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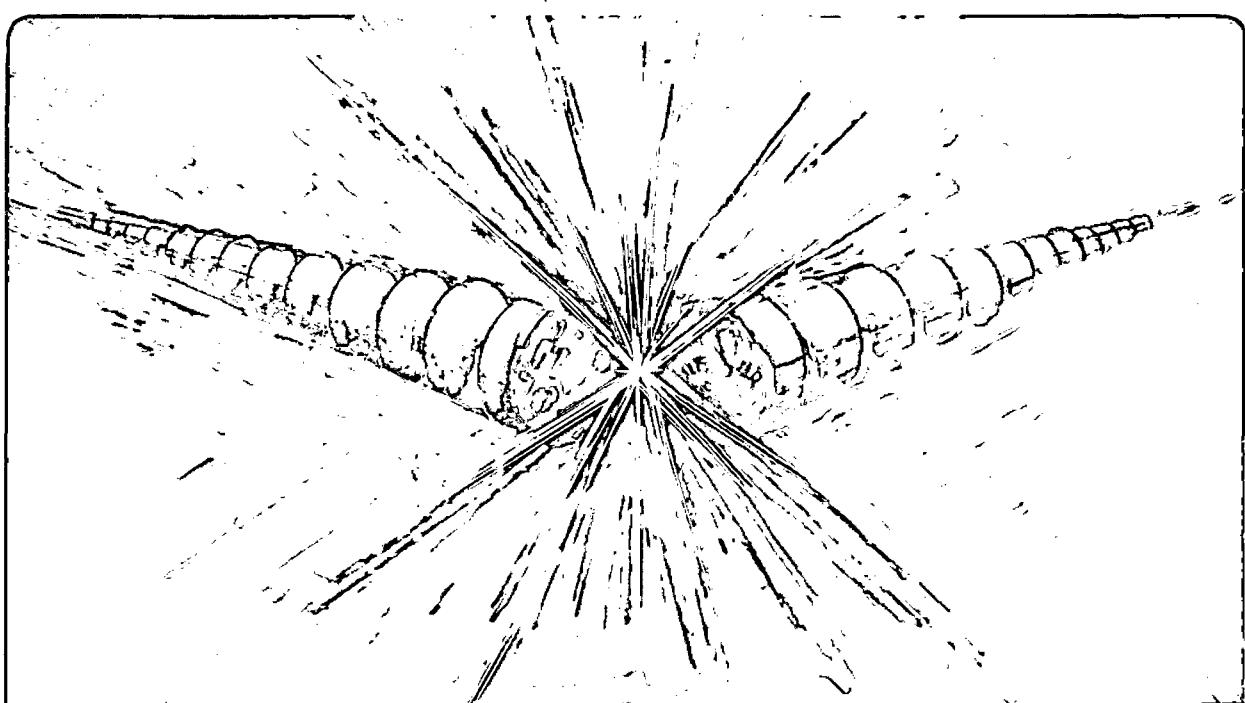
D7H-TEST RESULTS

S. Caspi

July 1982

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D7H-Test Results*

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July 30, 1982

*This work was supported by the Director, Office of Energy Research, Office of High Energy and Nuclear Physics, High Energy Physics Div., U.S. Dept. of Energy, under Contract No. DE-AC03-76SF00098.

D7H-Test Results*

S. Caspi

Data was reduced from the voltage-time relations stored in files D7H001 to D7H090 on HP1000. The I-B calibration curve is included in Fig. 1. The data base is shown in Table 1 and can be used by the 9845B. The data include the quench location, Q₂ layer 1 top, Q₃ layer 1 bottom and the quench current and its normalized value with respect to short sample, I_C = 4920A at 4.4 K, I_C = 6710 A at 1.8 K. The resistance (Ω/cm) was calculated using the propagation time according to the voltage change across the measured sections. The conductor potential length are L_{5,9} = 48.6 cm, L_{6,10} = 17.9 cm, L_{7, 11} = 40.6 cm (Fig. 8). The turn to turn velocity V_t was calculated dividing the nominal turn to turn distance (58 mil) by the propagation time (Trans. Time). The quench time T_q was measured from the time the resistive rise starts until the energy extraction system fires. Figures 2-6 are plots of the data base. The time to energy extracton can be estimated as:

$$T_q = \frac{V_0}{2IR'V} \quad (1)$$

where:

V₀ = trip voltage

R' = resistance per unit length

V = velocity

I = current

For a propagation which is axial only. The discontinuity in T_q (Fig. 4) is due to a drop in the propagation velocity when the temperature was

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lowered from 4.4 K to 1.8 K. Assuming $V_0 = .25$ volt and using I , R' , V values from the data base, equation 1 is plotted in Fig 5.

Resistivity

The resistance per unit length at the normal state is plotted in Fig. 6. The values at the magnet ends vary from $.9$ to $1.3 \mu\Omega/cm$ between 4000A and 7000 A and the straight section values are about 15 percent higher. For a 23 strand cable at 27 mil strand diameter and 1.8/1 S.C/copper ratio the total copper cross section area is $5.46 \times 10^{-2} \text{ cm}^2$. Assuming all the current had been switched to the copper the resistivity is $4.9 \times 10^{-8} - 7.1 \times 10^{-8}$ ($\Omega \text{ cm}$) and the corresponding resistivity ratio is therefore $RRR = 35$ to 20.

The alteration of the quench location between the halves of the inner shell is plotted in Fig.7 and the quench origin around the first inner turn is plotted in Fig. 8. All quenches occurred around the first turn! (The only exceptions were very fast ramp rates).

Temperature Rise

After the normal zone propagates through a measured section, its resistance keeps increasing due to a temperature increase. The resistance rise with respect to time is observed to be linear (Fig. 9) in the time scale before the energy extraction. Converting this values to a resistivity rise the results are given in Table 2. A simplified energy balance result in an approximate temperature-time relation.

$$MC \frac{dT}{dt} = I^2 R \quad (2)$$

$$M = \rho_d l A \quad (\rho_d = \text{density}, l = \text{length}, A = \text{crosssection area})$$

$$R = \rho_r l / A \quad (\rho_r = \text{resistivity})$$

The total mass assumes copper only (e.g. no liquid participation).

Equation (2) reduces to

$$C \frac{dT}{dt} = \frac{\rho_r}{\rho_d} \frac{I^2}{A^2}$$

$$\int C dT = \frac{I^2}{A^2} \frac{1}{\rho_d} \int \rho_r dt$$

The experiment shows that $\rho_r = \rho_r(t) = \alpha t$

therefore,

$$\int C dT = \frac{\alpha}{2\rho_d} \left(\frac{It}{A} \right)^2 \quad (3)$$

Equation (3) was solved for 2 nominal cases using $A = 5.46 \times 10^{-10} \text{ cm}^2$;

$$\rho_d = 8.94 \text{ (gr/cm}^3\text{)}$$

1. File = D7H008 (4.4 K)

$$I = 4220 \text{ A;}$$

$$\alpha = 1.1 \times 10^{-6} \Omega\text{-cm/sec}$$

$$\int C dT = 3.675 \times 10^{-4} \cdot t^2 \quad (t = \text{msec})$$

2. File = D7H061 (2.0 K)

$$I = 6340 \text{ A;}$$

$$\alpha = 2.46 \times 10^{-6} \Omega\text{-cm/sec}$$

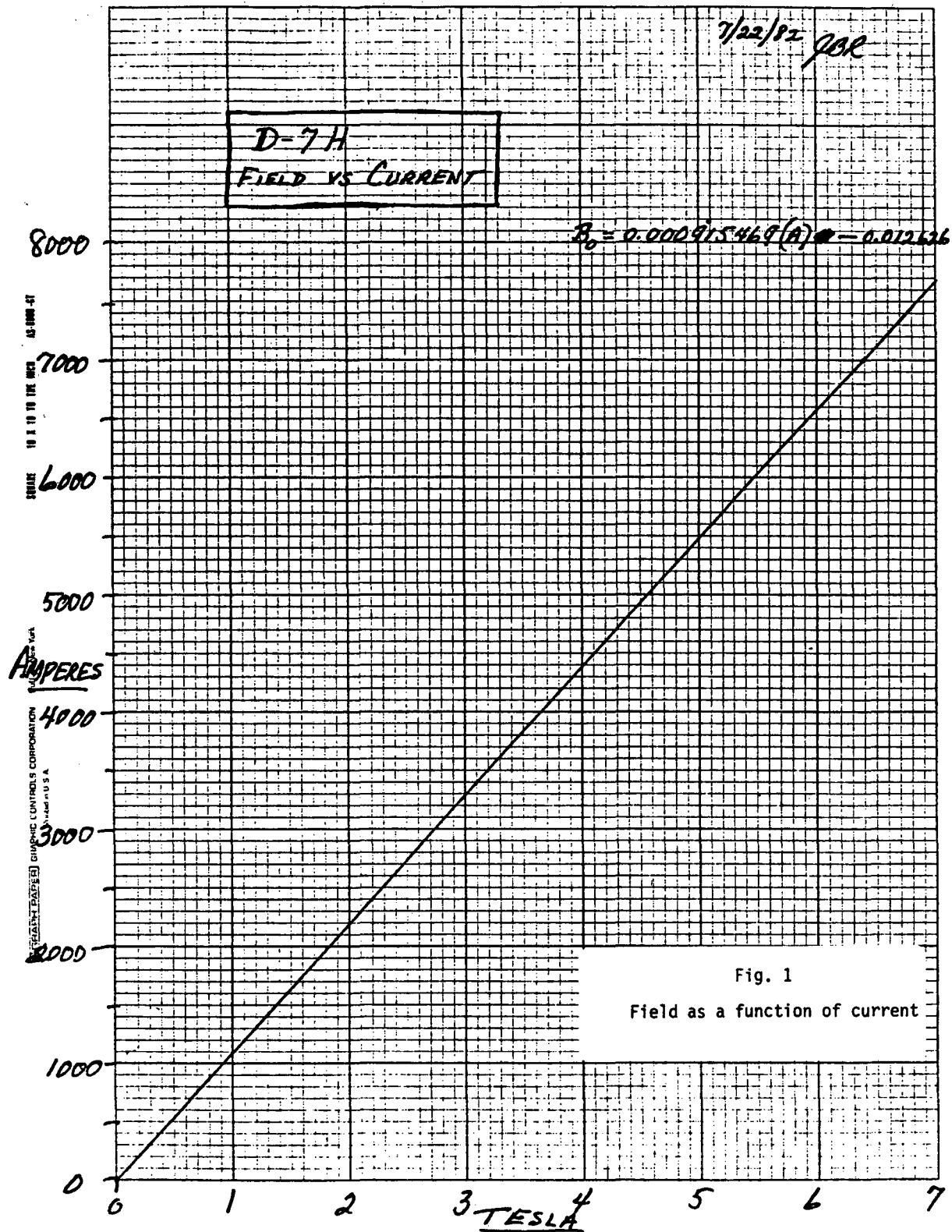
$$\int C dT = 1.855 \times 10^{-3} \cdot t^2 \quad (t = \text{msec})$$

The result from the two cases using integral values of specific heat for copper are shown in Fig. 10.

Magnet Rate Dependence and Losses

The magnet was ramped at various rates and the quench field recorded. Repeating the test both in the He I and He II result in the relations shown in Fig. 11. The normalized field data were then fitted to a parabolic relation and plotted in Fig. 12.

Using our standard procedure in He II to determine energy losses the average heat flux generated during a cycle is plotted in Fig. 13 for a number of different field rates.



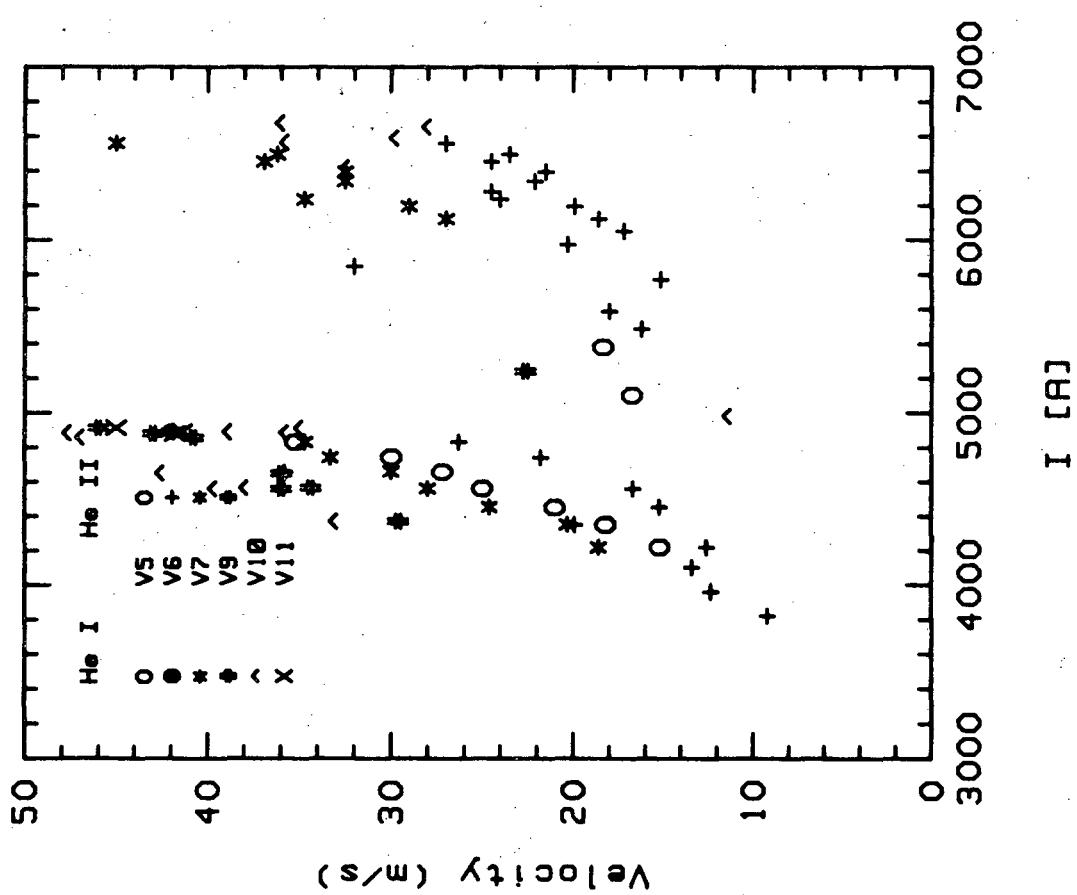
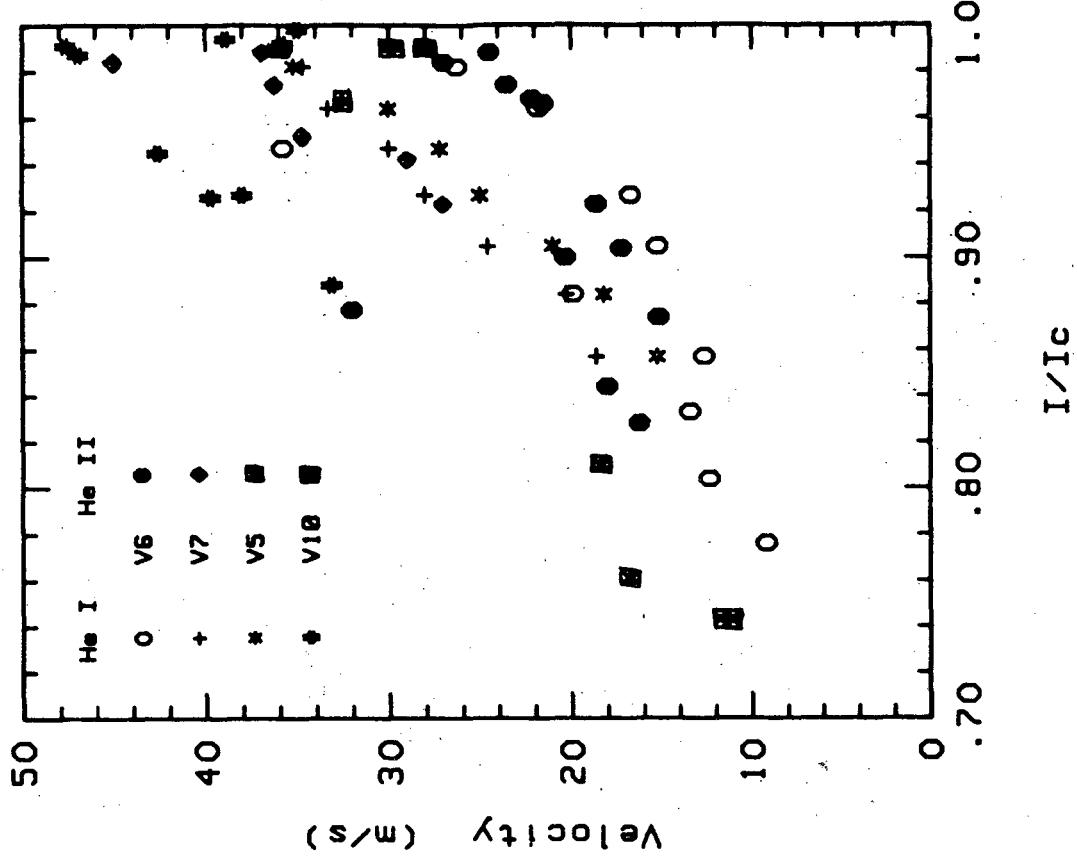


Fig. 2 Axial Velocity

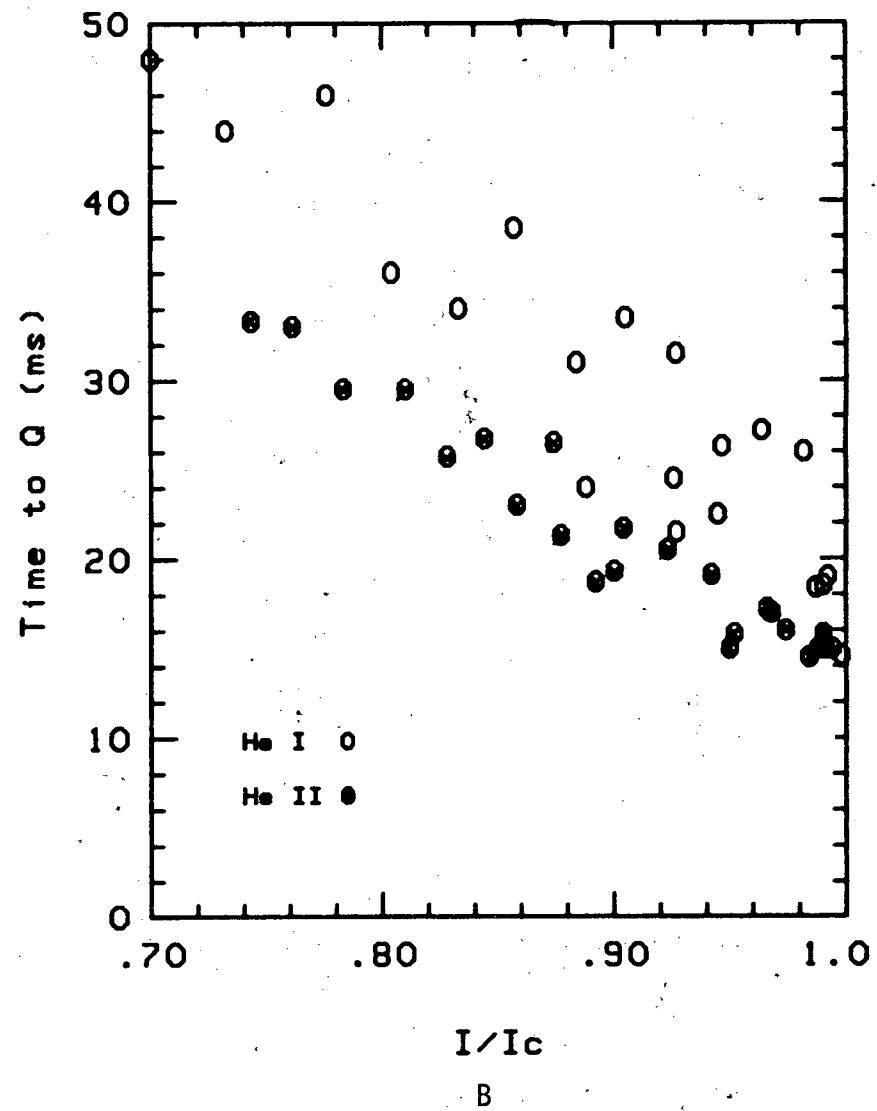
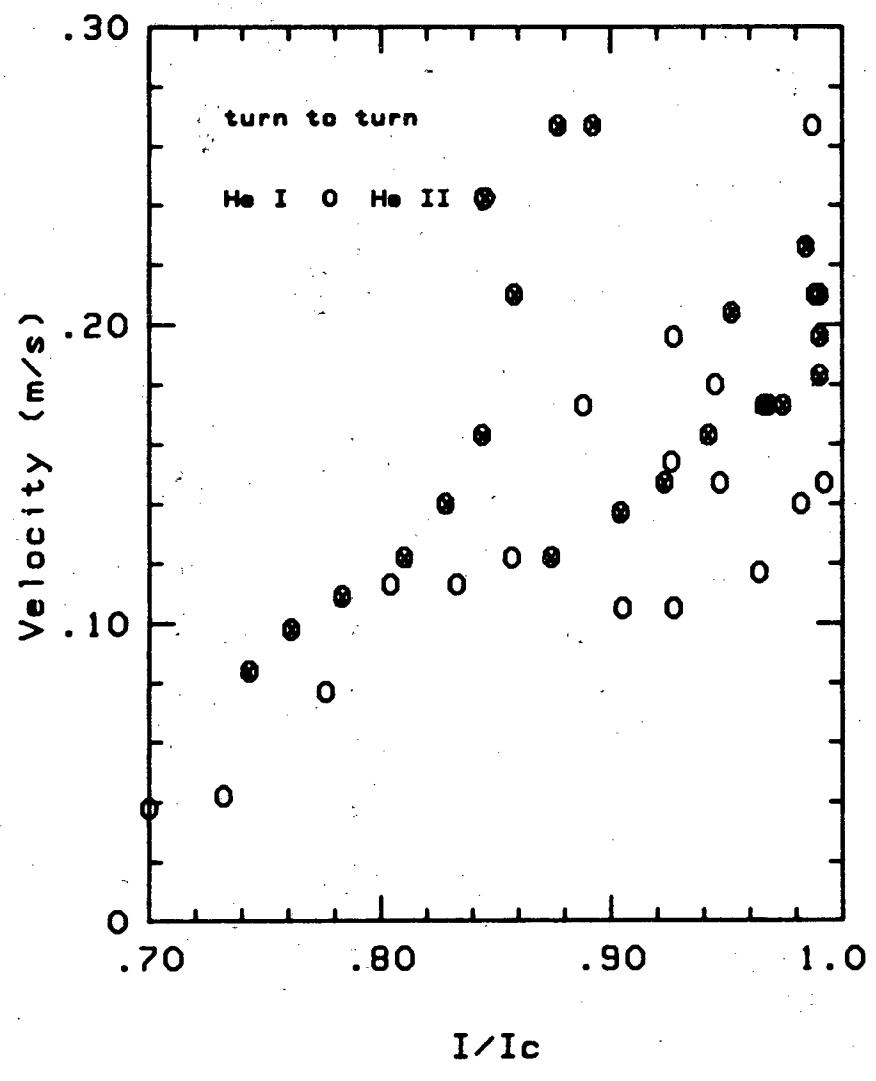


Fig. 3: A) Turn to turn velocity; B) Time from initial resistive rise to energy extraction as a function of normalized current.

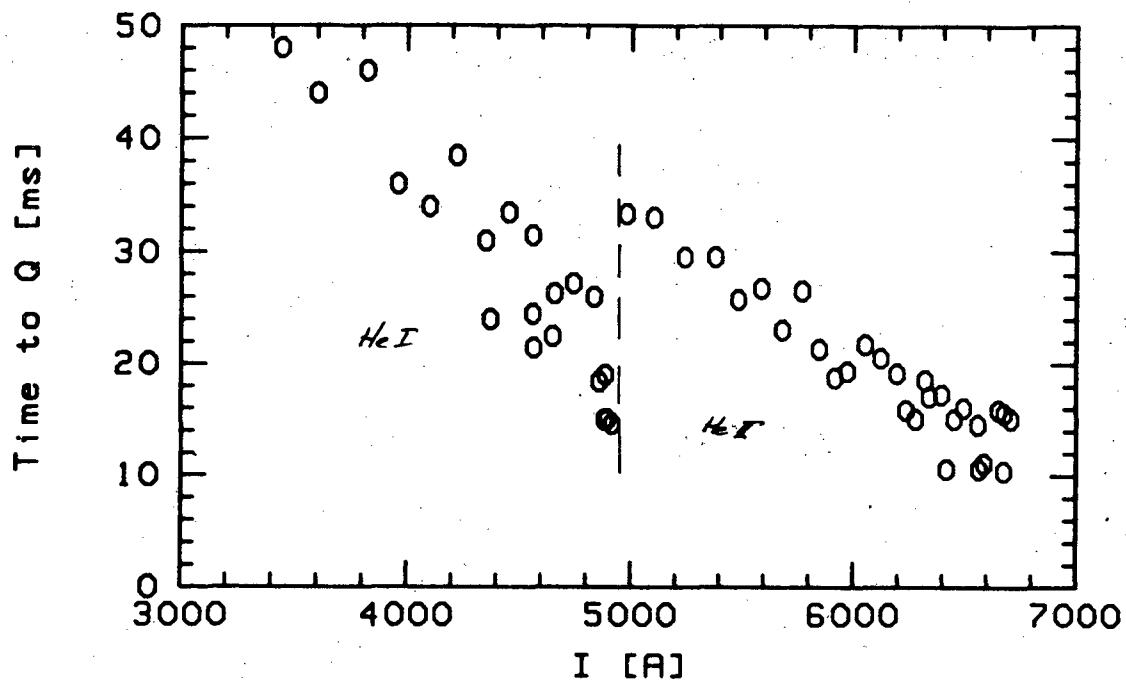


Fig. 4 Measured time from detection to extraction as a function of current.

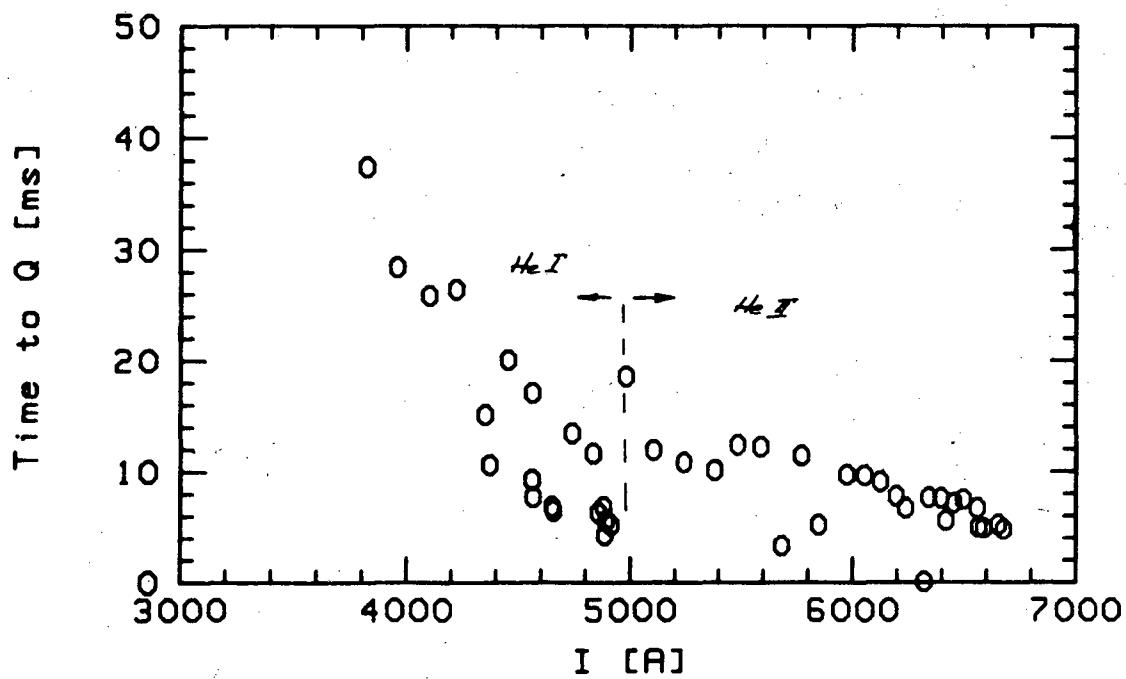
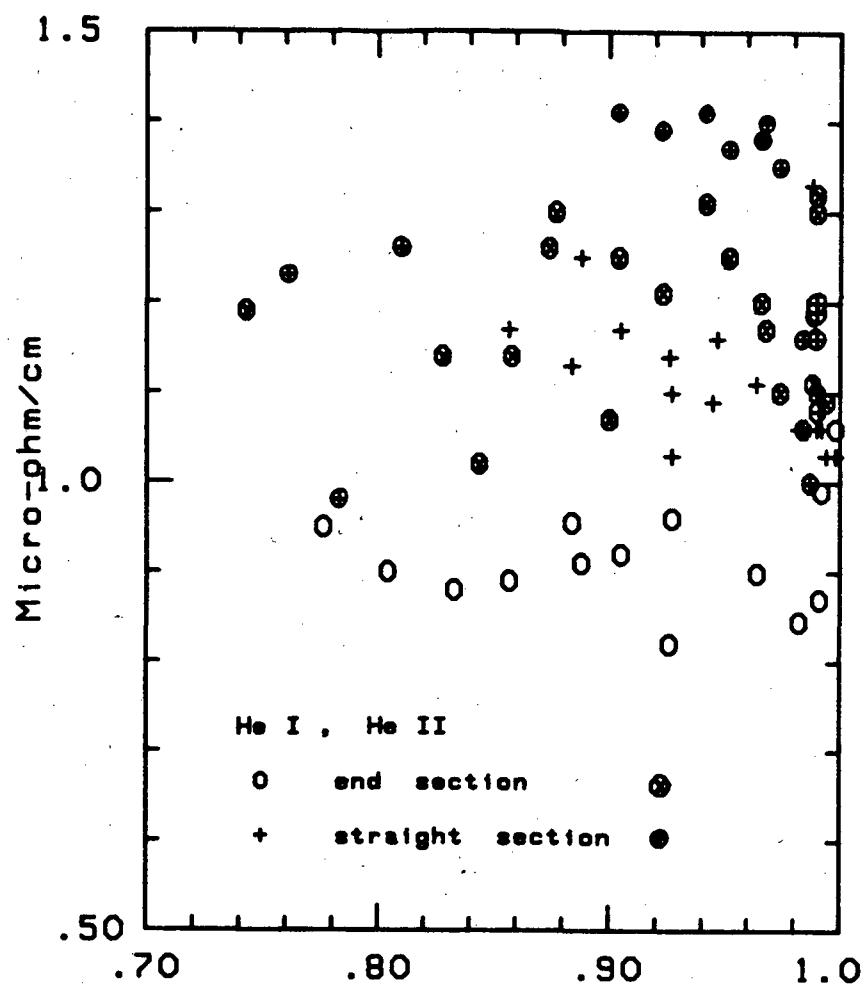


Fig. 5 Calculated time to extraction based on Equation 1 using the same data points.



I/I_c

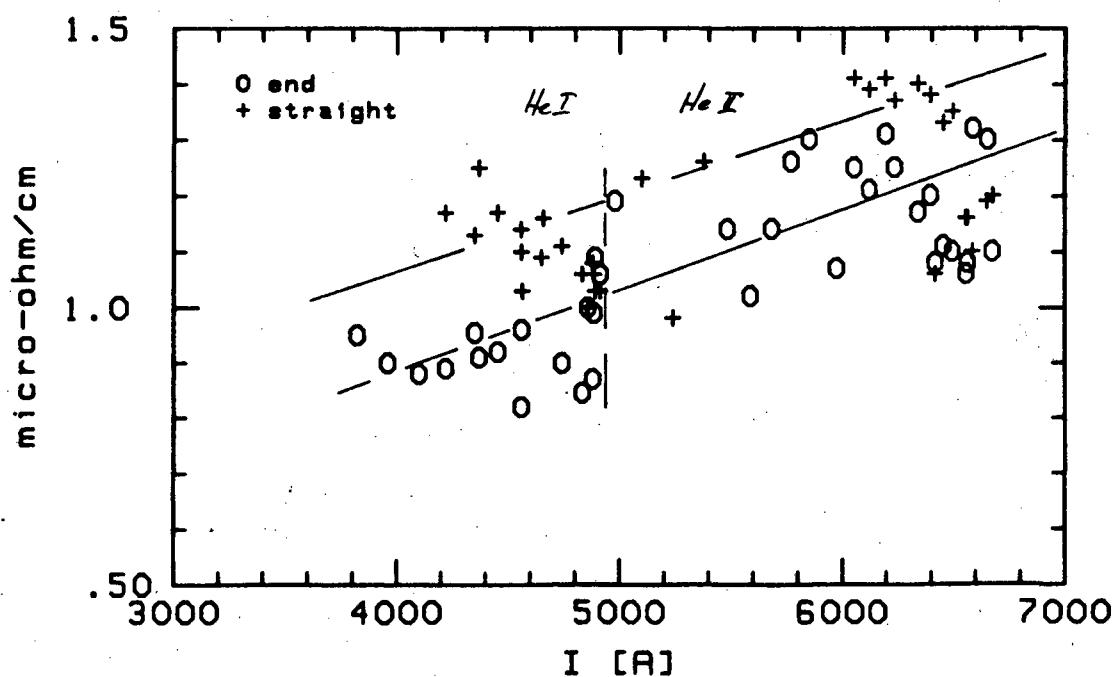


Fig. 6 Resistance per unit length during the transition from the S.C. state to the normal state.

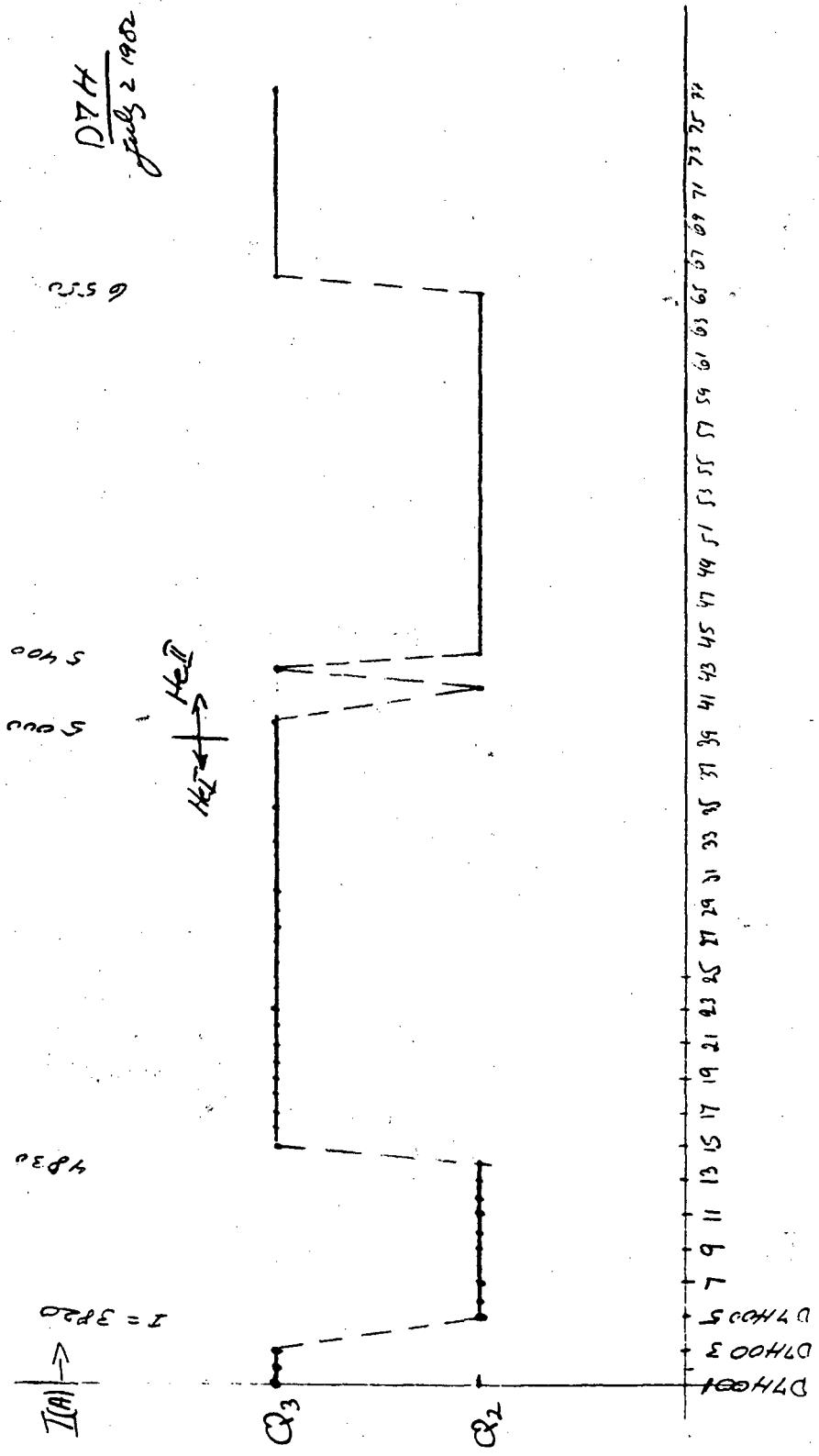


Fig. 7 Quench location variation per half inner shell as a function of storage file.

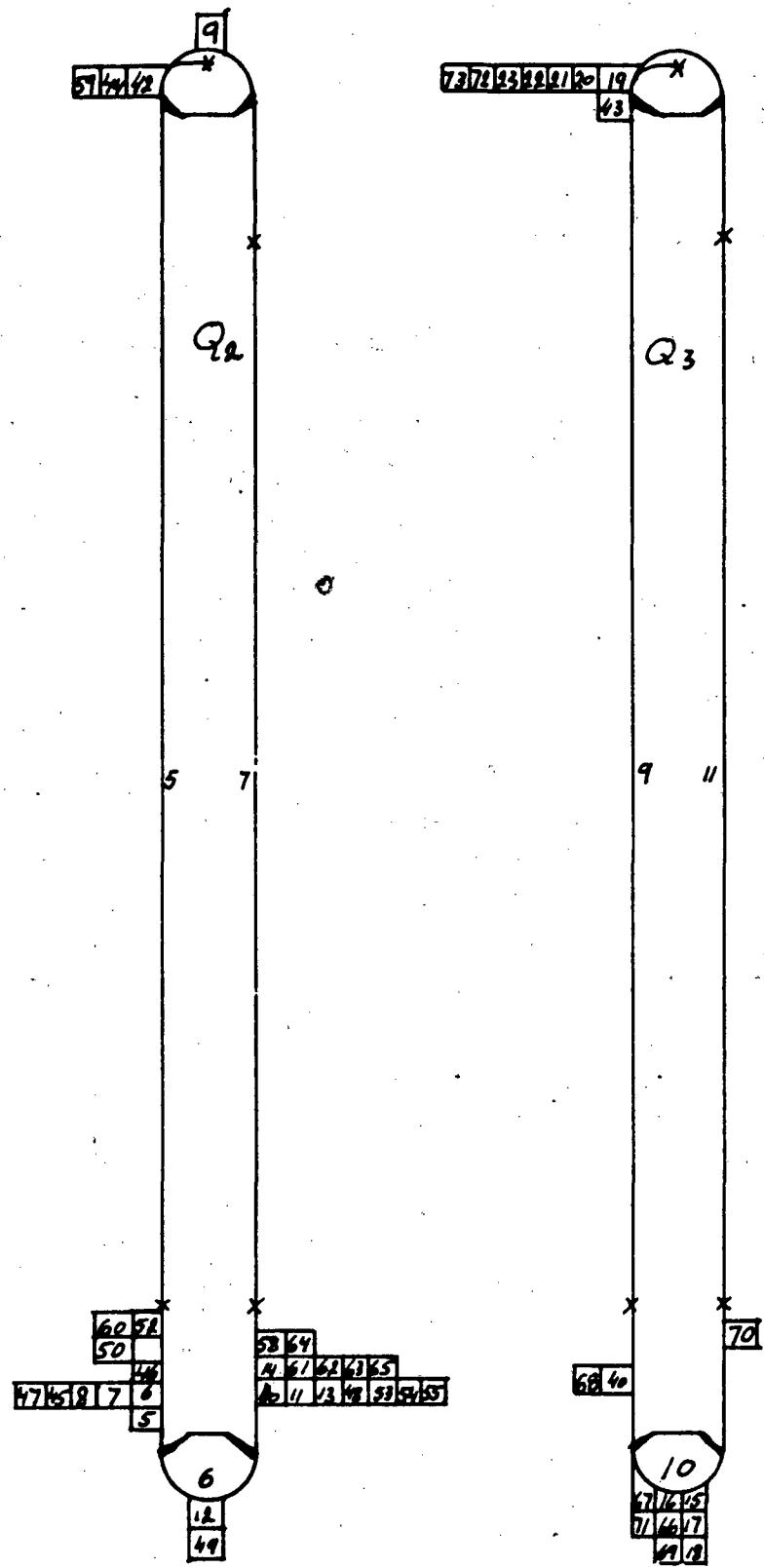


Fig. 8 Quench location in upper and lower inner shell.

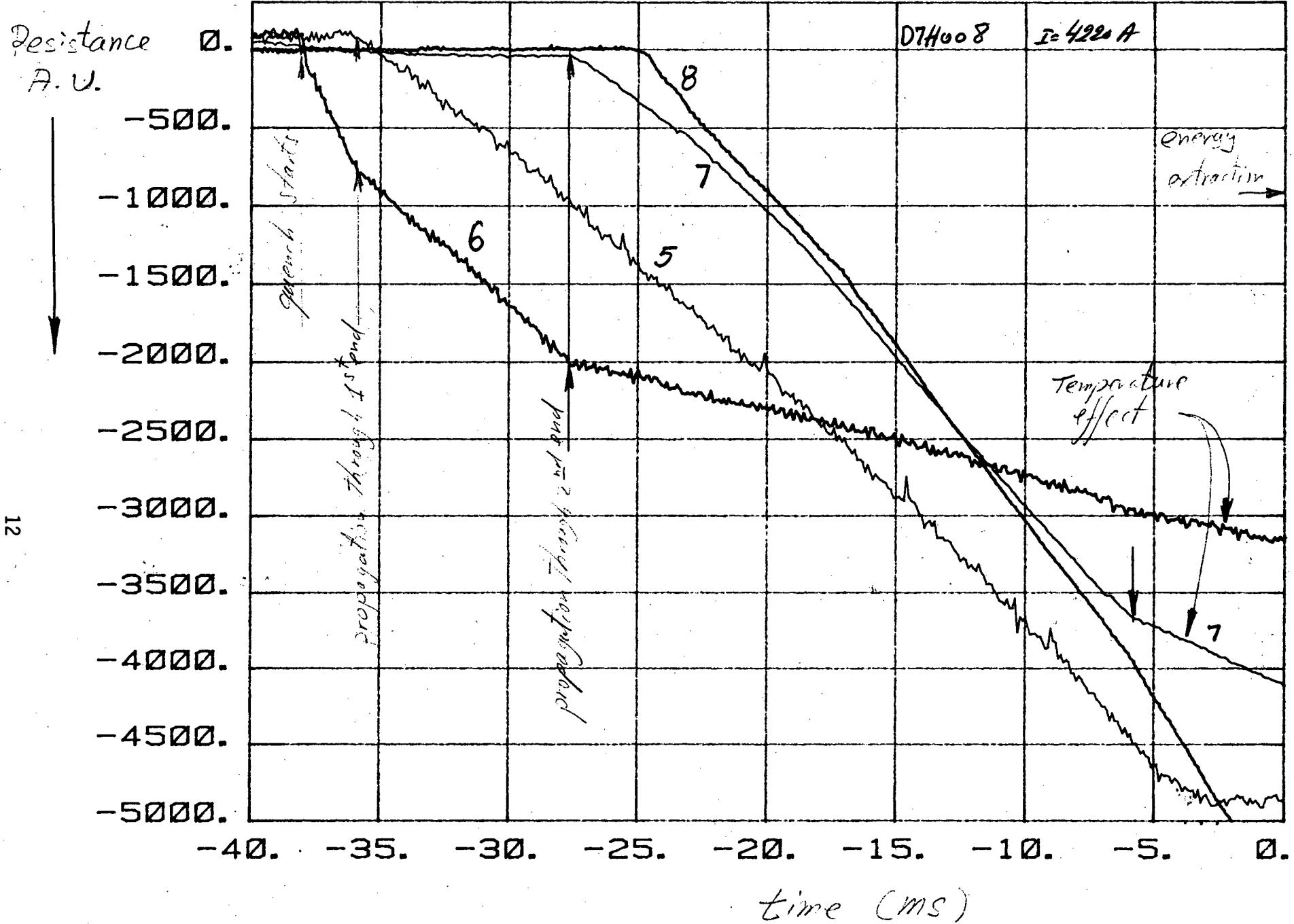


Fig. 9 Normal zone propagation and resistive rise prior to energy extraction.

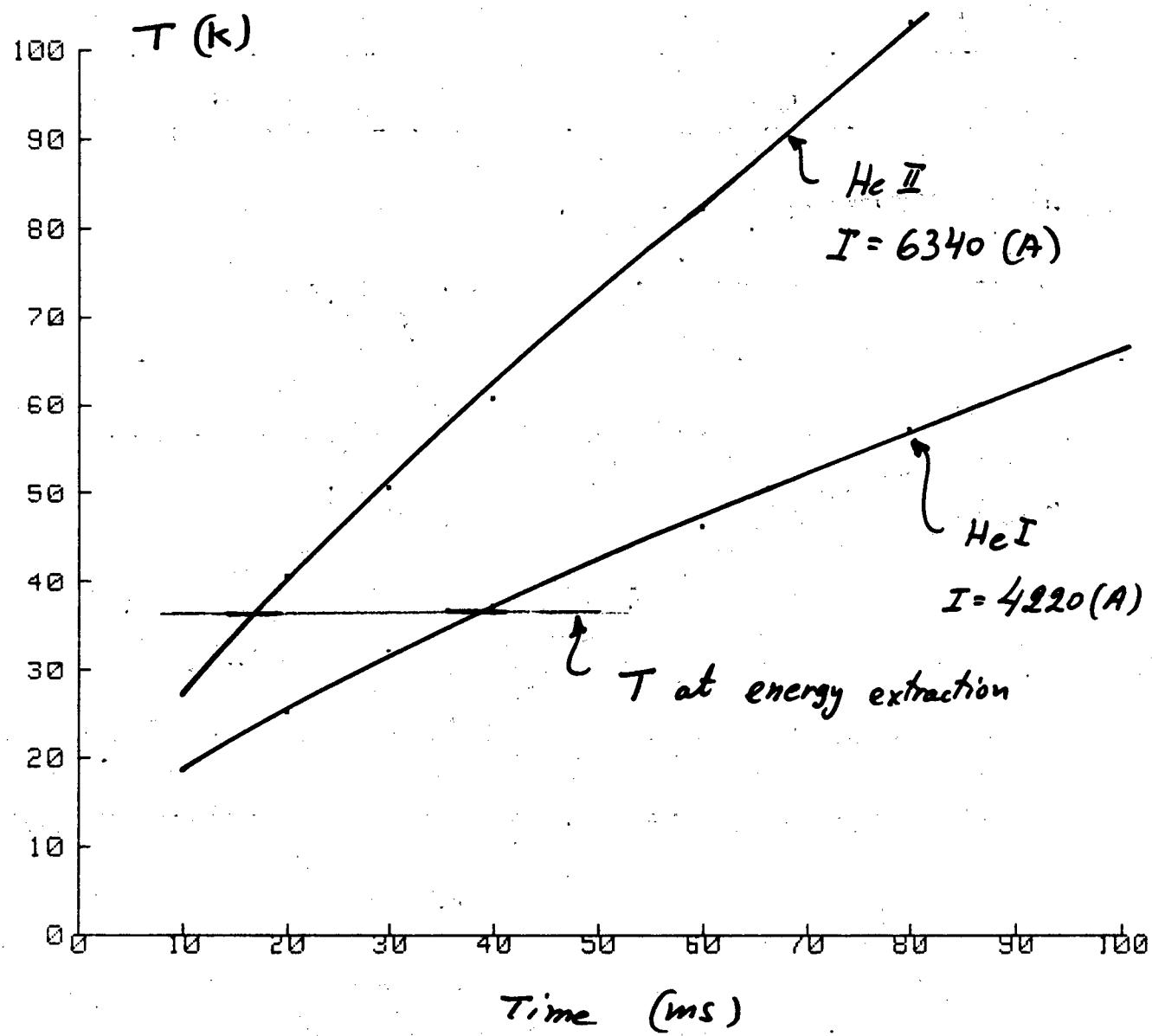


Fig. 10 Temperature history prior to energy extraction based on equation 3.

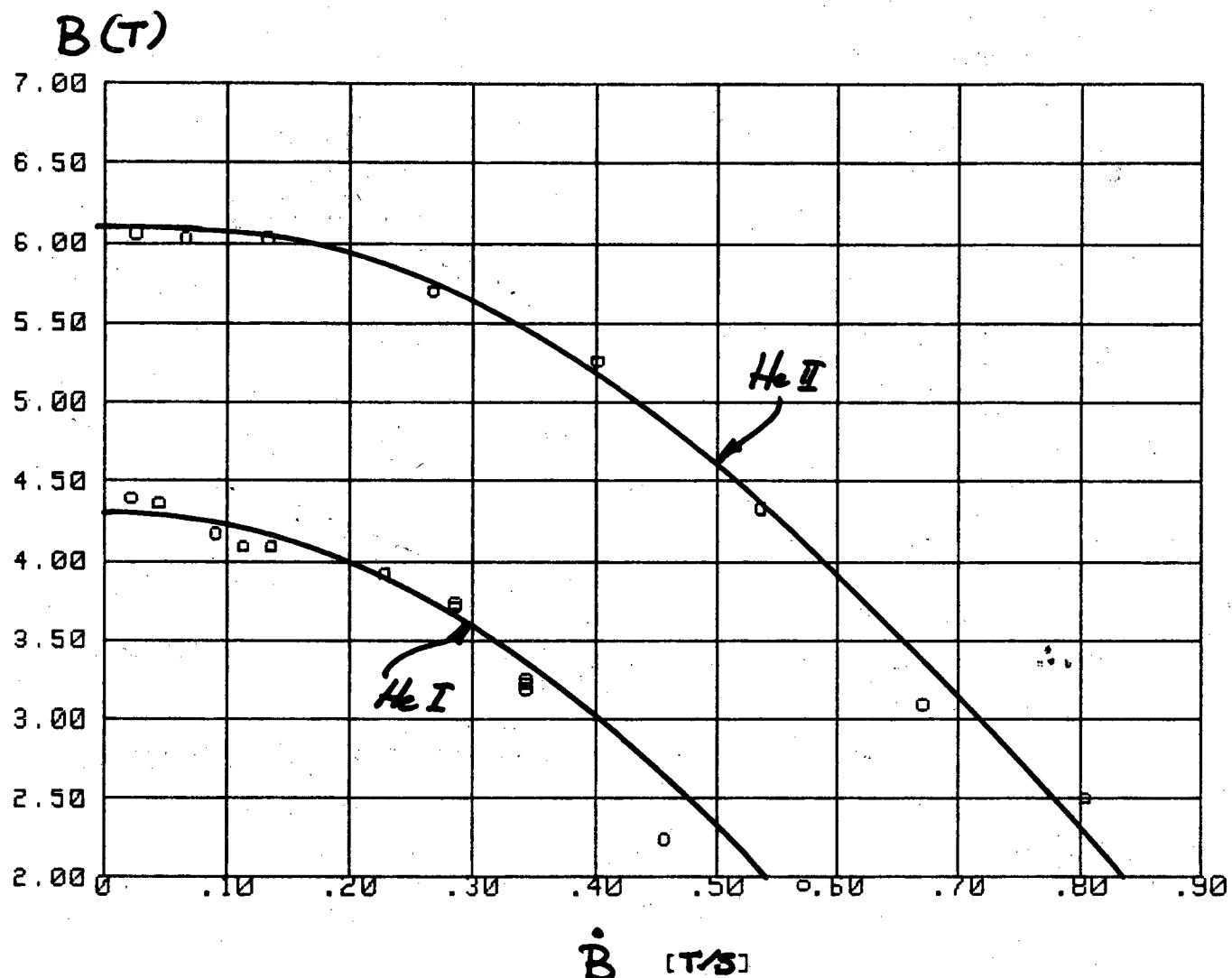


Fig. 11 Maximum field as a function of ramp rate.

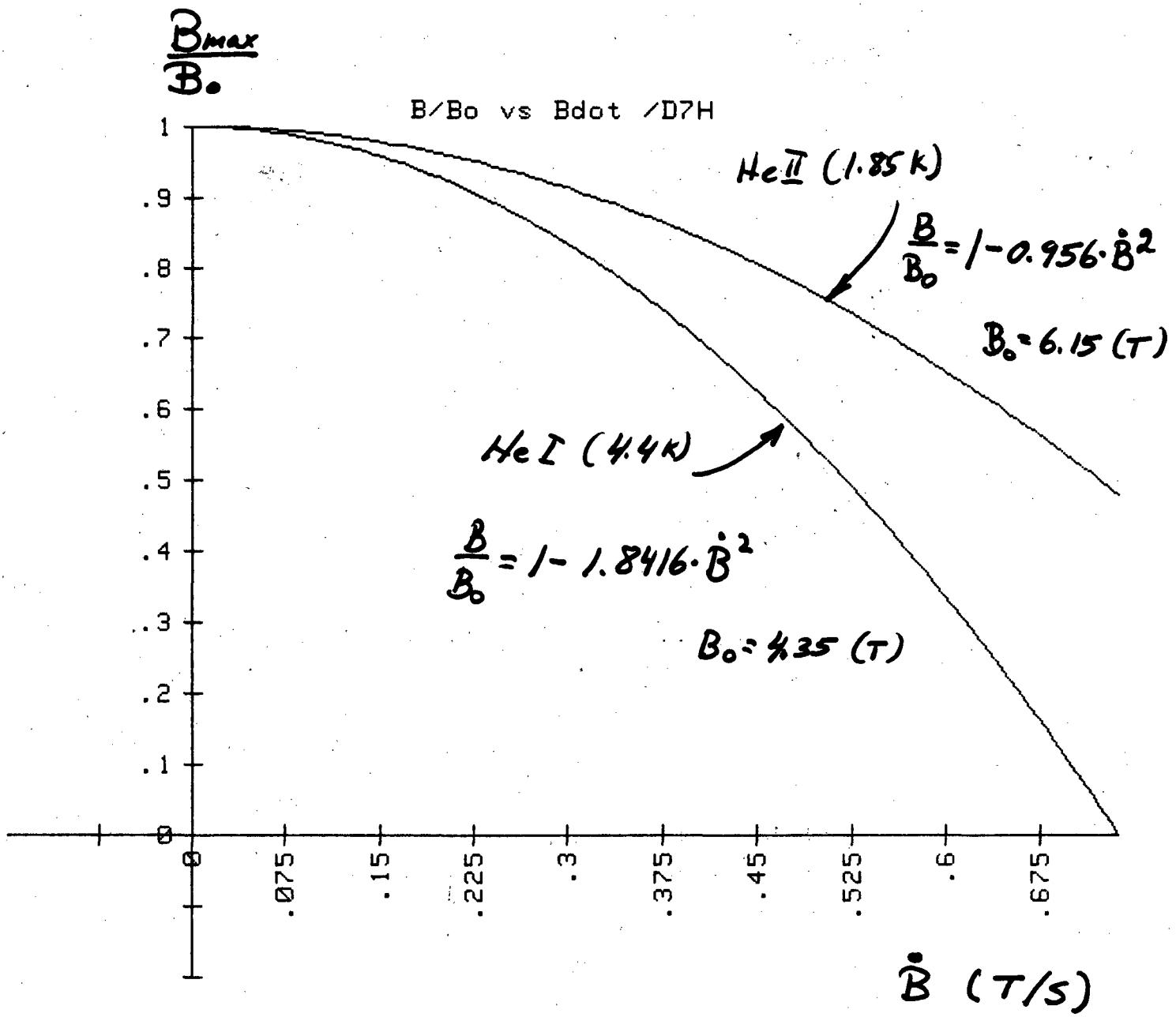


Fig. 12 Normalized maximum field as a function of ramp rate.
The lines are a least fit to the data.

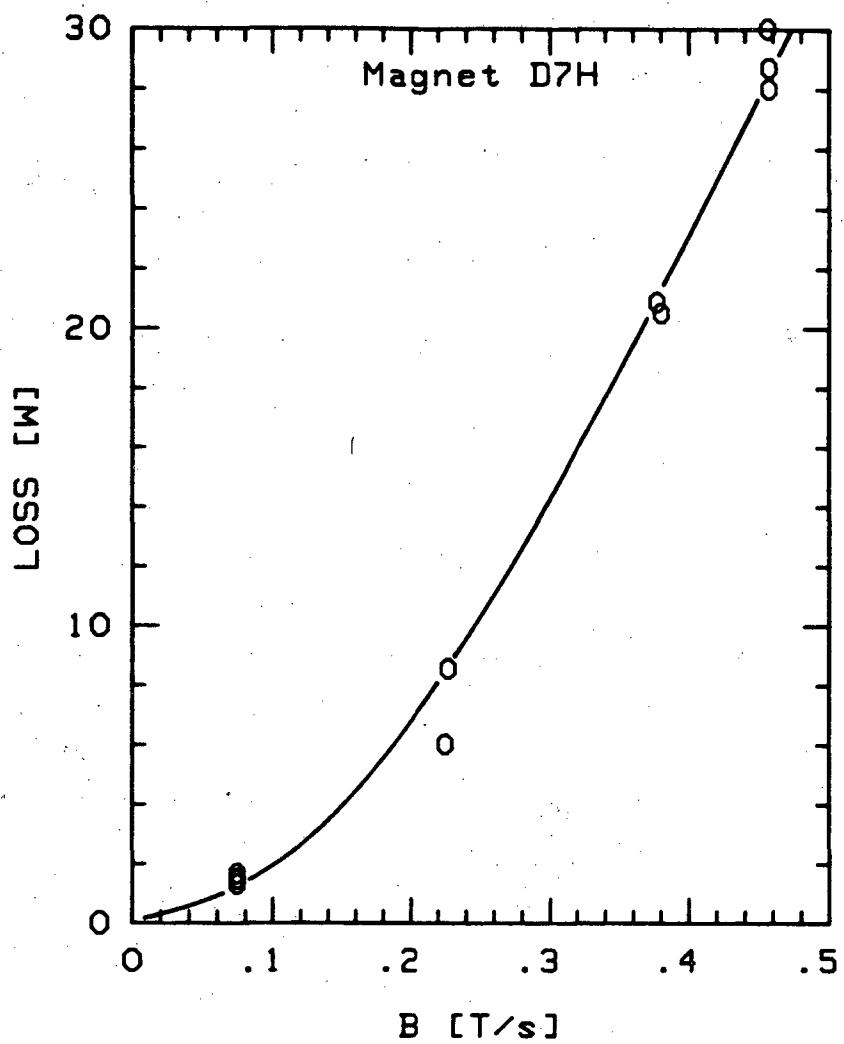


Fig. 13 Magnet loss during cycling around 0-3.85 (T).

| FILE NAME | LOCATION | I_q (A) | T_q (ms) | T (K) | I_q/I_c | MICROHM/CM (end) | MICROHM/CM (straight) | V_5 (m/s) | V_6 (m/s) | V_7 (m/s) | V_8 (m/s) | V_{10} (m/s) | V_{11} (m/s) | V_t (m/s) | TRANS. TIME (ms) |
|-----------|----------|-----------|------------|-------|-----------|------------------|-----------------------|-------------|-------------|-------------|-------------|----------------|----------------|-------------|------------------|
| D7H801 | | 0 | 0.0 | 0.00 | 0.00 | 0.00 | 0.00 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.000 | 0.0 |
| D7H802 | 03 | 3444 | 48.6 | 4.46 | .700 | 0.00 | 0.00 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | .030 | 38.0 |
| D7H803 | 03 | 3603 | 44.0 | 4.46 | .732 | 0.00 | 0.00 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | .042 | 35.0 |
| D7H805 | 02 | 3821 | 46.0 | 4.46 | .776 | .95 | 0.00 | 0.0 | 9.2 | 0.0 | 0.0 | 0.0 | 0.0 | .077 | 19.0 |
| D7H806 | 02 | 3959 | 36.0 | 4.46 | .804 | .98 | 0.00 | 0.0 | 12.0 | 0.0 | 0.0 | 0.0 | 0.0 | .113 | 13.0 |
| D7H807 | 02 | 4100 | 34.0 | 4.46 | .833 | .99 | 0.00 | 0.0 | 13.4 | 0.0 | 0.0 | 0.0 | 0.0 | .113 | 13.0 |
| D7H808 | 02 | 4220 | 30.5 | 4.46 | .857 | .99 | 1.17 | 15.2 | 12.6 | 10.6 | 0.0 | 0.0 | 0.0 | .122 | 12.0 |
| D7H809 | 02 | 4351 | 31.0 | 4.46 | .884 | .96 | 1.13 | 18.2 | 19.9 | 20.3 | 0.0 | 0.0 | 0.0 | .147 | 1.0 |
| D7H810 | 02 | 4453 | 33.5 | 4.46 | .905 | .92 | 1.17 | 21.0 | 15.2 | 24.6 | 0.0 | 0.0 | 0.0 | .105 | 14.0 |
| D7H811 | 02 | 4561 | 31.5 | 4.46 | .927 | .96 | 1.10 | 25.0 | 16.7 | 20.0 | 0.0 | 0.0 | 0.0 | .105 | 14.0 |
| D7H812 | 02 | 4650 | 26.3 | 4.46 | .947 | 0.00 | 1.16 | 27.2 | 35.0 | 30.0 | 0.0 | 0.0 | 0.0 | .147 | 10.0 |
| D7H813 | 02 | 4742 | 27.2 | 4.46 | .964 | .98 | 1.11 | 30.0 | 21.0 | 23.3 | 0.0 | 0.0 | 0.0 | .117 | 12.5 |
| D7H814 | 02 | 4833 | 26.0 | 4.46 | .982 | .95 | 1.06 | 35.2 | 26.3 | 34.7 | 0.0 | 0.0 | 0.0 | .146 | 10.5 |
| D7H815 | 03 | 4913 | 14.6 | 4.46 | .998 | 1.06 | 1.03 | 0.0 | 0.0 | 46.0 | 35.0 | 45.0 | 1.130 | 1.0 | |
| D7H816 | 03 | 4980 | 15.0 | 4.46 | .991 | .97 | 1.00 | 0.0 | 0.0 | 43.0 | 47.7 | 41.0 | 3.000 | .5 | |
| D7H817 | 03 | 4991 | 15.0 | 4.46 | .994 | 1.09 | 1.03 | 0.0 | 0.0 | 42.0 | 38.9 | 41.4 | 3.000 | .5 | |
| D7H818 | 03 | 4985 | 15.0 | 4.46 | .992 | .99 | 1.06 | 0.0 | 0.0 | 50.7 | 25.0 | 59.7 | .147 | 10.0 | |
| D7H819 | 03 | 4957 | 19.4 | 4.46 | .987 | 1.00 | 1.00 | 0.0 | 0.0 | 48.0 | 47.0 | 0.0 | .267 | 5.5 | |
| D7H820 | 03 | 4650 | 22.5 | 4.46 | .945 | 0.00 | 1.09 | 0.0 | 0.0 | 36.0 | 42.6 | 0.0 | .100 | 8.0 | |
| D7H821 | 03 | 4559 | 24.5 | 4.46 | .926 | .82 | 1.14 | 0.0 | 0.0 | 36.0 | 39.7 | 0.0 | .154 | 9.5 | |
| D7H822 | 03 | 4564 | 21.5 | 4.46 | .927 | 0.00 | 1.03 | 0.0 | 0.0 | 34.4 | 38.0 | 0.0 | .196 | 7.5 | |
| D7H823 | 03 | 4370 | 24.0 | 4.46 | .888 | .91 | 1.25 | 0.0 | 0.0 | 29.6 | 33.1 | 0.0 | .173 | 8.5 | |
| D7H840 | 03 | 4988 | 33.3 | 1.85 | .743 | 1.19 | 0.00 | 0.0 | 0.0 | 0.0 | 11.4 | 0.0 | .084 | 17.5 | |
| D7H842 | 02 | 5102 | 23.0 | 1.85 | .761 | 0.00 | 1.23 | 16.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.000 | 15.0 | |
| D7H843 | 03 | 5249 | 29.5 | 1.87 | .793 | 0.00 | .98 | 0.0 | 0.0 | 22.6 | 0.0 | 0.0 | .199 | 13.5 | |
| D7H844 | 02 | 5388 | 29.5 | 1.90 | .810 | 0.00 | 1.26 | 10.3 | 0.0 | 0.0 | 0.0 | 0.0 | .122 | 12.0 | |
| D7H845 | 02 | 5484 | 25.7 | 1.90 | .920 | 1.14 | 0.00 | 0.0 | 16.2 | 0.0 | 0.0 | 0.0 | .140 | 10.5 | |
| D7H846 | 02 | 5587 | 26.7 | 1.90 | .844 | 1.82 | 0.00 | 0.0 | 18.0 | 0.0 | 0.0 | 0.0 | .163 | 9.0 | |
| D7H847 | 02 | 5682 | 23.0 | 1.90 | .958 | 1.14 | 0.00 | 0.0 | 59.6 | 0.0 | 0.0 | 0.0 | .210 | 7.0 | |
| D7H848 | 02 | 5769 | 26.5 | 1.95 | .974 | 1.26 | 0.00 | 0.0 | 15.1 | 0.0 | 0.0 | 0.0 | .122 | 12.0 | |
| D7H849 | 02 | 5847 | 21.0 | 1.85 | .877 | 1.30 | 0.00 | 0.0 | 32.0 | 0.0 | 0.0 | 0.0 | .267 | 5.5 | |
| D7H850 | 02 | 5917 | 18.7 | 1.89 | .892 | 0.00 | 0.00 | 0.0 | 99.0 | 0.0 | 0.0 | 0.0 | .267 | 5.5 | |
| D7H852 | 02 | 5973 | 19.3 | 1.91 | .988 | 1.87 | 0.00 | 0.0 | 28.3 | 0.0 | 0.0 | 0.0 | .478 | 3.1 | |
| D7H853 | 02 | 6051 | 21.7 | 1.83 | .984 | 1.25 | 1.41 | 0.0 | 17.2 | 0.0 | 0.0 | 0.0 | .197 | 10.7 | |
| D7H854 | 02 | 6122 | 20.5 | 1.89 | .923 | 1.21 | 1.39 | 0.0 | 16.6 | 27.0 | 0.0 | 0.0 | .147 | 10.0 | |
| D7H855 | 02 | 6194 | 19.1 | 1.99 | .942 | 1.31 | 1.41 | 0.0 | 19.9 | 29.0 | 0.0 | 0.0 | .163 | 9.0 | |
| D7H856 | 02 | 6236 | 15.0 | 2.00 | .952 | 1.25 | 1.37 | 0.0 | 24.0 | 34.7 | 0.0 | 0.0 | .204 | 7.2 | |
| D7H860 | 02 | 6279 | 15.0 | 1.90 | .958 | 0.00 | 0.00 | 0.0 | 24.5 | 8.0 | 0.0 | 0.0 | .590 | 2.5 | |
| D7H861 | 02 | 6248 | 17.0 | 2.00 | .960 | 1.17 | 1.40 | 0.0 | 22.1 | 32.5 | 0.0 | 0.0 | .173 | 8.5 | |
| D7H862 | 02 | 6395 | 17.2 | 1.90 | .966 | 1.20 | 1.30 | 0.0 | 21.5 | 32.5 | 0.0 | 0.0 | .173 | 8.5 | |
| D7H863 | 02 | 6453 | 15.0 | 2.04 | .988 | 1.11 | 1.33 | 0.0 | 24.5 | 36.9 | 0.0 | 0.0 | .210 | 7.0 | |
| D7H864 | 02 | 6495 | 16.0 | 1.85 | .974 | 1.10 | 1.35 | 0.0 | 23.5 | 36.2 | 0.0 | 0.0 | .173 | 8.5 | |
| D7H865 | 02 | 6558 | 14.5 | 1.80 | .984 | 1.06 | 1.16 | 0.0 | 27.0 | 45.0 | 0.0 | 0.0 | .226 | 6.5 | |
| D7H866 | 03 | 6587 | 11.0 | 2.03 | .990 | 1.32 | 1.10 | 0.0 | 0.0 | 29.0 | 67.0 | 0.0 | 3.000 | .5 | |
| D7H867 | 03 | 6417 | 18.5 | 2.14 | .990 | 1.00 | 1.06 | 0.0 | 0.0 | 32.5 | 62.5 | 0.0 | 3.000 | .5 | |
| D7H868 | 03 | 6652 | 15.0 | 1.87 | .990 | 1.30 | 1.19 | 0.0 | 0.0 | 28.0 | 68.0 | 0.0 | .196 | 7.5 | |
| D7H869 | 03 | 6564 | 18.5 | 2.05 | .990 | 1.00 | 1.16 | 0.0 | 0.0 | 35.0 | 65.0 | 0.0 | 3.000 | .5 | |
| D7H870 | 03 | 6709 | 15.0 | 1.81 | .990 | 0.00 | 0.00 | 0.0 | 0.0 | 0.0 | 54.0 | 0.0 | .196 | 7.5 | |
| D7H871 | 03 | 6675 | 18.3 | 1.89 | .990 | 1.10 | 0.00 | 0.0 | 0.0 | 36.0 | 62.0 | 0.0 | 3.000 | .5 | |
| D7H872 | 03 | 6670 | 18.5 | 0.00 | .990 | 0.00 | 1.20 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | .210 | 7.0 | |
| D7H873 | 03 | 6320 | 18.5 | 0.00 | .990 | 0.00 | 0.00 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | .163 | 0.0 | |

Table I. Data base on the 9845B desktop; I_q = quench current; T_q = time from quench detection to energy extraction; I_q/I_c = normalized quench current; Microhm/cm = resistive rise from S.C. state to normal state per unit length; V_i = propagation velocity for section i; V_t = turn to turn velocity; Trans. time = turn to turn propagation time.

| File name | Resistivity rise | |
|-----------|------------------|----------|
| | micro_ohm-cm/s | straight |
| He I | | |
| D7H005 | 1.00 | - |
| D7H006 | 1.2 | - |
| D7H007 | 0.97 | - |
| D7H008 | 1.06 | 1.13 |
| D7H009 | 1.21 | 0.99 |
| D7H010 | 1.40 | 1.13 |
| D7H011 | 1.27 | 1.23 |
| D7H012 | 1.40 | 1.18 |
| D7H013 | 1.31 | 1.36 |
| D7H014 | 1.40 | 1.33 |
| D7H015 | 1.34 | - |
| D7H016 | 1.13 | - |
| D7H017 | 1.21 | 1.04 |
| D7H018 | 1.10 | 1.15 |
| He-II | | |
| D7H040 | 1.43 | - |
| D7H045 | 1.52 | - |
| D7H046 | 2.12 | - |
| D7H047 | 2.12 | - |
| D7H048 | 2.65 | - |
| D7H049 | 2.31 | - |
| D7H050 | 2.13 | - |
| D7H052 | 1.67 | - |
| D7H053 | 2.53 | - |
| D7H054 | 2.71 | - |
| D7H055 | 2.56 | - |
| D7H058 | 2.02 | - |
| D7H060 | 2.34 | - |
| D7H061 | 2.46 | - |
| D7H062 | 2.78 | - |
| D7H063 | 3.11 | - |
| D7H064 | 3.05 | - |
| D7H065 | 2.65 | - |

Table 2 Resistivity per second prior to energy extraction due to temperature rise only.

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