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TRANSFER BOUNDARY LAYERS

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Authors

McLarnon, F.R.

Muller, R.H.

Tobias, C.W.

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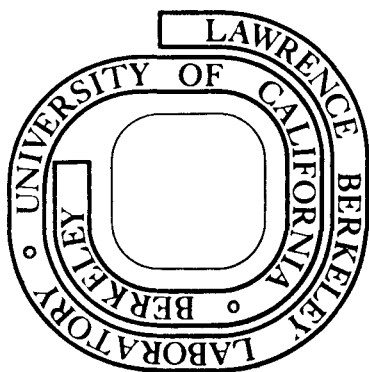
F. R. McLarnon, R. H. Muller and C. W. Tobias

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LIGHT-DEFLECTION ERRORS IN THE INTERFEROMETRY OF ELECTROCHEMICAL
MASS TRANSFER BOUNDARY LAYERS

F. R. McLarnon, R. H. Muller and C. W. Tobias

Inorganic Materials Research Division, Lawrence Berkeley Laboratory and
Department of Chemical Engineering; University of California
Berkeley, California 94720

ABSTRACT

The effect of light-deflection on interferograms of electrochemical mass transfer boundary layers can result in substantial errors if interferograms are interpreted in the conventional way. Corrections in boundary layer thickness, interfacial concentration and interfacial concentration gradient for the convection-free electrodeposition of Cu from aqueous CuSO_4 have been calculated to provide estimates for a wide range of experimental conditions.

Key Words

Interferometry; Refraction; Diffusion; Mass Transfer

INTRODUCTION

Concentration profiles of single solutes in electrolytes near working electrodes can, in principle, be quantitatively observed by interferometric techniques. Such observations are useful in the study of transport processes and in the analysis of different measures designed to provide uniform accessibility and increased reaction rates at electrodes. Some of the advantages of interferometry compared to other means of observing boundary layers and local transport rates are: high resolution for concentration changes (typically 10^{-5} M) and; the possibility of continuous observation without disturbance (e.g., of flow), not restricted to conditions of limiting current.

In the conventional interpretation of interferograms, local changes in the phase depicted by the interferogram are taken as a direct measure of local refractive index variations in the object. Such an interpretation is often not valid because it assumes that light travels along a straight line through the specimen. Refractive index variations normal to the propagation direction of a light beam produce a deflection of the beam (refraction, Schlieren effect) that results in two types of distortions in the interferogram:

- a) Geometrical distortion due to displacement of the beam normal to its propagation direction. This effect falsifies conventional interpretation of distance on the interferogram and causes displacement of the apparent electrode/electrolyte interface.
- b) Phase distortion due to increased geometrical path length and passage of the beam through regions of varying refractive-index. Quantitative concentration profiles,

therefore, often cannot be derived by the conventional interpretation of interferograms.

Figure 1 schematically shows the trajectories of two light rays traversing a cathodic concentration boundary layer. Ray ABC is only slightly deflected and stays within the boundary layer over its path AB because it propagates near the edge of the boundary layer where the refractive-index gradient is small. Ray DEF, which enters the electrolyte where the refractive-index gradient is high, is deflected so much that it leaves the boundary layer at the intersection with line GH (and then travels along a straight line) before leaving the electrolyte at point E. A deflected ray will contribute to the interferogram only if it passes through the aperture of the objective lens. For instance, if ray DEF were to be deflected at any higher angle, it would not pass through the objective lens and, therefore, would not contribute to the interferogram. The corresponding part of the boundary layer would then not be visible on the interferogram.

Details of computational techniques, that have been developed to account for the effect of light-deflection on interferograms of one-dimensional boundary layers, have been described elsewhere.^{1,2} Suffice it to say that for any concentration profile, the shapes of (double beam) interference fringes can now be calculated taking into account effects of light deflection. It has been found that distortions in the interferogram depend strongly on the position of the plane of focus of the imaging objective lens. Although for each concentration profile a plane of focus can be found³ for which the location of the electrode surface is not distorted on the interferogram, it is preferable to use a more

easily defined plane of focus at a fixed location and accept the resulting displacement of the electrode shadow. For the observation of cathodic boundary layers (to be considered here) we recommend² to focus on the inside of the cell wall on the light-entrance side of the cell, where suitable targets can be inscribed. (For anodic boundary layers, it would be preferable to focus on the inside of the cell wall on the light-exit side.)

It is the purpose of this paper to present calculations of light-deflection errors for the interferometric observation of boundary layers so that investigators may estimate errors to be expected under a wide range of experimental conditions.

LIGHT-DEFLECTION ERRORS

Figure 2 shows the experimental interferogram of a concentration boundary layer formed by constant-current electrolysis. Superimposed are the theoretical concentration profile, AE, derived by use of the Sand⁴ equation, and an interference fringe, BF, computed from the concentration profile by taking light-deflection effects into account.

The ordinate on Fig. 2 denotes distance from the true (undistorted) image of the electrode surface. Local changes in the phase of transmitted light, visible as displacements of originally straight interference fringes, have been related to local concentration changes, as shown on the abscissa. The relationship has been based on the conventional interpretation of interferograms that assumes straight-line light propagation. Thus, local changes in phase have been linearly related to changes in concentration (or refractive index) at the corresponding point in the image.

If the interferogram was free of light-deflection effects, the interference fringes would follow the theoretical concentration profile AE. The figure illustrates that the apparent location B of the interface on the interferogram has receded from its original position A, identified by $y = 0$. Also, the apparent concentration change over the boundary layer is smaller than the true change.

Conventional interpretation of the interferogram in Fig. 2 would therefore lead to a boundary layer thickness that is too large. If we define the extent of the boundary layer as the region containing 90% of the concentration variation, the error e_t in boundary layer thickness can be defined in terms of the ordinates of the points shown in Fig. 2 as

$$e_t = (y_F - y_B) - (y_E - y_A)$$

Similarly, the apparent interfacial concentration is too high and the error can be formulated as a difference of abscissas

$$e_c = C_B - C_A$$

The interfacial concentration (refractive index) gradient is too low. The error can be represented by the difference in slope of the two curves at the interface

$$e_g = \left. \frac{dC}{dy} \right|_B - \left. \frac{dC}{dy} \right|_A$$

In addition to the above absolute errors in the interferometry of boundary layers, it is often desirable to estimate the relative errors. Such relative errors in boundary layer thickness, interfacial concentration and interfacial concentration gradient, as shown in Figs. 8-13, are defined here as

$$\epsilon_t = \frac{e_t}{y_E}$$

$$\epsilon_c = \frac{e_c}{C_b - C_A}$$

$$\epsilon_g = \frac{e_g}{\left. \frac{dC}{dy} \right|_A}$$

CONVECTION-FREE BOUNDARY LAYERS

Diffusion boundary layers free of convection effects offer a useful model for optical investigation since the concentration profiles are easily derived, and experimental results can serve to test the optical calculations. Convection-free transport conditions are common in electrochemical studies, and the results can be used as a basis for convective transport studies.

The convectionless electrodeposition of a metal cation from a stagnant layer of an aqueous binary salt electrolyte is described by the time-dependent diffusion equation in one dimension^{*}

$$\frac{\partial C}{\partial t} = D \frac{\partial^2 C}{\partial y^2} \quad (1)$$

The current density is related to the interfacial concentration gradient by

$$i = \frac{zFD}{1-t_+} \left. \frac{\partial C}{\partial y} \right|_{y=0} \quad (2)$$

^{*} Concentration-independent diffusivity will be assumed. Solutions for variable diffusivity can also be obtained, although not in a convenient closed form.

For potentiostatic electrodeposition, the boundary conditions are

$$C = C_s \quad \text{at } y = 0, t > 0 \quad (3)$$

$$C = C_b \quad \text{at } t = 0, \text{ all } y \quad (4)$$

$$C = C_b \quad \text{as } y \rightarrow \infty. \quad (5)$$

The solution, first obtained by Cottrell,⁵ is

$$\theta = \operatorname{erf} \zeta \quad (6)$$

$$i = \frac{zF(\Delta C)}{1-t_+} \sqrt{\frac{D}{\pi t}} \quad (7)$$

where $\operatorname{erf} \zeta$ is the error function of dimensionless distance

$$\zeta = \frac{y}{2\sqrt{Dt}}, \quad (8)$$

$\Delta C = C_b - C_s$ and the dimensionless concentration

$$\theta = \frac{C - C_s}{\Delta C}. \quad (9)$$

For galvanostatic electrodeposition, the boundary conditions to

Eq. (1) are:

$$\frac{\partial C}{\partial y} = \text{constant} \quad \text{at } y = 0, t > 0 \quad (10)$$

$$C = C_b \quad \text{at } t = 0, \text{ all } y \quad (11)$$

$$C = C_b \quad \text{as } y \rightarrow \infty.$$

The solution, first obtained by Sand,⁴ is

$$\theta = 1 + \sqrt{\pi} \zeta (1 - \operatorname{erf} \zeta) - e^{-\zeta^2} \quad (13)$$

$$\Delta C = \frac{2i(1 - t_+)}{zF} \sqrt{\frac{t}{\pi D}} \quad (14)$$

Concentration profiles for use in the light-deflection analysis, with electrodeposition of Cu from aqueous CuSO_4 serving as a model, have been calculated. Equations (6) and (7) and Eqs. (13) and (14) have been used in this computation. The interfacial concentration has been set $C_s = 0$, and the values of the bulk concentration were $C_b = 0.01$, 0.10 or 0.20 M CuSO_4 ($\Delta C = 0.01$, 0.10 or 0.20). For constant potential calculations, time t is varied to give different concentration profiles and interfacial mass flux rates. For constant current calculations, various current densities are used (substituting Eq. (2) into Eq. (10)) to give different concentration profiles and interfacial mass flux rates. (Note that specification of i and ΔC fixes t through Eq. (14).) A diffusion coefficient⁶ $D = 6 \times 10^{-6} \text{ cm}^2/\text{sec}$ and Cu^{++} transference number⁷ $t_+ = 0.36$ (typical values for 0.1M CuSO_4 at 25°C) are used in all calculations. Representative concentration profiles employed in the optical analysis are shown in Figs. 3 and 4.

ERROR CALCULATIONS

Cell dimensions and optical constants must be specified in order to compute interferograms from concentration profiles. The electrode, which is assumed here to fully occupy the space between the glass sidewalls, was assigned widths of 1.0, 2.5, 5.0, 10.0 and 20.0 mm. In order to model our experimental cell, the glass sidewalls were assumed to be 12.7 mm wide with a refractive-index of 1.5231. However, refraction in the glass sidewalls has a negligible effect on light-deflection errors.³ Light of 632.8 nm wavelength is assumed incident parallel to the planar electrode surface and perpendicular to the glass sidewalls. The plane of focus is chosen as the plane where light enters the electrolyte. Electrolyte refractive-index was experimentally found to be a linear function of CuSO_4 concentration at 632.8 nm wavelength and 25°C:

$$n = 1.3311 + 0.029 C \quad (15)$$

Interferograms similar to the dashed line in Fig. 2 are now calculated from concentration profiles using the above-mentioned computational technique.¹

Absolute errors in boundary layer thickness, interfacial concentration and interfacial concentration gradient are shown in Figs. 5, 6 and 7, respectively for a 10 mm wide electrode. Current density (interfacial refractive-index gradient) was chosen as abscissa because it is an easily measured variable. Note that a positive error means that the value of a variable on the interferogram is larger than the true value.

Relative errors in boundary layer thickness, interfacial concentration and interfacial concentration gradient are shown in Figs. 8-13.

Figures 8-10 also demonstrate the dependence of errors on concentration difference ΔC . The effect of electrode width is illustrated in Figs. 11-13.

DISCUSSION

Figures 5-7 show that for a 10 mm wide electrode, the light-deflection errors depend strongly on current density and concentration difference ΔC and only weakly on the specific boundary condition (potentiostatic or galvanostatic). For current densities in the order of 1 mA/cm^2 , the errors are independent of ΔC and boundary condition. The weak dependence on boundary condition can be ascribed to the similarity between the respective concentration profiles; compare Figs. 3 and 4. Above about 2 mA/cm^2 for $\Delta C = 0.01 \text{ M CuSO}_4$, about 7 mA/cm^2 for $\Delta C = 0.1 \text{ M}$ and about 10 mA/cm^2 for $\Delta C = 0.2 \text{ M}$, the light rays entering the boundary layer at the electrode surface are deflected so much that they leave the boundary layer before they leave the electrolyte (as ray DEF in Fig. 1). This effect causes an error extremum in the curves of Figs. 5 and 6 and a knee in the curves of Fig. 7. The abrupt changes in the character of the error curves are due to the straight paths traversed by the deflected rays once they leave the boundary layer; at lower current densities the rays are continuously changing direction within the boundary layer. (Figure 2 illustrates an interferogram in which rays entering the cell near the electrode surface are deflected out of the boundary layer.) As infinite current density is approached, the error in boundary layer thickness approaches zero, the error in interfacial concentration approaches ΔC and the error in interfacial concentration gradient approaches negative infinity.

The trend toward apparent negative concentrations (i.e., on the interferogram) seen in Figs. 6, 9 and 12 is a result of the choice of focal plane position. For focus in the center of the cell, for instance, no such negative errors would occur.

Figures 8-10 show that, contrary to what one might expect, relative errors are generally smaller for larger concentration difference ΔC . However, for large concentration differences, interferogram interpretation can be impeded by crowding of the fringes near the interface.

Figures 11-13 show that similar to absolute errors derived analytically for constant concentration gradients of unlimited extent,³ relative errors strongly diminish with decreasing cell width, but are negligible only for electrodes thinner than a few mm.

Figures 5-13 can be used to estimate light deflection errors in experimental interferograms if all deflected portions of the test beam are accepted by the objective lens. The maximum angle $\phi_{\max}$ of light deflection within a boundary layer is given by^{2,3}

$$\tan \phi_{\max} = \sqrt{\left(\frac{n_b}{n_s}\right)^2 - 1} \quad (16)$$

and the maximum angle of deflected light emanating from the specimen cell can be calculated by substituting numerical values of refractive-index (e.g., Eq. (15)) into Eq. (16) and accounting for refraction in the glass sidewall. For example, the objective lens aperture must accept illumination at angles up to 1.59° for $\Delta C = 0.01 \text{ M CuSO}_4$, up to 4.65° for $\Delta C = 0.10 \text{ M}$ and up to 7.14° for $\Delta C = 0.20 \text{ M}$.

CONCLUSIONS

Light deflection effects in the interferometry of electrochemical mass transfer boundary layers can lead to serious errors in the derivation of concentration profiles unless appropriate corrections in the interpretation of interferograms are employed. The magnitude of errors encountered may be estimated from the data presented in Figs. 5-13, but the accurate interpretation of interferograms with significant light-deflection effects requires individual optical analysis.² Light-deflection errors are small (<10%) for small current densities (below 2.5 mA/cm^2 for a 1 cm wide electrode) or narrow electrodes (less than 2.5 mm for up to 10 mA/cm^2).

ACKNOWLEDGEMENTS

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NOMENCLATURE

C	concentration [mole/liter]
C_b	bulk concentration [mole/liter]
C_s	interfacial concentration [mole/liter]
D	diffusion coefficient [cm^2/sec]
e_t	absolute error in boundary layer thickness [mm]
e_c	absolute error in interfacial concentration [M CuSO_4]
e_g	absolute error in interfacial concentration gradient [$\text{M CuSO}_4 \text{ cm}^{-1}$]
F	Faraday constant [coul/equiv]
i	current density [A/cm^2]
n	refractive-index
n_b	bulk refractive-index
n_s	interfacial refractive-index
t	time after current (voltage) switch-on [s]
t_+	cation transference number
y	distance from electrode [mm]
z	cation valence
ΔC	$C_b - C_s$ [mole/liter]
ϵ_t	relative error in boundary layer thickness
ϵ_c	relative error in interfacial concentration
ϵ_g	relative error in interfacial concentration gradient
ζ	dimensionless distance (Eq. (8))
θ	dimensionless concentration (Eq. (9))
ϕ_{max}	maximum angle of deflection within a boundary layer

FIGURE CAPTIONS

Fig. 1. Schematic of light ray trajectories in a cathodic concentration boundary layer: refractive-index increases in the direction away from the electrode surface.

ABC Trajectory of a ray that remains inside the boundary layer.

DEF Trajectory of a ray that is deflected out of the boundary layer.

GH Edge of the boundary layer.

Fig. 2. Experimental interferogram of a concentration boundary layer during galvanostatic deposition of copper on a 10 mm wide electrode. $i = 10.0 \text{ mA/cm}^2$, $C_b = 0.1\text{M CuSO}_4$ and $t = 10.0 \text{ s}$.

—— Theroretical concentration profile AE corresponding to experimental conditions (calculated from Eq. (13)).

----- Computed interference fringe BF corresponding to theoretical concentration profile.

A True interfacial concentration and position.

B Apparent interfacial concentration and position.

E True (90%) boundary layer edge (position where $\theta = 0.9$).

F Apparent boundary layer edge.

Fig. 3. Concentration profiles for potentiostatic conditions.

——— $\Delta C = 0.1M \text{ CuSO}_4$
 ----- $\Delta C = 0.2M \text{ CuSO}_4$
 a $i = 10.0 \text{ mA/cm}^2$, $t = 17.5 \text{ s}$
 b $i = 20.0$, $t = 4.4 \text{ s}$
 c $i = 30.0$, $t = 1.9 \text{ s}$
 d $i = 10.0$, $t = 70.0 \text{ s}$
 e $i = 20.0$, $t = 17.5 \text{ s}$
 f $i = 30.0$, $t = 7.8 \text{ s}$

Fig. 4. Concentration profiles for galvanostatic conditions. ΔC and i designation as in Fig. 3.

a $t = 43.2 \text{ s}$
 b $t = 10.8 \text{ s}$
 c $t = 4.8 \text{ s}$
 d $t = 172.7 \text{ s}$
 e $t = 43.2 \text{ s}$
 f $t = 19.2 \text{ s}$

Fig. 5. Absolute error in boundary layer thickness. Electrode width = 10.0 mm.

——— potentiostatic boundary condition
 ----- galvanostatic boundary condition
 a $\Delta C = 0.01 M \text{ CuSO}_4$
 b $\Delta C = 0.10 M \text{ CuSO}_4$
 c $\Delta C = 0.20 M \text{ CuSO}_4$

Fig. 6. Absolute error in interfacial concentration. Designations as in Fig. 5.

Fig. 7. Absolute error in interfacial concentration gradient. Designations as in Fig. 5.

Fig. 8. Relative error in boundary layer thickness for various concentration differences. Electrode width = 10.0 mm, potentiostatic boundary condition.

a $\Delta C = 0.01 \text{ M CuSO}_4$

b $\Delta C = 0.10 \text{ M CuSO}_4$

c $\Delta C = 0.20 \text{ M CuSO}_4$

Fig. 9. Relative error in interfacial concentration for various concentration differences. Designations as in Fig. 8.

Fig. 10. Relative error in interfacial concentration gradient for various concentration differences. Designations as in Fig. 8.

Fig. 11. Relative error in boundary layer thickness for different electrode widths. $\Delta C = 0.1 \text{ M CuSO}_4$, potentiostatic boundary condition.

a electrode width = 20.0 mm

b 10.0 mm

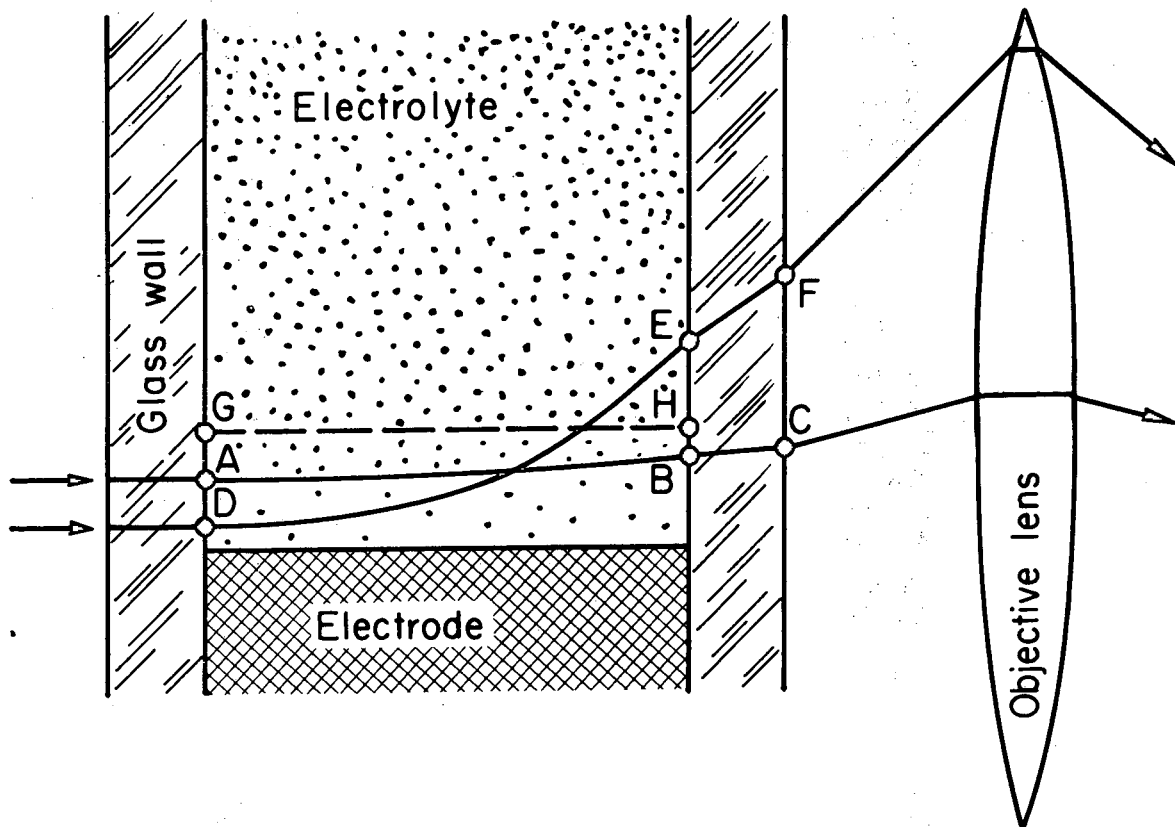
c 5.0 mm

d 2.5 mm

e 1.0 mm

Fig. 12. Relative error in interfacial concentration for different electrode widths. Designations as in Fig. 11.

Fig. 13. Relative error in interfacial concentration gradient for different electrode widths. Designations as in Fig. 11.



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Fig. 1

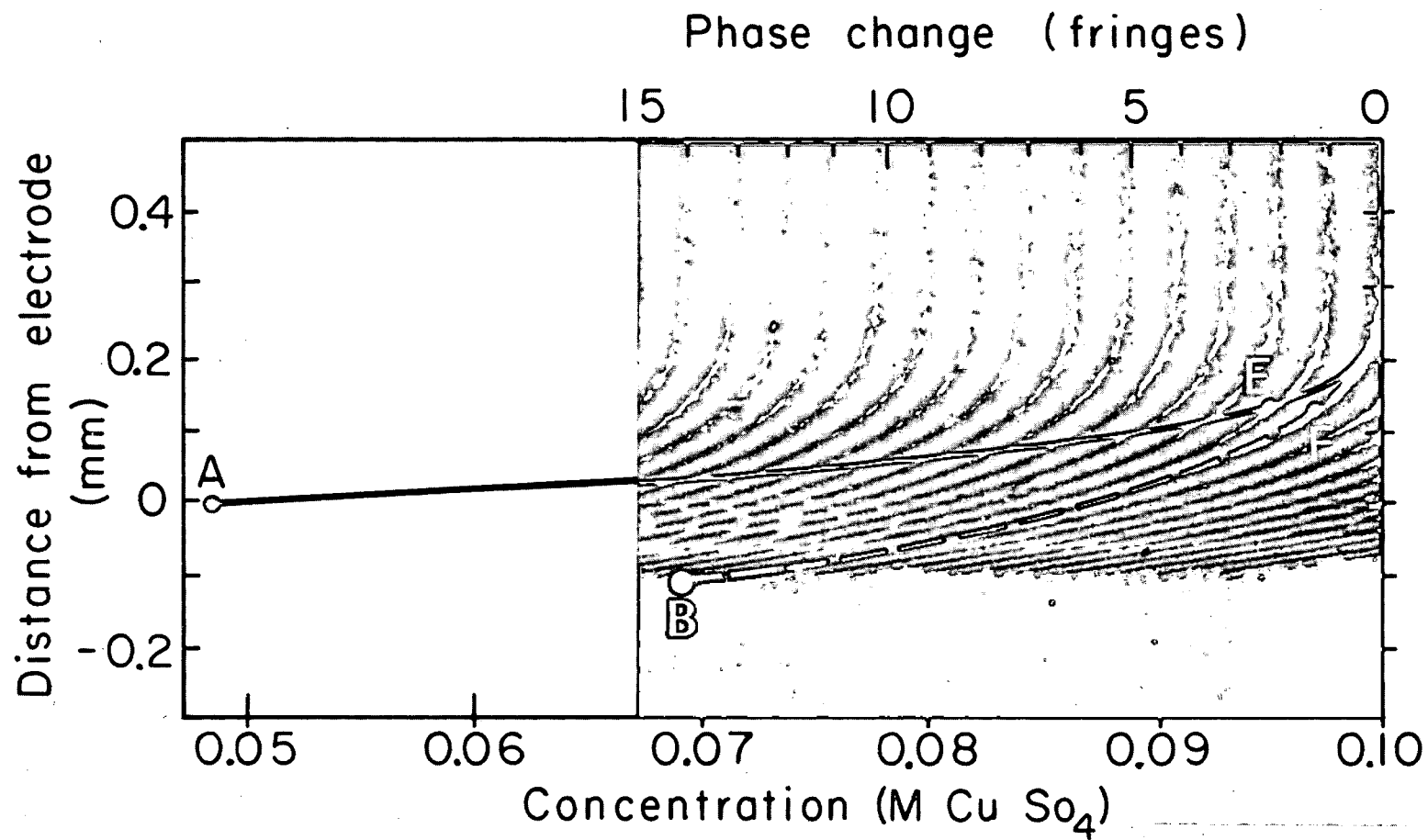
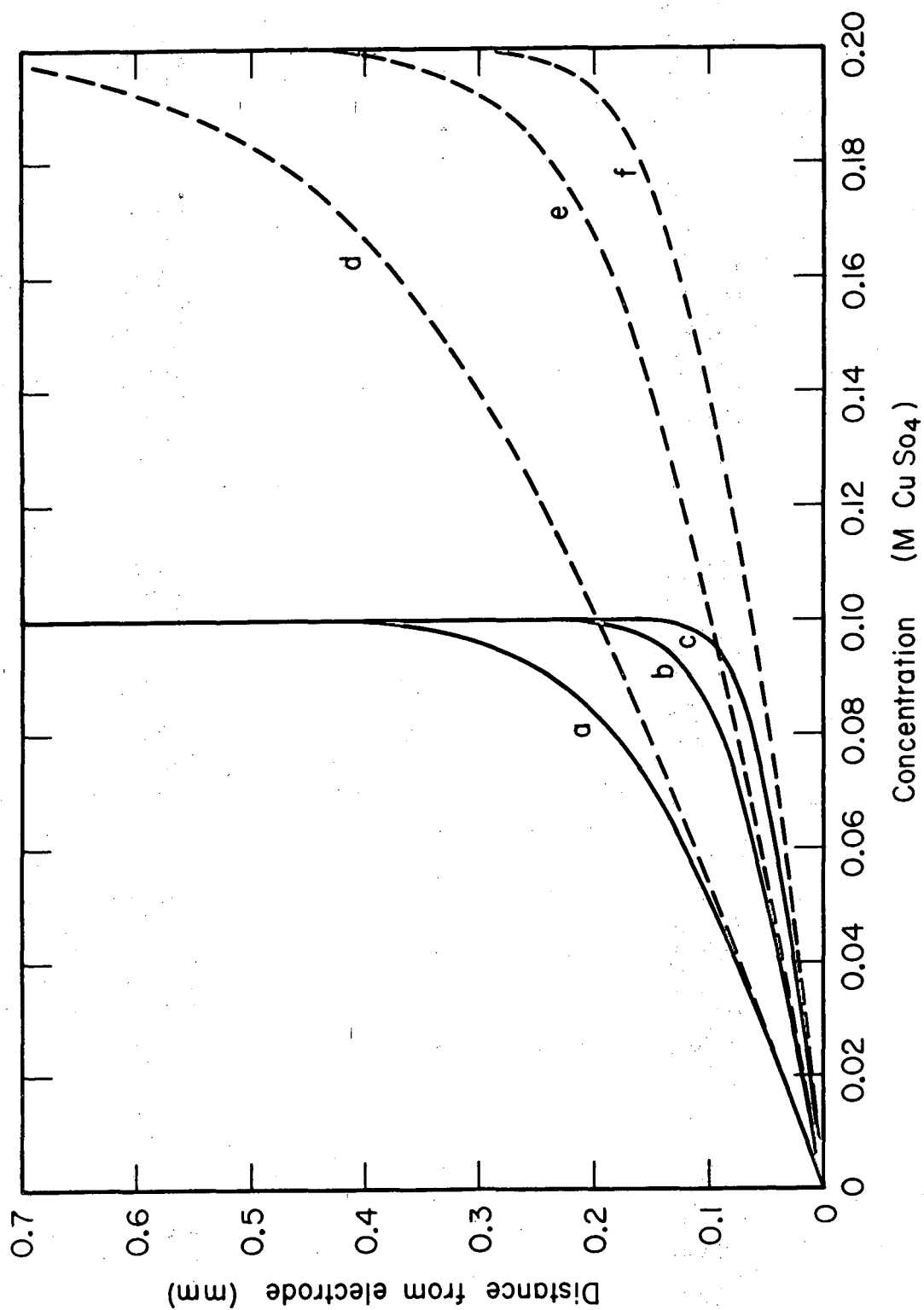
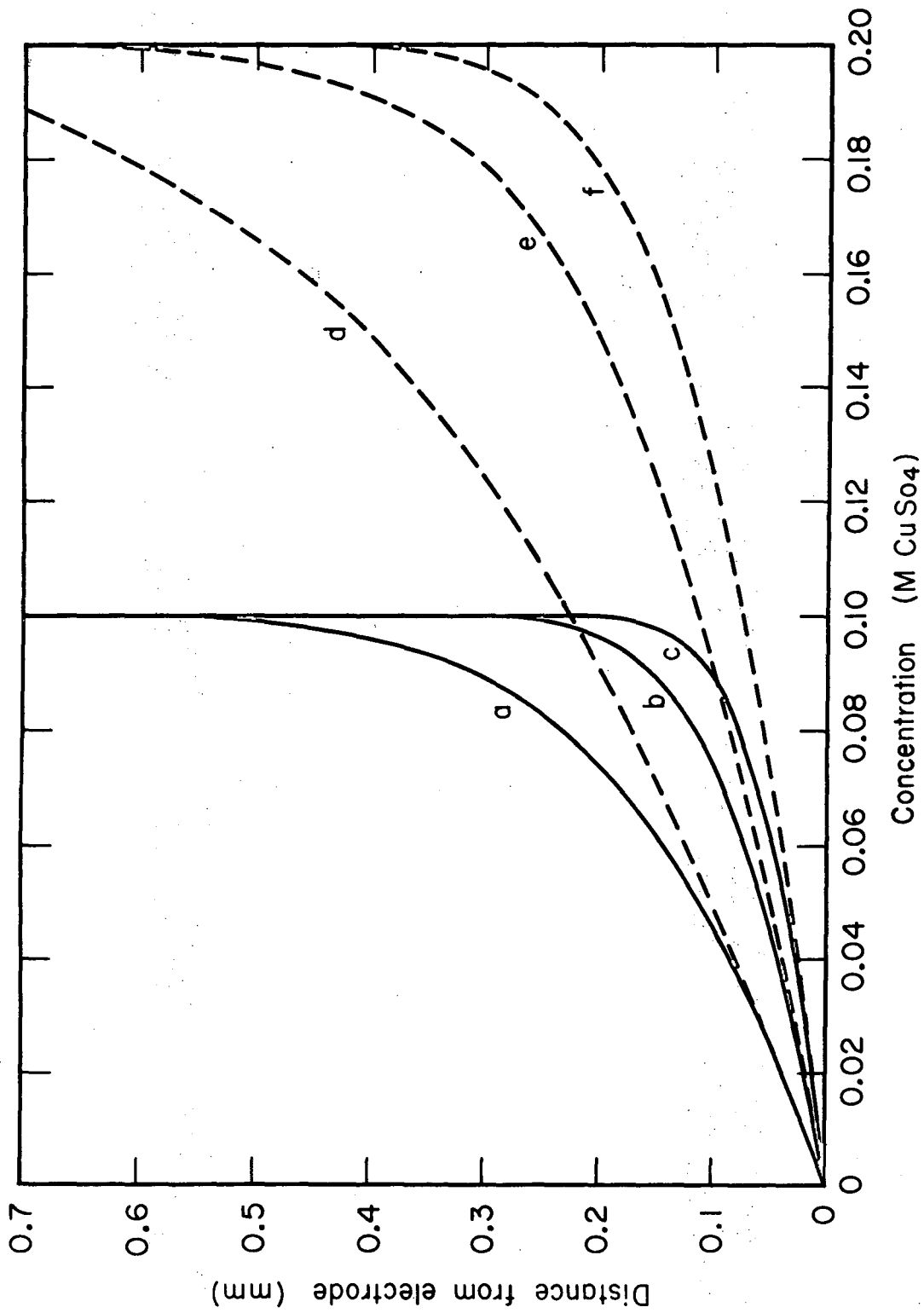


Fig. 2



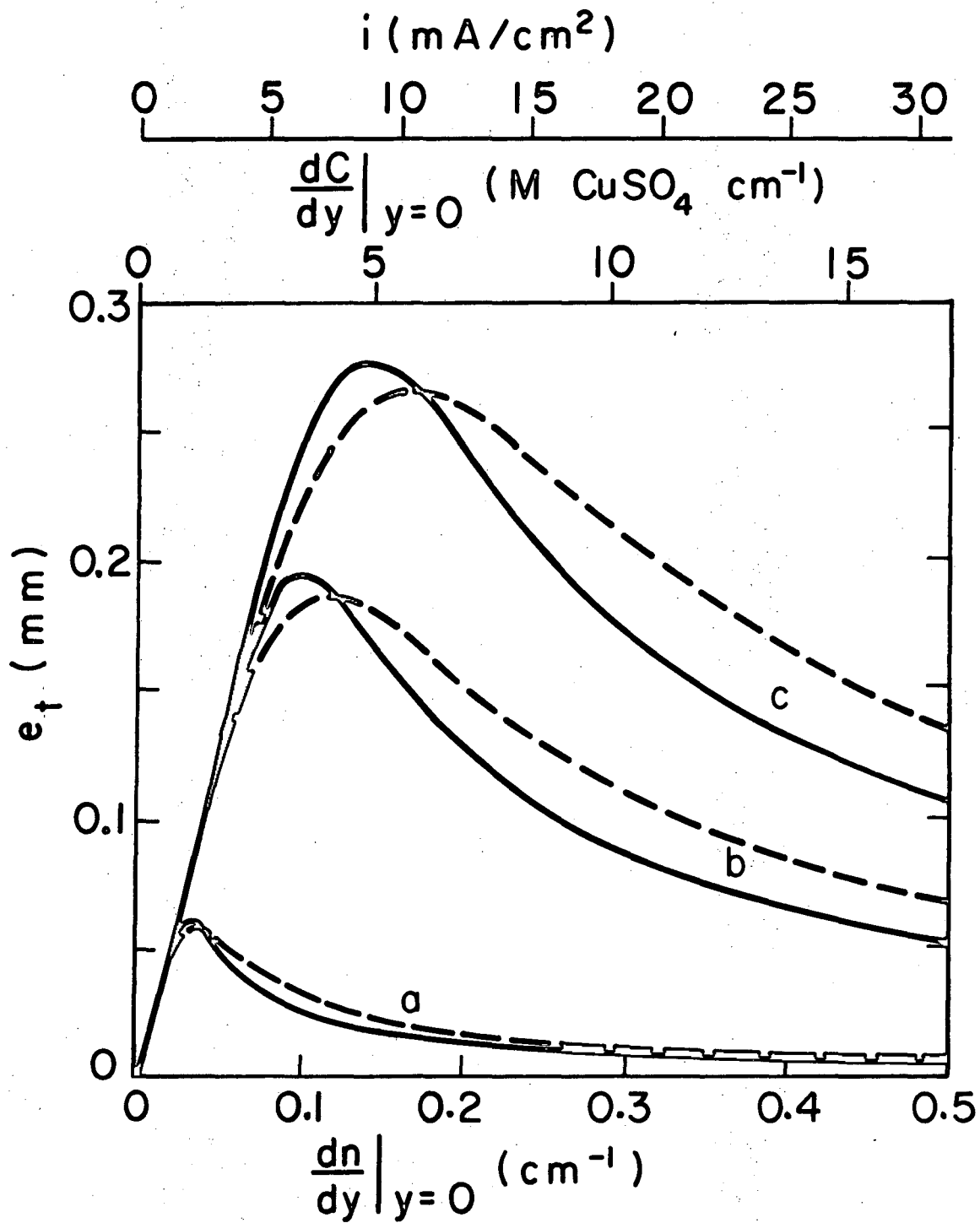
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Fig. 3



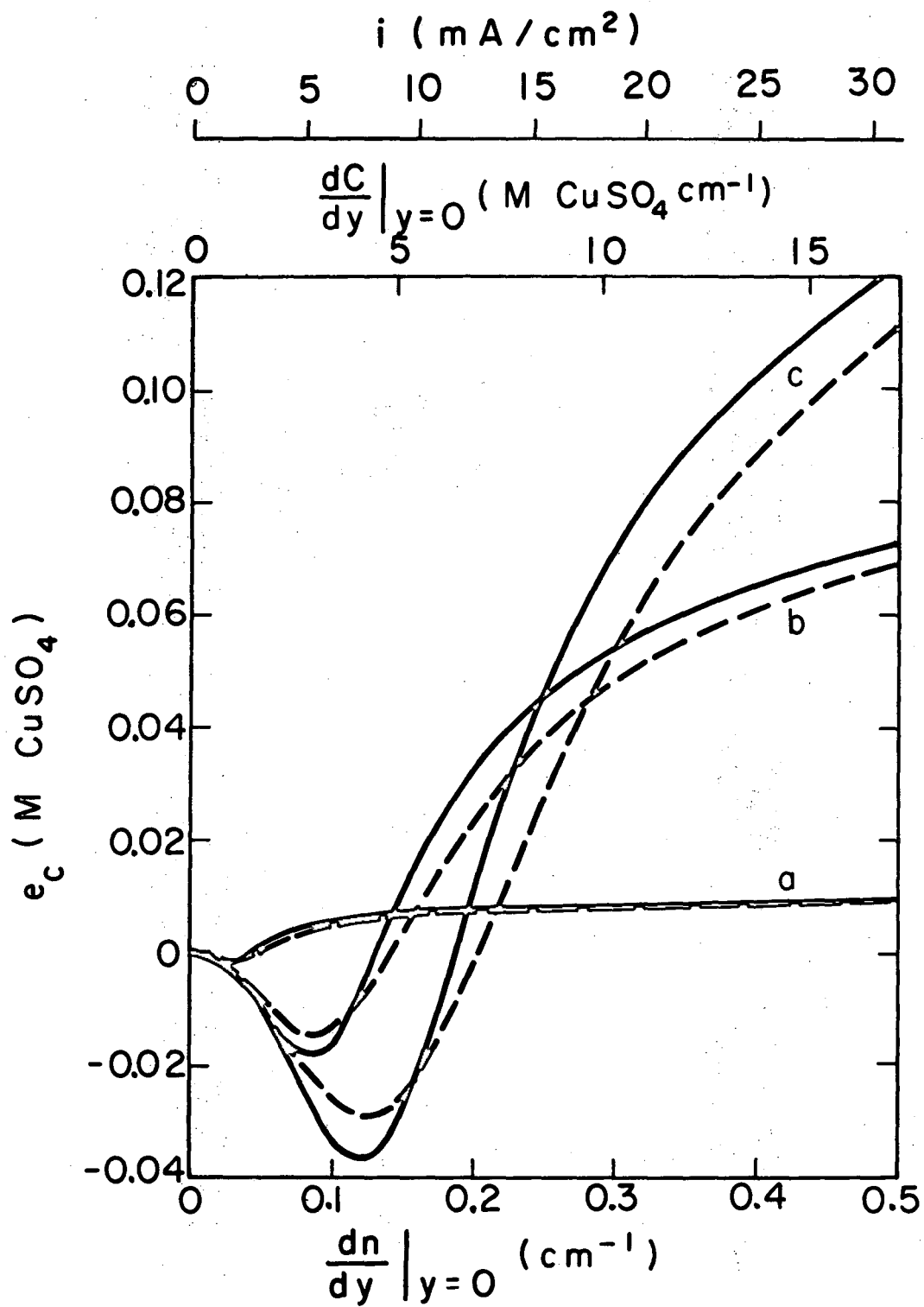
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Fig. 4



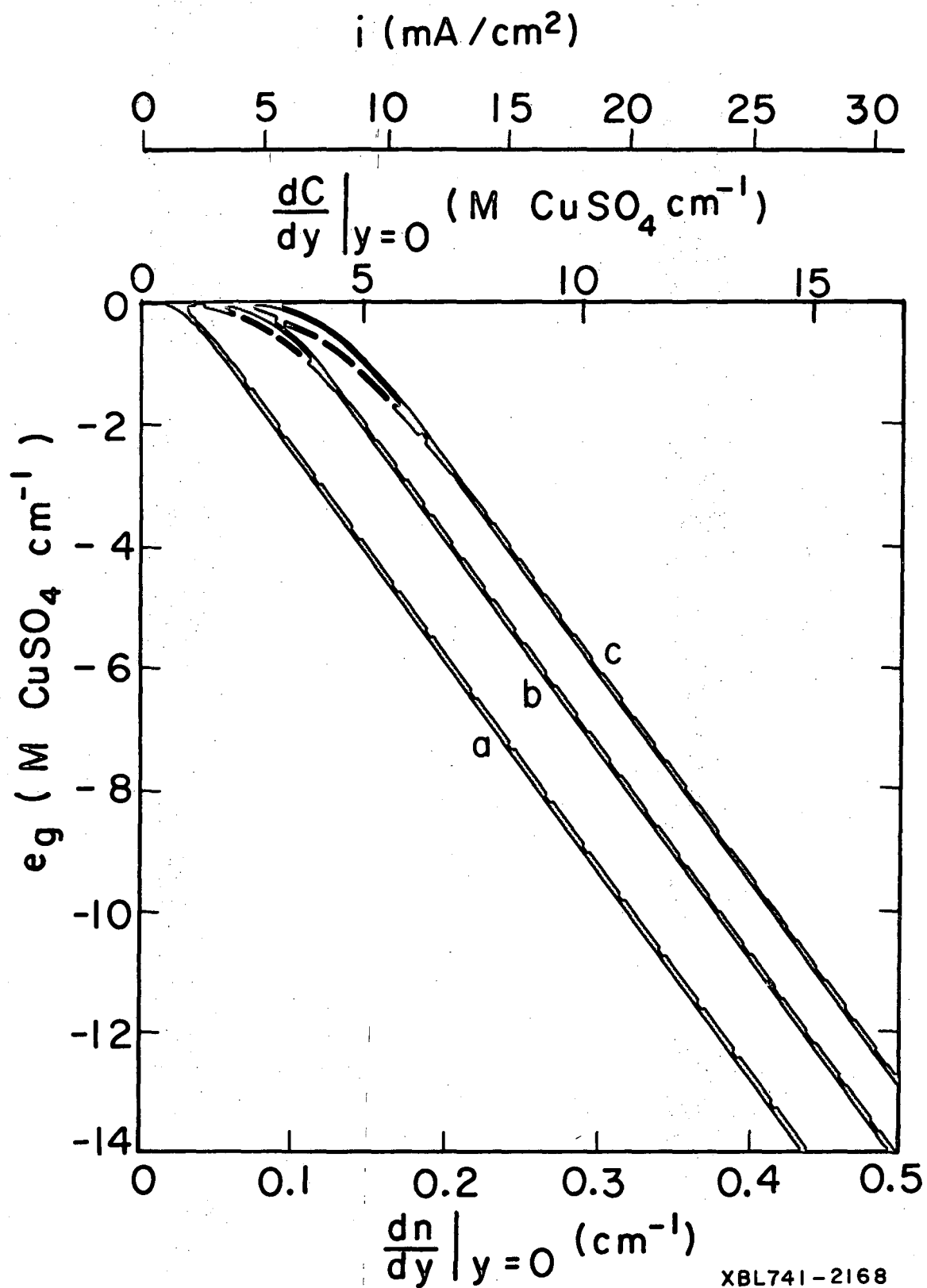
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Fig. 5



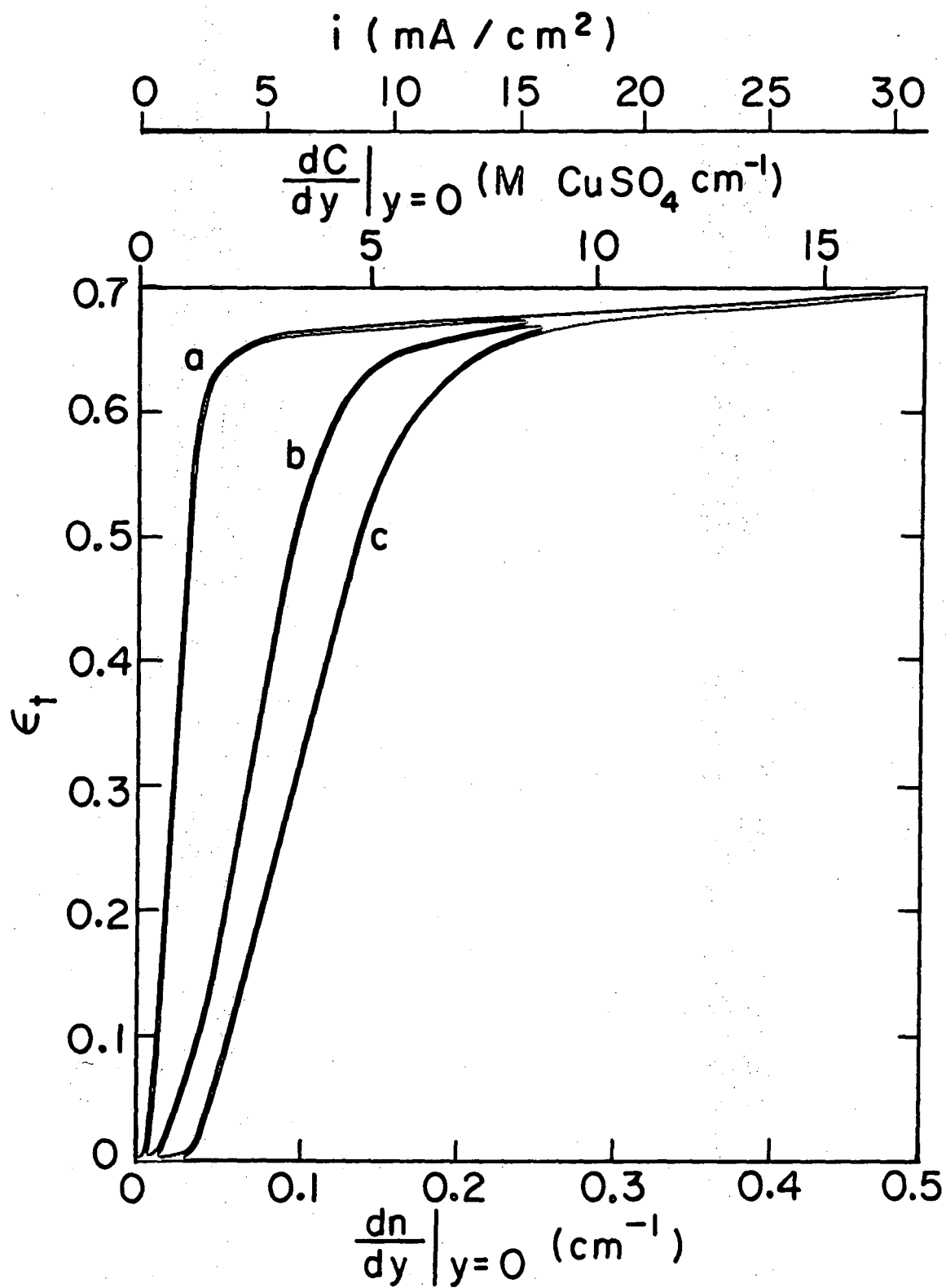
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Fig. 6



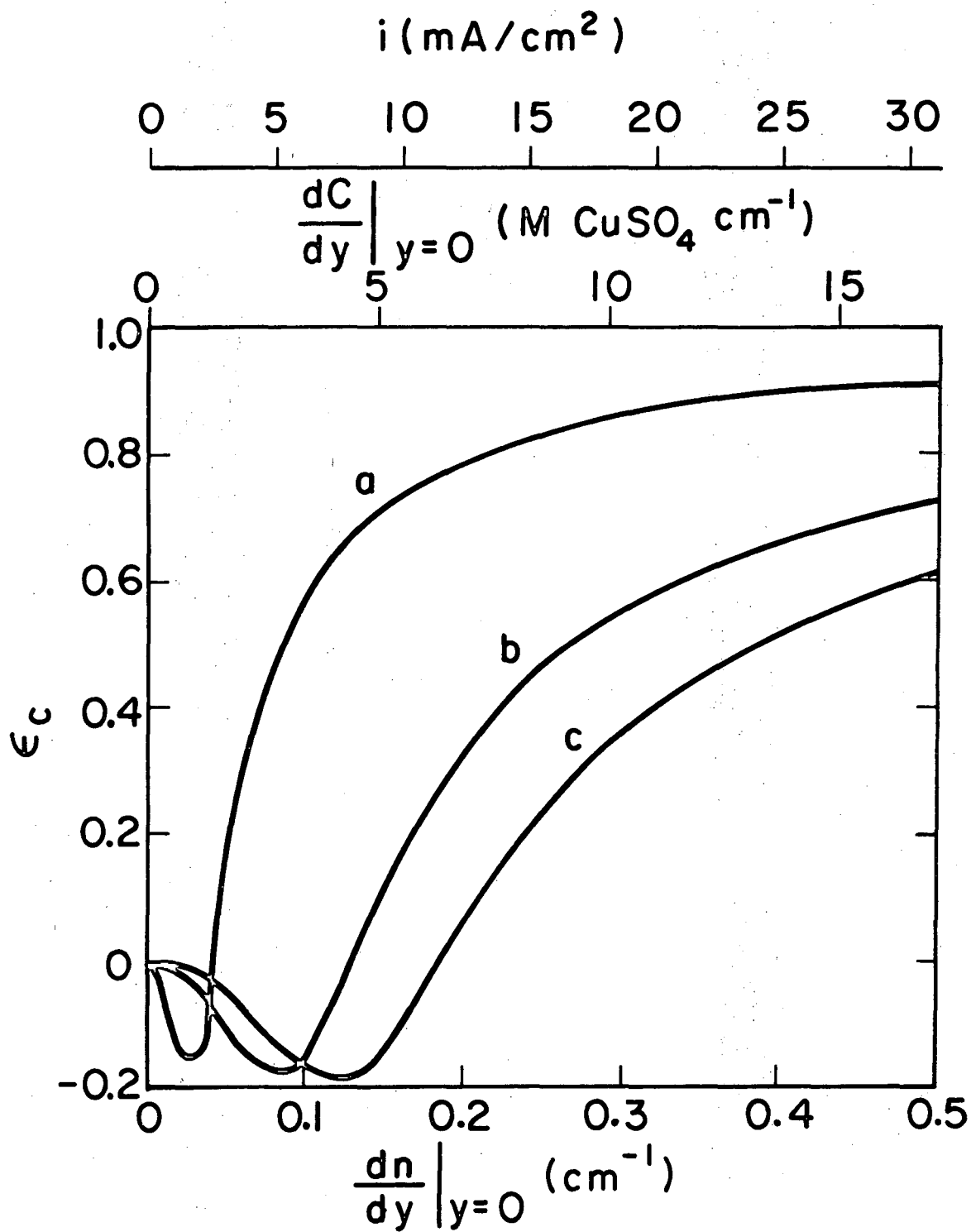
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Fig. 7



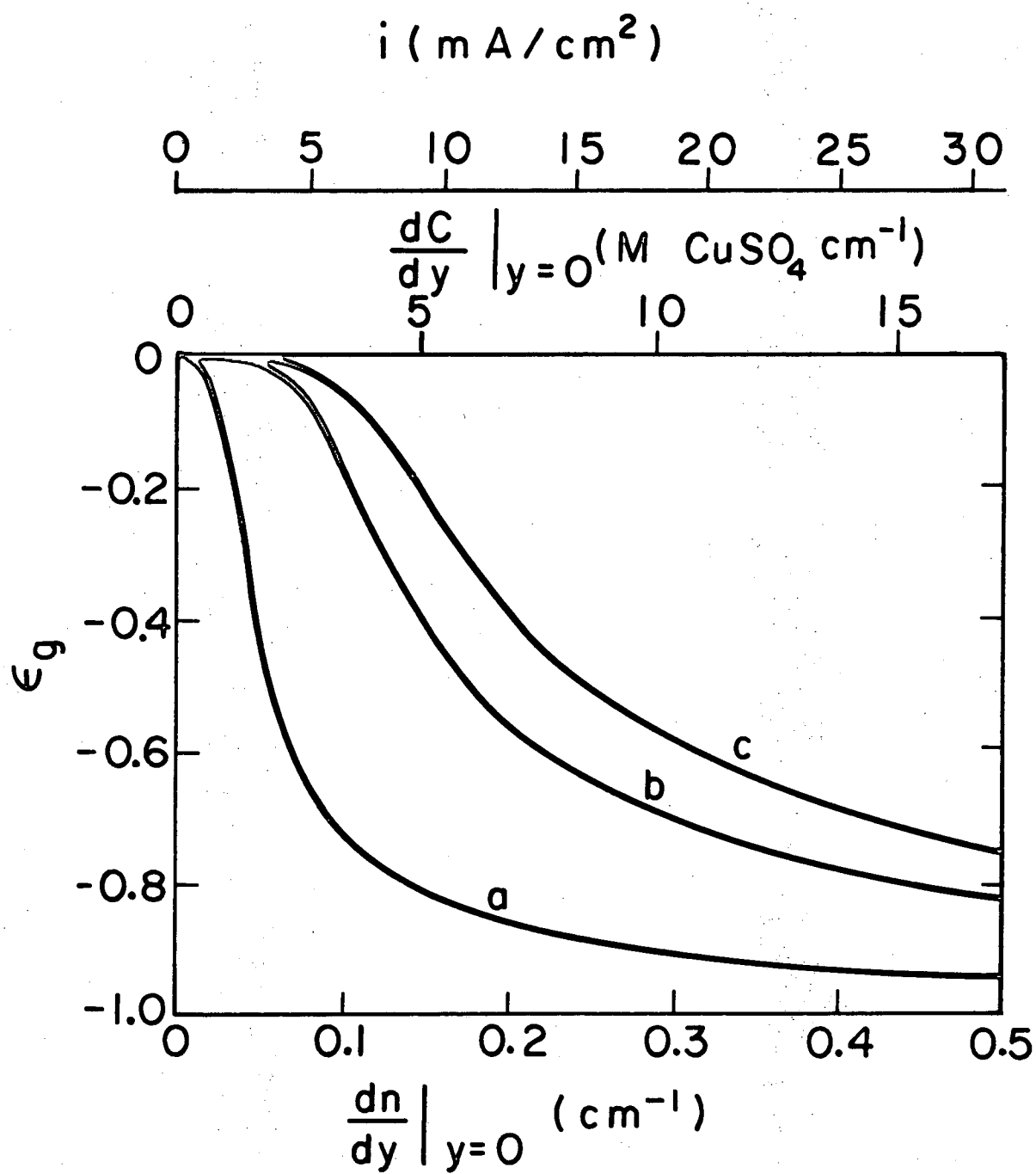
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Fig. 8



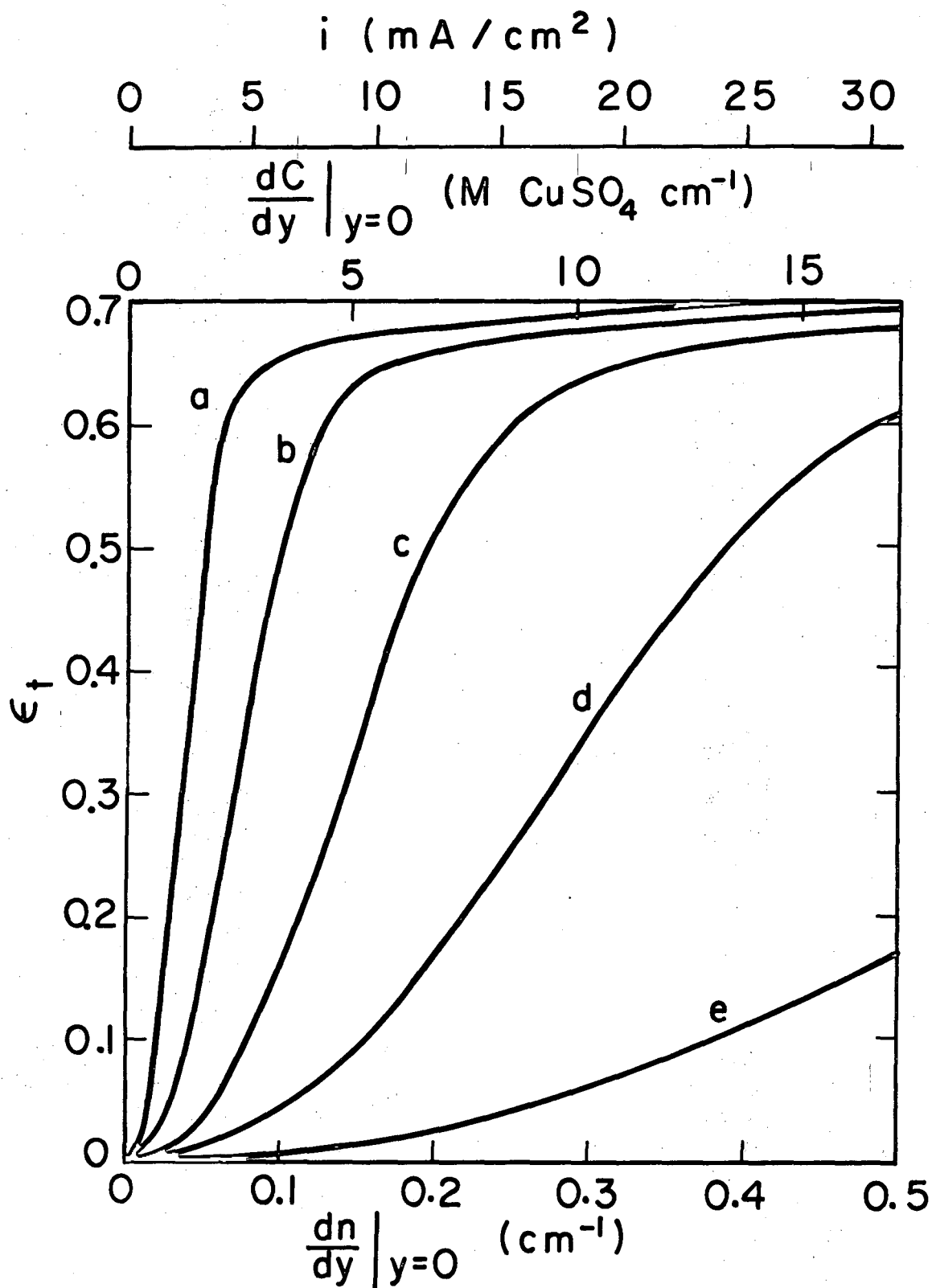
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Fig. 9



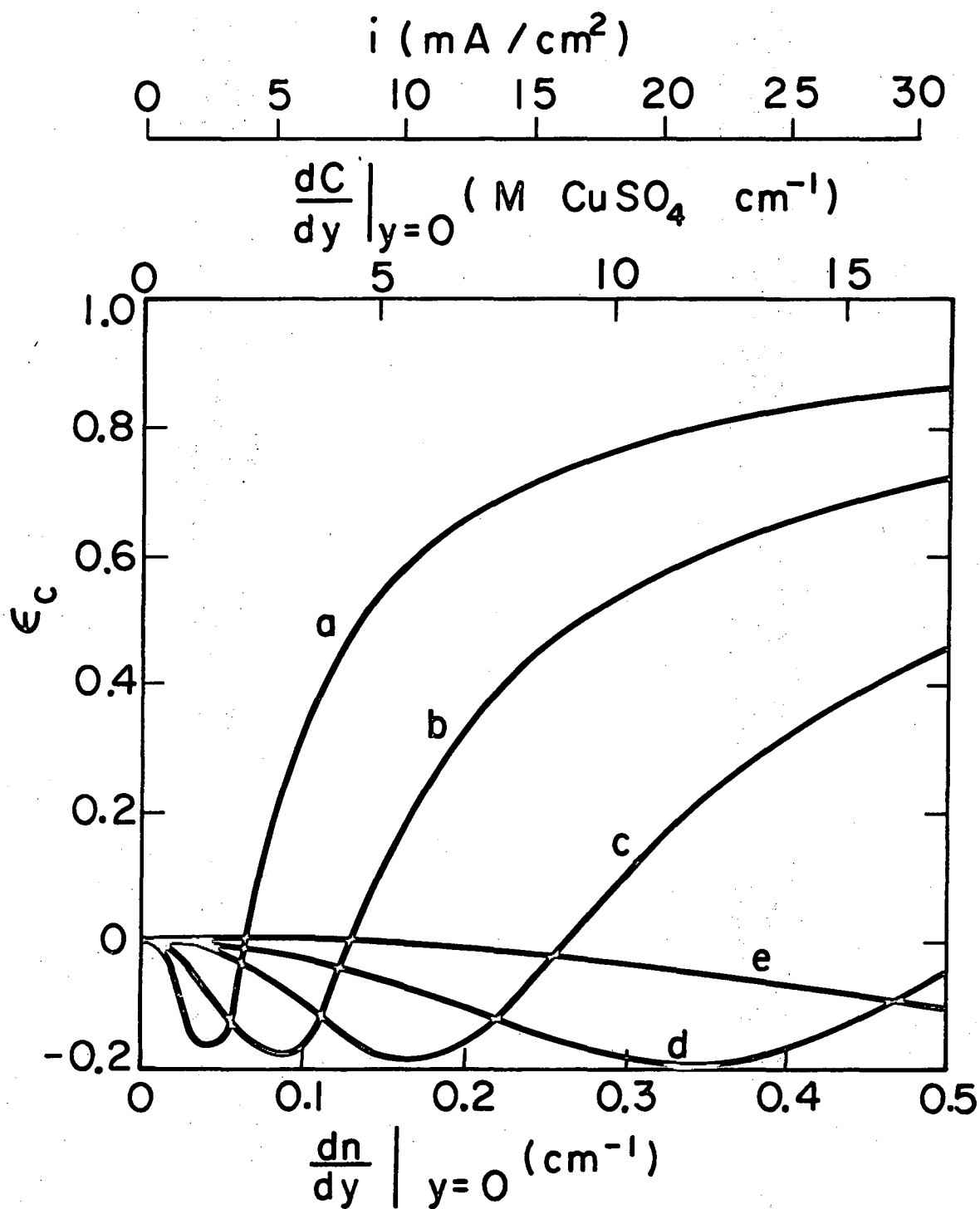
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Fig. 10



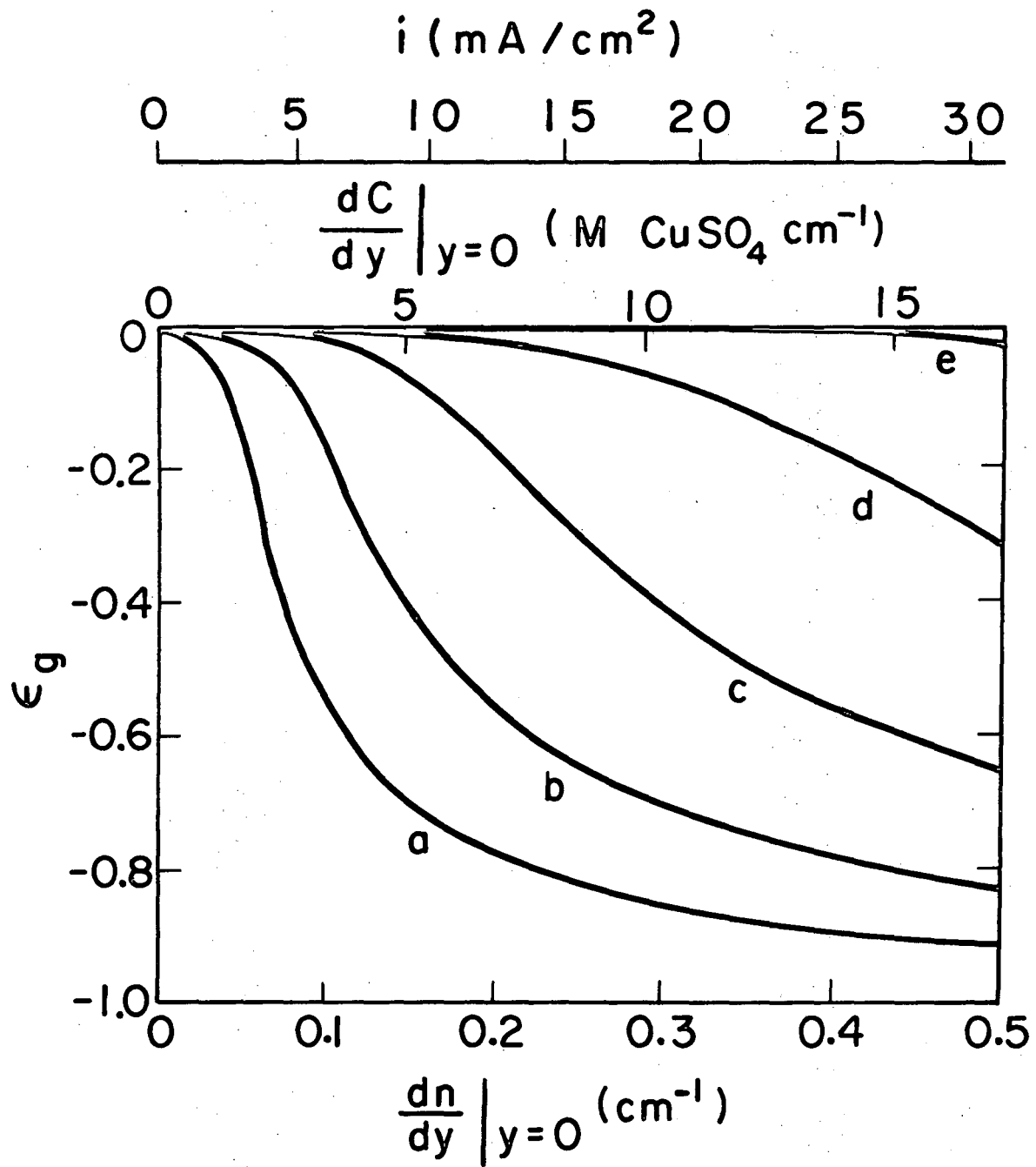
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Fig. 11



XBL74I - 2163

Fig. 12



XBL741-2162

Fig. 13

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