

1 **Cr(VI) Effect on Tc-99 Removal from Hanford Low-Activity Waste Simulant by Ferrous**  
2 **Hydroxide**

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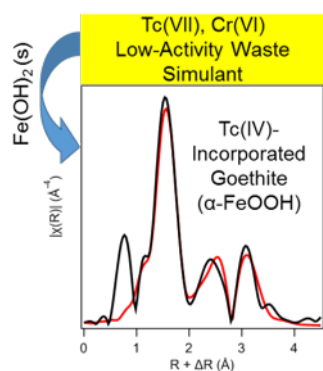
17  
18 **Abstract**

19 Here, Cr(VI) effects on Tc-immobilization by Fe(OH)<sub>2</sub>(s) are investigated while assessing  
20 Fe(OH)<sub>2</sub>(s) as a potential treatment method for Hanford low-activity waste destined for  
21 vitrification. Batch studies using simulated low-activity waste indicate that Tc(VII) and Cr(VI)  
22 removal is contingent on reduction to Tc(IV) and Cr(III). Furthermore, complete removal of both  
23 Cr and Tc depends on the amount of Fe(OH)<sub>2</sub>(s) present, where complete Cr and Tc removal  
24 requires more Fe(OH)<sub>2</sub>(s) (~200 g/L of simulant), than removing Cr alone (~50 g/L of simulant).

25 XRD analysis suggests that  $\text{Fe}(\text{OH})_2(\text{s})$  reaction and transformation in the simulant produces  
26 mostly goethite ( $\alpha\text{-FeOOH}$ ), where  $\text{Fe}(\text{OH})_2(\text{s})$  transformation to goethite rather than magnetite  
27 is likely due to the simulant chemistry, which includes high levels of nitrite and other  
28 constituents. Once reduced, a fraction of Cr(III) and Tc(IV) substitute for octahedral Fe(III)  
29 within the goethite crystal lattice as supported by XPS, XANES, and/or EXAFS results. The  
30 remaining Cr(III) forms oxide and/or hydroxide phases, whereas Tc(IV) not fully incorporated  
31 into goethite persists as either adsorbed or partially incorporated Tc(IV)-oxide species. As such,  
32 to fully incorporate Tc(IV) into the goethite crystal structure, additional  $\text{Fe}(\text{OH})_2(\text{s})$  ( $>200$  g/L of  
33 simulant) may be required.

34

### 35 TOC



36

## 37 1. Introduction

38 Technetium-99 (Tc) is a radioactive fission product present at nuclear waste legacy sites that  
39 is problematic due to its long half-life ( $2.1 \times 10^5$  years), high fission yield (~6%), and  
40 environmental mobility as Tc(VII) species in oxidizing environments.<sup>1-3</sup> Unfortunately, nuclear  
41 waste treatment and environmental remediation strategies targeting Tc are hindered by current  
42 high temperature treatment technologies and the presence of co-mingled redox-active  
43 competitors, e.g. Cr(VI).<sup>4-5</sup> For example, at the US Department of Energy Hanford Site  
44 (Washington State, USA) the baseline treatment plan for nuclear waste is vitrification,<sup>6-7</sup> which  
45 requires operating temperatures  $>1000$  °C that consequently causes Tc volatilization and low Tc-  
46 retention in the glass waste form. One strategy to overcome Tc volatilization is reduction of  
47 Tc(VII) to stable Tc(IV) with concurrent Tc(IV) incorporation into minerals,<sup>7-14</sup> although this  
48 treatment method is often complicated by the presence of co-mingled Cr(VI), which was used as  
49 a corrosion inhibitor in Hanford nuclear waste storage tanks.<sup>4</sup> Cr(VI) has a more favorable  
50 reduction potential, -0.16 V vs -0.36 V for Tc(VII) at pH 14,<sup>15-16</sup> and exists in Hanford nuclear  
51 waste streams at concentrations orders of magnitude greater than Tc.<sup>17</sup> As a result, reductants  
52 added to reduce Tc(VII) are consumed by Cr(VI). Thus, there remains a critical need for  
53 treatment technologies that can reduce Tc(VII) in the presence of Cr(VI).

54 In a preliminary study, ferrous hydroxide solid ( $\text{Fe}(\text{OH})_2(\text{s})$ ) was successfully used to reduce  
55 Tc(VII) in the presence of Cr(VI) and incorporate Tc(IV) into magnetite via  $\text{Fe}(\text{OH})_2(\text{s})$  mineral  
56 transformation under oxic conditions.<sup>18</sup> This work was performed under the high ionic strength  
57 and pH conditions expected for Hanford low-activity waste (LAW) streams, but used a simple  
58 solution chemistry that only considered Tc(VII) and Cr(VI) in 1 M NaOH. Here,  $\text{Fe}(\text{OH})_2(\text{s})$  is  
59 used to treat Tc in a simulated LAW solution, to assess (i) how complex and realistic waste

60 streams affect the efficacy of this approach and (ii) provide mechanistic evidence for Cr(VI)  
61 reduction and solid formation and how this impacts the Fe(OH)<sub>2</sub>(s) treatment mechanism for Tc.  
62 Hanford's liquid radioactive/chemical waste, currently stored in tanks but destined for pre-  
63 treatment and vitrification, varies from tank to tank due to the different separation processes used  
64 for spent nuclear fuel, resulting in complex mixtures of nitrate, nitrite, phosphate, sulfate, and  
65 organic based solvents.<sup>19</sup> As such, the exact LAW composition for treatment is not known, so for  
66 the purpose of this work, an overall average LAW simulant composition is used based on output  
67 from the Hanford Tank Waste Operations Simulator (HTWOS) model.<sup>17</sup> To arrive at this average  
68 composition, which includes nitrate, nitrite, sulfate, aluminum, Cr(VI) and other minor  
69 constituents, the HTWOS model tracks tank waste storage, retrieval, and multiple treatment and  
70 immobilization processes over ~20 years of operation.

71 The treatment approach described here involves reduction of Tc(VII) in the presence of  
72 Cr(VI) and removal of Tc from solution through incorporation into a solid iron oxide/hydroxide  
73 phase. Once reduced and stabilized, Tc is expected to be resistant to release from the iron  
74 oxide/hydroxide product(s), which may stabilize Tc during vitrification and increase Tc loading  
75 into glass. In addition, development and implementation of this approach could improve  
76 environmental remediation efforts that target co-mingled Tc(VII) and Cr(VI) contaminated  
77 areas.<sup>21</sup>

## 78 **2. Experimental**

79 **Fe(OH)<sub>2</sub>(s) Synthesis.** A detailed synthesis procedure for Fe(OH)<sub>2</sub>(s) and product  
80 characterization may be found in previously published work.<sup>18</sup> Briefly, Fe(OH)<sub>2</sub>(s) was prepared  
81 and stored inside an anoxic chamber (Coy Laboratories) that was maintained using a gas mix of  
82 N<sub>2</sub> (98%) and H<sub>2</sub> (2%). Fe(II)Cl<sub>2</sub>·4H<sub>2</sub>O (14 g, >95%, Fisher Scientific) was dissolved in N<sub>2</sub>-

100 purged double deionized water (400 g, DDI, Millipore 18Ω). Dissolved Fe(II) was then  
 101 precipitated as Fe(OH)<sub>2</sub>(s) by adding 8.2 mL of 10 M NaOH (Fisher Scientific) to solution and  
 102 mixing by hand. The solid was allowed to react overnight and then separated from the  
 103 supernatant using a 0.45 μm Nalgene® filter. The Fe(OH)<sub>2</sub>(s) was then allowed to dry for 24  
 104 hours before it was powdered using a mortar and pestle.

105 **Simulant Preparation.** A 5 M Na Hanford LAW simulant with 1080 ppm Cr(VI) was  
 106 generated as described previously,<sup>17</sup> and spiked with 1-100 ppm Tc(VII), using a 10,000 mg/L  
 107 Tc stock solution (NH<sub>4</sub>TcO<sub>4</sub>). The starting simulant was characterized using ion chromatography  
 108 (IC) and inductively coupled plasma optical emission spectrometry (ICP-OES) (Table 1).

109 **Table 1.** 5 M Na Average LAW Simulant Composition

Constituent	Target Concentration [mg/L]*	Measured Concentration [mg/L]	Constituent	Target Concentration [mg/L]*	Measured Concentration [mg/L]
Al	8280	8500	F <sup>-</sup>	600	<1000
Cr	1120	1080	Cl <sup>-</sup>	1500	<2500
P	1520	981	NO <sub>2</sub> <sup>-</sup>	26,000	26,800
K	1280	1300	Br <sup>-</sup>	-	<5000
Na	115,000	110,000	NO <sub>3</sub> <sup>-</sup>	101,000	102,000
S	2740	2810	SO <sub>4</sub> <sup>-</sup>	-	10,100
Ti	-	7.84	PO <sub>4</sub> <sup>-</sup>	-	<7500
pH		13.5	E <sub>h</sub> (SHE)		26 – 81 mV

\* Target Concentrations from Russell et al, 2013 for 5 M Na Average LAW Simulant;<sup>17</sup> target and measured concentrations determined using IC and ICP-OES.

-: Not identified

(SHE): Standard Hydrogen Electrode corrected

110  
 111 **Tc(VII) and Cr(VI) Treatment by Fe(OH)<sub>2</sub>(s).** Fe(OH)<sub>2</sub>(s) (~0.1-1.2 g) was added to LAW  
 112 simulant to achieve final Fe(OH)<sub>2</sub>(s):simulant ratios between 1 and 360 g/L. Fe(OH)<sub>2</sub>(s) was  
 113 removed from the anaerobic chamber immediately before simulant addition, after which  
 114 sample(s) reacted for 3 days (± 1 hour) in an oven set to 75 °C with occasional hand mixing. In  
 115 some instances, aliquots of Fe(OH)<sub>2</sub>(s) were added sequentially over the reaction period.<sup>18</sup> For  
 116 these samples, each aliquot of Fe(OH)<sub>2</sub>(s) was allowed to react with the simulant for ~24 hours

118 before sampling and subsequent  $\text{Fe}(\text{OH})_2(\text{s})$  addition. After 3 days, all samples were allowed to  
119 cool for  $\geq 2$  hours before the solid product was separated from the supernatant (0.45  $\mu\text{m}$   
120 Nalgene® filter), rinsed with  $\sim 50$  mL of DDI, and air-dried for  $\geq 24$  hours. The supernatant was  
121 analyzed to determine final Cr (ICP-OES) and Tc (ICP-MS) concentrations. The final pH of a  
122 representative set of supernatants was  $13.5 \pm 0.1$  and the  $E_h$  (SHE) ranged from 26 to 81 mV  
123 before and after the 3 day reaction period.

124 **X-ray Photoelectron Spectroscopy (XPS).** Samples were prepared by dusting carbon tape  
125 with dry sample powder. Tc-free samples were analyzed using a Physical Electronics Quantera  
126 Scanning X-ray Microprobe equipped with a focused monochromatic Al  $K\alpha$  X-ray (1486.7 eV)  
127 source for excitation and a spherical section analyzer. Tc-containing samples were analyzed  
128 using a Kratos Axis DLD spectrometer with a monochromatic Al  $K\alpha$  X-ray source. An 80 W X-  
129 ray beam was focused to 100  $\mu\text{m}$  (diameter) and scanned over the sample. High-energy  
130 resolution spectra were collected using a pass-energy of 69.0 eV and 0.125 eV step size. Spectra  
131 were charge-corrected to the main line, carbon 1s peak at 285.0 eV. Data analysis and peak  
132 fitting was performed in CasaXPS (version 2.3.15) (see SI for details).

133 **X-ray Diffraction (XRD).** XRD patterns were collected using a Rigaku Miniflex II XRD  
134 unit equipped with a Cu  $K\alpha$  radiation ( $\lambda=1.5418 \text{ \AA}$ , 30-40 kV, 15 mA) source. Samples were  
135 scanned, at minimum, between 3 – 90 degrees  $2\theta$  at 0.5 degrees/min using a 0.02 degree step  
136 size. Reitveld quantification refinements were performed for each pattern collected (see SI for  
137 details).

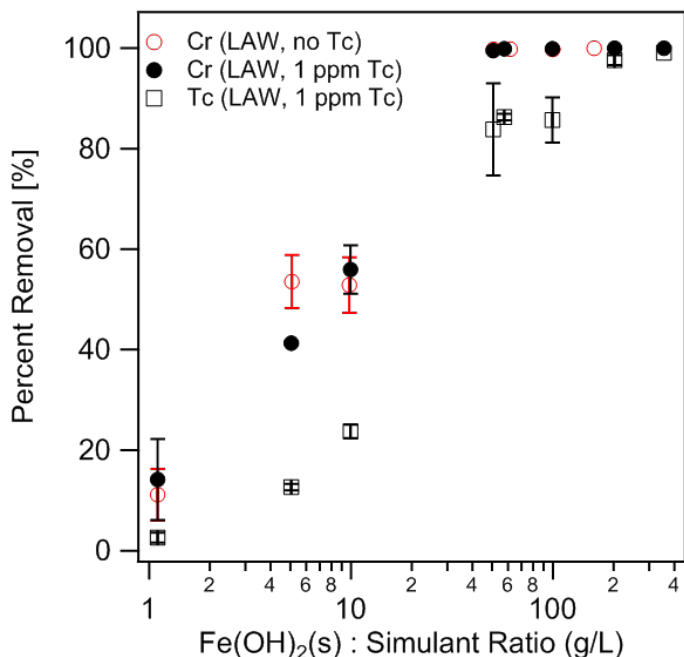
138 **X-ray Absorption Near Edge Structure (XANES) and Extended X-ray Absorption Fine  
139 Structure (EXAFS) Spectroscopy.** Tc K-edge (21,044 eV) spectra were collected on beamline  
140 11-2 at the Stanford Synchrotron Radiation Laboratory (SSRL) for samples spiked with Tc

141 concentrations  $\geq 100$  mg/L. Cr K-edge (5,989 eV) spectra were collected on SSRL beamlines 11-  
142 2 and 4-1. Dead-time correction and data reduction was performed using SixPack.<sup>22</sup> Data  
143 analysis was performed using ATHENA/ARTEMIS software.<sup>23</sup> Tc XANES spectra were energy  
144 calibrated using a Tc(VII) reference (pertechnetate ( $\text{TcO}_4^-$ ) adsorbed on Reillex-HPQ polymer  
145 resin) and fit using a linear combination of Tc(IV) and Tc(VII) standards.<sup>14, 24-25</sup> For EXAFS  
146 fitting, a Tc-substituted goethite ( $\alpha\text{-FeOOH}$ ) structure was used in addition to models for  
147  $\text{TcO}_2 \cdot 2\text{H}_2\text{O}$  and  $\text{TcO}_4^-$  as necessary. Cr XANES spectra were energy calibrated using a Cr foil  
148 reference and fit using a linear combination of Cr(III) and Cr(VI) standards. Additional sample  
149 preparation and analysis details are provided in the SI.

150

### 151 3. Results and Discussion

152 **Tc(VII) and Cr(VI) Removal by  $\text{Fe}(\text{OH})_2(\text{s})$ .** A viable material for removing contaminants  
153 from LAW must stabilize Tc with as little solid as possible to meet glass composition constraints  
154 and avoid costly operational changes. The minimum  $\text{Fe}(\text{OH})_2(\text{s})$  required to remove co-mingled  
155 Tc and Cr from the LAW simulant was determined as a function of  $\text{Fe}(\text{OH})_2(\text{s})$ :simulant ratio  
156 (Figure 1). Studies performed without Tc indicate that 50 g of  $\text{Fe}(\text{OH})_2(\text{s})$  per liter of simulant is  
157 required to remove Cr (1080 ppm) from solution. The addition of 1 ppm Tc does not change the  
158 minimum  $\text{Fe}(\text{OH})_2(\text{s})$  required to remove Cr(VI); though to remove  $>97.6\%$  Tc requires at least  
159 200 g  $\text{Fe}(\text{OH})_2(\text{s})$  per liter of simulant.



160

161 **Figure 1.** Cr and Tc removal from LAW simulant with 1 ppm Tc (black) and without Tc (red).  
 162 Cr(VI) results are indicated by filled or open circles, Tc results by open squares. Error bars  
 163 represent the standard deviation of results averaged from two to six replicate samples. Percent  
 164 removal assumed to be 100% if below ICP-OES detection limit for Cr (23  $\mu\text{g/L}$ ) or ICP-MS  
 165 detection limit for Tc (33  $\text{ng/L}$ ).

166 To better understand the additional Fe(OH)<sub>2</sub>(s) requirement needed to remove Tc(VII) from  
 167 the LAW simulant, the solution chemistry and redox and transformation processes must be  
 168 considered. Similar to the 1 M NaOH system,<sup>18</sup> the experimentally determined amount of  
 169 Fe(OH)<sub>2</sub>(s) needed to remove Tc (1 ppm) and Cr (1080 ppm) is ~35x more than the amount  
 170 needed to reduce Tc(VII) to Tc(IV), and Cr(VI) to Cr(III), based solely on redox requirements.  
 171 This is partially attributed to rapid oxidation of Fe(II) to Fe(III) by air and the additional Fe(II)  
 172 needed to form iron oxide/hydroxide phases that incorporate Tc and/or Cr,<sup>10, 26-29</sup> but is likely  
 173 also the result of the complex chemical environment, e.g., pH and competing contaminants in the  
 174 LAW simulant that require excess reductant due to competing chemical processes. For instance,  
 175 the Tc and Cr Pourbaix diagrams (see SI) for the simulant solution (Table 1), assuming 200 g of  
 176 Fe(OH)<sub>2</sub>(s) per liter, suggest that both constituents should remain in solution as oxidized TcO<sub>4</sub><sup>-</sup>



177 and  $\text{CrO}_4^{2-}$  given the pH and  $E_h$  conditions measured before  $\text{Fe}(\text{OH})_2(\text{s})$  addition and after the 3  
178 day reaction period. The Pourbaix diagrams predict that Fe(II) would preferentially facilitate the  
179 reduction and volatilization of nitrate and nitrite as  $\text{N}_2(\text{g})$ , with the remaining Fe(II) precipitating  
180 as the spinel hercynite ( $\text{Fe}(\text{II})\text{Al}(\text{III})_2\text{O}_4$ ).<sup>30-31</sup> Yet, at a 200 g/L  $\text{Fe}(\text{OH})_2(\text{s})$ :simulant ratio, neither  
181 Tc nor Cr are detected in solution at significant concentrations. Additionally, IC measurements  
182 of the remaining solution indicate negligible removal of nitrate and only ~45% removal of  
183 nitrite. Al(III) removal was determined to increase by ~45% with increasing  $\text{Fe}(\text{OH})_2(\text{s})$ :simulant  
184 ratio as determined by ICP-OES analysis, but was not completely removed as thermodynamics  
185 would predict in the Pourbaix diagrams. In the absence of *in situ*  $E_h$  measurements during  
186 reaction, these measurements demonstrate that the reduction potential of the simulant solution  
187 was significantly lowered upon addition of  $\text{Fe}(\text{OH})_2(\text{s})$ . Furthermore, kinetic processes may  
188 overcome thermodynamics early in the reaction, and as a result of these competing processes Tc  
189 and Cr are removed from solution.

190 Additional evidence for both a thermodynamically- and kinetically-driven system is that Tc  
191 removal is not contingent on complete Cr(VI) removal from the LAW simulant. Both  
192 contaminants are removed concurrently, despite a more favorable reduction potential for Cr(VI)  
193 versus Tc(VII).<sup>32</sup> This behavior is evident in [Figure 1](#), where, between  $\text{Fe}(\text{OH})_2(\text{s})$ :simulant ratios  
194 5-50 g/L, Tc removal begins before Cr removal has reached ~100%. However, between 50-100  
195 g/L, Tc removal plateaus until the  $\text{Fe}(\text{OH})_2(\text{s})$ :simulant ratio reaches 200 g/L. This was not seen  
196 in the simplified system and could be attributed to the presence of nitrite, which may compete  
197 more aggressively for reducing electrons without Cr(VI) present.

198 Finally, based on conclusions derived previously, the removal of Cr(VI) by  $\text{Fe}(\text{OH})_2(\text{s})$  in the  
199 LAW simulant should be contingent on Cr(VI) reduction to Cr(III).<sup>18</sup> Using the IC/ICP-MS

201 method previously reported<sup>30</sup> and detailed in the SI, the speciation of Cr in the final supernatant  
 202 was determined using stable mass isotope <sup>52</sup>Cr. Duplicate experiments with a  
 203 Fe(OH)<sub>2</sub>(s):simulant ratio of 9.8 g/L, a ratio below the requirement for complete Cr(VI) removal,  
 204 removed only 53(6) % of Cr from the LAW simulant with the rest remaining as Cr(VI) in  
 205 solution. This alludes to a reduction requirement for Cr(VI) removal that is confirmed via solid  
 206 characterization in the following sections. Removal of Tc(VII) from solution is also expected to  
 207 occur via reduction to Tc(IV).

## 208 Tc and Cr Immobilization in the Solid Phase

209 *Solid Characterization by XRD:* Solid phase(s) identification is critical for drawing mechanistic  
 210 conclusions from Cr and Tc immobilization. Two Tc-free samples prepared at 50 and 100 g/L  
 211 Fe(OH)<sub>2</sub>:simulant ratios were analyzed by XRD to identify and quantify the minerals formed  
 212 (Table 2, XRD patterns in the SI). For both samples, goethite ( $\alpha$ -FeOOH) accounts for 77% –  
 213 81% of the solid despite doubling the Fe(OH)<sub>2</sub>(s):simulant ratio. The remaining solid is  
 214 comprised of feroxyhyte ( $\delta$ -FeOOH), 14 – 17%, and trace amounts (1 – 6%) of amorphous  
 215 material and/or hematite (Fe<sub>2</sub>O<sub>3</sub>). High resolution Fe XPS scans collected from three samples  
 216 with Fe(OH)<sub>2</sub>(s):simulant ratios ranging from 50-200 g/L corroborate these XRD results, where  
 217 83-89 atomic % of Fe is present as goethite (Table 2).

218 **Table 2.** XRD and High Resolution XPS Analysis of Select Solid Phases

Sample		LAW-50-0Tc-1	LAW-100-0Tc	LAW-200-100Tc
Fe(OH) <sub>2</sub> (s):Simulant Ratio	g/L	50	100	200
Starting [Tc(VII)]	ppm	0	0	100
XRD Analysis				
Goethite ( $\alpha$ -FeOOH)	wt%	77	81	-
a	( $\text{\AA}$ ) <sup>*</sup>	4.602(2)	4.597(3)	-
b	( $\text{\AA}$ ) <sup>*</sup>	9.920(3)	9.913(2)	-
c	( $\text{\AA}$ ) <sup>*</sup>	3.0096(9)	3.0080(9)	-
Crystal Size	(nm) <sup>**</sup>	9.8(1)	10.7(1)	-
Feroxyhyte ( $\delta$ -FeOOH)	wt%	17	14	-
Hematite (Fe <sub>2</sub> O <sub>3</sub> )	wt%	-	3	-
Amorphous/Unidentified	wt%	6	1	-

<i>Survey XPS Analysis</i> **				
Cr 2p	<i>at %</i> *	1.6(1)	1.1(1)	0.13(1)
Tc 3d	<i>at %</i>	-	-	0.14(3)
Fe 2p	<i>at %</i>	7.3(4)	8.4(8)	1.7(2)
C 1s	<i>at %</i>	27(4)	19(6)	24(1)
O 1s	<i>at %</i>	64(3)	71(5)	74(1)
<i>Cr XPS Analysis</i> **				
CrOOH	<i>at %</i>	46(1)	38(14)	59(2)
Cr <sub>2</sub> O <sub>3</sub>	<i>at %</i>	28(10)	43(19)	32(4)
Cr(OH) <sub>3</sub>	<i>at %</i>	24.7(2)	18(5)	1(2)
Cr(VI)	<i>at %</i>	1.5	1.3(5)	8.3(8)
<i>Tc XPS Analysis</i> **				
Tc(VII)	<i>at %</i>	-	-	52(1)
Tc(IV)	<i>at %</i>	-	-	48(1)
<i>Fe XPS Analysis</i> **				
FeCr <sub>2</sub> O <sub>4</sub>	<i>at %</i>	0	0	5.7(2)
Fe <sub>3</sub> O <sub>4</sub>	<i>at %</i>	12(1)	11(2)	11(1)
FeOOH	<i>at %</i>	88(1)	89(2)	83(1)

(-) No Detected or Analyzed (\*) Atomic percent

Goethite ( $\alpha$ -FeOOH)<sup>33</sup>: a = 4.634 Å, b = 9.945 Å, c = 3.0321 Å

\*Values in parentheses are  $\pm 3\sigma$ , based on the error associated with the Reitveld refinement.

\*\* Values in parentheses are  $\pm 1\sigma$ . For XPS, the standard deviation is determined from of the average of two replicate spot analyses collected for each sample.

219

220 The formation of goethite instead of magnetite,<sup>18, 34-35</sup> or hercynite (as predicted by

221 Pourbaix diagrams presented in the SI), suggests that the solid product is also heavily influenced

222 by co-mingled constituents. As previously mentioned, an Fe(OH)<sub>2</sub>(s):simulant ratio of ~200 g/L

223 removes ~45% (~12,200 mg/L) of the simulant nitrite and ~45% of Al(III) (SI Figure S1). As

224 nitrite reduction continues, the ratio of Fe(III) to Fe(II) increases, as does the OH/Fe ratio, both

225 of which favor the formation of goethite over magnetite.<sup>36</sup> As goethite forms and Tc(VII) is

226 reduced to Tc(IV), incorporation of Tc(IV) into the goethite structure likely occurs via

227 substitution for Fe(III) due to their identical, six coordinate crystal radii (0.785 Å).<sup>27, 37-38</sup>

228 Substitution of Tc(IV) is not expected to significantly influence the bulk mineral phase

229 distribution determined by XRD nor change the goethite lattice parameters. Although charge

230 balance via Fe(II) substitution for Fe(III) may expand the lattice at concentrations higher than

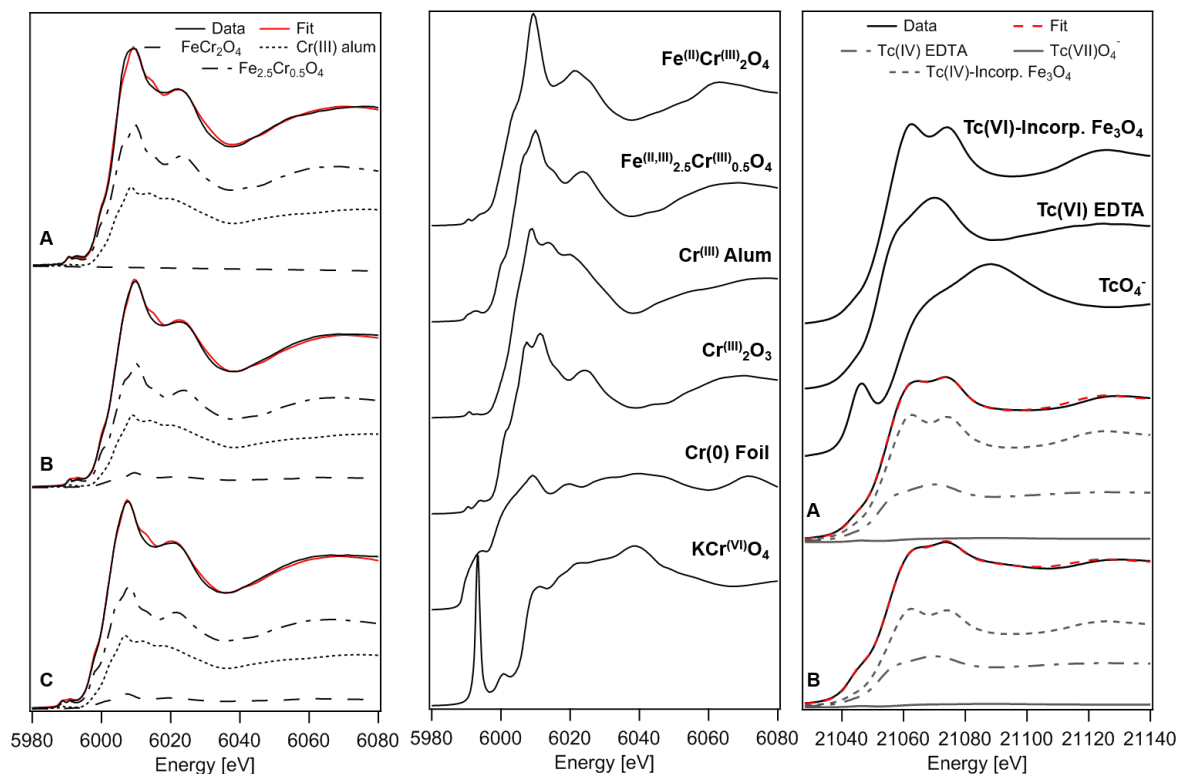
231 those tested here.<sup>10</sup>

232 In contrast, Cr(III) and/or Al(III) substitution into goethite would cause a decrease in  
233 calculated goethite lattice parameters since the crystal radius of six coordinate Cr(III), 0.755 Å,  
234 and Al(III), 0.670 Å, are smaller than Fe(III).<sup>33, 38-42</sup> Reitveld analysis of collected XRD patterns  
235 (Table 2 **Error! Reference source not found.**) provides the unit cell parameters  $a$ ,  $b$ , and  $c$  for  
236 goethite in the absence of Tc. All parameters decrease relative to unsubstituted goethite with  
237 increasing Fe(OH)<sub>2</sub>(s):simulant ratio.<sup>33</sup> This trend is indicative of increased substitution for  
238 Fe(III) by Cr(III) and/or Al(III) in goethite as both constituents are removed from the simulant  
239 (Figure 1 and SI Figure S1).

240 *Bulk Solid Phase Cr Speciation Determined by XANES:* Three samples were analyzed by  
241 XANES at SSRL to determine the bulk oxidation state and speciation of Cr following reduction  
242 and removal by Fe(OH)<sub>2</sub>(s) (Figure 2, left panel). As a control, one of the analyzed samples  
243 (LAW-50-0Tc) was prepared without Tc and at the minimum Fe(OH)<sub>2</sub>(s):simulant ratio needed  
244 to remove Cr(VI) from solution, 50 g/L. The remaining two samples were prepared with 100  
245 ppm Tc(VII) at two different Fe(OH)<sub>2</sub>(s):simulant ratios: 50 g/L (LAW-50-100Tc) and 200 g/L  
246 (LAW-200-100Tc). Linear combination analysis (LCA) of each sample initially considered six  
247 possible Cr standards: Cr foil, Cr<sub>2</sub>O<sub>3</sub>, Cr alum (KCr(SO<sub>4</sub>)<sub>2</sub>•12H<sub>2</sub>O, Cr(III) octahedrally  
248 coordinated by water), Fe<sub>2.5</sub>Cr<sub>0.5</sub>O<sub>4</sub>, FeCr<sub>2</sub>O<sub>4</sub>, and K<sub>2</sub>CrO<sub>4</sub> (Figure 2, middle panel). It is  
249 important to note that Cr(III) forms octahedrally coordinated species both in ordered (iron-  
250 containing oxides) and disordered environments. According to XRD results (Table 2), Cr would  
251 be incorporated into goethite, not spinel phases such as chromite (FeCr<sub>2</sub>O<sub>4</sub>) or Fe<sub>2.5</sub>Cr<sub>0.5</sub>O<sub>4</sub>.  
252 However, without a Cr-substituted goethite standard, Fe<sub>2.5</sub>Cr<sub>0.5</sub>O<sub>4</sub> and FeCr<sub>2</sub>O<sub>4</sub> standards are  
253 used here to represent the ordered octahedral environment expected for Cr-substituted goethite.<sup>43</sup>  
254 Furthermore, the disordered octahedral symmetry of Cr(III) in Cr alum<sup>44</sup> is assumed to represent

255 Cr(III) that has formed separate from the iron phase, e.g.,  $\text{Cr}(\text{OH})_3$  or an amorphous phase with a  
256 similar local structure.<sup>45</sup> Standards that did not contribute significantly to the LCA fit (value <  
257  $2\sigma$ ) were removed and the data refit using the remaining standards. The final Cr LCA results are  
258 shown in Table 3.

259 For all samples, the absence of the prominent Cr(VI) pre-edge feature confirms that Cr is  
260 present as Cr(III) and supports the proposed solution removal mechanism that requires Cr(VI)  
261 reduction to Cr(III). Furthermore, all samples contained Cr alum (35 – 38 %) and  $\text{Fe}_{2.5}\text{Cr}_{0.5}\text{O}_4$   
262 (58 – 62 %) as the major phases present regardless of  $\text{Fe}(\text{OH})_2$ :simulant ratio, although for the  
263 two samples with a  $\text{Fe}(\text{OH})_2$ (s):simulant ratio of 50 g/L a small contribution of  $\text{FeCr}_2\text{O}_4$  (6 %)  
264 was also determined. Overall, given the low solubility of Cr(III)-containing solids, Cr present in  
265 these samples is less susceptible to re-oxidation and release into the environment and exhibits a  
266 similar removal mechanism despite changes in Fe(II) resources and Tc(VII) presence.



267

268 **Figure 2.** (Left) Normalized and off-set Cr K edge XANES spectra with corresponding LCA fits  
 269 for Fe(OH)<sub>2</sub>(s):Simulant ratios (A) 200 g/L, 100 ppm Tc(VII), (B) 50 g/L, 100 ppm Tc(VII), and  
 270 (C) 50 g/L, no Tc(VII). The LCA fit (red) to the data (black) is the sum of the standard  
 271 contributions from FeCr<sub>2</sub>O<sub>4</sub> (dash line), Fe<sub>2.5</sub>Cr<sub>0.5</sub>O<sub>4</sub> (dot/dash line), and Cr alum (dotted line)  
 272 determined in the final fit. (Middle) Cr standards considered during LCA fitting, off-set for  
 273 clarity. (Right) Normalized and off-set Tc K-edge XANES spectra (black) for samples A and B  
 274 from left panel and the final Tc standards used during LCA fitting. The Tc LCA fit (red dashed  
 275 line) is the sum of the standard contributions from TcO<sub>4</sub><sup>-</sup> (line), TcEDTA (dot/dash), and Tc-  
 276 incorporated Fe<sub>3</sub>O<sub>4</sub> (dash).

277

278 **Table 3.** LCA and EXAFS Results from Cr and Tc K Edge XANES and EXAFS Spectra

Sample		LAW-50-0Tc	LAW-50-100Tc	LAW-200-100Tc
Fe(OH) <sub>2</sub> (s):Simulant Ratio	g/L	50	50	200
Starting [Tc(VII)]	ppm	0	100	100
<b>Cr XANES LCA Analysis</b>				
Cr Alum (KCr(SO <sub>4</sub> ) <sub>2</sub> •12H <sub>2</sub> O)	%	35(1)	35(1)	38(4)
	p*	<0.001	<0.001	<0.001
Fe <sub>2.5</sub> Cr <sub>0.5</sub> O <sub>4</sub>	%	58(2)	59(2)	62(4)
	p	<0.001	<0.001	<0.001
FeCr <sub>2</sub> O <sub>4</sub>	%	6(1)	6(1)	-
	p	0.287	0.304	-
<b>Tc XANES LCA Analysis</b>				
TcO <sub>4</sub> <sup>-</sup>	%	-	27.2(2)	9.0(3)
	p	-	<0.001	<0.001

Tc(IV) Incorporated Fe <sub>3</sub> O <sub>4</sub>	%	-	49(1)	63(1)
	p	-	<0.001	<0.001
Tc(IV) EDTA	%	-	26(1)	30(1)
	p	-	<0.001	<0.001
<b>Tc EXAFS Analysis</b>				
TcO <sub>4</sub> <sup>-</sup>	%	-	33(6)	0(0)
TcO <sub>2</sub> ·2H <sub>2</sub> O	%	-	32(8)	67(6)
Goethite	%	-	35(3)	33(6)

Values in parenthesis indicate the standard deviation of the last significant figure.

(-) No Detected

(\*) Probability that the improvement to the fit by adding the scattering shell is due to random error. A p value < 0.05 indicates that the improvement is greater than 2σ of the fit.

279

280 *Cr Speciation of the Solid Surface Determined by XPS:* Cr speciation was also analyzed by XPS

281 for select solid samples. XPS analysis is specific to the top 5 – 10 nm of the sample surface;

282 however, surface specificity may be limited here due to the small goethite crystal size (~10 nm)

283 determined by Reitveld refinements (Table 2 **Error! Reference source not found.**). Narrow,

284 high resolution scans for Cr are shown in Figure S2 for three Cr-containing solid samples with

285 Fe(OH)<sub>2</sub>(s):simulant ratios of 50, 100, and 200 g/L, where the 200 g/L sample was prepared with

286 100 ppm of Tc(VII). Peak fitting was performed only for the Cr 2p<sub>3/2</sub> peak. A single fitting

287 peak was used to account for surface Cr(VI), with three species considered for Cr(III): Cr<sub>2</sub>O<sub>3</sub>,

288 CrOOH, and Cr(OH)<sub>3</sub>. Chromite, FeCr<sub>2</sub>O<sub>4</sub>, was initially considered, but did not significantly

289 contribute to any of the sample fits as expected based on XRD and XANES results. CrOOH

290 accounts for Cr(III) oxyhydroxides and/or partial incorporation into goethite. A summary of the

291 Cr-phase distribution is provided in Table 2.

292 From XPS survey scans it is apparent that Cr only accounts for 0.13-1.6 atomic % of the

293 analyzed area, with Cr increasing with decreasing Fe(OH)<sub>2</sub>(s):simulant ratio. A minor amount of

294 Cr(VI), presumably loosely adsorbed to the sample, was detected in all samples (1.3 – 8.3 atomic

295 %). Cr(OH)<sub>3</sub> was the least abundant Cr(III) species detected, decreasing from 24.7(2) atomic %

296 to 1(2) atomic % with increasing Fe(OH)<sub>2</sub>(s):simulant ratio. However, distribution between the

297 two most abundant Cr(III) species, CrOOH and Cr<sub>2</sub>O<sub>3</sub>, did not indicate preferential formation of  
298 one species over the other as a function of Fe(OH)<sub>2</sub>(s):simulant ratio. Although, within error,  
299 CrOOH arguably dominates, accounting for ≤59 atomic % of surface Cr (LAW-200-100Tc).  
300 This corroborates conclusions derived from XANES analysis and suggests that Cr substitution  
301 into goethite is the favored mechanism for immobilization.

302 *Tc Speciation Determined by XANES and XPS:* The oxidation state of Tc immobilized in the  
303 solid was determined by LCA of collected Tc K-edge XANES spectra. The Tc K-edge spectra  
304 for LAW-200-100Tc and LAW-50-100Tc (Fe(OH)<sub>2</sub>(s):simulant ratios 200 g/L and 50 g/L,  
305 respectively, each with 100 ppm of Tc(VII)) and the standards used for LCA are provided in  
306 Figure 2 (right panel). Initially, LCA considered five Tc standards: TcO<sub>4</sub><sup>-</sup>, TcEDTA,<sup>24</sup>  
307 TcO<sub>2</sub>·xH<sub>2</sub>O,<sup>24</sup> Tc-incorporated Fe<sub>3</sub>O<sub>4</sub> (magnetite),<sup>12</sup> and Tc(V)POM.<sup>46</sup> Standards determined not  
308 to contribute significantly to the fit (value < 2σ) were removed, such that the only standards  
309 included in the final LCA fits were Tc(VII)O<sub>4</sub><sup>-</sup>, Tc(IV)-incorporated magnetite, which represents  
310 Tc(IV) in an ordered iron oxide octahedral environment (as in goethite), and Tc(IV)EDTA,  
311 which represents Tc(IV) in a disordered octahedral environment, e.g., surface sorbed, even  
312 though EDTA is not present in the sample.

313 With an increase in Fe(OH)<sub>2</sub>(s), the amount of Tc(IV) incorporated into iron oxide  
314 increases from 49(1)% (LAW-50-100Tc) to 63(1)% (LAW-200-100Tc). The remaining Tc(IV),  
315 modeled as Tc(IV)EDTA, is presumably sorbed or loosely incorporated at the surface of the  
316 solid where a disordered octahedral environment would be expected. Tc(IV) EDTA contributions  
317 also remain relatively consistent between samples, 26(1)-30(1)%. Any remaining Tc is present as  
318 Tc(VII)O<sub>4</sub><sup>-</sup> and decreases from 27.2(2)% to 9.0(3)% with increasing Fe(OH)<sub>2</sub>(s):simulant ratio.  
319 The presence of Tc(VII) in LAW-200-100Tc is unsurprising considering a 200 g/L



320 Fe(OH)<sub>2</sub>(s):simulant ratio is the requirement to remove 1 ppm of Tc(VII) from the simulant  
321 (Figure 1), not 100 ppm of Tc(VII) as present in this sample.

322 When Tc speciation was analyzed for LAW-200-100Tc by XPS, the results were  
323 significantly different from the bulk, with an almost equal distribution of Tc(VII) and Tc(IV)  
324 (Table 2). This difference is likely due to facile reoxidation of surface adsorbed Tc(IV) relative  
325 to Tc(IV) incorporated into the mineral. Such sensitivity to reoxidation is one difference between  
326 Tc and Cr behavior in this system, since reduction of Cr(VI) produces stable, insoluble phases  
327 including Cr(OH)<sub>3</sub> and Cr<sub>2</sub>O<sub>3</sub> that do not require Cr incorporation into iron oxide/hydroxide  
328 phases. Additionally, these results suggest that some surface specificity is provided by XPS,  
329 despite the small goethite crystal size, or that goethite crystallites have agglomerated into larger  
330 particles. It is important to note that Tc comprises only 0.14(3) atomic % of the LAW-200-100Tc  
331 surface and was calculated while only considering Tc, Cr, Fe, O, and Cr constituents; therefore,  
332 this contribution may be in fact lower.

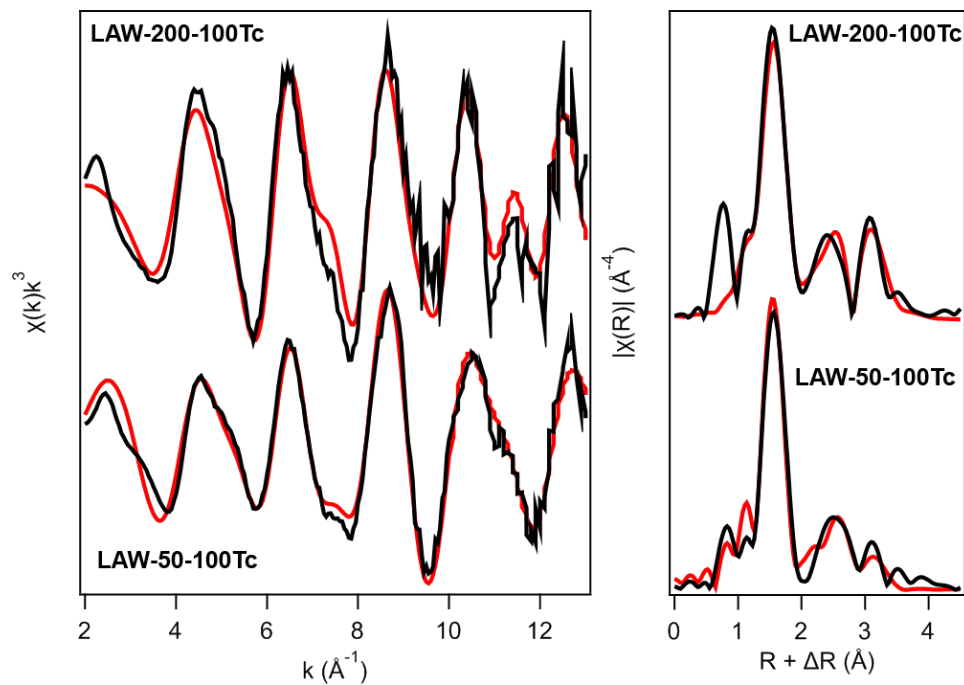
333 *Local Coordination Environment of Tc in the Solid:* To evaluate how Tc(IV) is immobilized in  
334 the solid, the local coordination environment of Tc in samples LAW-50-100Tc and LAW-200-  
335 100Tc was determined using EXAFS. Goethite<sup>39,47</sup> and magnetite<sup>25</sup> models, modified to account  
336 for Tc substitution for Fe(III), were initially used to fit the EXAFS spectra. Difficulties  
337 distinguishing between iron oxide/hydroxide environments is not uncommon, especially when  
338 Tc(IV) is divided among several species.<sup>6, 27, 48-49</sup> In addition, the local environment of Fe(III) in  
339 goethite is similar to that of the octahedral site of magnetite. In goethite, there are 4 Fe neighbors  
340 at 3.1 Å and an additional 4 Fe neighbors at 3.6 Å while in magnetite, there are 6 Fe neighbors at  
341 3.0 Å and 6 at 3.5 Å. EXAFS analysis can determine distances more precisely (0.02 Å error)  
342 than coordination numbers (20% error). For each sample, the R-factor determined using the

343 magnetite model was comparable if not better than the R-factor determined using the goethite  
344 model. Furthermore, F-test results for evaluating the probability that an included scattering shell  
345 contributes significantly to the EXAFS fit (SI Table S5) also favored the magnetite model.  
346 However, given the increase in Tc-Fe bond lengths determined during fitting, which more  
347 closely match the Fe-Fe bond lengths in goethite rather than magnetite, and the results from  
348 XRD and XPS analyses, it is unlikely that magnetite is present in the solid phase. Therefore, Tc-  
349 substituted goethite is assumed to be the most representative model and accounts for 30(8)% and  
350 33(6)% of Tc in samples LAW-50-100Tc and LAW-200-100Tc, respectively (Table 3). This  
351 distribution is lower than the range determined by XANES LCA, 49-63%, where a Tc-  
352 incorporated magnetite standard is used to account for the ordered structural environment of the  
353 iron (oxy)hydroxide phase rather than a goethite standard or model as used in the EXAFS  
354 interpretation.

355 In addition to goethite, including  $\text{TcO}_2 \cdot 2\text{H}_2\text{O}$  into the sample fits was required to account  
356 for the portion of Tc(IV) sorbed or partially incorporated at the goethite surface. Tc(IV) sorbed  
357 as  $\text{TcO}_2 \cdot 2\text{H}_2\text{O}$  requires incorporation of a Tc–Tc neighbor (bond length  $\sim 2.57 \text{ \AA}$ ) and a long Tc–  
358 O bond ( $\sim 2.47 \text{ \AA}$ ) that accounts for the hydrated oxygen.<sup>24</sup> Although, in instances where Tc may  
359 be partially incorporated into goethite, accounting for the long Tc – O bond often does not  
360 significantly contribute to the EXAFS fit.<sup>18</sup> With this modification to the EXAFS fit, 67(6) % of  
361 Tc was found to be present as sorbed or partially incorporated Tc(IV) in LAW-200-100Tc with  
362 the hydrated Tc-O scatter pathway contributing significantly to the fit as indicated by a p value  
363 (0.019) less than 0.05. For LAW-50-100Tc, including the long Tc–O bond did not significantly  
364 contribute to the fit, thus suggesting partial incorporation of Tc(IV) into the solid phase of up to  
365 42(7) %. This expansion to the sample EXAFS models aligns with interpretation of the XANES

366 spectra, which indicated that  $\geq 26\%$  of Tc(IV) is not completely incorporated into the iron  
367 oxide/hydroxide solid.

368 Finally, for LAW-50-100Tc, where the  $\text{Fe}(\text{OH})_2(\text{s})$ :simulant ratio is too low to reduce  
369 and immobilize all of the Tc present in solution,  $\text{TcO}_4^-$  was also included in the EXAFS fit and  
370 accounted for 28(3)% of bulk Tc in the solid.  $\text{TcO}_4^-$  may persist as a dissolved species in  
371 moisture retained by the sample between packaging and analysis or, if dried, as a pertechnetate  
372 salt, e.g.  $\text{NaTcO}_4$ . Despite XANES indication LAW-200-100Tc contains 9% Tc(VII),  
373 incorporating Tc(VII) into the EXAFS fit did not significantly improve the fit. The collected  
374 EXAFS spectra, their Fourier transforms, and final fits are shown in Figure 3.



375

376 **Figure 3.** EXAFS spectra (left) and their Fourier transforms (right) for Tc-containing samples  
377 LAW-200-100Tc (200 g/L  $\text{Fe}(\text{OH})_2(\text{s})$ :simulant ratio, 100 ppm Tc(VII)) and LAW-50-100Tc  
378 (50 g/L  $\text{Fe}(\text{OH})_2(\text{s})$ :simulant ratio, 100 ppm Tc(VII)). EXAFS fits (red) are based on a  
379 combination of Tc-incorporated goethite,  $\text{TcO}_2 \cdot 2\text{H}_2\text{O}$ , and  $\text{TcO}_4^-$  (LAW-50-100Tc only) models.

#### 380 4. Environmental Implications

381 One implication asserted after the first demonstration of Tc reduction and removal in the  
382 presence of Cr by  $\text{Fe}(\text{OH})_2(\text{s})$ , was that  $\text{Fe}(\text{OH})_2(\text{s})$  could be introduced into Hanford LAW to  
383 form Tc-incorporated magnetite, which would stabilize Tc, decrease its volatility during  
384 vitrification, and increase Tc loading in glass waste forms.<sup>18</sup> However, laboratory simulations of  
385  $\text{Fe}(\text{OH})_2(\text{s})$  addition to LAW indicate that the amount of  $\text{Fe}(\text{OH})_2(\text{s})$  required to remove Tc and  
386 Cr is approximately one order of magnitude larger than the control system. Such a large increase  
387 in  $\text{Fe}(\text{OH})_2(\text{s})$  required to address Cr and Tc in LAW may adversely affect the final glass waste  
388 form. Furthermore, under vitrification temperatures the stability of Tc is more favorable when  
389 incorporated into the iron (oxy)hydroxide phase compared to  $\text{TcO}_2 \cdot 2\text{H}_2\text{O}$ .<sup>6</sup> As such, this system  
390 would benefit from near complete incorporation of Tc into the goethite phase, which may require  
391 additional  $\text{Fe}(\text{OH})_2(\text{s})$  (>200 g/L). To this end  $\text{Fe}(\text{OH})_2(\text{s})$  may be more appropriately used as a  
392 localized remediation strategy for environmental contamination or for treating the less redox-  
393 sensitive melter off-gas and secondary waste streams where the concentrations of  $\text{Cr}(\text{VI})$ ,  $\text{NO}_2^-$ ,  
394 and other anions do not overwhelm the concentration of  $\text{Tc}(\text{VII})$  by orders of magnitude.

## 395 **5. Supporting Information**

396 Additional analysis procedures and results for IC/ICP-MS, XPS, and EXAFS are provided in the  
397 supporting information via the Internet at <http://pubs.acs.org>.

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414

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556 Tables.

557 **Table 1.** 5 M Na Average LAW Simulant Composition

Constituent	Target Concentration [mg/L]*	Concentration [mg/L]	Constituent	Target Concentration [mg/L]*	Concentration [mg/L]
Al	8280	8500	F <sup>-</sup>	600	<1000
Cr	1120	1080	Cl <sup>-</sup>	1500	<2500
P	1520	981	NO <sub>2</sub> <sup>-</sup>	26,000	26,800
K	1280	1300	Br <sup>-</sup>	-	<5000
Na	115,000	110,000	NO <sub>3</sub> <sup>-</sup>	101,000	102,000
S	2740	2810	SO <sub>4</sub> <sup>-</sup>	-	10,100
Ti	-	7.84	PO <sub>4</sub> <sup>-</sup>	-	<7500
pH		13.5			

\* Target Concentrations from Russell et al, 2013.<sup>17</sup>

-: Not identified

558

559 **Table 2.** XRD and High Resolution XPS Analysis of Select Solid Phases

Sample		LAW-50-0Tc-1	LAW-100-0Tc	LAW-200-100Tc
Fe(OH) <sub>2</sub> (s):Simulant Ratio	<i>g/L</i>	50	100	200
Starting [Tc(VII)]	<i>ppm</i>	0	0	100
<i>XRD Analysis</i>				
Goethite ( $\alpha$ -FeOOH)	<i>wt%</i>	77	81	-
	a ( $\text{\AA}$ )*	4.602(2)	4.597(3)	-
	b ( $\text{\AA}$ )*	9.920(3)	9.913(2)	-
	c ( $\text{\AA}$ )*	3.0096(9)	3.0080(9)	-
Crystal Size	( <i>nm</i> )**	9.8(1)	10.7(1)	-
Feroxyhyte ( $\delta$ -FeOOH)	<i>wt%</i>	17	14	-
Hematite (Fe <sub>2</sub> O <sub>3</sub> )	<i>wt%</i>	-	3	-
Amorphous/Unidentified	<i>wt%</i>	6	1	-
<i>Survey XPS Analysis</i> **				
Cr 2p	<i>at %</i> *	1.6(1)	1.1(1)	0.13(1)
Tc 3d	<i>at %</i>	-	-	0.14(3)
Fe 2p	<i>at %</i>	7.3(4)	8.4(8)	1.7(2)
C 1s	<i>at %</i>	27(4)	19(6)	24(1)
O 1s	<i>at %</i>	64(3)	71(5)	74(1)
<i>Cr XPS Analysis</i> **				
CrOOH	<i>at %</i>	46(1)	38(14)	59(2)
Cr <sub>2</sub> O <sub>3</sub>	<i>at %</i>	28(10)	43(19)	32(4)
Cr(OH) <sub>3</sub>	<i>at %</i>	24.7(2)	18(5)	1(2)
Cr(VI)	<i>at %</i>	1.5	1.3(5)	8.3(8)
<i>Tc XPS Analysis</i> **				
Tc(VII)	<i>at %</i>	-	-	52(1)
Tc(IV)	<i>at %</i>	-	-	48(1)
<i>Fe XPS Analysis</i> **				
FeCr <sub>2</sub> O <sub>4</sub>	<i>at %</i>	0	0	5.7(2)
Fe <sub>3</sub> O <sub>4</sub>	<i>at %</i>	12(1)	11(2)	11(1)
FeOOH	<i>at %</i>	88(1)	89(2)	83(1)

(-) No Detected or Analyzed (\*) Atomic percent

Goethite ( $\alpha$ -FeOOH)<sup>33</sup>: a = 4.634 Å, b = 9.945 Å, c = 3.0321 Å

\*Values in parentheses are  $\pm 3\sigma$ , based on the error associated with the Reitveld refinement.

\*\* Values in parentheses are  $\pm 1\sigma$ . For XPS, the standard deviation is determined from of the average of two replicate spot analyses collected for each sample.

560

561 **Table 3.** LCA and EXAFS Results from Cr and Tc K Edge XANES and EXAFS Spectra

Sample		LAW-50-0Tc	LAW-50-100Tc	LAW-200-100Tc
Fe(OH) <sub>2</sub> (s):Simulant Ratio	g/L	50	50	200
Starting [Tc(VII)]	ppm	0	100	100
<b>Cr XANES LCA Analysis</b>				
Cr Alum (KCr(SO <sub>4</sub> ) <sub>2</sub> •12H <sub>2</sub> O)	%	35(1)	35(1)	38(4)
	p*	<0.001	<0.001	<0.001
Fe <sub>2.5</sub> Cr <sub>0.5</sub> O <sub>4</sub>	%	58(2)	59(2)	62(4)
	p	<0.001	<0.001	<0.001
FeCr <sub>2</sub> O <sub>4</sub>	%	6(1)	6(1)	-
	p	0.287	0.304	-
<b>Tc XANES LCA Analysis</b>				
TcO <sub>4</sub> <sup>-</sup>	%	-	27.2(2)	9.0(3)
	p	-	<0.001	<0.001
Tc(IV) Incorporated Fe <sub>3</sub> O <sub>4</sub>	%	-	49(1)	63(1)
	p	-	<0.001	<0.001
Tc(IV) EDTA	%	-	26(1)	30(1)
	p	-	<0.001	<0.001
<b>Tc EXAFS Analysis</b>				
TcO <sub>4</sub> <sup>-</sup>	%	-	33(6)	0(0)
TcO <sub>2</sub> •2H <sub>2</sub> O	%	-	32(8)	67(6)
Goethite	%	-	35(3)	33(6)

Values in parenthesis indicate the standard deviation of the last significant figure.

(-) No Detected

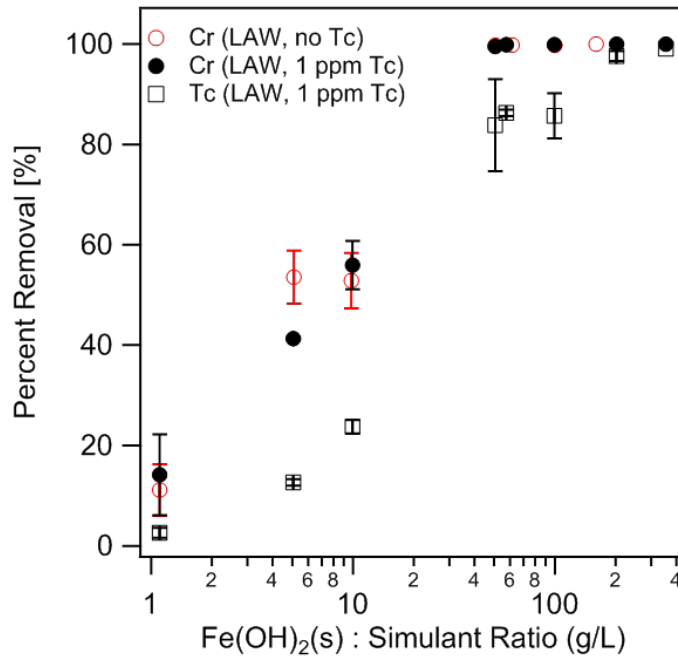
(\*) Probability that the improvement to the fit by adding the scattering shell is due to random error. A p value < 0.05 indicates that the improvement is greater than 2σ of the fit.

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564 Figures.

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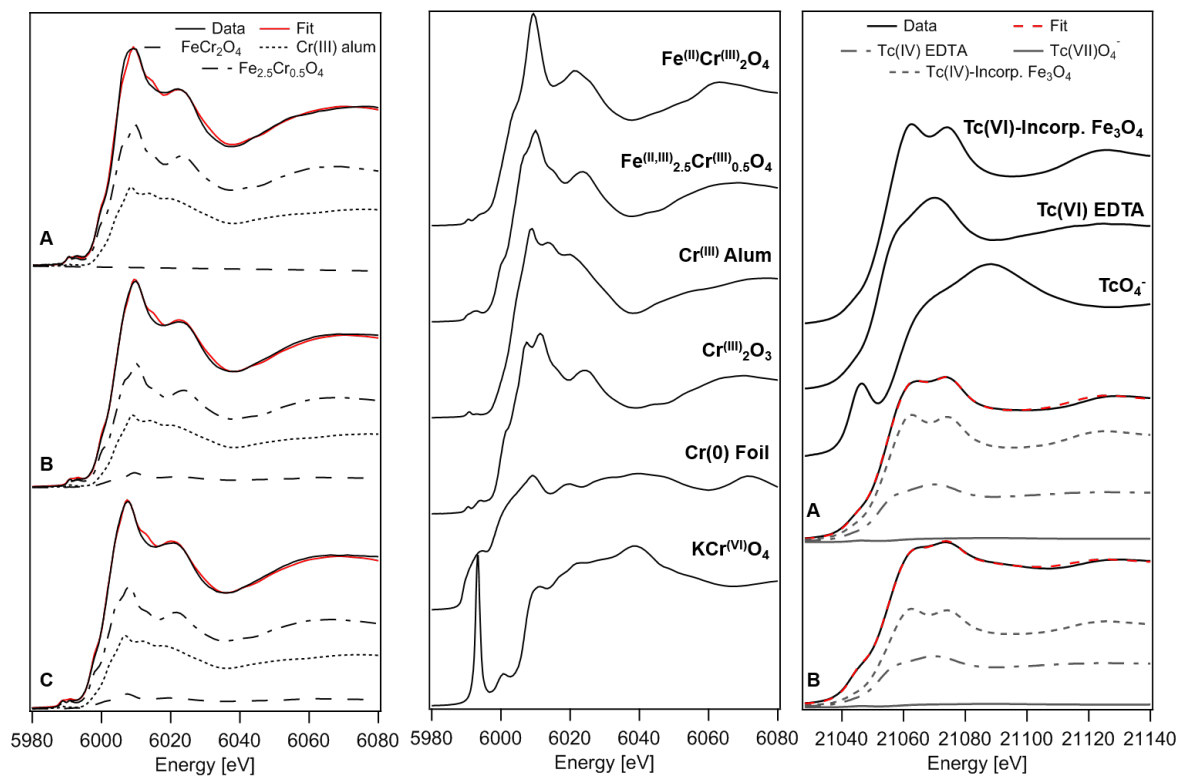


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567 **Figure 1.** Cr and Tc removal from LAW simulant with 1 ppm Tc (black) and without Tc (red).  
568 Cr(VI) results are indicated by filled circles, Tc results by open squares. Error bars represent the  
569 standard deviation of results averaged from two to six replicate samples. Percent removal  
570 assumed to be 100% if below ICP-OES detection limit for Cr (23 µg/L) or ICP-MS detection  
571 limit for Tc (33 ng/L).

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575 **Figure 2.** (Left) Normalized and off-set Cr K edge XANES spectra with corresponding LCA fits  
 576 for Fe(OH)<sub>2</sub>(s):Simulant ratios (A) 200 g/L, 100 ppm Tc(VII), (B) 50 g/L, 100 ppm Tc(VII), and  
 577 (C) 50 g/L, no Tc(VII). The LCA fit (red) to the data (black) is the sum of the standard  
 578 contributions from FeCr<sub>2</sub>O<sub>4</sub> (dash line), Fe<sub>2.5</sub>Cr<sub>0.5</sub>O<sub>4</sub> (dot/dash line), and Cr alum (dotted line)  
 579 determined in the final fit. (Middle) Cr standards considered during LCA fitting, off-set for  
 580 clarity. (Right) Normalized and off-set Tc K-edge XANES spectra (black) for samples A and B  
 581 from left panel and the final Tc standards used during LCA fitting. The Tc LCA fit (red dashed  
 582 line) is the sum of the standard contributions from TcO<sub>4</sub><sup>-</sup> (line), TcEDTA (dot/dash), and Tc-  
 583 incorporated Fe<sub>3</sub>O<sub>4</sub> (dash).

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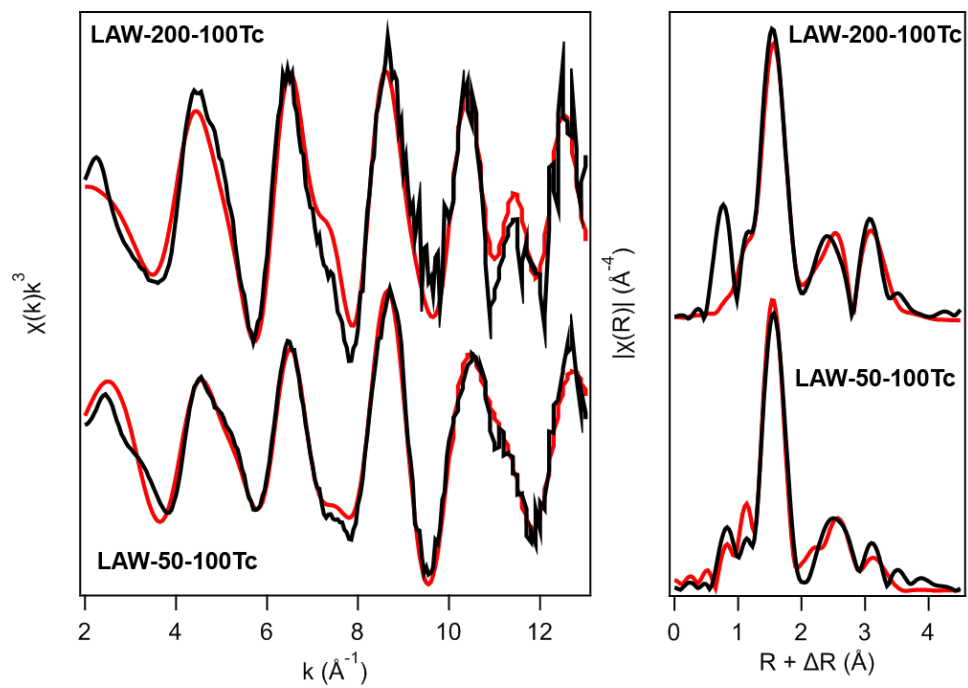
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593 **Figure 3.** EXAFS spectra (left) and their Fourier transforms (right) for Tc-containing samples  
 594 LAW-200-100Tc and LAW-50-100Tc. EXAFS fits (red) are based on a combination of Tc-  
 595 incorporated goethite,  $\text{TcO}_2 \cdot 2\text{H}_2\text{O}$ , and  $\text{TcO}_4^-$  (LAW-50-100Tc only) models.

596