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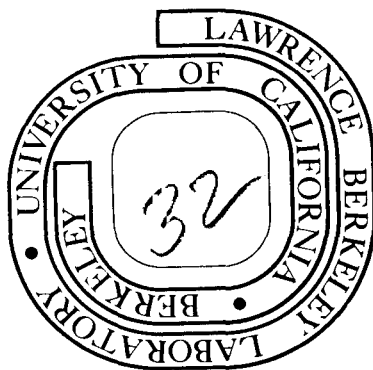
A. Y. Cheer

February 1978

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BOUNDL: A program for calculating flow past a semi-infinite flat plate using the vortex sheet method.

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Abstract

BOUNDL is a computer program which implements the Vortex Sheet Method for approximating boundary layers [1]. The specific problem of flow past a semi-infinite flat plate is considered. Listings of the main program and its subprograms, together with their respective flow charts, are enclosed to facilitate the documentation process.

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Introduction

Program BOUNDL was written by A. J. Chorin implementing his method described in [1]. In the process, it has gone through many generations of code, and thus can be confusing. In this paper, I will attempt to relate all the secrets that link the code to the method. References will be made to the lines of code and their corresponding formulae in [1] as much as possible.

Section one describes the function of the main routine and its relation to the subroutines. The next section describes subroutine WALL. This subroutine corresponds to pages 8, 9 and 10; the vorticity creation section of [1].

In section three, subroutine DISPL is documented. This routine calculates and prints the drag, the displacement thickness and the boundary layer for flow past a semi-infinite flat plate. Also it sets up formats for plotting figures 1 and 2 in [1]; and it sets up arrays like (UXA(I)) for further use by the main routine. Finally, section four documents subroutine STEP. Here, the random numbers η_i are generated and a random step taken according to the formulae on pages 4 to 7 of [1].

1. Program BOUNDL (main routine)

The following are definitions of variables in the COMMON file:

H h where $h = \Delta x =$ length of sheets

N Total number of vortex sheets created . (N increases in time by the total number of vortex sheets created at each time step IADD, and is decreased by the number of sheets Q_i with center (X_i, Y_i) that flowed out of the domain of interest.)

L Number of points on the x-axis where sheets are created (partition of the x-axis).

VEL U_∞ (velocity at infinity or freestream velocity)

RE Reynold's number

TSIG 2 times the variance

DT k where $k = \Delta t =$ time step

PI Constant $\pi = 3.1415926536$

TPI 2π

MM Number of sheets created at each point (X_i) of the x-axis. (The sum of all MM for each X_i $i = 1, \dots, L$ is equal to IADD where IADD = total number of vortex sheets created at each time step).

CM ξ_{\max} (maximum allowable intensity for each vortex sheet).

LOOK (30,30))
LS
MS
HX
XO
YO } Variables used in subroutine DISPL to aid the output formatting of figure 1 of [1].

X(500) Array storing the X-coordinate X_i

Y(500) Array storing the Y-coordinate Y_i

S(500) Array storing ξ_i (intensity of vortex sheet Q_i)

DX(500) Array storing U_i (first-velocity component of $\vec{U}_i = (U_i, V_i)$)

DY(500) Array storing V_i (2nd velocity component)

UXA(100) Array storing average velocity: U_i average

DRAGA Drag

VAR Variance of drag

RIGHT Rightmost point on the x-axis under consideration.

NOLD Holds the previous value of N (this variable is used to aid the sorting routine in subprogram WALL).

MN(500) Tags. (Each vortex sheet created is assigned a tag MN(I). This tag aids in the assigning of the random variable η_i . Every sheet with the same value MN(I) gets the same η_i).

MNO Holds the last tag used at the previous point. Usually $MNO = MNO + MNMAX$.

MNMAX Maximum number of sheets one is allowed to create at each position X_i .

Following is a list of local variables and their definitions:

NMAX Maximum number for N to reach

NMIN Minimum number for N

Note: NMAX and NMIN was not used in this particular problem.

NAV This is usually an integer > 0 . For each NAV number of steps, the main routine calculate averages for drag, variance and velocity.

CNAV NAV (Real variable, not integer)

NSTEP Total number of steps to be taken

TIME t = time

The first task BOUNDL does is initialize all its variables, a list of which are given above. This corresponds to lines 3-40 of the code. Figure 10 is the output corresponding to the values $L = 7$, $H = 0.2$, $DT = 0.2$, $NAV = 20$, $CM = 0.1$ and $RE = 1.E + 6$.

Secondly, the time step is advanced and a call to subroutine WALL to create vortex sheets is executed. After the vorticity is created, another call is made to subroutine DISPL. Here, the drag, the variance and the velocity profile (UXA(I)) are calculated, stored and displayed if desired.

Next, BOUNDL checks to see if twenty steps have been taken since the last time averages were computed. If yes, then the average profile, the average drag and the variance are calculated and printed. Loop 5 calculates the average profile, Loop 6 prints the profile and Loop 3 reinitializes the array UXA(I) to zero. Lines 59 and 62 of the code calculates the average drag and variance; lines 60 and 65 outputs the values, and lines 66 and 67 reinitializes the variables $VAR = 0$. and $DRAG = 0$.

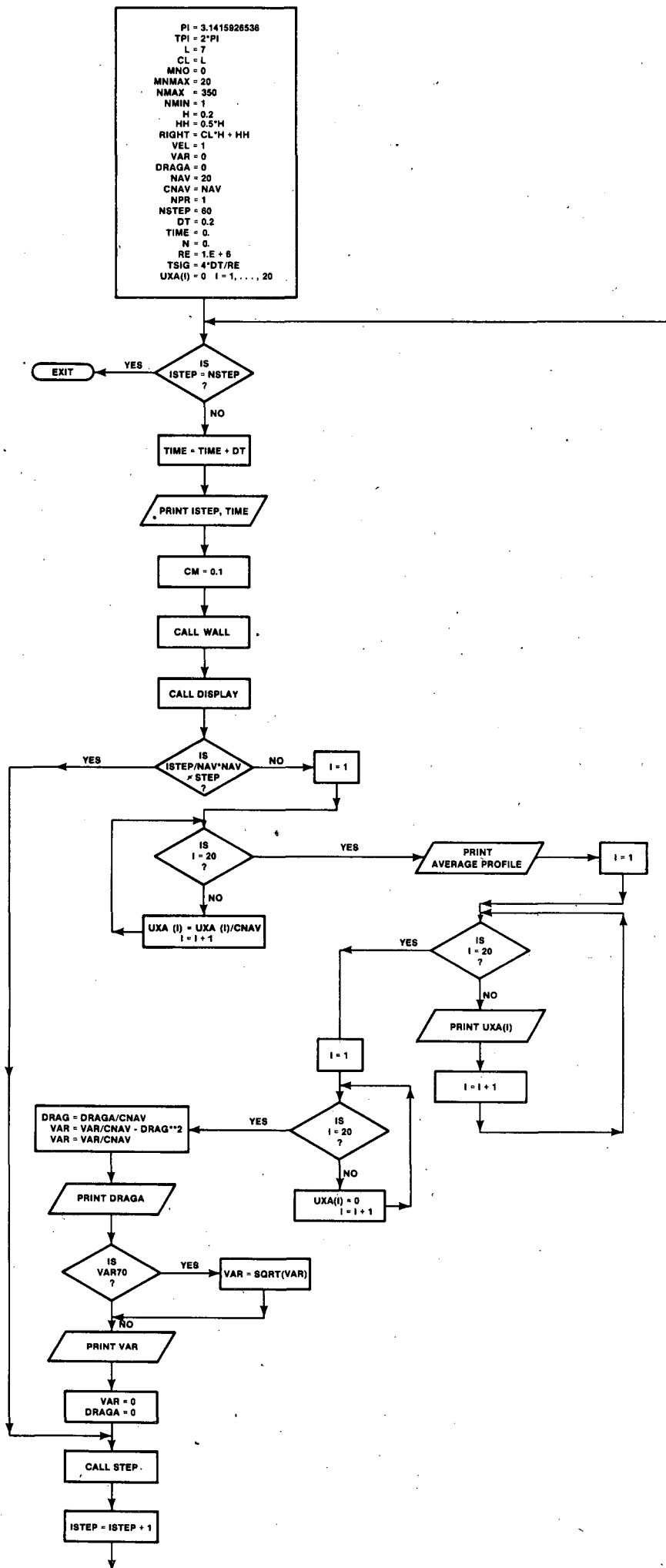
If twenty time steps have not elapsed, or after averages are computed, BOUNDL calls subroutine STEP to generate random numbers. Each vortex sheet with different tags gets assigned a different random number, and a random step is taken.

Finally, the controlling loop; loop 1; is advanced and the program checks to see if the number of steps already taken is $\leq NSTEP$. If yes, then the above process is repeated. If no, the program exits and execution halts.


```
1          PROGRAM BOUND (INPUT,CUTPUT)
2          COMMON/HH,K,L,VEL,RE,TSIG,CT,IPI,MN,CM
1          ,LOCK(30,30),LS,MS,FX,HY,XO,YO
1          ,X(SCC),Y(SCC),S(SCC),CX(500),CY(500)
1          ,UXA(100),DRACA,VAR,RIGHT,NCLD
1          ,MNO(500),MNO,MNMAX
C
C          INITIAL CALCULATIONS AND SETTINGS
3          PI=3.1415926536
4          TP1=2.*PI
5          L=10
6          L=12
7          L=6
9          L=13
10         L=7
11         CL=L
12         MNO=0.
13         MNMAX=20
14         MNMAX=350
15         NMIN=1
16         H=0.1
17         H=0.2
18         HH=0.5*H
19         RIGHT=CL*H+HH
20         VEL=1.
21         DRAGA=C.
22         NAV=5
23         NAV=20
24         CNAV=NAV
25         NPR=1
26         NSTEP=3
27         NSTEP=20
28         NSTEP=10
29         NSTEP=30
30         NSTEP=60
31         DT=0.1
32         CT=0.2
33         TIME=0.
34         N=0
35         RE=1.E+4
36         RE=1.E+6
37         TSIG=4.*CT/RE
38         DC2I=1,20
39         UXA(1)=0.
40         CONTINUE
C
C          TIME STEP
41         DO1 ISTEP=1,NSTEP
42         TIME=TIME+DT
43         PRINT9000
44         PRINT9001,ISTEP,TIME
45         CM=0.2
46         CM=0.1
47         CALL WALL
48         CALL DISPL
49         IF((ISTEP/NAV)*NAV).NE.ISTEP)GOTO4
50         DO5 I=1,20
51         UXA(I)=UXA(I)/CNAV
52         PRINT9004
53         DO6 I=1,20
54         PRINT9002,LXA(I)
55         DO3 I=1,20
56         UXA(I)=0.
57         CONTINUE
58         DRACA=DRAGA/CNAV
59         PRINT9003,DRACA
60         VAR=VAR/CNAV-DRAGA**2
61         VAR=VAR/CNAV
62         IF(VAR.GT.C.)VAR=SGRT(VAR)
63         PRINT9005,VAR
64         VAR=0.
65         DRAGA=C.
66         CONTINUE
67         CALL STEP
68         CONTINUE
69         CALL STEP
70         CONTINUE
71         CALL EXIT
72         FORMAT(/)
73         FORMAT(* STEP*,I5,* TIME*,F11.7)
74         FORMAT(1X,6F5.5)
75         FORMAT(* AVERAGE DRAG*,F11.7)
76         FORMAT(* AVERAGE PROFILE*)
77         FORMAT(* VARIANCE*,F11.7)
78         END
```

Fig. 1

PROGRAM BOUNDL



2. Subroutine WALL

This subroutine corresponds to the Vorticity Creation section of [1]. The new variables in this routine are:

EPS $0.5 * CM = 1/2 \xi_{\max}$ (this is the maximum allowable intensity of each vortex sheet for this run)

SS used to calculate U_i

IADD Counter for the number of vortex sheets created on this call.

For each $j=1, \dots, N$, $Y_j > 0$ and $|X_i - X_j| < h$, Loop 2 of this routine calculates:

$$U_i = U_\infty - \sum_{j=1}^N \xi_j d_j$$

which is a modification of equation (4a) of [1]. This summation is done in the following steps:

1) Line 90 corresponds to the condition $Y_j > 0$

2) Line 92 is: $D = \text{ABS}(XX - X(J))$
 $= |X_i - X_j|$

3) Line 93 is condition (4c) of [1]:

$$|X_i - X_j| < h$$

4) Line 95 is equation (4b) of [1] where:

$$\begin{aligned} C &= (H-D)/H \\ &= \frac{h - |X_i - X_j|}{h} \\ &= 1 - \frac{|X_i - X_j|}{h} \\ &= d_j \end{aligned}$$

5) Line 96: $SS = SS - S(J) * C$ $j=1, \dots, N$

$$= U_{\infty} - \sum_{j=1}^N \xi_j d_j$$

where SS is initialized to U_{∞} , $C = d_j$ and $S(J) = \xi_j$. This quantity SS also corresponds to U_0 on pg. 8 of [1].

Now that the value for U_0 is known, line 100 of the code checks to see if $|2U_0| < EPS$ ($=1/2 \xi_{max}$). If yes, then it advances to the next position X_{i+1} and calculate U_{i+1} as above. This is done so long as X_{i+1} is in the domain of interest, i.e., $X_{i+1} < RIGHT$. If $|2U_0| > EPS$, then it breaks $2U_0$ into an even number of vortex sheets, MM or DIV, each with the same intensity SS/DIV .

Next, loop 4 (lines 108-121) checks to see if the number of sheets created $JADD < MNMAX$, where $MNMAX$ is the maximum allowable. If no, then set $JADD = MNMAX$ and print a warning. Else, increase the counter IADD and create a new tag for each sheet: $MN(N + IADD) = MNO + JADD$. $MN(I)$ is the array of tags corresponding to the vortex sheet with center at $(X(I), Y(I))$ and intensity $S(I)$.

Note that JADD is reinitialized at each X_i position, but MNO is kept fixed for all X_i at the same time step. Hence, different vortex sheets, at different X position, at same time step, can have the same tag $MN(I)$.

Thus, we have that at each X_i position, $i=1, \dots, L$, U_i is calculated, and vortex sheets are created according to the above algorithms.

At this point, the variable N is updated: $N = N + IADD$. In words, the total number of sheets to date, equals the number before, plus the number created. Also, MNO is reinitialized to $MNO = MNO + MNMAX$.

This will ensure that brand new tags will be used at the next time step.

Loop 16 and 17 now takes over the task of sorting the sheets created above according to the values of their tag $MN(I)$. This sort is done to facilitate the assignment of the random number η_i in subroutine STEP, where the same η_i is assigned to sheets with the same tag $MN(I)$.

Now, for $I = 1, \dots, N$, loop 9 checks to see if $(X(I), Y(I))$ is in the domain of interest. i.e., $X(I) < \text{RIGHT}$ and $Y(I) > 0$. If yes, do nothing. If not in the domain of interest, delete it from the stack, decrease the number of vortex sheets N by one, and move the trailing stack up one position. This moving procedure is done in loop 10. Finally, print N and allow control to return to main routine.

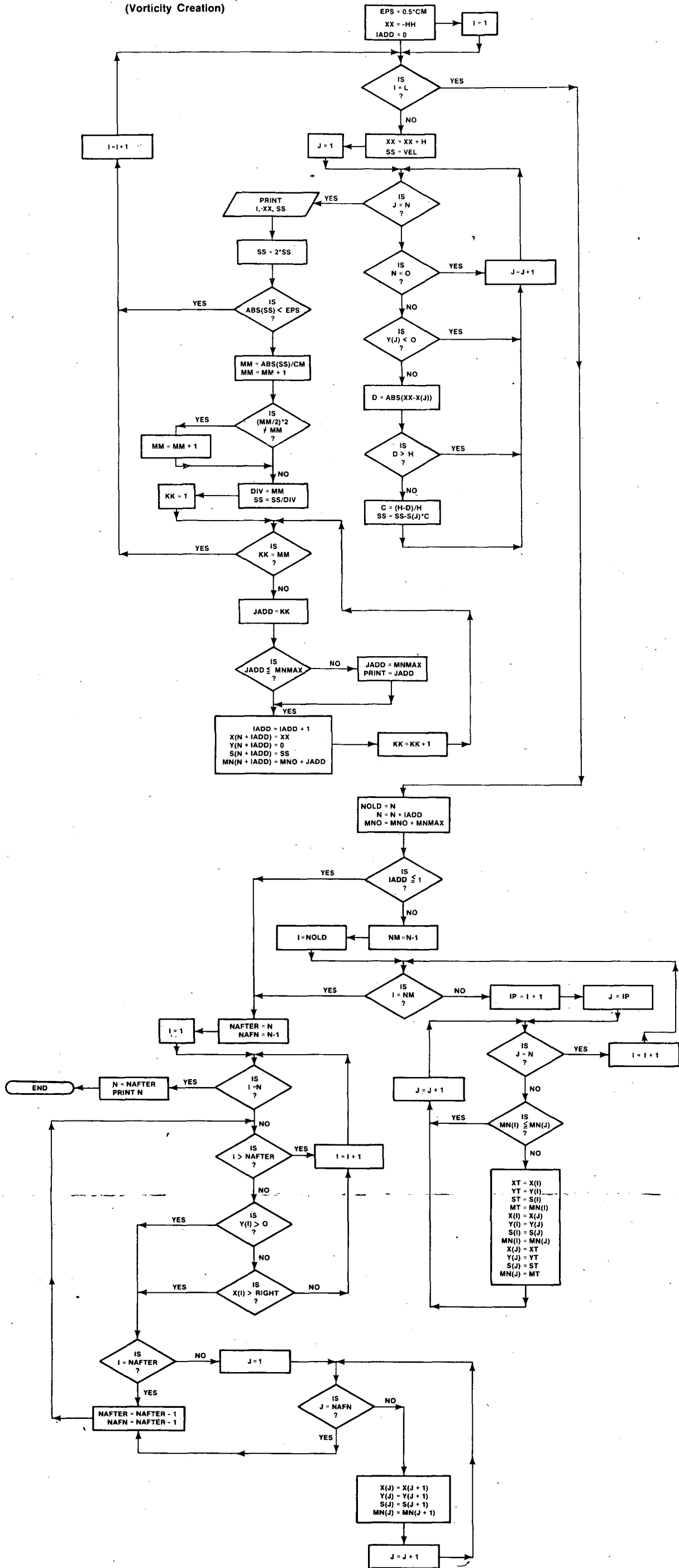
```

79      SUBROUTINE WALL
80      COMMON/HH,K,L,VEL,FE,TSIG,DT,TPI,MM,CM
1      ,LOOK(30,30),LS,MS,HX,HY,X0,Y0
1      ,X(500),Y(500),S(500),CX(500),CY(500)
1      ,UXA(100),DRAGA,VAR,RIGHT,NCLD
1      ,MN(500),MNO,MNMAX
C
31      EPS=0.5*CM
C      VORTICITY CREATION
82      XX=-HH
83      IACC=0
84      DO1 I=1,L
85      XX=XX+H
86      SS=VEL
87      DO2 J=1,N
88      IF(N.EQ.0)GOTO2
89      IF(Y(J).LT.0.)GOTO2
90      D=ABS(XX-X(J))
91      IF(D.GT.H)GOTO2
92      C=(H-D)/H
93      SS=SS-S(J)
94
95      *C
96      2 CONTINUE
97      PRINT9006,I,XX,SS
98      SS=2.*SS
99      IF(ABS(SS).LT.EPS)GOTO3
100     MM=(ABS(SS)/CM)
101     MM=MM+1
102     IF(((MM/2)*2).NE.MM)MM=MM+1
103     DIV=MM
104     SS=SS/DIV
105     DC4KK=1,MM
106     JADD=K
107     IF(JACC.LE.MNMAX)GOTO15
108     JADD=MNMAX
109     PRINT9007,JADD
110     FORMAT(* TCO FEW SLICES#,I6)
111     CONTINUE
112     IACC=IACC+1
113     X(N+IACC)=XX
114     Y(N+IACC)=C.
115     S(N+IACC)=SS
116     MN(N+IACC)=MNC+JADD
117
118     4 CONTINUE
119     3 CONTINUE
120     1 CONTINUE
121     NCLD=N
122     N=N+IACC
123     MNO=MNO+MNMAX
124     IF(IACC.LE.1)GOTO18
125     NM=N-1
126     DC16 I=NCLD,NM
127     IP=I+1
128     DO17 J=IP,N
129     IF(MN(I).LE.MN(J))GOTO17
130     XT=X(I)
131     YT=Y(I)
132     ST=S(I)
133     MT=MN(I)
134     X(I)=X(J)
135     Y(I)=Y(J)
136     S(I)=S(J)
137     MN(I)=MN(J)
138     X(J)=XT
139     Y(J)=YT
140     S(J)=ST
141     MN(J)=MT
142
143     17 CONTINUE
144     16 CONTINUE
145     18 CONTINUE
146
147     C
148     C
149     PURGE
150     NAFTER=N
151     NAFN=N-1
152     DO9 I=1,N
153     12 CONTINUE
154     IF(I.GT.NAFTER)GOTO9
155     IF(Y(I).LT.0.)GOTO14
156     IF(X(I).GT.RIGHT)GOTO14
157     GOTO9
158     14 CONTINUE
159     IF(I.EQ.NAFTER)GOTO13
160     DO10 J=1,NAFN
161     X(J)=X(J+1)
162     Y(J)=Y(J+1)
163     S(J)=S(J+1)
164     MN(J)=MN(J+1)
165
166     10 CONTINUE
167     13 CONTINUE
168     NAFTER=NAFTER-1
169     NAFN=NAFN-1
170     GOTO12
171     9 CONTINUE
172     N=NAFTER
173     PRINT9004,N
174     FORMAT(* N#,I5)
175     FORMAT(1X,I5,3F11.7)
176     RETURN
177     END

```

Fig. 3

SUBROUTINE WALL
(Vorticity Creation)



3. Subroutine DISPL

This subroutine does the following:

- 1) Sets up formats to output figures 1 and 2 of [1]
- 2) calculates and prints the drag, the displacement and the boundary layer, and
- 3) stores results of velocity profile, drag and variance for further use by the main program.

Here are definitions of some local variables:

JPR	If JPR = 1, then DISPL skips loops 1, 2 and 3 (lines 292 to 316) which outputs figure 1 of [1]. Also, skips loop 6 (lines 340 to 343) which outputs figure 2 of [1].
ETA	Similarity variable.
DRAGR	Real drag (for flow past a semi-infinite flat plate)
DRAG	Drag computed by this program
DISP	Displacement thickness
RBDL	Boundary Layer (computed)
RBDL1	Real boundary layer used for comparison.

The first thing DISPL does, after initializing its local variables, is set up formats to output figure 1 of [1]. Here, a printed "*" indicates the center of a vortex sheet. Note that this section of code (lines 291-317) is executed only if JPR \neq 1.

Next, loop 40 initializes array UX(I) to U_{∞} for $I = 1, \dots, N$.

Then, loop 4 calculates

$$U_j = U_j - \sum_{i=1}^N \xi_i d_i \quad j = 1, \dots, ku$$

for $|x - x_j| < h$.

Here, $ku \leq 20$ since 20 is the maximum number of partition points in the y-direction for each X_i .

Now, if $JPR \neq 1$, loop 6 calculates the values for ETA which are used in plotting figure 2 of [1]. If $JPR = 1$, DISPL jumps control to line 346 where the values of UX(I) calculated above are stored in array UXA(I). This array is used by the main routine to compute the average velocity profile.

The remainder of the code is devoted to calculating the drag and the displacement according to the specification of formulae on pages 12-14 of [1]:

a) Loop 7 calculates: $SS(JJ) = S(I) * C$

$$= \sum_{i=1}^M \xi_i d_i$$

where $M = \min(N, 100)$ and $|X - X_i| < h$.

b) Loops 10 and 11 sorts the array of vortex sheets such that

$$Y_1 \leq Y_2 \leq \dots \leq Y_m.$$

c) Loop 13 calculates $U = U - SS(JP)$

$$= U_{\infty} - \sum_{j=1}^{JJ} \xi_j d_j$$

where $SS(JP)$ is from loop 7 above.

d) Finally loop 12 calculates:

for $I=1, \dots, JJ$, where $JJ = \min(N, 100) = M$.

(i) Line 389 of code:

$$\text{DRAG} = \text{DRAG} + U * (\text{VEL} - U) * Z$$

$$= \sum_{i=1}^M U_i (U_\infty - U_i) \Delta Y_i$$

where $Z = YY(I) - YY(I - 1)$ (line 382 of code)

$$= Y_i - Y_{i-1}$$

$$= \Delta Y_i$$

and U is from loop 13 above.

(ii) Line 390 of code:

$$\text{DISP} = \text{DISP} + (\text{VEL} - U) * Z$$

$$= \sum_{i=1}^M (U_\infty - U_i) \Delta Y_i$$

Now, the real drag DRAGR and the computed drag DRAG are computed and printed. Also, the real and computed boundary layer, RBDL1 and RBDL respectively, are outputted. Finally, variables DRAGA and VAR are incremented and stored away for used by the main routine.

```

277
278
SUBROUTINE DISPL
COMMON,HH,N,L,VEL,RE,TSIG,CT,TPI,MN,CM
1 ,LOCK(30,30),LS,MS,FX,HY,X0,Y0
1 ,X(500),Y(500),S(500),CX(500),CY(500)
1 ,UXA(100),DRAGA,VAR,RIGHT,NGLD
1 ,MN(500),MNO,MNMAX
1 ,SOCK(30,30)
DIMENSIONLX(100),YY(100),SS(100)
JPR=1
X0=0.
Y0=0.
WHERE=1.
LS=30
MS=30
HX=1./30.
HY=0.4
HY=HY/SCRT(RE/WHERE)
IF(JPR.EQ.1)GOTO20
PRINT9008,FY
C
DO11=1,LS
DO1J=1,MS
SOCK(I,J)=0.
1 LOCK(I,J)=1H
DO2K=1,N
LK=(X(K)+X0)/FX
MK=(Y(K)+Y0)/FY
LK=LK+1
MK=MK+1
IF(LK.LT.1)GOTO2
IF(MK.LT.1)GOTO2
IF(LK.GT.LS)GOTO2
IF(MK.GT.MS)GOTO2
LOCK(LK,MK)=1F
SOCK(LK,MK)=SOCK(LK,MK)+S(K)
IF(SOCK(LK,MK).LT.0.)LOCK(LK,MK)=1HC
2 CONTINUE
DO3JJ=1,MS
J=MS-JJ+1
3 PRINT5004,(LOCK(I,J),I=1,LS)
20 CONTINUE
C
MU=20
HY=0.2
HY=HY/SCRT(RE/WHERE)
C VELOCITY PROFILE
DO40I=1,MU
UX(I)=VEL
DO4I=1,N
D=ABS(WHERE-X(I))
IF(D.GT.F)GOTO4
C=(H-D)/H
KU=Y(I)/HY
IF(KU.GT.MU)KU=MU
DO5J=1,KU
IF(KU.LT.1)GOTO5
LX(J)=LX(J)-S(I)
1 *C
5 CONTINUE
4 CONTINUE
PRINT5002
IF(JPR.EQ.1)GOTO21
DO6I=1,MU
CI=I
ETA=CI*HY*SCRT(RE/W/FRE)
6 PRINT5001,UX(I)
1 ,ETA
21 CONTINUE
DO14I=1,20
14 UXA(I)=UXA(I)+LX(I)
C

```

Fig. 5

```

347
-----348
349
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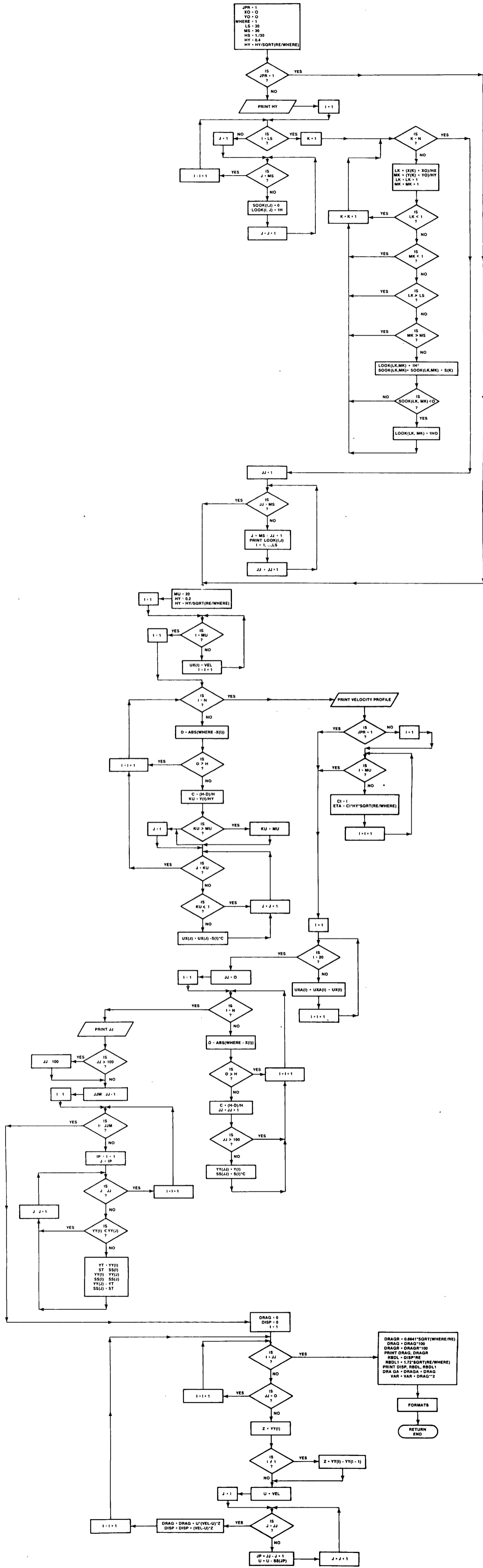
```

C
DRAG
JJ=0
DO7 I=1,N
D=ABS(WHERE-X(I))
IF(D.GT.H)GOTC7
C=(H-C)/H
JJ=JJ+1
IF(JJ.GT.100)GOTD7
YY(JJ)=Y(I)
SS(JJ)=S(I)
%C
7 CONTINUE
PRINT9005, JJ
IF(JJ.GT.100)JJ=100
JJM=JJ-1
DO10 I=1, JJM
IP=I+1
DO11 J=IP, JJ
IF(YY(I).LT.YY(J))GOTC11
YT=YY(J)
ST=SS(I)
YY(I)=YY(J)
SS(I)=SS(J)
YY(J)=YT
SS(J)=ST
11 CCNTINUE
10 CONTINUE
DRAG=0.
DISP=0.
DO12 I=1, JJ
IF(JJ.EQ.0)GOTC12
Z=YY(I)
IF(I.NE.1)Z=YY(I)-YY(I-1)
U=VEL
DO13 J=I, JJ
JP=JJ-J+1
L=L-SS(JP)
13 CONTINUE
DRAG=DRAG+L*(VEL-U)*Z
DISP=DISP+(VEL-L)*Z
12 CONTINUE
DRAGR=0.6641*SGRT(WHERE/FE)
DRAG=DRAG*100.
DRAGR=DRAGR*100.
PRINT9007, DRAG, DRAGR
RECL=CISP*RE
RBDL1=1.72*SGRT(RE*WHERE)
PRINT9009, DISP, RBDL, RBDL1
CRAGA=CRAGA+CFAC
VAR=VAR+DRAG**2
9000 FORMAT(/)
9001 FORMAT(1X,3F11.7)
9002 FORMAT(* VELOCITY PROFILE*)
9004 FORMAT(1X,60A1)
9005 FORMAT(* SHEETS IN SLICE*,I5)
9006 FORMAT(1X,F11.7)
9007 FORMAT(* DRAG*,2F11.7)
9008 FORMAT(* HY*,F11.7)
9009 FORMAT(* DISP AND RE*,3F15.7)
RETURN
END

```

Fig. 6

SUBROUTINE DISPL



4. Subroutine STEP

First, this subroutine creates the random numbers η_i . Then, each vortex sheet takes a random step as prescribed by formula (6a) and (6b) on page 6 of [1].

In order to use formulae (6a) and (6b), we need to know $\vec{U}_i = (U_i, V_i)$. So, for each vortex sheet Q_i , $i=1, \dots, N$, $|X_i - X_j| < h$, $Y_j > 0$, loop 1 and 2 calculates U_i and V_i in the following manner:

A) Lines 198 to 206 of the code corresponds to the integral (5b) of [1]: $U_\infty - I_1$.

1) line 198: $D = \text{ABS}(X(J) - X(I) - HH)$

$$= \left| X_j - X_i - \frac{h}{2} \right|$$

$$= \left| -(X_i - X_j + \frac{h}{2}) \right|$$

2) line 199: $D \leq H \Rightarrow 0 \leq d_j^+ \leq 1$

3) line 201: $C = (H - D)/H$

$$= \frac{h - \left| -(X_i - X_j + \frac{h}{2}) \right|}{h}$$

$$= 1 - \frac{\left| X_i - X_j + \frac{h}{2} \right|}{h}$$

$$= d_j^+$$

the smoothing coefficient corresponding to formula (5d) of [1].

4) line 202 and 203 corresponds to (5f) of [1].

Namely, $YY = \min(Y_j, Y_i)$

$= Y_j^*$ the displacement

5) line 205: $G1 = G1 + S(J) * YY * C$

$$= \sum_{j^+} \xi_j Y_j^* d_j^+$$

$$= U_\infty - I_1$$

B) Lines 207 to 215 calculates the integral $U - I_2$ which corresponds to (5c) of [1]:

1) line 207: $D = ABS(X(J) - X(I) + HH)$

$$= \left| X_j - X_i + \frac{h}{2} \right|$$

$$= \left| -(X_i - X_j - \frac{h}{2}) \right|$$

2) line 208: $D < H \Rightarrow 0 \leq d_j^- \leq 1$

3) line 210: $C = (H - D)/H$

$$= \frac{h - \left| -(X_i - X_j - \frac{h}{2}) \right|}{h}$$

$$= 1 - \frac{\left| X_i - X_j - \frac{h}{2} \right|}{h}$$

$$= d_j^- \quad \text{formula (5e) of [1].}$$

4) lines 211 and 212 again is: $YY = \min(Y_i, Y_j) = Y_j^*$

5) line 214: $G2 = G2 + S(J) * YY * C$

$$= \sum_{j^-} \xi_j Y_j^* d_j^-$$

$$= U_\infty - I_2 \quad \text{by (5c) of [1].}$$

c) Lines 216 to 220 calculates (4a) of [1]:

$$U_i = U_\infty - \frac{1}{2} \xi_i - \sum_j \xi_j d_j$$

1) line 189: $U = Vel \Rightarrow U = U_\infty$

2) line 190: $U = U - S(I) * 0.5$

$$= U_\infty - \frac{1}{2} \xi_i$$

3) line 216: $D = \text{ABS}(X(J) - X(I))$

$$= |X_j - X_i|$$

$$= |-(X_i - X_j)|$$

4) line 217: $D < H \Rightarrow |X_i - X_j| < h$

5) line 219: $C = (H - D)/H$

$$= 1 - \frac{|X_i - X_j|}{h}$$

$$= d_j \quad \text{by (4b) of [1].}$$

6) line 220: For $Y_j > Y_i$, $U = U - S(J) * C$

$$= U_\infty - \frac{1}{2} \xi_i - \sum_j \xi_j d_j$$

Now, if $Y_i = 0$ (i.e. on the wall) then the U_i component of velocity

$$DX(I) = 0. \quad \text{Else, } DX(I) = U = U_\infty - \frac{1}{2} \xi_i - \sum_j \xi_j d_j.$$

Also, if $X_i > RRI$ (i.e. outside domain of interest) then the V_i component

$$DY(I) = 0. \quad \text{Else, } DY(I) = (G1 - G2)/H$$

$$= \frac{(U_\infty - I_1) - (U_\infty - I_2)}{h}$$

$$= \frac{-I_1 + I_2}{h}$$

$$= V_i \quad \text{by (5a) of (1).}$$

Having calculated U_i and V_i , we have yet to find η_i before we can

take a random step. This random variable η_i is drawn from a gaussian

distribution with mean 0 and variance $\sqrt{4\nu k}$ in the following way:

$$\begin{aligned} Q1 &= \text{RANF}(0.) & \text{RANF}(0.) \text{ returns a pseudo-random number s.t.} \\ Q2 &= \text{RANF}(0.) & 0 < Q1 < 1 \\ & & 0 < Q2 < 1 \end{aligned}$$

$$QR = \text{SQRT}(-\text{TSIG} * \text{ALOG}(Q1))$$

$$\text{WALK} = QR * \text{SIN}(TPI * Q2)$$

where $\eta_i = \text{WALK}$. For further discussion, see reference [2] pg. 39.

Before actually taking the random step, a few things need to be checked. First, line 234 checks to see if the tags of the successive vortex sheets are the same. If they are, then they are assigned the same η_i . Since the tags are ordered linearly, this process is straightforward.

Next, the subroutine checks to see if $Y_i = 0$. If it is, then we wish to choose η_i s.t. η_i have different signs each time. This alternating of signs of the random variable η_i is to ensure that the random step, steps across the wall exactly one half of the time. This process of alternating signs is aided by the variable LIP which takes on values ± 1 . Now, $Y_i = 0$ and $LIP > 0$ implies that $\eta_i > 0$ the last time. So, jump to line 254 and generate $\eta_i = WALK > 0$ and set $LIP < 0$. If $Y_i = 0$ and $LIP < 0$ then generate $\eta_i = WALK < 0$ and so on. This corresponds to lines 239-260 of code.

With the appropriate η_i on hand, the random step is taken in the following manner:

Line 263: $X(I) = X(I) + DT * DX(I)$

$$X_i^{n+1} = X_i^n + kU_i$$

which is formula (6a) of [1].

Line 265: $Y(I) = Y(I) + DY(I) * DT + WALK$

$$Y_i^{n+1} = Y_i^n + kV_i + \eta_i$$

which is formula (6b) of (1).

Finally, if $Y_i^{n+1} < 0$ and $Y_i^n \neq 0$, then reflect the point by symmetry, setting $Y_i^{n+1} = -Y_i^{n+1}$. However, if $Y_i^{n+1} < 0$ and $Y_i^n = 0$ then Y_i^{n+1} is lost across the wall. This whole process is done for each vortex sheet Q_i , $i=1, \dots, N$.

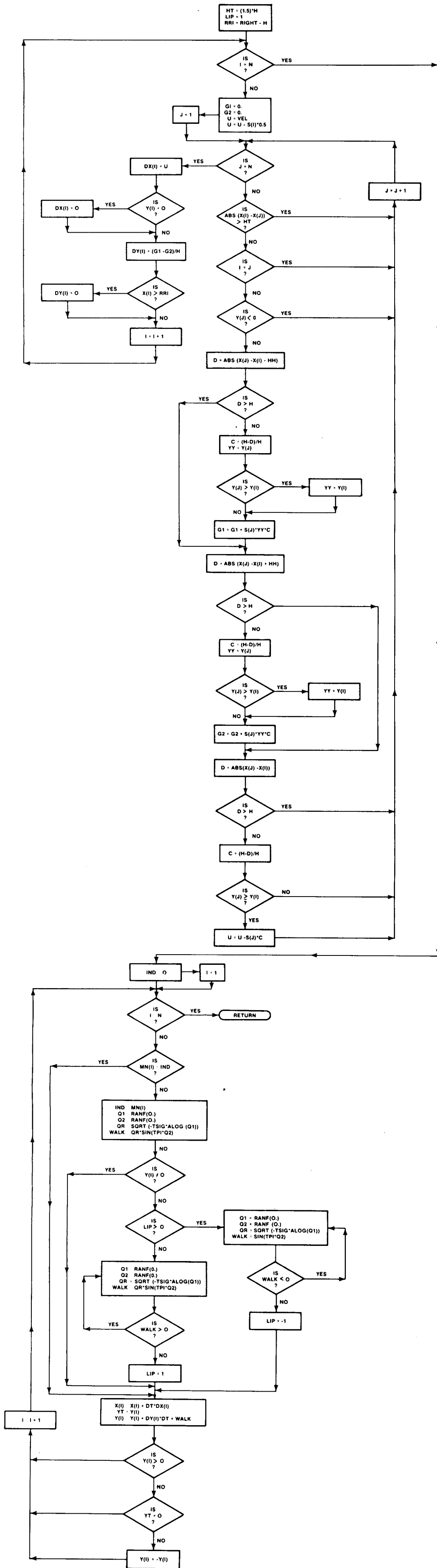
```

191          SUBROUTINE STEP
192          COMMON/HH,N,L,VEL,RE,TSIG,CT,TPI,MM,CM
1          ,LOOK(30,30),LS,MS,HX,HY,X0,Y0
1          ,X(500),Y(500),S(500),CX(500),CY(500)
1          ,UXA(100),DRAGA,VAR,RIGHT,ACLD
1          ,MN(500),MNO,MNMAX
          HT=1.5*H
          LIP=1
          RRI=RIGHT-1
          DO 11=1,N
          G1=0.
          G2=0.
          U=VFL
          U=U-S(I)*0.5
          DO 2J=1,N
          IF (ABS(X(I)-X(J)).GT.H1)GOTC2
          IF (I.EQ.J)GOTC2
          IF (Y(J).LT.C.)GOTC2
          D=ABS(X(J)-X(I)-FF)
          IF (D.GT.H)GOTC3
          C=(F-D)/F
          YY=Y(J)
          IF (Y(J).GT.Y(I))YY=Y(I)
          G1=G1+S(J)*YY
1          *C
          3 CONTINUE
          D=ABS(X(J)-X(I)+FF)
          IF (D.GT.H)GOTC4
          C=(F-D)/F
          YY=Y(J)
          IF (Y(J).GT.Y(I))YY=Y(I)
          G2=G2+S(J)*YY
1          *C
          4 CONTINUE
          D=ABS(X(J)-X(I))
          IF (D.GT.H)GOTC2
          C=(H-D)/F
          IF (Y(J).GE.Y(I))L=L-S(J)*C
          2 CONTINUE
          DX(I)=C
          IF (Y(I).EQ.C.)DX(I)=0.
          DY(I)=(G1-G2)/F
          IF (X(I).GT.RRI)DY(I)=0.
          1 CONTINUE
          INC=0
          DO 5I=1,N
          IF (MN(I).EQ.INC)GOTC5
          INC=MN(I)
          Q1=RANF(0.)
          Q2=RANF(0.)
          QR=SQRT(-TSIG*ALCG(C1))
          WALK=QR*SIN(TPI*Q2)
          IF (Y(I).NE.0.)GOTC8
          IF (LIP.GT.0)GOTO9
          10 CONTINUE
          Q1=RANF(0.)
          Q2=RANF(0.)
          CR=SQRT(-TSIG*ALCG(C1))
          WALK=CR*SIN(TPI*Q2)
          IF (WALK.CT.0.)GOTC10
          LIP=1
          GOTD8
          9 CONTINUE
          11 CONTINUE
          Q1=RANF(0.)
          Q2=RANF(0.)
          QR=SQRT(-TSIG*ALCG(C1))
          WALK=QR*SIN(TPI*Q2)
          IF (WALK.LT.0.)GOTC11
          LIP=-1
          8 CONTINUE
          6 CONTINUE
          X(I)=X(I)+CT*CX(I)
          Y(I)=Y(I)+CT*CY(I)
          Y(I)=Y(I)+DY(I)*DT
          1 +WALK
          IF (Y(I).CT.0.) GOTC7
          IF (Y(I).EQ.0.)GOTC7
          Y(I)=-Y(I)
          7 CONTINUE
          5 CONTINUE
          9001 FORMAT(1X,10F5.5)
          9002 FORMAT(1X,2I5,5F9.5)
          RETURN
          END

```

Fig. 8

Subroutine STEP



OUTPUT FROM PROGRAM BOUNDL

STEP	1 TIME	.2000000
1	.1000000	1.0000000
2	.3000000	1.0000000
3	.5000000	1.0000000
4	.7000000	1.0000000
5	.9000000	1.0000000
6	1.1000000	1.0000000
7	1.3000000	1.0000000

N 140
 VFLCCITY PRCFILE
 SHEETS IN SLICE 40
 DRAG .0664100
 DISP AND RE 0. 0. 1720.0000000

STEP	2 TIME	.4000000
1	.1000000	-.0000000
2	.3000000	-.0000000
3	.5000000	-.0000000
4	.7000000	-.0000000
5	.9000000	-.0000000
6	1.1000000	-.0000000
7	1.3000000	-.0000000

N 70
 VELOCITY PRCFILE
 SHEETS IN SLICE 20
 DRAG .0181800
 DISP AND RE .0000035 503.4693629 1720.0000000

STEP	3 TIME	.6000000
1	.1000000	.0000000
2	.3000000	-.0000000
3	.5000000	-.0000000
4	.7000000	-.0000000
5	.9000000	-.0000000
6	1.1000000	-.0000000
7	1.3000000	-.0000000

N 80
 VELOCITY PRCFILE
 SHEETS IN SLICE 20
 DRAG .0304548
 DISP AND RE .0007364 736.3841169 1720.0000000

STEP	20 TIME	4.0000000
1	.1000000	.4276434
2	.3000000	.0713727
3	.5000000	.0494275
4	.7000000	-.0091353
5	.9000000	.1512212
6	1.1000000	-.0592686
7	1.3000000	.0566237

N 144
 VELOCITY PRCFILE
 SHEETS IN SLICE 47
 DRAG .0651838
 DISP AND RE .0024371 2437.1317559 1720.0000000

AVERAGE PROFILE
 .13770
 .28023
 .37104
 .47500
 .55844
 .60854
 .67399
 .74609
 .78223
 .81019
 .86073
 .87580
 .89894
 .91307
 .93119
 .94748
 .95074
 .95788
 .96810
 .97418

AVERAGE DRAG .0420176
 VARIANCE .0042745

Fig. 10

OUTPUT FORMAT FOR PROGRAM BOUNDL

<u>STEP</u>	<u>ISTEP TIME</u>	<u>TIME</u>
I = 1	X(I)	S(I) = i
2	.	.
.	.	.
.	.	.
.	.	.
L	X(L)	.

N

VELOCITY PROFILE

SHEETS IN SLICE JJ

DRAG DRAG DRAGR

DISP AND RE DISP RBDL RBDL1

REFERENCES

- [1]: Chorin, A. J., Vortex Sheet Approximation of Boundary Layers,
J. Comput. Physics, 1978.
- [2]: J. M. Hammersley and D. C. Hamdscomb, Monte Carlo Methods, Methuen,
London 1964.

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