278 | 1.6063 | 1.6742 | 1.7055 |
| 54757. | 182.56 | 1.1840 | 1.2252 | 1.2304 | 1.2687 | 1.3709 | 1.4108 | 1.4699 | 1.5254 | 1.6052 | 1.6732 | 1.7025 |
| 54763. | 182.54 | 1.1844 | 1.2257 | 1.2297 | 1.2679 | 1.3709 | 1.4111 | 1.4680 | 1.5222 | 1.6036 | 1.6716 | 1.6997 |
| 54769. | 182.52 | 1.1835 | 1.2250 | 1.2295 | 1.2703 | 1.3709 | 1.4106 | 1.4664 | 1.5215 | 1.6023 | 1.6703 | 1.6984 |
| 54775. | 182.50 | 1.1830 | 1.2243 | 1.2297 | 1.2733 | 1.3714 | 1.4096 | 1.4659 | 1.5213 | 1.6023 | 1.6695 | 1.6992 |
| 54781. | 182.48 | 1.1835 | 1.2245 | 1.2306 | 1.2736 | 1.3730 | 1.4103 | 1.4648 | 1.5203 | 1.6020 | 1.6679 | 1.7003 |
| 54787. | 182.46 | 1.1849 | 1.2261 | 1.2309 | 1.2707 | 1.3735 | 1.4116 | 1.4648 | 1.5198 | 1.6020 | 1.6663 | 1.6997 |
| 54793. | 182.44 | 1.1860 | 1.2282 | 1.2293 | 1.2677 | 1.3720 | 1.4136 | 1.4661 | 1.5201 | 1.6023 | 1.6661 | 1.6984 |
| 54799. | 182.42 | 1.1876 | 1.2301 | 1.2284 | 1.2669 | 1.3735 | 1.4149 | 1.4678 | 1.5208 | 1.6025 | 1.6661 | 1.6986 |
| 54805. | 182.40 | 1.1883 | 1.2322 | 1.2297 | 1.2677 | 1.3765 | 1.4154 | 1.4680 | 1.5218 | 1.6033 | 1.6661 | 1.6992 |
| 54811. | 182.38 | 1.1885 | 1.2340 | 1.2311 | 1.2694 | 1.3775 | 1.4169 | 1.4688 | 1.5222 | 1.6039 | 1.6676 | 1.6989 |
| 54817. | 182.36 | 1.1896 | 1.2338 | 1.2318 | 1.2708 | 1.3770 | 1.4179 | 1.4707 | 1.5225 | 1.6031 | 1.6690 | 1.6989 |
| 54823. | 182.34 | 1.1903 | 1.2329 | 1.2327 | 1.2713 | 1.3765 | 1.4182 | 1.4710 | 1.5234 | 1.6025 | 1.6692 | 1.7000 |
| 54829. | 182.32 | 1.1903 | 1.2319 | 1.2343 | 1.2724 | 1.3785 | 1.4190 | 1.4696 | 1.5246 | 1.6047 | 1.6684 | 1.7006 |
| 54835. | 182.30 | 1.1899 | 1.2319 | 1.2347 | 1.2730 | 1.3780 | 1.4192 | 1.4691 | 1.5244 | 1.6076 | 1.6692 | 1.7006 |
| 54841. | 182.28 | 1.1912 | 1.2329 | 1.2345 | 1.2729 | 1.3780 | 1.4200 | 1.4702 | 1.5249 | 1.6087 | 1.6713 | 1.7022 |
| 54847. | 182.26 | 1.1921 | 1.2340 | 1.2338 | 1.2726 | 1.3801 | 1.4207 | 1.4726 | 1.5261 | 1.6092 | 1.6729 | 1.7047 |
| 54853. | 182.24 | 1.1926 | 1.2347 | 1.2352 | 1.2730 | 1.3795 | 1.4220 | 1.4758 | 1.5275 | 1.6103 | 1.6739 | 1.7060 |
| 54860. | 182.22 | 1.1928 | 1.2349 | 1.2379 | 1.2743 | 1.3795 | 1.4230 | 1.4766 | 1.5288 | 1.6119 | 1.6763 | 1.7077 |
| 54866. | 182.20 | 1.1942 | 1.2359 | 1.2390 | 1.2752 | 1.3816 | 1.4235 | 1.4780 | 1.5307 | 1.6130 | 1.6795 | 1.7110 |
| 54872. | 182.18 | 1.1949 | 1.2368 | 1.2381 | 1.2765 | 1.3846 | 1.4245 | 1.4801 | 1.5324 | 1.6143 | 1.6826 | 1.7153 |
| 54878. | 182.16 | 1.1953 | 1.2363 | 1.2388 | 1.2784 | 1.3841 | 1.4255 | 1.4818 | 1.5338 | 1.6162 | 1.6847 | 1.7189 |
| 54884. | 182.14 | 1.1960 | 1.2368 | 1.2410 | 1.2789 | 1.3846 | 1.4271 | 1.4820 | 1.5338 | 1.6186 | 1.6873 | 1.7227 |
| 54890. | 182.12 | 1.1962 | 1.2384 | 1.2421 | 1.2775 | 1.3866 | 1.4273 | 1.4826 | 1.5341 | 1.6219 | 1.6892 | 1.7257 |
| 54896. | 182.10 | 1.1955 | 1.2398 | 1.2417 | 1.2772 | 1.3871 | 1.4278 | 1.4839 | 1.5360 | 1.6237 | 1.6915 | 1.7277 |
| 54902. | 182.08 | 1.1949 | 1.2398 | 1.2419 | 1.2802 | 1.3866 | 1.4301 | 1.4855 | 1.5389 | 1.6243 | 1.6942 | 1.7301 |
| 54908. | 182.06 | 1.1942 | 1.2382 | 1.2424 | 1.2840 | 1.3851 | 1.4319 | 1.4855 | 1.5403 | 1.6275 | 1.6960 | 1.7334 |
| 54914. | 182.04 | 1.1924 | 1.2373 | 1.2419 | 1.2850 | 1.3846 | 1.4304 | 1.4853 | 1.5415 | 1.6324 | 1.6984 | 1.7375 |
| 54920. | 182.02 | 1.1901 | 1.2370 | 1.2403 | 1.2850 | 1.3836 | 1.4281 | 1.4864 | 1.5425 | 1.6355 | 1.7002 | 1.7400 |
| 54926. | 182.00 | 1.1880 | 1.2366 | 1.2403 | 1.2849 | 1.3831 | 1.4276 | 1.4885 | 1.5437 | 1.6353 | 1.7026 | 1.7386 |

| WAVENUMBER CM-1 | WAVELENGTH NM | CROSS SECTION X E19 | | | CM-2 | | | TEMPERATURE DEG. K | | | | |
|--------------------|------------------|---------------------|--------|--------|--------|--------|--------|--------------------|--------|--------|--------|--------|
| | | 151. | 182. | 196. | 223. | 247. | 268. | 301. | 333. | 372. | 423. | 485. |
| 54926. | 182.00 | 1.1880 | 1.2366 | 1.2403 | 1.2849 | 1.3831 | 1.4276 | 1.4885 | 1.5437 | 1.6353 | 1.7026 | 1.7386 |
| 54932. | 181.98 | 1.1869 | 1.2347 | 1.2415 | 1.2831 | 1.3816 | 1.4278 | 1.4885 | 1.5461 | 1.6323 | 1.7044 | 1.7381 |
| 54938. | 181.96 | 1.1867 | 1.2315 | 1.2419 | 1.2812 | 1.3826 | 1.4268 | 1.4858 | 1.5471 | 1.6302 | 1.7054 | 1.7397 |
| 54944. | 181.94 | 1.1862 | 1.2294 | 1.2406 | 1.2810 | 1.3846 | 1.4253 | 1.4834 | 1.5459 | 1.6294 | 1.7041 | 1.7405 |
| 54950. | 181.92 | 1.1862 | 1.2301 | 1.2374 | 1.2802 | 1.3806 | 1.4248 | 1.4818 | 1.5432 | 1.6275 | 1.7018 | 1.7383 |
| 54956. | 181.90 | 1.1874 | 1.2310 | 1.2356 | 1.2761 | 1.3801 | 1.4266 | 1.4818 | 1.5413 | 1.6264 | 1.7007 | 1.7372 |
| 54962. | 181.88 | 1.1883 | 1.2317 | 1.2358 | 1.2723 | 1.3816 | 1.4291 | 1.4828 | 1.5423 | 1.6280 | 1.7026 | 1.7383 |
| 54968. | 181.86 | 1.1887 | 1.2326 | 1.2356 | 1.2732 | 1.3876 | 1.4311 | 1.4847 | 1.5456 | 1.6323 | 1.7041 | 1.7394 |
| 54974. | 181.84 | 1.1903 | 1.2345 | 1.2354 | 1.2772 | 1.3866 | 1.4347 | 1.4874 | 1.5471 | 1.6369 | 1.7062 | 1.7411 |
| 54980. | 181.82 | 1.1933 | 1.2363 | 1.2356 | 1.2791 | 1.3866 | 1.4382 | 1.4909 | 1.5473 | 1.6417 | 1.7097 | 1.7438 |
| 54986. | 181.80 | 1.1953 | 1.2368 | 1.2381 | 1.2777 | 1.3927 | 1.4415 | 1.4944 | 1.5497 | 1.6468 | 1.7139 | 1.7471 |
| 54992. | 181.78 | 1.1964 | 1.2375 | 1.2397 | 1.2794 | 1.3952 | 1.4451 | 1.4966 | 1.5531 | 1.6517 | 1.7178 | 1.7518 |
| 54998. | 181.76 | 1.1969 | 1.2398 | 1.2403 | 1.2847 | 1.3988 | 1.4479 | 1.4995 | 1.5567 | 1.6565 | 1.7230 | 1.7553 |
| 55004. | 181.74 | 1.1985 | 1.2428 | 1.2424 | 1.2884 | 1.3993 | 1.4509 | 1.5052 | 1.5623 | 1.6608 | 1.7286 | 1.7578 |
| 55010. | 181.72 | 1.2003 | 1.2454 | 1.2453 | 1.2897 | 1.4023 | 1.4539 | 1.5108 | 1.5678 | 1.6637 | 1.7325 | 1.7600 |
| 55017. | 181.70 | 1.2001 | 1.2470 | 1.2480 | 1.2905 | 1.4054 | 1.4565 | 1.5133 | 1.5717 | 1.6640 | 1.7346 | 1.7622 |
| 55023. | 181.68 | 1.1987 | 1.2470 | 1.2500 | 1.2927 | 1.4064 | 1.4562 | 1.5133 | 1.5739 | 1.6627 | 1.7351 | 1.7638 |
| 55029. | 181.66 | 1.1967 | 1.2458 | 1.2514 | 1.2964 | 1.4054 | 1.4542 | 1.5143 | 1.5741 | 1.6613 | 1.7349 | 1.7630 |
| 55035. | 181.64 | 1.1951 | 1.2442 | 1.2518 | 1.2981 | 1.4043 | 1.4517 | 1.5146 | 1.5746 | 1.6592 | 1.7341 | 1.7589 |
| 55041. | 181.62 | 1.1939 | 1.2426 | 1.2514 | 1.2979 | 1.4018 | 1.4494 | 1.5116 | 1.5751 | 1.6570 | 1.7322 | 1.7545 |
| 55047. | 181.60 | 1.1924 | 1.2407 | 1.2505 | 1.2964 | 1.4008 | 1.4471 | 1.5079 | 1.5756 | 1.6543 | 1.7275 | 1.7515 |
| 55053. | 181.58 | 1.1908 | 1.2393 | 1.2489 | 1.2937 | 1.4008 | 1.4453 | 1.5057 | 1.5741 | 1.6514 | 1.7207 | 1.7468 |
| 55059. | 181.56 | 1.1910 | 1.2377 | 1.2462 | 1.2907 | 1.3968 | 1.4430 | 1.5046 | 1.5688 | 1.6471 | 1.7162 | 1.7403 |
| 55065. | 181.54 | 1.1926 | 1.2373 | 1.2446 | 1.2899 | 1.3947 | 1.4400 | 1.5020 | 1.5637 | 1.6425 | 1.7136 | 1.7351 |
| 55071. | 181.52 | 1.1939 | 1.2386 | 1.2446 | 1.2902 | 1.3952 | 1.4385 | 1.4985 | 1.5608 | 1.6396 | 1.7104 | 1.7315 |
| 55077. | 181.50 | 1.1942 | 1.2410 | 1.2446 | 1.2895 | 1.3952 | 1.4387 | 1.4958 | 1.5577 | 1.6380 | 1.7070 | 1.7279 |
| 55083. | 181.48 | 1.1942 | 1.2430 | 1.2430 | 1.2877 | 1.3952 | 1.4395 | 1.4944 | 1.5543 | 1.6355 | 1.7028 | 1.7238 |
| 55089. | 181.46 | 1.1946 | 1.2435 | 1.2421 | 1.2867 | 1.3937 | 1.4397 | 1.4928 | 1.5529 | 1.6339 | 1.6989 | 1.7194 |
| 55095. | 181.44 | 1.1955 | 1.2433 | 1.2435 | 1.2881 | 1.3922 | 1.4390 | 1.4923 | 1.5526 | 1.6318 | 1.6965 | 1.7156 |
| 55101. | 181.42 | 1.1962 | 1.2428 | 1.2455 | 1.2907 | 1.3932 | 1.4377 | 1.4925 | 1.5507 | 1.6286 | 1.6939 | 1.7121 |
| 55108. | 181.40 | 1.1971 | 1.2428 | 1.2473 | 1.2917 | 1.3947 | 1.4364 | 1.4917 | 1.5483 | 1.6259 | 1.6910 | 1.7096 |
| 55114. | 181.38 | 1.1983 | 1.2424 | 1.2478 | 1.2905 | 1.3927 | 1.4354 | 1.4901 | 1.5468 | 1.6237 | 1.6876 | 1.7069 |
| 55120. | 181.36 | 1.1987 | 1.2419 | 1.2478 | 1.2893 | 1.3912 | 1.4354 | 1.4890 | 1.5461 | 1.6213 | 1.6842 | 1.7052 |
| 55126. | 181.34 | 1.1978 | 1.2424 | 1.2482 | 1.2873 | 1.3907 | 1.4354 | 1.4877 | 1.5454 | 1.6197 | 1.6805 | 1.7030 |
| 55132. | 181.32 | 1.1971 | 1.2426 | 1.2489 | 1.2854 | 1.3897 | 1.4339 | 1.4863 | 1.5444 | 1.6184 | 1.6779 | 1.6995 |
| 55138. | 181.30 | 1.1971 | 1.2419 | 1.2478 | 1.2853 | 1.3892 | 1.4316 | 1.4847 | 1.5432 | 1.6162 | 1.6760 | 1.6962 |
| 55144. | 181.28 | 1.1974 | 1.2414 | 1.2471 | 1.2860 | 1.3892 | 1.4299 | 1.4834 | 1.5406 | 1.6146 | 1.6734 | 1.6945 |
| 55150. | 181.26 | 1.1971 | 1.2414 | 1.2473 | 1.2866 | 1.3887 | 1.4288 | 1.4818 | 1.5374 | 1.6130 | 1.6708 | 1.6918 |
| 55156. | 181.24 | 1.1967 | 1.2405 | 1.2457 | 1.2871 | 1.3876 | 1.4286 | 1.4804 | 1.5357 | 1.6108 | 1.6690 | 1.6880 |
| 55162. | 181.22 | 1.1962 | 1.2403 | 1.2437 | 1.2869 | 1.3861 | 1.4288 | 1.4788 | 1.5336 | 1.6087 | 1.6669 | 1.6847 |
| 55168. | 181.20 | 1.1964 | 1.2393 | 1.2442 | 1.2859 | 1.3846 | 1.4286 | 1.4766 | 1.5309 | 1.6063 | 1.6640 | 1.6814 |
| 55174. | 181.18 | 1.1969 | 1.2384 | 1.2444 | 1.2834 | 1.3846 | 1.4258 | 1.4753 | 1.5292 | 1.6033 | 1.6606 | 1.6792 |
| 55181. | 181.16 | 1.1967 | 1.2380 | 1.2433 | 1.2817 | 1.3816 | 1.4245 | 1.4734 | 1.5273 | 1.6004 | 1.6579 | 1.6773 |
| 55187. | 181.14 | 1.1958 | 1.2382 | 1.2430 | 1.2827 | 1.3821 | 1.4248 | 1.4723 | 1.5249 | 1.5985 | 1.6553 | 1.6745 |
| 55193. | 181.12 | 1.1951 | 1.2375 | 1.2433 | 1.2844 | 1.3816 | 1.4240 | 1.4718 | 1.5244 | 1.5977 | 1.6537 | 1.6718 |
| 55199. | 181.10 | 1.1955 | 1.2377 | 1.2430 | 1.2838 | 1.3821 | 1.4223 | 1.4707 | 1.5234 | 1.5977 | 1.6524 | 1.6702 |
| 55205. | 181.08 | 1.1955 | 1.2382 | 1.2428 | 1.2817 | 1.3831 | 1.4220 | 1.4691 | 1.5215 | 1.5977 | 1.6498 | 1.6688 |
| 55211. | 181.06 | 1.1955 | 1.2373 | 1.2424 | 1.2798 | 1.3811 | 1.4220 | 1.4678 | 1.5208 | 1.5961 | 1.6482 | 1.6677 |
| 55217. | 181.04 | 1.1962 | 1.2363 | 1.2410 | 1.2793 | 1.3801 | 1.4217 | 1.4656 | 1.5203 | 1.5931 | 1.6458 | 1.6677 |
| 55223. | 181.02 | 1.1964 | 1.2368 | 1.2415 | 1.2810 | 1.3816 | 1.4220 | 1.4648 | 1.5189 | 1.5929 | 1.6443 | 1.6682 |
| 55229. | 181.00 | 1.1960 | 1.2375 | 1.2412 | 1.2840 | 1.3821 | 1.4230 | 1.4656 | 1.5184 | 1.5945 | 1.6435 | 1.6693 |

| WAVENUMBER (CM-1) | WAVELENGTH NM | CROSS SECTION X E19 | | | CM-2 | | | TEMPERATURE DEG. K | | | | |
|----------------------|------------------|---------------------|--------|--------|--------|--------|--------|--------------------|--------|--------|--------|--------|
| | | 151. | 182. | 196. | 223. | 247. | 268. | 301. | 333. | 372. | 423. | 485. |
| 55229. | 181.00 | 1.1960 | 1.2375 | 1.2412 | 1.2840 | 1.3821 | 1.4230 | 1.4656 | 1.5184 | 1.5945 | 1.6435 | 1.6693 |
| 55235. | 180.98 | 1.1964 | 1.2377 | 1.2399 | 1.2838 | 1.3806 | 1.4225 | 1.4656 | 1.5181 | 1.5950 | 1.6437 | 1.6704 |
| 55241. | 180.96 | 1.1962 | 1.2373 | 1.2399 | 1.2799 | 1.3831 | 1.4215 | 1.4667 | 1.5177 | 1.5950 | 1.6453 | 1.6702 |
| 55248. | 180.94 | 1.1958 | 1.2373 | 1.2403 | 1.2763 | 1.3821 | 1.4217 | 1.4686 | 1.5186 | 1.5963 | 1.6466 | 1.6695 |
| 55254. | 180.92 | 1.1953 | 1.2366 | 1.2403 | 1.2745 | 1.3831 | 1.4225 | 1.4702 | 1.5191 | 1.5988 | 1.6477 | 1.6710 |
| 55260. | 180.90 | 1.1960 | 1.2361 | 1.2415 | 1.2759 | 1.3831 | 1.4230 | 1.4705 | 1.5184 | 1.5993 | 1.6490 | 1.6740 |
| 55266. | 180.88 | 1.1958 | 1.2352 | 1.2421 | 1.2791 | 1.3811 | 1.4225 | 1.4702 | 1.5181 | 1.5972 | 1.6500 | 1.6743 |
| 55272. | 180.86 | 1.1937 | 1.2340 | 1.2412 | 1.2798 | 1.3811 | 1.4200 | 1.4675 | 1.5184 | 1.5945 | 1.6508 | 1.6715 |
| 55278. | 180.84 | 1.1908 | 1.2338 | 1.2385 | 1.2779 | 1.3790 | 1.4172 | 1.4653 | 1.5193 | 1.5926 | 1.6495 | 1.6699 |
| 55284. | 180.82 | 1.1890 | 1.2345 | 1.2370 | 1.2761 | 1.3770 | 1.4162 | 1.4651 | 1.5189 | 1.5918 | 1.6461 | 1.6691 |
| 55290. | 180.80 | 1.1887 | 1.2333 | 1.2381 | 1.2739 | 1.3775 | 1.4174 | 1.4656 | 1.5169 | 1.5921 | 1.6437 | 1.6688 |
| 55296. | 180.78 | 1.1899 | 1.2308 | 1.2394 | 1.2727 | 1.3740 | 1.4184 | 1.4659 | 1.5150 | 1.5942 | 1.6437 | 1.6699 |
| 55303. | 180.76 | 1.1912 | 1.2301 | 1.2392 | 1.2736 | 1.3730 | 1.4197 | 1.4653 | 1.5148 | 1.5980 | 1.6458 | 1.6734 |
| 55309. | 180.74 | 1.1914 | 1.2315 | 1.2390 | 1.2746 | 1.3765 | 1.4230 | 1.4670 | 1.5167 | 1.6033 | 1.6495 | 1.6784 |
| 55315. | 180.72 | 1.1896 | 1.2331 | 1.2390 | 1.2749 | 1.3790 | 1.4261 | 1.4707 | 1.5201 | 1.6071 | 1.6545 | 1.6825 |
| 55321. | 180.70 | 1.1885 | 1.2345 | 1.2388 | 1.2744 | 1.3785 | 1.4271 | 1.4731 | 1.5230 | 1.6108 | 1.6613 | 1.6874 |
| 55327. | 180.68 | 1.1890 | 1.2338 | 1.2381 | 1.2736 | 1.3790 | 1.4283 | 1.4742 | 1.5256 | 1.6154 | 1.6671 | 1.6934 |
| 55333. | 180.66 | 1.1890 | 1.2322 | 1.2383 | 1.2739 | 1.3811 | 1.4299 | 1.4775 | 1.5297 | 1.6192 | 1.6716 | 1.6989 |
| 55339. | 180.64 | 1.1883 | 1.2319 | 1.2376 | 1.2751 | 1.3841 | 1.4311 | 1.4828 | 1.5319 | 1.6213 | 1.6750 | 1.7038 |
| 55345. | 180.62 | 1.1892 | 1.2347 | 1.2374 | 1.2759 | 1.3866 | 1.4329 | 1.4861 | 1.5326 | 1.6237 | 1.6792 | 1.7074 |
| 55352. | 180.60 | 1.1903 | 1.2368 | 1.2385 | 1.2771 | 1.3836 | 1.4352 | 1.4850 | 1.5350 | 1.6272 | 1.6837 | 1.7090 |
| 55358. | 180.58 | 1.1919 | 1.2363 | 1.2406 | 1.2795 | 1.3866 | 1.4367 | 1.4855 | 1.5401 | 1.6304 | 1.6863 | 1.7123 |
| 55364. | 180.56 | 1.1928 | 1.2368 | 1.2401 | 1.2816 | 1.3942 | 1.4367 | 1.4904 | 1.5456 | 1.6321 | 1.6873 | 1.7153 |
| 55370. | 180.54 | 1.1935 | 1.2403 | 1.2401 | 1.2825 | 1.3922 | 1.4370 | 1.4933 | 1.5464 | 1.6323 | 1.6884 | 1.7170 |
| 55376. | 180.52 | 1.1946 | 1.2419 | 1.2437 | 1.2829 | 1.3942 | 1.4382 | 1.4928 | 1.5459 | 1.6315 | 1.6892 | 1.7184 |
| 55382. | 180.50 | 1.1955 | 1.2405 | 1.2466 | 1.2845 | 1.3947 | 1.4395 | 1.4912 | 1.5468 | 1.6304 | 1.6879 | 1.7173 |
| 55388. | 180.48 | 1.1976 | 1.2386 | 1.2451 | 1.2886 | 1.3927 | 1.4397 | 1.4898 | 1.5468 | 1.6291 | 1.6863 | 1.7156 |
| 55395. | 180.46 | 1.2001 | 1.2384 | 1.2435 | 1.2918 | 1.3947 | 1.4400 | 1.4901 | 1.5452 | 1.6280 | 1.6850 | 1.7131 |
| 55401. | 180.44 | 1.2010 | 1.2403 | 1.2435 | 1.2901 | 1.3937 | 1.4402 | 1.4917 | 1.5444 | 1.6294 | 1.6842 | 1.7112 |
| 55407. | 180.42 | 1.2005 | 1.2430 | 1.2451 | 1.2876 | 1.3937 | 1.4415 | 1.4923 | 1.5447 | 1.6307 | 1.6837 | 1.7101 |
| 55413. | 180.40 | 1.2001 | 1.2451 | 1.2471 | 1.2875 | 1.3942 | 1.4430 | 1.4920 | 1.5444 | 1.6310 | 1.6842 | 1.7082 |
| 55419. | 180.38 | 1.2003 | 1.2465 | 1.2489 | 1.2878 | 1.3973 | 1.4438 | 1.4923 | 1.5439 | 1.6307 | 1.6847 | 1.7055 |
| 55425. | 180.36 | 1.2019 | 1.2470 | 1.2512 | 1.2890 | 1.3973 | 1.4438 | 1.4928 | 1.5437 | 1.6299 | 1.6844 | 1.7047 |
| 55431. | 180.34 | 1.2037 | 1.2465 | 1.2536 | 1.2904 | 1.3973 | 1.4438 | 1.4933 | 1.5444 | 1.6310 | 1.6850 | 1.7049 |
| 55438. | 180.32 | 1.2037 | 1.2468 | 1.2534 | 1.2900 | 1.4064 | 1.4448 | 1.4947 | 1.5456 | 1.6329 | 1.6865 | 1.7088 |
| 55444. | 180.30 | 1.2030 | 1.2479 | 1.2525 | 1.2907 | 1.3978 | 1.4466 | 1.4963 | 1.5468 | 1.6323 | 1.6871 | 1.7079 |
| 55450. | 180.28 | 1.2026 | 1.2481 | 1.2523 | 1.2935 | 1.4003 | 1.4473 | 1.4971 | 1.5478 | 1.6299 | 1.6868 | 1.7079 |
| 55456. | 180.26 | 1.2028 | 1.2475 | 1.2527 | 1.2946 | 1.3993 | 1.4463 | 1.4958 | 1.5497 | 1.6299 | 1.6871 | 1.7096 |
| 55462. | 180.24 | 1.2030 | 1.2481 | 1.2532 | 1.2932 | 1.3998 | 1.4440 | 1.4939 | 1.5490 | 1.6304 | 1.6876 | 1.7093 |
| 55468. | 180.22 | 1.2014 | 1.2491 | 1.2536 | 1.2918 | 1.3993 | 1.4430 | 1.4933 | 1.5466 | 1.6310 | 1.6873 | 1.7082 |
| 55474. | 180.20 | 1.1992 | 1.2488 | 1.2548 | 1.2923 | 1.3947 | 1.4443 | 1.4936 | 1.5456 | 1.6315 | 1.6868 | 1.7074 |
| 55481. | 180.18 | 1.1983 | 1.2477 | 1.2561 | 1.2935 | 1.3942 | 1.4453 | 1.4941 | 1.5459 | 1.6307 | 1.6858 | 1.7055 |
| 55487. | 180.16 | 1.1980 | 1.2465 | 1.2568 | 1.2939 | 1.3927 | 1.4435 | 1.4928 | 1.5456 | 1.6286 | 1.6839 | 1.7044 |
| 55493. | 180.14 | 1.1976 | 1.2447 | 1.2552 | 1.2941 | 1.3927 | 1.4405 | 1.4906 | 1.5454 | 1.6272 | 1.6826 | 1.7047 |
| 55499. | 180.12 | 1.1964 | 1.2426 | 1.2521 | 1.2938 | 1.3932 | 1.4392 | 1.4890 | 1.5442 | 1.6262 | 1.6818 | 1.7047 |
| 55505. | 180.10 | 1.1951 | 1.2414 | 1.2505 | 1.2927 | 1.3897 | 1.4375 | 1.4877 | 1.5398 | 1.6237 | 1.6787 | 1.7033 |
| 55511. | 180.08 | 1.1949 | 1.2405 | 1.2498 | 1.2918 | 1.3866 | 1.4342 | 1.4853 | 1.5365 | 1.6219 | 1.6753 | 1.7011 |
| 55518. | 180.06 | 1.1953 | 1.2384 | 1.2471 | 1.2897 | 1.3887 | 1.4339 | 1.4831 | 1.5365 | 1.6213 | 1.6745 | 1.6992 |
| 55524. | 180.04 | 1.1964 | 1.2382 | 1.2442 | 1.2877 | 1.3897 | 1.4352 | 1.4823 | 1.5365 | 1.6213 | 1.6737 | 1.6986 |
| 55530. | 180.02 | 1.1989 | 1.2410 | 1.2433 | 1.2870 | 1.3927 | 1.4377 | 1.4839 | 1.5353 | 1.6205 | 1.6739 | 1.6975 |
| 55536. | 180.00 | 1.2030 | 1.2461 | 1.2437 | 1.2859 | 1.3917 | 1.4413 | 1.4871 | 1.5343 | 1.6211 | 1.6758 | 1.6964 |

| WAVENUMBER CM-1 | WAVELENGTH NM | CROSS SECTION X E19 | | | CM-2, TEMPERATURE DEG. K | | | | | | | | | |
|--------------------|------------------|---------------------|--------|--------|--------------------------|--------|--------|--------|--------|--------|--------|--------|--|--|
| | | 151. | 182. | 196. | 223. | 247. | 268. | 301. | 333. | 372. | 423. | 485. | | |
| 55536. | 179.00 | 1.2030 | 1.2461 | 1.2437 | 1.2859 | 1.3917 | 1.4413 | 1.4871 | 1.5343 | 1.6211 | 1.6758 | 1.6964 | | |
| 55542. | 179.98 | 1.2071 | 1.2500 | 1.2453 | 1.2845 | 1.3962 | 1.4448 | 1.4906 | 1.5350 | 1.6229 | 1.6766 | 1.6970 | | |
| 55548. | 179.96 | 1.2096 | 1.2521 | 1.2482 | 1.2850 | 1.3973 | 1.4468 | 1.4920 | 1.5382 | 1.6245 | 1.6763 | 1.6962 | | |
| 55555. | 179.94 | 1.2108 | 1.2542 | 1.2518 | 1.2892 | 1.3988 | 1.4486 | 1.4920 | 1.5401 | 1.6240 | 1.6745 | 1.6945 | | |
| 55561. | 179.92 | 1.2117 | 1.2570 | 1.2561 | 1.2935 | 1.3988 | 1.4491 | 1.4925 | 1.5396 | 1.6219 | 1.6711 | 1.6934 | | |
| 55567. | 179.90 | 1.2126 | 1.2563 | 1.2593 | 1.2958 | 1.4028 | 1.4484 | 1.4941 | 1.5406 | 1.6197 | 1.6690 | 1.6910 | | |
| 55573. | 179.88 | 1.2119 | 1.2549 | 1.2609 | 1.2991 | 1.4028 | 1.4458 | 1.4941 | 1.5418 | 1.6165 | 1.6669 | 1.6855 | | |
| 55579. | 179.86 | 1.2094 | 1.2551 | 1.2624 | 1.3027 | 1.4008 | 1.4433 | 1.4920 | 1.5398 | 1.6117 | 1.6632 | 1.6773 | | |
| 55586. | 179.84 | 1.2067 | 1.2560 | 1.2631 | 1.3028 | 1.3988 | 1.4410 | 1.4882 | 1.5365 | 1.6063 | 1.6571 | 1.6685 | | |
| 55592. | 179.82 | 1.2039 | 1.2542 | 1.2615 | 1.3011 | 1.3947 | 1.4387 | 1.4831 | 1.5338 | 1.6001 | 1.6503 | 1.6608 | | |
| 55598. | 179.80 | 1.2014 | 1.2509 | 1.2595 | 1.2993 | 1.3912 | 1.4362 | 1.4791 | 1.5295 | 1.5963 | 1.6427 | 1.6554 | | |
| 55604. | 179.78 | 1.1996 | 1.2481 | 1.2581 | 1.2957 | 1.3881 | 1.4329 | 1.4742 | 1.5234 | 1.5923 | 1.6356 | 1.6491 | | |
| 55610. | 179.76 | 1.1974 | 1.2456 | 1.2563 | 1.2903 | 1.3846 | 1.4281 | 1.4694 | 1.5181 | 1.5872 | 1.6296 | 1.6420 | | |
| 55616. | 179.74 | 1.1946 | 1.2421 | 1.2532 | 1.2886 | 1.3836 | 1.4243 | 1.4664 | 1.5155 | 1.5819 | 1.6246 | 1.6354 | | |
| 55623. | 179.72 | 1.1924 | 1.2398 | 1.2494 | 1.2911 | 1.3816 | 1.4223 | 1.4640 | 1.5133 | 1.5767 | 1.6193 | 1.6302 | | |
| 55629. | 179.70 | 1.1901 | 1.2391 | 1.2473 | 1.2898 | 1.3785 | 1.4200 | 1.4594 | 1.5090 | 1.5733 | 1.6133 | 1.6274 | | |
| 55635. | 179.68 | 1.1896 | 1.2373 | 1.2451 | 1.2847 | 1.3750 | 1.4164 | 1.4546 | 1.5056 | 1.5700 | 1.6080 | 1.6247 | | |
| 55641. | 179.66 | 1.1912 | 1.2333 | 1.2428 | 1.2816 | 1.3679 | 1.4134 | 1.4513 | 1.5025 | 1.5660 | 1.6054 | 1.6214 | | |
| 55647. | 179.64 | 1.1908 | 1.2305 | 1.2401 | 1.2789 | 1.3659 | 1.4114 | 1.4492 | 1.4969 | 1.5625 | 1.6015 | 1.6179 | | |
| 55654. | 179.62 | 1.1883 | 1.2289 | 1.2390 | 1.2750 | 1.3654 | 1.4108 | 1.4484 | 1.4916 | 1.5606 | 1.5970 | 1.6135 | | |
| 55660. | 179.60 | 1.1865 | 1.2282 | 1.2385 | 1.2713 | 1.3633 | 1.4096 | 1.4473 | 1.4887 | 1.5580 | 1.5933 | 1.6099 | | |
| 55666. | 179.58 | 1.1867 | 1.2275 | 1.2370 | 1.2711 | 1.3623 | 1.4076 | 1.4443 | 1.4863 | 1.5545 | 1.5912 | 1.6083 | | |
| 55672. | 179.56 | 1.1883 | 1.2266 | 1.2365 | 1.2711 | 1.3618 | 1.4073 | 1.4419 | 1.4851 | 1.5531 | 1.5902 | 1.6069 | | |
| 55678. | 179.54 | 1.1890 | 1.2259 | 1.2358 | 1.2672 | 1.3649 | 1.4065 | 1.4406 | 1.4851 | 1.5537 | 1.5899 | 1.6066 | | |
| 55685. | 179.52 | 1.1883 | 1.2257 | 1.2338 | 1.2619 | 1.3674 | 1.4048 | 1.4416 | 1.4829 | 1.5545 | 1.5891 | 1.6069 | | |
| 55691. | 179.50 | 1.1880 | 1.2273 | 1.2329 | 1.2587 | 1.3633 | 1.4025 | 1.4425 | 1.4795 | 1.5537 | 1.5876 | 1.6058 | | |
| 55697. | 179.48 | 1.1880 | 1.2298 | 1.2340 | 1.2594 | 1.3608 | 1.4012 | 1.4419 | 1.4781 | 1.5520 | 1.5852 | 1.6055 | | |
| 55703. | 179.46 | 1.1878 | 1.2301 | 1.2345 | 1.2639 | 1.3613 | 1.4010 | 1.4411 | 1.4788 | 1.5507 | 1.5831 | 1.6064 | | |
| 55709. | 179.44 | 1.1871 | 1.2271 | 1.2340 | 1.2686 | 1.3628 | 1.4022 | 1.4406 | 1.4795 | 1.5499 | 1.5823 | 1.6055 | | |
| 55716. | 179.42 | 1.1865 | 1.2247 | 1.2324 | 1.2692 | 1.3649 | 1.4027 | 1.4406 | 1.4791 | 1.5499 | 1.5813 | 1.6044 | | |
| 55722. | 179.40 | 1.1858 | 1.2250 | 1.2315 | 1.2665 | 1.3633 | 1.4020 | 1.4408 | 1.4774 | 1.5507 | 1.5805 | 1.6039 | | |
| 55728. | 179.38 | 1.1862 | 1.2250 | 1.2313 | 1.2647 | 1.3583 | 1.4035 | 1.4390 | 1.4752 | 1.5488 | 1.5797 | 1.6022 | | |
| 55734. | 179.36 | 1.1880 | 1.2254 | 1.2322 | 1.2624 | 1.3568 | 1.4035 | 1.4344 | 1.4725 | 1.5475 | 1.5781 | 1.6011 | | |
| 55740. | 179.34 | 1.1892 | 1.2257 | 1.2320 | 1.2603 | 1.3618 | 1.4007 | 1.4314 | 1.4713 | 1.5483 | 1.5757 | 1.5995 | | |
| 55747. | 179.32 | 1.1890 | 1.2266 | 1.2313 | 1.2622 | 1.3588 | 1.3994 | 1.4309 | 1.4723 | 1.5483 | 1.5750 | 1.5979 | | |
| 55753. | 179.30 | 1.1885 | 1.2273 | 1.2309 | 1.2635 | 1.3598 | 1.4005 | 1.4314 | 1.4733 | 1.5475 | 1.5765 | 1.5984 | | |
| 55759. | 179.28 | 1.1880 | 1.2268 | 1.2318 | 1.2598 | 1.3618 | 1.4017 | 1.4325 | 1.4737 | 1.5483 | 1.5776 | 1.5992 | | |
| 55765. | 179.26 | 1.1876 | 1.2268 | 1.2329 | 1.2567 | 1.3573 | 1.4032 | 1.4336 | 1.4742 | 1.5496 | 1.5776 | 1.5970 | | |
| 55772. | 179.24 | 1.1887 | 1.2278 | 1.2347 | 1.2580 | 1.3608 | 1.4055 | 1.4336 | 1.4737 | 1.5488 | 1.5778 | 1.5949 | | |
| 55778. | 179.22 | 1.1901 | 1.2287 | 1.2354 | 1.2609 | 1.3613 | 1.4058 | 1.4328 | 1.4737 | 1.5472 | 1.5781 | 1.5949 | | |
| 55784. | 179.20 | 1.1896 | 1.2291 | 1.2336 | 1.2650 | 1.3618 | 1.4043 | 1.4314 | 1.4754 | 1.5472 | 1.5786 | 1.5973 | | |
| 55790. | 179.18 | 1.1890 | 1.2291 | 1.2324 | 1.2671 | 1.3618 | 1.4035 | 1.4320 | 1.4747 | 1.5486 | 1.5786 | 1.6003 | | |
| 55797. | 179.16 | 1.1894 | 1.2296 | 1.2331 | 1.2643 | 1.3633 | 1.4035 | 1.4325 | 1.4733 | 1.5494 | 1.5799 | 1.6028 | | |
| 55803. | 179.14 | 1.1896 | 1.2287 | 1.2338 | 1.2611 | 1.3613 | 1.4043 | 1.4328 | 1.4733 | 1.5496 | 1.5802 | 1.6039 | | |
| 55809. | 179.12 | 1.1887 | 1.2280 | 1.2340 | 1.2599 | 1.3649 | 1.4050 | 1.4344 | 1.4740 | 1.5510 | 1.5789 | 1.6039 | | |
| 55815. | 179.10 | 1.1876 | 1.2287 | 1.2345 | 1.2597 | 1.3603 | 1.4068 | 1.4371 | 1.4747 | 1.5520 | 1.5799 | 1.6033 | | |
| 55821. | 179.08 | 1.1871 | 1.2291 | 1.2343 | 1.2609 | 1.3603 | 1.4086 | 1.4381 | 1.4745 | 1.5518 | 1.5834 | 1.6039 | | |
| 55828. | 179.06 | 1.1865 | 1.2278 | 1.2347 | 1.2627 | 1.3654 | 1.4086 | 1.4379 | 1.4752 | 1.5529 | 1.5860 | 1.6064 | | |
| 55834. | 179.04 | 1.1858 | 1.2259 | 1.2347 | 1.2657 | 1.3639 | 1.4070 | 1.4379 | 1.4771 | 1.5553 | 1.5873 | 1.6102 | | |
| 55840. | 179.02 | 1.1846 | 1.2257 | 1.2340 | 1.2673 | 1.3639 | 1.4070 | 1.4373 | 1.4795 | 1.5580 | 1.5894 | 1.6154 | | |
| 55846. | 179.00 | 1.1846 | 1.2280 | 1.2345 | 1.2658 | 1.3623 | 1.4078 | 1.4371 | 1.4793 | 1.5588 | 1.5925 | 1.6209 | | |

| WAVENUMBER CM-1 | WAVELENGTH NM | CROSS SECTION X E19 | | | CM-2, TEMPERATURE DEG. K | | | | | | | |
|--------------------|------------------|---------------------|--------|--------|--------------------------|--------|--------|--------|--------|--------|--------|--------|
| | | 151. | 182. | 196. | 223. | 247. | 268. | 301. | 333. | 372. | 423. | 485. |
| 55846. | 179.00 | 1.1846 | 1.2280 | 1.2345 | 1.2658 | 1.3623 | 1.4078 | 1.4371 | 1.4793 | 1.5588 | 1.5925 | 1.6209 |
| 55853. | 178.98 | 1.1862 | 1.2294 | 1.2352 | 1.2637 | 1.3639 | 1.4083 | 1.4387 | 1.4783 | 1.5614 | 1.5960 | 1.6231 |
| 55859. | 178.96 | 1.1867 | 1.2284 | 1.2349 | 1.2634 | 1.3633 | 1.4098 | 1.4406 | 1.4807 | 1.5647 | 1.5975 | 1.6233 |
| 55865. | 178.94 | 1.1865 | 1.2271 | 1.2347 | 1.2634 | 1.3608 | 1.4111 | 1.4419 | 1.4836 | 1.5676 | 1.5994 | 1.6258 |
| 55871. | 178.92 | 1.1860 | 1.2278 | 1.2367 | 1.2633 | 1.3633 | 1.4124 | 1.4430 | 1.4861 | 1.5698 | 1.6029 | 1.6291 |
| 55878. | 178.90 | 1.1858 | 1.2282 | 1.2383 | 1.2628 | 1.3649 | 1.4139 | 1.4438 | 1.4877 | 1.5727 | 1.6075 | 1.6324 |
| 55884. | 178.88 | 1.1858 | 1.2280 | 1.2381 | 1.2611 | 1.3633 | 1.4152 | 1.4465 | 1.4894 | 1.5754 | 1.6101 | 1.6357 |
| 55890. | 178.86 | 1.1860 | 1.2280 | 1.2356 | 1.2608 | 1.3649 | 1.4157 | 1.4489 | 1.4918 | 1.5773 | 1.6120 | 1.6403 |
| 55896. | 178.84 | 1.1860 | 1.2287 | 1.2345 | 1.2639 | 1.3679 | 1.4152 | 1.4481 | 1.4930 | 1.5792 | 1.6141 | 1.6455 |
| 55903. | 178.82 | 1.1855 | 1.2280 | 1.2363 | 1.2673 | 1.3714 | 1.4136 | 1.4473 | 1.4945 | 1.5813 | 1.6162 | 1.6491 |
| 55909. | 178.80 | 1.1835 | 1.2261 | 1.2365 | 1.2693 | 1.3664 | 1.4131 | 1.4470 | 1.4974 | 1.5813 | 1.6170 | 1.6510 |
| 55915. | 178.78 | 1.1810 | 1.2266 | 1.2340 | 1.2698 | 1.3628 | 1.4144 | 1.4473 | 1.4971 | 1.5802 | 1.6196 | 1.6535 |
| 55921. | 178.76 | 1.1796 | 1.2282 | 1.2331 | 1.2677 | 1.3674 | 1.4159 | 1.4481 | 1.4959 | 1.5824 | 1.6235 | 1.6584 |
| 55928. | 178.74 | 1.1794 | 1.2275 | 1.2331 | 1.2639 | 1.3659 | 1.4167 | 1.4492 | 1.4998 | 1.5859 | 1.6264 | 1.6625 |
| 55934. | 178.72 | 1.1796 | 1.2245 | 1.2324 | 1.2620 | 1.3628 | 1.4162 | 1.4511 | 1.5029 | 1.5880 | 1.6288 | 1.6636 |
| 55940. | 178.70 | 1.1787 | 1.2227 | 1.2327 | 1.2624 | 1.3709 | 1.4184 | 1.4538 | 1.5020 | 1.5910 | 1.6306 | 1.6647 |
| 55946. | 178.68 | 1.1787 | 1.2217 | 1.2322 | 1.2633 | 1.3720 | 1.4220 | 1.4570 | 1.5032 | 1.5947 | 1.6325 | 1.6650 |
| 55953. | 178.66 | 1.1805 | 1.2224 | 1.2315 | 1.2656 | 1.3674 | 1.4248 | 1.4589 | 1.5061 | 1.5963 | 1.6335 | 1.6614 |
| 55959. | 178.64 | 1.1821 | 1.2243 | 1.2338 | 1.2695 | 1.3755 | 1.4263 | 1.4613 | 1.5073 | 1.5963 | 1.6346 | 1.6581 |
| 55965. | 178.62 | 1.1830 | 1.2245 | 1.2352 | 1.2726 | 1.3725 | 1.4291 | 1.4632 | 1.5092 | 1.5985 | 1.6361 | 1.6576 |
| 55971. | 178.60 | 1.1844 | 1.2261 | 1.2338 | 1.2738 | 1.3735 | 1.4306 | 1.4621 | 1.5116 | 1.6001 | 1.6359 | 1.6570 |
| 55978. | 178.58 | 1.1867 | 1.2303 | 1.2333 | 1.2728 | 1.3785 | 1.4286 | 1.4618 | 1.5123 | 1.5996 | 1.6335 | 1.6537 |
| 55984. | 178.56 | 1.1883 | 1.2312 | 1.2358 | 1.2709 | 1.3775 | 1.4276 | 1.4635 | 1.5140 | 1.5969 | 1.6304 | 1.6485 |
| 55990. | 178.54 | 1.1878 | 1.2308 | 1.2390 | 1.2706 | 1.3770 | 1.4273 | 1.4637 | 1.5155 | 1.5934 | 1.6272 | 1.6436 |
| 55997. | 178.52 | 1.1865 | 1.2298 | 1.2412 | 1.2728 | 1.3750 | 1.4261 | 1.4624 | 1.5145 | 1.5894 | 1.6248 | 1.6398 |
| 56003. | 178.50 | 1.1851 | 1.2289 | 1.2419 | 1.2751 | 1.3740 | 1.4261 | 1.4594 | 1.5111 | 1.5840 | 1.6196 | 1.6337 |
| 56009. | 178.48 | 1.1826 | 1.2296 | 1.2403 | 1.2749 | 1.3750 | 1.4243 | 1.4551 | 1.5046 | 1.5776 | 1.6125 | 1.6260 |
| 56015. | 178.46 | 1.1792 | 1.2291 | 1.2390 | 1.2721 | 1.3704 | 1.4195 | 1.4505 | 1.4998 | 1.5722 | 1.6052 | 1.6242 |
| 56022. | 178.44 | 1.1769 | 1.2261 | 1.2381 | 1.2716 | 1.3649 | 1.4154 | 1.4457 | 1.4964 | 1.5655 | 1.5981 | 1.6195 |
| 56028. | 178.42 | 1.1751 | 1.2217 | 1.2379 | 1.2732 | 1.3633 | 1.4096 | 1.4408 | 1.4911 | 1.5593 | 1.5920 | 1.6124 |
| 56034. | 178.40 | 1.1735 | 1.2176 | 1.2363 | 1.2721 | 1.3618 | 1.4030 | 1.4357 | 1.4851 | 1.5537 | 1.5847 | 1.6033 |
| 56040. | 178.38 | 1.1710 | 1.2136 | 1.2329 | 1.2676 | 1.3598 | 1.3984 | 1.4306 | 1.4807 | 1.5478 | 1.5768 | 1.5946 |
| 56047. | 178.36 | 1.1680 | 1.2097 | 1.2295 | 1.2634 | 1.3568 | 1.3944 | 1.4260 | 1.4762 | 1.5416 | 1.5705 | 1.5872 |
| 56053. | 178.34 | 1.1651 | 1.2074 | 1.2273 | 1.2607 | 1.3477 | 1.3918 | 1.4223 | 1.4718 | 1.5362 | 1.5645 | 1.5806 |
| 56059. | 178.32 | 1.1612 | 1.2057 | 1.2252 | 1.2579 | 1.3426 | 1.3903 | 1.4190 | 1.4680 | 1.5316 | 1.5587 | 1.5760 |
| 56066. | 178.30 | 1.1585 | 1.2041 | 1.2223 | 1.2543 | 1.3385 | 1.3878 | 1.4150 | 1.4631 | 1.5265 | 1.5526 | 1.5718 |
| 56072. | 178.28 | 1.1581 | 1.2030 | 1.2189 | 1.2500 | 1.3401 | 1.3840 | 1.4099 | 1.4585 | 1.5209 | 1.5469 | 1.5666 |
| 56078. | 178.26 | 1.1590 | 1.2032 | 1.2162 | 1.2464 | 1.3380 | 1.3809 | 1.4061 | 1.4542 | 1.5163 | 1.5411 | 1.5601 |
| 56084. | 178.24 | 1.1585 | 1.2025 | 1.2146 | 1.2439 | 1.3330 | 1.3784 | 1.4048 | 1.4487 | 1.5115 | 1.5361 | 1.5540 |
| 56091. | 178.22 | 1.1569 | 1.2016 | 1.2119 | 1.2416 | 1.3315 | 1.3764 | 1.4032 | 1.4431 | 1.5077 | 1.5319 | 1.5486 |
| 56097. | 178.20 | 1.1567 | 1.2009 | 1.2097 | 1.2390 | 1.3284 | 1.3743 | 1.3988 | 1.4409 | 1.5053 | 1.5282 | 1.5450 |
| 56103. | 178.18 | 1.1569 | 1.1992 | 1.2083 | 1.2374 | 1.3284 | 1.3721 | 1.3948 | 1.4395 | 1.5026 | 1.5235 | 1.5404 |
| 56110. | 178.16 | 1.1558 | 1.1974 | 1.2061 | 1.2370 | 1.3274 | 1.3698 | 1.3929 | 1.4354 | 1.4981 | 1.5190 | 1.5346 |
| 56116. | 178.14 | 1.1540 | 1.1969 | 1.2061 | 1.2336 | 1.3208 | 1.3690 | 1.3910 | 1.4301 | 1.4924 | 1.5146 | 1.5300 |
| 56122. | 178.12 | 1.1517 | 1.1979 | 1.2067 | 1.2304 | 1.3218 | 1.3685 | 1.3900 | 1.4285 | 1.4881 | 1.5109 | 1.5269 |
| 56129. | 178.10 | 1.1508 | 1.1972 | 1.2054 | 1.2309 | 1.3229 | 1.3672 | 1.3902 | 1.4250 | 1.4855 | 1.5077 | 1.5245 |
| 56135. | 178.08 | 1.1508 | 1.1930 | 1.2038 | 1.2297 | 1.3218 | 1.3650 | 1.3889 | 1.4241 | 1.4847 | 1.5043 | 1.5204 |
| 56141. | 178.06 | 1.1501 | 1.1909 | 1.2034 | 1.2262 | 1.3148 | 1.3632 | 1.3848 | 1.4202 | 1.4852 | 1.5007 | 1.5163 |
| 56148. | 178.04 | 1.1487 | 1.1918 | 1.2022 | 1.2230 | 1.3163 | 1.3612 | 1.3805 | 1.4156 | 1.4841 | 1.4962 | 1.5138 |
| 56154. | 178.02 | 1.1467 | 1.1914 | 1.2007 | 1.2204 | 1.3183 | 1.3576 | 1.3776 | 1.4146 | 1.4809 | 1.4920 | 1.5124 |
| 56160. | 178.00 | 1.1453 | 1.1893 | 1.1995 | 1.2203 | 1.3112 | 1.3556 | 1.3765 | 1.4127 | 1.4785 | 1.4894 | 1.5113 |

| WAVENUMBER CM-1 | WAVELENGTH NM | CROSS SECTION X E19 | | | CM-2, TEMPERATURE DEG. K | | | 301. | 333. | 372. | 423. | 485. |
|--------------------|------------------|---------------------|--------|--------|--------------------------|--------|--------|--------|--------|--------|--------|--------|
| | | 151. | 182. | 196. | 223. | 247. | 268. | | | | | |
| 56160. | 178.00 | 1.1453 | 1.1893 | 1.1995 | 1.2203 | 1.3112 | 1.3556 | 1.3765 | 1.4127 | 1.4785 | 1.4894 | 1.5113 |
| 56166. | 177.98 | 1.1451 | 1.1884 | 1.1998 | 1.2217 | 1.3132 | 1.3558 | 1.3757 | 1.4081 | 1.4774 | 1.4883 | 1.5108 |
| 56173. | 177.96 | 1.1465 | 1.1877 | 1.1991 | 1.2228 | 1.3183 | 1.3553 | 1.3738 | 1.4069 | 1.4769 | 1.4886 | 1.5111 |
| 56179. | 177.94 | 1.1478 | 1.1860 | 1.1975 | 1.2221 | 1.3117 | 1.3556 | 1.3741 | 1.4084 | 1.4742 | 1.4883 | 1.5089 |
| 56185. | 177.92 | 1.1476 | 1.1844 | 1.1971 | 1.2196 | 1.3087 | 1.3563 | 1.3754 | 1.4072 | 1.4723 | 1.4870 | 1.5075 |
| 56192. | 177.90 | 1.1469 | 1.1846 | 1.1980 | 1.2190 | 1.3132 | 1.3551 | 1.3762 | 1.4052 | 1.4747 | 1.4873 | 1.5089 |
| 56198. | 177.88 | 1.1476 | 1.1853 | 1.1980 | 1.2193 | 1.3122 | 1.3546 | 1.3765 | 1.4067 | 1.4774 | 1.4875 | 1.5097 |
| 56204. | 177.86 | 1.1499 | 1.1872 | 1.1962 | 1.2211 | 1.3107 | 1.3566 | 1.3746 | 1.4064 | 1.4779 | 1.4867 | 1.5130 |
| 56211. | 177.84 | 1.1506 | 1.1872 | 1.1941 | 1.2237 | 1.3148 | 1.3584 | 1.3725 | 1.4043 | 1.4809 | 1.4865 | 1.5184 |
| 56217. | 177.82 | 1.1506 | 1.1856 | 1.1948 | 1.2215 | 1.3122 | 1.3622 | 1.3738 | 1.4057 | 1.4844 | 1.4901 | 1.5228 |
| 56223. | 177.80 | 1.1512 | 1.1872 | 1.1966 | 1.2177 | 1.3132 | 1.3645 | 1.3792 | 1.4074 | 1.4868 | 1.4951 | 1.5253 |
| 56230. | 177.78 | 1.1519 | 1.1900 | 1.1962 | 1.2189 | 1.3137 | 1.3665 | 1.3857 | 1.4110 | 1.4892 | 1.5007 | 1.5291 |
| 56236. | 177.76 | 1.1517 | 1.1907 | 1.1957 | 1.2206 | 1.3148 | 1.3721 | 1.3883 | 1.4151 | 1.4914 | 1.5056 | 1.5327 |
| 56242. | 177.74 | 1.1508 | 1.1911 | 1.1975 | 1.2215 | 1.3198 | 1.3738 | 1.3881 | 1.4178 | 1.4946 | 1.5096 | 1.5379 |
| 56249. | 177.72 | 1.1503 | 1.1918 | 1.2002 | 1.2252 | 1.3158 | 1.3708 | 1.3908 | 1.4212 | 1.4973 | 1.5138 | 1.5428 |
| 56255. | 177.70 | 1.1512 | 1.1916 | 1.2013 | 1.2265 | 1.3183 | 1.3683 | 1.3937 | 1.4226 | 1.4965 | 1.5177 | 1.5431 |
| 56261. | 177.68 | 1.1517 | 1.1916 | 1.2016 | 1.2222 | 1.3173 | 1.3678 | 1.3927 | 1.4212 | 1.4962 | 1.5193 | 1.5417 |
| 56268. | 177.66 | 1.1515 | 1.1918 | 1.2011 | 1.2219 | 1.3168 | 1.3670 | 1.3881 | 1.4204 | 1.4989 | 1.5169 | 1.5428 |
| 56274. | 177.64 | 1.1517 | 1.1900 | 1.2002 | 1.2288 | 1.3168 | 1.3680 | 1.3827 | 1.4190 | 1.5034 | 1.5156 | 1.5469 |
| 56280. | 177.62 | 1.1528 | 1.1877 | 1.2000 | 1.2329 | 1.3224 | 1.3693 | 1.3803 | 1.4199 | 1.5077 | 1.5172 | 1.5543 |
| 56287. | 177.60 | 1.1524 | 1.1860 | 1.2004 | 1.2324 | 1.3249 | 1.3683 | 1.3843 | 1.4245 | 1.5139 | 1.5211 | 1.5639 |
| 56293. | 177.58 | 1.1510 | 1.1870 | 1.1986 | 1.2317 | 1.3254 | 1.3713 | 1.3913 | 1.4286 | 1.5217 | 1.5280 | 1.5724 |
| 56299. | 177.56 | 1.1499 | 1.1907 | 1.1975 | 1.2289 | 1.3249 | 1.3779 | 1.3975 | 1.4318 | 1.5276 | 1.5350 | 1.5798 |
| 56306. | 177.54 | 1.1492 | 1.1930 | 1.1986 | 1.2263 | 1.3274 | 1.3819 | 1.4034 | 1.4376 | 1.5333 | 1.5405 | 1.5872 |
| 56312. | 177.52 | 1.1474 | 1.1930 | 1.2000 | 1.2268 | 1.3289 | 1.3852 | 1.4102 | 1.4448 | 1.5381 | 1.5476 | 1.5938 |
| 56318. | 177.50 | 1.1458 | 1.1925 | 1.2009 | 1.2282 | 1.3330 | 1.3896 | 1.4153 | 1.4496 | 1.5437 | 1.5576 | 1.5987 |
| 56325. | 177.48 | 1.1462 | 1.1932 | 1.2018 | 1.2292 | 1.3350 | 1.3921 | 1.4182 | 1.4537 | 1.5507 | 1.5666 | 1.6036 |
| 56331. | 177.46 | 1.1474 | 1.1937 | 1.2034 | 1.2299 | 1.3355 | 1.3939 | 1.4201 | 1.4590 | 1.5561 | 1.5718 | 1.6080 |
| 56337. | 177.44 | 1.1476 | 1.1944 | 1.2052 | 1.2317 | 1.3365 | 1.3964 | 1.4233 | 1.4626 | 1.5588 | 1.5778 | 1.6124 |
| 56344. | 177.42 | 1.1462 | 1.1941 | 1.2072 | 1.2326 | 1.3385 | 1.3982 | 1.4268 | 1.4641 | 1.5598 | 1.5839 | 1.6151 |
| 56350. | 177.40 | 1.1465 | 1.1948 | 1.2095 | 1.2319 | 1.3385 | 1.3982 | 1.4267 | 1.4646 | 1.5596 | 1.5855 | 1.6154 |
| 56356. | 177.38 | 1.1474 | 1.1958 | 1.2086 | 1.2334 | 1.3380 | 1.3982 | 1.4277 | 1.4675 | 1.5596 | 1.5844 | 1.6135 |
| 56363. | 177.36 | 1.1465 | 1.1941 | 1.2077 | 1.2379 | 1.3370 | 1.3956 | 1.4244 | 1.4701 | 1.5582 | 1.5823 | 1.6116 |
| 56369. | 177.34 | 1.1449 | 1.1930 | 1.2083 | 1.2423 | 1.3380 | 1.3928 | 1.4225 | 1.4694 | 1.5550 | 1.5784 | 1.6105 |
| 56375. | 177.32 | 1.1446 | 1.1930 | 1.2077 | 1.2427 | 1.3406 | 1.3908 | 1.4215 | 1.4677 | 1.5515 | 1.5744 | 1.6080 |
| 56382. | 177.30 | 1.1444 | 1.1916 | 1.2058 | 1.2395 | 1.3355 | 1.3888 | 1.4196 | 1.4680 | 1.5475 | 1.5705 | 1.6017 |
| 56388. | 177.28 | 1.1428 | 1.1914 | 1.2047 | 1.2374 | 1.3310 | 1.3880 | 1.4185 | 1.4648 | 1.5435 | 1.5666 | 1.5962 |
| 56395. | 177.26 | 1.1417 | 1.1918 | 1.2043 | 1.2385 | 1.3320 | 1.3875 | 1.4180 | 1.4610 | 1.5418 | 1.5639 | 1.5935 |
| 56401. | 177.24 | 1.1419 | 1.1897 | 1.2038 | 1.2398 | 1.3340 | 1.3883 | 1.4163 | 1.4610 | 1.5397 | 1.5621 | 1.5905 |
| 56407. | 177.22 | 1.1428 | 1.1874 | 1.2040 | 1.2380 | 1.3289 | 1.3896 | 1.4145 | 1.4590 | 1.5367 | 1.5603 | 1.5864 |
| 56414. | 177.20 | 1.1417 | 1.1865 | 1.2025 | 1.2345 | 1.3284 | 1.3885 | 1.4142 | 1.4537 | 1.5338 | 1.5576 | 1.5833 |
| 56420. | 177.18 | 1.1399 | 1.1863 | 1.2004 | 1.2320 | 1.3274 | 1.3880 | 1.4126 | 1.4503 | 1.5306 | 1.5553 | 1.5828 |
| 56426. | 177.16 | 1.1394 | 1.1865 | 1.1998 | 1.2308 | 1.3284 | 1.3825 | 1.4099 | 1.4496 | 1.5287 | 1.5529 | 1.5806 |
| 56433. | 177.14 | 1.1401 | 1.1867 | 1.2004 | 1.2287 | 1.3274 | 1.3792 | 1.4088 | 1.4472 | 1.5265 | 1.5505 | 1.5762 |
| 56439. | 177.12 | 1.1410 | 1.1863 | 1.2009 | 1.2242 | 1.3254 | 1.3787 | 1.4085 | 1.4441 | 1.5236 | 1.5484 | 1.5713 |
| 56446. | 177.10 | 1.1410 | 1.1874 | 1.2016 | 1.2218 | 1.3254 | 1.3809 | 1.4091 | 1.4419 | 1.5214 | 1.5461 | 1.5688 |
| 56452. | 177.08 | 1.1399 | 1.1884 | 1.2022 | 1.2272 | 1.3218 | 1.3830 | 1.4077 | 1.4397 | 1.5193 | 1.5427 | 1.5669 |
| 56458. | 177.06 | 1.1392 | 1.1863 | 1.2018 | 1.2345 | 1.3218 | 1.3812 | 1.4053 | 1.4380 | 1.5179 | 1.5403 | 1.5642 |
| 56465. | 177.04 | 1.1394 | 1.1840 | 1.2007 | 1.2366 | 1.3229 | 1.3741 | 1.4061 | 1.4366 | 1.5196 | 1.5382 | 1.5645 |
| 56471. | 177.02 | 1.1406 | 1.1826 | 1.2000 | 1.2352 | 1.3198 | 1.3700 | 1.4075 | 1.4368 | 1.5182 | 1.5335 | 1.5650 |
| 56477. | 177.00 | 1.1406 | 1.1814 | 1.2000 | 1.2350 | 1.3163 | 1.3749 | 1.4058 | 1.4359 | 1.5131 | 1.5308 | 1.5628 |

| WAVENUMBER (CM-1) | WAVELENGTH NM | CROSS SECTION X E19 | | | TEMPERATURE DEG. K | | | | | | | | | |
|----------------------|------------------|---------------------|--------|--------|--------------------|--------|--------|--------|--------|--------|--------|--------|--|--|
| | | 151. | 182. | 196. | CM-2 223. | 247. | 268. | 301. | 333. | 372. | 423. | 485. | | |
| 56477. | 177.00 | 1.1406 | 1.1814 | 1.2000 | 1.2350 | 1.3163 | 1.3749 | 1.4058 | 1.4359 | 1.5131 | 1.5308 | 1.5628 | | |
| 56484. | 176.98 | 1.1408 | 1.1819 | 1.1993 | 1.2392 | 1.3168 | 1.3789 | 1.4023 | 1.4339 | 1.5091 | 1.5316 | 1.5598 | | |
| 56490. | 176.96 | 1.1428 | 1.1812 | 1.1968 | 1.2391 | 1.3173 | 1.3789 | 1.3988 | 1.4339 | 1.5067 | 1.5303 | 1.5573 | | |
| 56497. | 176.94 | 1.1460 | 1.1802 | 1.1944 | 1.2307 | 1.3163 | 1.3794 | 1.3962 | 1.4335 | 1.5040 | 1.5266 | 1.5543 | | |
| 56503. | 176.92 | 1.1474 | 1.1819 | 1.1953 | 1.2256 | 1.3168 | 1.3779 | 1.3953 | 1.4313 | 1.5026 | 1.5227 | 1.5494 | | |
| 56509. | 176.90 | 1.1469 | 1.1860 | 1.1971 | 1.2241 | 1.3188 | 1.3751 | 1.3951 | 1.4279 | 1.5005 | 1.5209 | 1.5412 | | |
| 56516. | 176.88 | 1.1469 | 1.1886 | 1.1966 | 1.2210 | 1.3183 | 1.3718 | 1.3951 | 1.4255 | 1.4975 | 1.5190 | 1.5335 | | |
| 56522. | 176.86 | 1.1469 | 1.1888 | 1.1964 | 1.2206 | 1.3143 | 1.3690 | 1.3927 | 1.4245 | 1.4932 | 1.5140 | 1.5280 | | |
| 56529. | 176.84 | 1.1469 | 1.1881 | 1.1984 | 1.2237 | 1.3132 | 1.3675 | 1.3862 | 1.4224 | 1.4871 | 1.5059 | 1.5220 | | |
| 56535. | 176.82 | 1.1462 | 1.1870 | 1.1998 | 1.2255 | 1.3127 | 1.3652 | 1.3800 | 1.4183 | 1.4804 | 1.4978 | 1.5157 | | |
| 56541. | 176.80 | 1.1444 | 1.1849 | 1.1991 | 1.2238 | 1.3107 | 1.3614 | 1.3762 | 1.4142 | 1.4747 | 1.4917 | 1.5100 | | |
| 56548. | 176.78 | 1.1426 | 1.1844 | 1.1989 | 1.2239 | 1.3107 | 1.3591 | 1.3722 | 1.4101 | 1.4699 | 1.4859 | 1.5050 | | |
| 56554. | 176.76 | 1.1408 | 1.1844 | 1.1993 | 1.2281 | 1.3092 | 1.3574 | 1.3679 | 1.4038 | 1.4669 | 1.4778 | 1.4985 | | |
| 56560. | 176.74 | 1.1390 | 1.1830 | 1.1982 | 1.2308 | 1.3067 | 1.3538 | 1.3638 | 1.3975 | 1.4637 | 1.4710 | 1.4913 | | |
| 56567. | 176.72 | 1.1369 | 1.1807 | 1.1955 | 1.2302 | 1.2981 | 1.3515 | 1.3590 | 1.3941 | 1.4583 | 1.4644 | 1.4853 | | |
| 56573. | 176.70 | 1.1340 | 1.1782 | 1.1941 | 1.2256 | 1.2950 | 1.3503 | 1.3539 | 1.3905 | 1.4522 | 1.4584 | 1.4793 | | |
| 56580. | 176.68 | 1.1315 | 1.1761 | 1.1932 | 1.2193 | 1.2950 | 1.3455 | 1.3507 | 1.3862 | 1.4481 | 1.4542 | 1.4738 | | |
| 56586. | 176.66 | 1.1312 | 1.1733 | 1.1905 | 1.2142 | 1.2935 | 1.3416 | 1.3488 | 1.3814 | 1.4455 | 1.4495 | 1.4686 | | |
| 56593. | 176.64 | 1.1294 | 1.1719 | 1.1894 | 1.2119 | 1.2905 | 1.3411 | 1.3474 | 1.3744 | 1.4420 | 1.4447 | 1.4642 | | |
| 56599. | 176.62 | 1.1265 | 1.1691 | 1.1885 | 1.2155 | 1.2834 | 1.3391 | 1.3458 | 1.3690 | 1.4401 | 1.4408 | 1.4626 | | |
| 56605. | 176.60 | 1.1249 | 1.1652 | 1.1849 | 1.2177 | 1.2844 | 1.3356 | 1.3437 | 1.3686 | 1.4377 | 1.4366 | 1.4590 | | |
| 56612. | 176.58 | 1.1235 | 1.1636 | 1.1799 | 1.2104 | 1.2803 | 1.3313 | 1.3404 | 1.3662 | 1.4334 | 1.4319 | 1.4538 | | |
| 56618. | 176.56 | 1.1206 | 1.1626 | 1.1761 | 1.2006 | 1.2753 | 1.3272 | 1.3377 | 1.3616 | 1.4288 | 1.4269 | 1.4483 | | |
| 56625. | 176.54 | 1.1174 | 1.1608 | 1.1750 | 1.1965 | 1.2738 | 1.3252 | 1.3350 | 1.3565 | 1.4248 | 1.4221 | 1.4448 | | |
| 56631. | 176.52 | 1.1149 | 1.1585 | 1.1741 | 1.1936 | 1.2753 | 1.3231 | 1.3313 | 1.3534 | 1.4213 | 1.4187 | 1.4456 | | |
| 56637. | 176.50 | 1.1128 | 1.1554 | 1.1727 | 1.1893 | 1.2692 | 1.3221 | 1.3275 | 1.3534 | 1.4197 | 1.4179 | 1.4462 | | |
| 56644. | 176.48 | 1.1099 | 1.1510 | 1.1700 | 1.1905 | 1.2672 | 1.3221 | 1.3237 | 1.3522 | 1.4181 | 1.4174 | 1.4426 | | |
| 56650. | 176.46 | 1.1078 | 1.1471 | 1.1666 | 1.1954 | 1.2667 | 1.3204 | 1.3208 | 1.3490 | 1.4159 | 1.4166 | 1.4396 | | |
| 56657. | 176.44 | 1.1074 | 1.1459 | 1.1637 | 1.1969 | 1.2631 | 1.3166 | 1.3192 | 1.3473 | 1.4124 | 1.4132 | 1.4390 | | |
| 56663. | 176.42 | 1.1058 | 1.1443 | 1.1614 | 1.1969 | 1.2662 | 1.3117 | 1.3157 | 1.3466 | 1.4092 | 1.4085 | 1.4385 | | |
| 56670. | 176.40 | 1.1026 | 1.1422 | 1.1578 | 1.1945 | 1.2667 | 1.3095 | 1.3130 | 1.3430 | 1.4073 | 1.4048 | 1.4382 | | |
| 56676. | 176.38 | 1.0999 | 1.1420 | 1.1538 | 1.1873 | 1.2636 | 1.3067 | 1.3127 | 1.3384 | 1.4060 | 1.4043 | 1.4382 | | |
| 56682. | 176.36 | 1.0999 | 1.1420 | 1.1526 | 1.1788 | 1.2596 | 1.3029 | 1.3116 | 1.3370 | 1.4052 | 1.4064 | 1.4349 | | |
| 56689. | 176.34 | 1.1006 | 1.1401 | 1.1535 | 1.1740 | 1.2591 | 1.3019 | 1.3095 | 1.3370 | 1.4033 | 1.4093 | 1.4316 | | |
| 56695. | 176.32 | 1.0999 | 1.1388 | 1.1533 | 1.1750 | 1.2555 | 1.3031 | 1.3068 | 1.3355 | 1.4003 | 1.4111 | 1.4297 | | |
| 56702. | 176.30 | 1.0965 | 1.1376 | 1.1524 | 1.1786 | 1.2550 | 1.3041 | 1.3052 | 1.3343 | 1.4012 | 1.4082 | 1.4303 | | |
| 56708. | 176.28 | 1.0956 | 1.1369 | 1.1522 | 1.1804 | 1.2581 | 1.3051 | 1.3060 | 1.3345 | 1.4033 | 1.4046 | 1.4333 | | |
| 56715. | 176.26 | 1.0969 | 1.1378 | 1.1531 | 1.1775 | 1.2576 | 1.3062 | 1.3065 | 1.3336 | 1.4025 | 1.4030 | 1.4363 | | |
| 56721. | 176.24 | 1.0978 | 1.1383 | 1.1538 | 1.1731 | 1.2611 | 1.3064 | 1.3068 | 1.3324 | 1.4014 | 1.4027 | 1.4377 | | |
| 56727. | 176.22 | 1.0974 | 1.1371 | 1.1535 | 1.1704 | 1.2591 | 1.3054 | 1.3052 | 1.3331 | 1.4017 | 1.4038 | 1.4390 | | |
| 56734. | 176.20 | 1.0978 | 1.1355 | 1.1506 | 1.1708 | 1.2545 | 1.3044 | 1.3041 | 1.3345 | 1.4036 | 1.4061 | 1.4404 | | |
| 56740. | 176.18 | 1.0990 | 1.1339 | 1.1475 | 1.1736 | 1.2576 | 1.3062 | 1.3060 | 1.3362 | 1.4065 | 1.4069 | 1.4420 | | |
| 56747. | 176.16 | 1.0994 | 1.1327 | 1.1454 | 1.1762 | 1.2581 | 1.3120 | 1.3079 | 1.3367 | 1.4076 | 1.4040 | 1.4459 | | |
| 56753. | 176.14 | 1.0985 | 1.1341 | 1.1443 | 1.1746 | 1.2571 | 1.3143 | 1.3081 | 1.3360 | 1.4073 | 1.4027 | 1.4483 | | |
| 56760. | 176.12 | 1.0974 | 1.1357 | 1.1441 | 1.1714 | 1.2550 | 1.3084 | 1.3089 | 1.3355 | 1.4076 | 1.4040 | 1.4486 | | |
| 56766. | 176.10 | 1.0972 | 1.1350 | 1.1441 | 1.1721 | 1.2586 | 1.3041 | 1.3108 | 1.3365 | 1.4103 | 1.4088 | 1.4486 | | |
| 56772. | 176.08 | 1.0976 | 1.1350 | 1.1466 | 1.1741 | 1.2621 | 1.3074 | 1.3130 | 1.3367 | 1.4135 | 1.4148 | 1.4514 | | |
| 56779. | 176.06 | 1.1008 | 1.1364 | 1.1493 | 1.1759 | 1.2631 | 1.3148 | 1.3149 | 1.3379 | 1.4159 | 1.4187 | 1.4552 | | |
| 56785. | 176.04 | 1.1063 | 1.1376 | 1.1506 | 1.1800 | 1.2616 | 1.3201 | 1.3167 | 1.3394 | 1.4213 | 1.4198 | 1.4593 | | |
| 56792. | 176.02 | 1.1074 | 1.1383 | 1.1533 | 1.1823 | 1.2611 | 1.3181 | 1.3178 | 1.3432 | 1.4264 | 1.4211 | 1.4634 | | |
| 56798. | 176.00 | 1.1063 | 1.1392 | 1.1578 | 1.1762 | 1.2652 | 1.3140 | 1.3197 | 1.3478 | 1.4275 | 1.4242 | 1.4675 | | |

| WAVENUMBER CM-1 | WAVELENGTH NM | CROSS SECTION X E19 | | | | | CM-2, TEMPERATURE DEG. K | | | | | |
|--------------------|------------------|---------------------|--------|--------|--------|--------|--------------------------|--------|--------|--------|--------|--------|
| | | 151. | 182. | 196. | 223. | 247. | 268. | 301. | 333. | 372. | 423. | 485. |
| 56798. | 176.00 | 1.1063 | 1.1392 | 1.1578 | 1.1762 | 1.2652 | 1.3140 | 1.3197 | 1.3478 | 1.4275 | 1.4242 | 1.4675 |
| 56805. | 175.98 | 1.1056 | 1.1404 | 1.1596 | 1.1662 | 1.2591 | 1.3158 | 1.3254 | 1.3505 | 1.4272 | 1.4300 | 1.4716 |
| 56811. | 175.96 | 1.1069 | 1.1418 | 1.1567 | 1.1662 | 1.2581 | 1.3206 | 1.3297 | 1.3517 | 1.4307 | 1.4363 | 1.4744 |
| 56818. | 175.94 | 1.1103 | 1.1429 | 1.1526 | 1.1757 | 1.2631 | 1.3216 | 1.3280 | 1.3548 | 1.4379 | 1.4382 | 1.4771 |
| 56824. | 175.92 | 1.1126 | 1.1457 | 1.1522 | 1.1846 | 1.2707 | 1.3221 | 1.3270 | 1.3582 | 1.4436 | 1.4366 | 1.4809 |
| 56831. | 175.90 | 1.1135 | 1.1476 | 1.1556 | 1.1908 | 1.2717 | 1.3231 | 1.3310 | 1.3608 | 1.4457 | 1.4382 | 1.4856 |
| 56837. | 175.88 | 1.1128 | 1.1478 | 1.1592 | 1.1931 | 1.2788 | 1.3239 | 1.3345 | 1.3623 | 1.4463 | 1.4434 | 1.4891 |
| 56844. | 175.86 | 1.1122 | 1.1487 | 1.1605 | 1.1937 | 1.2717 | 1.3254 | 1.3361 | 1.3630 | 1.4497 | 1.4476 | 1.4919 |
| 56850. | 175.84 | 1.1122 | 1.1503 | 1.1578 | 1.1960 | 1.2768 | 1.3285 | 1.3380 | 1.3630 | 1.4538 | 1.4495 | 1.4957 |
| 56856. | 175.82 | 1.1126 | 1.1517 | 1.1572 | 1.1957 | 1.2753 | 1.3330 | 1.3388 | 1.3645 | 1.4551 | 1.4526 | 1.4987 |
| 56863. | 175.80 | 1.1126 | 1.1515 | 1.1590 | 1.1928 | 1.2778 | 1.3358 | 1.3383 | 1.3681 | 1.4554 | 1.4589 | 1.5012 |
| 56869. | 175.78 | 1.1110 | 1.1492 | 1.1603 | 1.1893 | 1.2788 | 1.3356 | 1.3396 | 1.3703 | 1.4586 | 1.4615 | 1.5045 |
| 56876. | 175.76 | 1.1090 | 1.1455 | 1.1635 | 1.1857 | 1.2834 | 1.3368 | 1.3418 | 1.3712 | 1.4629 | 1.4607 | 1.5086 |
| 56882. | 175.74 | 1.1072 | 1.1432 | 1.1648 | 1.1840 | 1.2733 | 1.3394 | 1.3445 | 1.3729 | 1.4642 | 1.4621 | 1.5127 |
| 56889. | 175.72 | 1.1049 | 1.1429 | 1.1612 | 1.1844 | 1.2728 | 1.3386 | 1.3463 | 1.3744 | 1.4637 | 1.4628 | 1.5135 |
| 56895. | 175.70 | 1.1019 | 1.1434 | 1.1572 | 1.1820 | 1.2692 | 1.3338 | 1.3458 | 1.3748 | 1.4629 | 1.4644 | 1.5122 |
| 56902. | 175.68 | 1.0985 | 1.1425 | 1.1554 | 1.1768 | 1.2692 | 1.3285 | 1.3439 | 1.3760 | 1.4605 | 1.4694 | 1.5108 |
| 56908. | 175.66 | 1.0965 | 1.1404 | 1.1560 | 1.1770 | 1.2672 | 1.3262 | 1.3388 | 1.3789 | 1.4567 | 1.4699 | 1.5083 |
| 56915. | 175.64 | 1.0958 | 1.1385 | 1.1567 | 1.1832 | 1.2647 | 1.3229 | 1.3329 | 1.3789 | 1.4527 | 1.4626 | 1.5028 |
| 56921. | 175.62 | 1.0929 | 1.1369 | 1.1542 | 1.1920 | 1.2596 | 1.3178 | 1.3272 | 1.3753 | 1.4465 | 1.4552 | 1.4957 |
| 56928. | 175.60 | 1.0872 | 1.1344 | 1.1506 | 1.1975 | 1.2566 | 1.3188 | 1.3251 | 1.3705 | 1.4385 | 1.4510 | 1.4886 |
| 56934. | 175.58 | 1.0824 | 1.1320 | 1.1484 | 1.1938 | 1.2545 | 1.3226 | 1.3240 | 1.3647 | 1.4310 | 1.4460 | 1.4793 |
| 56941. | 175.56 | 1.0815 | 1.1297 | 1.1461 | 1.1890 | 1.2560 | 1.3196 | 1.3205 | 1.3563 | 1.4248 | 1.4395 | 1.4675 |
| 56947. | 175.54 | 1.0824 | 1.1258 | 1.1441 | 1.1892 | 1.2560 | 1.3140 | 1.3140 | 1.3488 | 1.4194 | 1.4316 | 1.4568 |
| 56954. | 175.52 | 1.0817 | 1.1242 | 1.1409 | 1.1875 | 1.2520 | 1.3100 | 1.3065 | 1.3425 | 1.4143 | 1.4235 | 1.4508 |
| 56960. | 175.50 | 1.0781 | 1.1242 | 1.1375 | 1.1846 | 1.2474 | 1.3057 | 1.3014 | 1.3382 | 1.4089 | 1.4135 | 1.4453 |
| 56967. | 175.48 | 1.0740 | 1.1204 | 1.1348 | 1.1826 | 1.2419 | 1.3024 | 1.2949 | 1.3360 | 1.4036 | 1.4059 | 1.4366 |
| 56973. | 175.46 | 1.0715 | 1.1144 | 1.1348 | 1.1820 | 1.2444 | 1.2981 | 1.2877 | 1.3304 | 1.3990 | 1.4019 | 1.4308 |
| 56980. | 175.44 | 1.0692 | 1.1119 | 1.1328 | 1.1806 | 1.2419 | 1.2955 | 1.2863 | 1.3237 | 1.3958 | 1.3980 | 1.4303 |
| 56986. | 175.42 | 1.0683 | 1.1130 | 1.1292 | 1.1714 | 1.2338 | 1.2932 | 1.2879 | 1.3198 | 1.3896 | 1.3920 | 1.4292 |
| 56993. | 175.40 | 1.0690 | 1.1121 | 1.1288 | 1.1575 | 1.2343 | 1.2877 | 1.2887 | 1.3155 | 1.3810 | 1.3880 | 1.4234 |
| 56999. | 175.38 | 1.0697 | 1.1065 | 1.1294 | 1.1522 | 1.2338 | 1.2811 | 1.2874 | 1.3124 | 1.3775 | 1.3843 | 1.4166 |
| 57006. | 175.36 | 1.0708 | 1.1021 | 1.1265 | 1.1592 | 1.2297 | 1.2783 | 1.2815 | 1.3090 | 1.3767 | 1.3788 | 1.4103 |
| 57012. | 175.34 | 1.0724 | 1.1003 | 1.1215 | 1.1637 | 1.2312 | 1.2788 | 1.2731 | 1.3039 | 1.3743 | 1.3725 | 1.4045 |
| 57019. | 175.32 | 1.0722 | 1.1001 | 1.1186 | 1.1593 | 1.2282 | 1.2783 | 1.2680 | 1.3001 | 1.3727 | 1.3670 | 1.4002 |
| 57025. | 175.30 | 1.0674 | 1.0996 | 1.1166 | 1.1602 | 1.2272 | 1.2770 | 1.2685 | 1.2993 | 1.3705 | 1.3628 | 1.3977 |
| 57032. | 175.28 | 1.0617 | 1.1003 | 1.1136 | 1.1639 | 1.2226 | 1.2780 | 1.2699 | 1.2964 | 1.3638 | 1.3623 | 1.3936 |
| 57038. | 175.26 | 1.0588 | 1.1005 | 1.1118 | 1.1617 | 1.2166 | 1.2757 | 1.2707 | 1.2892 | 1.3536 | 1.3628 | 1.3862 |
| 57045. | 175.24 | 1.0579 | 1.0998 | 1.1127 | 1.1577 | 1.2109 | 1.2681 | 1.2702 | 1.2853 | 1.3445 | 1.3570 | 1.3791 |
| 57051. | 175.22 | 1.0581 | 1.0980 | 1.1155 | 1.1558 | 1.2064 | 1.2643 | 1.2677 | 1.2841 | 1.3410 | 1.3471 | 1.3733 |
| 57058. | 175.20 | 1.0572 | 1.0938 | 1.1166 | 1.1532 | 1.2075 | 1.2656 | 1.2632 | 1.2791 | 1.3402 | 1.3421 | 1.3684 |
| 57064. | 175.18 | 1.0551 | 1.0880 | 1.1150 | 1.1498 | 1.2054 | 1.2636 | 1.2572 | 1.2740 | 1.3381 | 1.3384 | 1.3654 |
| 57071. | 175.16 | 1.0535 | 1.0827 | 1.1107 | 1.1477 | 1.2004 | 1.2567 | 1.2524 | 1.2728 | 1.3354 | 1.3334 | 1.3615 |
| 57077. | 175.14 | 1.0513 | 1.0808 | 1.1080 | 1.1445 | 1.2004 | 1.2486 | 1.2481 | 1.2728 | 1.3321 | 1.3276 | 1.3569 |
| 57084. | 175.12 | 1.0501 | 1.0836 | 1.1069 | 1.1448 | 1.2009 | 1.2433 | 1.2422 | 1.2706 | 1.3281 | 1.3192 | 1.3536 |
| 57090. | 175.10 | 1.0501 | 1.0861 | 1.1053 | 1.1442 | 1.1968 | 1.2418 | 1.2381 | 1.2660 | 1.3262 | 1.3142 | 1.3511 |
| 57097. | 175.08 | 1.0490 | 1.0873 | 1.1037 | 1.1373 | 1.1928 | 1.2430 | 1.2371 | 1.2605 | 1.3249 | 1.3137 | 1.3489 |
| 57103. | 175.06 | 1.0479 | 1.0878 | 1.1017 | 1.1341 | 1.1913 | 1.2441 | 1.2344 | 1.2547 | 1.3211 | 1.3108 | 1.3448 |
| 57110. | 175.04 | 1.0488 | 1.0861 | 1.0990 | 1.1350 | 1.1913 | 1.2448 | 1.2311 | 1.2506 | 1.3163 | 1.3066 | 1.3399 |
| 57116. | 175.02 | 1.0497 | 1.0841 | 1.0970 | 1.1460 | 1.1903 | 1.2418 | 1.2279 | 1.2508 | 1.3128 | 1.3037 | 1.3388 |
| 57123. | 175.00 | 1.0472 | 1.0852 | 1.0956 | 1.1466 | 1.1872 | 1.2362 | 1.2252 | 1.2504 | 1.3107 | 1.3006 | 1.3369 |

| WAVENUMBER CM-1 | WAVELENGTH NM | CROSS SECTION X E19 | | | CM-2 | | | TEMPERATURE DEG. K | | | | |
|--------------------|------------------|---------------------|--------|--------|--------|--------|--------|--------------------|--------|--------|--------|--------|
| | | 151. | 182. | 196. | 223. | 247. | 268. | 301. | 333. | 372. | 423. | 485. |
| 57123. | 175.00 | 1.0472 | 1.0852 | 1.0956 | 1.1466 | 1.1872 | 1.2362 | 1.2252 | 1.2504 | 1.3107 | 1.3004 | 1.3349 |
| 57129. | 174.98 | 1.0442 | 1.0857 | 1.0934 | 1.1370 | 1.1897 | 1.2319 | 1.2252 | 1.2475 | 1.3088 | 1.2964 | 1.3325 |
| 57136. | 174.96 | 1.0438 | 1.0834 | 1.0922 | 1.1272 | 1.1842 | 1.2294 | 1.2257 | 1.2436 | 1.3061 | 1.2922 | 1.3311 |
| 57142. | 174.94 | 1.0436 | 1.0808 | 1.0904 | 1.1199 | 1.1852 | 1.2319 | 1.2222 | 1.2412 | 1.3034 | 1.2898 | 1.3320 |
| 57149. | 174.92 | 1.0442 | 1.0790 | 1.0882 | 1.1145 | 1.1822 | 1.2334 | 1.2182 | 1.2414 | 1.3048 | 1.2885 | 1.3361 |
| 57156. | 174.90 | 1.0456 | 1.0771 | 1.0879 | 1.1157 | 1.1771 | 1.2294 | 1.2169 | 1.2414 | 1.3072 | 1.2869 | 1.3405 |
| 57162. | 174.88 | 1.0440 | 1.0760 | 1.0884 | 1.1152 | 1.1761 | 1.2296 | 1.2174 | 1.2388 | 1.3069 | 1.2861 | 1.3429 |
| 57169. | 174.86 | 1.0408 | 1.0755 | 1.0891 | 1.1139 | 1.1811 | 1.2321 | 1.2196 | 1.2368 | 1.3091 | 1.2882 | 1.3440 |
| 57175. | 174.84 | 1.0386 | 1.0757 | 1.0891 | 1.1161 | 1.1827 | 1.2281 | 1.2198 | 1.2412 | 1.3136 | 1.2911 | 1.3426 |
| 57182. | 174.82 | 1.0342 | 1.0748 | 1.0875 | 1.1201 | 1.1771 | 1.2240 | 1.2182 | 1.2453 | 1.3171 | 1.2935 | 1.3396 |
| 57188. | 174.80 | 1.0322 | 1.0711 | 1.0859 | 1.1227 | 1.1806 | 1.2268 | 1.2171 | 1.2436 | 1.3182 | 1.2964 | 1.3413 |
| 57195. | 174.78 | 1.0338 | 1.0660 | 1.0830 | 1.1189 | 1.1781 | 1.2289 | 1.2147 | 1.2407 | 1.3203 | 1.3019 | 1.3492 |
| 57201. | 174.76 | 1.0345 | 1.0637 | 1.0810 | 1.1139 | 1.1751 | 1.2294 | 1.2120 | 1.2419 | 1.3244 | 1.3069 | 1.3583 |
| 57208. | 174.74 | 1.0342 | 1.0655 | 1.0803 | 1.1115 | 1.1832 | 1.2301 | 1.2115 | 1.2463 | 1.3249 | 1.3095 | 1.3632 |
| 57214. | 174.72 | 1.0331 | 1.0653 | 1.0801 | 1.1078 | 1.1806 | 1.2268 | 1.2134 | 1.2494 | 1.3257 | 1.3137 | 1.3651 |
| 57221. | 174.70 | 1.0311 | 1.0627 | 1.0780 | 1.1030 | 1.1771 | 1.2212 | 1.2150 | 1.2516 | 1.3297 | 1.3184 | 1.3689 |
| 57228. | 174.68 | 1.0283 | 1.0625 | 1.0769 | 1.1001 | 1.1776 | 1.2192 | 1.2131 | 1.2549 | 1.3346 | 1.3253 | 1.3771 |
| 57234. | 174.66 | 1.0270 | 1.0639 | 1.0776 | 1.0994 | 1.1781 | 1.2200 | 1.2109 | 1.2574 | 1.3364 | 1.3323 | 1.3826 |
| 57241. | 174.64 | 1.0261 | 1.0653 | 1.0774 | 1.1011 | 1.1811 | 1.2197 | 1.2134 | 1.2578 | 1.3356 | 1.3339 | 1.3813 |
| 57247. | 174.62 | 1.0245 | 1.0627 | 1.0774 | 1.1057 | 1.1746 | 1.2210 | 1.2193 | 1.2561 | 1.3364 | 1.3342 | 1.3810 |
| 57254. | 174.60 | 1.0238 | 1.0590 | 1.0794 | 1.1118 | 1.1700 | 1.2271 | 1.2241 | 1.2532 | 1.3426 | 1.3355 | 1.3887 |
| 57260. | 174.58 | 1.0249 | 1.0588 | 1.0778 | 1.1161 | 1.1786 | 1.2337 | 1.2287 | 1.2545 | 1.3504 | 1.3373 | 1.3971 |
| 57267. | 174.56 | 1.0258 | 1.0618 | 1.0715 | 1.1143 | 1.1801 | 1.2352 | 1.2371 | 1.2612 | 1.3560 | 1.3400 | 1.4021 |
| 57273. | 174.54 | 1.0265 | 1.0641 | 1.0686 | 1.1096 | 1.1791 | 1.2344 | 1.2449 | 1.2687 | 1.3620 | 1.3452 | 1.4056 |
| 57280. | 174.52 | 1.0281 | 1.0658 | 1.0724 | 1.1088 | 1.1811 | 1.2357 | 1.2473 | 1.2730 | 1.3649 | 1.3547 | 1.4122 |
| 57287. | 174.50 | 1.0295 | 1.0662 | 1.0767 | 1.1088 | 1.1892 | 1.2372 | 1.2494 | 1.2742 | 1.3665 | 1.3628 | 1.4210 |
| 57293. | 174.48 | 1.0279 | 1.0639 | 1.0776 | 1.1016 | 1.1953 | 1.2377 | 1.2546 | 1.2757 | 1.3711 | 1.3681 | 1.4284 |
| 57300. | 174.46 | 1.0256 | 1.0627 | 1.0762 | 1.0932 | 1.1989 | 1.2390 | 1.2554 | 1.2805 | 1.3770 | 1.3709 | 1.4338 |
| 57306. | 174.44 | 1.0247 | 1.0639 | 1.0749 | 1.0961 | 1.1989 | 1.2433 | 1.2575 | 1.2870 | 1.3791 | 1.3741 | 1.4382 |
| 57313. | 174.42 | 1.0222 | 1.0632 | 1.0756 | 1.1052 | 1.1953 | 1.2491 | 1.2637 | 1.2926 | 1.3781 | 1.3791 | 1.4388 |
| 57319. | 174.40 | 1.0204 | 1.0618 | 1.0785 | 1.1147 | 1.1842 | 1.2507 | 1.2688 | 1.2976 | 1.3765 | 1.3846 | 1.4363 |
| 57326. | 174.38 | 1.0217 | 1.0627 | 1.0798 | 1.1262 | 1.1897 | 1.2504 | 1.2710 | 1.3013 | 1.3767 | 1.3885 | 1.4325 |
| 57333. | 174.36 | 1.0254 | 1.0653 | 1.0792 | 1.1303 | 1.2019 | 1.2512 | 1.2707 | 1.3029 | 1.3767 | 1.3917 | 1.4311 |
| 57339. | 174.34 | 1.0274 | 1.0683 | 1.0807 | 1.1225 | 1.2039 | 1.2484 | 1.2691 | 1.3005 | 1.3762 | 1.3935 | 1.4316 |
| 57346. | 174.32 | 1.0272 | 1.0697 | 1.0814 | 1.1132 | 1.1973 | 1.2430 | 1.2677 | 1.2974 | 1.3732 | 1.3912 | 1.4308 |
| 57352. | 174.30 | 1.0267 | 1.0690 | 1.0810 | 1.1118 | 1.1933 | 1.2441 | 1.2648 | 1.2964 | 1.3695 | 1.3859 | 1.4292 |
| 57359. | 174.28 | 1.0261 | 1.0690 | 1.0832 | 1.1172 | 1.1973 | 1.2456 | 1.2626 | 1.2955 | 1.3679 | 1.3822 | 1.4270 |
| 57365. | 174.26 | 1.0249 | 1.0692 | 1.0855 | 1.1190 | 1.1948 | 1.2441 | 1.2618 | 1.2943 | 1.3687 | 1.3772 | 1.4215 |
| 57372. | 174.24 | 1.0242 | 1.0683 | 1.0859 | 1.1139 | 1.2019 | 1.2517 | 1.2589 | 1.2940 | 1.3660 | 1.3715 | 1.4163 |
| 57379. | 174.22 | 1.0249 | 1.0662 | 1.0861 | 1.1107 | 1.1984 | 1.2565 | 1.2556 | 1.2921 | 1.3617 | 1.3715 | 1.4152 |
| 57385. | 174.20 | 1.0267 | 1.0637 | 1.0855 | 1.1153 | 1.1918 | 1.2453 | 1.2551 | 1.2875 | 1.3601 | 1.3746 | 1.4136 |
| 57392. | 174.18 | 1.0292 | 1.0614 | 1.0837 | 1.1236 | 1.1994 | 1.2392 | 1.2554 | 1.2863 | 1.3582 | 1.3733 | 1.4075 |
| 57398. | 174.16 | 1.0306 | 1.0609 | 1.0834 | 1.1288 | 1.1897 | 1.2385 | 1.2567 | 1.2865 | 1.3560 | 1.3686 | 1.4010 |
| 57405. | 174.14 | 1.0297 | 1.0625 | 1.0855 | 1.1310 | 1.1892 | 1.2367 | 1.2578 | 1.2836 | 1.3531 | 1.3657 | 1.3958 |
| 57412. | 174.12 | 1.0292 | 1.0639 | 1.0884 | 1.1284 | 1.1903 | 1.2337 | 1.2572 | 1.2824 | 1.3507 | 1.3662 | 1.3930 |
| 57418. | 174.10 | 1.0292 | 1.0646 | 1.0893 | 1.1279 | 1.1923 | 1.2278 | 1.2572 | 1.2836 | 1.3512 | 1.3662 | 1.3900 |
| 57425. | 174.08 | 1.0290 | 1.0669 | 1.0877 | 1.1378 | 1.1852 | 1.2299 | 1.2562 | 1.2846 | 1.3491 | 1.3633 | 1.3873 |
| 57431. | 174.06 | 1.0304 | 1.0720 | 1.0855 | 1.1431 | 1.1892 | 1.2304 | 1.2492 | 1.2836 | 1.3437 | 1.3562 | 1.3862 |
| 57438. | 174.04 | 1.0333 | 1.0743 | 1.0850 | 1.1547 | 1.1867 | 1.2223 | 1.2427 | 1.2827 | 1.3391 | 1.3463 | 1.3848 |
| 57445. | 174.02 | 1.0342 | 1.0715 | 1.0848 | 1.1771 | 1.1806 | 1.2190 | 1.2438 | 1.2810 | 1.3367 | 1.3379 | 1.3777 |
| 57451. | 174.00 | 1.0338 | 1.0681 | 1.0834 | 1.1736 | 1.1903 | 1.2212 | 1.2484 | 1.2764 | 1.3348 | 1.3350 | 1.3673 |

| WAVENUMBER CM-1 | WAVELENGTH NM | CROSS SECTION X E19 | | | CM-2 223. | TEMPERATURE DEG. K | | | 301. | 333. | 372. | 423. | 485. |
|--------------------|------------------|---------------------|--------|--------|--------------|--------------------|--------|--------|--------|--------|--------|--------|------|
| | | 151. | 182. | 196. | | 247. | 268. | | | | | | |
| 57451. | 174.00 | 1.0338 | 1.0681 | 1.0834 | 1.1736 | 1.1903 | 1.2212 | 1.2484 | 1.2764 | 1.3348 | 1.3350 | 1.3673 | |
| 57458. | 173.98 | 1.0317 | 1.0648 | 1.0832 | 1.1460 | 1.1908 | 1.2223 | 1.2478 | 1.2716 | 1.3316 | 1.3352 | 1.3563 | |
| 57464. | 173.96 | 1.0267 | 1.0602 | 1.0837 | 1.1300 | 1.1897 | 1.2190 | 1.2422 | 1.2692 | 1.3254 | 1.3318 | 1.3487 | |
| 57471. | 173.94 | 1.0233 | 1.0565 | 1.0819 | 1.1338 | 1.1822 | 1.2182 | 1.2397 | 1.2670 | 1.3163 | 1.3242 | 1.3492 | |
| 57478. | 173.92 | 1.0213 | 1.0558 | 1.0803 | 1.1395 | 1.1720 | 1.2220 | 1.2400 | 1.2646 | 1.3074 | 1.3184 | 1.3509 | |
| 57484. | 173.90 | 1.0177 | 1.0572 | 1.0828 | 1.1405 | 1.1710 | 1.2223 | 1.2371 | 1.2607 | 1.3050 | 1.3137 | 1.3476 | |
| 57491. | 173.88 | 1.0136 | 1.0579 | 1.0819 | 1.1390 | 1.1634 | 1.2101 | 1.2290 | 1.2532 | 1.3048 | 1.3077 | 1.3402 | |
| 57497. | 173.86 | 1.0122 | 1.0546 | 1.0769 | 1.1265 | 1.1558 | 1.1896 | 1.2139 | 1.2431 | 1.3002 | 1.2966 | 1.3295 | |
| 57504. | 173.84 | 1.0106 | 1.0465 | 1.0733 | 1.1120 | 1.1584 | 1.1799 | 1.2010 | 1.2366 | 1.2935 | 1.2846 | 1.3229 | |
| 57511. | 173.82 | 1.0052 | 1.0375 | 1.0697 | 1.1074 | 1.1584 | 1.1804 | 1.2012 | 1.2366 | 1.2868 | 1.2798 | 1.3188 | |
| 57517. | 173.80 | .9986 | 1.0345 | 1.0656 | 1.1130 | 1.1472 | 1.1774 | 1.2045 | 1.2354 | 1.2782 | 1.2783 | 1.3092 | |
| 57524. | 173.78 | .9927 | 1.0363 | 1.0632 | 1.1231 | 1.1361 | 1.1777 | 1.2015 | 1.2294 | 1.2701 | 1.2720 | 1.3005 | |
| 57531. | 173.76 | .9895 | 1.0375 | 1.0566 | 1.1281 | 1.1310 | 1.1860 | 1.1980 | 1.2233 | 1.2640 | 1.2641 | 1.2966 | |
| 57537. | 173.74 | .9911 | 1.0335 | 1.0517 | 1.1312 | 1.1280 | 1.1883 | 1.1934 | 1.2159 | 1.2621 | 1.2599 | 1.2898 | |
| 57544. | 173.72 | .9929 | 1.0284 | 1.0523 | 1.1364 | 1.1310 | 1.1827 | 1.1875 | 1.2079 | 1.2621 | 1.2596 | 1.2832 | |
| 57550. | 173.70 | .9924 | 1.0245 | 1.0501 | 1.1362 | 1.1290 | 1.1766 | 1.1854 | 1.2072 | 1.2575 | 1.2557 | 1.2829 | |
| 57557. | 173.68 | .9927 | 1.0231 | 1.0456 | 1.1229 | 1.1260 | 1.1685 | 1.1872 | 1.2072 | 1.2527 | 1.2441 | 1.2819 | |
| 57564. | 173.66 | .9922 | 1.0217 | 1.0435 | 1.1012 | 1.1204 | 1.1597 | 1.1891 | 1.2038 | 1.2529 | 1.2336 | 1.2769 | |
| 57570. | 173.64 | .9911 | 1.0178 | 1.0420 | 1.0958 | 1.1179 | 1.1495 | 1.1872 | 1.2014 | 1.2508 | 1.2305 | 1.2750 | |
| 57577. | 173.62 | .9868 | 1.0129 | 1.0393 | 1.1103 | 1.1245 | 1.1348 | 1.1741 | 1.2014 | 1.2457 | 1.2307 | 1.2747 | |
| 57584. | 173.60 | .9827 | 1.0141 | 1.0359 | 1.1079 | 1.1250 | 1.1277 | 1.1595 | 1.1992 | 1.2427 | 1.2300 | 1.2684 | |
| 57590. | 173.58 | .9820 | 1.0206 | 1.0343 | 1.0816 | 1.1234 | 1.1282 | 1.1630 | 1.1958 | 1.2417 | 1.2284 | 1.2602 | |
| 57597. | 173.56 | .9818 | 1.0240 | 1.0359 | 1.0643 | 1.1169 | 1.1224 | 1.1708 | 1.1917 | 1.2417 | 1.2255 | 1.2567 | |
| 57603. | 173.54 | .9815 | 1.0217 | 1.0390 | 1.0671 | 1.1088 | 1.1168 | 1.1633 | 1.1850 | 1.2430 | 1.2194 | 1.2567 | |
| 57610. | 173.52 | .9831 | 1.0210 | 1.0404 | 1.0775 | 1.1098 | 1.1191 | 1.1520 | 1.1826 | 1.2401 | 1.2158 | 1.2556 | |
| 57617. | 173.50 | .9824 | 1.0215 | 1.0381 | 1.0749 | 1.1088 | 1.1219 | 1.1455 | 1.1840 | 1.2355 | 1.2176 | 1.2498 | |
| 57623. | 173.48 | .9790 | 1.0199 | 1.0341 | 1.0602 | 1.1022 | 1.1237 | 1.1455 | 1.1830 | 1.2355 | 1.2173 | 1.2452 | |
| 57630. | 173.46 | .9774 | 1.0142 | 1.0291 | 1.0625 | 1.0900 | 1.1333 | 1.1471 | 1.1799 | 1.2374 | 1.2118 | 1.2482 | |
| 57637. | 173.44 | .9781 | 1.0143 | 1.0266 | 1.0707 | 1.1012 | 1.1483 | 1.1477 | 1.1773 | 1.2331 | 1.2053 | 1.2515 | |
| 57643. | 173.42 | .9747 | 1.0150 | 1.0266 | 1.0640 | 1.1072 | 1.1642 | 1.1506 | 1.1765 | 1.2277 | 1.2034 | 1.2506 | |
| 57650. | 173.40 | .9724 | 1.0136 | 1.0257 | 1.0670 | 1.0916 | 1.1736 | 1.1552 | 1.1758 | 1.2282 | 1.2029 | 1.2526 | |
| 57657. | 173.38 | .9745 | 1.0094 | 1.0246 | 1.0857 | 1.0951 | 1.1761 | 1.1571 | 1.1734 | 1.2288 | 1.2008 | 1.2564 | |
| 57663. | 173.36 | .9768 | 1.0076 | 1.0273 | 1.0873 | 1.1128 | 1.1723 | 1.1520 | 1.1712 | 1.2277 | 1.2021 | 1.2561 | |
| 57670. | 173.34 | .9784 | 1.0111 | 1.0300 | 1.0620 | 1.0997 | 1.1508 | 1.1444 | 1.1707 | 1.2307 | 1.2066 | 1.2528 | |
| 57677. | 173.32 | .9793 | 1.0148 | 1.0264 | 1.0503 | 1.0986 | 1.1265 | 1.1415 | 1.1727 | 1.2368 | 1.2071 | 1.2471 | |
| 57683. | 173.30 | .9784 | 1.0131 | 1.0221 | 1.0591 | 1.1078 | 1.1232 | 1.1434 | 1.1756 | 1.2355 | 1.2050 | 1.2476 | |
| 57690. | 173.28 | .9754 | 1.0085 | 1.0244 | 1.0586 | 1.1113 | 1.1348 | 1.1469 | 1.1780 | 1.2290 | 1.2084 | 1.2520 | |
| 57697. | 173.26 | .9706 | 1.0053 | 1.0255 | 1.0593 | 1.0971 | 1.1371 | 1.1506 | 1.1782 | 1.2290 | 1.2126 | 1.2468 | |
| 57703. | 173.24 | .9659 | .9999 | 1.0187 | 1.0718 | 1.0941 | 1.1310 | 1.1504 | 1.1768 | 1.2360 | 1.2113 | 1.2400 | |
| 57710. | 173.22 | .9656 | .9972 | 1.0147 | 1.0888 | 1.0941 | 1.1338 | 1.1407 | 1.1712 | 1.2384 | 1.2068 | 1.2400 | |
| 57717. | 173.20 | .9706 | .9988 | 1.0196 | 1.1087 | 1.0951 | 1.1376 | 1.1304 | 1.1662 | 1.2331 | 1.2053 | 1.2389 | |
| 57723. | 173.18 | .9763 | .9972 | 1.0237 | 1.1211 | 1.0941 | 1.1280 | 1.1286 | 1.1715 | 1.2296 | 1.2113 | 1.2386 | |
| 57730. | 173.16 | .9781 | .9960 | 1.0190 | 1.1078 | 1.0966 | 1.1161 | 1.1280 | 1.1802 | 1.2339 | 1.2184 | 1.2413 | |
| 57737. | 173.14 | .9777 | 1.0002 | 1.0118 | 1.0750 | 1.0809 | 1.1133 | 1.1307 | 1.1806 | 1.2390 | 1.2200 | 1.2435 | |
| 57743. | 173.12 | .9788 | 1.0046 | 1.0120 | 1.0470 | 1.0830 | 1.1259 | 1.1409 | 1.1780 | 1.2401 | 1.2200 | 1.2490 | |
| 57750. | 173.10 | .9804 | 1.0062 | 1.0174 | 1.0420 | 1.0956 | 1.1406 | 1.1469 | 1.1768 | 1.2398 | 1.2210 | 1.2547 | |
| 57757. | 173.08 | .9781 | 1.0057 | 1.0156 | 1.0557 | 1.1002 | 1.1346 | 1.1444 | 1.1787 | 1.2384 | 1.2160 | 1.2567 | |
| 57763. | 173.06 | .9734 | 1.0080 | 1.0106 | 1.0703 | 1.1017 | 1.1166 | 1.1501 | 1.1816 | 1.2384 | 1.2045 | 1.2610 | |
| 57770. | 173.04 | .9724 | 1.0090 | 1.0111 | 1.0814 | 1.1113 | 1.1041 | 1.1590 | 1.1845 | 1.2441 | 1.2042 | 1.2654 | |
| 57777. | 173.02 | .9745 | 1.0046 | 1.0140 | 1.0846 | 1.1002 | 1.1072 | 1.1582 | 1.1937 | 1.2462 | 1.2171 | 1.2635 | |
| 57783. | 173.00 | .9747 | 1.0004 | 1.0160 | 1.0742 | 1.0865 | 1.1138 | 1.1523 | 1.2009 | 1.2414 | 1.2213 | 1.2630 | |

| WAVENUMBER CM-1 | WAVELENGTH NM | CROSS SECTION X E19 | | | TEMPERATURE DEG. K | | | | | | | |
|--------------------|------------------|---------------------|--------|--------|--------------------|--------|--------|--------|--------|--------|--------|--------|
| | | 151. | 162. | 196. | CM-2 223. | 247. | 268. | 301. | 333. | 372. | 423. | 485. |
| 57783. | 173.00 | .9747 | 1.0004 | 1.0160 | 1.0742 | 1.0865 | 1.1138 | 1.1523 | 1.2009 | 1.2414 | 1.2213 | 1.2630 |
| 57790. | 172.98 | .9749 | .9985 | 1.0165 | 1.0787 | 1.0880 | 1.1133 | 1.1426 | 1.1999 | 1.2371 | 1.2184 | 1.2662 |
| 57797. | 172.96 | .9754 | 1.0013 | 1.0140 | 1.1035 | 1.0875 | 1.1178 | 1.1364 | 1.1995 | 1.2355 | 1.2210 | 1.2630 |
| 57803. | 172.94 | .9738 | 1.0034 | 1.0118 | 1.1020 | 1.0860 | 1.1226 | 1.1423 | 1.1956 | 1.2360 | 1.2278 | 1.2589 |
| 57810. | 172.92 | .9752 | 1.0062 | 1.0140 | 1.0853 | 1.1103 | 1.1143 | 1.1471 | 1.1917 | 1.2401 | 1.2357 | 1.2665 |
| 57817. | 172.90 | .9764 | 1.0134 | 1.0187 | 1.0797 | 1.0941 | 1.0945 | 1.1436 | 1.2033 | 1.2470 | 1.2457 | 1.2769 |
| 57823. | 172.88 | .9806 | 1.0150 | 1.0201 | 1.0756 | 1.0926 | 1.0925 | 1.1350 | 1.2188 | 1.2527 | 1.2515 | 1.2758 |
| 57830. | 172.86 | .9843 | 1.0080 | 1.0192 | 1.0779 | 1.1052 | 1.1054 | 1.1415 | 1.2173 | 1.2548 | 1.2468 | 1.2731 |
| 57837. | 172.84 | .9888 | 1.0013 | 1.0185 | 1.0955 | 1.1067 | 1.1097 | 1.1881 | 1.2064 | 1.2554 | 1.2441 | 1.2742 |
| 57843. | 172.82 | .9872 | 1.0011 | 1.0205 | 1.1211 | 1.1062 | 1.1115 | 1.2306 | 1.2021 | 1.2567 | 1.2520 | 1.2723 |
| 57850. | 172.80 | .9799 | 1.0064 | 1.0239 | 1.1371 | 1.1250 | 1.1110 | 1.2136 | 1.2043 | 1.2583 | 1.2588 | 1.2714 |
| 57857. | 172.78 | .9747 | 1.0092 | 1.0248 | 1.1224 | 1.1285 | 1.1112 | 1.1735 | 1.2036 | 1.2621 | 1.2515 | 1.2695 |
| 57864. | 172.76 | .9702 | 1.0078 | 1.0235 | 1.1105 | 1.1159 | 1.1171 | 1.1512 | 1.1987 | 1.2613 | 1.2405 | 1.2649 |
| 57870. | 172.74 | .9638 | 1.0029 | 1.0226 | 1.1307 | 1.1007 | 1.1171 | 1.1385 | 1.1975 | 1.2562 | 1.2428 | 1.2668 |
| 57877. | 172.72 | .9606 | .9983 | 1.0208 | 1.1385 | 1.0951 | 1.0955 | 1.1210 | 1.2021 | 1.2505 | 1.2491 | 1.2684 |
| 57884. | 172.70 | .9595 | .9921 | 1.0151 | 1.1458 | 1.0845 | 1.0649 | 1.1148 | 1.2016 | 1.2411 | 1.2531 | 1.2635 |
| 57890. | 172.68 | .9581 | .9802 | 1.0061 | 1.1652 | 1.0951 | 1.0527 | 1.1218 | 1.1903 | 1.2307 | 1.2531 | 1.2526 |
| 57897. | 172.66 | .9552 | .9742 | 1.0032 | 1.1507 | 1.0911 | 1.0436 | 1.1159 | 1.1809 | 1.2269 | 1.2431 | 1.2320 |
| 57904. | 172.64 | .9490 | .9779 | 1.0041 | 1.1124 | 1.0789 | 1.0228 | 1.1173 | 1.1867 | 1.2266 | 1.2281 | 1.2112 |
| 57910. | 172.62 | .9425 | .9793 | 1.0014 | 1.0864 | 1.0657 | 1.0276 | 1.1304 | 1.1876 | 1.2223 | 1.2160 | 1.2041 |
| 57917. | 172.60 | .9409 | .9749 | .9989 | 1.1031 | 1.0602 | 1.0755 | 1.1216 | 1.1676 | 1.2170 | 1.2071 | 1.2085 |
| 57924. | 172.58 | .9429 | .9682 | .9937 | 1.1561 | 1.0774 | 1.1201 | 1.1132 | 1.1577 | 1.2070 | 1.2076 | 1.2087 |
| 57931. | 172.56 | .9450 | .9591 | .9845 | 1.1722 | 1.0824 | 1.1318 | 1.1318 | 1.1681 | 1.1955 | 1.2116 | 1.2068 |
| 57937. | 172.54 | .9440 | .9561 | .9786 | 1.1318 | 1.0516 | 1.1199 | 1.1393 | 1.1693 | 1.1898 | 1.1977 | 1.2033 |
| 57944. | 172.52 | .9377 | .9584 | .9737 | 1.0873 | 1.0511 | 1.0907 | 1.1113 | 1.1599 | 1.1869 | 1.1777 | 1.1885 |
| 57951. | 172.50 | .9286 | .9531 | .9680 | 1.0815 | 1.0445 | 1.0766 | 1.0882 | 1.1534 | 1.1853 | 1.1772 | 1.1748 |
| 57957. | 172.48 | .9222 | .9450 | .9701 | 1.0907 | 1.0460 | 1.0915 | 1.0933 | 1.1541 | 1.1869 | 1.1835 | 1.1709 |
| 57964. | 172.46 | .9195 | .9443 | .9707 | 1.0679 | 1.0420 | 1.1034 | 1.0847 | 1.1577 | 1.1853 | 1.1879 | 1.1652 |
| 57971. | 172.44 | .9200 | .9473 | .9631 | 1.0634 | 1.0490 | 1.1001 | 1.0664 | 1.1493 | 1.1794 | 1.1900 | 1.1529 |
| 57978. | 172.42 | .9252 | .9510 | .9597 | 1.1202 | 1.0425 | 1.0806 | 1.0736 | 1.1324 | 1.1770 | 1.1745 | 1.1362 |
| 57984. | 172.40 | .9302 | .9584 | .9586 | 1.1744 | 1.0455 | 1.0471 | 1.0755 | 1.1264 | 1.1751 | 1.1493 | 1.1301 |
| 57991. | 172.38 | .9327 | .9652 | .9572 | 1.1724 | 1.0485 | 1.0377 | 1.0465 | 1.1348 | 1.1678 | 1.1362 | 1.1392 |
| 57998. | 172.36 | .9331 | .9635 | .9581 | 1.1349 | 1.0384 | 1.0654 | 1.0085 | 1.1457 | 1.1641 | 1.1360 | 1.1422 |
| 58005. | 172.34 | .9331 | .9622 | .9592 | 1.0941 | 1.0242 | 1.0613 | .9899 | 1.1459 | 1.1681 | 1.1425 | 1.1236 |
| 58011. | 172.32 | .9347 | .9649 | .9615 | 1.0522 | 1.0323 | 1.0023 | .9996 | 1.1437 | 1.1711 | 1.1512 | 1.1080 |
| 58018. | 172.30 | .9311 | .9603 | .9604 | 1.0348 | 1.0389 | .9607 | 1.0085 | 1.1454 | 1.1686 | 1.1517 | 1.1063 |
| 58025. | 172.28 | .9236 | .9517 | .9574 | 1.0728 | 1.0349 | .9906 | 1.0053 | 1.1430 | 1.1600 | 1.1520 | 1.1036 |
| 58031. | 172.26 | .9229 | .9478 | .9552 | 1.1093 | 1.0258 | 1.0507 | 1.0117 | 1.1379 | 1.1477 | 1.1567 | 1.0962 |
| 58038. | 172.24 | .9279 | .9429 | .9529 | 1.0870 | 1.0131 | 1.0649 | 1.0139 | 1.1394 | 1.1388 | 1.1449 | 1.0825 |
| 58045. | 172.22 | .9300 | .9360 | .9504 | 1.0936 | 1.0455 | 1.0367 | .9894 | 1.1396 | 1.1388 | 1.1262 | 1.0606 |
| 58052. | 172.20 | .9311 | .9415 | .9516 | 1.1320 | 1.0511 | 1.0091 | .9724 | 1.1317 | 1.1380 | 1.1241 | 1.0527 |
| 58058. | 172.18 | .9327 | .9550 | .9549 | 1.1140 | 1.0086 | .9972 | .9862 | 1.1237 | 1.1302 | 1.1247 | 1.0735 |
| 58065. | 172.16 | .9322 | .9547 | .9540 | 1.0889 | .9964 | 1.0093 | 1.0002 | 1.1218 | 1.1335 | 1.1173 | 1.0954 |
| 58072. | 172.14 | .9295 | .9503 | .9480 | 1.0883 | 1.0328 | 1.0157 | .9829 | 1.1319 | 1.1488 | 1.1136 | 1.0981 |
| 58079. | 172.12 | .9293 | .9547 | .9428 | 1.0608 | 1.0369 | .9878 | .9894 | 1.1348 | 1.1512 | 1.1186 | 1.0880 |
| 58085. | 172.10 | .9286 | .9508 | .9435 | 1.0015 | 1.0222 | .9609 | 1.0330 | 1.1206 | 1.1431 | 1.1226 | 1.0751 |
| 58092. | 172.08 | .9256 | .9422 | .9459 | .9702 | .9893 | .9584 | 1.0220 | 1.1155 | 1.1378 | 1.1194 | 1.0609 |
| 58099. | 172.06 | .9263 | .9501 | .9491 | 1.0041 | .9807 | .9642 | .9805 | 1.1273 | 1.1445 | 1.1231 | 1.0546 |
| 58106. | 172.04 | .9284 | .9566 | .9513 | 1.0581 | 1.0136 | .9521 | .9781 | 1.1432 | 1.1541 | 1.1318 | 1.0652 |
| 58112. | 172.02 | .9263 | .9478 | .9471 | 1.0726 | 1.0086 | .9371 | 1.0090 | 1.1440 | 1.1463 | 1.1283 | 1.0710 |

2. Cross Sections of First Order and Second Order Deconvolutions,
190-172 nm.

| WAVENUMBER CM-1 | WAVELENGTH NM | CROSS SECTION X E19, CM-2 | | | | |
|--------------------|------------------|---------------------------|----------------|-----------------------|----------------|----------------|
| | | FIRST ORDER (000) | ORDER (010) | SECOND ORDER (000) | ORDER (010) | ORDER (020) |
| 52619. | 189.98 | .8425 | 4.0464 | .8452 | 3.6497 | 2.8067 |
| 52624. | 189.96 | .8397 | 4.1100 | .8423 | 3.7366 | 2.6419 |
| 52630. | 189.94 | .8410 | 4.1298 | .8436 | 3.7562 | 2.6433 |
| 52635. | 189.92 | .8419 | 4.1564 | .8445 | 3.7877 | 2.6084 |
| 52641. | 189.90 | .8431 | 4.1793 | .8457 | 3.8153 | 2.5761 |
| 52646. | 189.88 | .8433 | 4.2051 | .8458 | 3.8483 | 2.5246 |
| 52652. | 189.86 | .8433 | 4.2290 | .8458 | 3.8802 | 2.4676 |
| 52658. | 189.84 | .8445 | 4.2359 | .8470 | 3.8862 | 2.4747 |
| 52663. | 189.82 | .8461 | 4.2386 | .8486 | 3.8878 | 2.4818 |
| 52669. | 189.80 | .8470 | 4.2420 | .8494 | 3.8949 | 2.4556 |
| 52674. | 189.78 | .8481 | 4.2385 | .8505 | 3.8929 | 2.4455 |
| 52680. | 189.76 | .8493 | 4.2327 | .8517 | 3.8906 | 2.4208 |
| 52685. | 189.74 | .8503 | 4.2260 | .8527 | 3.8887 | 2.3865 |
| 52691. | 189.72 | .8515 | 4.2170 | .8538 | 3.8826 | 2.3666 |
| 52696. | 189.70 | .8525 | 4.2086 | .8548 | 3.8779 | 2.3401 |
| 52702. | 189.68 | .8532 | 4.2102 | .8554 | 3.8896 | 2.2683 |
| 52707. | 189.66 | .8543 | 4.2060 | .8565 | 3.8900 | 2.2355 |
| 52713. | 189.64 | .8558 | 4.1894 | .8581 | 3.8662 | 2.2870 |
| 52719. | 189.62 | .8561 | 4.1818 | .8584 | 3.8554 | 2.3093 |
| 52724. | 189.60 | .8559 | 4.1815 | .8582 | 3.8546 | 2.3135 |
| 52730. | 189.58 | .8561 | 4.1818 | .8584 | 3.8563 | 2.3027 |
| 52735. | 189.56 | .8563 | 4.1867 | .8585 | 3.8694 | 2.2457 |
| 52741. | 189.54 | .8562 | 4.1939 | .8584 | 3.8850 | 2.1854 |
| 52746. | 189.52 | .8574 | 4.1881 | .8596 | 3.8796 | 2.1830 |
| 52752. | 189.50 | .8593 | 4.1776 | .8615 | 3.8635 | 2.2227 |
| 52758. | 189.48 | .8612 | 4.1710 | .8634 | 3.8551 | 2.2357 |
| 52763. | 189.46 | .8633 | 4.1727 | .8655 | 3.8608 | 2.2071 |
| 52769. | 189.44 | .8649 | 4.1666 | .8671 | 3.8518 | 2.2269 |
| 52774. | 189.42 | .8673 | 4.1542 | .8695 | 3.8337 | 2.2681 |
| 52780. | 189.40 | .8694 | 4.1535 | .8716 | 3.8369 | 2.2404 |
| 52785. | 189.38 | .8712 | 4.1549 | .8734 | 3.8439 | 2.2003 |
| 52791. | 189.36 | .8731 | 4.1483 | .8752 | 3.8373 | 2.2000 |
| 52797. | 189.34 | .8742 | 4.1472 | .8763 | 3.8419 | 2.1602 |
| 52802. | 189.32 | .8754 | 4.1462 | .8775 | 3.8472 | 2.1161 |
| 52808. | 189.30 | .8763 | 4.1441 | .8784 | 3.8489 | 2.0889 |
| 52813. | 189.28 | .8765 | 4.1388 | .8786 | 3.8437 | 2.0882 |
| 52819. | 189.26 | .8761 | 4.1327 | .8781 | 3.8391 | 2.0776 |
| 52824. | 189.24 | .8764 | 4.1267 | .8785 | 3.8336 | 2.0744 |
| 52830. | 189.22 | .8778 | 4.1164 | .8799 | 3.8230 | 2.0760 |
| 52836. | 189.20 | .8788 | 4.1048 | .8809 | 3.8110 | 2.0789 |
| 52841. | 189.18 | .8789 | 4.0985 | .8809 | 3.8046 | 2.0797 |
| 52847. | 189.16 | .8801 | 4.0905 | .8822 | 3.7949 | 2.0914 |
| 52852. | 189.14 | .8818 | 4.0876 | .8838 | 3.7943 | 2.0754 |
| 52858. | 189.12 | .8836 | 4.0794 | .8857 | 3.7850 | 2.0831 |
| 52864. | 189.10 | .8851 | 4.0755 | .8871 | 3.7822 | 2.0752 |
| 52869. | 189.08 | .8866 | 4.0749 | .8887 | 3.7799 | 2.0871 |
| 52875. | 189.06 | .8879 | 4.0829 | .8900 | 3.7906 | 2.0683 |
| 52880. | 189.04 | .8899 | 4.0884 | .8919 | 3.7988 | 2.0485 |
| 52886. | 189.02 | .8911 | 4.0921 | .8931 | 3.8053 | 2.0294 |
| 52892. | 189.00 | .8924 | 4.0905 | .8944 | 3.8043 | 2.0250 |

| WAVENUMBER CM-1 | WAVELENGTH NM | CROSS SECTION X E19, CM-2 | | ORDER | | |
|--------------------|------------------|---------------------------|-----------------|-----------------|-----------------|--------|
| | | FIRST (000) | SECOND (010) | SECOND (000) | SECOND (010) | (020) |
| 52897. | 188.98 | .8946 | 4.0843 | .8966 | 3.7955 | 2.0429 |
| 52903. | 188.96 | .8969 | 4.0783 | .8990 | 3.7860 | 2.0678 |
| 52908. | 188.94 | .8982 | 4.0806 | .9003 | 3.7899 | 2.0568 |
| 52914. | 188.92 | .8994 | 4.0820 | .9015 | 3.7933 | 2.0429 |
| 52920. | 188.90 | .9005 | 4.0825 | .9026 | 3.7930 | 2.0484 |
| 52925. | 188.88 | .9021 | 4.0851 | .9041 | 3.7974 | 2.0356 |
| 52931. | 188.86 | .9035 | 4.0891 | .9055 | 3.8038 | 2.0190 |
| 52936. | 188.84 | .9053 | 4.0881 | .9073 | 3.8039 | 2.0108 |
| 52942. | 188.82 | .9062 | 4.0915 | .9082 | 3.8085 | 2.0024 |
| 52948. | 188.80 | .9071 | 4.0973 | .9091 | 3.8134 | 2.0086 |
| 52953. | 188.78 | .9069 | 4.1147 | .9089 | 3.8319 | 2.0009 |
| 52959. | 188.76 | .9078 | 4.1252 | .9097 | 3.8433 | 1.9943 |
| 52964. | 188.74 | .9098 | 4.1275 | .9117 | 3.8462 | 1.9905 |
| 52970. | 188.72 | .9117 | 4.1313 | .9136 | 3.8527 | 1.9719 |
| 52976. | 188.70 | .9129 | 4.1400 | .9148 | 3.8639 | 1.9534 |
| 52981. | 188.68 | .9137 | 4.1529 | .9156 | 3.8803 | 1.9282 |
| 52987. | 188.66 | .9146 | 4.1618 | .9165 | 3.8907 | 1.9185 |
| 52992. | 188.64 | .9155 | 4.1637 | .9174 | 3.8888 | 1.9447 |
| 52998. | 188.62 | .9172 | 4.1489 | .9191 | 3.8679 | 1.9884 |
| 53004. | 188.60 | .9189 | 4.1366 | .9209 | 3.8517 | 2.0158 |
| 53009. | 188.58 | .9198 | 4.1400 | .9217 | 3.8585 | 1.9918 |
| 53015. | 188.56 | .9201 | 4.1556 | .9221 | 3.8787 | 1.9590 |
| 53021. | 188.54 | .9215 | 4.1651 | .9234 | 3.8886 | 1.9566 |
| 53026. | 188.52 | .9227 | 4.1817 | .9246 | 3.9058 | 1.9516 |
| 53032. | 188.50 | .9239 | 4.2022 | .9258 | 3.9293 | 1.9313 |
| 53037. | 188.48 | .9247 | 4.2246 | .9266 | 3.9551 | 1.9071 |
| 53043. | 188.46 | .9254 | 4.2454 | .9273 | 3.9778 | 1.8932 |
| 53049. | 188.44 | .9271 | 4.2657 | .9290 | 3.9975 | 1.8974 |
| 53054. | 188.42 | .9285 | 4.2897 | .9304 | 4.0257 | 1.8680 |
| 53060. | 188.40 | .9298 | 4.3126 | .9316 | 4.0532 | 1.8357 |
| 53066. | 188.38 | .9305 | 4.3326 | .9323 | 4.0784 | 1.7991 |
| 53071. | 188.36 | .9312 | 4.3613 | .9329 | 4.1165 | 1.7319 |
| 53077. | 188.34 | .9325 | 4.3843 | .9342 | 4.1441 | 1.6996 |
| 53083. | 188.32 | .9344 | 4.3937 | .9361 | 4.1531 | 1.7021 |
| 53088. | 188.30 | .9355 | 4.3997 | .9371 | 4.1633 | 1.6731 |
| 53094. | 188.28 | .9364 | 4.3992 | .9380 | 4.1636 | 1.6668 |
| 53099. | 188.26 | .9371 | 4.3984 | .9387 | 4.1638 | 1.6602 |
| 53105. | 188.24 | .9393 | 4.3875 | .9410 | 4.1494 | 1.6843 |
| 53111. | 188.22 | .9410 | 4.3807 | .9426 | 4.1411 | 1.6948 |
| 53116. | 188.20 | .9421 | 4.3772 | .9438 | 4.1391 | 1.6848 |
| 53122. | 188.18 | .9430 | 4.3767 | .9447 | 4.1410 | 1.6673 |
| 53128. | 188.16 | .9437 | 4.3783 | .9454 | 4.1418 | 1.6732 |
| 53133. | 188.14 | .9446 | 4.3793 | .9463 | 4.1411 | 1.6856 |
| 53139. | 188.12 | .9460 | 4.3762 | .9477 | 4.1372 | 1.6915 |
| 53145. | 188.10 | .9483 | 4.3709 | .9500 | 4.1327 | 1.6856 |
| 53150. | 188.08 | .9499 | 4.3673 | .9516 | 4.1314 | 1.6691 |
| 53156. | 188.06 | .9508 | 4.3651 | .9525 | 4.1281 | 1.6775 |
| 53162. | 188.04 | .9515 | 4.3683 | .9532 | 4.1350 | 1.6510 |
| 53167. | 188.02 | .9522 | 4.3707 | .9538 | 4.1387 | 1.6418 |
| 53173. | 188.00 | .9533 | 4.3712 | .9550 | 4.1384 | 1.6473 |

| WAVENUMBER CM-1 | WAVELENGTH NM | CROSS SECTION X E19, CM-2 | | | | |
|--------------------|------------------|---------------------------|--------|-----------------------|--------|--------|
| | | FIRST ORDER (000) | (010) | SECOND ORDER (000) | (010) | (020) |
| 53179. | 187.98 | .9545 | 4.3687 | .9562 | 4.1331 | 1.6667 |
| 53184. | 187.96 | .9559 | 4.3678 | .9575 | 4.1353 | 1.6450 |
| 53190. | 187.94 | .9571 | 4.3692 | .9586 | 4.1437 | 1.5956 |
| 53196. | 187.92 | .9580 | 4.3711 | .9595 | 4.1497 | 1.5662 |
| 53201. | 187.90 | .9586 | 4.3702 | .9601 | 4.1485 | 1.5684 |
| 53207. | 187.88 | .9591 | 4.3692 | .9606 | 4.1469 | 1.5726 |
| 53213. | 187.86 | .9608 | 4.3584 | .9623 | 4.1353 | 1.5786 |
| 53218. | 187.84 | .9620 | 4.3416 | .9636 | 4.1156 | 1.5986 |
| 53224. | 187.82 | .9628 | 4.3329 | .9643 | 4.1108 | 1.5719 |
| 53230. | 187.80 | .9633 | 4.3256 | .9649 | 4.1071 | 1.5458 |
| 53235. | 187.78 | .9634 | 4.3201 | .9649 | 4.1030 | 1.5359 |
| 53241. | 187.76 | .9631 | 4.3181 | .9646 | 4.1041 | 1.5146 |
| 53247. | 187.74 | .9630 | 4.3260 | .9644 | 4.1245 | 1.4258 |
| 53252. | 187.72 | .9634 | 4.3216 | .9647 | 4.1280 | 1.3702 |
| 53258. | 187.70 | .9646 | 4.3032 | .9660 | 4.1037 | 1.4114 |
| 53264. | 187.68 | .9663 | 4.2845 | .9678 | 4.0761 | 1.4751 |
| 53269. | 187.66 | .9678 | 4.2830 | .9692 | 4.0780 | 1.4508 |
| 53275. | 187.64 | .9691 | 4.2782 | .9705 | 4.0803 | 1.4001 |
| 53281. | 187.62 | .9711 | 4.2598 | .9725 | 4.0604 | 1.4108 |
| 53286. | 187.60 | .9725 | 4.2504 | .9739 | 4.0513 | 1.4086 |
| 53292. | 187.58 | .9744 | 4.2462 | .9758 | 4.0472 | 1.4075 |
| 53298. | 187.56 | .9762 | 4.2475 | .9776 | 4.0489 | 1.4051 |
| 53303. | 187.54 | .9778 | 4.2517 | .9791 | 4.0561 | 1.3843 |
| 53309. | 187.52 | .9787 | 4.2536 | .9800 | 4.0602 | 1.3683 |
| 53315. | 187.50 | .9796 | 4.2475 | .9810 | 4.0501 | 1.3966 |
| 53320. | 187.48 | .9799 | 4.2471 | .9813 | 4.0491 | 1.4010 |
| 53326. | 187.46 | .9796 | 4.2530 | .9809 | 4.0587 | 1.3753 |
| 53332. | 187.44 | .9793 | 4.2599 | .9806 | 4.0709 | 1.3369 |
| 53337. | 187.42 | .9795 | 4.2664 | .9808 | 4.0842 | 1.2898 |
| 53343. | 187.40 | .9800 | 4.2686 | .9812 | 4.0864 | 1.2892 |
| 53349. | 187.38 | .9818 | 4.2589 | .9832 | 4.0701 | 1.3360 |
| 53355. | 187.36 | .9840 | 4.2519 | .9853 | 4.0625 | 1.3401 |
| 53360. | 187.34 | .9858 | 4.2587 | .9870 | 4.0805 | 1.2610 |
| 53366. | 187.32 | .9876 | 4.2624 | .9888 | 4.0881 | 1.2334 |
| 53372. | 187.30 | .9901 | 4.2566 | .9914 | 4.0791 | 1.2563 |
| 53377. | 187.28 | .9922 | 4.2511 | .9934 | 4.0737 | 1.2546 |
| 53383. | 187.26 | .9928 | 4.2558 | .9940 | 4.0878 | 1.1890 |
| 53389. | 187.24 | .9933 | 4.2635 | .9944 | 4.1064 | 1.1116 |
| 53394. | 187.22 | .9935 | 4.2645 | .9946 | 4.1120 | 1.0790 |
| 53400. | 187.20 | .9943 | 4.2504 | .9954 | 4.0908 | 1.1291 |
| 53406. | 187.18 | .9960 | 4.2317 | .9972 | 4.0612 | 1.2061 |
| 53412. | 187.16 | .9972 | 4.2243 | .9984 | 4.0502 | 1.2315 |
| 53417. | 187.14 | .9981 | 4.2238 | .9993 | 4.0484 | 1.2408 |
| 53423. | 187.12 | .9995 | 4.2222 | 1.0008 | 4.0462 | 1.2454 |
| 53429. | 187.10 | 1.0007 | 4.2148 | 1.0020 | 4.0343 | 1.2774 |
| 53434. | 187.08 | 1.0016 | 4.2198 | 1.0028 | 4.0438 | 1.2454 |
| 53440. | 187.06 | 1.0028 | 4.2197 | 1.0040 | 4.0451 | 1.2351 |
| 53446. | 187.04 | 1.0039 | 4.2162 | 1.0052 | 4.0355 | 1.2784 |
| 53452. | 187.02 | 1.0044 | 4.2144 | 1.0057 | 4.0266 | 1.3288 |
| 53457. | 187.00 | 1.0048 | 4.2236 | 1.0061 | 4.0381 | 1.3122 |

| WAVENUMBER CM-1 | WAVELENGTH NM | CROSS SECTION X E19, CM-2 | | | | |
|--------------------|------------------|---------------------------|----------------|--------------------------|----------------|--------|
| | | FIRST ORDER (000) | ORDER (010) | SECOND ORDER (000) | ORDER (010) | (020) |
| 53463. | 186.98 | 1.0056 | 4.2310 | 1.0069 | 4.0492 | 1.2860 |
| 53469. | 186.96 | 1.0065 | 4.2360 | 1.0078 | 4.0562 | 1.2718 |
| 53474. | 186.94 | 1.0080 | 4.2265 | 1.0093 | 4.0396 | 1.3229 |
| 53480. | 186.92 | 1.0089 | 4.2205 | 1.0103 | 4.0276 | 1.3645 |
| 53486. | 186.90 | 1.0100 | 4.2249 | 1.0114 | 4.0307 | 1.3746 |
| 53492. | 186.88 | 1.0112 | 4.2303 | 1.0125 | 4.0345 | 1.3852 |
| 53497. | 186.86 | 1.0120 | 4.2408 | 1.0133 | 4.0494 | 1.3542 |
| 53503. | 186.84 | 1.0128 | 4.2482 | 1.0142 | 4.0595 | 1.3347 |
| 53509. | 186.82 | 1.0137 | 4.2571 | 1.0150 | 4.0717 | 1.3117 |
| 53514. | 186.80 | 1.0131 | 4.2684 | 1.0144 | 4.0806 | 1.3289 |
| 53520. | 186.78 | 1.0130 | 4.2818 | 1.0143 | 4.0923 | 1.3412 |
| 53526. | 186.76 | 1.0134 | 4.2934 | 1.0148 | 4.1038 | 1.3416 |
| 53532. | 186.74 | 1.0135 | 4.3134 | 1.0148 | 4.1306 | 1.2933 |
| 53537. | 186.72 | 1.0141 | 4.3198 | 1.0154 | 4.1370 | 1.2931 |
| 53543. | 186.70 | 1.0150 | 4.3232 | 1.0163 | 4.1372 | 1.3157 |
| 53549. | 186.68 | 1.0166 | 4.3298 | 1.0179 | 4.1406 | 1.3385 |
| 53555. | 186.66 | 1.0178 | 4.3527 | 1.0191 | 4.1691 | 1.2995 |
| 53560. | 186.64 | 1.0202 | 4.3707 | 1.0215 | 4.1906 | 1.2740 |
| 53566. | 186.62 | 1.0233 | 4.3759 | 1.0246 | 4.1913 | 1.3060 |
| 53572. | 186.60 | 1.0272 | 4.3781 | 1.0286 | 4.1869 | 1.3523 |
| 53578. | 186.58 | 1.0307 | 4.3941 | 1.0320 | 4.2048 | 1.3399 |
| 53583. | 186.56 | 1.0347 | 4.4179 | 1.0359 | 4.2377 | 1.2744 |
| 53589. | 186.54 | 1.0383 | 4.4317 | 1.0395 | 4.2547 | 1.2519 |
| 53595. | 186.52 | 1.0407 | 4.4472 | 1.0419 | 4.2728 | 1.2338 |
| 53601. | 186.50 | 1.0409 | 4.4824 | 1.0420 | 4.3236 | 1.1234 |
| 53606. | 186.48 | 1.0402 | 4.5175 | 1.0412 | 4.3760 | 1.0013 |
| 53612. | 186.46 | 1.0396 | 4.5343 | 1.0405 | 4.4012 | .9418 |
| 53618. | 186.44 | 1.0398 | 4.5345 | 1.0407 | 4.3995 | .9554 |
| 53624. | 186.42 | 1.0403 | 4.5256 | 1.0413 | 4.3844 | .9995 |
| 53629. | 186.40 | 1.0397 | 4.5224 | 1.0407 | 4.3790 | 1.0149 |
| 53635. | 186.38 | 1.0382 | 4.5319 | 1.0391 | 4.3966 | .9571 |
| 53641. | 186.36 | 1.0378 | 4.5345 | 1.0387 | 4.4029 | .9317 |
| 53647. | 186.34 | 1.0378 | 4.5235 | 1.0388 | 4.3883 | .9564 |
| 53652. | 186.32 | 1.0383 | 4.5113 | 1.0393 | 4.3762 | .9563 |
| 53658. | 186.30 | 1.0384 | 4.5018 | 1.0393 | 4.3709 | .9264 |
| 53664. | 186.28 | 1.0385 | 4.4939 | 1.0393 | 4.3731 | .8552 |
| 53670. | 186.26 | 1.0386 | 4.4766 | 1.0394 | 4.3603 | .8229 |
| 53675. | 186.24 | 1.0393 | 4.4464 | 1.0402 | 4.3234 | .8702 |
| 53681. | 186.22 | 1.0400 | 4.4185 | 1.0409 | 4.2871 | .9300 |
| 53687. | 186.20 | 1.0415 | 4.3924 | 1.0425 | 4.2564 | .9624 |
| 53693. | 186.18 | 1.0421 | 4.3835 | 1.0430 | 4.2541 | .9155 |
| 53698. | 186.16 | 1.0421 | 4.3875 | 1.0429 | 4.2688 | .8400 |
| 53704. | 186.14 | 1.0425 | 4.3792 | 1.0433 | 4.2630 | .8222 |
| 53710. | 186.12 | 1.0433 | 4.3651 | 1.0442 | 4.2446 | .8523 |
| 53716. | 186.10 | 1.0445 | 4.3577 | 1.0453 | 4.2386 | .8471 |
| 53722. | 186.08 | 1.0452 | 4.3530 | 1.0460 | 4.2361 | .8266 |
| 53727. | 186.06 | 1.0469 | 4.3398 | 1.0478 | 4.2230 | .8268 |
| 53733. | 186.04 | 1.0484 | 4.3288 | 1.0493 | 4.2090 | .8482 |
| 53739. | 186.02 | 1.0484 | 4.3344 | 1.0492 | 4.2200 | .8091 |
| 53745. | 186.00 | 1.0484 | 4.3383 | 1.0491 | 4.2337 | .7403 |

| WAVENUMBER CM-1 | WAVELENGTH NM | CROSS SECTION X E19, CM-2 | | | | |
|--------------------|------------------|---------------------------|--------|--------------------------|--------|-------|
| | | FIRST ORDER (000) | (010) | SECOND ORDER (000) | (010) | (020) |
| 53750. | 185.98 | 1.0492 | 4.3241 | 1.0499 | 4.2203 | .7349 |
| 53756. | 185.96 | 1.0504 | 4.3049 | 1.0512 | 4.1984 | .7534 |
| 53762. | 185.94 | 1.0514 | 4.2957 | 1.0522 | 4.1861 | .7754 |
| 53768. | 185.92 | 1.0519 | 4.2978 | 1.0526 | 4.1927 | .7437 |
| 53774. | 185.90 | 1.0537 | 4.2968 | 1.0544 | 4.1982 | .6978 |
| 53779. | 185.88 | 1.0565 | 4.2865 | 1.0572 | 4.1878 | .6983 |
| 53785. | 185.86 | 1.0593 | 4.2683 | 1.0601 | 4.1649 | .7319 |
| 53791. | 185.84 | 1.0620 | 4.2531 | 1.0627 | 4.1484 | .7405 |
| 53797. | 185.82 | 1.0651 | 4.2408 | 1.0658 | 4.1372 | .7334 |
| 53802. | 185.80 | 1.0677 | 4.2319 | 1.0684 | 4.1290 | .7279 |
| 53808. | 185.78 | 1.0702 | 4.2246 | 1.0709 | 4.1233 | .7166 |
| 53814. | 185.76 | 1.0720 | 4.2259 | 1.0727 | 4.1318 | .6653 |
| 53820. | 185.74 | 1.0736 | 4.2317 | 1.0742 | 4.1436 | .6232 |
| 53826. | 185.72 | 1.0747 | 4.2306 | 1.0753 | 4.1431 | .6190 |
| 53831. | 185.70 | 1.0747 | 4.2306 | 1.0753 | 4.1456 | .6012 |
| 53837. | 185.68 | 1.0740 | 4.2353 | 1.0745 | 4.1566 | .5568 |
| 53843. | 185.66 | 1.0740 | 4.2274 | 1.0746 | 4.1481 | .5611 |
| 53849. | 185.64 | 1.0751 | 4.2095 | 1.0757 | 4.1228 | .6136 |
| 53855. | 185.62 | 1.0764 | 4.1920 | 1.0771 | 4.0981 | .6643 |
| 53860. | 185.60 | 1.0778 | 4.1872 | 1.0784 | 4.0898 | .6891 |
| 53866. | 185.58 | 1.0797 | 4.1839 | 1.0804 | 4.0831 | .7131 |
| 53872. | 185.56 | 1.0803 | 4.1917 | 1.0810 | 4.0918 | .7069 |
| 53878. | 185.54 | 1.0798 | 4.2038 | 1.0804 | 4.1083 | .6759 |
| 53884. | 185.52 | 1.0795 | 4.2068 | 1.0802 | 4.1104 | .6819 |
| 53889. | 185.50 | 1.0802 | 4.2051 | 1.0808 | 4.1060 | .7014 |
| 53895. | 185.48 | 1.0811 | 4.2110 | 1.0818 | 4.1157 | .6744 |
| 53901. | 185.46 | 1.0817 | 4.2188 | 1.0823 | 4.1253 | .6616 |
| 53907. | 185.44 | 1.0829 | 4.2123 | 1.0836 | 4.1098 | .7254 |
| 53913. | 185.42 | 1.0834 | 4.2080 | 1.0841 | 4.0980 | .7788 |
| 53919. | 185.40 | 1.0831 | 4.2149 | 1.0839 | 4.1059 | .7715 |
| 53924. | 185.38 | 1.0832 | 4.2254 | 1.0840 | 4.1193 | .7511 |
| 53930. | 185.36 | 1.0844 | 4.2268 | 1.0852 | 4.1164 | .7816 |
| 53936. | 185.34 | 1.0848 | 4.2336 | 1.0856 | 4.1219 | .7903 |
| 53942. | 185.32 | 1.0859 | 4.2445 | 1.0867 | 4.1381 | .7531 |
| 53948. | 185.30 | 1.0873 | 4.2549 | 1.0880 | 4.1547 | .7091 |
| 53953. | 185.28 | 1.0892 | 4.2650 | 1.0899 | 4.1685 | .6831 |
| 53959. | 185.26 | 1.0894 | 4.2876 | 1.0900 | 4.2002 | .6187 |
| 53965. | 185.24 | 1.0891 | 4.3095 | 1.0896 | 4.2372 | .5112 |
| 53971. | 185.22 | 1.0898 | 4.3032 | 1.0903 | 4.2323 | .5014 |
| 53977. | 185.20 | 1.0909 | 4.2821 | 1.0914 | 4.2016 | .5699 |
| 53983. | 185.18 | 1.0921 | 4.2653 | 1.0927 | 4.1731 | .6520 |
| 53988. | 185.16 | 1.0934 | 4.2588 | 1.0941 | 4.1586 | .7091 |
| 53994. | 185.14 | 1.0937 | 4.2640 | 1.0945 | 4.1580 | .7502 |
| 54000. | 185.12 | 1.0946 | 4.2745 | 1.0953 | 4.1650 | .7747 |
| 54006. | 185.10 | 1.0957 | 4.2878 | 1.0965 | 4.1758 | .7922 |
| 54012. | 185.08 | 1.0963 | 4.3196 | 1.0971 | 4.2166 | .7291 |
| 54018. | 185.06 | 1.0967 | 4.3558 | 1.0974 | 4.2586 | .6883 |
| 54023. | 185.04 | 1.0973 | 4.3932 | 1.0980 | 4.2994 | .6640 |
| 54029. | 185.02 | 1.0967 | 4.4538 | 1.0972 | 4.3804 | .5190 |
| 54035. | 185.00 | 1.0951 | 4.5180 | 1.0954 | 4.4694 | .3443 |

| WAVENUMBER CM-1 | WAVELENGTH NM | CROSS SECTION X E15, CM-2 | | | | |
|--------------------|------------------|---------------------------|----------------|-----------------|----------------|-------|
| | | FIRST (000) | ORDER (010) | SECOND (000) | ORDER (010) | (020) |
| 54041. | 184.98 | 1.0934 | 4.5622 | 1.0936 | 4.5248 | .2645 |
| 54047. | 184.96 | 1.0930 | 4.5785 | 1.0933 | 4.5380 | .2871 |
| 54053. | 184.94 | 1.0935 | 4.5886 | 1.0938 | 4.5465 | .2977 |
| 54059. | 184.92 | 1.0938 | 4.5993 | 1.0941 | 4.5598 | .2798 |
| 54064. | 184.90 | 1.0937 | 4.6072 | 1.0940 | 4.5717 | .2511 |
| 54070. | 184.88 | 1.0944 | 4.6057 | 1.0947 | 4.5756 | .2129 |
| 54076. | 184.86 | 1.0949 | 4.6014 | 1.0951 | 4.5716 | .2107 |
| 54082. | 184.84 | 1.0957 | 4.5912 | 1.0959 | 4.5556 | .2520 |
| 54088. | 184.82 | 1.0969 | 4.5807 | 1.0972 | 4.5446 | .2557 |
| 54094. | 184.80 | 1.0983 | 4.5704 | 1.0986 | 4.5391 | .2218 |
| 54099. | 184.78 | 1.1006 | 4.5507 | 1.1008 | 4.5167 | .2409 |
| 54105. | 184.76 | 1.1030 | 4.5296 | 1.1032 | 4.4930 | .2591 |
| 54111. | 184.74 | 1.1047 | 4.5189 | 1.1049 | 4.4874 | .2230 |
| 54117. | 184.72 | 1.1061 | 4.5134 | 1.1063 | 4.4888 | .1742 |
| 54123. | 184.70 | 1.1078 | 4.5011 | 1.1080 | 4.4770 | .1705 |
| 54129. | 184.68 | 1.1093 | 4.4789 | 1.1095 | 4.4511 | .1963 |
| 54135. | 184.66 | 1.1097 | 4.4674 | 1.1098 | 4.4415 | .1832 |
| 54140. | 184.64 | 1.1090 | 4.4642 | 1.1091 | 4.4440 | .1431 |
| 54146. | 184.62 | 1.1090 | 4.4587 | 1.1091 | 4.4414 | .1221 |
| 54152. | 184.60 | 1.1094 | 4.4560 | 1.1095 | 4.4461 | .0698 |
| 54158. | 184.58 | 1.1102 | 4.4473 | 1.1102 | 4.4450 | .0164 |
| 54164. | 184.56 | 1.1111 | 4.4237 | 1.1112 | 4.4135 | .0721 |
| 54170. | 184.54 | 1.1118 | 4.3990 | 1.1119 | 4.3810 | .1270 |
| 54176. | 184.52 | 1.1120 | 4.3905 | 1.1121 | 4.3773 | .0934 |
| 54182. | 184.50 | 1.1128 | 4.3803 | 1.1129 | 4.3716 | .0613 |
| 54187. | 184.48 | 1.1131 | 4.3671 | 1.1132 | 4.3595 | .0538 |
| 54193. | 184.46 | 1.1141 | 4.3500 | 1.1142 | 4.3409 | .0646 |
| 54199. | 184.44 | 1.1149 | 4.3374 | 1.1150 | 4.3277 | .0689 |
| 54205. | 184.42 | 1.1157 | 4.3272 | 1.1158 | 4.3176 | .0679 |
| 54211. | 184.40 | 1.1165 | 4.3146 | 1.1166 | 4.3043 | .0723 |
| 54217. | 184.38 | 1.1168 | 4.3077 | 1.1168 | 4.2990 | .0618 |
| 54223. | 184.36 | 1.1176 | 4.2974 | 1.1176 | 4.2898 | .0541 |
| 54229. | 184.34 | 1.1182 | 4.2934 | 1.1182 | 4.2901 | .0234 |
| 54234. | 184.32 | 1.1197 | 4.2816 | 1.1197 | 4.2773 | .0309 |
| 54240. | 184.30 | 1.1212 | 4.2667 | 1.1213 | 4.2552 | .0810 |
| 54246. | 184.28 | 1.1222 | 4.2590 | 1.1223 | 4.2440 | .1062 |
| 54252. | 184.26 | 1.1216 | 4.2640 | 1.1217 | 4.2515 | .0887 |
| 54258. | 184.24 | 1.1206 | 4.2740 | 1.1207 | 4.2686 | .0383 |
| 54264. | 184.22 | 1.1202 | 4.2862 | 1.1202 | 4.2862 | 0. |
| 54270. | 184.20 | 1.1202 | 4.2822 | 1.1202 | 4.2822 | 0. |
| 54276. | 184.18 | 1.1208 | 4.2590 | 1.1208 | 4.2573 | .0118 |
| 54282. | 184.16 | 1.1215 | 4.2304 | 1.1216 | 4.2121 | .1289 |
| 54288. | 184.14 | 1.1221 | 4.2224 | 1.1222 | 4.1988 | .1669 |
| 54293. | 184.12 | 1.1228 | 4.2271 | 1.1230 | 4.2050 | .1569 |
| 54299. | 184.10 | 1.1237 | 4.2250 | 1.1239 | 4.2007 | .1719 |
| 54305. | 184.08 | 1.1259 | 4.2133 | 1.1262 | 4.1806 | .2310 |
| 54311. | 184.06 | 1.1270 | 4.2193 | 1.1272 | 4.1907 | .2020 |
| 54317. | 184.04 | 1.1264 | 4.2441 | 1.1265 | 4.2289 | .1072 |
| 54323. | 184.02 | 1.1255 | 4.2685 | 1.1256 | 4.2634 | .0364 |
| 54329. | 184.00 | 1.1259 | 4.2785 | 1.1259 | 4.2744 | .0292 |

| WAVENUMBER CM-1 | WAVELENGTH NM | CROSS SECTION X E19 | | CM-2 | | |
|--------------------|------------------|-------------------------|----------------|--------------------------|----------------|-------|
| | | FIRST ORDER (000) | ORDER (010) | SECOND ORDER (000) | ORDER (010) | (020) |
| 54335. | 183.98 | 1.1270 | 4.2838 | 1.1271 | 4.2801 | .0265 |
| 54341. | 183.96 | 1.1290 | 4.2878 | 1.1290 | 4.2847 | .0213 |
| 54347. | 183.94 | 1.1313 | 4.2857 | 1.1314 | 4.2845 | .0085 |
| 54352. | 183.92 | 1.1337 | 4.2781 | 1.1338 | 4.2720 | .0436 |
| 54358. | 183.90 | 1.1367 | 4.2720 | 1.1368 | 4.2617 | .0733 |
| 54364. | 183.88 | 1.1392 | 4.2679 | 1.1393 | 4.2588 | .0639 |
| 54370. | 183.86 | 1.1404 | 4.2716 | 1.1404 | 4.2697 | .0136 |
| 54376. | 183.84 | 1.1413 | 4.2766 | 1.1413 | 4.2766 | 0. |
| 54382. | 183.82 | 1.1429 | 4.2817 | 1.1429 | 4.2817 | 0. |
| 54388. | 183.80 | 1.1442 | 4.2729 | 1.1442 | 4.2729 | 0. |
| 54394. | 183.78 | 1.1443 | 4.2690 | 1.1443 | 4.2690 | 0. |
| 54400. | 183.76 | 1.1443 | 4.2611 | 1.1443 | 4.2611 | 0. |
| 54406. | 183.74 | 1.1449 | 4.2538 | 1.1449 | 4.2507 | .0220 |
| 54412. | 183.72 | 1.1453 | 4.2511 | 1.1453 | 4.2453 | .0407 |
| 54418. | 183.70 | 1.1460 | 4.2503 | 1.1460 | 4.2503 | 0. |
| 54423. | 183.68 | 1.1469 | 4.2498 | 1.1469 | 4.2498 | 0. |
| 54429. | 183.66 | 1.1470 | 4.2603 | 1.1470 | 4.2603 | 0. |
| 54435. | 183.64 | 1.1466 | 4.2669 | 1.1466 | 4.2669 | 0. |
| 54441. | 183.62 | 1.1468 | 4.2593 | 1.1468 | 4.2593 | 0. |
| 54447. | 183.60 | 1.1469 | 4.2482 | 1.1470 | 4.2409 | .0514 |
| 54453. | 183.58 | 1.1458 | 4.2517 | 1.1459 | 4.2386 | .0925 |
| 54459. | 183.56 | 1.1439 | 4.2677 | 1.1439 | 4.2607 | .0494 |
| 54465. | 183.54 | 1.1429 | 4.2817 | 1.1429 | 4.2809 | .0057 |
| 54471. | 183.52 | 1.1418 | 4.2884 | 1.1418 | 4.2862 | .0156 |
| 54477. | 183.50 | 1.1406 | 4.2974 | 1.1407 | 4.2930 | .0311 |
| 54483. | 183.48 | 1.1399 | 4.3037 | 1.1399 | 4.2957 | .0564 |
| 54489. | 183.46 | 1.1389 | 4.3121 | 1.1390 | 4.2985 | .0962 |
| 54495. | 183.44 | 1.1375 | 4.3264 | 1.1376 | 4.3117 | .1035 |
| 54501. | 183.42 | 1.1354 | 4.3510 | 1.1354 | 4.3440 | .0497 |
| 54507. | 183.40 | 1.1343 | 4.3736 | 1.1343 | 4.3730 | .0044 |
| 54512. | 183.38 | 1.1338 | 4.3897 | 1.1338 | 4.3888 | .0067 |
| 54518. | 183.36 | 1.1341 | 4.4005 | 1.1342 | 4.3951 | .0377 |
| 54524. | 183.34 | 1.1357 | 4.4086 | 1.1357 | 4.4037 | .0347 |
| 54530. | 183.32 | 1.1390 | 4.4166 | 1.1390 | 4.4166 | 0. |
| 54536. | 183.30 | 1.1439 | 4.4111 | 1.1439 | 4.4089 | .0156 |
| 54542. | 183.28 | 1.1488 | 4.4017 | 1.1489 | 4.3935 | .0581 |
| 54548. | 183.26 | 1.1527 | 4.4007 | 1.1527 | 4.3953 | .0381 |
| 54554. | 183.24 | 1.1558 | 4.4091 | 1.1558 | 4.4091 | 0. |
| 54560. | 183.22 | 1.1592 | 4.4092 | 1.1592 | 4.4092 | 0. |
| 54566. | 183.20 | 1.1620 | 4.4044 | 1.1620 | 4.4044 | 0. |
| 54572. | 183.18 | 1.1643 | 4.4063 | 1.1643 | 4.4063 | 0. |
| 54578. | 183.16 | 1.1659 | 4.4106 | 1.1659 | 4.4106 | 0. |
| 54584. | 183.14 | 1.1649 | 4.4229 | 1.1649 | 4.4229 | 0. |
| 54590. | 183.12 | 1.1630 | 4.4311 | 1.1630 | 4.4311 | 0. |
| 54596. | 183.10 | 1.1626 | 4.4155 | 1.1626 | 4.4155 | 0. |
| 54602. | 183.08 | 1.1628 | 4.3926 | 1.1628 | 4.3926 | 0. |
| 54608. | 183.06 | 1.1616 | 4.3761 | 1.1616 | 4.3761 | 0. |
| 54614. | 183.04 | 1.1588 | 4.3720 | 1.1588 | 4.3720 | 0. |
| 54620. | 183.02 | 1.1572 | 4.3733 | 1.1572 | 4.3733 | 0. |
| 54626. | 183.00 | 1.1568 | 4.3665 | 1.1568 | 4.3665 | 0. |

| WAVENUMBER CM-1 | WAVELENGTH NM | CROSS SECTION X E19, CM-2 | | | | |
|--------------------|------------------|---------------------------|----------------|--------------------------|----------------|-------|
| | | FIRST ORDER (000) | ORDER (010) | SECOND ORDER (000) | ORDER (010) | (020) |
| 54632. | 182.98 | 1.1563 | 4.3483 | 1.1563 | 4.3483 | 0. |
| 54638. | 182.96 | 1.1561 | 4.3147 | 1.1561 | 4.3147 | 0. |
| 54644. | 182.94 | 1.1551 | 4.2833 | 1.1551 | 4.2833 | 0. |
| 54650. | 182.92 | 1.1551 | 4.2562 | 1.1551 | 4.2562 | 0. |
| 54656. | 182.90 | 1.1557 | 4.2377 | 1.1557 | 4.2377 | 0. |
| 54662. | 182.88 | 1.1557 | 4.2283 | 1.1557 | 4.2283 | 0. |
| 54668. | 182.86 | 1.1551 | 4.2347 | 1.1551 | 4.2347 | 0. |
| 54673. | 182.84 | 1.1556 | 4.2225 | 1.1556 | 4.2225 | 0. |
| 54679. | 182.82 | 1.1579 | 4.1965 | 1.1579 | 4.1965 | 0. |
| 54685. | 182.80 | 1.1593 | 4.1878 | 1.1593 | 4.1878 | 0. |
| 54691. | 182.78 | 1.1596 | 4.1842 | 1.1596 | 4.1842 | 0. |
| 54697. | 182.76 | 1.1599 | 4.1710 | 1.1599 | 4.1710 | 0. |
| 54703. | 182.74 | 1.1601 | 4.1641 | 1.1601 | 4.1641 | 0. |
| 54709. | 182.72 | 1.1607 | 4.1592 | 1.1607 | 4.1592 | 0. |
| 54715. | 182.70 | 1.1607 | 4.1513 | 1.1607 | 4.1513 | 0. |
| 54721. | 182.68 | 1.1605 | 4.1383 | 1.1605 | 4.1383 | 0. |
| 54727. | 182.66 | 1.1609 | 4.1268 | 1.1609 | 4.1268 | 0. |
| 54733. | 182.64 | 1.1610 | 4.1189 | 1.1610 | 4.1189 | 0. |
| 54739. | 182.62 | 1.1616 | 4.1093 | 1.1616 | 4.1093 | 0. |
| 54745. | 182.60 | 1.1620 | 4.1050 | 1.1620 | 4.1050 | 0. |
| 54751. | 182.58 | 1.1622 | 4.1020 | 1.1622 | 4.1020 | 0. |
| 54757. | 182.56 | 1.1629 | 4.0797 | 1.1629 | 4.0797 | 0. |
| 54763. | 182.54 | 1.1635 | 4.0518 | 1.1635 | 4.0518 | 0. |
| 54769. | 182.52 | 1.1626 | 4.0523 | 1.1626 | 4.0523 | 0. |
| 54775. | 182.50 | 1.1620 | 4.0541 | 1.1620 | 4.0541 | 0. |
| 54781. | 182.48 | 1.1626 | 4.0428 | 1.1626 | 4.0428 | 0. |
| 54787. | 182.46 | 1.1641 | 4.0294 | 1.1641 | 4.0294 | 0. |
| 54793. | 182.44 | 1.1653 | 4.0244 | 1.1653 | 4.0244 | 0. |
| 54799. | 182.42 | 1.1669 | 4.0192 | 1.1669 | 4.0192 | 0. |
| 54805. | 182.40 | 1.1676 | 4.0224 | 1.1676 | 4.0224 | 0. |
| 54811. | 182.38 | 1.1678 | 4.0242 | 1.1678 | 4.0242 | 0. |
| 54817. | 182.36 | 1.1690 | 4.0191 | 1.1690 | 4.0191 | 0. |
| 54823. | 182.34 | 1.1696 | 4.0215 | 1.1696 | 4.0215 | 0. |
| 54829. | 182.32 | 1.1696 | 4.0310 | 1.1696 | 4.0310 | 0. |
| 54835. | 182.30 | 1.1692 | 4.0321 | 1.1692 | 4.0321 | 0. |
| 54841. | 182.28 | 1.1705 | 4.0273 | 1.1705 | 4.0273 | 0. |
| 54847. | 182.26 | 1.1714 | 4.0308 | 1.1714 | 4.0308 | 0. |
| 54853. | 182.24 | 1.1718 | 4.0384 | 1.1718 | 4.0384 | 0. |
| 54860. | 182.22 | 1.1720 | 4.0474 | 1.1720 | 4.0474 | 0. |
| 54866. | 182.20 | 1.1733 | 4.0529 | 1.1733 | 4.0529 | 0. |
| 54872. | 182.18 | 1.1740 | 4.0617 | 1.1740 | 4.0617 | 0. |
| 54878. | 182.16 | 1.1743 | 4.0700 | 1.1743 | 4.0700 | 0. |
| 54884. | 182.14 | 1.1751 | 4.0653 | 1.1751 | 4.0653 | 0. |
| 54890. | 182.12 | 1.1753 | 4.0663 | 1.1753 | 4.0663 | 0. |
| 54896. | 182.10 | 1.1744 | 4.0861 | 1.1744 | 4.0861 | 0. |
| 54902. | 182.08 | 1.1736 | 4.1130 | 1.1736 | 4.1130 | 0. |
| 54908. | 182.06 | 1.1728 | 4.1287 | 1.1728 | 4.1287 | 0. |
| 54914. | 182.04 | 1.1708 | 4.1503 | 1.1708 | 4.1503 | 0. |
| 54920. | 182.02 | 1.1683 | 4.1737 | 1.1683 | 4.1737 | 0. |
| 54926. | 182.00 | 1.1660 | 4.1973 | 1.1660 | 4.1973 | 0. |

| WAVENUMBER CM-1 | WAVELENGTH NM | CROSS SECTION X E19 CM-2 | | | | |
|--------------------|------------------|--------------------------|----------------|--------------------------|----------------|-------|
| | | FIRST ORDER (000) | ORDER (010) | SECOND ORDER (000) | ORDER (010) | (020) |
| 54932. | 181.98 | 1.1647 | 4.2237 | 1.1647 | 4.2237 | 0. |
| 54938. | 181.96 | 1.1645 | 4.2329 | 1.1645 | 4.2329 | 0. |
| 54944. | 181.94 | 1.1640 | 4.2268 | 1.1640 | 4.2268 | 0. |
| 54950. | 181.92 | 1.1642 | 4.2055 | 1.1642 | 4.2055 | 0. |
| 54956. | 181.90 | 1.1655 | 4.1824 | 1.1655 | 4.1824 | 0. |
| 54962. | 181.88 | 1.1664 | 4.1842 | 1.1664 | 4.1842 | 0. |
| 54968. | 181.86 | 1.1667 | 4.2076 | 1.1667 | 4.2076 | 0. |
| 54974. | 181.84 | 1.1683 | 4.2087 | 1.1683 | 4.2087 | 0. |
| 54980. | 181.82 | 1.1714 | 4.1901 | 1.1714 | 4.1901 | 0. |
| 54986. | 181.80 | 1.1734 | 4.1956 | 1.1734 | 4.1956 | 0. |
| 54992. | 181.78 | 1.1744 | 4.2150 | 1.1744 | 4.2150 | 0. |
| 54998. | 181.76 | 1.1747 | 4.2401 | 1.1747 | 4.2401 | 0. |
| 55004. | 181.74 | 1.1761 | 4.2735 | 1.1761 | 4.2735 | 0. |
| 55010. | 181.72 | 1.1776 | 4.3049 | 1.1776 | 4.3049 | 0. |
| 55017. | 181.70 | 1.1772 | 4.3370 | 1.1772 | 4.3370 | 0. |
| 55023. | 181.68 | 1.1756 | 4.3638 | 1.1756 | 4.3638 | 0. |
| 55029. | 181.66 | 1.1735 | 4.3788 | 1.1735 | 4.3788 | 0. |
| 55035. | 181.64 | 1.1718 | 4.3935 | 1.1718 | 4.3935 | 0. |
| 55041. | 181.62 | 1.1705 | 4.4055 | 1.1705 | 4.4055 | 0. |
| 55047. | 181.60 | 1.1688 | 4.4196 | 1.1688 | 4.4196 | 0. |
| 55053. | 181.58 | 1.1672 | 4.4185 | 1.1672 | 4.4185 | 0. |
| 55059. | 181.56 | 1.1678 | 4.3753 | 1.1678 | 4.3753 | 0. |
| 55065. | 181.54 | 1.1697 | 4.3243 | 1.1697 | 4.3243 | 0. |
| 55071. | 181.52 | 1.1713 | 4.2926 | 1.1713 | 4.2926 | 0. |
| 55077. | 181.50 | 1.1718 | 4.2661 | 1.1718 | 4.2661 | 0. |
| 55083. | 181.48 | 1.1720 | 4.2393 | 1.1720 | 4.2393 | 0. |
| 55089. | 181.46 | 1.1725 | 4.2255 | 1.1725 | 4.2255 | 0. |
| 55095. | 181.44 | 1.1734 | 4.2171 | 1.1734 | 4.2171 | 0. |
| 55101. | 181.42 | 1.1743 | 4.1974 | 1.1743 | 4.1974 | 0. |
| 55108. | 181.40 | 1.1754 | 4.1724 | 1.1754 | 4.1724 | 0. |
| 55114. | 181.38 | 1.1767 | 4.1525 | 1.1767 | 4.1525 | 0. |
| 55120. | 181.36 | 1.1772 | 4.1443 | 1.1772 | 4.1443 | 0. |
| 55126. | 181.34 | 1.1763 | 4.1448 | 1.1763 | 4.1448 | 0. |
| 55132. | 181.32 | 1.1756 | 4.1416 | 1.1756 | 4.1416 | 0. |
| 55138. | 181.30 | 1.1757 | 4.1321 | 1.1757 | 4.1321 | 0. |
| 55144. | 181.28 | 1.1761 | 4.1096 | 1.1761 | 4.1096 | 0. |
| 55150. | 181.26 | 1.1760 | 4.0863 | 1.1760 | 4.0863 | 0. |
| 55156. | 181.24 | 1.1757 | 4.0756 | 1.1757 | 4.0756 | 0. |
| 55162. | 181.22 | 1.1753 | 4.0624 | 1.1753 | 4.0624 | 0. |
| 55168. | 181.20 | 1.1757 | 4.0397 | 1.1757 | 4.0397 | 0. |
| 55174. | 181.18 | 1.1763 | 4.0229 | 1.1763 | 4.0229 | 0. |
| 55181. | 181.16 | 1.1762 | 4.0093 | 1.1762 | 4.0093 | 0. |
| 55187. | 181.14 | 1.1754 | 3.9964 | 1.1754 | 3.9964 | 0. |
| 55193. | 181.12 | 1.1747 | 3.9971 | 1.1747 | 3.9971 | 0. |
| 55199. | 181.10 | 1.1751 | 3.9866 | 1.1751 | 3.9866 | 0. |
| 55205. | 181.08 | 1.1752 | 3.9716 | 1.1752 | 3.9716 | 0. |
| 55211. | 181.06 | 1.1753 | 3.9660 | 1.1753 | 3.9660 | 0. |
| 55217. | 181.04 | 1.1761 | 3.9574 | 1.1761 | 3.9574 | 0. |
| 55223. | 181.02 | 1.1763 | 3.9450 | 1.1763 | 3.9450 | 0. |
| 55229. | 181.00 | 1.1760 | 3.9437 | 1.1760 | 3.9437 | 0. |

| WAVENUMBER CM-1 | WAVELENGTH NM | CROSS SECTION X E19 CM-2 | | | | |
|--------------------|------------------|--------------------------|--------|--------------------------|--------|-------|
| | | FIRST ORDER (000) | (010) | SECOND ORDER (000) | (010) | (020) |
| 55235. | 180.98 | 1.1764 | 3.9387 | 1.1764 | 3.9387 | 0. |
| 55241. | 180.96 | 1.1762 | 3.9368 | 1.1762 | 3.9368 | 0. |
| 55248. | 180.94 | 1.1757 | 3.9466 | 1.1757 | 3.9466 | 0. |
| 55254. | 180.92 | 1.1752 | 3.9540 | 1.1752 | 3.9540 | 0. |
| 55260. | 180.90 | 1.1760 | 3.9437 | 1.1760 | 3.9437 | 0. |
| 55266. | 180.88 | 1.1758 | 3.9427 | 1.1758 | 3.9427 | 0. |
| 55272. | 180.86 | 1.1735 | 3.9592 | 1.1735 | 3.9592 | 0. |
| 55278. | 180.84 | 1.1704 | 3.9858 | 1.1704 | 3.9858 | 0. |
| 55284. | 180.82 | 1.1685 | 3.9948 | 1.1685 | 3.9948 | 0. |
| 55290. | 180.80 | 1.1683 | 3.9810 | 1.1683 | 3.9810 | 0. |
| 55296. | 180.78 | 1.1697 | 3.9579 | 1.1697 | 3.9579 | 0. |
| 55303. | 180.76 | 1.1711 | 3.9476 | 1.1711 | 3.9476 | 0. |
| 55309. | 180.74 | 1.1712 | 3.9612 | 1.1712 | 3.9612 | 0. |
| 55315. | 180.72 | 1.1691 | 4.0002 | 1.1691 | 4.0002 | 0. |
| 55321. | 180.70 | 1.1678 | 4.0305 | 1.1678 | 4.0305 | 0. |
| 55327. | 180.68 | 1.1681 | 4.0477 | 1.1681 | 4.0477 | 0. |
| 55333. | 180.66 | 1.1679 | 4.0800 | 1.1679 | 4.0800 | 0. |
| 55339. | 180.64 | 1.1670 | 4.1021 | 1.1670 | 4.1021 | 0. |
| 55345. | 180.62 | 1.1679 | 4.1016 | 1.1679 | 4.1016 | 0. |
| 55352. | 180.60 | 1.1690 | 4.1131 | 1.1690 | 4.1131 | 0. |
| 55358. | 180.58 | 1.1704 | 4.1426 | 1.1704 | 4.1426 | 0. |
| 55364. | 180.56 | 1.1710 | 4.1800 | 1.1710 | 4.1800 | 0. |
| 55370. | 180.54 | 1.1717 | 4.1816 | 1.1717 | 4.1816 | 0. |
| 55376. | 180.52 | 1.1729 | 4.1703 | 1.1729 | 4.1703 | 0. |
| 55382. | 180.50 | 1.1738 | 4.1713 | 1.1738 | 4.1713 | 0. |
| 55388. | 180.48 | 1.1760 | 4.1572 | 1.1760 | 4.1572 | 0. |
| 55395. | 180.46 | 1.1787 | 4.1277 | 1.1787 | 4.1277 | 0. |
| 55401. | 180.44 | 1.1797 | 4.1154 | 1.1797 | 4.1154 | 0. |
| 55407. | 180.42 | 1.1792 | 4.1211 | 1.1792 | 4.1211 | 0. |
| 55413. | 180.40 | 1.1788 | 4.1214 | 1.1788 | 4.1214 | 0. |
| 55419. | 180.38 | 1.1790 | 4.1161 | 1.1790 | 4.1161 | 0. |
| 55425. | 180.36 | 1.1807 | 4.1038 | 1.1807 | 4.1038 | 0. |
| 55431. | 180.34 | 1.1826 | 4.0972 | 1.1826 | 4.0972 | 0. |
| 55438. | 180.32 | 1.1825 | 4.1067 | 1.1825 | 4.1067 | 0. |
| 55444. | 180.30 | 1.1817 | 4.1209 | 1.1817 | 4.1209 | 0. |
| 55450. | 180.28 | 1.1812 | 4.1315 | 1.1812 | 4.1315 | 0. |
| 55456. | 180.26 | 1.1813 | 4.1451 | 1.1813 | 4.1451 | 0. |
| 55462. | 180.24 | 1.1816 | 4.1382 | 1.1816 | 4.1382 | 0. |
| 55468. | 180.22 | 1.1800 | 4.1301 | 1.1800 | 4.1301 | 0. |
| 55474. | 180.20 | 1.1778 | 4.1370 | 1.1778 | 4.1370 | 0. |
| 55481. | 180.18 | 1.1768 | 4.1454 | 1.1768 | 4.1454 | 0. |
| 55487. | 180.16 | 1.1765 | 4.1450 | 1.1765 | 4.1450 | 0. |
| 55493. | 180.14 | 1.1761 | 4.1461 | 1.1761 | 4.1461 | 0. |
| 55499. | 180.12 | 1.1749 | 4.1447 | 1.1749 | 4.1447 | 0. |
| 55505. | 180.10 | 1.1738 | 4.1187 | 1.1738 | 4.1187 | 0. |
| 55511. | 180.08 | 1.1737 | 4.0940 | 1.1737 | 4.0940 | 0. |
| 55518. | 180.06 | 1.1742 | 4.0913 | 1.1742 | 4.0913 | 0. |
| 55524. | 180.04 | 1.1753 | 4.0839 | 1.1753 | 4.0839 | 0. |
| 55530. | 180.02 | 1.1780 | 4.0577 | 1.1780 | 4.0577 | 0. |
| 55536. | 180.00 | 1.1824 | 4.0222 | 1.1824 | 4.0222 | 0. |

| WAVENUMBER CM-1 | WAVELENGTH NM | CROSS SECTION X E19, CM-2 | | SECOND ORDER | | (020) |
|--------------------|------------------|---------------------------|--------|--------------|--------|-------|
| | | FIRST ORDER (000) | (010) | (000) | (010) | |
| 55542. | 179.98 | 1.1867 | 4.0001 | 1.1867 | 4.0001 | 0. |
| 55548. | 179.96 | 1.1892 | 4.0086 | 1.1892 | 4.0086 | 0. |
| 55555. | 179.94 | 1.1903 | 4.0155 | 1.1903 | 4.0155 | 0. |
| 55561. | 179.92 | 1.1913 | 4.0055 | 1.1913 | 4.0055 | 0. |
| 55567. | 179.90 | 1.1922 | 4.0073 | 1.1922 | 4.0073 | 0. |
| 55573. | 179.88 | 1.1914 | 4.0215 | 1.1914 | 4.0215 | 0. |
| 55579. | 179.86 | 1.1889 | 4.0225 | 1.1889 | 4.0225 | 0. |
| 55586. | 179.84 | 1.1862 | 4.0147 | 1.1862 | 4.0147 | 0. |
| 55592. | 179.82 | 1.1834 | 4.0122 | 1.1834 | 4.0122 | 0. |
| 55598. | 179.80 | 1.1810 | 3.9950 | 1.1810 | 3.9950 | 0. |
| 55604. | 179.78 | 1.1795 | 3.9590 | 1.1795 | 3.9590 | 0. |
| 55610. | 179.76 | 1.1774 | 3.9319 | 1.1774 | 3.9319 | 0. |
| 55616. | 179.74 | 1.1746 | 3.9302 | 1.1746 | 3.9302 | 0. |
| 55623. | 179.72 | 1.1724 | 3.9277 | 1.1724 | 3.9277 | 0. |
| 55629. | 179.70 | 1.1703 | 3.9092 | 1.1703 | 3.9092 | 0. |
| 55635. | 179.68 | 1.1699 | 3.8857 | 1.1699 | 3.8857 | 0. |
| 55641. | 179.66 | 1.1718 | 3.8505 | 1.1718 | 3.8505 | 0. |
| 55647. | 179.64 | 1.1717 | 3.8089 | 1.1717 | 3.8089 | 0. |
| 55654. | 179.62 | 1.1694 | 3.7839 | 1.1694 | 3.7839 | 0. |
| 55660. | 179.60 | 1.1676 | 3.7731 | 1.1676 | 3.7731 | 0. |
| 55666. | 179.58 | 1.1680 | 3.7528 | 1.1680 | 3.7528 | 0. |
| 55672. | 179.56 | 1.1697 | 3.7326 | 1.1697 | 3.7326 | 0. |
| 55678. | 179.54 | 1.1705 | 3.7279 | 1.1705 | 3.7279 | 0. |
| 55685. | 179.52 | 1.1699 | 3.7152 | 1.1699 | 3.7152 | 0. |
| 55691. | 179.50 | 1.1697 | 3.6904 | 1.1697 | 3.6904 | 0. |
| 55697. | 179.48 | 1.1698 | 3.6793 | 1.1698 | 3.6793 | 0. |
| 55703. | 179.46 | 1.1696 | 3.6862 | 1.1696 | 3.6862 | 0. |
| 55709. | 179.44 | 1.1688 | 3.6964 | 1.1688 | 3.6964 | 0. |
| 55716. | 179.42 | 1.1682 | 3.6973 | 1.1682 | 3.6973 | 0. |
| 55722. | 179.40 | 1.1675 | 3.6886 | 1.1675 | 3.6886 | 0. |
| 55728. | 179.38 | 1.1681 | 3.6685 | 1.1681 | 3.6685 | 0. |
| 55734. | 179.36 | 1.1702 | 3.6351 | 1.1702 | 3.6351 | 0. |
| 55740. | 179.34 | 1.1715 | 3.6176 | 1.1715 | 3.6176 | 0. |
| 55747. | 179.32 | 1.1712 | 3.6268 | 1.1712 | 3.6268 | 0. |
| 55753. | 179.30 | 1.1706 | 3.6381 | 1.1706 | 3.6381 | 0. |
| 55759. | 179.28 | 1.1701 | 3.6446 | 1.1701 | 3.6446 | 0. |
| 55765. | 179.26 | 1.1696 | 3.6512 | 1.1696 | 3.6512 | 0. |
| 55772. | 179.24 | 1.1708 | 3.6399 | 1.1708 | 3.6399 | 0. |
| 55778. | 179.22 | 1.1723 | 3.6305 | 1.1723 | 3.6305 | 0. |
| 55784. | 179.20 | 1.1717 | 3.6472 | 1.1717 | 3.6472 | 0. |
| 55790. | 179.18 | 1.1711 | 3.6457 | 1.1711 | 3.6457 | 0. |
| 55797. | 179.16 | 1.1716 | 3.6320 | 1.1716 | 3.6320 | 0. |
| 55803. | 179.14 | 1.1718 | 3.6307 | 1.1718 | 3.6307 | 0. |
| 55809. | 179.12 | 1.1708 | 3.6422 | 1.1708 | 3.6422 | 0. |
| 55815. | 179.10 | 1.1696 | 3.6552 | 1.1696 | 3.6552 | 0. |
| 55821. | 179.08 | 1.1691 | 3.6570 | 1.1691 | 3.6570 | 0. |
| 55828. | 179.06 | 1.1684 | 3.6665 | 1.1684 | 3.6665 | 0. |
| 55834. | 179.04 | 1.1676 | 3.6862 | 1.1676 | 3.6862 | 0. |
| 55840. | 179.02 | 1.1662 | 3.7133 | 1.1662 | 3.7133 | 0. |
| 55846. | 179.00 | 1.1662 | 3.7117 | 1.1662 | 3.7117 | 0. |

| WAVENUMBER CM-1 | WAVELENGTH NM | CROSS SECTION X E19, CM-2 | | | | | |
|--------------------|------------------|---------------------------|---------------------------|-------|--------------------------|----------------|-------|
| | | FIRST ORDER (000) | SECTION ORDER (010) | X E19 | SECOND ORDER (000) | ORDER (010) | (020) |
| 55853. | 178.98 | 1.1679 | 3.6930 | | 1.1679 | 3.6930 | 0. |
| 55859. | 178.96 | 1.1683 | 3.7086 | | 1.1683 | 3.7086 | 0. |
| 55865. | 178.94 | 1.1679 | 3.7328 | | 1.1679 | 3.7328 | 0. |
| 55871. | 178.92 | 1.1673 | 3.7559 | | 1.1673 | 3.7559 | 0. |
| 55878. | 178.90 | 1.1669 | 3.7699 | | 1.1669 | 3.7699 | 0. |
| 55884. | 178.88 | 1.1669 | 3.7833 | | 1.1669 | 3.7833 | 0. |
| 55890. | 178.86 | 1.1669 | 3.8010 | | 1.1669 | 3.8010 | 0. |
| 55896. | 178.84 | 1.1669 | 3.8104 | | 1.1669 | 3.8104 | 0. |
| 55903. | 178.82 | 1.1662 | 3.8256 | | 1.1662 | 3.8256 | 0. |
| 55909. | 178.80 | 1.1640 | 3.8620 | | 1.1640 | 3.8620 | 0. |
| 55915. | 178.78 | 1.1613 | 3.8764 | | 1.1613 | 3.8764 | 0. |
| 55921. | 178.76 | 1.1599 | 3.8764 | | 1.1599 | 3.8764 | 0. |
| 55928. | 178.74 | 1.1595 | 3.9085 | | 1.1595 | 3.9085 | 0. |
| 55934. | 178.72 | 1.1595 | 3.9317 | | 1.1595 | 3.9317 | 0. |
| 55940. | 178.70 | 1.1586 | 3.9306 | | 1.1586 | 3.9306 | 0. |
| 55946. | 178.68 | 1.1586 | 3.9401 | | 1.1586 | 3.9401 | 0. |
| 55953. | 178.66 | 1.1603 | 3.9509 | | 1.1603 | 3.9509 | 0. |
| 55959. | 178.64 | 1.1619 | 3.9496 | | 1.1619 | 3.9496 | 0. |
| 55965. | 178.62 | 1.1627 | 3.9585 | | 1.1627 | 3.9585 | 0. |
| 55971. | 178.60 | 1.1641 | 3.9681 | | 1.1641 | 3.9681 | 0. |
| 55978. | 178.58 | 1.1665 | 3.9581 | | 1.1665 | 3.9581 | 0. |
| 55984. | 178.56 | 1.1681 | 3.9608 | | 1.1681 | 3.9608 | 0. |
| 55990. | 178.54 | 1.1675 | 3.9760 | | 1.1675 | 3.9760 | 0. |
| 55997. | 178.52 | 1.1661 | 3.9768 | | 1.1661 | 3.9768 | 0. |
| 56003. | 178.50 | 1.1649 | 3.9594 | | 1.1649 | 3.9594 | 0. |
| 56009. | 178.48 | 1.1626 | 3.9249 | | 1.1626 | 3.9249 | 0. |
| 56015. | 178.46 | 1.1593 | 3.9099 | | 1.1593 | 3.9099 | 0. |
| 56022. | 178.44 | 1.1570 | 3.8985 | | 1.1570 | 3.8985 | 0. |
| 56028. | 178.42 | 1.1554 | 3.8688 | | 1.1554 | 3.8688 | 0. |
| 56034. | 178.40 | 1.1541 | 3.8321 | | 1.1541 | 3.8321 | 0. |
| 56040. | 178.38 | 1.1517 | 3.8142 | | 1.1517 | 3.8142 | 0. |
| 56047. | 178.36 | 1.1488 | 3.7989 | | 1.1488 | 3.7989 | 0. |
| 56053. | 178.34 | 1.1460 | 3.7836 | | 1.1460 | 3.7836 | 0. |
| 56059. | 178.32 | 1.1421 | 3.7799 | | 1.1421 | 3.7799 | 0. |
| 56066. | 178.30 | 1.1395 | 3.7593 | | 1.1395 | 3.7593 | 0. |
| 56072. | 178.28 | 1.1394 | 3.7257 | | 1.1394 | 3.7257 | 0. |
| 56078. | 178.26 | 1.1406 | 3.6857 | | 1.1406 | 3.6857 | 0. |
| 56084. | 178.24 | 1.1404 | 3.6456 | | 1.1404 | 3.6456 | 0. |
| 56091. | 178.22 | 1.1390 | 3.6122 | | 1.1390 | 3.6122 | 0. |
| 56097. | 178.20 | 1.1389 | 3.5961 | | 1.1389 | 3.5961 | 0. |
| 56103. | 178.18 | 1.1392 | 3.5837 | | 1.1392 | 3.5837 | 0. |
| 56110. | 178.16 | 1.1383 | 3.5588 | | 1.1383 | 3.5588 | 0. |
| 56116. | 178.14 | 1.1367 | 3.5290 | | 1.1367 | 3.5290 | 0. |
| 56122. | 178.12 | 1.1345 | 3.5161 | | 1.1345 | 3.5161 | 0. |
| 56129. | 178.10 | 1.1336 | 3.5103 | | 1.1336 | 3.5103 | 0. |
| 56135. | 178.08 | 1.1336 | 3.5032 | | 1.1336 | 3.5032 | 0. |
| 56141. | 178.06 | 1.1331 | 3.4771 | | 1.1331 | 3.4771 | 0. |
| 56148. | 178.04 | 1.1319 | 3.4502 | | 1.1319 | 3.4502 | 0. |
| 56154. | 178.02 | 1.1299 | 3.4558 | | 1.1299 | 3.4558 | 0. |
| 56160. | 178.00 | 1.1285 | 3.4502 | | 1.1285 | 3.4502 | 0. |

| WAVENUMBER CM-1 | WAVELENGTH NM | CROSS SECTION X E19, CM-2 | | | | |
|--------------------|------------------|---------------------------|----------------|-----------------|----------------|-------|
| | | FIRST (000) | ORDER (010) | SECOND (000) | ORDER (010) | (020) |
| 56166. | 177.98 | 1.1285 | 3.4152 | 1.1285 | 3.4152 | 0. |
| 56173. | 177.96 | 1.1301 | 3.3963 | 1.1301 | 3.3963 | 0. |
| 56179. | 177.94 | 1.1314 | 3.3994 | 1.1314 | 3.3994 | 0. |
| 56185. | 177.92 | 1.1312 | 3.3913 | 1.1312 | 3.3913 | 0. |
| 56192. | 177.90 | 1.1306 | 3.3802 | 1.1306 | 3.3802 | 0. |
| 56198. | 177.88 | 1.1313 | 3.3873 | 1.1313 | 3.3873 | 0. |
| 56204. | 177.86 | 1.1337 | 3.3695 | 1.1337 | 3.3695 | 0. |
| 56211. | 177.84 | 1.1346 | 3.3482 | 1.1346 | 3.3482 | 0. |
| 56217. | 177.82 | 1.1345 | 3.3592 | 1.1345 | 3.3592 | 0. |
| 56223. | 177.80 | 1.1350 | 3.3686 | 1.1350 | 3.3686 | 0. |
| 56230. | 177.78 | 1.1356 | 3.3923 | 1.1356 | 3.3923 | 0. |
| 56236. | 177.76 | 1.1351 | 3.4261 | 1.1351 | 3.4261 | 0. |
| 56242. | 177.74 | 1.1340 | 3.4534 | 1.1340 | 3.4534 | 0. |
| 56249. | 177.72 | 1.1333 | 3.4837 | 1.1333 | 3.4837 | 0. |
| 56255. | 177.70 | 1.1342 | 3.4887 | 1.1342 | 3.4887 | 0. |
| 56261. | 177.68 | 1.1348 | 3.4742 | 1.1348 | 3.4742 | 0. |
| 56268. | 177.66 | 1.1346 | 3.4692 | 1.1346 | 3.4693 | 0. |
| 56274. | 177.64 | 1.1349 | 3.4569 | 1.1349 | 3.4569 | 0. |
| 56280. | 177.62 | 1.1360 | 3.4566 | 1.1360 | 3.4566 | 0. |
| 56287. | 177.60 | 1.1353 | 3.4956 | 1.1353 | 3.4956 | 0. |
| 56293. | 177.58 | 1.1336 | 3.5374 | 1.1336 | 3.5374 | 0. |
| 56299. | 177.56 | 1.1322 | 3.5700 | 1.1322 | 3.5700 | 0. |
| 56306. | 177.54 | 1.1312 | 3.6205 | 1.1312 | 3.6205 | 0. |
| 56312. | 177.52 | 1.1289 | 3.6895 | 1.1289 | 3.6895 | 0. |
| 56318. | 177.50 | 1.1269 | 3.7382 | 1.1269 | 3.7382 | 0. |
| 56325. | 177.48 | 1.1271 | 3.7679 | 1.1271 | 3.7679 | 0. |
| 56331. | 177.46 | 1.1280 | 3.8016 | 1.1280 | 3.8016 | 0. |
| 56337. | 177.44 | 1.1280 | 3.8287 | 1.1280 | 3.8287 | 0. |
| 56344. | 177.42 | 1.1265 | 3.8500 | 1.1265 | 3.8500 | 0. |
| 56350. | 177.40 | 1.1268 | 3.8519 | 1.1268 | 3.8519 | 0. |
| 56356. | 177.38 | 1.1275 | 3.8687 | 1.1275 | 3.8687 | 0. |
| 56363. | 177.36 | 1.1264 | 3.8953 | 1.1264 | 3.8953 | 0. |
| 56369. | 177.34 | 1.1248 | 3.9006 | 1.1248 | 3.9006 | 0. |
| 56375. | 177.32 | 1.1246 | 3.8892 | 1.1246 | 3.8892 | 0. |
| 56382. | 177.30 | 1.1243 | 3.8929 | 1.1243 | 3.8929 | 0. |
| 56388. | 177.28 | 1.1228 | 3.8784 | 1.1228 | 3.8784 | 0. |
| 56395. | 177.26 | 1.1219 | 3.8558 | 1.1219 | 3.8558 | 0. |
| 56401. | 177.24 | 1.1221 | 3.8544 | 1.1221 | 3.8544 | 0. |
| 56407. | 177.22 | 1.1232 | 3.8326 | 1.1232 | 3.8326 | 0. |
| 56414. | 177.20 | 1.1223 | 3.7981 | 1.1223 | 3.7981 | 0. |
| 56420. | 177.18 | 1.1206 | 3.7834 | 1.1206 | 3.7834 | 0. |
| 56426. | 177.16 | 1.1201 | 3.7812 | 1.1201 | 3.7812 | 0. |
| 56433. | 177.14 | 1.1210 | 3.7576 | 1.1210 | 3.7576 | 0. |
| 56439. | 177.12 | 1.1221 | 3.7270 | 1.1221 | 3.7270 | 0. |
| 56446. | 177.10 | 1.1223 | 3.7097 | 1.1223 | 3.7097 | 0. |
| 56452. | 177.08 | 1.1212 | 3.6997 | 1.1212 | 3.6997 | 0. |
| 56458. | 177.06 | 1.1206 | 3.6910 | 1.1206 | 3.6910 | 0. |
| 56465. | 177.04 | 1.1209 | 3.6786 | 1.1209 | 3.6786 | 0. |
| 56471. | 177.02 | 1.1221 | 3.6721 | 1.1221 | 3.6721 | 0. |
| 56477. | 177.00 | 1.1222 | 3.6650 | 1.1222 | 3.6650 | 0. |

| WAVENUMBER CM-1 | WAVELENGTH NM | CROSS SECTION X E19 | | CM-2 | | (020) |
|--------------------|------------------|-------------------------|----------------|--------------------------|----------------|-------|
| | | FIRST ORDER (000) | ORDER (010) | SECOND ORDER (000) | ORDER (010) | |
| 56484. | 176.98 | 1.1225 | 3.6478 | 1.1225 | 3.6478 | 0. |
| 56490. | 176.96 | 1.1246 | 3.6344 | 1.1246 | 3.6344 | 0. |
| 56497. | 176.94 | 1.1280 | 3.6097 | 1.1280 | 3.6097 | 0. |
| 56503. | 176.92 | 1.1296 | 3.5829 | 1.1296 | 3.5829 | 0. |
| 56509. | 176.90 | 1.1293 | 3.5594 | 1.1293 | 3.5594 | 0. |
| 56516. | 176.88 | 1.1294 | 3.5405 | 1.1294 | 3.5405 | 0. |
| 56522. | 176.86 | 1.1295 | 3.5326 | 1.1295 | 3.5326 | 0. |
| 56529. | 176.84 | 1.1296 | 3.5160 | 1.1296 | 3.5160 | 0. |
| 56535. | 176.82 | 1.1291 | 3.4883 | 1.1291 | 3.4883 | 0. |
| 56541. | 176.80 | 1.1275 | 3.4681 | 1.1275 | 3.4681 | 0. |
| 56548. | 176.78 | 1.1258 | 3.4478 | 1.1258 | 3.4478 | 0. |
| 56554. | 176.76 | 1.1242 | 3.4102 | 1.1242 | 3.4102 | 0. |
| 56560. | 176.74 | 1.1227 | 3.3725 | 1.1227 | 3.3725 | 0. |
| 56567. | 176.72 | 1.1207 | 3.3598 | 1.1207 | 3.3598 | 0. |
| 56573. | 176.70 | 1.1178 | 3.3509 | 1.1178 | 3.3509 | 0. |
| 56580. | 176.68 | 1.1154 | 3.3338 | 1.1154 | 3.3338 | 0. |
| 56586. | 176.66 | 1.1154 | 3.2979 | 1.1154 | 3.2979 | 0. |
| 56593. | 176.64 | 1.1139 | 3.2547 | 1.1139 | 3.2547 | 0. |
| 56599. | 176.62 | 1.1112 | 3.2316 | 1.1112 | 3.2316 | 0. |
| 56605. | 176.60 | 1.1095 | 3.2392 | 1.1095 | 3.2392 | 0. |
| 56612. | 176.58 | 1.1081 | 3.2297 | 1.1081 | 3.2297 | 0. |
| 56618. | 176.56 | 1.1053 | 3.2128 | 1.1053 | 3.2128 | 0. |
| 56625. | 176.54 | 1.1023 | 3.1941 | 1.1023 | 3.1941 | 0. |
| 56631. | 176.52 | 1.0998 | 3.1864 | 1.0998 | 3.1864 | 0. |
| 56637. | 176.50 | 1.0976 | 3.2006 | 1.0976 | 3.2006 | 0. |
| 56644. | 176.48 | 1.0946 | 3.2106 | 1.0946 | 3.2106 | 0. |
| 56650. | 176.46 | 1.0925 | 3.1995 | 1.0925 | 3.1995 | 0. |
| 56657. | 176.44 | 1.0922 | 3.1887 | 1.0922 | 3.1887 | 0. |
| 56663. | 176.42 | 1.0906 | 3.1940 | 1.0906 | 3.1940 | 0. |
| 56670. | 176.40 | 1.0874 | 3.1871 | 1.0874 | 3.1871 | 0. |
| 56676. | 176.38 | 1.0848 | 3.1689 | 1.0848 | 3.1689 | 0. |
| 56682. | 176.36 | 1.0849 | 3.1579 | 1.0849 | 3.1579 | 0. |
| 56689. | 176.34 | 1.0856 | 3.1531 | 1.0856 | 3.1531 | 0. |
| 56695. | 176.32 | 1.0850 | 3.1460 | 1.0850 | 3.1460 | 0. |
| 56702. | 176.30 | 1.0815 | 3.1594 | 1.0815 | 3.1594 | 0. |
| 56708. | 176.28 | 1.0805 | 3.1670 | 1.0805 | 3.1670 | 0. |
| 56715. | 176.26 | 1.0819 | 3.1512 | 1.0819 | 3.1512 | 0. |
| 56721. | 176.24 | 1.0829 | 3.1357 | 1.0829 | 3.1357 | 0. |
| 56727. | 176.22 | 1.0825 | 3.1439 | 1.0825 | 3.1439 | 0. |
| 56734. | 176.20 | 1.0828 | 3.1522 | 1.0828 | 3.1522 | 0. |
| 56740. | 176.18 | 1.0840 | 3.1576 | 1.0840 | 3.1576 | 0. |
| 56747. | 176.16 | 1.0844 | 3.1588 | 1.0844 | 3.1588 | 0. |
| 56753. | 176.14 | 1.0835 | 3.1594 | 1.0835 | 3.1594 | 0. |
| 56760. | 176.12 | 1.0823 | 3.1628 | 1.0823 | 3.1628 | 0. |
| 56766. | 176.10 | 1.0821 | 3.1721 | 1.0821 | 3.1721 | 0. |
| 56772. | 176.08 | 1.0825 | 3.1710 | 1.0825 | 3.1710 | 0. |
| 56779. | 176.06 | 1.0858 | 3.1589 | 1.0858 | 3.1589 | 0. |
| 56785. | 176.04 | 1.0915 | 3.1337 | 1.0916 | 3.1169 | .1189 |
| 56792. | 176.02 | 1.0925 | 3.1564 | 1.0925 | 3.1451 | .0795 |
| 56798. | 176.00 | 1.0910 | 3.2001 | 1.0910 | 3.2001 | 0. |

| WAVENUMBER CM-1 | WAVELENGTH NM | CROSS SECTION X E19 | | CM-2 | | |
|--------------------|------------------|-------------------------|----------------|--------------------------|----------------|-------|
| | | FIRST ORDER (000) | ORDER (010) | SECOND ORDER (000) | ORDER (010) | (020) |
| 56805. | 175.98 | 1.0901 | 3.2261 | 1.0901 | 3.2261 | 0. |
| 56811. | 175.96 | 1.0914 | 3.2268 | 1.0914 | 3.2268 | 0. |
| 56818. | 175.94 | 1.0949 | 3.2284 | 1.0949 | 3.2284 | 0. |
| 56824. | 175.92 | 1.0971 | 3.2398 | 1.0971 | 3.2398 | 0. |
| 56831. | 175.90 | 1.0979 | 3.2543 | 1.0979 | 3.2543 | 0. |
| 56837. | 175.88 | 1.0971 | 3.2708 | 1.0971 | 3.2708 | 0. |
| 56844. | 175.86 | 1.0964 | 3.2804 | 1.0964 | 3.2783 | .0150 |
| 56850. | 175.84 | 1.0964 | 3.2804 | 1.0965 | 3.2664 | .0994 |
| 56856. | 175.82 | 1.0967 | 3.2896 | 1.0968 | 3.2735 | .1139 |
| 56863. | 175.80 | 1.0965 | 3.3180 | 1.0965 | 3.3143 | .0259 |
| 56869. | 175.78 | 1.0947 | 3.3461 | 1.0947 | 3.3461 | 0. |
| 56876. | 175.76 | 1.0925 | 3.3667 | 1.0925 | 3.3667 | 0. |
| 56882. | 175.74 | 1.0905 | 3.3922 | 1.0905 | 3.3922 | 0. |
| 56889. | 175.72 | 1.0880 | 3.4195 | 1.0880 | 3.4195 | 0. |
| 56895. | 175.70 | 1.0848 | 3.4429 | 1.0848 | 3.4429 | 0. |
| 56902. | 175.68 | 1.0812 | 3.4752 | 1.0812 | 3.4752 | 0. |
| 56908. | 175.66 | 1.0789 | 3.5116 | 1.0789 | 3.5116 | 0. |
| 56915. | 175.64 | 1.0781 | 3.5163 | 1.0781 | 3.5163 | 0. |
| 56921. | 175.62 | 1.0753 | 3.5074 | 1.0753 | 3.5074 | 0. |
| 56928. | 175.60 | 1.0695 | 3.5078 | 1.0695 | 3.5078 | 0. |
| 56934. | 175.58 | 1.0648 | 3.4943 | 1.0648 | 3.4943 | 0. |
| 56941. | 175.56 | 1.0643 | 3.4340 | 1.0643 | 3.4340 | 0. |
| 56947. | 175.54 | 1.0657 | 3.3687 | 1.0657 | 3.3687 | 0. |
| 56954. | 175.52 | 1.0653 | 3.3237 | 1.0653 | 3.3237 | 0. |
| 56960. | 175.50 | 1.0618 | 3.3140 | 1.0618 | 3.3140 | 0. |
| 56967. | 175.48 | 1.0576 | 3.3242 | 1.0576 | 3.3242 | 0. |
| 56973. | 175.46 | 1.0553 | 3.2968 | 1.0553 | 3.2968 | 0. |
| 56980. | 175.44 | 1.0532 | 3.2594 | 1.0532 | 3.2594 | 0. |
| 56986. | 175.42 | 1.0525 | 3.2346 | 1.0525 | 3.2346 | 0. |
| 56993. | 175.40 | 1.0535 | 3.1960 | 1.0535 | 3.1960 | 0. |
| 56999. | 175.38 | 1.0544 | 3.1668 | 1.0544 | 3.1668 | 0. |
| 57006. | 175.36 | 1.0558 | 3.1325 | 1.0558 | 3.1325 | 0. |
| 57012. | 175.34 | 1.0578 | 3.0815 | 1.0578 | 3.0815 | 0. |
| 57019. | 175.32 | 1.0578 | 3.0528 | 1.0578 | 3.0528 | 0. |
| 57025. | 175.30 | 1.0527 | 3.0788 | 1.0527 | 3.0788 | 0. |
| 57032. | 175.28 | 1.0469 | 3.0942 | 1.0469 | 3.0942 | 0. |
| 57038. | 175.26 | 1.0442 | 3.0569 | 1.0442 | 3.0569 | 0. |
| 57045. | 175.24 | 1.0435 | 3.0322 | 1.0435 | 3.0322 | 0. |
| 57051. | 175.22 | 1.0438 | 3.0213 | 1.0438 | 3.0213 | 0. |
| 57058. | 175.20 | 1.0431 | 2.9879 | 1.0431 | 2.9879 | 0. |
| 57064. | 175.18 | 1.0412 | 2.9613 | 1.0412 | 2.9618 | 0. |
| 57071. | 175.16 | 1.0396 | 2.9631 | 1.0396 | 2.9631 | 0. |
| 57077. | 175.14 | 1.0373 | 2.9779 | 1.0373 | 2.9779 | 0. |
| 57084. | 175.12 | 1.0361 | 2.9686 | 1.0361 | 2.9686 | 0. |
| 57090. | 175.10 | 1.0364 | 2.9322 | 1.0364 | 2.9322 | 0. |
| 57097. | 175.08 | 1.0355 | 2.8962 | 1.0355 | 2.8962 | 0. |
| 57103. | 175.06 | 1.0347 | 2.8578 | 1.0347 | 2.8578 | 0. |
| 57110. | 175.04 | 1.0359 | 2.8194 | 1.0359 | 2.8194 | 0. |
| 57116. | 175.02 | 1.0368 | 2.8149 | 1.0368 | 2.8149 | 0. |
| 57123. | 175.00 | 1.0342 | 2.8286 | 1.0342 | 2.8286 | 0. |

| WAVENUMBER CM-1 | WAVELENGTH NM | CROSS SECTION X E19, CM-2 | | SECOND ORDER | | |
|--------------------|------------------|---------------------------|--------|--------------|--------|-------|
| | | FIRST ORDER (000) | (010) | (000) | (010) | (020) |
| 57129. | 174.98 | 1.0312 | 2.8259 | 1.0312 | 2.8259 | 0. |
| 57136. | 174.96 | 1.0310 | 2.7978 | 1.0310 | 2.7978 | 0. |
| 57142. | 174.94 | 1.0309 | 2.7801 | 1.0310 | 2.7787 | .0099 |
| 57149. | 174.92 | 1.0316 | 2.7777 | 1.0317 | 2.7629 | .1045 |
| 57156. | 174.90 | 1.0330 | 2.7683 | 1.0333 | 2.7359 | .2289 |
| 57162. | 174.88 | 1.0315 | 2.7585 | 1.0319 | 2.7083 | .3554 |
| 57169. | 174.86 | 1.0282 | 2.7642 | 1.0286 | 2.7079 | .3985 |
| 57175. | 174.84 | 1.0257 | 2.8138 | 1.0258 | 2.7926 | .1501 |
| 57182. | 174.82 | 1.0208 | 2.8758 | 1.0208 | 2.8758 | 0. |
| 57188. | 174.80 | 1.0188 | 2.8758 | 1.0188 | 2.8758 | 0. |
| 57195. | 174.78 | 1.0206 | 2.8421 | 1.0208 | 2.8103 | .2252 |
| 57201. | 174.76 | 1.0213 | 2.8469 | 1.0217 | 2.7914 | .3929 |
| 57208. | 174.74 | 1.0207 | 2.8837 | 1.0210 | 2.8383 | .3206 |
| 57214. | 174.72 | 1.0194 | 2.9155 | 1.0196 | 2.8847 | .2183 |
| 57221. | 174.70 | 1.0171 | 2.9464 | 1.0173 | 2.9214 | .1769 |
| 57228. | 174.68 | 1.0140 | 2.9912 | 1.0142 | 2.9666 | .1742 |
| 57234. | 174.66 | 1.0125 | 3.0197 | 1.0126 | 2.9954 | .1719 |
| 57241. | 174.64 | 1.0115 | 3.0289 | 1.0116 | 3.0134 | .1100 |
| 57247. | 174.62 | 1.0099 | 3.0263 | 1.0100 | 3.0064 | .1406 |
| 57254. | 174.60 | 1.0093 | 3.0081 | 1.0097 | 2.9496 | .4139 |
| 57260. | 174.58 | 1.0104 | 3.0110 | 1.0110 | 2.9305 | .5697 |
| 57267. | 174.56 | 1.0110 | 3.0578 | 1.0114 | 2.9969 | .4308 |
| 57273. | 174.54 | 1.0113 | 3.1123 | 1.0115 | 3.0808 | .2230 |
| 57280. | 174.52 | 1.0127 | 3.1355 | 1.0130 | 3.1032 | .2287 |
| 57287. | 174.50 | 1.0141 | 3.1356 | 1.0145 | 3.0786 | .4031 |
| 57293. | 174.48 | 1.0124 | 3.1582 | 1.0128 | 3.0907 | .4772 |
| 57300. | 174.46 | 1.0097 | 3.2115 | 1.0100 | 3.1604 | .3620 |
| 57306. | 174.44 | 1.0083 | 3.2689 | 1.0085 | 3.2430 | .1835 |
| 57313. | 174.42 | 1.0054 | 3.3300 | 1.0054 | 3.3300 | 0. |
| 57319. | 174.40 | 1.0032 | 3.3816 | 1.0032 | 3.3816 | 0. |
| 57326. | 174.38 | 1.0043 | 3.4020 | 1.0043 | 3.4020 | 0. |
| 57333. | 174.36 | 1.0081 | 3.3898 | 1.0081 | 3.3898 | 0. |
| 57339. | 174.34 | 1.0104 | 3.3574 | 1.0104 | 3.3574 | 0. |
| 57346. | 174.32 | 1.0104 | 3.3342 | 1.0104 | 3.3342 | 0. |
| 57352. | 174.30 | 1.0099 | 3.3297 | 1.0099 | 3.3297 | 0. |
| 57359. | 174.28 | 1.0093 | 3.3266 | 1.0093 | 3.3266 | 0. |
| 57365. | 174.26 | 1.0081 | 3.3252 | 1.0081 | 3.3252 | 0. |
| 57372. | 174.24 | 1.0074 | 3.3276 | 1.0074 | 3.3276 | 0. |
| 57379. | 174.22 | 1.0082 | 3.3079 | 1.0082 | 3.3079 | 0. |
| 57385. | 174.20 | 1.0104 | 3.2594 | 1.0104 | 3.2594 | 0. |
| 57392. | 174.18 | 1.0131 | 3.2331 | 1.0131 | 3.2331 | 0. |
| 57398. | 174.16 | 1.0146 | 3.2253 | 1.0146 | 3.2253 | 0. |
| 57405. | 174.14 | 1.0138 | 3.2084 | 1.0138 | 3.2084 | 0. |
| 57412. | 174.12 | 1.0133 | 3.2023 | 1.0133 | 3.2023 | 0. |
| 57418. | 174.10 | 1.0133 | 3.2118 | 1.0133 | 3.2118 | 0. |
| 57425. | 174.08 | 1.0130 | 3.2211 | 1.0130 | 3.2211 | 0. |
| 57431. | 174.06 | 1.0145 | 3.2037 | 1.0145 | 3.2037 | 0. |
| 57438. | 174.04 | 1.0177 | 3.1771 | 1.0177 | 3.1771 | 0. |
| 57445. | 174.02 | 1.0187 | 3.1576 | 1.0187 | 3.1576 | 0. |
| 57451. | 174.00 | 1.0186 | 3.1240 | 1.0186 | 3.1240 | 0. |

| WAVENUMBER CM-1 | WAVELENGTH NM | CROSS SECTION X E19 | | CM-2 | | |
|--------------------|------------------|---------------------|----------------|-----------------|----------------|-------|
| | | FIRST (000) | ORDER (010) | SECOND (000) | ORDER (010) | (020) |
| 57458. | 173.98 | 1.0166 | 3.1002 | 1.0166 | 3.1002 | 0. |
| 57464. | 173.96 | 1.0115 | 3.1149 | 1.0115 | 3.1149 | 0. |
| 57471. | 173.94 | 1.0080 | 3.1204 | 1.0080 | 3.1204 | 0. |
| 57478. | 173.92 | 1.0060 | 3.1149 | 1.0060 | 3.1149 | 0. |
| 57484. | 173.90 | 1.0025 | 3.1084 | 1.0025 | 3.1084 | 0. |
| 57491. | 173.88 | .9986 | 3.0767 | .9986 | 3.0767 | 0. |
| 57497. | 173.86 | .9977 | 3.0064 | .9977 | 3.0064 | 0. |
| 57504. | 173.84 | .9963 | 2.9658 | .9963 | 2.9658 | 0. |
| 57511. | 173.82 | .9906 | 3.0021 | .9906 | 3.0021 | 0. |
| 57517. | 173.80 | .9837 | 3.0371 | .9837 | 3.0371 | 0. |
| 57524. | 173.78 | .9778 | 3.0294 | .9778 | 3.0294 | 0. |
| 57531. | 173.76 | .9748 | 3.0027 | .9748 | 3.0027 | 0. |
| 57537. | 173.74 | .9769 | 2.9336 | .9769 | 2.9336 | 0. |
| 57544. | 173.72 | .9793 | 2.8583 | .9793 | 2.8583 | 0. |
| 57550. | 173.70 | .9788 | 2.8561 | .9788 | 2.8561 | 0. |
| 57557. | 173.68 | .9791 | 2.8541 | .9791 | 2.8541 | 0. |
| 57564. | 173.66 | .9788 | 2.8306 | .9788 | 2.8306 | 0. |
| 57570. | 173.64 | .9778 | 2.8191 | .9778 | 2.8191 | 0. |
| 57577. | 173.62 | .9732 | 2.8480 | .9732 | 2.8480 | 0. |
| 57584. | 173.60 | .9690 | 2.8582 | .9690 | 2.8582 | 0. |
| 57590. | 173.58 | .9685 | 2.8361 | .9685 | 2.8361 | 0. |
| 57597. | 173.56 | .9685 | 2.8050 | .9685 | 2.8050 | 0. |
| 57603. | 173.54 | .9686 | 2.7541 | .9686 | 2.7541 | 0. |
| 57610. | 173.52 | .9704 | 2.7244 | .9704 | 2.7244 | 0. |
| 57617. | 173.50 | .9696 | 2.7402 | .9696 | 2.7402 | 0. |
| 57623. | 173.48 | .9660 | 2.7552 | .9660 | 2.7552 | 0. |
| 57630. | 173.46 | .9645 | 2.7415 | .9645 | 2.7415 | 0. |
| 57637. | 173.44 | .9654 | 2.7162 | .9654 | 2.7162 | 0. |
| 57643. | 173.42 | .9619 | 2.7328 | .9619 | 2.7328 | 0. |
| 57650. | 173.40 | .9595 | 2.7427 | .9595 | 2.7427 | 0. |
| 57657. | 173.38 | .9618 | 2.7096 | .9618 | 2.7096 | 0. |
| 57663. | 173.36 | .9644 | 2.6768 | .9644 | 2.6768 | 0. |
| 57670. | 173.34 | .9661 | 2.6621 | .9661 | 2.6621 | 0. |
| 57677. | 173.32 | .9670 | 2.6718 | .9670 | 2.6718 | 0. |
| 57683. | 173.30 | .9658 | 2.7008 | .9658 | 2.7008 | 0. |
| 57690. | 173.28 | .9625 | 2.7399 | .9625 | 2.7399 | 0. |
| 57697. | 173.26 | .9575 | 2.7738 | .9575 | 2.7738 | 0. |
| 57703. | 173.24 | .9526 | 2.7943 | .9526 | 2.7943 | 0. |
| 57710. | 173.22 | .9526 | 2.7521 | .9526 | 2.7521 | 0. |
| 57717. | 173.20 | .9581 | 2.6790 | .9581 | 2.6790 | 0. |
| 57723. | 173.18 | .9639 | 2.6825 | .9639 | 2.6825 | 0. |
| 57730. | 173.16 | .9653 | 2.7391 | .9653 | 2.7391 | 0. |
| 57737. | 173.14 | .9648 | 2.7450 | .9648 | 2.7450 | 0. |
| 57743. | 173.12 | .9661 | 2.7170 | .9661 | 2.7170 | 0. |
| 57750. | 173.10 | .9679 | 2.6968 | .9679 | 2.6968 | 0. |
| 57757. | 173.08 | .9653 | 2.7273 | .9653 | 2.7273 | 0. |
| 57763. | 173.06 | .9602 | 2.7818 | .9602 | 2.7818 | 0. |
| 57770. | 173.04 | .9590 | 2.8114 | .9590 | 2.8114 | 0. |
| 57777. | 173.02 | .9607 | 2.8699 | .9607 | 2.8699 | 0. |
| 57783. | 173.00 | .9605 | 2.9254 | .9605 | 2.9254 | 0. |

| WAVENUMBER CM-1 | WAVELENGTH NM | CROSS SECTION X E19, CM-2 | | SECOND ORDER | | |
|--------------------|------------------|---------------------------|--------|--------------|--------|--------|
| | | FIRST ORDER (000) | (010) | (000) | (010) | (020) |
| 57790. | 172.98 | .9607 | 2.9162 | .9607 | 2.9162 | 0. |
| 57797. | 172.96 | .9613 | 2.9097 | .9613 | 2.9097 | 0. |
| 57803. | 172.94 | .9598 | 2.8896 | .9598 | 2.8896 | 0. |
| 57810. | 172.92 | .9615 | 2.8494 | .9615 | 2.8494 | 0. |
| 57817. | 172.90 | .9642 | 2.9195 | .9642 | 2.9195 | 0. |
| 57823. | 172.88 | .9657 | 3.0271 | .9657 | 3.0271 | 0. |
| 57830. | 172.86 | .9697 | 2.9903 | .9697 | 2.9903 | 0. |
| 57837. | 172.84 | .9751 | 2.8740 | .9751 | 2.8740 | 0. |
| 57843. | 172.82 | .9736 | 2.8508 | .9736 | 2.8508 | 0. |
| 57850. | 172.80 | .9658 | 2.9173 | .9658 | 2.9173 | 0. |
| 57857. | 172.78 | .9603 | 2.9468 | .9603 | 2.9468 | 0. |
| 57864. | 172.76 | .9558 | 2.9383 | .9558 | 2.9383 | 0. |
| 57870. | 172.74 | .9492 | 2.9719 | .9492 | 2.9719 | 0. |
| 57877. | 172.72 | .9455 | 3.0298 | .9455 | 3.0298 | 0. |
| 57884. | 172.70 | .9444 | 3.0332 | .9444 | 3.0332 | 0. |
| 57890. | 172.68 | .9435 | 2.9534 | .9435 | 2.9534 | 0. |
| 57897. | 172.66 | .9410 | 2.8987 | .9410 | 2.8987 | 0. |
| 57904. | 172.64 | .9341 | 2.9862 | .9341 | 2.9862 | 0. |
| 57910. | 172.62 | .9272 | 3.0370 | .9272 | 3.0370 | 0. |
| 57917. | 172.60 | .9267 | 2.8899 | .9267 | 2.8899 | 0. |
| 57924. | 172.58 | .9294 | 2.7982 | .9294 | 2.7982 | 0. |
| 57931. | 172.56 | .9310 | 2.8662 | .9310 | 2.8662 | 0. |
| 57937. | 172.54 | .9299 | 2.8824 | .9299 | 2.8824 | 0. |
| 57944. | 172.52 | .9237 | 2.8506 | .9237 | 2.8506 | 0. |
| 57951. | 172.50 | .9145 | 2.8605 | .9145 | 2.8605 | 0. |
| 57957. | 172.48 | .9077 | 2.9091 | .9077 | 2.9091 | 0. |
| 57964. | 172.46 | .9046 | 2.9557 | .9046 | 2.9557 | 0. |
| 57971. | 172.44 | .9057 | 2.8860 | .9057 | 2.8860 | 0. |
| 57978. | 172.42 | .9121 | 2.7175 | .9121 | 2.7175 | 0. |
| 57984. | 172.40 | .9178 | 2.6365 | .9178 | 2.6365 | 0. |
| 57991. | 172.38 | .9199 | 2.6860 | .9199 | 2.6860 | 0. |
| 57998. | 172.36 | .9197 | 2.7694 | .9197 | 2.7694 | 0. |
| 58005. | 172.34 | .9197 | 2.7710 | .9197 | 2.7710 | 0. |
| 58011. | 172.32 | .9215 | 2.7429 | .9215 | 2.7429 | 0. |
| 58018. | 172.30 | .9176 | 2.7805 | .9176 | 2.7805 | 0. |
| 58025. | 172.28 | .9098 | 2.8120 | .9098 | 2.8120 | 0. |
| 58031. | 172.26 | .9094 | 2.7764 | .9094 | 2.7764 | 0. |
| 58038. | 172.24 | .9146 | 2.7547 | .9146 | 2.7547 | 0. |
| 58045. | 172.22 | .9168 | 2.7421 | .9168 | 2.7421 | 0. |
| 58052. | 172.20 | .9184 | 2.6723 | .9184 | 2.6723 | 0. |
| 58058. | 172.18 | .9206 | 2.5984 | .9206 | 2.5984 | 0. |
| 58065. | 172.16 | .9201 | 2.5868 | .9201 | 2.5868 | 0. |
| 58072. | 172.14 | .9167 | 2.6847 | .9167 | 2.6847 | 0. |
| 58079. | 172.12 | .9163 | 2.7089 | .9163 | 2.7089 | 0. |
| 58085. | 172.10 | .9164 | 2.6015 | .9164 | 2.6015 | 0. |
| 58092. | 172.08 | .9135 | 2.5814 | .9135 | 2.5814 | 0. |
| 58099. | 172.06 | .9136 | 2.6699 | .9136 | 2.6699 | 0. |
| 58106. | 172.04 | .9149 | 2.7813 | .9149 | 2.7813 | 0. |
| 58112. | 172.02 | .9126 | 2.8017 | .9126 | 2.8017 | 0. |
| 190. | .00 | 4.0381 | .8435 | 3.6517 | 2.7340 | 52613. |

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FIGURE CAPTIONS

- Figure 1 Optical arrangement of spectrometer, mirror housing and gas cell.
- Figure 2 ——— results of Bates and Hays¹²
○○○○○ this study
----- approximate Rayleigh scattering of N₂O
- Figure 3 Result of Sporer and Bohner, microphotometer tracing; C, 5 atmospheres N₂O; B, 1.5 atmospheres N₂O; A, vacuum baseline.
- Figure 4 Shorter wavelength absorption of N₂O.
○○○○ this study
—— Bates and Hays¹²
- Figure 5 Rate of N₂O destruction, j, vs altitude, Km.
—— this study
---- Bates and Hays¹²
- Figure 6 Schematic drawing of the stainless steel cell.
- Figure 7 Cross section, cm² x 10²¹ vs wavelength, nm, for five temperatures,
—— this work, Δ data points of Zelikoff et al¹⁰. Note the discontinuity at 210 nm due to two different "room temperatures." The estimated standard deviation of wavelength (± 0.04 nm) and cross section (± 2%) is indicated by the cross on the 263 K curve. Resolution 0.7 nm.
- Figure 8 Absorption spectrum of N₂O from Zelikoff et al¹⁰. Note the bulges superimposed on the absorption continuum.

- Figure 9 High resolution spectrum in the structured region. Cross section, $\text{cm}^2 \times 10^{19}$, vs wavelength, nm. Temperature = 302 K. Pressure is 44 torr N_2O . Resolution 0.075 nm. Compare the structuring observed here with Figure 8.
- Figure 10 Relative rotational populations vs J quantum number for three different temperatures of N_2O .
- Figure 11 Relative vibrational state population vs temperature, K, for N_2O .
- Figure 12 In the vibronically induced case on the right, transitions are allowed; otherwise all transitions are parity forbidden.
- Figure 13 Vibronically induced transitions from ν_2'' (0 or 1) in the ground electronic state to upper level vibrations of ν_2 in the upper state.
- Figure 14 Quartz cell design.
- Figure 15 Absorption spectrum of N_2O at 11 different temperatures. Axes in this and all following figures are cross section (CSN) $\times 10^{-19} \text{ cm}^2$ vs wavenumber, cm^{-1} . Temperatures are 151, 182, 196, 223, 243, 268, 301, 303, 372, 423 and 485 K.
- Figure 16 Densitometer tracing of plate exposure on the 3m spectrograph, in the region of structuring of N_2O .
- Figure 17 Results of first order deconvolution into the (000) and (010) state spectra. Axes are cross section (CSN) $\times 10^{-19} \text{ cm}^2$ vs wavenumbers, cm^{-1} , corrected for vacuum.

- Figure 18 Comparison of observed spectra (data points) with convoluted spectra (solid lines) for every other temperature studied.
- Figure 19 Results of second order iteration: deconvolution into (000), (010) corrected for higher order vibrations, and the contribution of the higher order vibrations.
- Figure 20a Comparison of observed spectra (data points) with the
20b convoluted spectra using the results of Figure 19 (solid lines) for each temperature.
- Figure 21 Top curve, the absorption spectrum at 151 K; middle curve, an energy-weighted Gaussian curve empirically fit to the data.
- Figure 22 Difference spectrum at 151 K, formed by subtracting the "background absorption" from the observed spectrum. Solid vertical lines denote selected peaks. Downward arrows indicate the progression of 970 cm^{-1} . The difference spectrum is shown at each temperature in Figures 22a-k.
- Figure 23 Histogram of frequency of occurrence of energy spacings between selected peaks vs energy in wavenumbers. Shadings indicate contribution of individual temperatures. Energy separations are in bins of 20 cm^{-1} . See text for details.
- Figure 24 Difference spectrum at 485 K superimposed on the difference spectrum at 151 K. Note the presence of alternate features in the cold spectrum and the presence of consecutive features in the hot spectrum. Scaling is the same for both cases.

- Figure 25 Difference spectrum at 485 K with the calculated peak positions and assignments of ν_2 "(0) and ν_2 " (1) superimposed. ω_2 is presumed to be an odd integer.
- Figure 26 Potential energy diagram in the ν_3 coordinate taken from Figure 8 of reference 106. In this figure the repulsive curve has been relabeled ${}^1\Delta$ in agreement with references 104a, b and 14.
- Figure 27 Figure 26 has been altered to reflect the avoided crossing proposed in C_s symmetry. In parentheses the $C_{\infty v}$ states are shown. Note that the ${}^1A'$ state from ${}^1\Delta$ is unperturbed. The Franck-Condon region is shown by the two vertical lines.
- Figure 28a $N^{15}NO$ at 148, 213, 301, 372, 442 and 503 K.
- Figure 28b ${}^{15}NNO$ at 148, 213, 301, 372, 442 and 503 K.
- Figure 28c ${}^{15}N^{15}NO$ at 148, 213, 301, 372, 442 and 503 K.
- Figure 28d NNO at 148, 213, 301, 372, 442 and 503 K.
- Figure 29a Superposition of first order deconvolution, $NNO/N^{15}NO$ (red-shifted).
- Figure 29b Superposition of first order deconvolution, $NNO/{}^{15}NNO$ (red-shifted).
- Figure 29c Superposition of first order deconvolution, $NNO/{}^{15}N^{15}NO$ (red-shifted).
- Figure 29d Superposition of first order deconvolution, $N^{15}NO/{}^{15}NNO$ (red-shifted).

- Figure 29e Superposition of first order deconvolution, $N^{15}NO/^{15}N^{15}NO$ (red-shifted).
- Figure 29f Superposition of first order deconvolution, $^{15}NNO/^{15}N^{15}NO$ (red-shifted).
- Figure 30a Result of Second Order Deconvolution for $N^{15}NO$.
- Figure 30b Result of Second Order Deconvolution for ^{15}NNO .
- Figure 30c Result of Second Order Deconvolution for $^{15}N^{15}NO$.
- Figure 30d Result of Second Order Deconvolution for Unlabeled NNO .
- Figure 31 Ultraviolet Absorption Spectrum of Contaminated Sample of 95% ^{15}NNO with Reference Beam Containing Equal Pressure of 99% Sample of ^{15}NNO .

Errata

Page No.

- | | | | |
|------|-------------------------------|---|-----|
| viii | line 16 | $l_{\Delta} \leftarrow \chi l_{\Sigma}^{+}$ | |
| 23 | line 2 | $j = \sum_i \sigma_i(\lambda_i) I(y, z, \lambda_i) \phi(\lambda_i)$ | |
| 57 | last word | than | |
| 60 | 4th line from bottom | to be distinguished from Σ^{+}). | |
| 65 | 4th line from bottom | asymmetric | |
| 66 | 4th line | $l_{\Sigma}^{-} \leftarrow l_{\Sigma}^{+}$ | |
| 76 | Equation | $\sum_I Y(I) = \sum_I Y(I-1)/4 + Y(I)/2 + Y(I+1)/4$ | |
| 78 | line 10 | H ₂ : Lyman α , | |
| 78 | line 13 | OCS | |
| 101 | (Table 5) last column, line 3 | | 967 |

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