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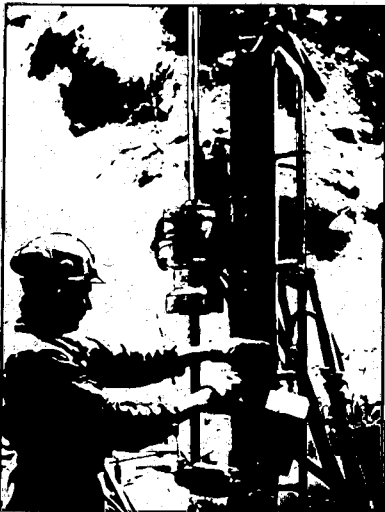
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## SEISMIC VELOCITIES AND ATTENUATION IN A HEATED UNDERGROUND GRANITIC REPOSITORY

Volume II

B.N.P. Paulsson

Lawrence Berkeley Laboratory  
University of California  
Berkeley, California 94720

January 1983

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SEISMIC VELOCITIES AND ATTENUATION  
IN A HEATED UNDERGROUND GRANITIC REPOSITORY  
Volume II

Bjorn Nils Patrick Paulsson

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SEISMIC VELOCITIES AND ATTENUATION IN  
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## Appendix A:1 - pole plots

The orientation of the fractures logged in core from vertical and horizontal boreholes drilled for the H9 heater experiment is an important part of the data base used for the analysis of the cross hole ultrasonic P and S wave velocities and attenuation.

The fractures were divided up into several subgroups. These groups include whether the fracture comes from a horizontal or vertical borehole; if the fracture is open or closed in the core; and which mineral was the dominant mineral coating the fracture surfaces.

The core was broken at several places for most fractures but only breaks in the core which coincided with a natural fracture was counted as an open fracture. A closed fracture is defined as a fracture found in the core with a mineral infilling and having a traceable exposure over the entire circumference. Most common of the fracture infilling materials were chlorite, epidote and calcite. Occurrences of fluorite, pyrite and hematite were also recorded. The implication of whether the fracture is from a horizontal or a vertical borehole is that that the fracture spacing calculated for a rock mass from core is only correct for fractures which are perpendicular to the drilling direction. The apparent spacing between fractures vary as  $x_a = \frac{x_r}{\sin \alpha}$  where  $x_a$  is the apparent spacing and  $x_r$  the real spacing of this fracture set measured along a line perpendicular to the fracture surface.  $\alpha$  is the angle between the axis of the borehole and the fracture plane. This bias is partly corrected for in the pole plot of all the fractures as there are fractures from vertical holes, as well as from horizontal holes drilled in three different directions. In Figure A:1.1 the relative frequency of all the oriented fractures

around the H9 heater experiment are shown. This includes fractures from both horizontal and vertical boreholes. In Figure A:1.2 the fractures from the vertical holes drilled from the full scale drift are shown. Figure A:1.3 shows the fractures logged in core from the horizontal boreholes drilled from the extensometer drift. The difference of the position of the main pole is indeed striking and confirms the statement above. These two latter figure show fracture data from the same body of Stripa quartz monzonite. From the vertical boreholes there appear to be two major poles striking N - NE with a dip of  $55^\circ$  and  $35^\circ$  respectively. From the data obtained from the horizontal boreholes the major pole appear to be a vertical set with a N - S strike.

In Figure A:1.4 the closed fractures from the vertical and the horizontal boreholes are presented. In Figure A:1.5 the closed fractures from the vertical holes are shown. In Figure A:1.6 the open fractures for all the holes are shown and in Figure A:1.7 the fractures from the horizontal holes are seen. An interesting phenomenon is that open fractures tend to be more perpendicular to the drill direction than the closed fractures. A possible explanation for this is that when the drill direction is perpendicular to a fracture the fracture surface is small compared to if the drill passes a fracture at an angle other than  $90^\circ$ . This increase the likelihood that this fractures will break in the drilling process. In Figure A:1.8 the calcite fractures from all the boreholes in the H9 area are shown. It is notisable that the calcite filled fractures lack a dominant direction.

Schmidt equal-area pole plot for vertical and horizontal holes H9% occurrence

Lower hemisphere

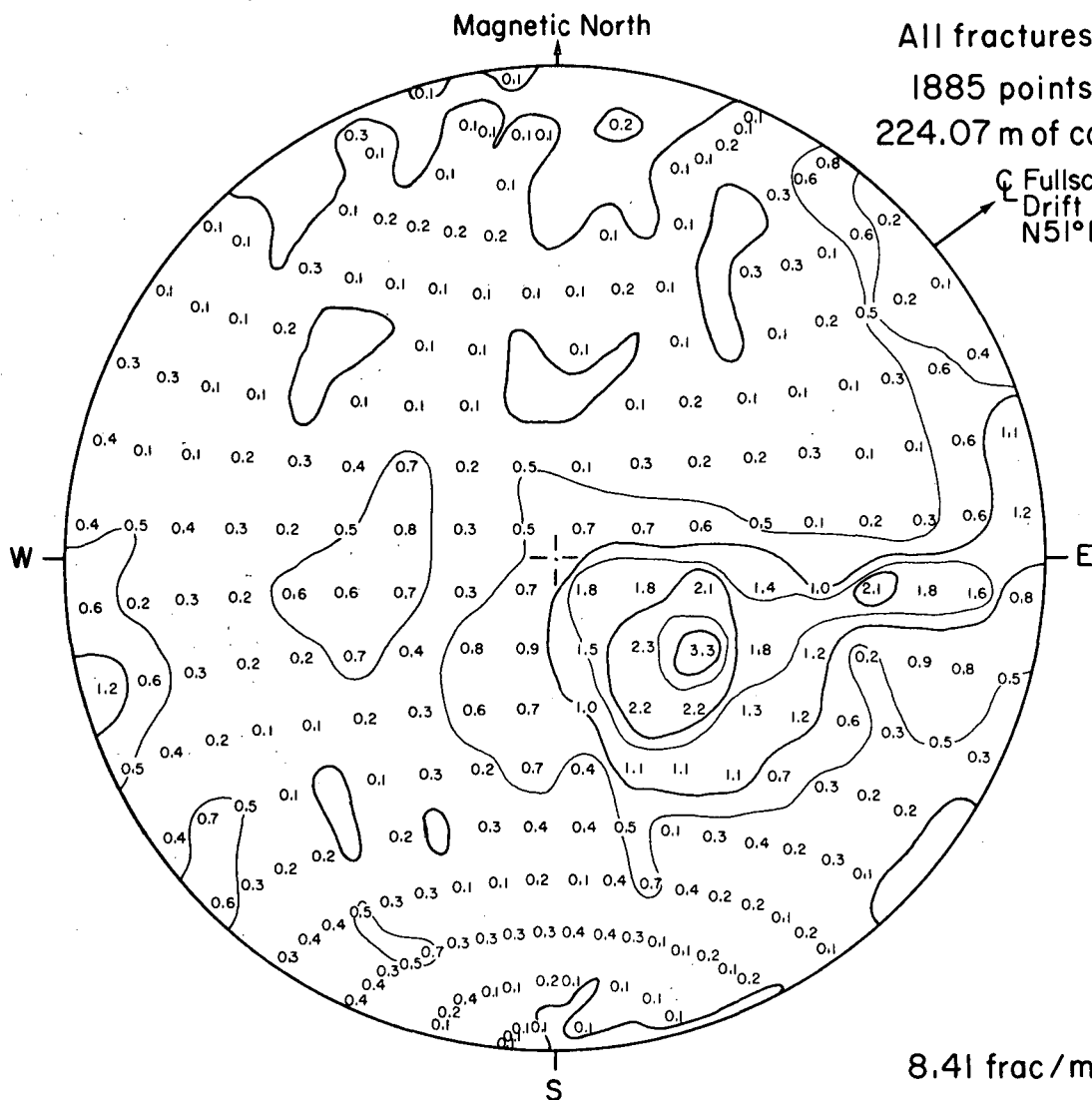
All mineralization

All fractures

1885 points

224.07 m of core

Fullscale Drift N51°E



XBL 8012-6589

Fig. A:1.1 Schmidt equal-area pole plot for fractures from vertical and horizontal boreholes in the H9 area.

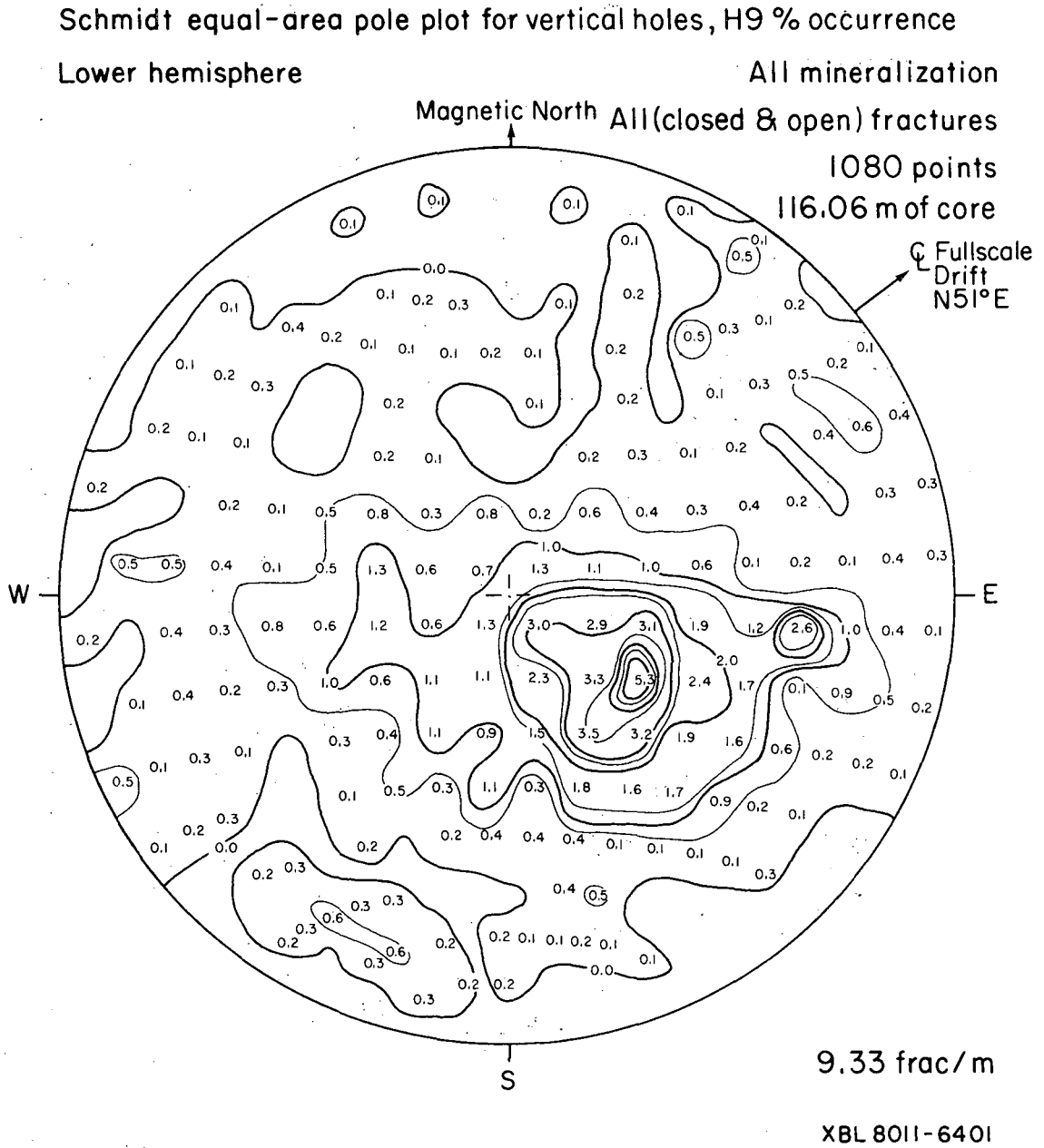


Fig. A:1.2 Schmidt equal-area pole plot for fractures from vertical boreholes in the H9 area.

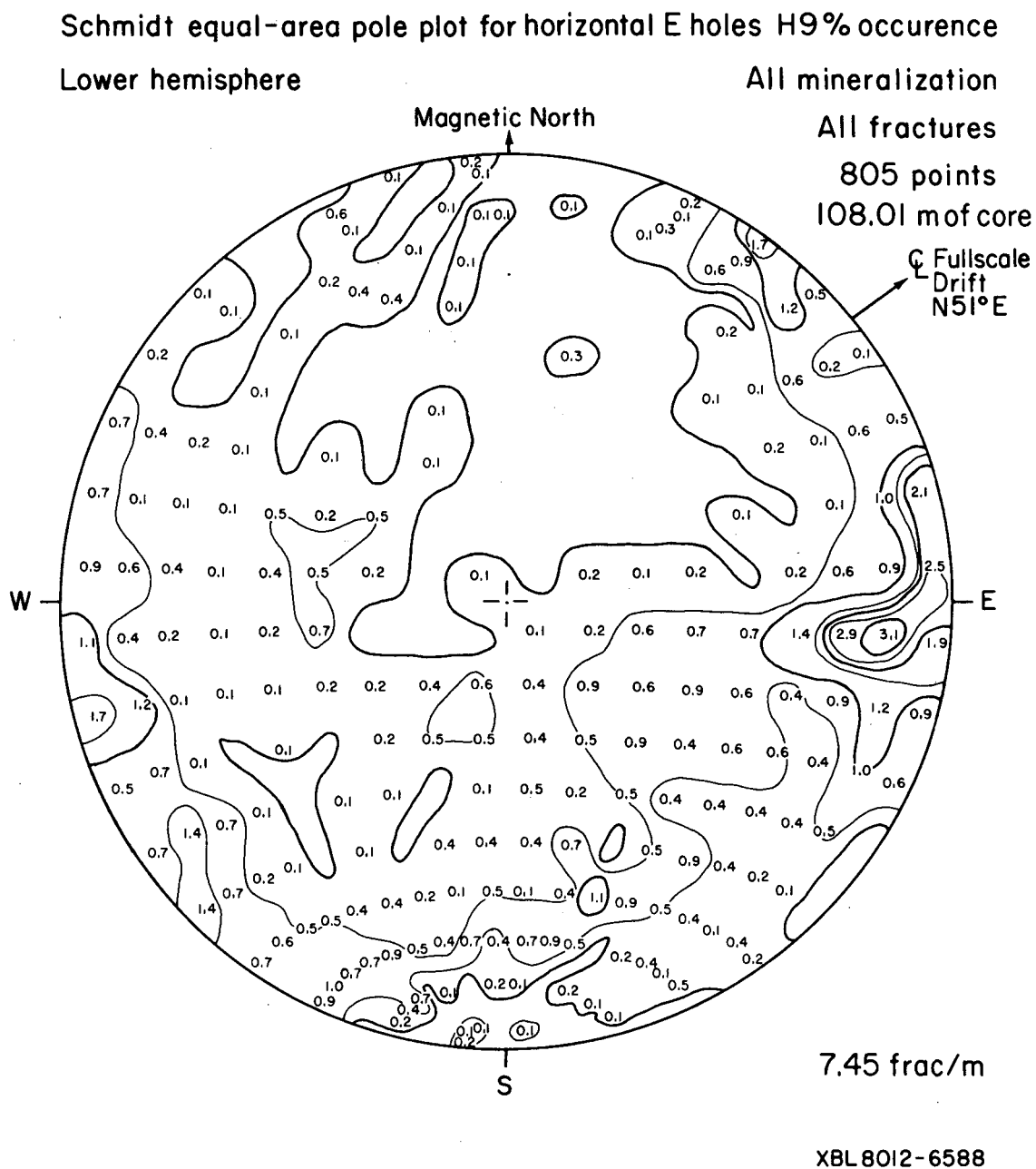


Fig. A:1.3 Schmidt equal-area pole plot for fractures from horizontal boreholes in the H9 area.

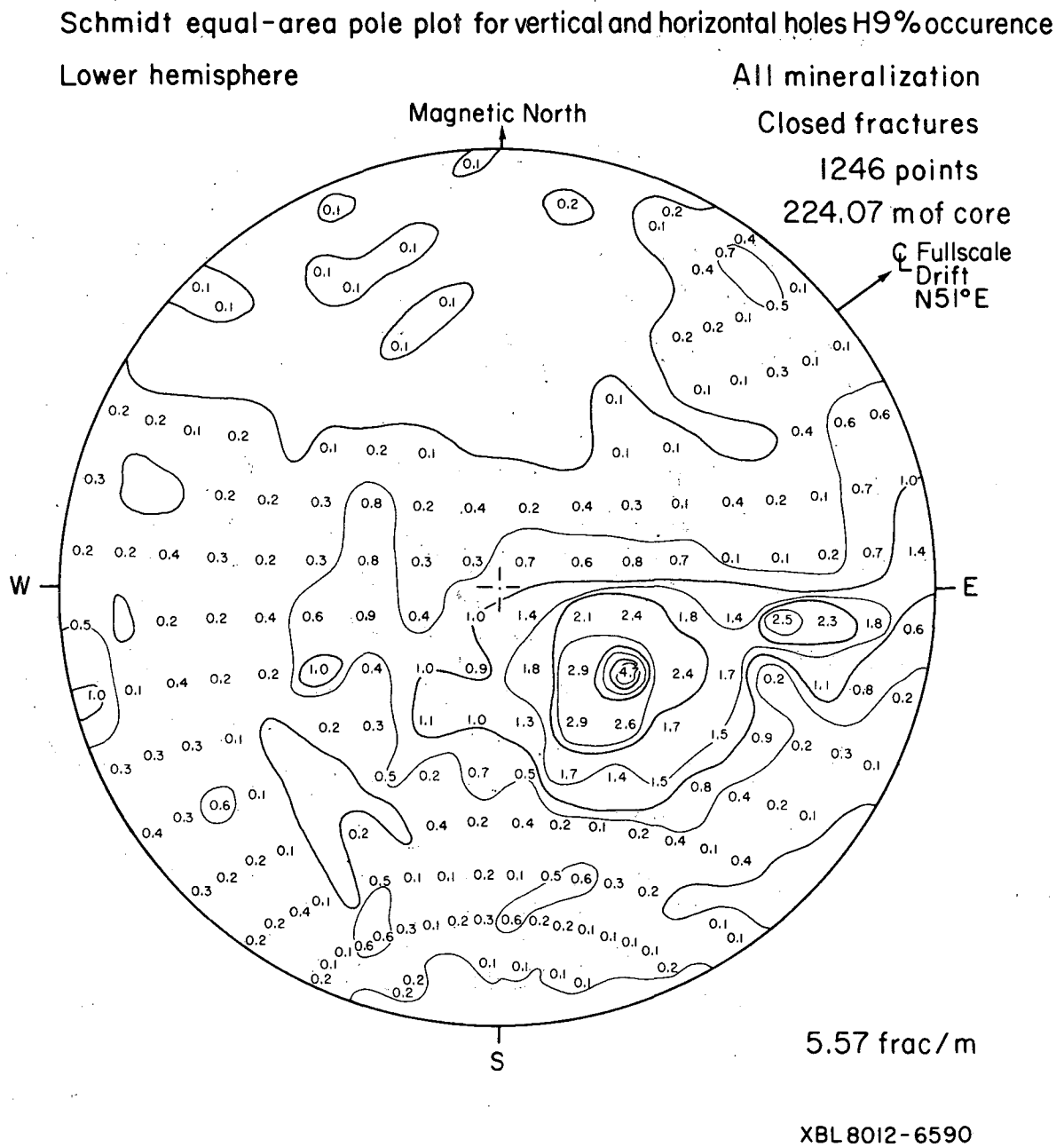
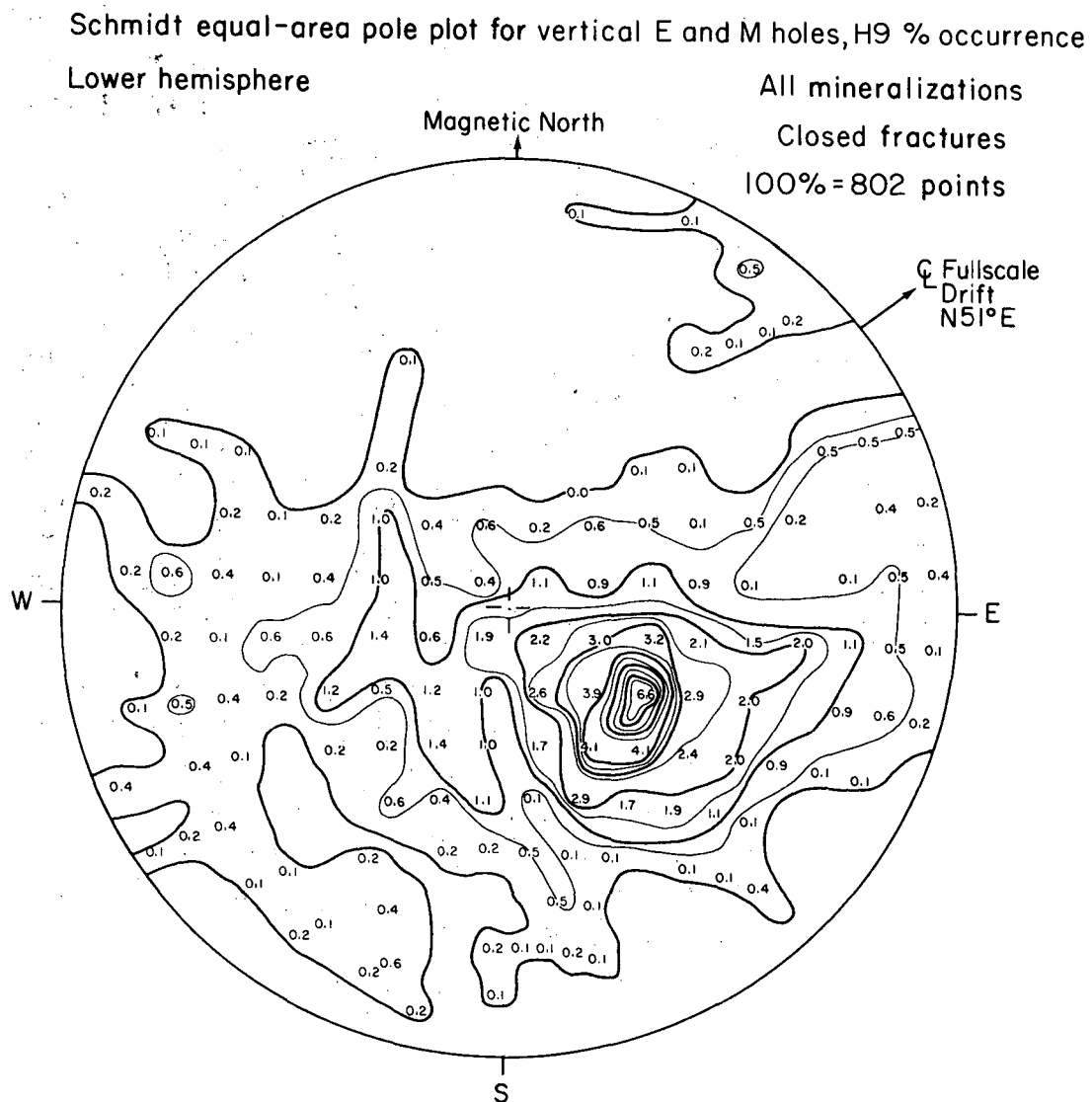
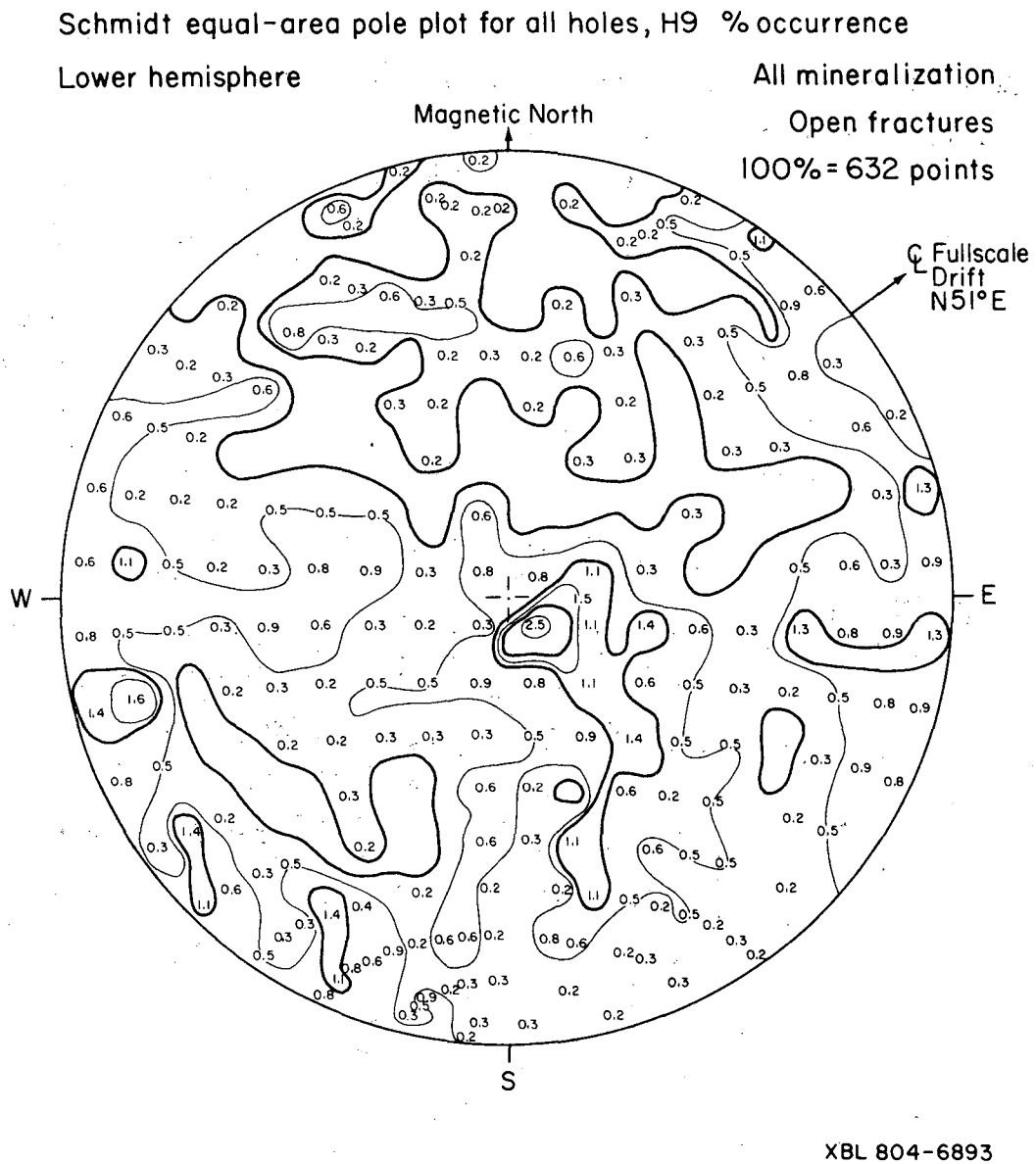


Fig. A:1.4 Schmidt equal-area pole plot for closed fractures from vertical and horizontal boreholes in the H9 area.



XBL 801-6786

Fig. A:1.5 Schmidt equal-area pole plot for closed fractures from vertical boreholes drilled from the fullscale drift in the H9 area.



XBL 804-6893

Fig. A:1.6 Schmidt equal-area pole plot for open fractures from vertical and horizontal boreholes in the H9 area.



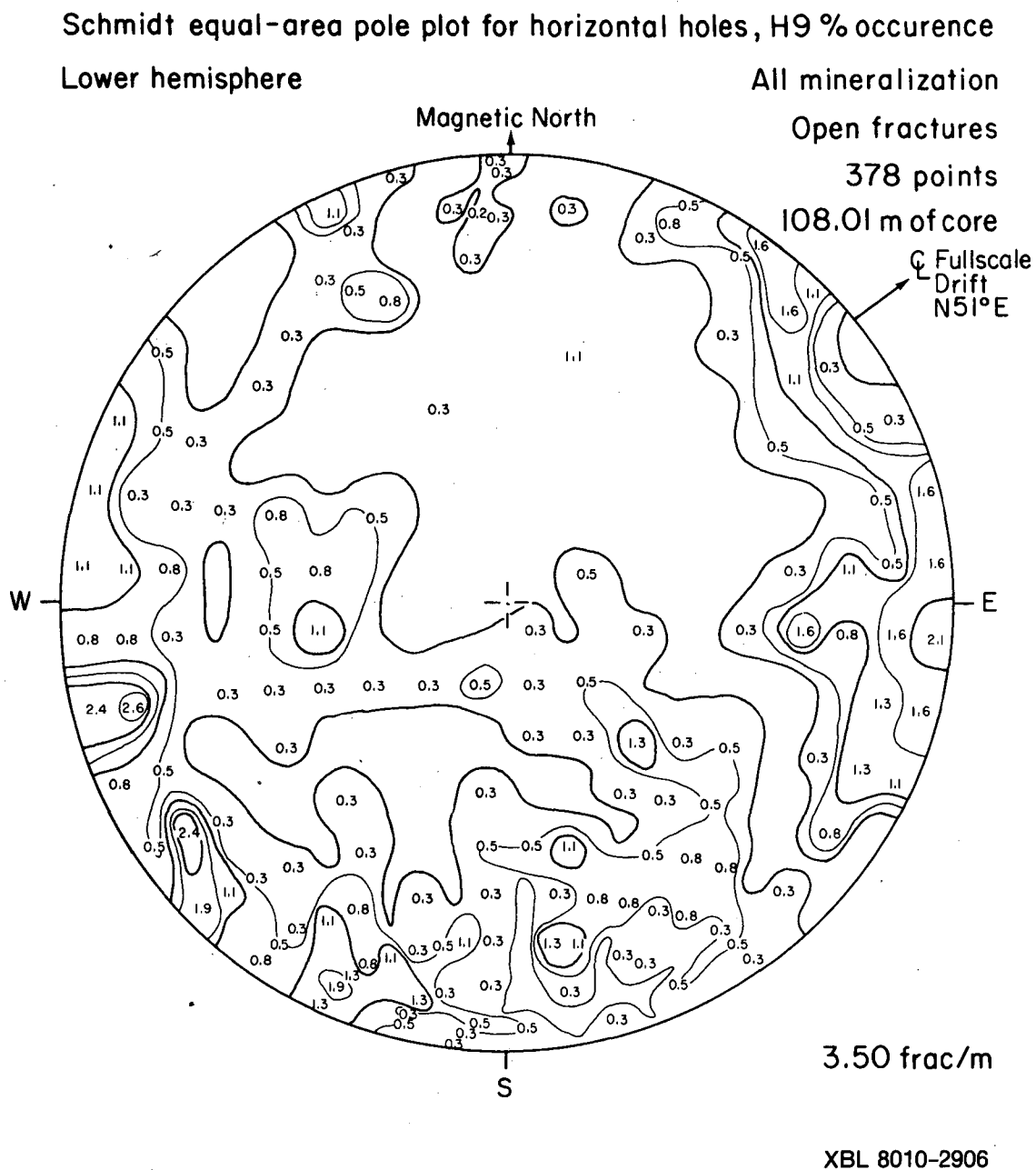
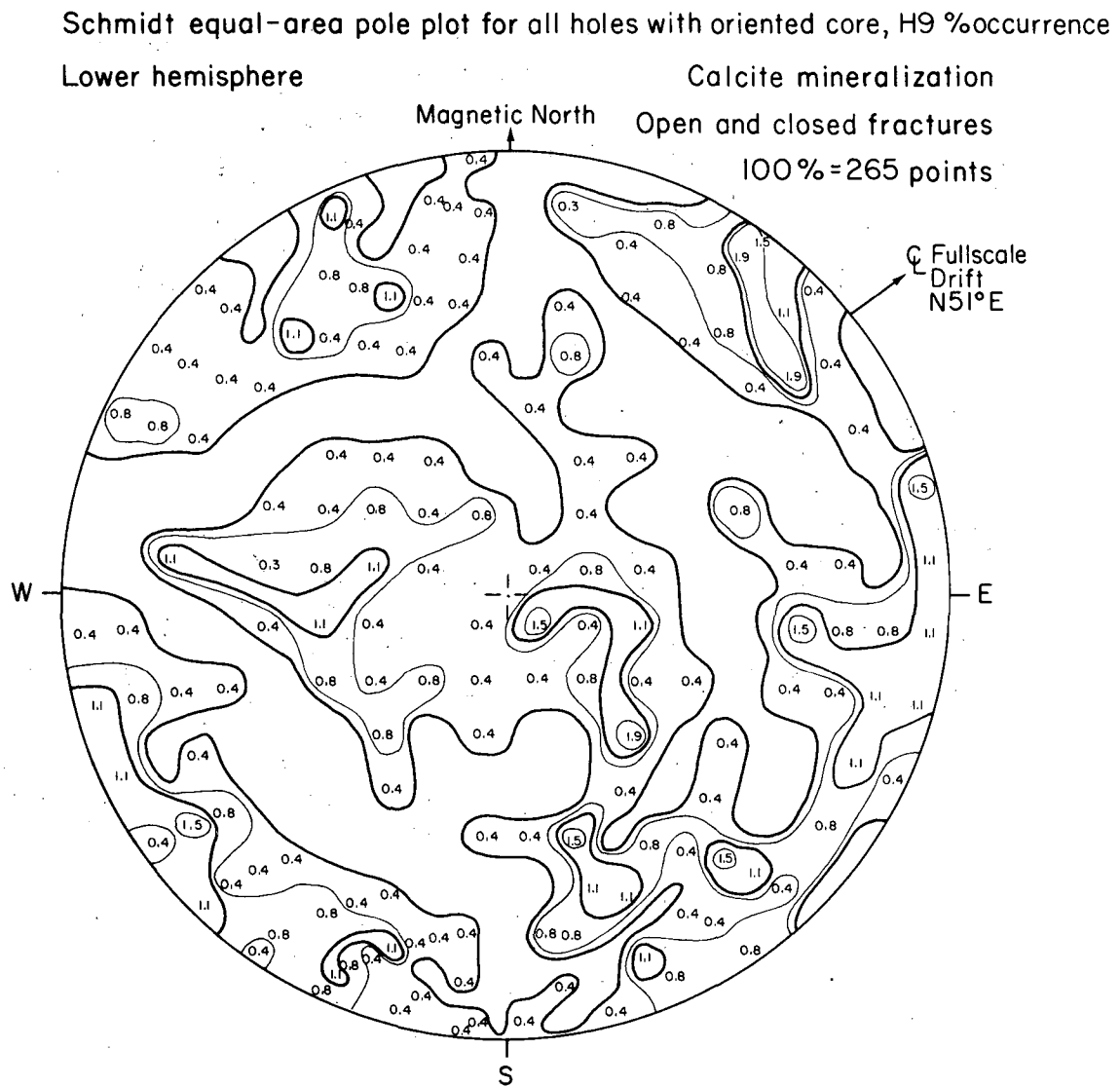


Fig. A:1.7 Schmidt equal-area pole plot for open fractures from horizontal boreholes in the H9 area.



XBL 804-6894

Fig. A:1.8 Schmidt equal-area pole plot for calcite fractures from the vertical and horizontal boreholes in the H9 area.

## Appendix A:2 - geologic cross sections

The six cross section presented in this appendix have the geological information superimposed. The basic geological information is presented in this way rather than in a hard to digest table. The small fracture trace beside the strike dip is the apparent dip in this cross section. That makes it possible to correlate fractures from borehole to borehole.

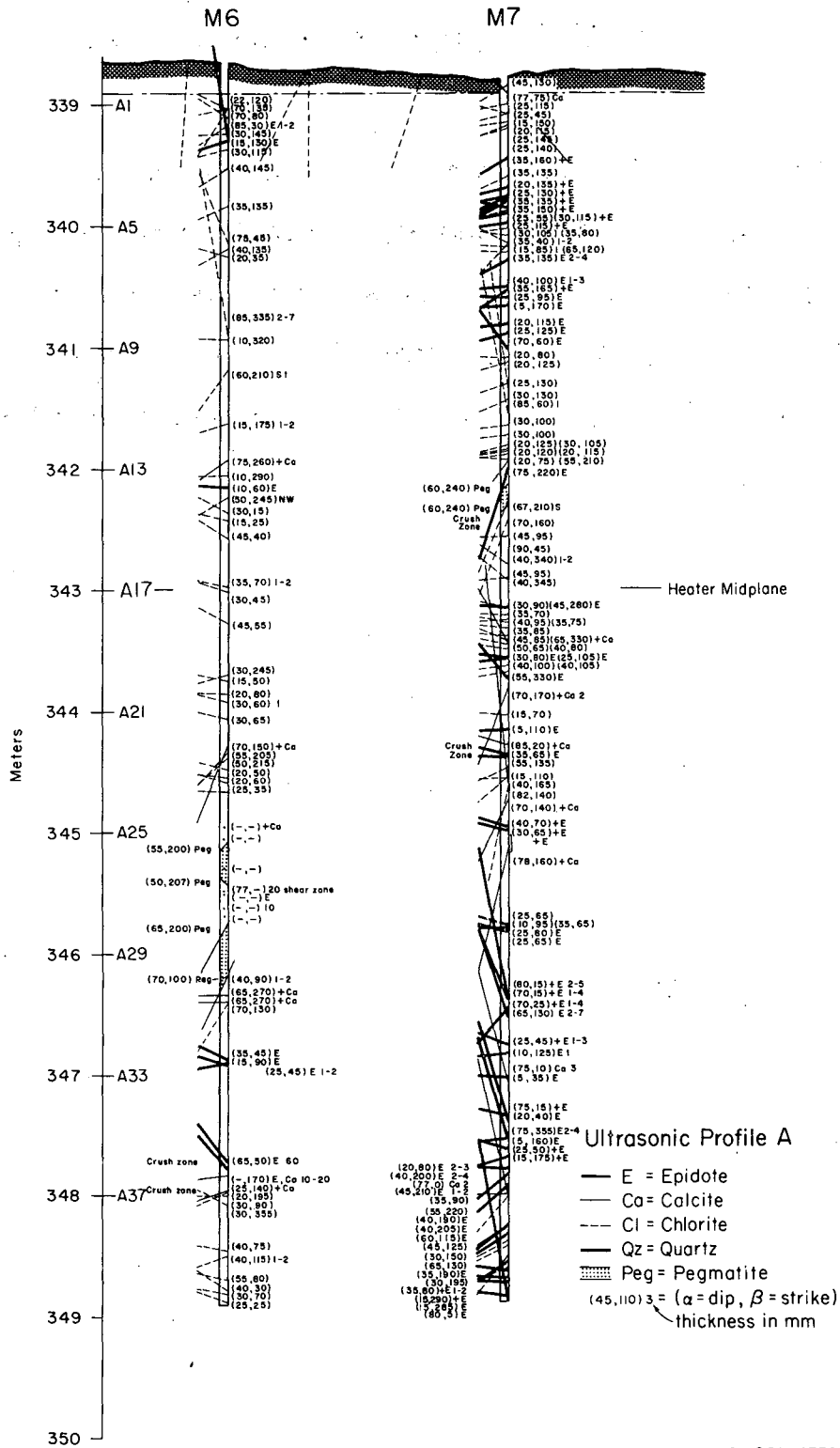


Fig. A:2.1 Section M7-M6, showing the location apparent dip and orientation information for open and closed fractures.

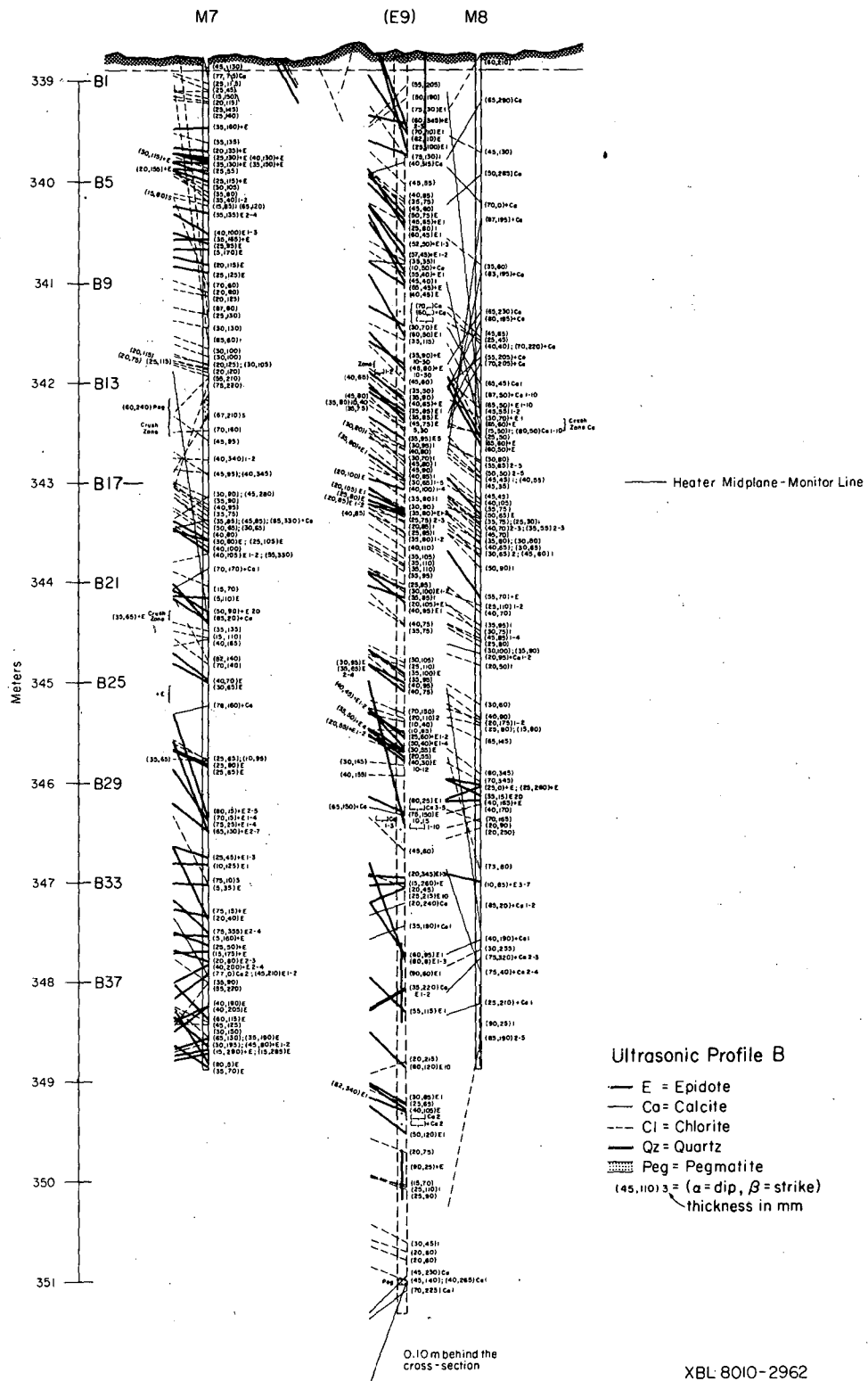


Fig. A:2.2 Section M8-M7, showing the location, apparent dip and orientation information for open and closed fractures.

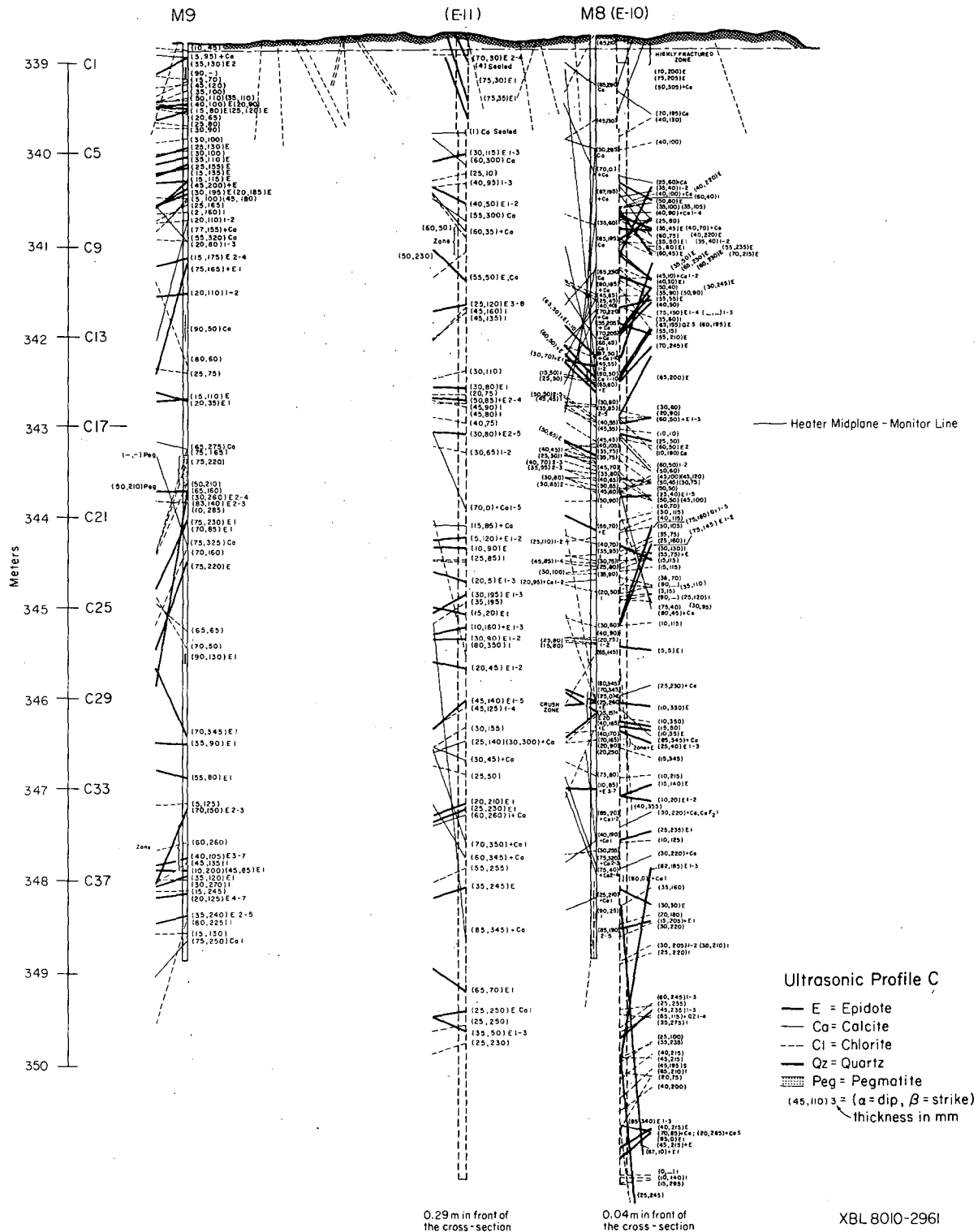
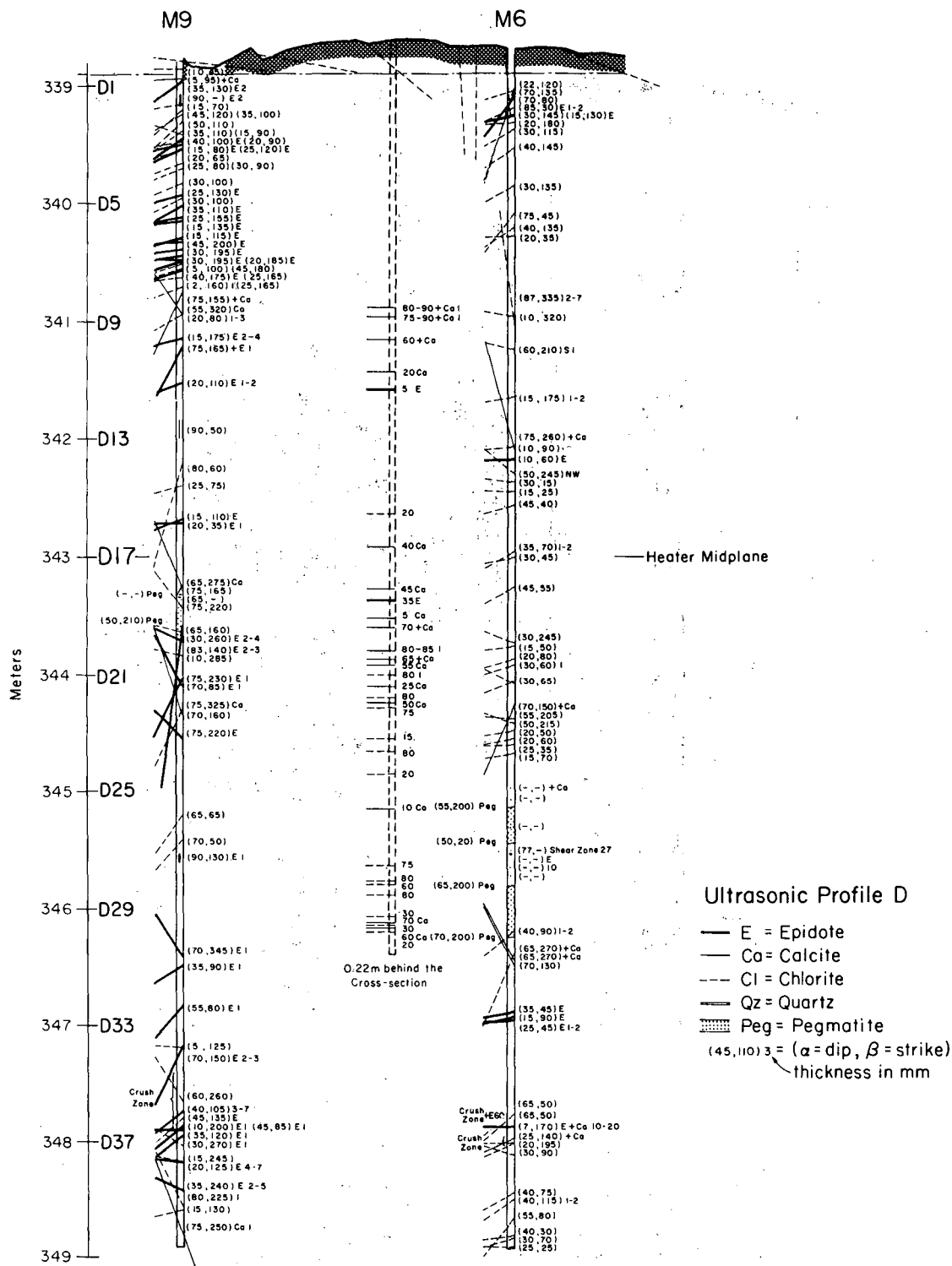


Fig. A:2.3 Section M8-M9, showing the location, apparent dip and orientation information for open and closed fractures.



XBL 803-6857

Fig. A:2.4 Section M9-M6, showing the location, apparent dip and orientation information for open and closed fractures.

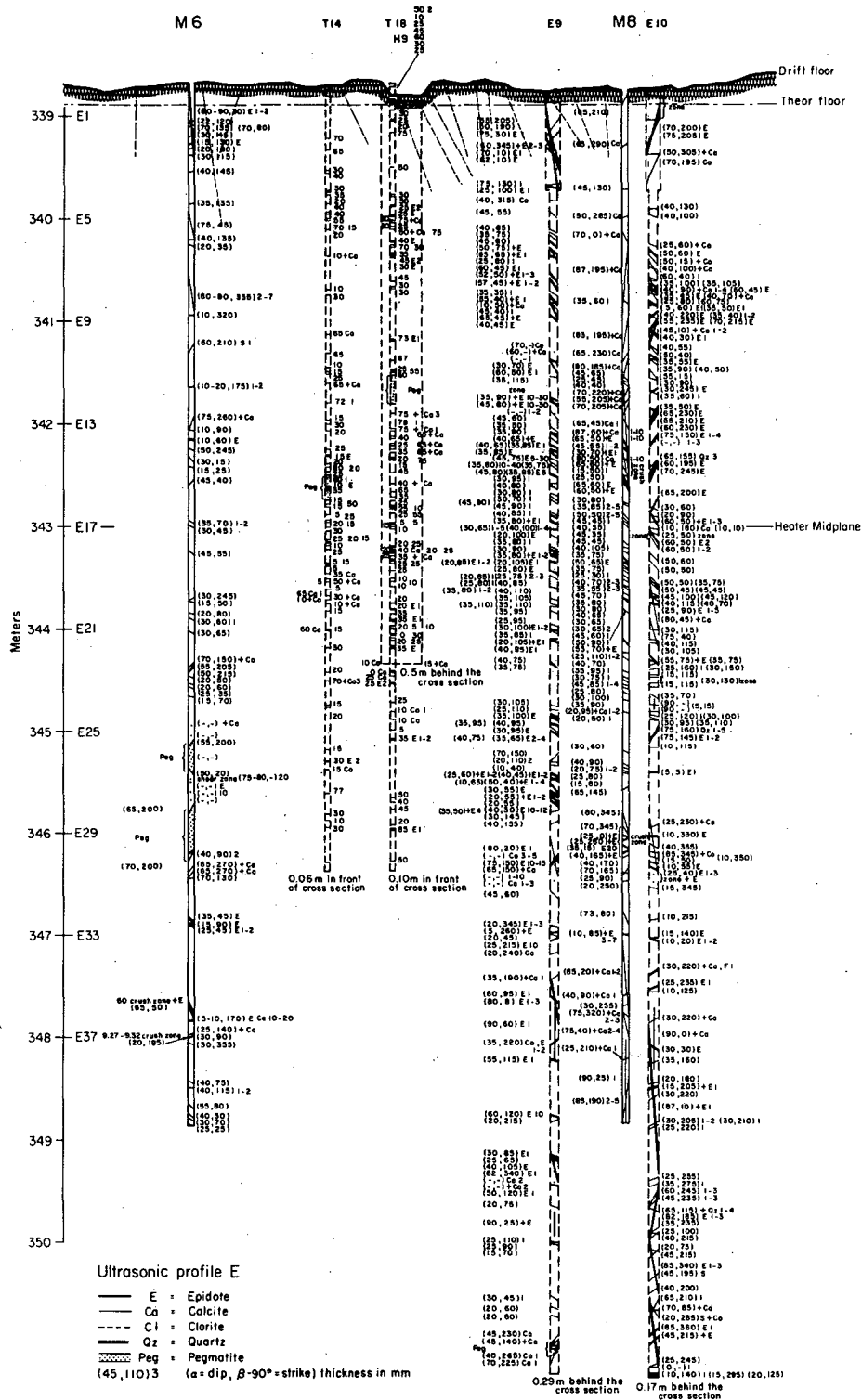


Fig. A:2.5 Section M8-M6, showing the location, apparent dip and orientation information for open and closed fractures.



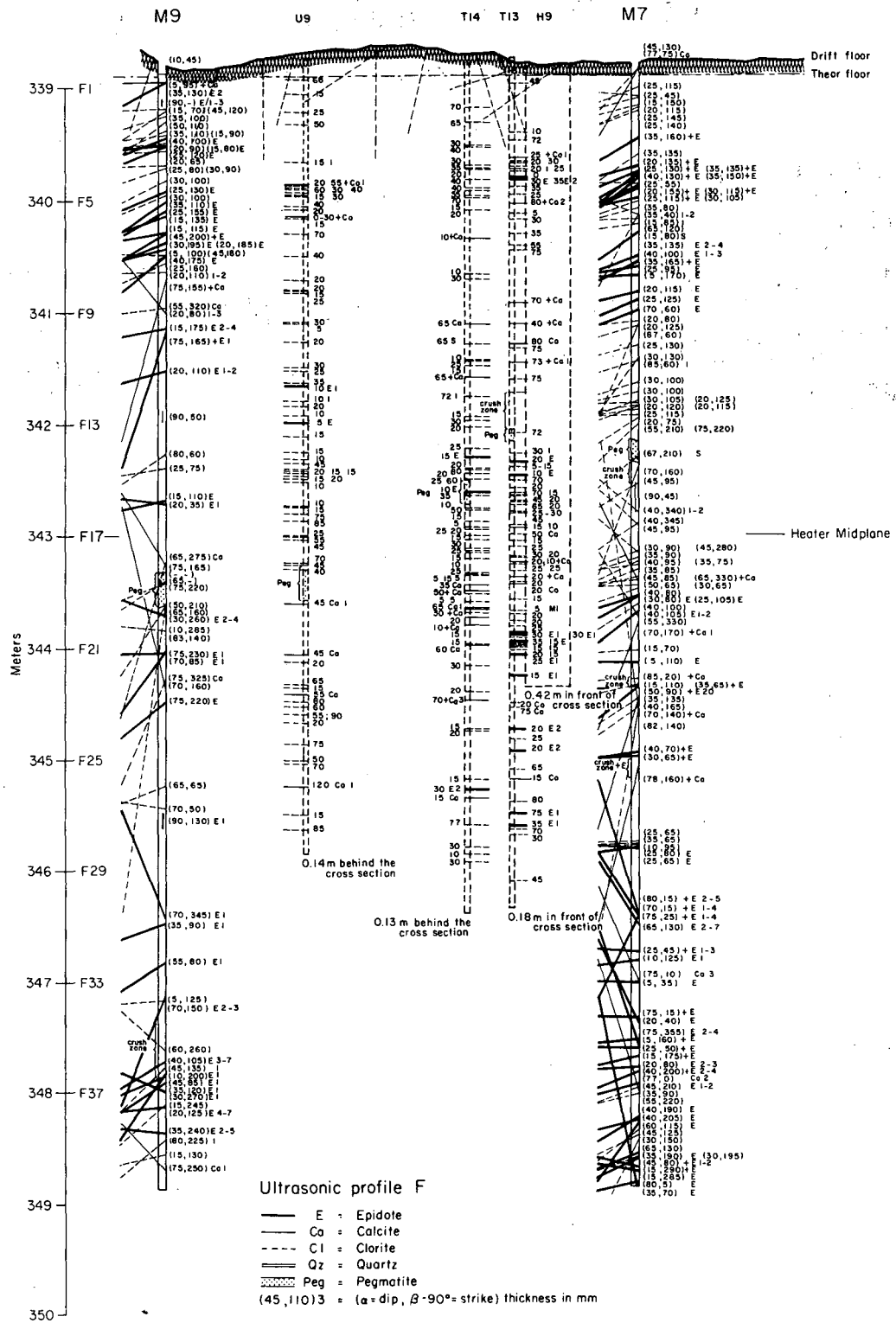


Fig. A:2.6 Section M7-M9, showing the location, apparent dip and orientation information for open and closed fractures.

**Appendix B:1 - Coordinates for boreholes  
M6, M7, M8 and M9.**

In this appendix the survey data from the location survey of the boreholes M6-M9 are given in Tables B:1.1 - 4. The coordinate system used in tables B:1.5 - 8 is the coordinate system for the mine. In tables B:1.5 - 8 the coordinates for the data points in the four monitor holes are presented.



# KOORDINATFORTECKNING

341

Datum

17/1 1978

Sid

Område Stripa-Full scale nr. M6 Uppdragsnr \_\_\_\_\_

Plankordinaternas beräknade i system Mine system Beräknat av: LW

Höjderna angivna i meter över Mine system Kontroll av: LW

Punkt bet	Mar-ke-ring	Koordinater			Anmärkningar Tolerance
		Xmeter	Ymeter	Zmeter	
15					
02		323 610	1009 340	338 897	
		323 608	1009 342	338 670	
		- 002	+ 002	- 227	
		Radial dist.:	0,003 m		0,020 m
		Direction:	150,000 gon		
		323 610	1009 340	338 897	
		323 615	1009 353	343 679	
		+ 005	+ 013	4 782	
		Radial dist.:	0,014 m		
		Direction:	76,6250 gon		
		323 610	1009 340	348 897	
		323 621	1009 361	348 903	
		+ 011	+ 021	+ 006	
		Radial dist.:	0,024 m		
		Direction:	69,2822 gon		
		323 608	1009 342	338 670	
		323 621	1009 361	348 903	
		+ 013	+ 019	10 233	
		Radial dist.:	0,023 m		0,089 m
		Direction:	61,7996 gon		
		Inclination:	0,1431 gon		0,5555 gon

2.5 11. 68. 0119



# KOORDINATFORTECKNING

Datum

17/1 1978

Sid

Punkt bet		Mar-ke-ring	Koordinater				Anmärkingar	
			Xmeter		Ymeter		Tolerance	
Område		Stripa-Full scale nr. 177		Uppdragsnr				
Plankordinaterna beräknade i system		Mine system		Beräknat av: LW				
Höjderna angivna i meter över		Mine system		Kontroll av: LW				
02	Theoret. top	15	322	524	1007	313	338 897	
	Real top		322	529	1007	304	338 785	
	Diff.		+ 005		- 009		- 112	
	Radial dist.:		0.010		m		0.020 m	
	Direction:		332,2229		gon			
	Theor.		322	524	1007	313	338 897	
	Real		322	547	1007	311	343 793	
	Diff		+ 023		- 002		4 896	
	Radial dist.:		0.023		m			
	Direction:		394,4781		gon			
	Theoret. bottom		322	524	1007	313	348 897	
	Real bottom		322	564	1007	325	348 881	
	Diff.		+ 040		+ 012		- 016	
	Radial dist.:		0.042		m			
	Direction:		18,5547		gon			
	Real top		322	529	1007	304	338 785	
	Real bottom		322	564	1007	325	348 881	
	Diff.		+ 035		+ 021		10 096	
	Radial dist.:		0,041		m		0,088 m	
	Direction:		34,4042		gon			
	Inclination:		0,2585		gon		0.5555 gon	



# KOORDINATFORTECKNING

Datum

17/1 1978

Sid.

Punkt bet	Marke-ring	Koordinater			Anmärkningar Tolerance
		Xmeter	Ymeter	Zmeter	
Område <u>Stripa Full scale nr. M8</u> Uppdragsnr. _____					
Plankordinaterna beräknade i system <u>Mine system</u>				Beräknat av: <u>LW</u>	
Höjderna angivna i meter över <u>Mine system</u>				Kontroll av: <u>LW</u>	
02		15	20		
Theoret. top		324 224	1005 146	338 897	
Real top		324 223	1005 145	338 760	
Diff.		- 001	- 001	- 137	
		Radial dist.:	0,001 m		0.020 m
		Direction:	250,0000 gon		
Theor.		324 224	1005 146	338 897	
Real		324 235	1005 161	343 780	
Diff		+ 011	+ 015	4 883	
		Radial dist.:	0,019 m		
		Direction:	59,7180 gon		
Theoret. bottom		324 224	1005 146	348 897	
Real bottom		324 242	1005 178	348 887	
Diff.		+ 018	+ 032	- 010	
		Radial dist.:	0,037 m		
		Direction:	67,3803 gon		
Real top		324 223	1005 145	338 760	
Real bottom		324 242	1005 178	348 887	
Diff.		+ 019	+ 033	10 127	
		Radial dist.:	0,038 m		0,088 m
		Direction:	66,7428 gon		
		Inclination:	0,2389 gon		0,5555 gon



# KOORDINATFORTECKNING

Datum

171, 1978

Sid

Punkt bet		Marke-ring	Koordinater						Anmärkingar
			Xmeter		Ymeter		Zmeter	Tolerance	
Område <u>Stripa- Full scale</u> nr. <u>M9</u> Uppdrag nr. _____									
Plankoordinaterna beräknade i system <u>Mine system</u> Beräknat av: <u>LW</u>									
Höjderna angivna i meter över <u>Mine system</u> Kontroll av: <u>LW</u>									
02	Theoret. top		326	426	1009	044	338	897	medelplan i orten
	Real top		326	422	1009	042	338	765	beräknas verkliga höjd
	Diff.		-004		-002		-132		har 132 mm över flög
			Radial dist.:		0.004	m			0.020 m
			Direction:		229,5167	gon			från Don medels 100:E etc.
	Theor.		326	426	1009	044	338	897	Heor. medelplanet
	Real		326	447	1009	019	343	784	beräknas med djup
	Diff		+021		-025		4	887	djup från medelplanet
			Radial dist.:		0.033	m			
			Direction:		344,4781	gon			
	Theoret. bottom		326	426	1009	044	348	897	
	Real bottom		326	466	1008	995	348	898	
	Diff.		+040		-049		+001		
			Radial dist.:		0.063	m			
			Direction:		343,5841	gon			
	Real top		326	422	1009	042	338	765	
	Real bottom		326	466	1008	995	348	898	
	Diff.		+044		-047		10	133	
			Radial dist.:		0,064	m			0,088 m
			Direction:		347,9020	gon			
			Inclination:		0,4021	gon	hitt vertikallinjen		0.5555 gon

Project: Ultrasonic cross hole  
monitoring  
Coordinates for  
data points

M6

#	X	Y	Z
A	323 608	1009342	338 670
C 1	323 608	1009 342	339 000
C 2	323 609	343	339 250
C 3	609	344	339 500
C 4	609	344	339 750
C 5	610	345	340 000
C 6	610	345	340 250
C 7	610	346	340 500
C 8	611	346	340 750
C 9	611	347	341 000
C 10	611	347	341 250
C 11	612	348	341 500
C 12	612	349	341 750
C 13	612	349	342 000
C 14	613	350	342 250
C 15	613	350	342 500
C 16	614	351	342 750
C 17	614	351	343 000
C 18	614	352	343 250
C 19	615	352	343 500
B	323 615	1009 353	343 679
C 20	323 615	1009 353	343 750
C 21	615	353	344 000
C 22	616	354	344 250
C 23	616	354	344 500
C 24	616	355	344 750
C 25	617	355	345 000
C 26	617	355	345 250
C 27	617	356	345 500
C 28	617	356	345 750
C 29	618	357	346 000
C 30	618	357	346 250
C 31	618	357	346 500
C 32	619	358	346 750
C 33	619	358	347 000
C 34	619	359	347 250
C 35	620	359	347 500
C 36	620	359	347 750
C 37	620	360	348 000
C 38	620	360	348 250
C 39	621	361	348 500
C 40	621	361	348 750
C	323 621	1009 361	348 903

Project: Ultrasonic cross hole  
monitoring  
coordinates for  
data points

M7

#	X	Y	Z
A	322 529	1007 304	338 785
C 41	322 530	1007 304	339 000
C 42	322 531	" 305	339 250
C 43	322 532	" 305	339 500
C 44	322 533	" 306	339 750
C 45	322 533	" 306	340 000
C 46	322 534	" 306	340 250
C 47	322 535	" 307	340 500
C 48	322 536	" 307	340 750
C 49	322 537	" 307	341 000
C 50	322 538	" 307	341 250
C 51	322 539	" 308	341 500
C 52	322 540	" 308	341 750
C 53	4 541	" 309	342 000
C 54	" 541	" 309	342 250
C 55	" 542	" 309	342 500
C 56	" 543	" 310	342 750
C 57	" 544	" 310	343 000
C 58	" 545	" 310	343 250
C 59	" 546	" 311	343 500
C 60	" 547	" 311	343 750
B	322 547	1007 311	343 793
C 61	" 548	" 311	344 000
C 62	" 548	" 312	344 250
C 63	" 549	" 313	344 500
C 64	" 550	" 314	344 750
C 65	" 551	" 314	345 000
C 66	" 552	" 315	345 250
C 67	" 553	" 316	345 500
C 68	" 554	" 316	345 750
C 69	" 554	" 317	346 000
C 70	" 555	" 318	346 250
C 71	" 556	" 318	346 500
C 72	" 557	" 319	346 750
C 73	" 558	" 320	347 000
C 74	" 559	" 320	347 250
C 75	" 559	" 321	347 500
C 76	" 560	" 322	347 750
C 77	" 561	" 323	348 000
C 78	" 562	" 323	348 250
C 79	" 563	" 324	348 500
C 80	" 564	" 325	348 750
C	322 564	1007 325	348 881



Project: Ultra sonic cross hole  
monitoring  
coordinates  
for data points

M 8

#	X	Y	Z
A	324 223	1005 145	338 760
C 8 1	324 224	1005 146	339 000
C 8 2	324 224	1005 147	339 250
C 8 3	324 225	1005 147	339 500
C 8 4	324 225	1005 148	339 750
C 8 5	324 226	1005 149	340 000
C 8 6	324 227	1005 150	340 250
C 8 7	324 227	1005 151	340 500
C 8 8	324 228	1005 151	340 750
C 8 9	324 228	1005 152	341 000
C 9 0	324 229	1005 153	341 250
C 9 1	324 230	1005 154	341 500
C 9 2	324 230	1005 155	341 750
C 9 3	324 231	1005 155	342 000
C 9 4	324 231	1005 156	342 250
C 9 5	324 232	1005 157	342 500
C 9 6	324 233	1005 158	342 750
C 9 7	324 233	1005 159	343 000
C 9 8	324 234	1005 159	343 250
C 9 9	324 234	1005 160	343 500
C 10 0	324 235	1005 161	343 750
B	324 235	1005 161	343 790
C 10 1	324 235	1005 162	344 000
C 10 2	324 236	1005 163	344 250
C 10 3	324 236	1005 164	344 500
C 10 4	324 237	1005 164	344 750
C 10 5	324 237	1005 165	345 000
C 10 6	324 237	1005 166	345 250
C 10 7	324 238	1005 167	345 500
C 10 8	324 238	1005 168	345 750
C 10 9	324 238	1005 169	346 000
C 11 0	324 239	1005 170	346 250
C 11 1	324 239	1005 171	346 500
C 11 2	324 239	1005 171	346 750
C 11 3	324 240	1005 172	347 000
C 11 4	324 240	1005 173	347 250
C 11 5	324 240	1005 174	347 500
C 11 6	324 241	1005 175	347 750
C 11 7	324 241	1005 176	348 000
C 11 8	324 241	1005 177	348 250
C 11 9	324 242	1005 178	348 500
C 12 0	324 242	1005 178	348 750
C	324 242	1005 178	348 887

Project: Ultrasonic Cross hole  
monitoring  
Coordinates for data points

M9

#	X	Y	Z	
A	326.422	1009.042	338.765	A
C 121	326.423	1009.041	339.000	
C 122	326.424	1009.040	339.250	
C 123	326.426	1009.039	339.500	
C 124	326.427	1009.038	339.750	
C 125	326.428	1009.036	340.000	
C 126	326.429	1009.035	340.250	
C 127	326.431	1009.034	340.500	
C 128	326.432	1009.033	340.750	
C 129	326.433	1009.032	341.000	
C 130	326.434	1009.031	341.250	
C 131	326.436	1009.030	341.500	
C 132	326.437	1009.028	341.750	
C 133	326.438	1009.027	342.000	
C 134	326.439	1009.026	342.250	
C 135	" 441	" .085	342.500	
C 136	" 442	" .024	342.750	
C 137	" 443	" .023	343.000	
C 138	" 444	" .021	343.250	
C 139	" 446	" .020	343.500	
C 140	" 447	" .019	343.750	
B	326.447	1009.019	343.784	B
C 141	" 448	" .018	344.000	
C 142	" 449	" .017	344.250	
C 143	" 450	" .016	344.500	
C 144	" 450	" .015	344.750	
C 145	" 451	" .013	345.000	
C 146	" 452	" .012	345.250	
C 147	" 453	" .011	345.500	
C 148	" 454	" .010	345.750	
C 149	" 455	" .009	346.000	
C 150	" 456	" .008	346.250	
C 151	" 457	" .006	346.500	
C 152	" 458	" .005	346.750	
C 153	" 459	" .004	347.000	
C 154	" 460	" .003	347.250	
C 155	" 461	" .002	347.500	
C 156	" 462	" .000	347.750	
C 157	" 463	1008.999	348.000	
C 158	" 464	" .998	348.250	
C 159	" 465	" .997	348.500	
C 160	" 465	" .996	348.750	
C	326.466	1008.995	348.898	C

## Appendix C:1 - Tables for the monitor and reference lines

In this appendix the tabulated data and result from the monitor and reference lines are presented. In the first of the nine columns the Julian heater day is listed. In the second column the recorded time of arrival for the P waves,  $t_p$  are shown. This is not corrected for the instrument delay of  $6.2 \times 10^{-6}$  s which was done before the  $V_p$  was calculated. In the third column the arrival time for the S waves,  $t_s$  are given. The instrument delay for the S waves were  $11.3 \times 10^{-6}$  s which should be subtracted from the arrival times of the S waves before  $V_s$  is calculated. The  $V_p$  and the  $V_s$  are shown in columns 4 and 5 respectively.

Using the expressions in Chapter 7 the Poissons ratio and the dynamic moduli were calculated and they are presented in column 6 through 9.

Day # and mean temperature in line M7-M6					
Day #	Temp	Day #	Temp	Day #	Temp
0	11.3	343	60.8	456	18.0
6	31.8	344	61.0	459	17.4
8	34.8	351	61.0	462	17.3
11	39.3	362	61.0	466	17.1
12	40.0	376	61.7	469	16.6
13	41.8	383	61.8	473	16.3
14	42.8	398	61.8	476	16.0
15	43.8	399	59.0	480	16.1
18	46.0	400	54.6	483	16.1
21	47.2	403	44.5	497	15.1
36	51.8	404	41.4	501	14.6
43	53.2	405	39.0	503	14.7
50	53.9	406	37.1	505	14.7
57	55.0	410	32.5	508	14.4
64	55.7	411	31.1	510	14.2
78	56.7	412	30.4	512	14.1
91	57.3	413	29.7	515	14.1
110	57.8	414	29.2	518	14.1
118	58.6	417	27.4	522	14.1
133	58.8	418	26.9	526	14.1
159	59.0	419	26.0	530	14.1
176	59.2	420	25.9	533	13.7
195	59.7	424	23.9	536	13.6
210	59.9	426	23.6	539	13.6
222	60.0	428	22.8	543	13.5
238	60.0	431	21.9	546	13.5
252	60.0	433	21.6	550	12.8
267	60.0	435	20.9	557	12.7
271	60.0	438	20.3	564	12.6
329	60.9	440	20.1	571	12.6
330	60.9	442	19.8	575	12.3
333	60.9	447	19.1	585	12.3
334	60.9	449	18.6	657	10.0
335	60.9	452	18.3		
337	60.9	454	18.1		

Table C:1.1

Table C:1.1 Mean temperature in monitor line M7-M6 for days when travel times and waveforms were collected.

Day # and mean temperatures in line M8-M9					
Day #	Temp	Day #	Temp	Day #	Temp
0	11.0	343	36.7	456	17.8
6	16.3	344	36.9	459	17.4
8	17.8	351	37.0	462	17.0
11	19.9	362	37.0	466	16.9
12	21.2	376	37.7	469	16.8
13	22.1	383	37.6	473	16.3
14	22.8	398	37.6	476	15.9
15	23.7	399	37.6	480	15.9
18	24.7	400	37.6	483	15.9
21	25.8	403	34.9	497	15.0
36	28.0	404	34.0	501	14.9
43	29.2	405	32.4	503	14.9
50	29.9	406	31.7	505	14.9
57	31.0	410	29.4	508	14.8
64	31.9	411	28.2	510	14.3
78	32.7	412	27.9	512	14.2
91	33.7	413	27.4	515	14.2
110	33.8	414	27.0	518	14.2
118	34.6	417	25.5	522	14.2
133	34.7	418	25.3	526	13.9
159	35.0	419	24.6	530	13.9
176	35.5	420	24.3	533	13.9
195	35.5	424	22.7	536	13.8
210	35.6	426	22.7	539	13.8
222	35.9	428	21.9	543	13.9
238	35.9	431	20.9	546	13.9
252	36.0	433	20.9	550	13.2
267	36.0	435	20.1	557	13.2
271	36.0	438	20.0	564	13.1
329	36.6	440	19.8	571	12.9
330	36.6	442	19.3	575	13.0
333	36.6	447	18.8	585	13.0
334	36.6	449	18.2	657	10.0
335	36.6	452	18.0		
337	36.6	454	17.8		

Table C:1.2

6

Table C:1.2 Mean temperature in monitor line M8-M9 for days when traveltimes and waveforms were collected.

Day #'s and mean temperatures in line M8-M6					
Day #	Temp	Day #	Temp	Day #	Temp
0	11.2	343	65.0	456	18.0
6	35.9	344	65.3	459	17.3
8	39.0	351	65.3	462	17.2
11	43.2	362	65.3	466	17.0
12	44.7	376	65.7	469	16.5
13	45.8	383	65.9	473	16.2
14	46.8	398	66.0	476	16.0
15	47.9	399	60.0	480	16.0
18	49.9	400	54.9	483	16.0
21	51.0	403	44.7	497	15.0
36	54.5	404	41.4	501	14.6
43	55.9	405	38.8	503	14.6
50	57.5	406	36.9	505	14.6
57	58.6	410	32.6	508	14.3
64	59.2	411	31.1	510	14.1
78	60.5	412	30.3	512	14.0
91	61.3	413	29.8	515	14.0
110	61.9	414	29.2	518	14.0
118	62.6	417	27.2	522	14.0
133	62.9	418	26.8	526	14.0
159	63.2	419	26.0	530	14.0
176	63.4	420	25.8	533	13.7
195	63.8	424	23.8	536	13.5
210	63.9	426	23.5	539	13.5
222	64.2	428	22.7	543	13.4
238	64.2	431	21.8	546	13.4
252	64.2	433	21.5	550	12.6
267	64.2	435	20.8	557	12.7
271	64.2	438	20.2	564	12.5
329	65.0	440	20.0	571	12.5
330	65.0	442	19.8	575	12.3
333	65.0	447	19.0	585	12.3
334	65.0	449	18.4	657	10.0
335	65.0	452	18.2		
337	65.0	454	18.0		

Table C:1.3

Table C:1.3 Mean temperature in monitor line M8-M6 for days when velocity and waveforms were collected.

Day #'s and mean temperatures in line M7-M9					
Day #	Temp	Day #	Temp	Day #	Temp
0	11.0	343	62.3	456	17.8
6	35.4	344	62.4	459	17.3
8	38.2	351	62.6	462	17.0
11	41.9	362	62.6	466	16.9
12	43.0	376	62.9	469	16.4
13	44.1	383	63.1	473	16.2
14	44.8	398	63.1	476	16.0
15	45.8	399	54.8	480	15.9
18	47.5	400	49.7	483	15.9
21	48.7	403	40.8	497	15.0
36	52.1	404	38.3	501	14.6
43	53.8	405	36.2	503	14.5
50	55.0	406	34.8	505	14.5
57	56.2	410	30.9	508	14.4
64	56.7	411	29.8	510	14.2
78	57.8	412	29.2	512	14.2
91	58.6	413	28.7	515	14.1
110	59.3	414	28.0	518	14.1
118	59.9	417	26.4	522	14.1
133	60.2	418	25.9	526	13.9
159	60.4	419	25.3	530	13.9
176	60.5	420	24.9	533	13.7
195	60.9	424	23.2	536	13.4
210	61.0	426	22.9	539	13.4
222	61.3	428	22.4	543	13.4
238	61.3	431	21.4	546	13.4
252	61.4	433	21.2	550	12.8
261	61.4	435	20.6	557	12.8
271	61.4	438	19.9	564	12.5
329	62.2	440	19.8	571	12.3
330	62.2	442	19.7	575	12.2
333	62.2	447	18.8	585	12.2
334	62.2	449	18.2	657	10.0
335	62.2	452	18.0		
337	62.2	454	17.8		

Table C:1.4

Table C:1.4 Mean temperature in monitor line M7-M9 for days when traveltimes and waveforms were collected.

PROCESS DATE 19 JAN, 1981

LINE AND FILE NAME:

MON76

DAY	P-TIME (SEC)	S-TIME (SEC)	P-VELOCITY (M/SEC)	S-VELOCITY (M/SEC)	POISS.RATIO	YOUNGS MOD (PA)	BULK MOD (PA)	SHEAR MOD (PA)
-44	4.01600E-04	6.81800E-04	5686.57	3353.42	.233414	7.27497E+10	4.54824E+10	2.94912E+10
21	3.92600E-04	6.71400E-04	5819.02	3406.26	.239366	7.54223E+10	4.82301E+10	3.04278E+10
36	3.90000E-04	6.60500E-04	5858.44	3463.45	.231355	7.74722E+10	4.80636E+10	3.14581E+10
43	3.90300E-04	6.61100E-04	5853.87	3460.25	.231473	7.73366E+10	4.80004E+10	3.14000E+10
50	3.92800E-04	6.60000E-04	5816.01	3466.12	.224602	7.71662E+10	4.66998E+10	3.15066E+10
57	3.93900E-04	6.59200E-04	5799.51	3470.4	.221091	7.71350E+10	4.60933E+10	3.15845E+10
64	3.92900E-04	6.60600E-04	5814.51	3462.91	.22517	7.70593E+10	4.67315E+10	3.14484E+10
78	3.90500E-04	6.60500E-04	5850.82	3463.45	.230277	7.74044E+10	4.78295E+10	3.14581E+10
91	3.88800E-04	6.60500E-04	5876.82	3463.45	.233925	7.76339E+10	4.86291E+10	3.14581E+10
110	3.89200E-04	6.60200E-04	5870.68	3465.05	.232692	7.76281E+10	4.84012E+10	3.14872E+10
133	3.89300E-04	6.60500E-04	5869.15	3463.45	.232857	7.75667E+10	4.83928E+10	3.14581E+10
159	3.87000E-04	6.53000E-04	5904.6	3503.93	.228214	7.90915E+10	4.85012E+10	3.21978E+10
176	3.87200E-04	6.50200E-04	5901.5	3519.28	.224062	7.95165E+10	4.80281E+10	3.24806E+10
195	3.87600E-04	6.51800E-04	5895.31	3510.49	.225302	7.91999E+10	4.80527E+10	3.23185E+10
210	3.87300E-04	6.52500E-04	5899.95	3506.66	.226895	7.91298E+10	4.82903E+10	3.22480E+10
222	3.86500E-04	6.59500E-04	5912.36	3468.79	.237551	7.81024E+10	4.95984E+10	3.15553E+10
238	3.86100E-04	6.56600E-04	5918.58	3484.38	.234784	7.86299E+10	4.94125E+10	3.18395E+10
252	3.86400E-04	6.54500E-04	5913.91	3495.76	.23147	7.89317E+10	4.89900E+10	3.20477E+10
267	3.88100E-04	6.59400E-04	5887.59	3469.33	.234035	7.79046E+10	4.88189E+10	3.15650E+10
329	3.88100E-04	6.63700E-04	5887.59	3446.46	.239351	7.72122E+10	4.93719E+10	3.11503E+10
330	3.89300E-04	6.62000E-04	5869.15	3455.46	.23474	7.73274E+10	4.85859E+10	3.13132E+10
333	3.87100E-04	6.61000E-04	5903.05	3460.78	.238138	7.77791E+10	4.95039E+10	3.14097E+10
334	3.89000E-04	6.59200E-04	5873.75	3470.4	.231854	7.78149E+10	4.83660E+10	3.15845E+10
335	3.89400E-04	6.58600E-04	5867.61	3473.61	.230223	7.78561E+10	4.80990E+10	3.16431E+10
337	3.90000E-04	6.57300E-04	5858.44	3480.6	.227231	7.79796E+10	4.76470E+10	3.17705E+10
344	3.90200E-04	6.69300E-04	5855.39	3417.13	.241765	7.60515E+10	4.90842E+10	3.06223E+10
351	3.89700E-04	6.72500E-04	5863.02	3400.59	.246526	7.56058E+10	4.97131E+10	3.03266E+10
362	3.87600E-04	6.64200E-04	5895.31	3443.82	.240991	7.71960E+10	4.96739E+10	3.11026E+10
376	3.89800E-04	6.72100E-04	5861.5	3402.65	.245863	7.56572E+10	4.96171E+10	3.03633E+10
383	3.89100E-04	6.69900E-04	5872.21	3414.01	.244704	7.60926E+10	4.96760E+10	3.05665E+10
398	3.90400E-04	6.65800E-04	5852.34	3435.4	.237125	7.65798E+10	4.85528E+10	3.09507E+10
399	3.90300E-04	6.64200E-04	5853.87	3443.82	.235363	7.68459E+10	4.83971E+10	3.11026E+10
400	3.90900E-04	6.79300E-04	5844.74	3365.97	.251879	7.43925E+10	4.99706E+10	2.97123E+10
403	3.93500E-04	6.80700E-04	5805.5	3358.93	.2484	7.38758E+10	4.89374E+10	2.95882E+10
404	3.94900E-04	6.86400E-04	5784.59	3330.57	.252049	7.28458E+10	4.89652E+10	2.90907E+10
405	3.95300E-04	6.83300E-04	5778.64	3345.04	.247824	7.32714E+10	4.84262E+10	2.93597E+10
406	3.93600E-04	6.85900E-04	5804	3333.04	.253974	7.30661E+10	4.94976E+10	2.91338E+10
410	3.97000E-04	6.82900E-04	5753.51	3347.93	.244027	7.31355E+10	4.76193E+10	2.93947E+10
411	3.96500E-04	6.84100E-04	5760.88	3341.96	.246385	7.30130E+10	4.79815E+10	2.92899E+10
412	3.97600E-04	6.82600E-04	5744.69	3349.43	.242488	7.31103E+10	4.73183E+10	2.94209E+10
413	3.95900E-04	6.86800E-04	5769.75	3328.6	.250576	7.26740E+10	4.85613E+10	2.90562E+10
414	3.96000E-04	6.88700E-04	5768.27	3319.27	.252475	7.23767E+10	4.87336E+10	2.88935E+10
417	3.97000E-04	6.86000E-04	5753.51	3332.56	.247559	7.26707E+10	4.79786E+10	2.91252E+10
418	3.97400E-04	6.93100E-04	5747.62	3297.84	.254601	7.15668E+10	4.86057E+10	2.85217E+10
419	3.96400E-04	6.90700E-04	5762.35	3309.49	.253892	7.20326E+10	4.87812E+10	2.87236E+10
420	3.98100E-04	6.90700E-04	5737.36	3309.49	.250672	7.18475E+10	4.80274E+10	2.87236E+10
424	3.97800E-04	6.89300E-04	5741.75	3316.33	.2497	7.20885E+10	4.80014E+10	2.88423E+10
426	3.98300E-04	6.91600E-04	5734.43	3305.12	.251279	7.16923E+10	4.80406E+10	2.86476E+10
429	3.98800E-04	6.92000E-04	5727.13	3303.17	.250767	7.15788E+10	4.78660E+10	2.86140E+10
431	3.98800E-04	6.93000E-04	5727.13	3298.33	.25186	7.14314E+10	4.79778E+10	2.85301E+10
433	3.98200E-04	6.87900E-04	5735.89	3323.19	.247366	7.22519E+10	4.76657E+10	2.89618E+10
435	3.98000E-04	6.93300E-04	5738.82	3296.88	.253692	7.14730E+10	4.83620E+10	2.85050E+10
438	3.98600E-04	6.93300E-04	5730.05	3296.88	.252564	7.14086E+10	4.80990E+10	2.85050E+10
440	3.98200E-04	6.93500E-04	5735.89	3295.91	.253532	7.14220E+10	4.82971E+10	2.84883E+10
442	3.98100E-04	6.93100E-04	5737.36	3297.84	.253289	7.14919E+10	4.82966E+10	2.85217E+10
447	3.98100E-04	6.89600E-04	5737.36	3314.86	.249457	7.20107E+10	4.79031E+10	2.88168E+10
449	3.98000E-04	6.92200E-04	5738.82	3302.2	.252501	7.16360E+10	4.82400E+10	2.85972E+10
452	3.98100E-04	6.92200E-04	5737.36	3302.2	.252313	7.16252E+10	4.81960E+10	2.85972E+10



454	3.98000E-04	6.92600E-04	5738.82	3300.26	.252936	7.15767E+10	4.82848E+10	2.85636E+10
456	3.98100E-04	6.92600E-04	5737.36	3300.26	.252747	7.15659E+10	4.82407E+10	2.85636E+10
459	3.97500E-04	6.92500E-04	5746.15	3300.75	.253768	7.16453E+10	4.84945E+10	2.85720E+10
462	3.97500E-04	6.91900E-04	5746.15	3303.66	.253119	7.17345E+10	4.84273E+10	2.86224E+10
466	3.97300E-04	6.92100E-04	5749.09	3302.69	.253712	7.17263E+10	4.85383E+10	2.86056E+10
469	3.97700E-04	6.92100E-04	5743.22	3302.69	.252959	7.16832E+10	4.83612E+10	2.86056E+10
473	3.98100E-04	6.92100E-04	5737.36	3302.69	.252204	7.16400E+10	4.81847E+10	2.86056E+10
476	3.97800E-04	6.92200E-04	5741.75	3302.2	.252879	7.16576E+10	4.83283E+10	2.85972E+10
480	3.97700E-04	6.92500E-04	5743.22	3300.75	.253392	7.16238E+10	4.84060E+10	2.85720E+10
483	3.98000E-04	6.92100E-04	5738.82	3302.69	.252393	7.16508E+10	4.82288E+10	2.86056E+10
497	3.96800E-04	6.92100E-04	5756.45	3302.69	.25465	7.17800E+10	4.87603E+10	2.86056E+10
501	3.96700E-04	6.92500E-04	5757.93	3300.75	.255266	7.17309E+10	4.88496E+10	2.85720E+10
503	3.96600E-04	6.92300E-04	5759.4	3301.72	.255239	7.17715E+10	4.88718E+10	2.85888E+10
505	3.96600E-04	6.92200E-04	5759.4	3302.2	.255132	7.17864E+10	4.88606E+10	2.85972E+10
508	3.97500E-04	6.92600E-04	5746.15	3300.26	.253876	7.16304E+10	4.85056E+10	2.85636E+10
510	3.97700E-04	6.92500E-04	5743.22	3300.75	.253392	7.16238E+10	4.84060E+10	2.85720E+10
512	3.96900E-04	6.92400E-04	5754.98	3301.23	.254785	7.17245E+10	4.87494E+10	2.85804E+10
515	3.97200E-04	6.92300E-04	5750.56	3301.72	.254116	7.17072E+10	4.86050E+10	2.85888E+10
518	3.96800E-04	6.92500E-04	5756.45	3300.75	.255079	7.17202E+10	4.88051E+10	2.85720E+10
522	3.96900E-04	6.92600E-04	5754.98	3300.26	.255	7.16946E+10	4.87718E+10	2.85636E+10
526	3.96500E-04	6.92100E-04	5760.88	3302.69	.255211	7.18121E+10	4.88940E+10	2.86056E+10
530	3.97500E-04	6.92500E-04	5746.15	3300.75	.253768	7.16453E+10	4.84945E+10	2.85720E+10
533	3.97500E-04	6.92400E-04	5746.15	3301.23	.25366	7.16602E+10	4.84833E+10	2.85804E+10
536	3.97600E-04	6.92800E-04	5744.69	3299.3	.253904	7.15900E+10	4.84837E+10	2.85468E+10
539	3.97400E-04	6.92700E-04	5747.62	3299.78	.254171	7.16263E+10	4.85611E+10	2.85552E+10
543	3.96600E-04	6.92900E-04	5759.4	3298.81	.25588	7.16818E+10	4.89389E+10	2.85385E+10
546	3.96800E-04	6.92800E-04	5756.45	3299.3	.2554	7.16754E+10	4.88386E+10	2.85468E+10
550	3.97000E-04	6.92600E-04	5753.51	3300.26	.254813	7.16839E+10	4.87274E+10	2.85636E+10
557	3.96900E-04	6.92500E-04	5754.98	3300.75	.254893	7.17096E+10	4.87606E+10	2.85720E+10
564	3.97400E-04	6.92600E-04	5747.62	3300.26	.254064	7.16412E+10	4.85499E+10	2.85636E+10
571	3.97100E-04	6.85000E-04	5752.03	3337.49	.246233	7.28091E+10	4.78188E+10	2.92117E+10
575	3.97000E-04	6.94800E-04	5753.51	3289.64	.257154	7.13561E+10	4.89721E+10	2.83800E+10
585	3.97200E-04	6.89100E-04	5750.56	3317.31	.250628	7.21846E+10	4.82442E+10	2.88594E+10
701	3.94300E-04	6.84600E-04	5793.53	3339.48	.251212	7.31869E+10	4.90291E+10	2.92464E+10

LENGTH OF LINE M7-M6 IS 2.24847 METER.

DENSITY USED IS 2622.5 KG/M<sup>3</sup>

Table C:1.5 day #,  $t_p$ ,  $t_p$ ,  $V_p$ ,  $V_s$ ,  $\nu$ ,  $E_d$ ,  $K_d$ , and  $G_d$  for monitor line

M7-M6

PROCESS DATE :19 JAN,1981

LINE AND FILE NAME:

MON89

DAY	P-TIME (SEC)	S-TIME (SEC)	P-VELOCITY (M/SEC)	S-VELOCITY (M/SEC)	POISS.RATIO	YOUNGS MOD (PA)	BULK MOD (PA)	SHEAR MOD (PA)
-42	7.55300E-04	1.27140E-03	5867.52	3488.1	.226721	7.82835E+10	4.77434E+10	3.19076E+10
21	7.51200E-04	1.27020E-03	5899.81	3491.43	.230519	7.86756E+10	4.86588E+10	3.19685E+10
36	7.46900E-04	1.26580E-03	5934.06	3503.67	.232407	7.93501E+10	4.94222E+10	3.21931E+10
43	7.48800E-04	1.26450E-03	5918.88	3507.31	.229428	7.93226E+10	4.88611E+10	3.22599E+10
50	7.47500E-04	1.26400E-03	5929.26	3508.71	.230554	7.94586E+10	4.91493E+10	3.22857E+10
57	7.48100E-04	1.26390E-03	5924.46	3508.99	.229815	7.94236E+10	4.89934E+10	3.22909E+10
64	7.48200E-04	1.26310E-03	5923.67	3511.23	.22917	7.94834E+10	4.89135E+10	3.23321E+10
78	7.44800E-04	1.26270E-03	5950.93	3512.35	.232707	7.97631E+10	4.97351E+10	3.23528E+10
91	7.46100E-04	1.26050E-03	5940.48	3518.54	.2298	7.98555E+10	4.92570E+10	3.24669E+10
110	7.44700E-04	1.25900E-03	5951.74	3522.77	.230375	8.00851E+10	4.95041E+10	3.25450E+10
159	7.45400E-04	1.25710E-03	5946.1	3528.14	.228313	8.01949E+10	4.91957E+10	3.26443E+10
176	7.46300E-04	1.25610E-03	5938.87	3530.98	.226612	8.02126E+10	4.89004E+10	3.26968E+10
195	7.45200E-04	1.25630E-03	5947.71	3530.41	.228001	8.02776E+10	4.91900E+10	3.26863E+10
210	7.45800E-04	1.26360E-03	5942.89	3509.83	.232186	7.96148E+10	4.95461E+10	3.23063E+10
222	7.46200E-04	1.26840E-03	5939.68	3496.43	.23487	7.91801E+10	4.97743E+10	3.20601E+10
238	7.44300E-04	1.25860E-03	5954.97	3523.9	.230559	8.01484E+10	4.95769E+10	3.25659E+10
252	7.45400E-04	1.25640E-03	5946.1	3530.13	.227842	8.02543E+10	4.91468E+10	3.26810E+10
267	7.43100E-04	1.25530E-03	5964.66	3533.25	.229709	8.05186E+10	4.96494E+10	3.27389E+10
271	7.45000E-04	1.25540E-03	5949.32	3532.96	.227621	8.03689E+10	4.91771E+10	3.27336E+10
329	7.45100E-04	1.25400E-03	5948.52	3536.94	.226557	8.04803E+10	4.90536E+10	3.28074E+10
330	7.45600E-04	1.25800E-03	5944.5	3525.6	.228692	8.01038E+10	4.92084E+10	3.25972E+10
333	7.46400E-04	1.26100E-03	5938.07	3517.13	.229795	7.97913E+10	4.92166E+10	3.24409E+10
334	7.46400E-04	1.25960E-03	5938.07	3521.08	.22886	7.99096E+10	4.91196E+10	3.25137E+10
335	7.46700E-04	1.26170E-03	5935.67	3515.16	.229924	7.97104E+10	4.91901E+10	3.24046E+10
337	7.46800E-04	1.25720E-03	5934.86	3527.86	.226788	8.00825E+10	4.88525E+10	3.26391E+10
343	7.46400E-04	1.25770E-03	5938.07	3526.44	.227582	8.00701E+10	4.89873E+10	3.26129E+10
344	7.47800E-04	1.26150E-03	5926.86	3515.73	.228551	7.96469E+10	4.89024E+10	3.24150E+10
351	7.47600E-04	1.26710E-03	5928.46	3500.05	.232482	7.91907E+10	4.93367E+10	3.21265E+10
362	7.48000E-04	1.26600E-03	5925.26	3503.12	.231316	7.92545E+10	4.91622E+10	3.21829E+10
376	7.46600E-04	1.26620E-03	5936.47	3502.56	.233001	7.93377E+10	4.95244E+10	3.21726E+10
383	7.47700E-04	1.26790E-03	5927.66	3497.82	.232894	7.91163E+10	4.93664E+10	3.20856E+10
398	7.46900E-04	1.26830E-03	5934.06	3496.71	.234036	7.91392E+10	4.95928E+10	3.20652E+10
399	7.46100E-04	1.27440E-03	5940.48	3479.82	.238003	7.86794E+10	5.02045E+10	3.17562E+10
400	7.46200E-04	1.27530E-03	5939.68	3477.34	.239262	7.85965E+10	5.02398E+10	3.17110E+10
403	7.47200E-04	1.26820E-03	5931.66	3496.98	.233641	7.91265E+10	4.95112E+10	3.20703E+10
404	7.47900E-04	1.26870E-03	5926.06	3495.59	.233194	7.90349E+10	4.93711E+10	3.20448E+10
405	7.48000E-04	1.27230E-03	5925.26	3485.61	.235411	7.87255E+10	4.95899E+10	3.18621E+10
406	7.49000E-04	1.27260E-03	5917.29	3485.06	.234447	7.86391E+10	4.93556E+10	3.18520E+10
410	7.50500E-04	1.27880E-03	5905.36	3467.74	.236844	7.80105E+10	4.94070E+10	3.15361E+10
411	7.50500E-04	1.28100E-03	5905.36	3461.73	.238232	7.78277E+10	4.95526E+10	3.14269E+10
412	7.50700E-04	1.28180E-03	5903.77	3459.55	.23852	7.77478E+10	4.95562E+10	3.13874E+10
413	7.51200E-04	1.28290E-03	5899.81	3456.56	.238674	7.76230E+10	4.95059E+10	3.13331E+10
414	7.51400E-04	1.28280E-03	5898.23	3456.83	.238398	7.76179E+10	4.94504E+10	3.13380E+10
417	7.52500E-04	1.27780E-03	5889.53	3470.48	.234034	7.79563E+10	4.88510E+10	3.15860E+10
418	7.53900E-04	1.27800E-03	5878.51	3469.93	.232631	7.78430E+10	4.85240E+10	3.15760E+10
419	7.53000E-04	1.27850E-03	5885.59	3468.56	.233939	7.78641E+10	4.87758E+10	3.15511E+10
420	7.53300E-04	1.27700E-03	5883.23	3470.2	.233224	7.78928E+10	4.86630E+10	3.15810E+10
425	7.53700E-04	1.27160E-03	5880.08	3487.55	.228654	7.83819E+10	4.81439E+10	3.18975E+10
426	7.56100E-04	1.27540E-03	5861.26	3477.07	.22849	7.79010E+10	4.78197E+10	3.17060E+10
428	7.56400E-04	1.27700E-03	5858.92	3472.67	.229214	7.77500E+10	4.78545E+10	3.16259E+10
431	7.50700E-04	1.27820E-03	5856.58	3469.38	.229671	7.76316E+10	4.78624E+10	3.15660E+10
433	7.57100E-04	1.27770E-03	5853.46	3470.75	.228897	7.76440E+10	4.77333E+10	3.15909E+10
435	7.57200E-04	1.27740E-03	5852.68	3471.57	.228587	7.76612E+10	4.76894E+10	3.16059E+10
438	7.57500E-04	1.27820E-03	5850.34	3469.38	.228781	7.75754E+10	4.76709E+10	3.15609E+10
440	7.57000E-04	1.27740E-03	5854.24	3471.57	.22881	7.76753E+10	4.77373E+10	3.16059E+10
442	7.57500E-04	1.28000E-03	5850.34	3464.46	.229966	7.74300E+10	4.77902E+10	3.14795E+10
447	7.58300E-04	1.28000E-03	5844.12	3462.28	.229604	7.73098E+10	4.76523E+10	3.14368E+10
449	7.58100E-04	1.28650E-03	5845.67	3465.28	.229103	7.74123E+10	4.76272E+10	3.14014E+10

452	7.58000E-04	1.28760E-03	5846.45	3462.28	.229937	7.73306E+10	4.77238E+10	3.14368E+10
454	7.58400E-04	1.28860E-03	5843.34	3459.55	.230149	7.72223E+10	4.76944E+10	3.13874E+10
456	7.58600E-04	1.28750E-03	5841.79	3462.55	.229206	7.72969E+10	4.75743E+10	3.14418E+10
459	7.59300E-04	1.28740E-03	5836.36	3462.82	.228362	7.72560E+10	4.74913E+10	3.14468E+10
462	7.59000E-04	1.28750E-03	5838.68	3462.55	.228762	7.72690E+10	4.74792E+10	3.14418E+10
466	7.59400E-04	1.28970E-03	5835.58	3456.56	.229764	7.70646E+10	4.75291E+10	3.13331E+10
469	7.59200E-04	1.28980E-03	5837.13	3456.29	.230005	7.70704E+10	4.75832E+10	3.13282E+10
473	7.59500E-04	1.28930E-03	5834.81	3457.65	.229391	7.70897E+10	4.74792E+10	3.13528E+10
476	7.60000E-04	1.29080E-03	5830.94	3453.57	.229821	7.69350E+10	4.74592E+10	3.12790E+10
480	7.61500E-04	1.29130E-03	5836.36	3452.22	.230918	7.69432E+10	4.76578E+10	3.12544E+10
483	7.64200E-04	1.29120E-03	5815.51	3452.49	.227867	7.67646E+10	4.70142E+10	3.12593E+10
497	7.65000E-04	1.29270E-03	5809.36	3448.42	.227968	7.65903E+10	4.69248E+10	3.11858E+10
501	7.65000E-04	1.29210E-03	5809.36	3450.05	.227572	7.66377E+10	4.68856E+10	3.12152E+10
503	7.65000E-04	1.29250E-03	5809.36	3448.96	.227836	7.66061E+10	4.69117E+10	3.11956E+10
505	7.64600E-04	1.29240E-03	5812.43	3449.24	.228214	7.66417E+10	4.69988E+10	3.12005E+10
508	7.64400E-04	1.29310E-03	5813.97	3447.34	.228896	7.66000E+10	4.70914E+10	3.11662E+10
510	7.64200E-04	1.29400E-03	5815.51	3444.91	.229705	7.65424E+10	4.71969E+10	3.11223E+10
512	7.63800E-04	1.29330E-03	5818.59	3446.8	.229689	7.66255E+10	4.72453E+10	3.11564E+10
515	7.64200E-04	1.29380E-03	5815.51	3445.45	.229575	7.65583E+10	4.71839E+10	3.11320E+10
518	7.64300E-04	1.29380E-03	5814.74	3445.45	.229465	7.65514E+10	4.71604E+10	3.11320E+10
522	7.64100E-04	1.29400E-03	5816.28	3444.91	.229816	7.65493E+10	4.72204E+10	3.11223E+10
526	7.63900E-04	1.29370E-03	5817.82	3445.72	.22984	7.65868E+10	4.72478E+10	3.11369E+10
530	7.64200E-04	1.29370E-03	5815.51	3445.72	.229509	7.65662E+10	4.71774E+10	3.11369E+10
533	7.64500E-04	1.29370E-03	5813.2	3445.72	.229178	7.65456E+10	4.71070E+10	3.11369E+10
536	7.64100E-04	1.29450E-03	5816.28	3443.56	.230141	7.65096E+10	4.72529E+10	3.10979E+10
539	7.63900E-04	1.29440E-03	5817.82	3443.83	.230296	7.65312E+10	4.72934E+10	3.11028E+10
543	7.63800E-04	1.29240E-03	5818.59	3449.24	.2291	7.66970E+10	4.71866E+10	3.12005E+10
546	7.63900E-04	1.29340E-03	5817.82	3446.53	.229644	7.66106E+10	4.72283E+10	3.11515E+10
550	7.63600E-04	1.29390E-03	5820.13	3445.18	.230301	7.65915E+10	4.73314E+10	3.11271E+10
557	7.64000E-04	1.29380E-03	5817.05	3445.45	.229795	7.65720E+10	4.72308E+10	3.11320E+10
564	7.62300E-04	1.29510E-03	5830.16	3441.94	.2325	7.65842E+10	4.77160E+10	3.10687E+10
571	7.64700E-04	1.29170E-03	5811.66	3451.13	.227641	7.66902E+10	4.69297E+10	3.12348E+10
575	7.64000E-04	1.29080E-03	5817.05	3453.57	.227826	7.68102E+10	4.70349E+10	3.12700E+10
585	7.63600E-04	1.29100E-03	5820.13	3453.03	.228402	7.68221E+10	4.71421E+10	3.12691E+10
711	7.56900E-04	1.27740E-03	5855.02	3471.57	.228921	7.76823E+10	4.77612E+10	3.16050E+10

LENGTH OF LINE M8-M9 IS 4.39536 METER.

DENSITY USED IS 2622.5 KG/M<sup>3</sup>

Table C:1.6 day #,  $t_p$ ,  $t_s$ ,  $V_p$ ,  $V_s$ ,  $\nu$ ,  $E_d$ ,  $K_d$ , and  $G_d$  for monitor line

M8-M9

PROCESS DATE :19 JAN,1981

LINE AND FILE NAME:

MOMBG

DAY	P-TIME (SEC)	S-TIME (SEC)	P-VELOCITY (M/SEC)	S-VELOCITY (M/SEC)	POISS.RATIO	YOUNGS MOD (PA)	BULK MOD (PA)	SHEAR MOD (PA)
-7	7.11300E-04	1.25060E-03	5930.31	3349.72	.265728	7.44910E+10	5.29947E+10	2.94261E+10
6	7.07800E-04	1.23640E-03	5959.89	3413.16	.255984	7.67436E+10	5.24171E+10	3.85512E+10
15	7.07400E-04	1.22240E-03	5963.29	3452.61	.247877	7.80213E+10	5.15762E+10	3.12616E+10
18	7.04800E-04	1.22020E-03	5985.48	3458.9	.24931	7.83954E+10	5.21198E+10	3.13755E+10
21	7.03700E-04	1.20700E-03	5994.92	3497.08	.242096	7.96731E+10	5.14876E+10	3.20721E+10
36	7.02000E-04	1.20000E-03	6009.57	3517.67	.239394	8.04389E+10	5.14436E+10	3.24509E+10
43	7.03200E-04	1.19600E-03	5999.23	3529.55	.235313	8.07164E+10	5.08251E+10	3.26704E+10
50	7.03400E-04	1.21370E-03	5997.5	3477.6	.246744	7.90826E+10	5.20439E+10	3.17156E+10
57	7.03800E-04	1.19300E-03	5994.06	3538.51	.232544	8.09449E+10	5.04413E+10	3.28365E+10
64	7.03700E-04	1.19330E-03	5994.92	3537.61	.23287	8.09252E+10	5.04906E+10	3.28198E+10
78	7.01700E-04	1.19220E-03	6012.16	3540.91	.234454	8.11802E+10	5.09518E+10	3.28810E+10
91	7.02200E-04	1.19160E-03	6007.84	3542.71	.233454	8.11969E+10	5.07711E+10	3.29144E+10
110	7.01500E-04	1.19050E-03	6013.89	3546.01	.233515	8.13525E+10	5.08799E+10	3.29759E+10
118	7.01200E-04	1.19100E-03	6016.49	3544.51	.234212	8.13295E+10	5.09991E+10	3.29479E+10
133	6.99800E-04	1.18330E-03	6028.63	3567.8	.230488	8.21530E+10	5.08035E+10	3.33823E+10
159	6.99800E-04	1.18970E-03	6028.63	3548.42	.234955	8.15581E+10	5.12857E+10	3.30207E+10
176	6.99600E-04	1.18900E-03	6030.37	3550.53	.234707	8.16386E+10	5.12883E+10	3.30599E+10
185	7.00200E-04	1.18960E-03	6025.16	3548.72	.234418	8.15364E+10	5.11684E+10	3.30263E+10
210	6.99400E-04	1.19110E-03	6032.11	3544.21	.236381	8.14586E+10	5.15001E+10	3.29423E+10
222	6.99800E-04	1.19210E-03	6028.63	3541.21	.236598	8.13350E+10	5.14645E+10	3.28866E+10
238	6.99100E-04	1.19140E-03	6034.72	3543.31	.236933	8.14535E+10	5.16051E+10	3.29256E+10
252	7.00300E-04	1.19420E-03	6024.29	3534.92	.237446	8.11020E+10	5.14828E+10	3.27699E+10
267	7.00100E-04	1.19410E-03	6026.03	3535.22	.237609	8.11264E+10	5.15302E+10	3.27754E+10
320	6.99300E-04	1.19040E-03	6032.98	3546.31	.236019	8.15314E+10	5.14755E+10	3.29815E+10
330	7.00200E-04	1.18970E-03	6025.16	3548.42	.234487	8.15272E+10	5.11758E+10	3.30207E+10
333	7.00200E-04	1.19110E-03	6025.16	3544.21	.23545	8.13972E+10	5.12803E+10	3.29423E+10
334	7.00200E-04	1.19020E-03	6025.16	3546.92	.234831	8.14808E+10	5.12132E+10	3.29927E+10
335	6.99700E-04	1.18970E-03	6029.5	3548.42	.235072	8.15658E+10	5.13132E+10	3.30207E+10
337	7.00600E-04	1.18950E-03	6021.69	3549.02	.233879	8.15147E+10	5.10512E+10	3.30319E+10
341	7.00900E-04	1.19310E-03	6019.09	3538.21	.236004	8.11583E+10	5.12370E+10	3.28309E+10
342	7.00400E-04	1.19270E-03	6023.42	3539.41	.236311	8.12335E+10	5.13443E+10	3.28532E+10
398	7.00500E-04	1.19320E-03	6022.55	3537.91	.236536	8.11795E+10	5.13539E+10	3.28254E+10
399	7.00700E-04	1.19450E-03	6020.82	3534.03	.237188	8.10439E+10	5.13953E+10	3.27533E+10
400	7.01100E-04	1.19430E-03	6017.36	3534.62	.236589	8.10321E+10	5.12711E+10	3.27644E+10
403	7.03300E-04	1.19970E-03	5988.36	3518.56	.237707	8.03700E+10	5.10688E+10	3.24673E+10
404	7.04500E-04	1.20630E-03	5988.06	3499.13	.240737	7.96792E+10	5.12217E+10	3.21096E+10
405	7.04900E-04	1.20920E-03	5984.63	3490.66	.242189	7.93867E+10	5.13211E+10	3.19544E+10
406	7.05200E-04	1.20220E-03	5982.06	3511.18	.23721	8.00008E+10	5.07381E+10	3.23311E+10
410	7.07800E-04	1.20730E-03	5959.89	3496.2	.237659	7.93487E+10	5.04107E+10	3.20560E+10
411	7.07600E-04	1.20090E-03	5961.59	3515.01	.233552	7.99387E+10	5.00027E+10	3.24018E+10
412	7.08100E-04	1.20280E-03	5957.34	3509.41	.234272	7.97305E+10	5.00076E+10	3.22986E+10
413	7.08400E-04	1.20090E-03	5954.8	3515.01	.232619	7.98782E+10	4.97906E+10	3.24018E+10
414	7.08800E-04	1.20150E-03	5951.41	3513.24	.232565	7.97942E+10	4.97281E+10	3.23692E+10
417	7.09400E-04	1.20110E-03	5946.33	3514.42	.231586	7.97844E+10	4.95407E+10	3.23909E+10
418	7.09600E-04	1.20000E-03	5944.64	3517.67	.230586	7.98672E+10	4.94080E+10	3.24509E+10
419	7.10000E-04	1.19960E-03	5941.26	3518.86	.229834	7.98722E+10	4.92735E+10	3.24728E+10
420	7.10300E-04	1.19860E-03	5938.73	3521.82	.228776	7.99380E+10	4.91217E+10	3.25275E+10
424	7.12000E-04	1.19970E-03	5924.43	3518.56	.227629	7.97091E+10	4.87569E+10	3.24673E+10
426	7.11700E-04	1.20210E-03	5926.95	3511.47	.229575	7.95204E+10	4.90096E+10	3.23365E+10
428	7.11900E-04	1.20140E-03	5925.27	3513.54	.228848	7.95669E+10	4.89066E+10	3.23746E+10
431	7.12000E-04	1.20130E-03	5924.43	3513.83	.228659	7.95680E+10	4.88733E+10	3.23806E+10
433	7.12400E-04	1.20150E-03	5921.07	3513.24	.228325	7.95197E+10	4.87835E+10	3.23692E+10
435	7.12200E-04	1.20150E-03	5922.75	3513.24	.228562	7.95350E+10	4.88356E+10	3.23692E+10
438	7.12500E-04	1.20220E-03	5920.23	3511.18	.228699	7.94504E+10	4.88082E+10	3.23311E+10
440	7.12700E-04	1.20350E-03	5918.56	3507.35	.229374	7.93208E+10	4.88502E+10	3.22606E+10
442	7.13200E-04	1.20360E-03	5914.37	3507.05	.228853	7.92739E+10	4.87275E+10	3.22552E+10
447	7.13600E-04	1.20460E-03	5911.03	3504.11	.229081	7.91558E+10	4.86958E+10	3.22012E+10
449	7.13300E-04	1.21490E-03	5913.53	3494.74	.231656	7.88979E+10	4.90029E+10	3.20292E+10

452	7.13600E-04	1.21520E-03	5911.03	3493.87	.231513	7.88492E+10	4.89466E+10	3.20131E+10
454	7.13300E-04	1.21530E-03	5913.53	3493.58	.231931	7.88628E+10	4.90315E+10	3.20078E+10
456	7.13500E-04	1.21640E-03	5911.86	3490.37	.232454	7.87514E+10	4.90580E+10	3.19490E+10
459	7.13600E-04	1.21590E-03	5911.03	3491.82	.231995	7.87878E+10	4.89965E+10	3.19757E+10
462	7.13600E-04	1.21460E-03	5911.03	3495.62	.231098	7.89018E+10	4.89037E+10	3.20453E+10
466	7.13600E-04	1.21550E-03	5911.03	3492.99	.23172	7.88229E+10	4.89680E+10	3.19971E+10
469	7.14000E-04	1.21560E-03	5907.69	3492.7	.231322	7.87843E+10	4.88716E+10	3.19917E+10
473	7.14100E-04	1.21580E-03	5906.85	3492.12	.231343	7.87593E+10	4.88599E+10	3.19811E+10
476	7.14400E-04	1.21480E-03	5904.35	3495.03	.2303	7.88242E+10	4.87111E+10	3.20345E+10
480	7.17300E-04	1.21580E-03	5896.86	3492.12	.229939	7.86695E+10	4.85505E+10	3.19810E+10
483	7.17400E-04	1.21500E-03	5896.02	3494.45	.229265	7.87315E+10	4.84678E+10	3.20238E+10
497	7.17200E-04	1.22790E-03	5897.69	3457.18	.238244	7.76240E+10	4.94252E+10	3.13444E+10
501	7.17200E-04	1.22840E-03	5897.69	3455.75	.238573	7.75805E+10	4.94597E+10	3.13185E+10
503	7.17400E-04	1.22960E-03	5896.02	3452.33	.239137	7.74621E+10	4.94909E+10	3.12565E+10
505	7.17100E-04	1.22900E-03	5898.52	3454.04	.23908	7.75353E+10	4.95268E+10	3.12874E+10
508	7.16900E-04	1.21660E-03	5900.18	3489.78	.230962	7.86298E+10	4.87104E+10	3.19384E+10
510	7.17000E-04	1.21980E-03	5899.35	3480.49	.233041	7.83436E+10	4.89112E+10	3.17685E+10
512	7.17200E-04	1.21650E-03	5897.69	3490.08	.230542	7.86161E+10	4.86261E+10	3.15437E+10
515	7.17100E-04	1.21680E-03	5898.52	3489.2	.230866	7.85975E+10	4.86731E+10	3.19277E+10
518	7.17000E-04	1.21710E-03	5899.35	3488.33	.23119	7.85788E+10	4.87202E+10	3.19117E+10
522	7.17100E-04	1.21770E-03	5898.52	3486.58	.231487	7.85191E+10	4.87370E+10	3.18798E+10
526	7.16600E-04	1.22030E-03	5902.68	3479.04	.233843	7.83293E+10	4.90495E+10	3.17420E+10
530	7.16800E-04	1.21940E-03	5901.02	3481.65	.233	7.83932E+10	4.89345E+10	3.17896E+10
533	7.16700E-04	1.22120E-03	5901.85	3476.44	.234338	7.82435E+10	4.90871E+10	3.16945E+10
536	7.16900E-04	1.21980E-03	5900.18	3480.49	.233157	7.83510E+10	4.89370E+10	3.17685E+10
539	7.16800E-04	1.21790E-03	5901.02	3486	.231973	7.85239E+10	4.88284E+10	3.18692E+10
543	7.16900E-04	1.22970E-03	5900.18	3452.04	.239762	7.74883E+10	4.96265E+10	3.12513E+10
546	7.16600E-04	1.22780E-03	5902.68	3457.47	.238852	7.76749E+10	4.95728E+10	3.13496E+10
550	7.16400E-04	1.23110E-03	5904.35	3448.06	.241229	7.74010E+10	4.98516E+10	3.11792E+10
557	7.16000E-04	1.22790E-03	5907.69	3457.18	.239591	7.77084E+10	4.97347E+10	3.13444E+10
564	7.16300E-04	1.22770E-03	5905.18	3457.75	.239123	7.77048E+10	4.96434E+10	3.13547E+10
571	7.16100E-04	1.22310E-03	5906.85	3470.96	.236301	7.81210E+10	4.93752E+10	3.15946E+10
575	7.17200E-04	1.22140E-03	5897.69	3475.86	.233898	7.81897E+10	4.89723E+10	3.16840E+10
585	7.17300E-04	1.22780E-03	5896.86	3457.47	.238066	7.76256E+10	4.93925E+10	3.13496E+10
704	7.13100E-04	1.22880E-03	5915.21	3434.46	.245721	7.70698E+10	5.05153E+10	3.09338E+10

LENGTH OF LINE M8-M6 IS 4.18146 METER.

DENSITY USED IS 2622.5 KG/M<sup>3</sup>

Table C:1.7 day #,  $t_p$ ,  $t_s$ ,  $V_p$ ,  $V_s$ ,  $\nu$ ,  $E_d$ ,  $K_d$ , and  $G_d$  for monitor line

M8-M6

PROCESS DATE :19 JAN,1981

LINE AND FILE NAME:

MON79

DAY	P-TIME (SEC)	S-TIME (SEC)	P-VELOCITY (M/SEC)	S-VELOCITY (M/SEC)	POISS.RATIO	YOUNGS MOD (PA)	BULK MOD (PA)	SHEAR MOD (PA)
-43	7.37300E-04	1.32180E-03	5748.48	3206.95	.27407	6.87264E+10	5.06988E+10	2.69712E+10
0	7.39500E-04	1.32070E-03	5731.23	3209.65	.271529	6.87046E+10	5.01192E+10	2.70165E+10
6	7.27600E-04	1.25640E-03	5825.77	3375.4	.247335	7.45382E+10	4.91679E+10	2.98790E+10
8	7.23200E-04	1.25090E-03	5861.52	3390.38	.248616	7.52784E+10	4.99094E+10	3.01447E+10
11	7.21800E-04	1.24970E-03	5872.99	3393.66	.24936	7.54693E+10	5.01843E+10	3.02032E+10
12	7.19900E-04	1.25040E-03	5888.62	3391.74	.25177	7.55295E+10	5.0721E+10	3.01691E+10
13	7.20700E-04	1.25020E-03	5882.03	3392.29	.250816	7.54962E+10	5.04956E+10	3.01788E+10
14	7.19800E-04	1.25010E-03	5889.45	3392.57	.251695	7.55615E+10	5.07181E+10	3.01837E+10
15	7.18900E-04	1.24470E-03	5896.89	3407.42	.249371	7.60831E+10	5.05948E+10	3.04485E+10
21	7.21600E-04	1.24150E-03	5874.63	3416.28	.244509	7.61817E+10	4.96963E+10	3.06072E+10
43	7.17600E-04	1.21450E-03	5907.66	3492.94	.231261	7.87914E+10	4.88648E+10	3.19962E+10
50	7.19000E-04	1.21450E-03	5896.06	3492.94	.229629	7.86870E+10	4.85056E+10	3.19962E+10
57	7.18700E-04	1.21420E-03	5898.54	3493.81	.229772	7.87354E+10	4.85612E+10	3.20122E+10
64	7.20000E-04	1.21290E-03	5887.8	3497.59	.22734	7.87498E+10	4.81367E+10	3.20815E+10
78	7.17400E-04	1.21270E-03	5909.32	3498.18	.230253	7.89630E+10	4.87884E+10	3.20922E+10
91	7.16200E-04	1.21210E-03	5919.31	3499.93	.231239	7.91052E+10	4.90554E+10	3.21242E+10
110	7.16400E-04	1.21350E-03	5917.64	3495.85	.231968	7.89678E+10	4.91034E+10	3.20495E+10
112	7.16500E-04	1.21560E-03	5916.81	3489.75	.233284	7.87768E+10	4.92264E+10	3.19378E+10
159	7.15600E-04	1.21070E-03	5924.32	3504.01	.230973	7.92729E+10	4.91109E+10	3.21993E+10
176	7.14600E-04	1.21140E-03	5932.68	3501.97	.232617	7.92862E+10	4.94210E+10	3.21617E+10
195	7.14800E-04	1.21100E-03	5931.01	3503.13	.232111	7.93065E+10	4.93403E+10	3.21832E+10
222	7.16300E-04	1.22170E-03	5918.48	3472.17	.2376	7.82576E+10	4.97063E+10	3.16167E+10
333	7.14900E-04	1.22150E-03	5930.17	3472.74	.239041	7.83747E+10	5.00556E+10	3.16271E+10
334	7.14900E-04	1.23620E-03	5930.17	3431.06	.2484	7.70827E+10	5.10617E+10	3.08726E+10
337	7.16600E-04	1.23010E-03	5915.98	3448.24	.242728	7.75024E+10	5.02078E+10	3.11824E+10
349	7.16700E-04	1.22190E-03	5915.14	3471.59	.237281	7.82116E+10	4.96168E+10	3.16062E+10
362	7.16200E-04	1.23440E-03	5919.31	3436.11	.245885	7.71540E+10	5.06031E+10	3.09635E+10
383	7.15700E-04	1.22300E-03	5923.48	3468.44	.239129	7.81863E+10	4.99521E+10	3.15489E+10
398	7.17300E-04	1.24640E-03	5910.15	3402.73	.252079	7.60382E+10	5.11173E+10	3.03648E+10
399	7.17400E-04	1.25010E-03	5909.32	3392.57	.254182	7.57116E+10	5.13330E+10	3.01837E+10
400	7.23700E-04	1.25530E-03	5857.44	3378.38	.250755	7.48748E+10	5.00677E+10	2.99318E+10
419	7.43900E-04	1.26790E-03	5697.04	3344.51	.237061	7.25774E+10	4.60039E+10	2.93346E+10
431	7.47500E-04	1.28570E-03	5669.38	3297.8	.244304	7.09773E+10	4.62642E+10	2.85209E+10
433	7.44300E-04	1.37250E-03	5693.96	3087.5	.291758	6.45865E+10	5.16919E+10	2.49995E+10
435	7.48100E-04	1.37040E-03	5664.79	3092.27	.287769	6.45862E+10	5.07200E+10	2.50768E+10
438	7.51100E-04	1.37200E-03	5641.98	3088.64	.286031	6.43474E+10	5.01221E+10	2.50178E+10
440	7.50800E-04	1.37410E-03	5644.25	3083.88	.287215	6.42083E+10	5.02921E+10	2.49408E+10
442	7.50000E-04	1.37470E-03	5650.32	3082.52	.288132	6.41975E+10	5.05012E+10	2.49188E+10
447	7.50700E-04	1.37650E-03	5645.01	3078.46	.28836	6.40397E+10	5.04314E+10	2.48532E+10
449	7.50800E-04	1.37730E-03	5644.25	3076.65	.288632	6.39782E+10	5.04477E+10	2.48241E+10
452	7.50300E-04	1.37800E-03	5648.04	3075.08	.289343	6.39479E+10	5.05939E+10	2.47986E+10
454	7.50300E-04	1.37840E-03	5648.04	3074.18	.289518	6.39192E+10	5.06133E+10	2.47841E+10
456	7.50600E-04	1.37800E-03	5645.77	3075.08	.289101	6.39359E+10	5.05265E+10	2.47986E+10
459	7.50900E-04	1.37800E-03	5643.49	3075.08	.288859	6.39239E+10	5.04592E+10	2.47986E+10
462	7.50800E-04	1.37800E-03	5644.25	3075.08	.28894	6.39279E+10	5.04816E+10	2.47986E+10
466	7.46000E-04	1.37840E-03	5680.87	3074.18	.292948	6.40892E+10	5.15886E+10	2.47841E+10
469	7.46800E-04	1.37900E-03	5674.74	3072.83	.292572	6.40143E+10	5.14349E+10	2.47624E+10
473	7.45600E-04	1.37880E-03	5683.95	3073.28	.293435	6.40759E+10	5.16996E+10	2.47696E+10
476	7.45700E-04	1.37810E-03	5683.18	3074.85	.293057	6.41227E+10	5.16428E+10	2.47950E+10
480	7.45100E-04	1.37840E-03	5687.79	3074.18	.293659	6.41244E+10	5.17949E+10	2.47841E+10
483	7.45200E-04	1.37710E-03	5687.02	3077.11	.293024	6.42151E+10	5.17091E+10	2.48313E+10
497	7.45300E-04	1.37790E-03	5686.25	3075.3	.293288	6.41530E+10	5.17248E+10	2.48023E+10
501	7.45600E-04	1.37530E-03	5683.95	3081.17	.291932	6.43303E+10	5.15299E+10	2.48969E+10
503	7.44700E-04	1.37600E-03	5690.87	3079.59	.292949	6.43149E+10	5.17705E+10	2.48714E+10
505	7.44400E-04	1.37540E-03	5693.19	3080.94	.292929	6.43705E+10	5.18104E+10	2.48933E+10
508	7.44200E-04	1.37500E-03	5694.73	3081.84	.292916	6.44076E+10	5.18370E+10	2.49079E+10
510	7.45100E-04	1.37430E-03	5687.79	3083.43	.291899	6.44230E+10	5.15958E+10	2.49335E+10
512	7.41000E-04	1.37460E-03	5719.53	3082.75	.295272	6.45628E+10	5.25599E+10	2.49225E+10

515	7.44700E-04	1.37510E-03	5690.87	3081.62	.292562	6.43805E+10	5.17268E+10	2.49042E+10
518	7.43600E-04	1.37460E-03	5699.36	3082.75	.293221	6.44606E+10	5.19560E+10	2.49225E+10
522	7.43300E-04	1.37460E-03	5701.68	3082.75	.293458	6.44724E+10	5.20253E+10	2.49225E+10
526	7.42900E-04	1.37310E-03	5704.78	3086.14	.293132	6.45982E+10	5.20447E+10	2.49774E+10
530	7.44300E-04	1.37380E-03	5693.96	3084.56	.29232	6.44913E+10	5.17554E+10	2.49518E+10
533	7.43700E-04	1.37390E-03	5698.59	3084.33	.292841	6.45079E+10	5.18987E+10	2.49481E+10
536	7.43100E-04	1.37410E-03	5703.23	3083.88	.293403	6.45169E+10	5.20472E+10	2.49408E+10
539	7.42900E-04	1.37470E-03	5704.78	3082.52	.293818	6.44809E+10	5.21228E+10	2.49188E+10
543	7.43500E-04	1.37560E-03	5700.14	3080.49	.293728	6.43913E+10	5.20278E+10	2.48860E+10
546	7.43100E-04	1.37380E-03	5703.23	3084.56	.293274	6.45389E+10	5.20326E+10	2.49518E+10
550	7.38200E-04	1.37390E-03	5741.41	3084.33	.297168	6.47238E+10	5.31833E+10	2.49481E+10
557	7.38700E-04	1.37450E-03	5737.49	3082.97	.297029	6.46599E+10	5.30946E+10	2.49261E+10
706	7.52200E-04	1.35180E-03	5633.66	3135.18	.275675	6.57674E+10	4.88632E+10	2.57775E+10

LENGTH OF LINE M7-M9 IS 4.20271 METER.

DENSITY USED IS 2622.5 KG/M<sup>3</sup>

Table C:1.8 day #,  $t_p$ ,  $t_s$ ,  $V_p$ ,  $V_s$ ,  $\nu$ ,  $E_d$ ,  $K_d$ , and  $G_d$  for monitor line

M7-M9

PROCESS DATE :19 JAN,1981

LINE AND FILE NAME:

REF96

DAY	P-TIME (SEC)	S-TIME (SEC)	P-VELOCITY (M/SEC)	S-VELOCITY (M/SEC)	POISS.RATIO	YOUNGS MOD (PA)	BULK MOD (PA)	SHEAR MOD (PA)
-1	4.7700E-04	8.0710E-04	5899.45	3490.15	.230772	7.86341E+10	4.86787E+10	3.19450E+10
0	4.7660E-04	8.0690E-04	5904.46	3491.03	.231267	7.87053E+10	4.88126E+10	3.19611E+10
5	4.7690E-04	8.0700E-04	5900.7	3490.59	.230844	7.86584E+10	4.87068E+10	3.19531E+10
6	4.7660E-04	8.0640E-04	5904.46	3493.22	.230747	7.87710E+10	4.87590E+10	3.20013E+10
19	4.7640E-04	8.0650E-04	5906.98	3492.78	.231203	7.87804E+10	4.88475E+10	3.19932E+10
20	4.7500E-04	8.0980E-04	5924.62	3478.35	.237005	7.84988E+10	4.97467E+10	3.17294E+10
20	4.7520E-04	8.0430E-04	5922.09	3502.47	.231025	7.92066E+10	4.90794E+10	3.21710E+10
20	4.7680E-04	8.1100E-04	5901.95	3473.13	.235126	7.81444E+10	4.91708E+10	3.16342E+10
20	4.7530E-04	8.0970E-04	5920.83	3478.78	.236391	7.84794E+10	4.96185E+10	3.17373E+10
113	4.7420E-04	8.0950E-04	5934.74	3479.65	.238072	7.86255E+10	5.00299E+10	3.17532E+10
116	4.7450E-04	8.0910E-04	5930.94	3481.4	.237158	7.86463E+10	4.98692E+10	3.17851E+10
118	4.7460E-04	8.1060E-04	5929.68	3474.87	.238489	7.84356E+10	4.99887E+10	3.16659E+10
118	4.7500E-04	8.1050E-04	5924.62	3475.3	.237707	7.84058E+10	4.98208E+10	3.16738E+10
119	4.7490E-04	8.1030E-04	5925.88	3476.17	.237678	7.84432E+10	4.98390E+10	3.16897E+10
119	4.7460E-04	8.1020E-04	5929.68	3476.61	.238089	7.84889E+10	4.99464E+10	3.16976E+10
132	4.7430E-04	8.0960E-04	5933.48	3479.22	.238001	7.86013E+10	5.00011E+10	3.17453E+10
223	4.7450E-04	8.1140E-04	5930.94	3471.39	.239453	7.83398E+10	5.01125E+10	3.16026E+10
223	4.7360E-04	8.1000E-04	5942.36	3477.48	.23959	7.86234E+10	5.03202E+10	3.17135E+10
320	4.7510E-04	8.0990E-04	5923.35	3477.91	.236935	7.84746E+10	4.97181E+10	3.17214E+10
336	4.7470E-04	8.0870E-04	5928.41	3483.15	.236412	7.86777E+10	4.97479E+10	3.18170E+10
336	4.7470E-04	8.0870E-04	5928.41	3483.15	.236412	7.86777E+10	4.97479E+10	3.18170E+10
337	4.7470E-04	8.0600E-04	5928.41	3494.98	.233662	7.90371E+10	4.94591E+10	3.20335E+10
343	4.7460E-04	8.1200E-04	5929.68	3468.79	.239878	7.82493E+10	5.01362E+10	3.15552E+10
344	4.7460E-04	8.1240E-04	5929.68	3467.06	.240272	7.81960E+10	5.01782E+10	3.15237E+10
344	4.7440E-04	8.1590E-04	5932.21	3451.98	.244014	7.77510E+10	5.06219E+10	3.12501E+10
348	4.7450E-04	8.1400E-04	5930.94	3460.15	.242008	7.79936E+10	5.03850E+10	3.13982E+10
349	4.7450E-04	8.1340E-04	5930.94	3462.74	.241422	7.80735E+10	5.03223E+10	3.14452E+10
349	4.7520E-04	8.1340E-04	5922.09	3462.74	.240246	7.79995E+10	5.00471E+10	3.14452E+10
350	4.7490E-04	8.1080E-04	5925.88	3474	.238178	7.83767E+10	4.98918E+10	3.16500E+10
350	4.7520E-04	8.1040E-04	5922.09	3475.74	.237266	7.83974E+10	4.97318E+10	3.16817E+10
354	4.7480E-04	8.0930E-04	5927.14	3480.53	.236845	7.85870E+10	4.97723E+10	3.17691E+10
354	4.7510E-04	8.1570E-04	5923.35	3452.83	.24266	7.77051E+10	5.03258E+10	3.16256E+10
355	4.7500E-04	8.1500E-04	5924.62	3455.84	.242147	7.78083E+10	5.02924E+10	3.13201E+10
355	4.7460E-04	8.1080E-04	5929.68	3474	.238688	7.84090E+10	5.00098E+10	3.16500E+10
356	4.7450E-04	8.1480E-04	5930.94	3456.7	.242786	7.78871E+10	5.04683E+10	3.13357E+10
356	4.7510E-04	8.1410E-04	5923.35	3459.72	.241102	7.79172E+10	5.01595E+10	3.13904E+10
357	4.7450E-04	8.1370E-04	5930.94	3461.44	.241715	7.80335E+10	5.03537E+10	3.14217E+10
357	4.7520E-04	8.1470E-04	5922.09	3457.13	.241521	7.78272E+10	5.01827E+10	3.13435E+10
358	4.7490E-04	8.1450E-04	5925.88	3457.99	.241827	7.78852E+10	5.02707E+10	3.13591E+10
362	4.7510E-04	8.1440E-04	5923.35	3458.42	.241395	7.78775E+10	5.01907E+10	3.13669E+10
375	4.7500E-04	8.1020E-04	5924.62	3476.61	.237407	7.84456E+10	4.97891E+10	3.16976E+10
375	4.7500E-04	8.1050E-04	5924.62	3475.3	.237707	7.84058E+10	4.98208E+10	3.16738E+10
385	4.7550E-04	8.1250E-04	5918.3	3466.63	.23885	7.80869E+10	4.98354E+10	3.15159E+10
398	4.7550E-04	8.1270E-04	5918.3	3465.76	.239049	7.80604E+10	4.98563E+10	3.15001E+10
398	4.7510E-04	8.1220E-04	5923.35	3467.92	.23923	7.81693E+10	4.99606E+10	3.15395E+10
419	4.7520E-04	8.1240E-04	5922.09	3467.06	.239259	7.81321E+10	4.99424E+10	3.15237E+10
420	4.7530E-04	8.1100E-04	5920.83	3473.13	.237696	7.83070E+10	4.97559E+10	3.16342E+10
424	4.7540E-04	8.1240E-04	5919.56	3467.06	.238921	7.81108E+10	4.98640E+10	3.15237E+10
424	4.7540E-04	8.0940E-04	5919.56	3480.09	.235916	7.85082E+10	4.95474E+10	3.17612E+10
424	4.7480E-04	8.0920E-04	5927.14	3480.96	.236744	7.86003E+10	4.97617E+10	3.17771E+10
425	4.7560E-04	8.0890E-04	5917.04	3482.27	.235064	7.85525E+10	4.94160E+10	3.18010E+10
425	4.7540E-04	8.0920E-04	5919.56	3480.96	.235713	7.85347E+10	4.95262E+10	3.17771E+10
425	4.7550E-04	8.0930E-04	5918.3	3480.53	.235642	7.85106E+10	4.94977E+10	3.17691E+10
426	4.7480E-04	8.0950E-04	5927.14	3479.65	.237046	7.85604E+10	4.97935E+10	3.17532E+10
566	4.7690E-04	8.1270E-04	5925.88	3495.42	.23321	7.90280E+10	4.93697E+10	3.20416E+10
566	4.7870E-04	8.1610E-04	5903.21	3480.53	.233567	7.83787E+10	4.90297E+10	3.17691E+10
699	4.7530E-04	8.1070E-04	5920.83	3474.43	.237396	7.83468E+10	4.97243E+10	3.16579E+10
701	4.7590E-04	8.0420E-04	5913.26	3502.91	.229683	7.91402E+10	4.87946E+10	3.21791E+10



706	4.76000E-04	8.04800E-04	5912	3500.26	.230135	7.90496E+10	4.88204E+10	3.21305E+10
708	4.76200E-04	8.06100E-04	5909.49	3494.54	.231139	7.88556E+10	4.88825E+10	3.20255E+10
710	4.76000E-04	8.05500E-04	5912	3497.18	.230866	7.89573E+10	4.88959E+10	3.20739E+10
712	4.76000E-04	8.05000E-04	5912	3499.38	.230344	7.90232E+10	4.88420E+10	3.21143E+10
712	4.76400E-04	8.05200E-04	5906.98	3498.5	.229346	7.89515E+10	4.87077E+10	3.20981E+10
712	4.76400E-04	8.05000E-04	5906.98	3499.38	.229636	7.89778E+10	4.86862E+10	3.21143E+10
712	4.76200E-04	8.05200E-04	5909.49	3498.5	.2302	7.89742E+10	4.87856E+10	3.20981E+10
756	4.76000E-04	8.05400E-04	5912	3497.62	.230762	7.89705E+10	4.88852E+10	3.20819E+10

LENGTH OF LINE REF. LINE M9-M6 IS 2.77746 METER.

DENSITY USED IS 2622.5 KG/M<sup>3</sup>

Table C:1.9 day #,  $t_p$ ,  $t_s$ ,  $V_p$ ,  $V_s$ ,  $\nu$ ,  $E_d$ ,  $K_d$ , and  $G_d$  for reference line  
M9-M6

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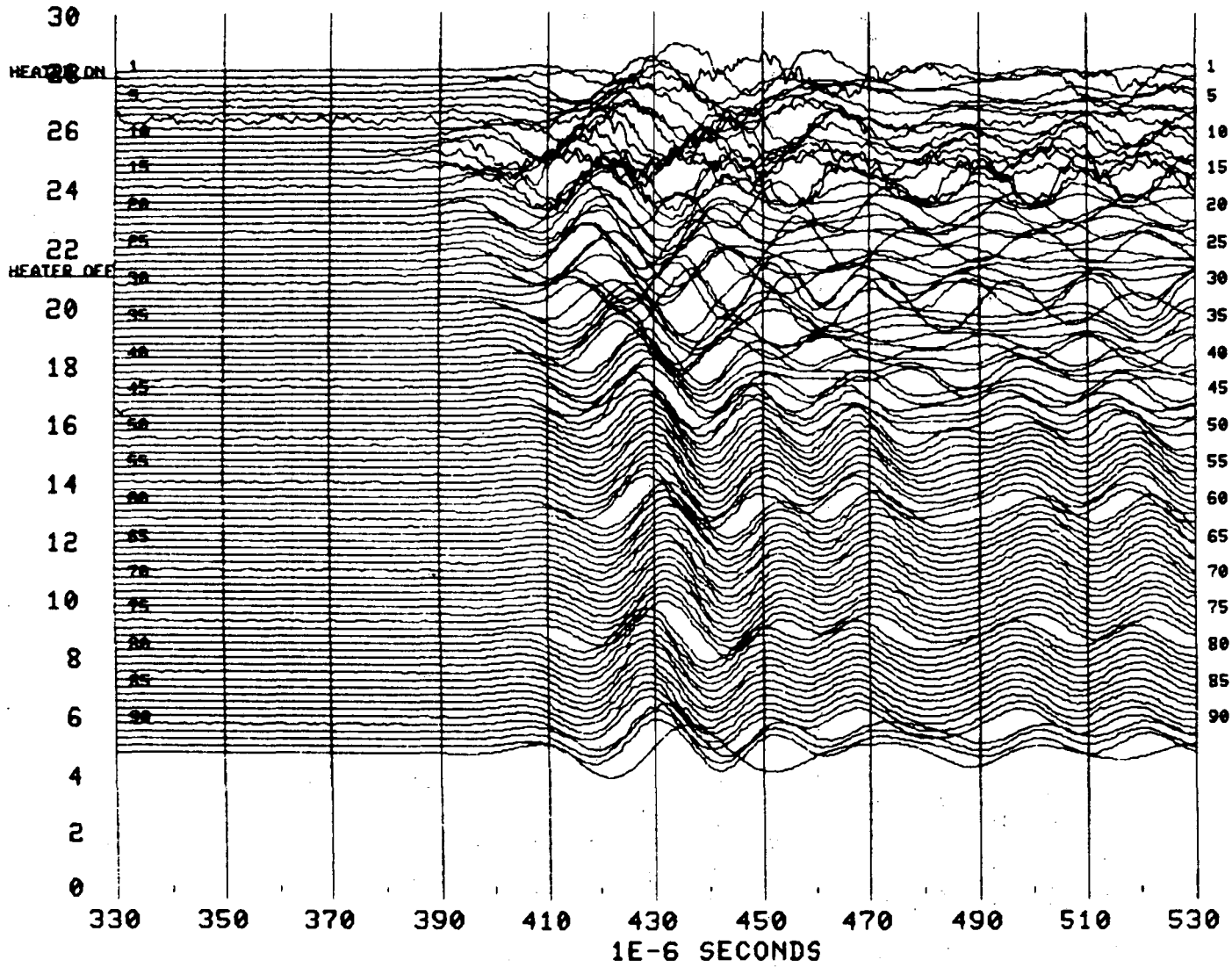
## Appendix C:2 - P waveforms from the monitor and reference lines

The P waveforms make up the data base where the arrival times and change in arrival times for the P waves in the heater midplane can be verified. The P-waveforms shown in this appendix are digitized from the AM taperecorder and graphed. The waveform were averaged 4 times to improve the signal to noise ratio. The primary source of noise was the taperecorder. In Figure 3.5 in Chapter 3 a polaroid photograph of a typical signal is shown and note the high signal to noise ratio. The high frequency noise seen in the figures in this appendix are all generated by the recording process.

The signals are normalized before graphing because the amplitude control was poor and the amplitude depended on the coupling between the transducer and the borehole wall as well as the rock. The vertical spacing in the figures do not represent equal time. The time between each recording is obtained from the tables in Appendix C:1.

PROFILE AND FILE NAME : M7-M6, M76P0., P-WAVES  
FIELD WORK : 1978-80 HEATER DAYS : -44-701 PLOTDATE : 830112

Fig. C:2.1 P waveforms from monitor line M7-M6



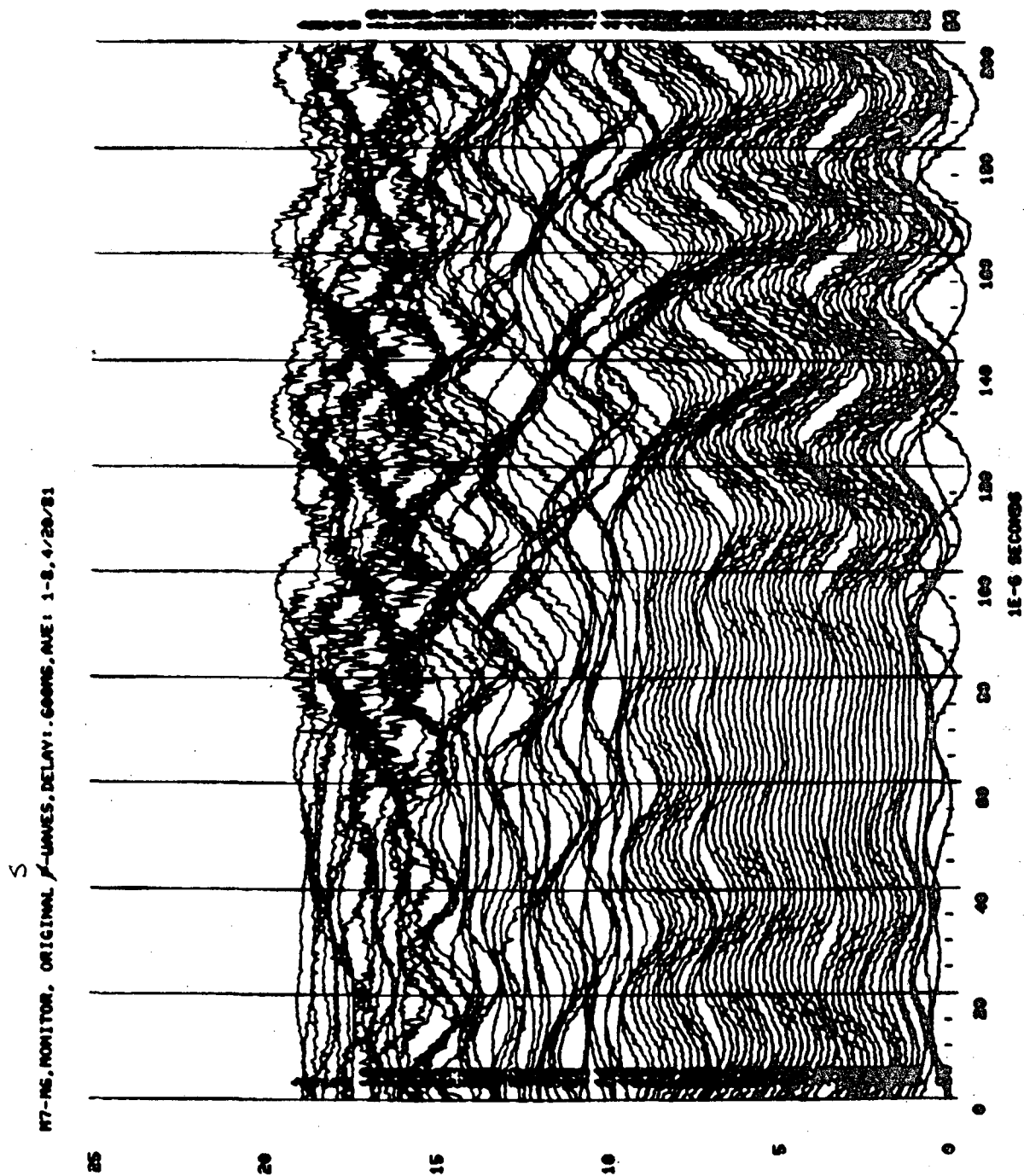
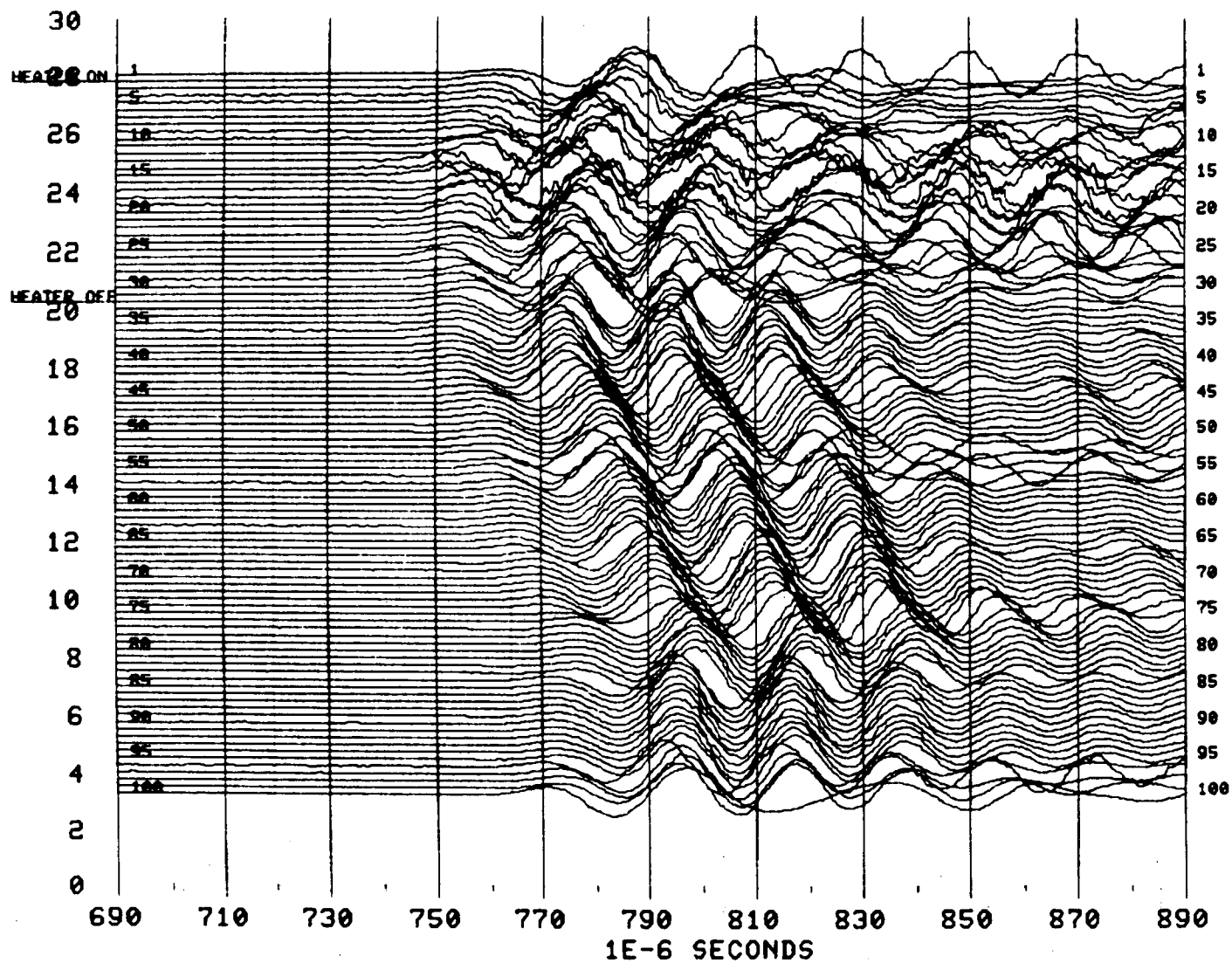


Fig. C:2.2 S waveforms from monitor line M7-M6

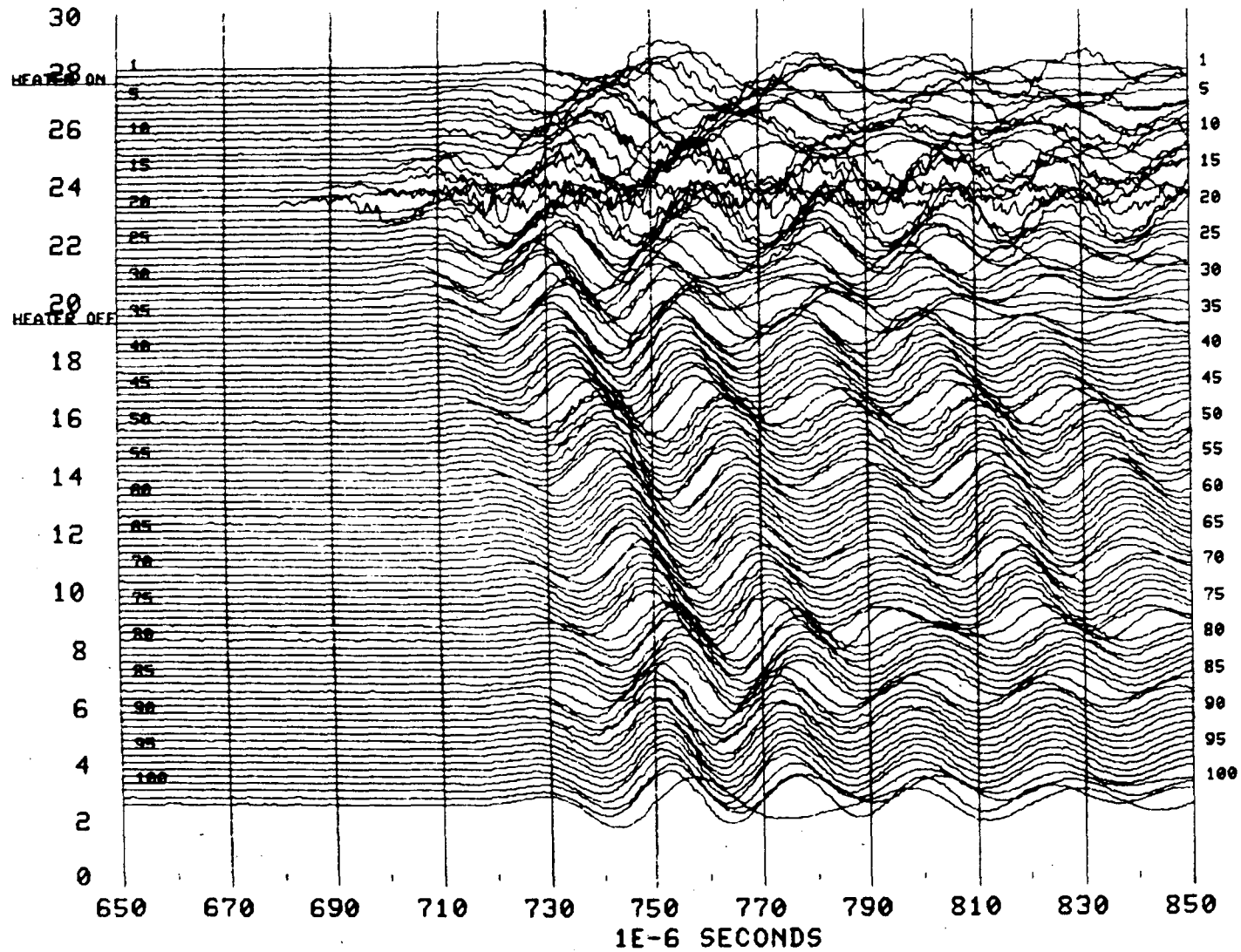
PROFILE AND FILE NAME : M8-M9, M89P0., P-WAVES  
FIELD WORK : 1978-80 HEATER DAYS : -42-711 PLOTDATE : 830112

Fig. C:2.3 P waveforms from monitor line M8-M9



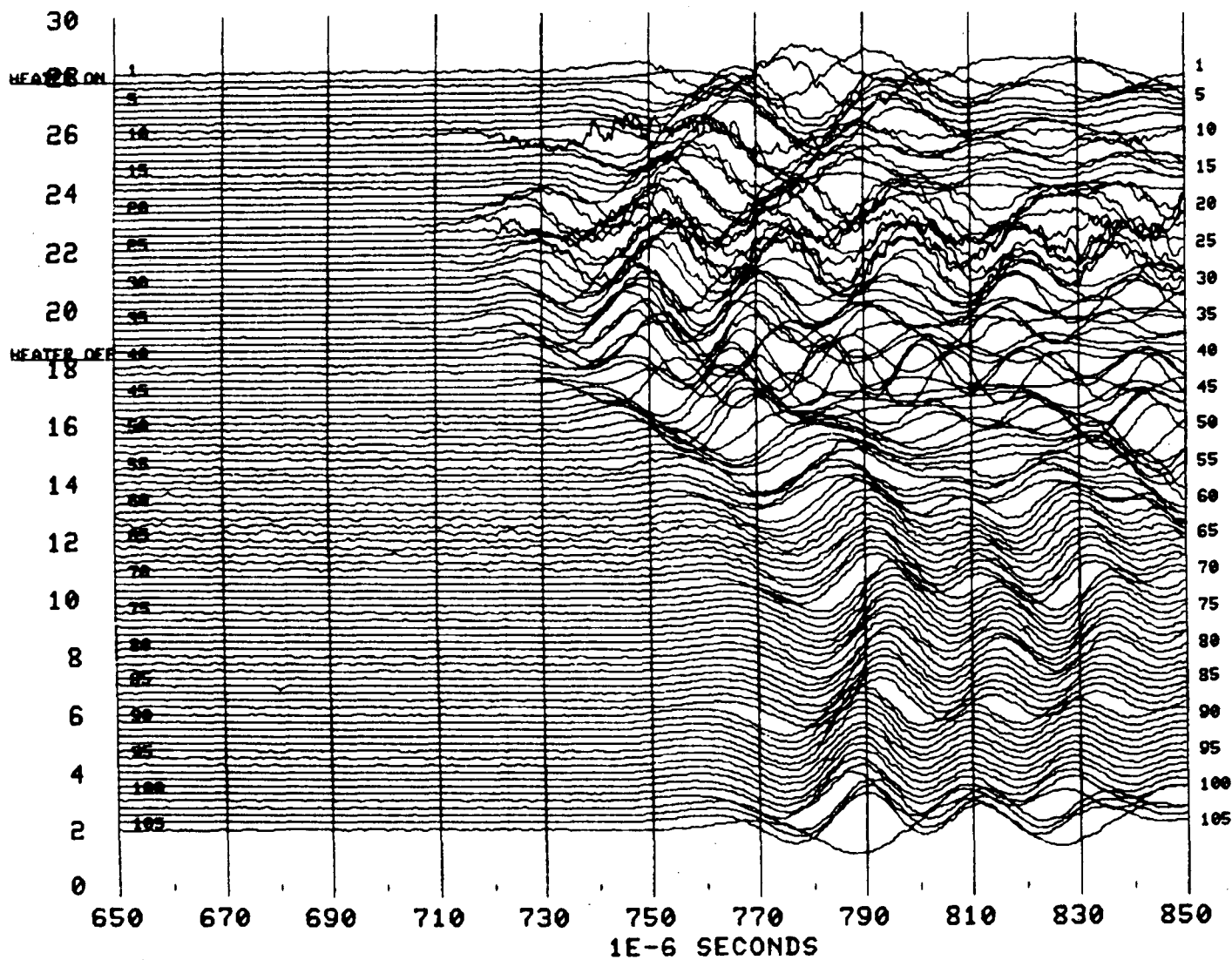
PROFILE AND FILE NAME : M8-M6, M86P0., P-WAVES  
FIELD WORK : 78-80 HEATER DAYS : -43-704 PLOTDATE : 830112

Fig. C:2.4 P wavelforms from monitor line M8-M6



PROFILE AND FILE NAME : M7-M9, M79P0., P-WAVES  
FIELD WORK : 1978-80 HEATER DAYS : -43-706 PLOTDATE : 830112

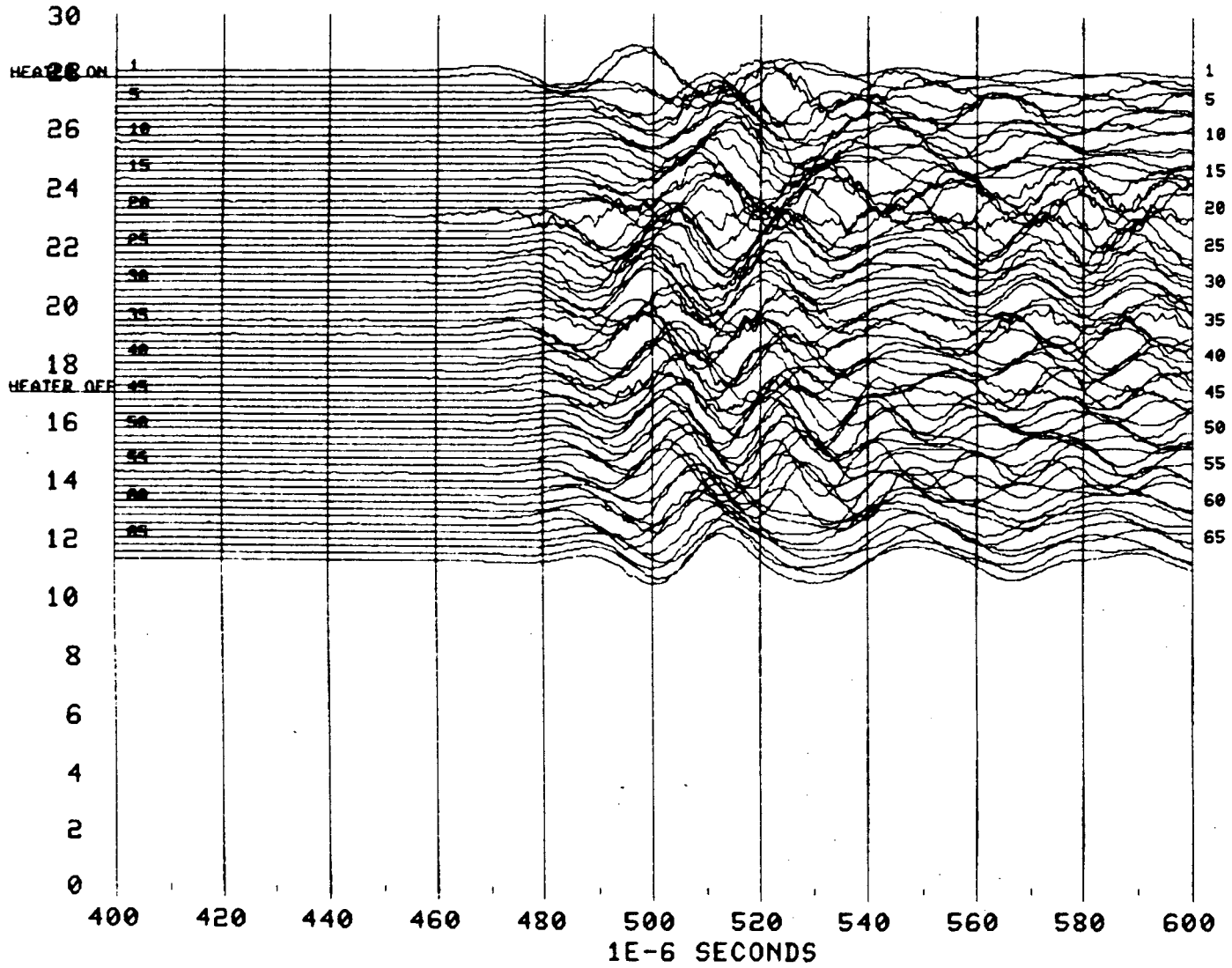
Fig. C:2.5 P waveforms from monitor line M7-M9





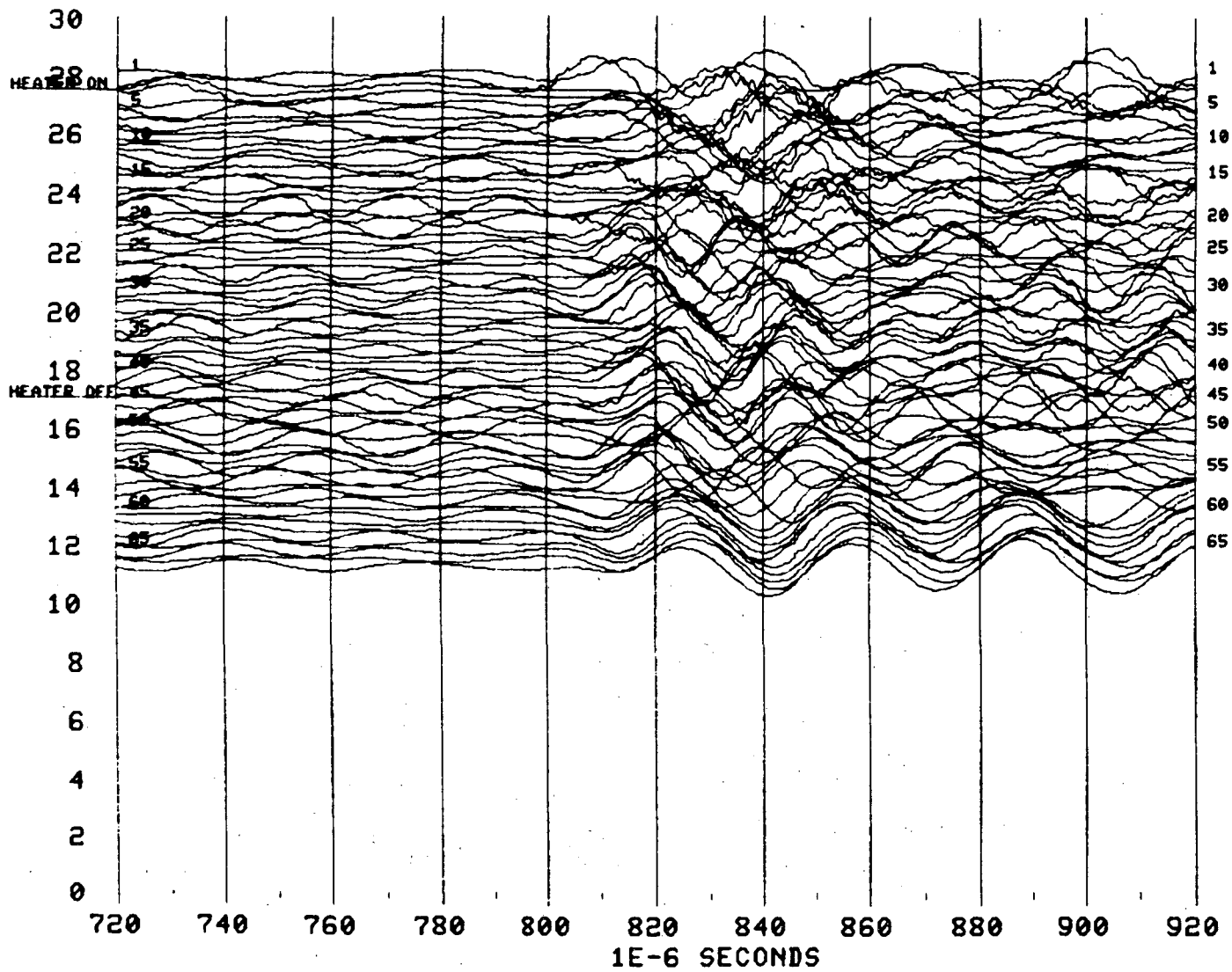
PROFILE AND FILE NAME : M9-M6, R96P0., P-WAVES  
FIELD WORK :78-80 HEATER DAYS : -1-756 PLOTDATE : 830112

Fig. C:2.6 P waveforms from reference line M9-M6



PROFILE AND FILE NAME : M9-M6, R9650., S-WAVES  
FIELD WORK :78-80 HEATER DAYS : -1-756 PLOTDATE : 830112

Fig. C:2.7 S waveforms from reference line M9-m6



### Appendix C:3 - Tables for the survey data in six cross sections

In this appendix results from the cross hole surveys in the six ultrasonic sections are presented. In the first of the nine columns the Julian heater day is listed. In the second column the recorded time of arrival for the P waves,  $t_p$  are shown. This is not corrected for the instrument delay of  $6.2 \times 10^{-6}$  s. which was done before the  $V_p$  was calculated. In the third column the arrival time for the S waves,  $t^s$  are given. The instrument delay for the S waves were  $11.3 \times 10^{-6}$  s which should be subtracted from the arrival times of the S waves before  $V_s$  is calculated. The  $V_p$  and the  $V_s$  are shown in columns 4 and 5 respectively.

Using the expressions in Chapter 7 the Poissons ratio and the dynamic moduli were calculated and they are presented in column 6 through 9. The density used for the calculation of the dynamic moduli is  $2622 \text{ kg/m}^3$ .

PROFILE AND FILE NAME : M7-M6 SURVA.1

DATE FOR FIELD WORK : 11 JULY, 1978 DAYS AFTER HEATER TURN ON : -44 PROCESS DATE : 20 JAN, 1981

LINE #	P-TIME (SEC)	S-TIME (SEC)	P-VELOCITY (M/SEC)	S-VELOCITY (M/SEC)	POISS.RATIO	YOUNGS MOD (PA)	BULK MOD (PA)	SHEAR MOD (PA)
3	3.85100E-04	6.60200E-04	5938.24	3467.41	.24133	7.82784E+10	5.04364E+10	3.15381E+10
5	3.87400E-04	6.64300E-04	5902.41	3445.64	.241523	7.73106E+10	4.98501E+10	3.11354E+10
7	3.86400E-04	6.65700E-04	5915.31	3436.74	.245226	7.71412E+10	5.04639E+10	3.09748E+10
9	3.87600E-04	6.67600E-04	5896.7	3426.79	.245032	7.66832E+10	5.01261E+10	3.07957E+10
11	3.93300E-04	6.73900E-04	5809.87	3394.2	.240923	7.49836E+10	4.82376E+10	3.02128E+10
13	4.02600E-04	6.61600E-04	5671.04	3456.87	.204367	7.54866E+10	4.25565E+10	3.13387E+10
15	4.00200E-04	6.98100E-04	5708.12	3274.61	.254729	7.05690E+10	4.79531E+10	2.81212E+10
17	4.01600E-04	6.94400E-04	5685.38	3290.88	.248068	7.08937E+10	4.69000E+10	2.84014E+10
19	4.01800E-04	7.04300E-04	5682.51	3243.87	.258302	6.94475E+10	4.78886E+10	2.75957E+10
21	4.03300E-04	6.87400E-04	5658.52	3323.47	.236679	7.16452E+10	4.53472E+10	2.89668E+10
23	3.98800E-04	6.56300E-04	5723.38	3483.72	.205726	7.67505E+10	4.34689E+10	3.18275E+10
25	4.00700E-04	6.72500E-04	5695.82	3398.37	.223624	7.41197E+10	4.46974E+10	3.02870E+10
27	3.88000E-04	6.51300E-04	5880.04	3507.81	.223739	7.89781E+10	4.76470E+10	3.22692E+10
29	3.86700E-04	6.45700E-04	5900.13	3538.78	.219073	8.00722E+10	4.75047E+10	3.28414E+10
31	3.89300E-04	6.66000E-04	5854.87	3426	.239654	7.63168E+10	4.88560E+10	3.07815E+10
33	3.85300E-04	6.61900E-04	5914.01	3446.05	.242962	7.74188E+10	5.01994E+10	3.11429E+10
35	3.91100E-04	6.65400E-04	5824.89	3427.61	.235165	7.61121E+10	4.78990E+10	3.08105E+10
37	3.88200E-04	6.83300E-04	5863.87	3333.33	.261297	7.35056E+10	5.13229E+10	2.91389E+10
39	3.88000E-04	6.63100E-04	5864.33	3435.1	.238829	7.66719E+10	4.89282E+10	3.09453E+10

LINE # DISTANCE

(M)

3	2.25
6	2.25
7	2.249
9	2.249
11	2.249
13	2.248
15	2.249
17	2.248
19	2.248
21	2.247
23	2.247
25	2.247
27	2.245
29	2.245
31	2.243
33	2.242
35	2.242
37	2.24
39	2.239

DENSITY : 2622.5 KG/M<sup>3</sup>

INSTRUMENT DELAY FOR P-WAVE : 6.20000E-06 SEC.

INSTRUMENT DELAY FOR S-WAVE : 1.13000E-05 SEC.

Table C:3.1  $day\#$ ,  $t_p$ ,  $t_s$ ,  $V_p$ ,  $V_s$ ,  $\nu$ ,  $E_d$ ,  $K_d$ , and  $G_d$  for survey #1 at 44 days before heater turn on in cross section M7-M6.

PROFILE AND FILE NAME : M7-M6 SURVA.2

DATE FOR FIELD WORK : 3 AUG,1979 DAYS AFTER HEATER TURN ON : 344 PROCESS DATE : 20 JAN,1981

LINE #	P-TIME (SEC)	S-TIME (SEC)	P-VELOCITY (M/SEC)	S-VELOCITY (M/SEC)	POISS.RATIO	YOUNGS MOD (PA)	BULK MOD (PA)	SHEAR MOD (PA)
3	3.84500E-04	6.53900E-04	5947.66	3501.4	.234807	7.94014E+10	4.99016E+10	3.21513E+10
5	3.83200E-04	6.48600E-04	5968.17	3530.52	.230839	8.04681E+10	4.98265E+10	3.26883E+10
7	3.83800E-04	6.47900E-04	5956.04	3532.83	.228599	8.04269E+10	4.93900E+10	3.27311E+10
9	3.83200E-04	6.54900E-04	5965.52	3494.41	.238822	7.93416E+10	5.06306E+10	3.20230E+10
11	3.85400E-04	6.46200E-04	5930.91	3542.29	.222735	8.04722E+10	4.83726E+10	3.29067E+10
13	3.91700E-04	6.44200E-04	5831.39	3551.9	.205082	7.97415E+10	4.50643E+10	3.30855E+10
15	3.88400E-04	6.46400E-04	5884.35	3541.18	.216108	7.99857E+10	4.69578E+10	3.28859E+10
17	3.89200E-04	6.46100E-04	5869.45	3541.27	.213813	7.98392E+10	4.64960E+10	3.28878E+10
19	3.90500E-04	6.61000E-04	5849.6	3460.06	.230915	7.72930E+10	4.78740E+10	3.13966E+10
21	3.91000E-04	6.71500E-04	5839.4	3403.51	.242747	7.55063E+10	4.89184E+10	3.03788E+10
23	3.91300E-04	6.62500E-04	5834.85	3450.55	.231103	7.68806E+10	4.76518E+10	3.12243E+10
25	3.91200E-04	6.60600E-04	5836.36	3460.65	.228889	7.71922E+10	4.74542E+10	3.14073E+10
27	3.86100E-04	6.54800E-04	5909.45	3488.73	.232504	7.86809E+10	4.90230E+10	3.19191E+10
29	3.84500E-04	6.40400E-04	5934.44	3568.59	.216787	8.12743E+10	4.78287E+10	3.33971E+10
31	3.85600E-04	6.43700E-04	5911.97	3546.81	.218843	8.04207E+10	4.76724E+10	3.29906E+10
33	3.82600E-04	6.51800E-04	5956.43	3500.39	.236232	7.94472E+10	5.02001E+10	3.21328E+10
35	3.82500E-04	6.48400E-04	5958.01	3519.07	.232114	8.00299E+10	4.97910E+10	3.24767E+10
37	3.81500E-04	6.68200E-04	5968.56	3409.96	.257713	7.67051E+10	5.27646E+10	3.04930E+10

LINE # DISTANCE

LINE #	DISTANCE (M)
3	2.25
5	2.25
7	2.249
9	2.249
11	2.249
13	2.248
15	2.249
17	2.248
19	2.248
21	2.247
23	2.247
25	2.247
27	2.245
29	2.245
31	2.243
33	2.242
35	2.242
37	2.24

DENSITY : 2622.5 KG/M<sup>3</sup>

INSTRUMENT DELAY FOR P-WAVE : 6.20000E-06 SEC.

INSTRUMENT DELAY FOR S-WAVE : 1.13000E-06 SEC.

Table C:3.2  $day\#$ ,  $t_p$ ,  $t_s$ ,  $V_p$ ,  $V_s$ ,  $\nu$ ,  $E_d$ ,  $K_d$ , and  $G_d$  for survey # 2 at 344 days after the heater turn on in cross section M7-M6.

PROFILE AND FILE NAME : M7-M6 SURVA.3

DATE FOR FIELD WORK : 22 OCT.,1979 DAYS AFTER HEATER TURN ON : 424 PROCESS DATE : 20 JAN.,1981

LINE #	P-TIME (SEC)	S-TIME (SEC)	P-VELOCITY (M/SEC)	S-VELOCITY (M/SEC)	POISS.RATIO	YOUNGS MOD (PA)	BULK MOD (PA)	SHEAR MOD (PA)
3	3.85000E-04	6.42800E-04	5939.81	3562.95	.218982	8.11636E+10	4.81366E+10	3.32915E+10
5	3.86200E-04	6.45400E-04	5921.05	3548.34	.21981	8.05541E+10	4.79164E+10	3.30191E+10
7	3.88000E-04	6.45600E-04	5890.52	3545.64	.215918	8.01750E+10	4.70375E+10	3.29689E+10
9	3.89600E-04	6.52100E-04	5865.94	3509.68	.221208	7.88985E+10	4.71668E+10	3.23035E+10
11	3.91400E-04	6.54800E-04	5838.53	3494.95	.220791	7.82111E+10	4.66861E+10	3.20330E+10
13	4.05100E-04	6.85700E-04	5635.5	3333.33	.230936	7.17362E+10	4.44357E+10	2.91389E+10
15	4.05500E-04	6.79000E-04	5632.36	3368.28	.22163	7.26945E+10	4.35240E+10	2.97531E+10
17	3.97000E-04	6.77800E-04	5752.3	3372.84	.238034	7.38704E+10	4.69975E+10	2.98338E+10
19	3.97900E-04	6.88500E-04	5739.09	3319.55	.248618	7.21662E+10	4.78463E+10	2.88984E+10
21	3.96500E-04	6.92900E-04	5757.11	3296.66	.256066	7.15987E+10	4.89194E+10	2.85012E+10
23	3.94100E-04	6.70600E-04	5792.73	3408.16	.23529	7.52583E+10	4.73841E+10	3.04618E+10
25	3.93600E-04	6.77800E-04	5800.21	3371.34	.244889	7.42133E+10	4.84842E+10	2.98072E+10
27	3.85700E-04	6.49900E-04	5915.68	3515.5	.227017	7.95373E+10	4.85606E+10	3.24108E+10
29	3.85300E-04	6.41600E-04	5921.92	3561.8	.216603	8.09529E+10	4.76087E+10	3.32701E+10
31	3.86200E-04	6.51700E-04	5902.63	3502.5	.228277	7.90311E+10	4.84753E+10	3.21715E+10
33	3.83500E-04	6.48100E-04	5942.22	3520.73	.229526	7.99371E+10	4.92574E+10	3.25073E+10
35	3.82900E-04	6.42600E-04	5951.69	3551.4	.223534	8.09396E+10	4.87941E+10	3.30762E+10
37	3.83300E-04	6.41400E-04	5940.07	3554.99	.220973	8.09335E+10	4.83426E+10	3.31430E+10

LINE # DISTANCE

(M)

3	2.25
5	2.25
7	2.249
9	2.249
11	2.249
13	2.248
15	2.249
17	2.248
19	2.248
21	2.247
23	2.247
25	2.247
27	2.245
29	2.245
31	2.243
33	2.242
35	2.242
37	2.24

DENSITY : 2622.6 KG/M<sup>3</sup>

INSTRUMENT DELAY FOR P-WAVE : 6.20000E-06 SEC.

INSTRUMENT DELAY FOR S-WAVE : 1.13000E-05 SEC.

Table C.3.3  $day\#$ ,  $t_p$ ,  $t_s$ ,  $V_p$ ,  $V_s$ ,  $\nu$ ,  $E_d$ ,  $K_d$ , and  $G_d$  for survey # 3 at 424 days after heater turn on and 26 days after the H9 heater was turned off, in cross section M7-M6.

PROFILE AND FILE NAME : M7-M6 SURVA.4

DATE FOR FIELD WORK : 25 JULY,1980 DAYS AFTER HEATER TURN ON : 701 PROCESS DATE : 20 JAN,1981

LINE #	P-TIME (SEC)	S-TIME (SEC)	P-VELOCITY (M/SEC)	S-VELOCITY (M/SEC)	POISS.RATIO	YOUNGS MOD (PA)	BULK MOD (PA)	SHEAR MOD (PA)
1	3.86100E-04	6.50200E-04	5922.61	3521.68	.226524	7.97849E+10	4.86239E+10	3.25248E+10
3	3.88700E-04	6.49700E-04	5882.35	3524.44	.219986	7.94840E+10	4.73095E+10	3.25758E+10
5	3.84700E-04	6.44400E-04	5944.52	3553.94	.221879	8.09457E+10	4.85074E+10	3.31235E+10
7	3.87200E-04	6.47600E-04	5902.89	3534.5	.22054	7.99747E+10	4.76959E+10	3.27620E+10
9	3.88200E-04	6.47300E-04	5887.43	3536.16	.217827	7.98722E+10	4.71769E+10	3.27929E+10
11	3.91100E-04	6.53900E-04	5843.08	3499.84	.22025	7.83957E+10	4.67058E+10	3.21228E+10
13	4.07000E-04	7.14000E-04	5608.78	3199.09	.258904	6.75757E+10	4.67143E+10	2.68391E+10
15	4.00100E-04	7.23300E-04	5709.57	3158.71	.279473	6.69569E+10	5.06036E+10	2.61658E+10
17	3.94300E-04	6.53500E-04	5792.32	3500.47	.212334	7.79147E+10	4.51419E+10	3.21342E+10
19	3.94900E-04	7.16600E-04	5783.38	3187.3	.281892	6.83033E+10	5.21939E+10	2.66416E+10
21	3.95400E-04	7.58900E-04	5773.38	3005.62	.314107	6.22650E+10	5.58250E+10	2.36910E+10
23	3.93000E-04	7.95900E-04	5809.2	2863.88	.339464	5.76217E+10	5.98221E+10	2.15092E+10
25	3.92800E-04	6.72000E-04	5812.21	3400.94	.239676	7.52058E+10	4.81489E+10	3.03328E+10
27	3.85400E-04	6.47100E-04	5920.36	3530.98	.223952	8.00390E+10	4.83244E+10	3.26969E+10
29	3.85600E-04	6.49200E-04	5917.24	3519.36	.226312	7.96662E+10	4.85141E+10	3.24820E+10
31	3.85600E-04	6.47300E-04	5911.97	3526.73	.22377	7.98343E+10	4.81690E+10	3.26182E+10
33	3.82300E-04	6.43700E-04	5961.18	3545.22	.226377	8.08457E+10	4.92440E+10	3.29612E+10
35	3.82200E-04	6.45400E-04	5962.77	3535.72	.22886	8.05756E+10	4.95289E+10	3.27847E+10
37	3.82200E-04	6.40000E-04	5957.45	3562.91	.221578	8.13347E+10	4.86878E+10	3.32908E+10
39	3.82700E-04	6.43000E-04	5946.88	3544.4	.224531	8.06867E+10	4.88178E+10	3.29460E+10

LINE #	DISTANCE (M)
1	2.25
3	2.25
5	2.25
7	2.249
9	2.249
11	2.249
13	2.248
15	2.249
17	2.248
19	2.248
21	2.247
23	2.247
25	2.247
27	2.245
29	2.245
31	2.243
33	2.242
35	2.242
37	2.24
39	2.239

DENSITY : 2622.5 KG/M<sup>3</sup>

INSTRUMENT DELAY FOR P-WAVE : 6.20000E-06 SEC.

INSTRUMENT DELAY FOR S-WAVE : 1.13000E-05 SEC.

Table C:3.4  $day\#$ ,  $t_p$ ,  $t_s$ ,  $V_p$ ,  $V_s$ ,  $\nu$ ,  $E_d$ ,  $K_d$ , and  $G_d$  for survey # 4 at 701 days after heater turn on and 403 days after the H9 heater was turned off, in cross section M7-M6.

PROFILE AND FILE NAME : M7-M8 SURV.1

DATE FOR FIELD WORK : 13 JULY, 1978 DAYS AFTER HEATER TURN ON : -44 PROCESS DATE : 20 JAN, 1981

LINE #	P-TIME (SEC)	S-TIME (SEC)	P-VELOCITY (M/SEC)	S-VELOCITY (M/SEC)	POISS.RATIO	YOUNGS MOD (PA)	BULK MOD (PA)	SHEAR MOD (PA)
1	4.71700E-04	9.43400E-04	5772.29	2882.74	.333857	5.81387E+10	5.83220E+10	2.17934E+10
3	4.57400E-04	8.85600E-04	5955.23	3073.32	.318496	6.53189E+10	5.99794E+10	2.47702E+10
5	4.64700E-04	8.27400E-04	5858.23	3291.26	.26939	7.21217E+10	5.21239E+10	2.84080E+10
7	4.64500E-04	8.81000E-04	5858.61	3087.27	.307776	6.53775E+10	5.66852E+10	2.49957E+10
9	4.62500E-04	8.88300E-04	5879.9	3059.29	.314403	6.45233E+10	5.79421E+10	2.45447E+10
11	4.74800E-04	8.31800E-04	5723.43	3268.74	.25797	7.04979E+10	4.85463E+10	2.80205E+10
13	4.73700E-04	8.34200E-04	5736.9	3259.21	.261718	7.02961E+10	4.91687E+10	2.78573E+10
15	4.74100E-04	8.22000E-04	5727.72	3306.79	.250253	7.16626E+10	4.78234E+10	2.86592E+10
17	4.67400E-04	8.32600E-04	5808.76	3261.9	.269714	7.08587E+10	5.12830E+10	2.79034E+10
19	4.63400E-04	8.19200E-04	5857.39	3314.77	.264429	7.28695E+10	5.15552E+10	2.88152E+10
21	4.61300E-04	8.12400E-04	5880.03	3340.41	.261741	7.38439E+10	5.16552E+10	2.92627E+10
23	4.57200E-04	8.68500E-04	5933.48	3121.79	.308614	6.68906E+10	5.82512E+10	2.55578E+10
25	4.58900E-04	8.48600E-04	5908.99	3194.79	.293466	6.92446E+10	5.58782E+10	2.67671E+10
27	4.55100E-04	8.30400E-04	5959.01	3265.78	.285358	7.19024E+10	5.58314E+10	2.79698E+10
29	4.54800E-04	7.62300E-04	5958.54	3559.25	.222623	8.12374E+10	4.88129E+10	3.32226E+10
31	4.54400E-04	7.98500E-04	5961.62	3394.31	.260168	7.61512E+10	5.29199E+10	3.02147E+10
33	4.53100E-04	7.82200E-04	5978.97	3466.08	.246913	7.85703E+10	5.17413E+10	3.15059E+10
35	4.54000E-04	7.56500E-04	5964.72	3584.27	.21741	8.20322E+10	4.83812E+10	3.36913E+10
37	4.55700E-04	7.80300E-04	5939.93	3472.04	.240503	7.84355E+10	5.03766E+10	3.16144E+10
39	4.54400E-04	7.77000E-04	5954.03	3485.7	.239392	7.89831E+10	5.05121E+10	3.18636E+10

LINE #	DISTANCE (M)
1	2.687
3	2.687
5	2.686
7	2.685
9	2.683
11	2.682
13	2.682
15	2.68
17	2.679
19	2.678
21	2.676
23	2.676
25	2.675
27	2.675
29	2.673
31	2.672
33	2.672
35	2.671
37	2.67
39	2.669

DENSITY : 2622.5 KG/M<sup>3</sup>

INSTRUMENT DELAY FOR P-WAVE : 6.20000E-06 SEC.

INSTRUMENT DELAY FOR S-WAVE : 1.13000E-05 SEC.

Table C:3.5  $day\#$ ,  $t_p$ ,  $t_s$ ,  $V_p$ ,  $V_s$ ,  $\nu$ ,  $E_d$ ,  $K_d$ , and  $G_d$  for survey # 1 at 44 days before heater turn on in cross section M7-M8.



PROFILE AND FILE NAME : M7-M8 SURVB.2

DATE FOR FIELD WORK : 14-15 DEC, 1978 DAYS AFTER HEATER TURN ON : 112 PROCESS DATE : 21 JAN, 1981

LINE #	P-TIME (SEC)	S-TIME (SEC)	P-VELOCITY (M/SEC)	S-VELOCITY (M/SEC)	POISS.RATIO	YOUNGS MOD (PA)	BULK MOD (PA)	SHEAR MOD (PA)
3	4.53900E-04	7.78100E-04	6001.79	3504.17	.241405	7.99521E+10	5.15298E+10	3.22023E+10
5	4.53900E-04	7.83900E-04	5999.55	3476.57	.247229	7.90668E+10	5.21333E+10	3.16970E+10
7	4.56200E-04	7.77900E-04	5961.37	3502.48	.236419	7.95540E+10	5.03033E+10	3.21711E+10
9	4.54200E-04	7.74200E-04	5986.17	3516.84	.236466	8.02110E+10	5.07277E+10	3.24356E+10
11	4.55200E-04	7.84900E-04	5967.95	3466.91	.245319	7.85074E+10	5.13763E+10	3.15210E+10
13	4.51200E-04	7.81000E-04	5944.15	3484.47	.238231	7.88536E+10	5.02056E+10	3.18412E+10
15	4.53900E-04	7.68700E-04	5986.15	3538.42	.231478	8.08707E+10	5.01949E+10	3.28348E+10
17	4.51200E-04	7.68200E-04	6020.22	3539.44	.235877	8.12062E+10	5.12426E+10	3.28537E+10
19	4.54900E-04	7.64300E-04	5968.35	3556.44	.224714	8.12477E+10	4.91899E+10	3.31701E+10
21	4.52500E-04	7.69200E-04	5995.97	3530.81	.234584	8.07262E+10	5.06915E+10	3.26937E+10
23	4.54000E-04	7.67500E-04	5965.22	3538.75	.228489	8.06892E+10	4.95310E+10	3.28409E+10
25	4.55100E-04	7.82100E-04	5959.01	3470.42	.243377	7.85439E+10	5.10112E+10	3.15849E+10
27	4.54200E-04	7.95000E-04	5970.98	3413.3	.2573	7.68303E+10	5.27608E+10	3.05537E+10
29	4.53700E-04	7.78800E-04	5973.18	3482.74	.242469	7.90446E+10	5.11554E+10	3.18095E+10
31	4.54100E-04	7.74900E-04	5965.62	3499.21	.237739	7.94905E+10	5.05161E+10	3.21112E+10
33	4.51000E-04	7.72800E-04	6007.19	3508.86	.241062	8.01442E+10	5.15851E+10	3.22886E+10
35	4.54500E-04	7.89400E-04	5958.06	3432.72	.251558	7.73524E+10	5.18916E+10	3.09024E+10
37	4.51000E-04	7.76000E-04	6002.7	3491.57	.24433	7.95649E+10	5.18670E+10	3.19710E+10

LINE # DISTANCE

	(M)
3	2.687
5	2.686
7	2.685
9	2.683
11	2.682
13	2.682
15	2.68
17	2.679
19	2.678
21	2.676
23	2.676
25	2.675
27	2.675
29	2.673
31	2.672
33	2.672
35	2.671
37	2.67

DENSITY : 2622.5 KG/M<sup>3</sup>

INSTRUMENT DELAY FOR P-WAVE : 6.80000E-06 SEC.

INSTRUMENT DELAY FOR S-WAVE : 1.13000E-06 SEC.

Table C:3.6  $day\#$ ,  $t_p$ ,  $t_s$ ,  $V_p$ ,  $V_s$ ,  $\nu$ ,  $E_d$ ,  $K_d$ , and  $G_d$  for survey # 2 at 112 days after the heater was turned on in cross section M7-M8.

PROFILE AND FILE NAME : M7-M8 SURUB.3

DATE FOR FIELD WORK : 7 AUG,1979 DAYS AFTER HEATER TURN ON : 348 PROCESS DATE : 21 JAN,1981

LINE #	P-TIME (SEC)	S-TIME (SEC)	P-VELOCITY (M/SEC)	S-VELOCITY (M/SEC)	POISS.RATIO	YOUNGS MOD (PA)	BULK MOD (PA)	SHEAR MOD (PA)
3	4.53500E-04	7.53900E-04	6007.15	3618.37	.215296	8.34551E+10	4.88549E+10	3.43353E+10
5	4.54100E-04	7.55600E-04	5996.87	3608.76	.21614	8.30701E+10	4.87740E+10	3.41532E+10
7	4.56400E-04	7.73400E-04	5964.02	3523.16	.231987	8.02077E+10	4.98780E+10	3.25522E+10
9	4.53500E-04	7.68700E-04	5998.21	3542.38	.232215	8.11003E+10	5.04759E+10	3.29084E+10
11	4.55800E-04	7.89600E-04	5965.3	3445.97	.249585	7.78278E+10	5.17993E+10	3.11415E+10
13	4.54700E-04	7.89000E-04	5979.93	3448.63	.250843	7.80264E+10	5.21935E+10	3.11895E+10
15	4.52400E-04	7.38600E-04	6006.27	3684.86	.198224	8.53347E+10	4.71291E+10	3.56088E+10
17	4.51300E-04	7.47100E-04	6018.87	3640.94	.211446	8.42317E+10	4.86516E+10	3.47649E+10
19	4.59700E-04	7.62500E-04	6024.75	3564.96	.230612	8.20398E+10	5.07514E+10	3.33292E+10
21	4.49500E-04	7.54400E-04	6036.54	3601.13	.22375	8.32369E+10	5.02183E+10	3.40089E+10
23	4.51800E-04	7.29700E-04	6005.39	3724.94	.187347	8.64097E+10	4.60626E+10	3.63877E+10
25	4.52400E-04	7.33900E-04	5995.07	3701.91	.191858	8.56686E+10	4.63361E+10	3.59391E+10
27	4.50500E-04	7.36600E-04	6020.71	3688.13	.199684	8.55903E+10	4.75001E+10	3.56720E+10
29	4.51400E-04	7.72200E-04	6004.04	3512.95	.239731	8.02446E+10	5.13857E+10	3.23637E+10
31	4.50200E-04	7.71200E-04	6018.02	3516.25	.240823	8.04666E+10	5.17450E+10	3.24247E+10
33	4.49800E-04	7.93300E-04	6023.44	3416.88	.262768	7.73265E+10	5.43254E+10	3.06179E+10
35	4.51000E-04	7.95100E-04	6004.95	3407.76	.262486	7.68970E+10	5.39596E+10	3.04546E+10
37	4.49700E-04	8.15800E-04	6020.29	3318.83	.281709	7.40467E+10	5.65352E+10	2.88859E+10

LINE # DISTANCE  
(M)

3	2.687
5	2.686
7	2.685
9	2.683
11	2.682
13	2.682
15	2.68
17	2.679
19	2.678
21	2.676
23	2.676
25	2.675
27	2.675
29	2.673
31	2.672
33	2.672
35	2.671
37	2.67

DENSITY : 2622.5 KG/M<sup>3</sup>

INSTRUMENT DELAY FOR P-WAVE : 6.20000E-06 SEC.

INSTRUMENT DELAY FOR S-WAVE : 1.13000E-05 SEC.

Table C:3.7  $day\#$ ,  $t_p$ ,  $t_s$ ,  $V_p$ ,  $V_s$ ,  $\nu$ ,  $E_d$ ,  $K_d$ , and  $G_d$  for survey # 3 at 348 days after the heater was turned on in cross section M7-M8.

PROFILE AND FILE NAME : M7-M8 SURUB.4

DATE FOR FIELD WORK : 23 OCT,1979 DAYS AFTER HEATER TURN ON : 456 PROCESS DATE : 21 JAN,1981

LINE #	P-TIME (SEC)	S-TIME (SEC)	P-VELOCITY (M/SEC)	S-VELOCITY (M/SEC)	POISS.RATIO	YOUNGS MOD (PA)	BULK MOD (PA)	SHEAR MOD (PA)
3	4.54300E-04	7.76600E-04	5996.43	3511.04	.239155	8.01204E+10	5.11928E+10	3.23286E+10
5	4.57200E-04	7.88300E-04	5955.65	3456.89	.245957	7.80942E+10	5.12342E+10	3.13390E+10
7	4.63100E-04	8.00900E-04	5876.56	3400.46	.248309	7.57080E+10	5.01330E+10	3.03242E+10
9	4.62200E-04	7.90700E-04	5883.77	3442.39	.239773	7.70563E+10	4.93520E+10	3.10768E+10
11	4.70200E-04	8.23400E-04	5780.17	3302.55	.257664	7.19463E+10	4.94812E+10	2.86032E+10
13	4.78800E-04	8.26100E-04	5674.99	3291.61	.246508	7.08363E+10	4.65737E+10	2.84139E+10
15	4.72500E-04	8.15200E-04	5747.37	3333.75	.246472	7.26597E+10	4.77657E+10	2.91461E+10
17	4.65100E-04	8.10600E-04	5837.87	3351.68	.254152	7.38961E+10	5.00960E+10	2.94606E+10
19	4.59300E-04	7.81800E-04	5910.4	3475.67	.235691	7.82945E+10	4.93706E+10	3.16805E+10
21	4.54300E-04	7.88000E-04	5971.88	3445.35	.250548	7.78595E+10	5.20203E+10	3.11301E+10
23	4.53800E-04	7.86800E-04	5978.55	3450.68	.250226	7.80805E+10	5.21008E+10	3.12265E+10
25	4.53200E-04	8.09600E-04	5984.34	3350.87	.271633	7.48898E+10	5.46561E+10	2.94463E+10
27	4.51900E-04	7.70900E-04	6001.79	3521.59	.237476	8.04933E+10	5.11022E+10	3.25232E+10
29	4.52000E-04	7.89400E-04	5995.96	3435.29	.255672	7.77229E+10	5.30180E+10	3.09487E+10
31	4.51400E-04	7.79800E-04	6001.8	3476.9	.247441	7.90953E+10	5.21959E+10	3.17030E+10
33	4.48600E-04	7.70600E-04	6039.78	3519.03	.24303	8.07371E+10	5.23649E+10	3.24759E+10
35	4.50800E-04	7.74500E-04	6007.65	3499.74	.243157	7.98624E+10	5.18231E+10	3.21208E+10
37	4.49200E-04	7.70200E-04	6027.09	3518.25	.24156	8.06059E+10	5.19823E+10	3.24615E+10

LINE # DISTANCE

(M)

3	2.687
5	2.686
7	2.685
9	2.683
11	2.682
13	2.682
15	2.68
17	2.679
19	2.678
21	2.676
23	2.676
25	2.675
27	2.675
29	2.673
31	2.672
33	2.672
35	2.671
37	2.67

DENSITY : 2622.5 KG/M-3

INSTRUMENT DELAY FOR P-WAVE : 6.20000E-06 SEC.

INSTRUMENT DELAY FOR S-WAVE : 1.13000E-05 SEC.

Table C:3.8  $day\#$ ,  $t_p$ ,  $t_s$ ,  $V_p$ ,  $V_s$ ,  $\nu$ ,  $E_d$ ,  $K_d$ , and  $G_d$  for survey # 4 at 456 days after the heater was turned on, and 58 days after the heater was turned off, in cross-section M7-M8.

PROFILE AND FILE NAME : M7-M8 SURV.5

DATE FOR FIELD WORK : 1 AUG,1980 DAYS AFTER HEATER TURN ON : 708 PROCESS DATE : 21 JAN,1981

LINE #	P-TIME (SEC)	S-TIME (SEC)	P-VELOCITY (M/SEC)	S-VELOCITY (M/SEC)	POISS.RATIO	YOUNGS MOD (PA)	BULK MOD (PA)	SHEAR MOD (PA)
1	4.63200E-04	8.79000E-04	5879.65	3096.69	.308062	6.57915E+10	5.71293E+10	2.51485E+10
3	4.54200E-04	8.83900E-04	5997.77	3079.3	.321032	6.56998E+10	6.11840E+10	2.48668E+10
5	4.58100E-04	8.87300E-04	5943.79	3066.21	.31869	6.50268E+10	5.97750E+10	2.46558E+10
7	4.66800E-04	8.66800E-04	5829.35	3138.52	.2959	6.69523E+10	5.46729E+10	2.58324E+10
9	4.66300E-04	9.28500E-04	5831.34	2925.21	.331874	5.97753E+10	5.92565E+10	2.24403E+10
11	4.71200E-04	9.34100E-04	5767.74	2906.37	.329834	5.89176E+10	5.77059E+10	2.21523E+10
13	4.81400E-04	9.57600E-04	5643.94	2834.2	.331398	5.60936E+10	5.54497E+10	2.10657E+10
15	4.75900E-04	9.31500E-04	5705.77	2912.41	.32383	5.88956E+10	5.57184E+10	2.22444E+10
17	4.65800E-04	8.90700E-04	5828.98	3046.4	.312109	6.38686E+10	5.66538E+10	2.43382E+10
19	4.60500E-04	8.62400E-04	5894.78	3146.52	.300777	6.75473E+10	5.65089E+10	2.59642E+10
21	4.55400E-04	8.50200E-04	5957.26	3189.89	.299012	6.93283E+10	5.74897E+10	2.66850E+10
23	4.56000E-04	8.73300E-04	5949.31	3104.41	.312917	6.63652E+10	5.91229E+10	2.52740E+10
25	4.54700E-04	8.86700E-04	5964.33	3055.75	.322044	6.47479E+10	6.06402E+10	2.44878E+10
27	4.51600E-04	8.06000E-04	6005.84	3366.05	.271011	7.55329E+10	5.49755E+10	2.97137E+10
29	4.52300E-04	8.80500E-04	5991.93	3075.24	.3212	6.55349E+10	6.10878E+10	2.48013E+10
31	4.52200E-04	8.82400E-04	5991.03	3067.39	.322364	6.52580E+10	6.12283E+10	2.46747E+10
33	4.49300E-04	7.77700E-04	6030.24	3486.43	.248949	7.96255E+10	5.28614E+10	3.18770E+10
35	4.51200E-04	7.86600E-04	6002.25	3445.12	.254351	7.80859E+10	5.29793E+10	3.11260E+10
37	4.50500E-04	7.98800E-04	6009.45	3390.48	.266528	7.63628E+10	5.45124E+10	3.01465E+10
39	4.49800E-04	8.48700E-04	6016.68	3187.25	.304958	6.95302E+10	5.94147E+10	2.66408E+10

LINE # DISTANCE

LINE #	DISTANCE (M)
1	2.687
3	2.687
5	2.686
7	2.685
9	2.683
11	2.682
13	2.682
15	2.68
17	2.679
19	2.678
21	2.676
23	2.676
25	2.675
27	2.675
29	2.673
31	2.672
33	2.672
35	2.671
37	2.67
39	2.669

DENSITY : 2622.5 KG/M<sup>3</sup>

INSTRUMENT DELAY FOR P-WAVE : 6.20000E-06 SEC.

INSTRUMENT DELAY FOR S-WAVE : 1.13000E-05 SEC.

Table C:3.9  $day\#$ ,  $t_p$ ,  $t_s$ ,  $V_p$ ,  $V_s$ ,  $\nu$ ,  $E_d$ ,  $K_d$ , and  $G_d$  for survey # 5 at 708 days after the heater was turned on, and 310 days after the heater was turned off, in cross section M7-M8

PROFILE AND FILE NAME : M8-M9 SURVC.1

DATE FOR FIELD WORK : 13 JULY, 1978 DAYS AFTER HEATER TURN ON : -42 PROCESS DATE : 21 JAN, 1981

LINE #	P-TIME (SEC)	S-TIME (SEC)	P-VELOCITY (M/SEC)	S-VELOCITY (M/SEC)	POISS.RATIO	YOUNGS MOD (PA)	BULK MOD (PA)	SHEAR MOD (PA)
1	7.57800E-04	1.26450E-03	5876.8	3524.58	.219124	7.94342E+10	4.71347E+10	3.25784E+10
5	7.56400E-04	1.27310E-03	5879.77	3495.8	.226621	7.86228E+10	4.79327E+10	3.20485E+10
9	7.54600E-04	1.26600E-03	5888.56	3512.39	.223861	7.91925E+10	4.77976E+10	3.23535E+10
13	7.54700E-04	1.26320E-03	5879.76	3515.46	.221822	7.91984E+10	4.74506E+10	3.24100E+10
17	7.55300E-04	1.27140E-03	5867.04	3487.82	.226722	7.82707E+10	4.77356E+10	3.15024E+10
21	7.57800E-04	1.27120E-03	5840.87	3484.4	.223749	7.79282E+10	4.70154E+10	3.18399E+10
25	7.54100E-04	1.25340E-03	5860.41	3528.7	.215619	7.93912E+10	4.65286E+10	3.26547E+10
29	7.52200E-04	1.27000E-03	5868.63	3478.19	.229271	7.80010E+10	4.80191E+10	3.17265E+10
33	7.61000E-04	1.28250E-03	5792.26	3439.27	.227725	7.61691E+10	4.66251E+10	3.10204E+10
37	7.59500E-04	1.28270E-03	5795.83	3434.01	.229522	7.60475E+10	4.68600E+10	3.09256E+10

LINE #	DISTANCE (M)
1	4.417
5	4.411
9	4.407
13	4.401
17	4.395
21	4.39
25	4.383
29	4.378
33	4.372
37	4.366

DENSITY : 2622.5 KG/M<sup>3</sup>

INSTRUMENT DELAY FOR P-WAVE : 6.20000E-06 SEC.

INSTRUMENT DELAY FOR S-WAVE : 1.13000E-05 SEC.

Table C:3.10  $day\#$ ,  $t_p$ ,  $t_s$ ,  $V_p$ ,  $V_s$ ,  $\nu$ ,  $E_d$ ,  $K_d$ , and  $G_d$  for survey # 1 at 42 days before heater was turned on in cross section M8-M9.

PROFILE AND FILE NAME : M8-M9 SURVC.2

DATE FOR FIELD WORK : 20 DEC,1978 DAYS AFTER HEATER TURN ON : 118 PROCESS DATE : 21 JAN,1981

LINE #	P-TIME (SEC)	S-TIME (SEC)	P-VELOCITY (M/SEC)	S-VELOCITY (M/SEC)	POISS.RATIO	YOUNGS MOD (PA)	BULK MOD (PA)	SHEAR MOD (PA)
1	7.54500E-04	1.27410E-03	5902.71	3497.78	.229418	7.88914E+10	4.85933E+10	3.20840E+10
5	7.50900E-04	1.26850E-03	5923.19	3508.59	.229731	7.94001E+10	4.89636E+10	3.22835E+10
9	7.47100E-04	1.26790E-03	5948.17	3507.08	.233556	7.95786E+10	4.97783E+10	3.22558E+10
13	7.45900E-04	1.25560E-03	5949.71	3536.93	.22673	8.04909E+10	4.90912E+10	3.28071E+10
17	7.47900E-04	1.26660E-03	5925.58	3517.97	.227834	7.97020E+10	4.88073E+10	3.24564E+10
21	7.47600E-04	1.26690E-03	5921.23	3496.34	.232351	7.90144E+10	4.92028E+10	3.20584E+10
25	7.44100E-04	1.25460E-03	5939.83	3525.3	.228105	8.00519E+10	4.90704E+10	3.25917E+10
29	7.47100E-04	1.25950E-03	5909.03	3507.46	.228001	7.92369E+10	4.85621E+10	3.22625E+10
33	7.53800E-04	1.28910E-03	5848.05	3421.51	.23977	7.61239E+10	4.87542E+10	3.07008E+10
37	7.51500E-04	1.28860E-03	5858.04	3418.15	.241887	7.61043E+10	4.91414E+10	3.06406E+10

LINE #	DISTANCE (M)
1	4.417
5	4.411
9	4.407
13	4.401
17	4.395
21	4.39
25	4.383
29	4.378
33	4.372
37	4.366

DENSITY : 2622.5 KG/M<sup>3</sup>

INSTRUMENT DELAY FOR P-WAVE : 6.20000E-06 SEC.

INSTRUMENT DELAY FOR S-WAVE : 1.13000E-05 SEC.

Table C:3.11  $day\#$ ,  $t_p$ ,  $t_s$ ,  $V_p$ ,  $V_s$ ,  $\nu$ ,  $E_d$ ,  $K_d$ , and  $G_d$  for survey # 2 at 118 days after the heater was turned on in cross section M8-M9.

PROFILE AND FILE NAME : M8-M9 SURUC.3

DATE FOR FIELD WORK : 2 AUG,1979 DAYS AFTER HEATER TURN ON : 343 PROCESS DATE : 21 JAN,1981

LINE #	P-TIME (SEC)	S-TIME (SEC)	P-VELOCITY (M/SEC)	S-VELOCITY (M/SEC)	POISS.RATIO	YOUNGS MOD (PA)	BULK MOD (PA)	SHEAR MOD (PA)
5	7.51500E-04	1.27490E-03	5918.42	3490.82	.233257	7.88232E+10	4.92504E+10	3.19573E+10
9	7.46300E-04	1.25940E-03	5954.6	3530.97	.228839	8.03578E+10	4.93912E+10	3.26966E+10
13	7.44400E-04	1.27740E-03	5961.8	3476.03	.242484	7.87414E+10	5.09622E+10	3.16871E+10
17	7.46400E-04	1.25770E-03	5937.58	3526.16	.227582	8.00569E+10	4.89792E+10	3.26076E+10
21	7.49100E-04	1.25700E-03	5909.27	3524.12	.224014	7.97322E+10	4.81498E+10	3.25700E+10
25	7.44900E-04	1.25460E-03	5933.4	3525.3	.227193	7.99925E+10	4.88701E+10	3.25917E+10
29	7.45900E-04	1.26230E-03	5918.62	3499.6	.231218	7.90892E+10	4.90418E+10	3.21183E+10
33	7.43000E-04	1.27230E-03	5933.77	3467.09	.240809	7.82313E+10	5.03047E+10	3.15243E+10
37	7.51500E-04	1.27610E-03	5858.04	3451.93	.234032	7.71251E+10	4.83209E+10	3.12492E+10

LINE # DISTANCE  
(M)

5	4.411
9	4.407
13	4.401
17	4.395
21	4.39
25	4.383
29	4.378
33	4.372
37	4.366

DENSITY : 2622.6 KG/M<sup>3</sup>

INSTRUMENT DELAY FOR P-WAVE : 6.20000E-06 SEC.

INSTRUMENT DELAY FOR S-WAVE : 1.13000E-05 SEC.

Table C:3.12  $day\#$ ,  $t_p$ ,  $t_s$ ,  $V_p$ ,  $V_s$ ,  $\nu$ ,  $E_d$ ,  $K_d$ , and  $G_d$  for survey # 3 at 343 days after the heater was turned on in cross section M8-M9.

PROFILE AND FILE NAME : M8-M9 SURUC.4

DATE FOR FIELD WORK : 23 OCT,1979 DAYS AFTER HEATER TURN ON : 425 PROCESS DATE : 21 JAN,1981

LINE #	P-TIME (SEC)	S-TIME (SEC)	P-VELOCITY (M/SEC)	S-VELOCITY (M/SEC)	POISS.RATIO	YOUNGS MOD (PA)	BULK MOD (PA)	SHEAR MOD (PA)
5	7.54100E-04	1.24350E-03	5897.85	3579.78	.208354	8.12178E+10	4.64135E+10	3.36068E+10
9	7.52400E-04	1.25460E-03	5905.92	3544.6	.218491	8.02975E+10	4.75399E+10	3.29496E+10
13	7.51900E-04	1.26270E-03	5901.84	3516.86	.2247	7.94485E+10	4.80982E+10	3.24359E+10
17	7.53700E-04	1.27160E-03	5879.6	3487.26	.228654	7.83691E+10	4.81360E+10	3.18923E+10
21	7.54600E-04	1.26850E-03	5865.85	3491.89	.225561	7.83792E+10	4.75996E+10	3.19769E+10
25	7.48500E-04	1.26110E-03	5904.62	3506.96	.227491	7.91818E+10	4.84276E+10	3.22535E+10
29	7.46900E-04	1.26800E-03	5910.62	3483.73	.233842	7.85404E+10	4.91815E+10	3.18276E+10
33	7.54200E-04	1.27940E-03	5844.92	3447.68	.233207	7.68838E+10	4.80296E+10	3.11723E+10
37	7.53900E-04	1.27800E-03	5839.24	3446.75	.232631	7.68066E+10	4.78779E+10	3.11556E+10

LINE # DISTANCE

(M)

5	4.411
9	4.407
13	4.401
17	4.396
21	4.39
25	4.383
29	4.378
33	4.372
37	4.366

DENSITY : 2622.5 KG/M<sup>3</sup>

INSTRUMENT DELAY FOR P-WAVE : 6.20000E-06 SEC.

INSTRUMENT DELAY FOR S-WAVE : 1.13000E-05 SEC.

Table C:3.13  $day\#$ ,  $t_p$ ,  $t_s$ ,  $V_p$ ,  $V_s$ ,  $\nu$ ,  $E_d$ ,  $K_d$ , and  $G_d$  for survey # 4 at 425 days after the heater was turned on and 27 days after the heater was turned off, in cross section M8-M9.



PROFILE AND FILE NAME : M8-M9 SURUC.5

DATE FOR FIELD WORK : 4-5 AUG,1980 DAYS AFTER HEATER TURN ON : 711 PROCESS DATE : 21 JAN,1981

LINE #	P-TIME (SEC)	S-TIME (SEC)	P-VELOCITY (M/SEC)	S-VELOCITY (M/SEC)	POISS.RATIO	YOUNGS MOD (PA)	BULK MOD (PA)	SHEAR MOD (PA)
1	7.56000E-04	1.27530E-03	5890.9	3494.46	.228536	7.86853E+10	4.83092E+10	3.20240E+10
3	7.55800E-04	1.27340E-03	5889.81	3498.14	.227496	7.87843E+10	4.81855E+10	3.20915E+10
5	7.55900E-04	1.27470E-03	5883.69	3491.37	.22825	7.85280E+10	4.81618E+10	3.19674E+10
7	7.60300E-04	1.28060E-03	5846.7	3473.57	.227247	7.76656E+10	4.74578E+10	3.15422E+10
9	7.53400E-04	1.28200E-03	5898.02	3468.17	.235742	7.79603E+10	4.91694E+10	3.15439E+10
11	7.54700E-04	1.29420E-03	5883.77	3432.85	.241957	7.67646E+10	4.95813E+10	3.09047E+10
13	7.55200E-04	1.26690E-03	5875.83	3505.1	.223789	7.88592E+10	4.75839E+10	3.22193E+10
15	7.57800E-04	1.27540E-03	5851.52	3479.15	.226584	7.78736E+10	4.74696E+10	3.17441E+10
17	7.56900E-04	1.27740E-03	5854.54	3471.29	.228921	7.76696E+10	4.77534E+10	3.16007E+10
19	7.64700E-04	1.29810E-03	5791.69	3413.9	.233778	7.54194E+10	4.72159E+10	3.05644E+10
21	7.53900E-04	1.27230E-03	5871.34	3481.36	.228895	7.81194E+10	4.80252E+10	3.17844E+10
23	7.47100E-04	1.26490E-03	5921.18	3499.52	.231594	7.91098E+10	4.91233E+10	3.21168E+10
25	7.47300E-04	1.26460E-03	5914.18	3497.17	.231174	7.89764E+10	4.89638E+10	3.20736E+10
27	7.44300E-04	1.27720E-03	5935.51	3460.78	.242467	7.80509E+10	5.05118E+10	3.14097E+10
29	7.46700E-04	1.26780E-03	5912.22	3484.28	.233932	7.85712E+10	4.92175E+10	3.18377E+10
31	7.50700E-04	1.27470E-03	5875.08	3462.09	.234005	7.75779E+10	4.86086E+10	3.14334E+10
33	7.53500E-04	1.27790E-03	5859.39	3451.76	.233005	7.70533E+10	4.80990E+10	3.12462E+10
35	7.61200E-04	1.30950E-03	5788.08	3366.2	.244452	7.39611E+10	4.82369E+10	2.97163E+10
37	7.51100E-04	1.27880E-03	5861.19	3444.58	.236195	7.69315E+10	4.86038E+10	3.11162E+10

LINE #	DISTANCE (M)
1	4.417
3	4.415
5	4.411
7	4.409
9	4.407
11	4.404
13	4.401
15	4.398
17	4.395
19	4.393
21	4.39
23	4.387
25	4.383
27	4.381
29	4.378
31	4.374
33	4.372
35	4.37
37	4.366

DENSITY : 2622.5 KG/M-3

INSTRUMENT DELAY FOR P-WAVE : 6.20000E-06 SEC.

INSTRUMENT DELAY FOR S-WAVE : 1.13000E-06 SEC.

Table C:3.14  $day\#$ ,  $t_p$ ,  $t_s$ ,  $V_p$ ,  $V_s$ ,  $\nu$ ,  $E_d$ ,  $K_d$ , and  $G_d$  for survey # 5 at day 711 after the heater was turned on and 313 days after the heater was turned off, in cross section M8-M9.

PROFILE AND FILE NAME : M6-M9 SURVD.1

DATE FOR FIELD WORK : 13 JULY,1978 DAYS AFTER HEATER TURN ON : -42 PROCESS DATE : 21 JAN,1981

LINE #	P-TIME (SEC)	S-TIME (SEC)	P-VELOCITY (M/SEC)	S-VELOCITY (M/SEC)	POISS.RATIO	YOUNGS MOD (PA)	BULK MOD (PA)	SHEAR MOD (PA)
1	4.78000E-04	8.15900E-04	5881.73	3448.02	.237991	7.72376E+10	4.91317E+10	3.11947E+10
5	4.78000E-04	8.24000E-04	5890.21	3419.47	.24583	7.64048E+10	5.01008E+10	3.06642E+10
9	4.81300E-04	8.02700E-04	5859.82	3517.82	.218268	7.90742E+10	4.67787E+10	3.24535E+10
13	4.84000E-04	8.11000E-04	5835.08	3486.31	.222425	7.79290E+10	4.67916E+10	3.18748E+10
17	4.82000E-04	8.02200E-04	5868.01	3530.16	.216406	7.95082E+10	4.67266E+10	3.26816E+10
21	4.92200E-04	7.76100E-04	5755.14	3657.17	.161342	8.14694E+10	4.00942E+10	3.50756E+10
25	4.87300E-04	8.09400E-04	5817.92	3507.08	.214607	7.83561E+10	4.57592E+10	3.22557E+10
29	4.86800E-04	8.15800E-04	5830.21	3482.91	.222547	7.77849E+10	4.67255E+10	3.18126E+10
33	4.81700E-04	8.20900E-04	5901.16	3465.91	.236696	7.79189E+10	4.93212E+10	3.15029E+10
37	4.88300E-04	7.63300E-04	5928.67	3736.7	.151108	8.43021E+10	4.02714E+10	3.06178E+10

LINE #	DISTANCE (M)
1	2.775
5	2.779
9	2.784
13	2.788
17	2.792
21	2.797
25	2.799
29	2.802
33	2.806
37	2.81

DENSITY : 2622.5 KG/M<sup>3</sup>

INSTRUMENT DELAY FOR P-WAVE : 6.20000E-06 SEC.

INSTRUMENT DELAY FOR S-WAVE : 1.13000E-05 SEC.

Table C:3.15  $day\#$ ,  $t_p$ ,  $t_s$ ,  $V_p$ ,  $V_s$ ,  $\nu$ ,  $E_d$ ,  $K_d$ , and  $G_d$  for survey # 1 at 42 days before heater was turned on in cross section M6-M9.

PROFILE AND FILE NAME : M6-M9 SURVD.2

DATE FOR FIELD WORK : 21 DEC,1978 DAYS AFTER HEATER TURN ON : 119 PROCESS DATE : 21 JAN,1981

LINE #	P-TIME (SEC)	S-TIME (SEC)	P-VELOCITY (M/SEC)	S-VELOCITY (M/SEC)	POISS.RATIO	YOUNGS MOD (PA)	BULK MOD (PA)	SHEAR MOD (PA)
5	4.72900E-04	8.14600E-04	5954.57	3459.48	.245242	7.81665E+10	5.11377E+10	3.13861E+10
9	4.74000E-04	8.21400E-04	5939.83	3436.61	.24841	7.73328E+10	5.12293E+10	3.09725E+10
13	4.75100E-04	8.09900E-04	5945.83	3491.11	.236935	7.90713E+10	5.00961E+10	3.19626E+10
17	4.74100E-04	8.07500E-04	5967.09	3506.66	.236231	7.97318E+10	5.03798E+10	3.22479E+10
21	4.82500E-04	8.28400E-04	5872.35	3423.08	.242665	7.63720E+10	4.94634E+10	3.07291E+10
25	4.80000E-04	8.24200E-04	5907.56	3443.23	.24275	7.72789E+10	5.00674E+10	3.10919E+10
29	4.79900E-04	8.13400E-04	5915.14	3493.33	.232212	7.88697E+10	4.90872E+10	3.20033E+10
33	4.78200E-04	8.21600E-04	5944.92	3462.92	.243219	7.81946E+10	5.07532E+10	3.14484E+10
37	4.82900E-04	8.36700E-04	5894.69	3404.41	.249756	7.59721E+10	5.05987E+10	3.03948E+10

LINE #	DISTANCE (M)
5	2.779
9	2.784
13	2.788
17	2.792
21	2.797
25	2.799
29	2.802
33	2.806
37	2.81

DENSITY : 2622.5 KG/M<sup>3</sup>

INSTRUMENT DELAY FOR P-WAVE : 6.20000E-06 SEC.

INSTRUMENT DELAY FOR S-WAVE : 1.13000E-05 SEC.

Table C:3.16  $day\#$ ,  $t_p$ ,  $t_s$ ,  $V_p$ ,  $V_s$ ,  $\nu$ ,  $E_d$ ,  $K_d$ , and  $G_d$  for survey # 2 at 119 days after the heater was turned on in cross section M6-M9.

PROFILE AND FILE NAME : M6-M9 SURVD.3

DATE FOR FIELD WORK : 2 AUG,1979 DAYS AFTER HEATER TURN ON : 343 PROCESS DATE : 21 JAN,1981

LINE #	P-TIME (SEC)	S-TIME (SEC)	P-VELOCITY (M/SEC)	S-VELOCITY (M/SEC)	POISS.RATIO	YOUNGS MOD (PA)	BULK MOD (PA)	SHEAR MOD (PA)
5	4.73000E-04	8.07700E-04	5953.3	3489.45	.238319	7.90847E+10	5.03696E+10	3.19323E+10
9	4.75200E-04	8.14800E-04	5936.03	3464.84	.241618	7.81808E+10	5.04298E+10	3.14834E+10
13	4.75300E-04	8.15800E-04	5943.3	3465.51	.242424	7.82616E+10	5.06399E+10	3.14955E+10
17	4.74600E-04	8.04300E-04	5960.72	3520.81	.232082	8.01068E+10	4.98329E+10	3.25087E+10
21	4.82300E-04	8.30800E-04	5874.82	3413.06	.245261	7.60839E+10	4.97790E+10	3.05494E+10
25	4.81500E-04	8.26100E-04	5888.91	3435.2	.242105	7.68790E+10	4.96837E+10	3.09470E+10
29	4.79800E-04	8.11500E-04	5916.39	3501.62	.230427	7.91299E+10	4.89230E+10	3.21555E+10
33	4.77400E-04	8.18600E-04	5955.01	3475.78	.241648	7.86773E+10	5.07559E+10	3.16826E+10
37	4.82500E-04	8.29800E-04	5899.64	3433.11	.243995	7.69023E+10	5.00656E+10	3.09094E+10

LINE #	DISTANCE (M)
5	2.779
9	2.784
13	2.788
17	2.792
21	2.797
25	2.799
29	2.802
33	2.806
37	2.81

DENSITY : 2622.5 KG/M<sup>3</sup>

INSTRUMENT DELAY FOR P-WAVE : 6.20000E-06 SEC.

INSTRUMENT DELAY FOR S-WAVE : 1.13000E-05 SEC.

Table C:3.17  $day\#$ ,  $t_p$ ,  $t_s$ ,  $V_p$ ,  $V_s$ ,  $\nu$ ,  $E_d$ ,  $K_d$ , and  $G_d$  for survey # 3 at 343 days after the heater was turned on in cross section M6-M9.

PROFILE AND FILE NAME : M6-M9 SURVD.4

DATE FOR FIELD WORK : 24 OCT,1979 DAYS AFTER HEATER TURN ON : 426 PROCESS DATE : 21 JAN,1981

LINE #	P-TIME (SEC)	S-TIME (SEC)	P-VELOCITY (M/SEC)	S-VELOCITY (M/SEC)	POISS.RATIO	YOUNGS MOD (PA)	BULK MOD (PA)	SHEAR MOD (PA)
5	4.74200E-04	8.04500E-04	5938.03	3503.53	.23299	7.93810E+10	4.95494E+10	3.21005E+10
9	4.78100E-04	8.17300E-04	5899.55	3454.09	.239207	7.75457E+10	4.95575E+10	3.12884E+10
13	4.82600E-04	8.17500E-04	5852.23	3458.2	.23173	7.72611E+10	4.79997E+10	3.13628E+10
17	4.78700E-04	8.06300E-04	5909	3511.95	.226916	7.93701E+10	4.84406E+10	3.23454E+10
21	4.82900E-04	8.38200E-04	5867.48	3382.51	.251114	7.50795E+10	5.02771E+10	3.00051E+10
25	4.82300E-04	8.28800E-04	5879.02	3423.85	.243373	7.64499E+10	4.96504E+10	3.07430E+10
29	4.82000E-04	8.03100E-04	5889.03	3538.77	.217415	7.99630E+10	4.71616E+10	3.28413E+10
33	4.77500E-04	8.18000E-04	5953.74	3478.37	.240898	7.87468E+10	5.06536E+10	3.17298E+10
37	4.83200E-04	8.08300E-04	5890.99	3525.72	.220947	7.96046E+10	4.75444E+10	3.25096E+10

LINE # DISTANCE

(M)

5	2.779
9	2.784
13	2.788
17	2.792
21	2.797
25	2.799
29	2.802
33	2.806
37	2.81

DENSITY : 2622.5 KG/M<sup>3</sup>

INSTRUMENT DELAY FOR P-WAVE : 6.20000E-06 SEC.

INSTRUMENT DELAY FOR S-WAVE : 1.13000E-05 SEC.

Table C:3.18  $day\#$ ,  $t_p$ ,  $t_s$ ,  $V_p$ ,  $V_s$ ,  $\nu$ ,  $E_d$ ,  $K_d$ , and  $G_d$  for survey # 4 at 426 days after the heater was turned on and 28 days after the heater was turned off, in cross section M6-M9.

PROFILE AND FILE NAME : M6-M9 SURUD.5

DATE FOR FIELD WORK : 3-4 AUG,1980 DAYS AFTER HEATER TURN ON : 710 PROCESS DATE : 21 JAN,1981

LINE #	P-TIME (SEC)	S-TIME (SEC)	P-VELOCITY (M/SEC)	S-VELOCITY (M/SEC)	POISS.RATIO	YOUNGS MOD (PA)	BULK MOD (PA)	SHEAR MOD (PA)
1	4.81700E-04	8.32800E-04	5835.86	3377.87	.248084	7.46965E+10	4.94190E+10	2.99245E+10
5	4.74800E-04	8.20300E-04	5930.43	3435.11	.247541	7.72113E+10	5.09729E+10	3.09454E+10
9	4.80000E-04	8.13700E-04	5875.9	3469.59	.232346	7.78099E+10	4.84518E+10	3.15698E+10
13	4.88200E-04	8.33100E-04	5784.23	3392.55	.237802	7.47222E+10	4.74973E+10	3.01834E+10
17	4.78100E-04	8.07700E-04	5916.51	3505.78	.229459	7.92552E+10	4.88251E+10	3.22318E+10
21	4.88400E-04	8.67800E-04	5800.5	3265.62	.267982	7.09233E+10	5.09467E+10	2.79670E+10
25	4.82900E-04	8.62600E-04	5871.62	3287.91	.271601	7.21003E+10	5.26128E+10	2.83502E+10
29	4.81900E-04	8.25700E-04	5890.27	3440.57	.241061	7.70547E+10	4.95964E+10	3.10439E+10
33	4.77000E-04	8.18700E-04	5960.07	3475.36	.242409	7.87060E+10	5.09245E+10	3.16748E+10
37	4.82500E-04	8.27900E-04	5899.64	3441.1	.242187	7.71483E+10	4.98736E+10	3.10534E+10

LINE #	DISTANCE (M)
1	2.775
5	2.779
9	2.784
13	2.788
17	2.792
21	2.797
25	2.799
29	2.802
33	2.806
37	2.81

DENSITY : 8622.5 KG/M<sup>3</sup>

INSTRUMENT DELAY FOR P-WAVE : 6.20000E-06 SEC.

INSTRUMENT DELAY FOR S-WAVE : 1.13000E-05 SEC.

Table C:3.19  $day\#$ ,  $t_p$ ,  $t_s$ ,  $V_p$ ,  $V_s$ ,  $\nu$ ,  $E_d$ ,  $K_d$ , and  $G_d$  for survey # 5 at 710 days after the heater was turned on and 312 days after the heater was turned off, in cross section M6-M9.

PROFILE AND FILE NAME : M8-M6 SURVE.1

DATE FOR FIELD WORK : 11 JULY,1978 DAYS AFTER HEATER TURN ON : -44 PROCESS DATE : 20 JAN,1981

LINE #	P-TIME (SEC)	S-TIME (SEC)	P-VELOCITY (M/SEC)	S-VELOCITY (M/SEC)	POISS.RATIO	YOUNGS MOD (PA)	BULK MOD (PA)	SHEAR MOD (PA)
1	7.18200E-04	1.24100E-03	5877.81	3403.27	.247844	7.58051E+10	5.01046E+10	3.03744E+10
3	7.13100E-04	1.25550E-03	5921.63	3364.41	.261664	7.49044E+10	5.23801E+10	2.96848E+10
5	7.11200E-04	1.21000E-03	5936.17	3491.28	.235585	7.89928E+10	4.97909E+10	3.19658E+10
7	7.17800E-04	1.23630E-03	5879.71	3415.51	.245349	7.61987E+10	4.98712E+10	3.05933E+10
9	7.17400E-04	1.30660E-03	5883.01	3230.14	.284212	7.02789E+10	5.42808E+10	2.73626E+10
11	7.25600E-04	1.25450E-03	5813.18	3363.9	.248282	7.40874E+10	4.90546E+10	2.96757E+10
13	7.29800E-04	1.27510E-03	5778.05	3308.28	.256148	7.21090E+10	4.92846E+10	2.87025E+10
15	7.22100E-04	1.29280E-03	5841.6	3263.36	.27317	7.11153E+10	5.22530E+10	2.79284E+10
17	7.16500E-04	1.32540E-03	5886.25	3181.65	.293622	6.86841E+10	5.54678E+10	2.65472E+10
19	7.15300E-04	1.25380E-03	5896.21	3364.99	.258487	7.47414E+10	5.15785E+10	2.96950E+10
21	7.17200E-04	1.25590E-03	5880.45	3359.31	.257778	7.44475E+10	5.12254E+10	2.95949E+10
23	7.16800E-04	1.23500E-03	5882.35	3415.87	.245613	7.62309E+10	4.99442E+10	3.05998E+10
25	7.18500E-04	1.21290E-03	5868.31	3478.69	.229105	7.80130E+10	4.79970E+10	3.17357E+10
27	7.11100E-04	1.27420E-03	5928.5	3309.05	.273739	7.31531E+10	5.38855E+10	2.87159E+10
29	7.11400E-04	1.22280E-03	5924.56	3448.62	.243769	7.75845E+10	5.04651E+10	3.11893E+10
31	7.11800E-04	1.28940E-03	5918.37	3267.35	.280802	7.17165E+10	5.45296E+10	2.79967E+10
33	7.09100E-04	1.22380E-03	5941.1	3444.12	.246914	7.75782E+10	5.10881E+10	3.11081E+10
35	7.14200E-04	1.29690E-03	5896.89	3247.51	.282344	7.09335E+10	5.43161E+10	2.76577E+10
37	7.14900E-04	1.21940E-03	5889.66	3455.01	.237657	7.74898E+10	4.92293E+10	3.13051E+10
39	7.07500E-04	1.21230E-03	5950.38	3474.6	.241304	7.86021E+10	5.06401E+10	3.16611E+10

LINE # DISTANCE

LINE #	DISTANCE (M)
1	4.185
3	4.186
5	4.185
7	4.184
9	4.184
11	4.182
13	4.181
15	4.182
17	4.181
19	4.181
21	4.181
23	4.18
25	4.18
27	4.179
29	4.178
31	4.176
33	4.176
35	4.175
37	4.174
39	4.173

DENSITY : 2622.5 KG/M<sup>3</sup>

INSTRUMENT DELAY FOR P-WAVE : 6.20000E-06 SEC.

INSTRUMENT DELAY FOR S-WAVE : 1.13000E-05 SEC.

Table C:3.20  $day\#$ ,  $t_p$ ,  $t_s$ ,  $V_p$ ,  $V_s$ ,  $\nu$ ,  $E_d$ ,  $K_d$ , and  $G_d$ , for survey # 1 at at day -44 before the heater was turned on in cross section M8-M6.

PROFILE AND FILE NAME : M8-M6 SURVE.2

DATE FOR FIELD WORK : 17 AUG,1978 DAYS AFTER HEATER TURN ON : -7 PROCESS DATE : 20 JAN,1981

LINE #	P-TIME (SEC)	S-TIME (SEC)	P-VELOCITY (M/SEC)	S-VELOCITY (M/SEC)	POISS.RATIO	YOUNGS MOD (PA)	BULK MOD (PA)	SHEAR MOD (PA)
1	7.19600E-04	1.24610E-03	5866.27	3389.21	.249486	7.52791E+10	5.00831E+10	3.01240E+10
2	7.14700E-04	1.28930E-03	5906.85	3274.65	.278146	7.18878E+10	5.40053E+10	2.81219E+10
3	7.12200E-04	1.26020E-03	5929.18	3351.75	.26518	7.45488E+10	5.29120E+10	2.94618E+10
4	7.12700E-04	1.26180E-03	5923.57	3346.66	.265575	7.43458E+10	5.28568E+10	2.93724E+10
5	7.10500E-04	1.26340E-03	5942.07	3342.38	.268577	7.43319E+10	5.35326E+10	2.92974E+10
6	7.14400E-04	1.33760E-03	5907.94	3154.64	.300581	6.78864E+10	5.67370E+10	2.60985E+10
7	7.15400E-04	1.23790E-03	5899.61	3411.05	.248915	7.62177E+10	5.05922E+10	3.05136E+10
8	7.18600E-04	1.23920E-03	5873.1	3407.44	.2463	7.58971E+10	4.98602E+10	3.04490E+10
9	7.18000E-04	1.27790E-03	5878.06	3303.33	.2692	7.26407E+10	5.24558E+10	2.86167E+10
10	7.20900E-04	1.24710E-03	5852.81	3384.85	.248724	7.50398E+10	4.97725E+10	3.00466E+10
11	7.24200E-04	1.28760E-03	5824.51	3276.66	.268495	7.14326E+10	5.14262E+10	2.81565E+10
12	7.25800E-04	1.24770E-03	5810.17	3381.59	.24387	7.46041E+10	4.85457E+10	2.99887E+10
13	7.25400E-04	1.20360E-03	5813.4	3506.67	.214016	7.82995E+10	4.56316E+10	3.22481E+10
14	7.20200E-04	1.21980E-03	5857.14	3460.49	.231877	7.73727E+10	4.80953E+10	3.14044E+10
15	7.20500E-04	1.23280E-03	5854.68	3423.66	.240169	7.62443E+10	4.89063E+10	3.07395E+10
16	7.16700E-04	1.27240E-03	5884.59	3315.36	.267489	7.30720E+10	5.23789E+10	2.88255E+10
17	7.11300E-04	1.25960E-03	5929.65	3349.35	.265728	7.44746E+10	5.29830E+10	2.94197E+10
18	7.10700E-04	1.25370E-03	5934.71	3365.26	.263034	7.50236E+10	5.27667E+10	2.96998E+10
19	7.12100E-04	1.28380E-03	5922.94	3285.66	.277738	7.23489E+10	5.42519E+10	2.83113E+10
20	7.12900E-04	1.22810E-03	5916.23	3436.06	.245497	7.71277E+10	5.05087E+10	3.09626E+10
21	7.15700E-04	1.22990E-03	5892.88	3430.99	.243586	7.67819E+10	4.99075E+10	3.08712E+10
22	7.14000E-04	1.23040E-03	5907.04	3429.58	.245753	7.68527E+10	5.03792E+10	3.08459E+10
23	7.14400E-04	1.20300E-03	5902.29	3507.59	.227005	7.91791E+10	4.83398E+10	3.22652E+10
24	7.14600E-04	1.22660E-03	5900.62	3439.48	.242684	7.71066E+10	4.99428E+10	3.10242E+10
25	7.11600E-04	1.25730E-03	5925.72	3354.73	.264159	7.46215E+10	5.27344E+10	2.95143E+10
26	7.10700E-04	1.25680E-03	5933.29	3356.08	.264766	7.47172E+10	5.29382E+10	2.95380E+10
27	7.07600E-04	1.22040E-03	5958.08	3456.29	.246401	7.80951E+10	5.13245E+10	3.13292E+10
28	7.07000E-04	1.19400E-03	5963.18	3533.44	.229457	8.05109E+10	4.95984E+10	3.27424E+10
29	7.15000E-04	1.22160E-03	5894.47	3452.04	.238995	7.74401E+10	4.94499E+10	3.12512E+10
30	7.08000E-04	1.21840E-03	5951.84	3460.36	.244692	7.81718E+10	5.10311E+10	3.14020E+10
31	7.10100E-04	1.21520E-03	5932.66	3468.73	.24029	7.82724E+10	5.02306E+10	3.15541E+10
32	7.05700E-04	1.20360E-03	5969.98	3502.47	.237579	7.96284E+10	5.05729E+10	3.21710E+10
33	7.07600E-04	1.22540E-03	5953.81	3439.59	.24953	7.75361E+10	5.15937E+10	3.10261E+10
34	7.12100E-04	1.19840E-03	5914.44	3516.97	.226486	7.95694E+10	4.84859E+10	3.24380E+10
35	7.12400E-04	1.22820E-03	5911.92	3430.85	.246103	7.69312E+10	5.05002E+10	3.08687E+10
36	7.10500E-04	1.25590E-03	5926.45	3353.69	.264462	7.45927E+10	5.27818E+10	2.94958E+10
37	7.08600E-04	1.24870E-03	5942.48	3373.2	.262301	7.53433E+10	5.28218E+10	2.98401E+10
38	7.08900E-04	1.22200E-03	5938.52	3446.77	.245996	7.76400E+10	5.09441E+10	3.11558E+10
39	7.07000E-04	1.22100E-03	5954.62	3449.62	.247432	7.78581E+10	5.13776E+10	3.12073E+10

Table C:3.21  $day\#$ ,  $t_p$ ,  $t_s$ ,  $V_p$ ,  $V_s$ ,  $\nu$ ,  $E_d$ ,  $K_d$ , and  $G_d$ , for survey # 2 at day -7 before the heater was turned on in cross section M8-M6.



LINE # DISTANCE

(M)

1	4.185
2	4.185
3	4.186
4	4.185
5	4.185
6	4.184
7	4.184
8	4.184
9	4.184
10	4.183
11	4.182
12	4.181
13	4.181
14	4.182
15	4.182
16	4.181
17	4.181
18	4.181
19	4.181
20	4.181
21	4.181
22	4.181
23	4.18
24	4.18
25	4.18
26	4.18
27	4.179
28	4.179
29	4.178
30	4.177
31	4.176
32	4.176
33	4.176
34	4.175
35	4.175
36	4.174
37	4.174
38	4.173
39	4.173

DENSITY : 2622.5 KG/M<sup>3</sup>

INSTRUMENT DELAY FOR P-WAVE : 6.20000E-06 SEC.

INSTRUMENT DELAY FOR S-WAVE : 1.13000E-05 SEC.

PROFILE AND FILE NAME : M8-M6 SURVE.3

DATE FOR FIELD WORK : 30 AUG.,1978 DAYS AFTER HEATER TURN ON : 6 PROCESS DATE : 20 JAN.,1981

LINE #	P-TIME (SEC)	S-TIME (SEC)	P-VELOCITY (M/SEC)	S-VELOCITY (M/SEC)	POISS.RATIO	YOUNGS MOD (PA)	BULK MOD (PA)	SHEAR MOD (PA)
3	7.15700E-04	1.32950E-03	5899.93	3175.54	.296076	6.85507E+10	5.60264E+10	2.64455E+10
5	7.10500E-04	1.29610E-03	5942.07	3257.32	.285204	7.15216E+10	5.54957E+10	2.78250E+10
7	7.15100E-04	1.28970E-03	5902.1	3272.84	.277985	7.17994E+10	5.38998E+10	2.80909E+10
9	7.14900E-04	1.25430E-03	5903.77	3366.05	.259178	7.48296E+10	5.17876E+10	2.97137E+10
11	7.20300E-04	1.27700E-03	5856.32	3304.1	.266524	7.25213E+10	5.17692E+10	2.86300E+10
13	7.18200E-04	1.24690E-03	5872.19	3383.78	.25144	7.51554E+10	5.03939E+10	3.00276E+10
15	7.11500E-04	1.22980E-03	5929.39	3432.09	.248075	7.71087E+10	5.10130E+10	3.08910E+10
17	7.07800E-04	1.23640E-03	5959.24	3412.78	.255984	7.67268E+10	5.24055E+10	3.05445E+10
19	7.08300E-04	1.21470E-03	5954.99	3474.32	.241975	7.86319E+10	5.07909E+10	3.16560E+10
21	7.11800E-04	1.21200E-03	5925.45	3482.14	.236244	7.86214E+10	4.96806E+10	3.17985E+10
23	7.12900E-04	1.21280E-03	5914.82	3478.98	.235524	7.84335E+10	4.94270E+10	3.17410E+10
25	7.11500E-04	1.21310E-03	5926.56	3478.12	.237321	7.85084E+10	4.98126E+10	3.17251E+10

LINE # DISTANCE

(M)

3	4.186
5	4.185
7	4.184
9	4.184
11	4.182
13	4.181
15	4.182
17	4.181
19	4.181
21	4.181
23	4.18
25	4.18

DENSITY : 2622.5 KG/M<sup>3</sup>

INSTRUMENT DELAY FOR P-WAVE : 6.20000E-06 SEC.

INSTRUMENT DELAY FOR S-WAVE : 1.13000E-05 SEC.

Table C:3.22  $day\#$ ,  $t_p$ ,  $t_s$ ,  $V_p$ ,  $V_s$ ,  $\nu$ ,  $E_d$ ,  $K_d$ , and  $G_d$ , for survey # 3 at day 6 after the heater was turned on in cross section M8-M6.

PROFILE AND FILE NAME : M8-M6 SURVE.4

DATE FOR FIELD WORK : 8 SEP.,1978 DAYS AFTER HEATER TURN ON : 15 PROCESS DATE : 20 JAN.,1981

LINE #	P-TIME (SEC)	S-TIME (SEC)	P-VELOCITY (M/SEC)	S-VELOCITY (M/SEC)	POISS.RATIO	YOUNGS MOD (PA)	BULK MOD (PA)	SHEAR MOD (PA)
3	7.16500E-04	1.24850E-03	5893.28	3383.45	.254162	7.53040E+10	5.10527E+10	3.00216E+10
5	7.11300E-04	1.22740E-03	5935.33	3441.33	.246792	7.74447E+10	5.09756E+10	3.10576E+10
7	7.13300E-04	1.23640E-03	5917.13	3415.23	.250224	7.64846E+10	5.10355E+10	3.05883E+10
9	7.13100E-04	1.25480E-03	5918.8	3364.7	.261267	7.48935E+10	5.22855E+10	2.96898E+10
11	7.14900E-04	1.26180E-03	5900.95	3344.26	.263421	7.41129E+10	5.22114E+10	2.93303E+10
13	7.14300E-04	1.25580E-03	5904.53	3359.58	.260637	7.46287E+10	5.19634E+10	2.95996E+10
15	7.09200E-04	1.23180E-03	5948.79	3426.46	.251756	7.70829E+10	5.17521E+10	3.07899E+10
17	7.08900E-04	1.24890E-03	5949.91	3378.31	.262114	7.55516E+10	5.29327E+10	2.99306E+10
19	7.10000E-04	1.25270E-03	5940.61	3367.97	.263165	7.51524E+10	5.28867E+10	2.97476E+10
21	7.09600E-04	1.22330E-03	5943.99	3449.67	.246056	7.77746E+10	5.10444E+10	3.12083E+10
23	7.12400E-04	1.22470E-03	5919	3444.87	.243885	7.74230E+10	5.03829E+10	3.11215E+10
25	7.12800E-04	1.27850E-03	5915.65	3298.61	.274389	7.27293E+10	5.37276E+10	2.85350E+10

LINE #	DISTANCE (M)
3	4.186
5	4.185
7	4.184
9	4.184
11	4.182
13	4.181
15	4.182
17	4.181
19	4.181
21	4.181
23	4.18
25	4.18

DENSITY : 2622.5 KG/M-3

INSTRUMENT DELAY FOR P-WAVE : 6.20000E-06 SEC.

INSTRUMENT DELAY FOR S-WAVE : 1.13000E-05 SEC.

Table C:3.23  $day\#$  ,  $t_p$  ,  $t_s$  ,  $V_p$  ,  $V_s$  ,  $\nu$  ,  $E_d$  ,  $K_d$  , and  $G_d$  , for survey # 4 at day 15 after the heater was turned on in cross section M8-M6.

PROFILE AND FILE NAME : M8-M6 SURVEY.5

DATE FOR FIELD WORK : 13-14 SEP., 1978 DAYS AFTER HEATER TURN ON : 20 PROCESS DATE : 20 JAN, 1981

LINE #	P-TIME (SEC)	S-TIME (SEC)	P-VELOCITY (M/SEC)	S-VELOCITY (M/SEC)	POISS.RATIO	YOUNGS MOD. (PA)	BULK MOD (PA)	SHEAR MOD (PA)
3	7.14800E-04	1.22110E-03	5907.42	3460.08	.238891	7.77946E+10	4.96565E+10	3.13969E+10
5	7.09700E-04	1.22110E-03	5948.83	3459.25	.244549	7.81126E+10	5.09639E+10	3.13819E+10
7	7.12600E-04	1.22760E-03	5922.99	3439.94	.245508	7.73025E+10	5.06253E+10	3.10325E+10
9	7.11300E-04	1.21950E-03	5933.91	3463	.241754	7.81064E+10	5.04082E+10	3.14500E+10
11	7.13800E-04	1.21130E-03	5910.12	3485	.233474	7.85744E+10	4.91348E+10	3.18508E+10
13	7.13300E-04	1.21290E-03	5912.88	3479.53	.235133	7.84331E+10	4.93538E+10	3.17509E+10
15	7.07600E-04	1.20820E-03	5962.36	3494.03	.238487	7.93029E+10	5.05411E+10	3.20161E+10
17	7.07400E-04	1.20730E-03	5962.63	3495.82	.238115	7.93605E+10	5.05059E+10	3.20489E+10
19	7.09500E-04	1.21290E-03	5944.83	3479.53	.239452	7.87074E+10	5.03473E+10	3.17509E+10
21	7.09300E-04	1.21550E-03	5946.52	3472.01	.241381	7.84899E+10	5.05826E+10	3.16139E+10
23	7.13000E-04	1.20930E-03	5913.98	3489.15	.233034	7.87335E+10	4.91533E+10	3.19267E+10
25	7.15800E-04	1.23840E-03	5890.64	3406.41	.248797	7.60029E+10	5.04260E+10	3.04304E+10
27	7.06500E-04	1.22210E-03	5967.44	3451.44	.248661	7.80171E+10	5.17344E+10	3.12403E+10
29	7.09300E-04	1.24890E-03	5942.26	3375.89	.261714	7.54194E+10	5.27513E+10	2.98876E+10
31	7.09700E-04	1.24720E-03	5936.03	3378.91	.260342	7.54724E+10	5.24861E+10	2.99412E+10
33	7.06900E-04	1.22240E-03	5959.75	3448.11	.248417	7.78514E+10	5.15743E+10	3.11800E+10
35	7.11300E-04	1.21870E-03	5921.15	3457.84	.241234	7.78413E+10	5.01362E+10	3.13564E+10
37	7.05900E-04	1.20440E-03	5965.41	3498.45	.237886	7.94653E+10	5.05285E+10	3.20072E+10

LINE #	DISTANCE (M)
3	4.186
5	4.185
7	4.184
9	4.184
11	4.182
13	4.181
15	4.182
17	4.181
19	4.181
21	4.181
23	4.18
25	4.18
27	4.179
29	4.178
31	4.176
33	4.176
35	4.175
37	4.174

DENSITY : 2022.5 KG/M<sup>3</sup>

INSTRUMENT DELAY FOR P-WAVE : 6.20000E-06 SEC.

INSTRUMENT DELAY FOR S-WAVE : 1.13000E-05 SEC.

Table C:3.24  $day\#$ ,  $t_p$ ,  $t_s$ ,  $V_p$ ,  $V_s$ ,  $\nu$ ,  $E_d$ ,  $K_d$ , and  $G_d$ , for survey # 5 at day 20 after the heater was turned on in cross section M8-M6.

PROFILE AND FILE NAME : M8-M6 SURVE.6

DATE FOR FIELD WORK : 13 DEC.,1978 DAYS AFTER HEATER TURN ON : 111 PROCESS DATE : 20 JAN,1981

LINE #	P-TIME (SEC)	S-TIME (SEC)	P-VELOCITY (M/SEC)	S-VELOCITY (M/SEC)	POISS.RATIO	YOUNGS MOD (PA)	BULK MOD (PA)	SHEAR MOD (PA)
5	7.07000E-04	1.23520E-03	5971.75	3419.4	.256101	7.70316E+10	5.26389E+10	3.06630E+10
6	7.13800E-04	1.20230E-03	5912.94	3513.01	.227224	7.94382E+10	4.85369E+10	3.23650E+10
7	7.12200E-04	1.21560E-03	5926.35	3474.22	.23819	7.83874E+10	4.99009E+10	3.16540E+10
8	7.10700E-04	1.21180E-03	5938.96	3485.21	.237363	7.88318E+10	5.00259E+10	3.18548E+10
9	7.09800E-04	1.20860E-03	5946.56	3494.53	.236246	7.91822E+10	5.00354E+10	3.20253E+10
10	7.12300E-04	1.21070E-03	5924.09	3487.58	.234795	7.87749E+10	4.95056E+10	3.18980E+10
11	7.10000E-04	1.19890E-03	5942.03	3521.39	.229343	7.99551E+10	4.92352E+10	3.25194E+10
12	7.13300E-04	1.22720E-03	5912.88	3438.6	.244491	7.71795E+10	5.03437E+10	3.10085E+10
13	7.14500E-04	1.19470E-03	5902.87	3533.04	.220895	7.99320E+10	4.77312E+10	3.27350E+10
14	7.09400E-04	1.19120E-03	5947.1	3544.37	.224571	8.06877E+10	4.88255E+10	3.29453E+10
15	7.07300E-04	1.18740E-03	5964.91	3555.82	.22437	8.11966E+10	4.90977E+10	3.31585E+10
16	7.07300E-04	1.19180E-03	5963.49	3541.72	.227539	8.07623E+10	4.94030E+10	3.28960E+10
17	7.03400E-04	1.18900E-03	5996.84	3550.14	.230218	8.13239E+10	5.02405E+10	3.30527E+10
18	7.04600E-04	1.20590E-03	5986.54	3499.92	.24036	7.96009E+10	5.11548E+10	3.21241E+10
19	7.06600E-04	1.20780E-03	5969.45	3494.36	.239355	7.93736E+10	5.07547E+10	3.20221E+10
20	7.06900E-04	1.19440E-03	5966.89	3533.94	.229858	8.05597E+10	4.97020E+10	3.27516E+10
21	7.08600E-04	1.18940E-03	5952.45	3548.93	.224239	8.08738E+10	4.88792E+10	3.30302E+10
22	7.06100E-04	1.20010E-03	5973.71	3516.99	.234748	8.01063E+10	5.03334E+10	3.24383E+10
23	7.07400E-04	1.21260E-03	5961.21	3479.56	.241612	7.88462E+10	5.08578E+10	3.17515E+10
24	7.13700E-04	1.20150E-03	5908.13	3512.01	.226776	7.93640E+10	4.84121E+10	3.23466E+10
25	7.10400E-04	1.20870E-03	5935.81	3490.9	.235625	7.89780E+10	4.97892E+10	3.19587E+10
26	7.05600E-04	1.20640E-03	5976.55	3497.62	.23956	7.95348E+10	5.08977E+10	3.20819E+10
27	7.04400E-04	1.19770E-03	5985.39	3522.42	.235081	8.03754E+10	5.05661E+10	3.25385E+10
28	7.06000E-04	1.20310E-03	5971.71	3506.46	.236898	7.97659E+10	5.05202E+10	3.22443E+10
29	7.05400E-04	1.20460E-03	5975.4	3501.22	.23859	7.96362E+10	5.07735E+10	3.21479E+10
30	7.06000E-04	1.23340E-03	5968.85	3417.89	.256069	7.69617E+10	5.25843E+10	3.06359E+10
31	7.05100E-04	1.22550E-03	5975.1	3439.3	.252256	7.76925E+10	5.22668E+10	3.10210E+10
32	7.04500E-04	1.22000E-03	5980.24	3454.95	.249509	7.82291E+10	5.20505E+10	3.13040E+10
33	7.04700E-04	1.21370E-03	5978.53	3473.05	.245317	7.87859E+10	5.15582E+10	3.16329E+10
34	7.07200E-04	1.23000E-03	5955.78	3425.78	.252774	7.71148E+10	5.19867E+10	3.07776E+10
35	7.09000E-04	1.21810E-03	5940.52	3459.56	.243398	7.80545E+10	5.06975E+10	3.13876E+10
36	7.06500E-04	1.22480E-03	5960.3	3439.64	.250336	7.75886E+10	5.17954E+10	3.10271E+10

Table C:3.25  $day\#$ ,  $t_p$ ,  $t_s$ ,  $V_p$ ,  $V_s$ ,  $\nu$ ,  $E_d$ ,  $K_d$ , and  $G_d$ , for survey # 6 at day 111 after the heater was turned on in cross section M8-M6.

LINE #	DISTANCE (M)
5	4.185
6	4.184
7	4.184
8	4.184
9	4.184
10	4.183
11	4.182
12	4.181
13	4.181
14	4.182
15	4.182
16	4.181
17	4.181
18	4.181
19	4.181
20	4.181
21	4.181
22	4.181
23	4.18
24	4.18
25	4.18
26	4.18
27	4.179
28	4.179
29	4.178
30	4.177
31	4.176
32	4.176
33	4.176
34	4.175
35	4.175
36	4.174

DENSITY : 2622.6 KG/M<sup>3</sup>

INSTRUMENT DELAY FOR P-WAVE : 6.20000E-06 SEC.

INSTRUMENT DELAY FOR S-WAVE : 1.13000E-05 SEC.

PROFILE AND FILE NAME : M8-M6 SURVEY.7

DATE FOR FIELD WORK : 20 DEC,1978 DAYS AFTER HEATER TURN ON : 118 PROCESS DATE : 20 JAN,1981

LINE #	P-TIME (SEC)	S-TIME (SEC)	P-VELOCITY (M/SEC)	S-VELOCITY (M/SEC)	POISS.RATIO	YOUNGS MOD (PA)	BULK MOD (PA)	SHEAR MOD (PA)
3	7.14000E-04	1.18790E-03	5914.1	3557.71	.21645	8.07570E+10	4.74678E+10	3.31937E+10
5	7.05500E-04	1.24010E-03	5984.56	3405.76	.260502	7.66863E+10	5.33660E+10	3.04189E+10
7	7.08200E-04	1.21850E-03	5960.11	3465.87	.244536	7.84112E+10	5.11561E+10	3.15022E+10
9	7.06100E-04	1.20470E-03	5978	3505.95	.237859	7.98046E+10	5.07389E+10	3.22349E+10
11	7.08400E-04	1.20820E-03	5955.57	3494.03	.237577	7.92447E+10	5.03288E+10	3.20161E+10
13	7.06500E-04	1.20160E-03	5970.3	3512.56	.235307	7.99407E+10	5.03355E+10	3.23566E+10
15	7.01900E-04	1.19650E-03	6011.21	3528.52	.237157	8.07896E+10	5.12281E+10	3.26513E+10
17	7.01200E-04	1.19100E-03	6015.83	3544.12	.234212	8.13116E+10	5.09878E+10	3.29407E+10
19	7.02300E-04	1.22020E-03	6006.32	3458.52	.251989	7.85463E+10	5.27842E+10	3.13686E+10
21	7.02700E-04	1.20110E-03	6002.87	3514.04	.23933	8.02685E+10	5.13220E+10	3.23838E+10
23	7.06800E-04	1.20790E-03	5966.31	3493.23	.239195	7.93121E+10	5.06842E+10	3.20015E+10
25	7.06600E-04	1.21040E-03	5968.02	3485.95	.241069	7.91012E+10	5.09153E+10	3.18682E+10
27	7.03400E-04	1.20120E-03	5993.98	3512.06	.238599	8.01309E+10	5.10907E+10	3.23474E+10
29	7.04400E-04	1.21090E-03	5983.96	3482.83	.24385	7.91366E+10	5.14910E+10	3.18112E+10
31	7.04600E-04	1.19610E-03	5979.38	3524.65	.233751	8.03903E+10	5.03227E+10	3.25796E+10
33	7.04700E-04	1.22700E-03	5978.53	3435.06	.253591	7.75835E+10	5.24761E+10	3.09445E+10
35	7.09800E-04	1.23100E-03	5933.77	3422.97	.250632	7.68567E+10	5.13677E+10	3.07272E+10
37	7.04800E-04	1.21450E-03	5974.81	3469.08	.245718	7.86311E+10	5.15381E+10	3.15606E+10
39	7.04500E-04	1.23190E-03	5975.94	3418.81	.256734	7.70440E+10	5.27844E+10	3.06525E+10

LINE #	DISTANCE (M)
3	4.186
5	4.185
7	4.184
9	4.184
11	4.182
13	4.181
15	4.182
17	4.181
19	4.181
21	4.181
23	4.18
25	4.18
27	4.179
29	4.178
31	4.176
33	4.176
35	4.175
37	4.174
39	4.173

DENSITY : 2622.5 KG/M<sup>3</sup>

INSTRUMENT DELAY FOR P-WAVE : 6.20000E-06 SEC.

INSTRUMENT DELAY FOR S-WAVE : 1.13000E-05 SEC.

Table C:3.26  $day\#$ ,  $t_p$ ,  $t_s$ ,  $V_p$ ,  $V_s$ ,  $\nu$ ,  $E_d$ ,  $K_d$ , and  $G_d$ , for survey # 7 at day 118 after the heater was turned on in cross section M8-M6.

PROFILE AND FILE NAME : M8-M6 SURVE.REU

DATE FOR FIELD WORK : 21 DEC.,1978 DAYS AFTER HEATER TURN ON : 119 PROCESS DATE : 20 JAN,1981

LINE #	P-TIME (SEC)	S-TIME (SEC)	P-VELOCITY (M/SEC)	S-VELOCITY (M/SEC)	POISS.RATIO	YOUNGS MOD (PA)	BULK MOD (PA)	SHEAR MOD (PA)
11	7.10400E-04	1.22120E-03	5938.65	3456.48	.243844	7.79436E+10	5.07136E+10	3.13318E+10
13	7.09600E-04	1.22850E-03	5943.99	3434.93	.249306	7.73127E+10	5.13991E+10	3.09422E+10
15	7.04300E-04	1.20740E-03	5990.55	3496.36	.241685	7.96141E+10	5.13675E+10	3.20589E+10
17	7.02300E-04	1.21650E-03	6006.32	3469.13	.249701	7.88848E+10	5.25270E+10	3.15615E+10
19	7.02800E-04	1.19760E-03	6002.01	3524.4	.236865	8.05821E+10	5.10397E+10	3.25752E+10
21	7.03300E-04	1.21390E-03	5997.7	3476.63	.24698	7.90538E+10	5.20736E+10	3.16981E+10
23	7.06500E-04	1.21870E-03	5968.87	3461.98	.246525	7.83604E+10	5.15242E+10	3.14315E+10

LINE #	DISTANCE (M)
11	4.182
13	4.181
15	4.182
17	4.181
19	4.181
21	4.181
23	4.18

DENSITY : 2622.5 KG/M<sup>3</sup>

INSTRUMENT DELAY FOR P-WAVE : 6.20000E-06 SEC.

INSTRUMENT DELAY FOR S-WAVE : 1.13000E-05 SEC.

Table C:3.27  $day\#$ ,  $t_p$ ,  $t_s$ ,  $V_p$ ,  $V_s$ ,  $\nu$ ,  $E_d$ ,  $K_d$ , and  $G_d$ , for reverse survey at day 119 after the heater was turned on in cross section M8-M6.



PROFILE AND FILE NAME : M8-M6 SURVE.8

DATE FOR FIELD WORK : 31 JULY,1979 DAYS AFTER HEATER TURN ON : 341 PROCESS DATE : 20 JAN,1981

LINE #	P-TIME (SEC)	S-TIME (SEC)	P-VELOCITY (M/SEC)	S-VELOCITY (M/SEC)	POISS.RATIO	YOUNGS MOD (PA)	BULK MOD (PA)	SHEAR MOD (PA)
3	7.09100E-04	1.21630E-03	5955.33	3473.86	.242124	7.86203E+10	5.08127E+10	3.16475E+10
4	7.05200E-04	1.20080E-03	5987.12	3518.28	.236265	8.02636E+10	5.07223E+10	3.24622E+10
5	7.04500E-04	1.22410E-03	5993.13	3450.69	.252038	7.81944E+10	5.25580E+10	3.12268E+10
6	7.06500E-04	1.23530E-03	5974.58	3418.3	.256677	7.70176E+10	5.27540E+10	3.06433E+10
7	7.07200E-04	1.22290E-03	5968.62	3453.28	.248406	7.80847E+10	5.17266E+10	3.12738E+10
8	7.04200E-04	1.20660E-03	5994.27	3500.38	.241272	7.97704E+10	5.13864E+10	3.21325E+10
9	7.06700E-04	1.20570E-03	5972.88	3503.01	.237843	7.96700E+10	5.06504E+10	3.21810E+10
10	7.07800E-04	1.20570E-03	5962.09	3502.18	.236585	7.95510E+10	5.03332E+10	3.21656E+10
11	7.08200E-04	1.20470E-03	5957.27	3504.27	.23545	7.95732E+10	5.01311E+10	3.22041E+10
12	7.06700E-04	1.19300E-03	5968.59	3538.12	.229109	8.07015E+10	4.96519E+10	3.28293E+10
13	7.07700E-04	1.19240E-03	5960.08	3539.92	.227486	8.06769E+10	4.93412E+10	3.28626E+10
14	7.04300E-04	1.19100E-03	5990.55	3544.97	.230555	8.11095E+10	5.01708E+10	3.29564E+10
15	7.03400E-04	1.18910E-03	5998.28	3550.69	.230288	8.13537E+10	5.02720E+10	3.30629E+10
16	7.03000E-04	1.18520E-03	6000.29	3561.63	.227998	8.17036E+10	5.00630E+10	3.32670E+10
17	7.00400E-04	1.19270E-03	6022.76	3539.02	.236311	8.12156E+10	5.13330E+10	3.28459E+10
18	7.00000E-04	1.18370E-03	6026.23	3566.19	.230532	8.20818E+10	5.07678E+10	3.33522E+10
19	7.02000E-04	1.18470E-03	6008.91	3563.15	.228844	8.18296E+10	5.02968E+10	3.32953E+10
20	7.01900E-04	1.20640E-03	6009.77	3498.45	.243717	7.98397E+10	5.19216E+10	3.20972E+10
21	7.03100E-04	1.19240E-03	5999.43	3539.92	.232951	8.10360E+10	5.05751E+10	3.28626E+10
22	7.05100E-04	1.19830E-03	5982.26	3522.32	.234678	8.03449E+10	5.04701E+10	3.25368E+10
23	7.06200E-04	1.20100E-03	5971.43	3513.49	.235246	7.99791E+10	5.03480E+10	3.23737E+10
24	7.07700E-04	1.20090E-03	5958.66	3513.79	.233436	7.98753E+10	4.99412E+10	3.23792E+10
25	7.05900E-04	1.19510E-03	5973.99	3531	.231532	8.05354E+10	4.99968E+10	3.26973E+10
26	7.05100E-04	1.22810E-03	5980.83	3435.24	.253835	7.76068E+10	5.25439E+10	3.09478E+10
27	7.02500E-04	1.19490E-03	6001.72	3530.75	.235375	8.07754E+10	5.08740E+10	3.26927E+10
28	7.02300E-04	1.19650E-03	6003.45	3525.99	.236696	8.06436E+10	5.10459E+10	3.26045E+10
29	7.03300E-04	1.21530E-03	5993.4	3470.1	.247865	7.88128E+10	5.20970E+10	3.15791E+10
30	7.04700E-04	1.18690E-03	5979.96	3553.08	.227165	8.12565E+10	4.96371E+10	3.31074E+10
31	7.03900E-04	1.21590E-03	5985.38	3466.71	.24759	7.86417E+10	5.19272E+10	3.15174E+10
32	7.02000E-04	1.21730E-03	6001.72	3462.69	.250521	7.86435E+10	5.25385E+10	3.14443E+10
33	7.03500E-04	1.20500E-03	5988.81	3498.37	.241008	7.96619E+10	5.12641E+10	3.20956E+10
34	7.05400E-04	1.20050E-03	5971.11	3510.76	.235831	7.98928E+10	5.04050E+10	3.23235E+10
35	7.07900E-04	1.19670E-03	5949.84	3522.02	.230287	8.00452E+10	4.94632E+10	3.25311E+10
36	7.05700E-04	1.20740E-03	5967.12	3489.67	.240109	7.92091E+10	5.07963E+10	3.19364E+10
37	7.04500E-04	1.18630E-03	5977.37	3552.34	.226976	8.12102E+10	4.95744E+10	3.30936E+10
38	7.02900E-04	1.18770E-03	5989.67	3547.26	.229896	8.11709E+10	5.00862E+10	3.29991E+10

Table C:3.28  $day\#$ ,  $t_p$ ,  $t_s$ ,  $V_p$ ,  $V_s$ ,  $\nu$ ,  $E_d$ ,  $K_d$ , and  $G_d$ , for survey # 8 at day 341 after the heater was turned on in cross section M8-M6.

LINE # DISTANCE  
(M)

3 4.186  
4 4.185  
5 4.185  
6 4.184  
7 4.184  
8 4.184  
9 4.184  
10 4.183  
11 4.182  
12 4.181  
13 4.181  
14 4.182  
15 4.182  
16 4.181  
17 4.181  
18 4.181  
19 4.181  
20 4.181  
21 4.181  
22 4.181  
23 4.18  
24 4.18  
25 4.18  
26 4.18  
27 4.179  
28 4.179  
29 4.178  
30 4.177  
31 4.176  
32 4.176  
33 4.176  
34 4.175  
35 4.175  
36 4.174  
37 4.174  
38 4.173

DENSITY : 2622.5 KG/M-3

INSTRUMENT DELAY FOR P-WAVE : 6.20000E-06 SEC.

INSTRUMENT DELAY FOR S-WAVE : 1.13000E-05 SEC.

PROFILE AND FILE NAME : M8-M6 SURVE.9

DATE FOR FIELD WORK : 18 OCT,1979 DAYS AFTER HEATER TURN ON : 420 PROCESS DATE : 20 JAN,1981

LINE #	P-TIME (SEC)	S-TIME (SEC)	P-VELOCITY (M/SEC)	S-VELOCITY (M/SEC)	POISS.RATIO	YOUNGS MOD (PA)	BULK MOD (PA)	SHEAR MOD (PA)
3	7.09100E-04	1.20320E-03	5955.33	3512.04	.233385	7.97927E+10	4.98800E+10	3.23470E+10
4	7.08600E-04	1.22710E-03	5958.14	3442.18	.249511	7.76519E+10	5.16668E+10	3.10729E+10
5	7.08600E-04	1.23090E-03	5958.14	3431.45	.251843	7.73128E+10	5.19246E+10	3.08796E+10
6	7.10700E-04	1.23530E-03	5938.96	3418.3	.252299	7.67493E+10	5.16412E+10	3.06433E+10
7	7.13500E-04	1.25560E-03	5915.45	3362.53	.261322	7.48005E+10	5.22325E+10	2.96516E+10
8	7.13900E-04	1.25910E-03	5912.11	3353.1	.262897	7.44744E+10	5.23503E+10	2.94855E+10
9	7.15000E-04	1.25450E-03	5902.93	3365.51	.259192	7.48064E+10	5.17745E+10	2.97041E+10
10	7.20900E-04	1.25300E-03	5852.81	3368.77	.252287	7.45404E+10	5.01523E+10	2.97617E+10
11	7.23200E-04	1.25140E-03	5832.64	3372.31	.248921	7.44964E+10	4.94508E+10	2.98243E+10
12	7.27600E-04	1.25090E-03	5795.67	3372.86	.243937	7.42234E+10	4.83106E+10	2.98341E+10
13	7.27700E-04	1.22570E-03	5794.87	3442.85	.227227	7.62970E+10	4.66181E+10	3.10851E+10
14	7.24200E-04	1.24120E-03	5824.51	3400.28	.241496	7.52869E+10	4.85401E+10	3.03210E+10
15	7.21700E-04	1.23750E-03	5844.86	3410.54	.241868	7.57646E+10	4.89186E+10	3.05043E+10
16	7.17800E-04	1.23870E-03	5875.49	3406.39	.246847	7.58834E+10	4.99589E+10	3.04301E+10
17	7.10500E-04	1.19680E-03	5936.39	3526.78	.227263	8.00645E+10	4.89266E+10	3.26191E+10
18	7.13300E-04	1.23450E-03	5912.88	3418.08	.249058	7.65409E+10	5.08357E+10	3.06394E+10
19	7.14000E-04	1.23480E-03	5907.04	3417.25	.248496	7.64690E+10	5.06745E+10	3.06244E+10
20	7.13800E-04	1.23150E-03	5908.71	3426.49	.246659	7.67700E+10	5.05051E+10	3.07903E+10
21	7.12400E-04	1.23230E-03	5920.42	3424.24	.248661	7.67925E+10	5.09223E+10	3.07499E+10
22	7.13300E-04	1.23450E-03	5912.88	3418.08	.249058	7.65409E+10	5.08357E+10	3.06394E+10
23	7.14500E-04	1.22100E-03	5901.45	3455.4	.239162	7.76016E+10	4.95847E+10	3.13121E+10
24	7.14800E-04	1.22960E-03	5898.96	3431.01	.244378	7.68319E+10	5.00947E+10	3.08716E+10
25	7.11500E-04	1.21420E-03	5926.56	3474.94	.238053	7.84112E+10	4.98900E+10	3.16671E+10
26	7.08800E-04	1.21270E-03	5949.33	3479.27	.240108	7.87376E+10	5.04938E+10	3.17463E+10
27	7.06600E-04	1.20200E-03	5966.59	3509.7	.235463	7.98206E+10	5.02896E+10	3.23039E+10
28	7.05500E-04	1.20630E-03	5975.98	3497.07	.239607	7.95130E+10	5.08930E+10	3.20719E+10
29	7.07300E-04	1.21050E-03	5959.21	3483.99	.240348	7.89665E+10	5.06874E+10	3.18324E+10
30	7.07300E-04	1.21130E-03	5957.78	3480.83	.240874	7.88568E+10	5.07197E+10	3.17747E+10
31	7.06100E-04	1.21210E-03	5966.57	3477.68	.242737	7.88323E+10	5.10712E+10	3.17172E+10
32	7.03500E-04	1.23380E-03	5988.81	3415.95	.258882	7.70467E+10	5.32567E+10	3.06012E+10
33	7.04900E-04	1.21570E-03	5976.81	3467.29	.246372	7.85910E+10	5.16446E+10	3.15279E+10
34	7.07200E-04	1.22120E-03	5955.78	3450.7	.247341	7.79013E+10	5.13875E+10	3.12269E+10
35	7.09100E-04	1.22540E-03	5939.68	3438.76	.247917	7.73989E+10	5.11729E+10	3.10113E+10
36	7.07200E-04	1.22440E-03	5954.35	3440.77	.249339	7.75778E+10	5.15822E+10	3.10475E+10
37	7.05100E-04	1.22440E-03	5972.24	3440.77	.251584	7.77172E+10	5.21418E+10	3.10475E+10

Table C:3.29  $day\#$ ,  $t_p$ ,  $t_s$ ,  $V_p$ ,  $V_s$ ,  $\nu$ ,  $E_d$ ,  $K_d$ , and  $G_d$ , for survey # 9 at day 420 after the heater was turned on and 22 days after the heater was turned off in cross section M8-M6.

LINE #	DISTANCE (M)
3	4.186
4	4.185
5	4.185
6	4.184
7	4.184
8	4.184
9	4.184
10	4.183
11	4.182
12	4.181
13	4.181
14	4.182
15	4.182
16	4.181
17	4.181
18	4.181
19	4.181
20	4.181
21	4.181
22	4.181
23	4.18
24	4.18
25	4.18
26	4.18
27	4.179
28	4.179
29	4.178
30	4.177
31	4.176
32	4.176
33	4.176
34	4.175
35	4.175
36	4.174
37	4.174

DENSITY : 2622.5 KG/M<sup>3</sup>

INSTRUMENT DELAY FOR P-WAVE : 6.20000E-06 SEC.

INSTRUMENT DELAY FOR S-WAVE : 1.13000E-06 SEC.

PROFILE AND FILE NAME : M8-M6 SURVE.10

DATE FOR FIELD WORK : 28 JULY,1980 DAYS AFTER HEATER TURN ON : 704 PROCESS DATE : 20 JAN.,1981

LINE #	P-TIME (SEC)	S-TIME (SEC)	P-VELOCITY (M/SEC)	S-VELOCITY (M/SEC)	POISS.RATIO	YOUNGS MOD (PA)	BULK MOD (PA)	SHEAR MOD (PA)
1	7.13100E-04	1.28480E-03	5920.21	3286.22	.277333	7.23507E+10	5.41545E+10	2.83210E+10
2	7.09600E-04	1.24650E-03	5949.67	3388.12	.26004	7.58658E+10	5.26935E+10	3.01045E+10
3	7.08000E-04	1.22420E-03	5964.66	3451.23	.248354	7.79887E+10	5.16524E+10	3.12366E+10
4	7.07700E-04	1.25030E-03	5965.79	3377.72	.264097	7.56440E+10	5.34428E+10	2.99202E+10
5	7.07500E-04	1.24010E-03	5967.49	3405.76	.258468	7.65625E+10	5.28311E+10	3.04189E+10
6	7.12300E-04	1.30850E-03	5925.51	3225.41	.289479	7.03606E+10	5.57035E+10	2.72826E+10
7	7.15700E-04	1.34100E-03	5897.11	3146.57	.300986	6.75607E+10	5.65796E+10	2.59652E+10
8	7.17800E-04	1.29160E-03	5879.71	3267.98	.276493	7.15029E+10	5.33189E+10	2.80076E+10
9	7.19700E-04	1.34030E-03	5864.05	3148.23	.297527	6.74520E+10	5.55234E+10	2.59925E+10
10	7.26100E-04	1.29600E-03	5810.53	3256.01	.271128	7.06817E+10	5.14712E+10	2.78027E+10
11	7.30700E-04	1.36050E-03	5772.26	3099.61	.297405	6.53787E+10	5.37843E+10	2.51960E+10
12	7.36100E-04	1.32390E-03	5728.18	3185.28	.276185	6.79132E+10	5.05724E+10	2.66079E+10
13	7.37800E-04	1.30940E-03	5714.87	3220.86	.267252	6.89529E+10	4.93760E+10	2.72057E+10
14	7.27900E-04	1.26800E-03	5794.65	3327.76	.253955	7.28336E+10	4.93362E+10	2.90416E+10
15	7.25200E-04	1.20340E-03	5816.41	3508.1	.214115	7.83697E+10	4.56883E+10	3.22744E+10
16	7.20100E-04	1.24750E-03	5856.56	3382.14	.249811	7.49847E+10	4.99521E+10	2.99984E+10
17	7.13100E-04	1.22880E-03	5914.56	3434.09	.245721	7.70529E+10	5.05042E+10	3.09270E+10
18	7.14200E-04	1.26920E-03	5905.37	3323.79	.268158	7.34830E+10	5.28256E+10	2.89723E+10
19	7.16000E-04	1.23630E-03	5890.39	3413.06	.247286	7.62078E+10	5.02595E+10	3.05495E+10
20	7.16600E-04	1.25150E-03	5885.42	3371.23	.255828	7.48605E+10	5.10982E+10	2.98052E+10
21	7.14900E-04	1.19770E-03	5899.53	3524.11	.222599	7.96393E+10	4.78485E+10	3.25697E+10
22	7.13800E-04	1.19960E-03	5908.71	3518.47	.225302	7.95603E+10	4.82713E+10	3.24656E+10
23	7.14400E-04	1.23170E-03	5902.29	3425.11	.246137	7.66760E+10	5.03394E+10	3.07655E+10
24	7.13800E-04	1.20530E-03	5907.29	3500.84	.229334	7.90241E+10	4.86603E+10	3.21410E+10
25	7.10400E-04	1.22470E-03	5935.81	3444.87	.246069	7.75590E+10	5.09056E+10	3.11215E+10
26	7.06900E-04	1.22140E-03	5965.46	3454.26	.247791	7.80904E+10	5.16043E+10	3.12914E+10
27	7.05300E-04	1.21030E-03	5977.69	3485.4	.242459	7.91651E+10	5.12314E+10	3.18582E+10
28	7.05000E-04	1.21330E-03	5980.25	3476.71	.244731	7.89145E+10	5.15237E+10	3.16994E+10
29	7.05000E-04	1.21350E-03	5978.82	3475.3	.244859	7.88586E+10	5.15131E+10	3.16737E+10
30	7.06100E-04	1.22020E-03	5968	3455.21	.247905	7.81403E+10	5.16607E+10	3.13086E+10
31	7.05000E-04	1.21860E-03	5975.96	3458.96	.248094	7.83219E+10	5.18195E+10	3.13766E+10
32	7.02800E-04	1.21600E-03	5994.83	3466.42	.248848	7.87079E+10	5.22312E+10	3.15122E+10
33	7.04200E-04	1.22090E-03	5982.81	3452.38	.250389	7.81679E+10	5.21932E+10	3.12574E+10
34	7.07100E-04	1.22180E-03	5956.63	3448.99	.247826	7.78543E+10	5.14553E+10	3.11960E+10
35	7.08700E-04	1.22690E-03	5943.06	3434.52	.24928	7.72924E+10	5.13803E+10	3.09348E+10
36	7.06400E-04	1.22400E-03	5961.15	3441.91	.249949	7.76669E+10	5.17674E+10	3.10680E+10
37	7.04400E-04	1.22400E-03	5978.23	3441.91	.252083	7.77995E+10	5.23021E+10	3.10680E+10
38	7.02400E-04	1.20920E-03	5993.97	3483.6	.24497	7.92428E+10	5.17866E+10	3.18252E+10
39	7.01900E-04	1.20500E-03	5998.27	3495.85	.242806	7.96627E+10	5.16230E+10	3.20495E+10

Table C:3.30  $day\#$ ,  $t_p$ ,  $t_s$ ,  $V_p$ ,  $V_s$ ,  $\nu$ ,  $E_d$ ,  $K_d$ , and  $G_d$ , for survey # 10 at day 704 after the heater was turned on and 306 days after the heater was turned off in cross section M8-M6.

LINE #	DISTANCE (M)
1	4.185
2	4.185
3	4.186
4	4.185
5	4.185
6	4.184
7	4.184
8	4.184
9	4.184
10	4.183
11	4.182
12	4.181
13	4.181
14	4.182
15	4.182
16	4.181
17	4.181
18	4.181
19	4.181
20	4.181
21	4.181
22	4.181
23	4.18
24	4.18
25	4.18
26	4.18
27	4.179
28	4.179
29	4.178
30	4.177
31	4.176
32	4.176
33	4.176
34	4.175
35	4.175
36	4.174
37	4.174
38	4.173
39	4.173

DENSITY : 2622.5 KG/M<sup>3</sup>

INSTRUMENT DELAY FOR P-WAVE : 0 SEC.

INSTRUMENT DELAY FOR S-WAVE : 0 SEC.

PROFILE AND FILE NAME : M7-M9 SURUF.1

DATE FOR FIELD WORK : 12 JULY, 1978 DAYS AFTER HEATER TURN ON : -43 PROCESS DATE : 20 JAN., 1981

LINE #	P-TIME (SEC)	S-TIME (SEC)	P-VELOCITY (M/SEC)	S-VELOCITY (M/SEC)	POISS.RATIO	YOUNGS MOD (PA)	BULK MOD (PA)	SHEAR MOD (PA)
1	7.22400E-04	1.39450E-03	5874.06	3041.5	.316845	6.38933E+10	5.81415E+10	2.42600E+10
3	7.23100E-04	1.31840E-03	5868.32	3218.58	.284882	6.98129E+10	5.40888E+10	2.71671E+10
5	7.23900E-04	1.23760E-03	5860.39	3429.83	.239515	7.64790E+10	4.89337E+10	3.08524E+10
7	7.32500E-04	1.22890E-03	5791	3454.34	.223827	7.65940E+10	4.62234E+10	3.12928E+10
9	7.31300E-04	1.27790E-03	5799.2	3319.91	.256251	7.26231E+10	4.96570E+10	2.89047E+10
11	7.34600E-04	1.27310E-03	5772.93	3332.54	.250104	7.28186E+10	4.85659E+10	2.91250E+10
13	7.32500E-04	1.36420E-03	5786.87	3106.66	.297551	6.56836E+10	5.40743E+10	2.53106E+10
15	7.34800E-04	1.25730E-03	5769.97	3374	.240198	7.40501E+10	4.75042E+10	2.58542E+10
17	7.37300E-04	1.32180E-03	5748.87	3207.17	.27407	6.87359E+10	5.07058E+10	2.69749E+10
19	7.43500E-04	1.29270E-03	5699.17	3279.23	.252538	7.06446E+10	4.75795E+10	2.82006E+10
21	7.40800E-04	1.26400E-03	5718.76	3353.56	.237944	7.30226E+10	4.64421E+10	2.94935E+10
23	7.28000E-04	1.31170E-03	5820.17	3230.54	.277361	6.99215E+10	5.23429E+10	2.73695E+10
25	7.19700E-04	1.28330E-03	5883.67	3300.31	.270457	7.25798E+10	5.26987E+10	2.85645E+10
27	7.18500E-04	1.23920E-03	5890.78	3417.22	.246407	7.63397E+10	5.01721E+10	3.06239E+10
29	7.16200E-04	1.23260E-03	5909.86	3435.68	.244753	7.70646E+10	5.03202E+10	3.09558E+10
31	7.16000E-04	1.20930E-03	5910.12	3501.67	.229535	7.90745E+10	4.87275E+10	3.21563E+10
33	7.19300E-04	1.24470E-03	5879.96	3399.55	.248949	7.57063E+10	5.02595E+10	3.03080E+10
35	7.23200E-04	1.25610E-03	5847.98	3368.41	.251753	7.44929E+10	5.00125E+10	2.97554E+10
37	7.17900E-04	1.26020E-03	5890.12	3356.55	.259542	7.44295E+10	5.15888E+10	2.95463E+10
39	7.16800E-04	1.23140E-03	5896.43	3434.14	.243338	7.69081E+10	4.99412E+10	3.09281E+10

LINE #	DISTANCE (M)
1	4.207
3	4.207
5	4.206
7	4.206
9	4.205
11	4.205
13	4.203
15	4.204
17	4.203
19	4.202
21	4.201
23	4.201
25	4.198
27	4.196
29	4.196
31	4.195
33	4.193
35	4.193
37	4.192
39	4.19

DENSITY : 2622.5 KG/M<sup>3</sup>

INSTRUMENT DELAY FOR P-WAVE : 6.20000E-06 SEC.

INSTRUMENT DELAY FOR S-WAVE : 1.13000E-05 SEC.

Table C:3.31  $day\#$ ,  $t_p$ ,  $t_s$ ,  $V_p$ ,  $V_s$ ,  $\nu$ ,  $E_d$ ,  $K_d$ , and  $G_d$ , for survey # 1 at day -43 before the heater was turned on in cross section M7-M9.

PROFILE AND FILE NAME : M7-M9 SURF.2

DATE FOR FIELD WORK : 23-24 AUG,1978 DAYS AFTER HEATER TURN ON : 00 PROCESS DATE : 20 JAN,1981

LINE #	P-TIME (SEC)	S-TIME (SEC)	P-VELOCITY (M/SEC)	S-VELOCITY (M/SEC)	POISS.RATIO	YOUNGS MOD (PA)	BULK MOD (PA)	SHEAR MOD (PA)
2	7.23800E-04	1.35310E-03	5861.2	3134.6	.299705	6.69812E+10	5.57355E+10	2.57679E+10
3	7.19100E-04	1.35470E-03	5901.25	3131.61	.304	6.70745E+10	5.70362E+10	2.57187E+10
4	7.22500E-04	1.20410E-03	5871.84	3526.16	.217988	7.94313E+10	4.69431E+10	3.26076E+10
5	7.23400E-04	1.20790E-03	5864.47	3514.96	.219679	7.90372E+10	4.69921E+10	3.24008E+10
6	7.29600E-04	1.35940E-03	5814.21	3119.95	.297805	6.62597E+10	5.46169E+10	2.55276E+10
7	7.29600E-04	1.34650E-03	5814.21	3150.09	.292248	6.72569E+10	5.39560E+10	2.60232E+10
8	7.29200E-04	1.39190E-03	5816.04	3045.78	.311061	6.37918E+10	5.62719E+10	2.43283E+10
9	7.28600E-04	1.23230E-03	5820.87	3443.9	.230716	7.65603E+10	4.73851E+10	3.11040E+10
10	7.32100E-04	1.27720E-03	5791.43	3320.96	.255046	7.25992E+10	4.93965E+10	2.89229E+10
11	7.29200E-04	1.41620E-03	5816.04	2993.1	.319875	6.20182E+10	5.73843E+10	2.34940E+10
12	7.28300E-04	1.30430E-03	5821.91	3251.35	.273375	7.06041E+10	5.19243E+10	2.77232E+10
13	7.31500E-04	1.43740E-03	5794.84	2947.2	.325542	6.03890E+10	5.76921E+10	2.27790E+10
14	7.35200E-04	1.28100E-03	5765.43	3310.23	.254121	7.20778E+10	4.88573E+10	2.87364E+10
15	7.31100E-04	1.35650E-03	5799.42	3125.19	.295387	6.63585E+10	5.40521E+10	2.56134E+10
16	7.33800E-04	1.41270E-03	5776.53	2999.14	.315478	6.20617E+10	5.60562E+10	2.35890E+10
17	7.39500E-04	1.32070E-03	5731.62	3209.87	.271529	6.87141E+10	5.01261E+10	2.70203E+10
18	7.40000E-04	1.31320E-03	5726.36	3227.59	.267198	6.92384E+10	4.95688E+10	2.73195E+10
19	7.33000E-04	1.27650E-03	5781.51	3321.21	.253733	7.25345E+10	4.90894E+10	2.89274E+10
20	7.36300E-04	1.30240E-03	5755.38	3254.59	.264949	7.02766E+10	4.98307E+10	2.77784E+10
21	7.32700E-04	1.29560E-03	5782.52	3271.04	.264715	7.09759E+10	5.02766E+10	2.80600E+10
22	7.29000E-04	1.29580E-03	5812.12	3270.53	.268319	7.11560E+10	5.11883E+10	2.80513E+10
23	7.25700E-04	1.31080E-03	5838.78	3232.78	.278062	7.01061E+10	5.28813E+10	2.74074E+10
24	7.18500E-04	1.24040E-03	5894.99	3416.32	.247153	7.63453E+10	5.03237E+10	3.06079E+10
25	7.17300E-04	1.24030E-03	5903.53	3415.79	.248371	7.63959E+10	5.06008E+10	3.05983E+10
26	7.18500E-04	1.24710E-03	5892.18	3396.18	.251247	7.56955E+10	5.07167E+10	3.02480E+10
27	7.16500E-04	1.25100E-03	5907.36	3384.69	.255637	7.54479E+10	5.14590E+10	3.00437E+10
28	7.13500E-04	1.23050E-03	5932.42	3441.6	.246357	7.74300E+10	5.08785E+10	3.10625E+10
29	7.14200E-04	1.23290E-03	5926.55	3474.84	.247103	7.71722E+10	5.08587E+10	3.09406E+10
30	7.14000E-04	1.23410E-03	5926.82	3430.65	.248063	7.70433E+10	5.09674E+10	3.08652E+10
31	7.13700E-04	1.23600E-03	5929.33	3425.33	.249555	7.68963E+10	5.11731E+10	3.07695E+10
32	7.15000E-04	1.22100E-03	5917.04	3466.98	.238601	7.80869E+10	4.97877E+10	3.15222E+10
33	7.16900E-04	1.24050E-03	5899.82	3411.16	.248919	7.62227E+10	5.05963E+10	3.05155E+10
34	7.17900E-04	1.24220E-03	5891.53	3406.45	.248901	7.60111E+10	5.04522E+10	3.04318E+10
35	7.20000E-04	1.32630E-03	5867.62	3188.59	.290471	6.88164E+10	5.47389E+10	2.66833E+10
36	7.17900E-04	1.29410E-03	5890.12	3267.85	.27766	7.15625E+10	5.36434E+10	2.80053E+10

Table C.3.32  $day\#$ ,  $t_p$ ,  $t_s$ ,  $V_p$ ,  $V_s$ ,  $\nu$ ,  $E_d$ ,  $K_d$ , and  $G_d$ , for survey # 2 at day 00 which is the day the heater was turned on in cross section M7-M9.



LINE # DISTANCE

(M)

2	4.206
3	4.207
4	4.206
5	4.206
6	4.206
7	4.206
8	4.205
9	4.205
10	4.204
11	4.205
12	4.204
13	4.203
14	4.203
15	4.204
16	4.203
17	4.203
18	4.202
19	4.202
20	4.202
21	4.201
22	4.201
23	4.201
24	4.199
25	4.198
26	4.197
27	4.196
28	4.196
29	4.196
30	4.195
31	4.195
32	4.194
33	4.193
34	4.193
35	4.193
36	4.192

DENSITY : 2622.5 KG/M<sup>3</sup>

INSTRUMENT DELAY FOR P-WAVE : 6.20000E-06 SEC.

INSTRUMENT DELAY FOR S-WAVE : 1.13000E-05 SEC.

PROFILE AND FILE NAME : M7-M9 SURUF.3

DATE FOR FIELD WORK : 30 AUG.,1978 DAYS AFTER HEATER TURN ON : 6 PROCESS DATE : 20 JAN,1981

LINE #	P-TIME (SEC)	S-TIME (SEC)	P-VELOCITY (M/SEC)	S-VELOCITY (M/SEC)	POISS.RATIO	YOUNGS MOD (PA)	BULK MOD (PA)	SHEAR MOD (PA)
3	7.21000E-04	1.24970E-03	5885.56	3397.13	.2502	7.56742E+10	5.04898E+10	3.02649E+10
5	7.21500E-04	1.22740E-03	5880.05	3458.6	.23551	7.75160E+10	4.88462E+10	3.13701E+10
7	7.25400E-04	1.25600E-03	5848.16	3379.13	.249402	7.48267E+10	4.97655E+10	2.99450E+10
9	7.25100E-04	1.24100E-03	5849.21	3419.53	.240383	7.60738E+10	4.88371E+10	3.06654E+10
11	7.23100E-04	1.22430E-03	5865.53	3466.61	.2316	7.76292E+10	4.82049E+10	3.15156E+10
13	7.21500E-04	1.27280E-03	5875.86	3331.75	.263063	7.35385E+10	5.17287E+10	2.91112E+10
15	7.22300E-04	1.35850E-03	5870.69	3120.55	.303095	6.65553E+10	5.63345E+10	2.55374E+10
17	7.27600E-04	1.25640E-03	5826.17	3375.63	.247335	7.45485E+10	4.91747E+10	2.98831E+10
19	7.27500E-04	1.23890E-03	5825.59	3422.94	.236364	7.59784E+10	4.80324E+10	3.07266E+10
21	7.29300E-04	1.25960E-03	5809.71	3365.38	.247497	7.41058E+10	4.89141E+10	2.97018E+10
23	7.25800E-04	1.24760E-03	5837.97	3398.04	.243807	7.53280E+10	4.90047E+10	3.02812E+10
25	7.18500E-04	1.24310E-03	5893.58	3408.02	.248816	7.60761E+10	5.04784E+10	3.04593E+10

LINE #	DISTANCE (M)
3	4.207
5	4.206
7	4.206
9	4.205
11	4.205
13	4.203
15	4.204
17	4.203
19	4.202
21	4.201
23	4.201
25	4.198

DENSITY : 2622.5 KG/M<sup>3</sup>

INSTRUMENT DELAY FOR P-WAVE : 6.20000E-06 SEC.

INSTRUMENT DELAY FOR S-WAVE : 1.13000E-05 SEC.

Table C:3.33  $day\#$ ,  $t_p$ ,  $t_s$ ,  $V_p$ ,  $V_s$ ,  $\nu$ ,  $E_d$ ,  $K_d$ , and  $G_d$ , for survey # 3 at day 6 after the heater was turned on in cross section M7-M9.

PROFILE AND FILE NAME : M7-M9 SURV.4

DATE FOR FIELD WORK : 7 SEP.,1978 DAYS AFTER HEATER TURN ON : 13 PROCESS DATE : 20 JAN,1978

LINE #	P-TIME (SEC)	S-TIME (SEC)	P-VELOCITY (M/SEC)	S-VELOCITY (M/SEC)	POISS.RATIO	YOUNGS MOD (PA)	BULK MOD (PA)	SHEAR MOD (PA)
3	7.21400E-04	1.28180E-03	5882.27	3311.29	.268056	7.29255E+10	5.24016E+10	2.87549E+10
5	7.21600E-04	1.21230E-03	5879.23	3502.08	.225019	7.88026E+10	4.77624E+10	3.21638E+10
7	7.25000E-04	1.23310E-03	5851.42	3442.46	.235344	7.67841E+10	4.83546E+10	3.10781E+10
9	7.22400E-04	1.23970E-03	5871.26	3423.15	.242505	7.63653E+10	4.94283E+10	3.07304E+10
11	7.21800E-04	1.22340E-03	5876.19	3469.19	.232483	7.78003E+10	4.84706E+10	3.15624E+10
13	7.21600E-04	1.24600E-03	5875.03	3404.07	.247307	7.58080E+10	5.00001E+10	3.03886E+10
15	7.20900E-04	1.25970E-03	5882.19	3367.51	.256231	7.47193E+10	5.10862E+10	2.97395E+10
17	7.23500E-04	1.29590E-03	5859.47	3271.84	.273475	7.15021E+10	5.26079E+10	2.80736E+10
19	7.27100E-04	1.26560E-03	5828.83	3350.08	.253364	7.37789E+10	4.98569E+10	2.94323E+10
21	7.27100E-04	1.29180E-03	5827.44	3280.75	.267989	7.15826E+10	5.14218E+10	2.82268E+10
23	7.25800E-04	1.30160E-03	5837.97	3255.83	.27428	7.08491E+10	5.23134E+10	2.77997E+10
25	7.17700E-04	1.25900E-03	5900.21	3364.59	.259057	7.47576E+10	5.17118E+10	2.96879E+10
27	7.17800E-04	1.24700E-03	5896.57	3395.65	.251918	7.57123E+10	5.08651E+10	3.02385E+10
29	7.14500E-04	1.25060E-03	5924.04	3385.78	.257445	7.56054E+10	5.19507E+10	3.00631E+10
31	7.15000E-04	1.23990E-03	5918.45	3414.46	.250562	7.64705E+10	5.10953E+10	3.05744E+10
33	7.19400E-04	1.24870E-03	5879.14	3388.56	.25127	7.53574E+10	5.04949E+10	3.01124E+10
35	7.22400E-04	1.25570E-03	5854.51	3369.5	.252343	7.46759E+10	5.01875E+10	2.97745E+10

LINE #	DISTANCE (M)
3	4.207
5	4.206
7	4.206
9	4.205
11	4.205
13	4.203
15	4.204
17	4.203
19	4.202
21	4.201
23	4.201
25	4.198
27	4.196
29	4.196
31	4.195
33	4.193
35	4.193

DENSITY : 2622.5 KG/M-3

INSTRUMENT DELAY FOR P-WAVE : 6.20000E-06 SEC.

INSTRUMENT DELAY FOR S-WAVE : 1.13000E-05 SEC.

Table C:3.34  $day\#$ ,  $t_p$ ,  $t_s$ ,  $V_p$ ,  $V_s$ ,  $\nu$ ,  $E_d$ ,  $K_d$ , and  $G_d$ , for survey # 4 at day 13 after the heater was turned on in cross section M7-M9.

PROFILE AND FILE NAME : M7-M9 SURF.S

DATE FOR FIELD WORK : 14 SEP,1978 DAYS AFTER HEATER TURN ON : 20 PROCESS DATE : 20 JAN,1981

LINE #	P-TIME (SEC)	S-TIME (SEC)	P-VELOCITY (M/SEC)	S-VELOCITY (M/SEC)	POISS.RATIO	YOUNGS MOD (PA)	BULK MOD (PA)	SHEAR MOD (PA)
3	7.18300E-04	1.24700E-03	5907.88	3404.55	.251396	7.60780E+10	5.10035E+10	3.03973E+10
5	7.16800E-04	1.20880E-03	5918.94	3512.32	.228244	7.94726E+10	4.87401E+10	3.23521E+10
7	7.23600E-04	1.21920E-03	5862.84	3482.08	.227507	7.80631E+10	4.77463E+10	3.17974E+10
9	7.22500E-04	1.21660E-03	5870.44	3488.76	.226984	7.83296E+10	4.78175E+10	3.19196E+10
11	7.20300E-04	1.22520E-03	5888.53	3464.04	.235403	7.77536E+10	4.89761E+10	3.14689E+10
13	7.17900E-04	1.22810E-03	5905.58	3454.14	.240004	7.75977E+10	4.97429E+10	3.12893E+10
15	7.18100E-04	1.23410E-03	5905.32	3438.01	.243635	7.70998E+10	5.01237E+10	3.09977E+10
17	7.21600E-04	1.24150E-03	5875.03	3416.52	.244509	7.61922E+10	4.97031E+10	3.06114E+10
19	7.24700E-04	1.23140E-03	5848.3	3443.98	.234553	7.68027E+10	4.82222E+10	3.11055E+10
21	7.25900E-04	1.23720E-03	5837.15	3426.87	.237035	7.61944E+10	4.82919E+10	3.07972E+10
23	7.21300E-04	1.22630E-03	5874.7	3457.61	.235003	7.74402E+10	4.87051E+10	3.13522E+10
25	7.14700E-04	1.22850E-03	5925.19	3448.9	.243788	7.75984E+10	5.04780E+10	3.11944E+10
27	7.14200E-04	1.22460E-03	5926.55	3458.34	.241838	7.79013E+10	5.02923E+10	3.13653E+10
29	7.12700E-04	1.21340E-03	5939.14	3490.56	.236156	7.89966E+10	4.99010E+10	3.19525E+10
31	7.12400E-04	1.22620E-03	5940.24	3452.96	.244839	7.78470E+10	5.08483E+10	3.12679E+10
33	7.17400E-04	1.23470E-03	5895.67	3427.33	.244775	7.66918E+10	5.00812E+10	3.08055E+10
35	7.20000E-04	1.25350E-03	5874.19	3375.46	.253514	7.49103E+10	5.06522E+10	2.98801E+10
37	7.13700E-04	1.23410E-03	5925.09	3428.2	.248384	7.69530E+10	5.09725E+10	3.08210E+10

LINE #	DISTANCE (M)
3	4.207
5	4.206
7	4.206
9	4.205
11	4.205
13	4.203
15	4.204
17	4.203
19	4.202
21	4.201
23	4.201
25	4.198
27	4.196
29	4.196
31	4.195
33	4.193
35	4.193
37	4.192

DENSITY : 2622.5 KG/M<sup>3</sup>

INSTRUMENT DELAY FOR P-WAVE : 6.20000E-06 SEC.

INSTRUMENT DELAY FOR S-WAVE : 1.13000E-05 SEC.

Table C:3.35  $day\#$ ,  $t_p$ ,  $t_s$ ,  $V_p$ ,  $V_s$ ,  $\nu$ ,  $E_d$ ,  $K_d$ , and  $G_d$ , for survey # 5 at day 20 after the heater was turned on in cross section M7-M9.

PROFILE AND FILE NAME : M7-M9 SURV.6

DATE FOR FIELD WORK : 13 DEC,1978 DAYS AFTER HEATER TURN ON : 111 PROCESS DATE : 20 JAN,1981

LINE #	P-TIME (SEC)	S-TIME (SEC)	P-VELOCITY (M/SEC)	S-VELOCITY (M/SEC)	POISS.RATIO	YOUNGS MOD (PA)	BULK MOD (PA)	SHEAR MOD (PA)
3	7.21100E-04	1.26180E-03	5884.74	3364.25	.257245	7.46351E+10	5.12416E+10	2.96820E+10
4	7.20100E-04	1.23210E-03	5891.58	3445.28	.240158	7.72097E+10	4.95236E+10	3.11290E+10
5	7.18400E-04	1.18100E-03	5905.64	3595.79	.205431	8.17481E+10	4.62530E+10	3.39082E+10
6	7.25300E-04	1.25550E-03	5848.98	3380.49	.249204	7.48750E+10	4.97583E+10	2.99691E+10
7	7.24100E-04	1.22270E-03	5858.75	3472.02	.229348	7.77291E+10	4.78654E+10	3.16140E+10
8	7.23000E-04	1.21970E-03	5866.35	3479.81	.228557	7.80282E+10	4.79095E+10	3.17560E+10
9	7.21100E-04	1.21730E-03	5881.94	3486.73	.229114	7.83746E+10	4.82212E+10	3.18825E+10
10	7.19600E-04	1.21790E-03	5892.91	3484.17	.231273	7.83968E+10	4.86223E+10	3.18357E+10
11	7.17800E-04	1.21030E-03	5909.22	3507.09	.228114	7.92278E+10	4.85669E+10	3.22559E+10
12	7.13300E-04	1.20610E-03	5945.41	3518.58	.23048	7.99015E+10	4.94097E+10	3.24676E+10
13	7.16700E-04	1.20530E-03	5915.55	3520.1	.225893	7.96724E+10	4.84436E+10	3.24957E+10
14	7.18500E-04	1.23150E-03	5900.6	3444.52	.241537	7.72613E+10	4.98210E+10	3.11152E+10
15	7.17300E-04	1.21540E-03	5911.97	3491.4	.232225	7.87836E+10	4.90359E+10	3.19680E+10
16	7.14600E-04	1.21010E-03	5933.09	3506.01	.231725	7.94117E+10	4.93347E+10	3.22360E+10
17	7.16500E-04	1.21560E-03	5917.22	3489.99	.233284	7.87876E+10	4.92332E+10	3.19422E+10
18	7.21500E-04	1.23150E-03	5874.46	3443.7	.238213	7.70178E+10	4.90334E+10	3.11004E+10
19	7.19100E-04	1.23340E-03	5894.23	3438.34	.242096	7.70193E+10	4.87726E+10	3.10037E+10
20	7.21800E-04	1.25390E-03	5872	3381.62	.251891	7.50864E+10	5.04391E+10	2.99892E+10
21	7.20500E-04	1.22290E-03	5881.28	3467.32	.233634	7.77890E+10	4.86730E+10	3.15284E+10
22	7.20500E-04	1.21660E-03	5881.28	3485.44	.229331	7.83302E+10	4.82324E+10	3.18589E+10
23	7.19100E-04	1.20410E-03	5892.83	3521.97	.222143	7.95129E+10	4.76940E+10	3.25301E+10
24	7.13500E-04	1.21780E-03	5936.66	3480.31	.238178	7.86621E+10	5.00735E+10	3.17653E+10
25	7.13000E-04	1.24770E-03	5939.45	3395.34	.257284	7.60232E+10	5.22032E+10	3.02331E+10
26	7.15500E-04	1.23820E-03	5917.1	3420.02	.248993	7.66594E+10	5.09013E+10	3.06885E+10
27	7.14600E-04	1.23610E-03	5923.21	3425.87	.248659	7.68652E+10	5.09700E+10	3.07791E+10
28	7.12300E-04	1.21380E-03	5942.5	3489.4	.236879	7.89902E+10	5.00341E+10	3.19313E+10
29	7.13300E-04	1.23150E-03	5934.1	3438.78	.247198	7.73553E+10	5.09986E+10	3.10116E+10
30	7.13200E-04	1.24030E-03	5933.52	3413.34	.252695	7.65510E+10	5.15901E+10	3.05545E+10
31	7.12800E-04	1.23010E-03	5936.88	3441.91	.246862	7.74753E+10	5.10100E+10	3.10681E+10
32	7.14300E-04	1.24090E-03	5922.89	3410.87	.251905	7.63916E+10	5.13188E+10	3.05102E+10
33	7.16200E-04	1.22870E-03	5905.63	3444.23	.24227	7.72938E+10	4.99838E+10	3.11099E+10
34	7.16300E-04	1.23650E-03	5904.8	3422.3	.247088	7.66087E+10	5.04845E+10	3.07150E+10
35	7.19400E-04	1.23600E-03	5879.14	3423.7	.243424	7.64460E+10	4.96579E+10	3.07401E+10
36	7.19200E-04	1.23470E-03	5879.38	3426.52	.242816	7.65346E+10	4.95979E+10	3.07908E+10

Table C:3.36  $day\#$ ,  $t_p$ ,  $t_s$ ,  $V_p$ ,  $V_s$ ,  $\nu$ ,  $E_d$ ,  $K_d$ , and  $G_d$ , for survey # 6 at day 111 after the heater was turned on in cross section M7-M9.

LINE #	DISTANCE (M)
3	4.207
4	4.206
5	4.206
6	4.206
7	4.206
8	4.205
9	4.205
10	4.204
11	4.205
12	4.204
13	4.203
14	4.203
15	4.204
16	4.203
17	4.203
18	4.202
19	4.202
20	4.202
21	4.201
22	4.201
23	4.201
24	4.199
25	4.198
26	4.197
27	4.196
28	4.196
29	4.196
30	4.195
31	4.195
32	4.194
33	4.193
34	4.193
35	4.193
36	4.192

DENSITY : 2622.5 KG/M<sup>3</sup>

INSTRUMENT DELAY FOR P-WAVE : 6.20000E-06 SEC.

INSTRUMENT DELAY FOR S-WAVE : 1.13000E-05 SEC.

PROFILE AND FILE NAME : M7-M9 SURVF.7

DATE FOR FIELD WORK : 3 JAN,1979 DAYS AFTER HEATER TURN ON : 132 PROCESS DATE : 20 JAN,1981

LINE #	P-TIME (SEC)	S-TIME (SEC)	P-VELOCITY (M/SEC)	S-VELOCITY (M/SEC)	POISS.RATIO	YOUNGS MOD (PA)	BULK MOD (PA)	SHEAR MOD (PA)
3	7.18200E-04	1.24650E-03	5908.71	3405.93	.251199	7.61276E+10	5.09964E+10	3.04219E+10
5	7.14800E-04	1.21080E-03	5935.65	3506.46	.231973	7.94483E+10	4.94032E+10	3.22443E+10
7	7.20700E-04	1.21880E-03	5886.63	3483.23	.230615	7.83126E+10	4.84514E+10	3.18185E+10
9	7.17400E-04	1.21440E-03	5912.54	3495.14	.231424	7.89009E+10	4.89625E+10	3.20364E+10
11	7.16500E-04	1.22220E-03	5920.03	3472.62	.237705	7.82849E+10	4.97435E+10	3.16250E+10
13	7.13700E-04	1.26530E-03	5940.64	3351.67	.266523	7.46246E+10	5.32705E+10	2.94604E+10
15	7.12400E-04	1.24440E-03	5952.99	3409.29	.255965	7.65688E+10	5.22936E+10	3.04821E+10

LINE # DISTANCE

	(M)
3	4.207
5	4.206
7	4.206
9	4.205
11	4.205
13	4.203
15	4.204

DENSITY : 2622.5 KG/M<sup>3</sup>

INSTRUMENT DELAY FOR P-WAVE : 6.20000E-06 SEC.

INSTRUMENT DELAY FOR S-WAVE : 1.13000E-05 SEC.

Table C:3.37  $day\#$ ,  $t_p$ ,  $t_s$ ,  $V_p$ ,  $V_s$ ,  $\nu$ ,  $E_d$ ,  $K_d$ , and  $G_d$ , for survey # 7 at day 132 after the heater was turned on in cross section M7-M9.

PROFILE AND FILE NAME : M7-R9 SURUF.8

DATE FOR FIELD WORK : 4 JAN,1979 DAYS AFTER HEATER TURN ON : 133 PROCESS DATE : 20 JAN,1981

LINE #	P-TIME (SEC)	S-TIME (SEC)	P-VELOCITY (M/SEC)	S-VELOCITY (M/SEC)	POISS.RATIO	YOUNGS MOD (PA)	BULK MOD (PA)	SHEAR MOD (PA)
29	7.09800E-04	1.22850E-03	5963.62	3447.26	.249092	7.78551E+10	5.17156E+10	3.11647E+10
33	7.13500E-04	1.22710E-03	5928.18	3448.76	.244209	7.76183E+10	5.05741E+10	3.11918E+10
37	7.11600E-04	1.25700E-03	5942.73	3365.18	.263992	7.50768E+10	5.30185E+10	2.96983E+10

LINE #	DISTANCE (M)
29	4.196
33	4.193
37	4.192

DENSITY : 2622.5 KG/M-3

INSTRUMENT DELAY FOR P-WAVE : 6.20000E-06 SEC.

INSTRUMENT DELAY FOR S-WAVE : 1.13000E-05 SEC.



PROFILE AND FILE NAME : M7-M9 SURF.9

DATE FOR FIELD WORK : 8 AUG.,1979 DAYS AFTER HEATER TURN ON : 349 PROCESS DATE : 20 JAN.,1981

LINE #	P-TIME (SEC)	S-TIME (SEC)	P-VELOCITY (M/SEC)	S-VELOCITY (M/SEC)	POISS.RATIO	YOUNGS MOD (PA)	BULK MOD (PA)	SHEAR MOD (PA)
3	7.19600E-04	1.24130E-03	5897.11	3420.32	.246534	7.64864E+10	5.02937E+10	3.06796E+10
4	7.18000E-04	1.23580E-03	5908.96	3434.87	.244818	7.70322E+10	5.03119E+10	3.09411E+10
5	7.16300E-04	1.25110E-03	5923.11	3392.48	.255901	7.58117E+10	5.17628E+10	3.01822E+10
6	7.21700E-04	1.24590E-03	5878.41	3406.77	.247139	7.59183E+10	5.00396E+10	3.04370E+10
7	7.20400E-04	1.28430E-03	5889.11	3304.01	.270326	7.27348E+10	5.27812E+10	2.86284E+10
8	7.19000E-04	1.20700E-03	5899.27	3516.77	.224351	7.94217E+10	4.80211E+10	3.24342E+10
9	7.18300E-04	1.21570E-03	5905.07	3491.36	.231272	7.87209E+10	4.88231E+10	3.19673E+10
10	7.17900E-04	1.21400E-03	5906.98	3495.47	.230568	7.88609E+10	4.87821E+10	3.20425E+10
11	7.16200E-04	1.20330E-03	5922.54	3527.68	.225066	7.99621E+10	4.84734E+10	3.26358E+10
12	7.12800E-04	1.20160E-03	5949.62	3531.88	.22792	8.03393E+10	4.92130E+10	3.27136E+10
13	7.14300E-04	1.20560E-03	5935.6	3519.22	.228954	7.98313E+10	4.90885E+10	3.24794E+10
14	7.15000E-04	1.23310E-03	5929.74	3440.01	.246366	7.73588E+10	5.08336E+10	3.10337E+10
15	7.14800E-04	1.29360E-03	5932.83	3278.48	.280195	7.21718E+10	5.47241E+10	2.81878E+10
16	7.15800E-04	1.21300E-03	5923.06	3497.55	.232321	7.90671E+10	4.92300E+10	3.20806E+10
17	7.16700E-04	1.22190E-03	5915.55	3471.83	.237281	7.82224E+10	4.96237E+10	3.16106E+10
18	7.21300E-04	1.21380E-03	5876.1	3494.39	.226435	7.85474E+10	4.78543E+10	3.20227E+10
19	7.19500E-04	1.24820E-03	5890.93	3397.2	.260864	7.57179E+10	5.06538E+10	3.02662E+10
20	7.22200E-04	1.30020E-03	5868.72	3260.14	.276836	7.11794E+10	5.31592E+10	2.78733E+10
21	7.20500E-04	1.35740E-03	5881.28	3120.87	.300025	6.66166E+10	5.66540E+10	2.55427E+10
22	7.18300E-04	1.26720E-03	5899.45	3345.01	.263088	7.41266E+10	5.21477E+10	2.93434E+10
23	7.21000E-04	1.21730E-03	5877.17	3483.42	.229231	7.82330E+10	4.81548E+10	3.18219E+10
24	7.11700E-04	1.21310E-03	5951.81	3493.93	.237094	7.92092E+10	5.02138E+10	3.20142E+10
25	7.11700E-04	1.21810E-03	5950.39	3478.62	.240397	7.87264E+10	5.05427E+10	3.17344E+10
26	7.11900E-04	1.22200E-03	5947.29	3466.59	.242704	7.83282E+10	5.07381E+10	3.15152E+10
27	7.11700E-04	1.21450E-03	5947.55	3487.37	.238026	7.89715E+10	5.02412E+10	3.18941E+10
28	7.09100E-04	1.20750E-03	5969.55	3507.77	.236307	7.97876E+10	5.04297E+10	3.22685E+10
29	7.09800E-04	1.22440E-03	5963.62	3458.91	.246532	7.82216E+10	5.14342E+10	3.13757E+10
30	7.09700E-04	1.21640E-03	5963.04	3481.04	.241521	7.89073E+10	5.08792E+10	3.17785E+10
31	7.10000E-04	1.21860E-03	5960.5	3474.7	.242614	7.86892E+10	5.09540E+10	3.16628E+10
32	7.11900E-04	1.22000E-03	5943.03	3469.84	.241411	7.83937E+10	5.05266E+10	3.15744E+10
33	7.13400E-04	1.23160E-03	5929.02	3436.04	.247153	7.72292E+10	5.09064E+10	3.09622E+10
34	7.14200E-04	1.24130E-03	5922.32	3408.94	.252251	7.63266E+10	5.13467E+10	3.04758E+10
35	7.16900E-04	1.24050E-03	5899.82	3411.16	.248919	7.62227E+10	5.05963E+10	3.05155E+10
36	7.15000E-04	1.24020E-03	5914.22	3411.18	.250745	7.63350E+10	5.10421E+10	3.05158E+10
37	7.11600E-04	1.23180E-03	5942.73	3434.66	.249207	7.72942E+10	5.13665E+10	3.09373E+10
38	7.11000E-04	1.23060E-03	5944.95	3436.4	.249107	7.73663E+10	5.13939E+10	3.09687E+10

Table C:3.38  $day\#$ ,  $t_p$ ,  $t_s$ ,  $V_p$ ,  $V_s$ ,  $\nu$ ,  $E_d$ ,  $K_d$ , and  $G_d$ , for survey # 9 at day 349 after the heater was turned on in cross section M7-M9.

LINE #	DISTANCE (M)
3	4.207
4	4.206
5	4.206
6	4.206
7	4.206
8	4.205
9	4.205
10	4.204
11	4.205
12	4.204
13	4.203
14	4.203
15	4.204
16	4.203
17	4.203
18	4.202
19	4.202
20	4.202
21	4.201
22	4.201
23	4.199
24	4.198
25	4.197
26	4.196
27	4.196
28	4.196
29	4.195
30	4.195
31	4.194
32	4.193
33	4.193
34	4.193
35	4.192
36	4.192
37	4.192
38	4.19

DENSITY : 2622.5 KG/M<sup>3</sup>

INSTRUMENT DELAY FOR P-WAVE : 6.20000E-06 SEC.

INSTRUMENT DELAY FOR S-WAVE : 1.13000E-05 SEC.

PROFILE AND FILE NAME : M7-M9 SURUF.10

DATE FOR FIELD WORK : 17 OCT.1979 DAYS AFTER HEATER TURN ON : 419 PROCESS DATE : 20 JAN,1981

LINE #	P-TIME (SEC)	S-TIME (SEC)	P-VELOCITY (M/SEC)	S-VELOCITY (M/SEC)	POISS.RATIO	YOUNGS MOD (PA)	BULK MOD (PA)	SHEAR MOD (PA)
3	7.18900E-04	1.24520E-03	5902.9	3409.51	.249676	7.61953E+10	5.07311E+10	3.04860E+10
4	7.19500E-04	1.24620E-03	5895.54	3405.94	.249652	7.60343E+10	5.06192E+10	3.04222E+10
5	7.20600E-04	1.24810E-03	5887.46	3400.71	.24965	7.58007E+10	5.04631E+10	3.03288E+10
6	7.26100E-04	1.25760E-03	5842.48	3374.79	.249637	7.46488E+10	4.96936E+10	2.98682E+10
7	7.29300E-04	1.26320E-03	5816.62	3359.69	.249673	7.39845E+10	4.92585E+10	2.96016E+10
8	7.27700E-04	1.26040E-03	5828.14	3366.42	.249655	7.42802E+10	4.94518E+10	2.97203E+10
9	7.28200E-04	1.26130E-03	5824.1	3364	.249675	7.41745E+10	4.93855E+10	2.96775E+10
10	7.32700E-04	1.26910E-03	5786.65	3342.34	.249681	7.32229E+10	4.87530E+10	2.92966E+10
11	7.34500E-04	1.27220E-03	5773.72	3334.92	.249671	7.28974E+10	4.85344E+10	2.91666E+10
12	7.33600E-04	1.27060E-03	5779.49	3338.36	.249646	7.30465E+10	4.86288E+10	2.92269E+10
13	7.38900E-04	1.27980E-03	5736.32	3313.36	.249661	7.19574E+10	4.79066E+10	2.87908E+10
14	7.52300E-04	1.30300E-03	5633.29	3253.85	.249661	6.93958E+10	4.62013E+10	2.77658E+10
15	7.53000E-04	1.30420E-03	5629.35	3251.61	.249654	6.92996E+10	4.61359E+10	2.77275E+10
16	7.71700E-04	1.33660E-03	5490.53	3171.36	.249669	6.59221E+10	4.38899E+10	2.63758E+10
17	7.44300E-04	1.28920E-03	5694.35	3288.99	.249691	7.09044E+10	4.72112E+10	2.83688E+10
18	7.42800E-04	1.28660E-03	5704.59	3294.91	.249689	7.11598E+10	4.73809E+10	2.84710E+10
19	7.36900E-04	1.27630E-03	5750.65	3321.74	.249638	7.23204E+10	4.81440E+10	2.89365E+10
20	7.34800E-04	1.27270E-03	5767.23	3331.22	.249659	7.27350E+10	4.84241E+10	2.91019E+10
21	7.31500E-04	1.26700E-03	5792.09	3345.54	.249667	7.33624E+10	4.88433E+10	2.93528E+10
22	7.24800E-04	1.25540E-03	5846.09	3376.74	.249667	7.47368E+10	4.97583E+10	2.99027E+10
23	7.24100E-04	1.25420E-03	5851.79	3380	.249674	7.48817E+10	4.98561E+10	2.99605E+10
24	7.15900E-04	1.24000E-03	5916.58	3417.43	.249672	7.65494E+10	5.09661E+10	3.06278E+10
25	7.15100E-04	1.23860E-03	5921.85	3420.52	.249663	7.66870E+10	5.10559E+10	3.06831E+10
26	7.16100E-04	1.24030E-03	5912.1	3414.97	.249644	7.64374E+10	5.08858E+10	3.05837E+10
27	7.14000E-04	1.23670E-03	5928.23	3424.19	.249666	7.68519E+10	5.11662E+10	3.07490E+10
28	7.11000E-04	1.23150E-03	5953.46	3438.78	.249662	7.75081E+10	5.16023E+10	3.10116E+10
29	7.11900E-04	1.23300E-03	5945.87	3434.56	.249626	7.73156E+10	5.14668E+10	3.09355E+10
30	7.11800E-04	1.23290E-03	5945.29	3434.02	.249671	7.72942E+10	5.14618E+10	3.09258E+10
31	7.11300E-04	1.23200E-03	5949.51	3436.55	.24965	7.74070E+10	5.15325E+10	3.09715E+10
32	7.12600E-04	1.23430E-03	5937.15	3429.27	.24968	7.70812E+10	5.13219E+10	3.08404E+10
33	7.16200E-04	1.24050E-03	5905.63	3411.16	.249661	7.62679E+10	5.07764E+10	3.05155E+10
34	7.16800E-04	1.24150E-03	5900.65	3408.39	.249637	7.61426E+10	5.06881E+10	3.04659E+10
35	7.19700E-04	1.24660E-03	5876.66	3394.32	.249685	7.55181E+10	5.02821E+10	3.02148E+10
36	7.19900E-04	1.24690E-03	5873.62	3392.68	.249657	7.54437E+10	5.02269E+10	3.01858E+10
37	7.14300E-04	1.23720E-03	5920.07	3419.53	.249654	7.66422E+10	5.10242E+10	3.06653E+10

Table C:3.39  $day\#$ ,  $t_p$ ,  $t_s$ ,  $V_p$ ,  $V_s$ ,  $\nu$ ,  $E_d$ ,  $K_d$ , and  $G_d$ , for survey # 10 at day 419 after the heater was turned on and 21 days after the heater was turned off in cross section M7-M9.

LINE #	DISTANCE
	(M)
3	4.207
4	4.206
5	4.206
6	4.206
7	4.206
8	4.205
9	4.205
10	4.204
11	4.205
12	4.204
13	4.203
14	4.203
15	4.204
16	4.203
17	4.203
18	4.202
19	4.202
20	4.202
21	4.201
22	4.201
23	4.201
24	4.199
25	4.198
26	4.197
27	4.196
28	4.196
29	4.196
30	4.195
31	4.195
32	4.194
33	4.193
34	4.193
35	4.193
36	4.192
37	4.192

DENSITY : 2622.5 KG/M<sup>3</sup>

INSTRUMENT DELAY FOR P-WAVE : 6.20000E-06 SEC.

INSTRUMENT DELAY FOR S-WAVE : 1.13000E-05 SEC.

PROFILE AND FILE NAME : M7-M9 SURV.11

DATE FOR FIELD WORK : 30 JULY,1980 DAYS AFTER HEATER TURN ON : 707 PROCESS DATE : 20 JAN,1981

LINE #	P-TIME (SEC)	S-TIME (SEC)	P-VELOCITY (M/SEC)	S-VELOCITY (M/SEC)	POISS.RATIO	YOUNGS MOD (PA)	BULK MOD (PA)	SHEAR MOD (PA)
1	7.33400E-04	1.23250E-03	5785.2	3444.69	.225361	7.62623E+10	4.62803E+10	3.11183E+10
2	7.24600E-04	1.24440E-03	5854.68	3410.92	.243091	7.58560E+10	4.92106E+10	3.05111E+10
3	7.21000E-04	1.22430E-03	5885.56	3468.26	.234005	7.78549E+10	4.87822E+10	3.15456E+10
4	7.20500E-04	1.23160E-03	5888.28	3446.69	.239391	7.72252E+10	4.93876E+10	3.11545E+10
5	7.22000E-04	1.25180E-03	5875.94	3390.57	.250422	7.53958E+10	5.03488E+10	3.01481E+10
6	7.31900E-04	1.24000E-03	5795.78	3423.13	.232143	7.67275E+10	4.71194E+10	3.07300E+10
7	7.36300E-04	1.25040E-03	5760.85	3394.4	.234095	7.45795E+10	4.67456E+10	3.02163E+10
8	7.37100E-04	1.24770E-03	5753.18	3401	.231407	7.47070E+10	4.63570E+10	3.03340E+10
9	7.39900E-04	1.26630E-03	5731.23	3350.6	.240373	7.30369E+10	4.68858E+10	2.94415E+10
10	7.44400E-04	1.31720E-03	5694.93	3219.24	.265201	6.87718E+10	4.88160E+10	2.71782E+10
11	7.45400E-04	1.32210E-03	5688.58	3207.96	.266843	6.83797E+10	4.88797E+10	2.69882E+10
12	7.43300E-04	1.31380E-03	5703.43	3227.64	.264429	6.90891E+10	4.88806E+10	2.73203E+10
13	7.47200E-04	1.29000E-03	5672.06	3286.93	.247199	7.06745E+10	4.65942E+10	2.83333E+10
14	7.51500E-04	1.34520E-03	5639.34	3150.91	.273057	6.62927E+10	4.86854E+10	2.60368E+10
15	7.50100E-04	1.32530E-03	5651.3	3199.39	.264156	6.78705E+10	4.79629E+10	2.68442E+10
16	7.48500E-04	1.33280E-03	5662.13	3180.48	.26952	6.73549E+10	4.87064E+10	2.65277E+10
17	7.52200E-04	1.32890E-03	5634.05	3189.89	.264099	6.74649E+10	4.76647E+10	2.66850E+10
18	7.52900E-04	1.35220E-03	5627.43	3133.72	.275259	6.56845E+10	4.87113E+10	2.67534E+10
19	7.41000E-04	1.36280E-03	5718.56	3109.14	.290175	6.54145E+10	5.19595E+10	2.53510E+10
20	7.35500E-04	1.37610E-03	5761.69	3078.84	.300166	6.46425E+10	5.39135E+10	2.48593E+10
21	7.33400E-04	1.38560E-03	5776.95	3056.83	.305664	6.39861E+10	5.48476E+10	2.45052E+10
22	7.27800E-04	1.23570E-03	5821.79	3431.07	.233912	7.61883E+10	4.77213E+10	3.08727E+10
23	7.24600E-04	1.23110E-03	5847.72	3444.01	.234466	7.67985E+10	4.82038E+10	3.11060E+10
24	7.18000E-04	1.22800E-03	5899.13	3451.14	.239828	7.74518E+10	4.96157E+10	3.12349E+10
25	7.16700E-04	1.26960E-03	5908.51	3336.25	.265968	7.39069E+10	5.26331E+10	2.91899E+10
26	7.16800E-04	1.22650E-03	5906.28	3453.75	.240186	7.75916E+10	4.97739E+10	3.12822E+10
27	7.14900E-04	1.23930E-03	5920.7	3416.94	.250302	7.65658E+10	5.11057E+10	3.06189E+10
28	7.11800E-04	1.23800E-03	5946.71	3420.56	.252775	7.68799E+10	5.18287E+10	3.06838E+10
29	7.11800E-04	1.21710E-03	5946.71	3479.85	.23963	7.87332E+10	5.03982E+10	3.17567E+10
30	7.12200E-04	1.22280E-03	5941.93	3462.65	.242888	7.81618E+10	5.06664E+10	3.14436E+10
31	7.12300E-04	1.22020E-03	5941.08	3470.1	.241096	7.83852E+10	5.04597E+10	3.15790E+10
32	7.13000E-04	1.22910E-03	5933.79	3443.91	.246019	7.75131E+10	5.08653E+10	3.11043E+10
33	7.14700E-04	1.23410E-03	5918.14	3429.02	.247313	7.69236E+10	5.07370E+10	3.08357E+10
34	7.15700E-04	1.27240E-03	5909.8	3324.87	.268446	7.35475E+10	5.29377E+10	2.89912E+10
35	7.18900E-04	1.26980E-03	5883.26	3331.74	.263942	7.35895E+10	5.19571E+10	2.91111E+10
36	7.17600E-04	1.26980E-03	5892.61	3330.95	.265206	7.36280E+10	5.22642E+10	2.90972E+10
37	7.13100E-04	1.24950E-03	5930.12	3385.56	.258229	7.56425E+10	5.21448E+10	3.00591E+10
38	7.11800E-04	1.22610E-03	5939.89	3449.13	.245648	7.77247E+10	5.09299E+10	3.11985E+10

Table C:3.40  $day\#$ ,  $t_p$ ,  $t_s$ ,  $V_p$ ,  $V_s$ ,  $\nu$ ,  $E_d$ ,  $K_d$ , and  $G_d$ , for survey # 11 at day 707 after the heater was turned on and 309 days after the heater was turned off in cross section M7-M9.

LINE # DISTANCE

(M)

1	4.207
2	4.206
3	4.207
4	4.206
5	4.206
6	4.206
7	4.206
8	4.205
9	4.205
10	4.204
11	4.205
12	4.204
13	4.203
14	4.203
15	4.204
16	4.203
17	4.203
18	4.202
19	4.202
20	4.201
21	4.201
22	4.201
23	4.199
24	4.198
25	4.197
26	4.196
27	4.196
28	4.196
29	4.195
30	4.195
31	4.194
32	4.193
33	4.193
34	4.193
35	4.192
36	4.192
37	4.192
38	4.19

DENSITY : 2622.5 KG/M<sup>3</sup>

INSTRUMENT DELAY FOR P-WAVE : 6.20000E-06 SEC.

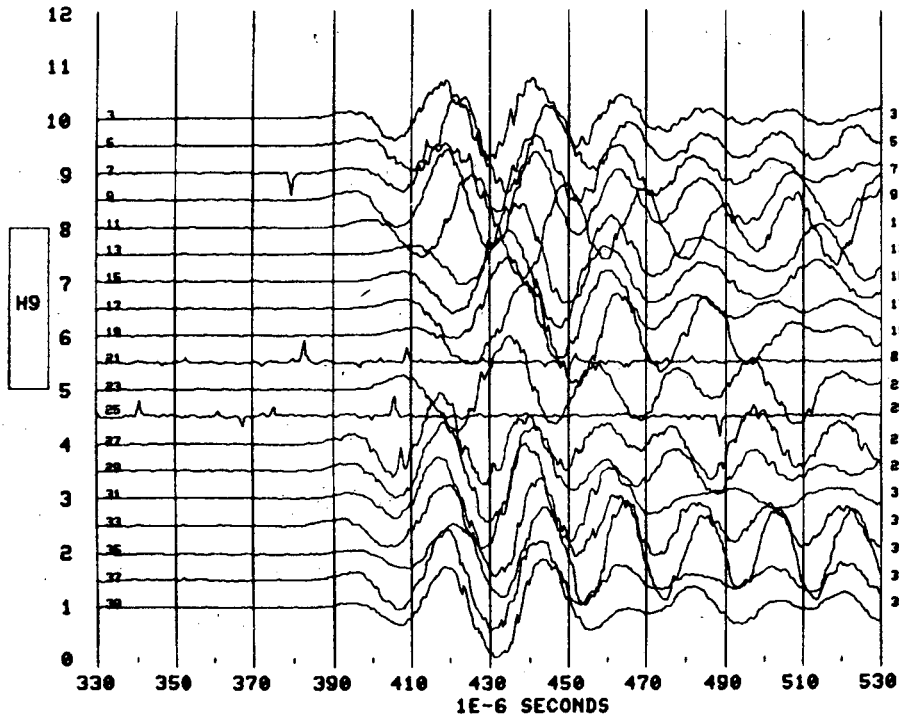
INSTRUMENT DELAY FOR S-WAVE : 1.13000E-05 SEC.

### Appendix C:4 - P waveforms from surveys in six cross sections.

In this appendix the P-waveforms from the cross-hole ultrasonic surveys between the four monitor holes in the H9 area. The order in which the cross sections are presented is the same as in previous appendices starting with cross section M7-M6. In this cross section four surveys were performed. In cross section M7-M8, which follows, and in cross section M8-M9 as well as in cross section M6-M9 five surveys were performed during the course of the H9 heater experiment. The two main cross sections M8-M6 and M7-M9 follows both with 8 surveys presented.

The data is presented so the distance between two consecutive numbers represents a vertical distance of 0.25 m. In using this convention the heater shown in each figure is placed on the right level relative to the P wave signals.

PROFILE AND FILE NAME : M7-M6, SURVA.1  
 DATE FOR FIELD WORK : 780711 HEATER DAYS : -44 PLOTDATE : 821117



PROFILE AND FILE NAME : M7-M6, SURVA.2  
 DATE FOR FIELD WORK : 790803 HEATER DAYS : 344 PLOTDATE : 821117

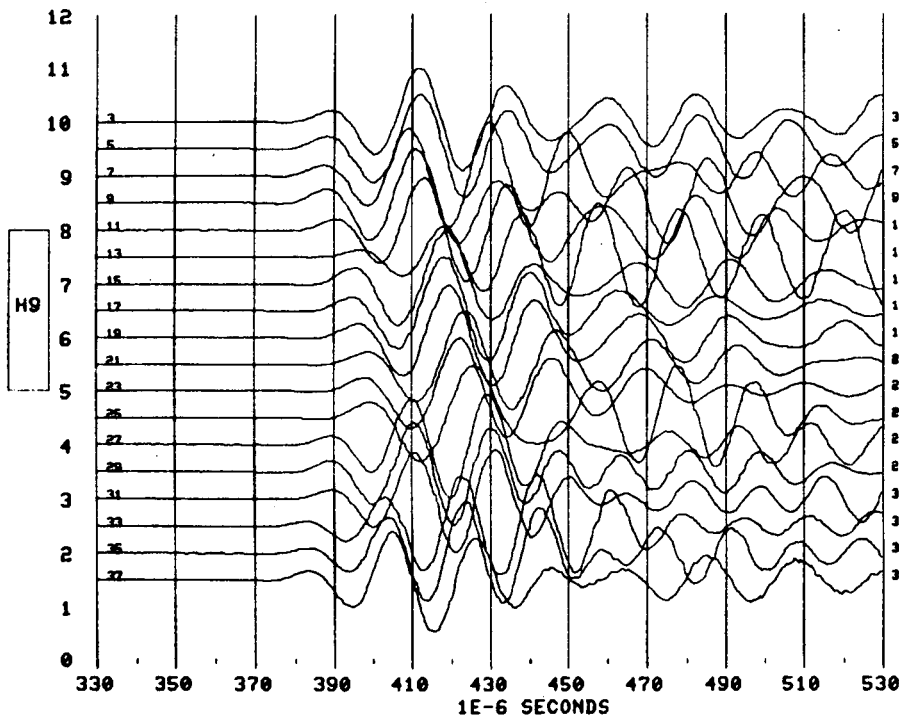
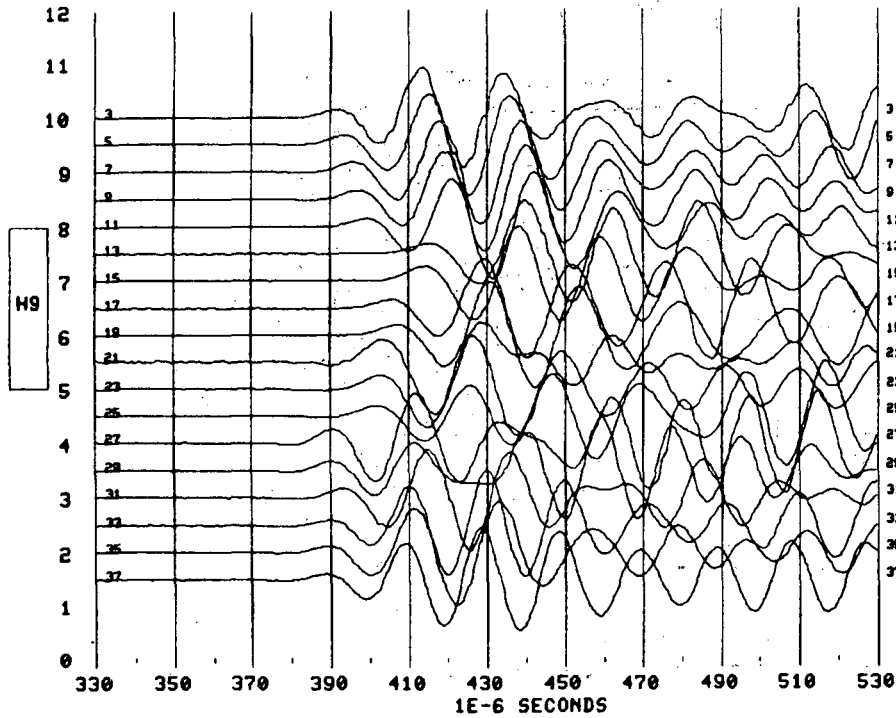


Fig. C:4.1a P waves for survey # 1 in cross section M7-M6

Fig. C:4.1b P waves for survey # 2 in cross section M7-M6



PROFILE AND FILE NAME : M7-M6, SURVA.3  
 DATE FOR FIELD WORK : 791022 HEATER DAYS : 424 PLOTDATE : 821117



PROFILE AND FILE NAME : M7-M6, SURVA.4  
 DATE FOR FIELD WORK : 800725 HEATER DAYS : 701 PLOTDATE : 821117

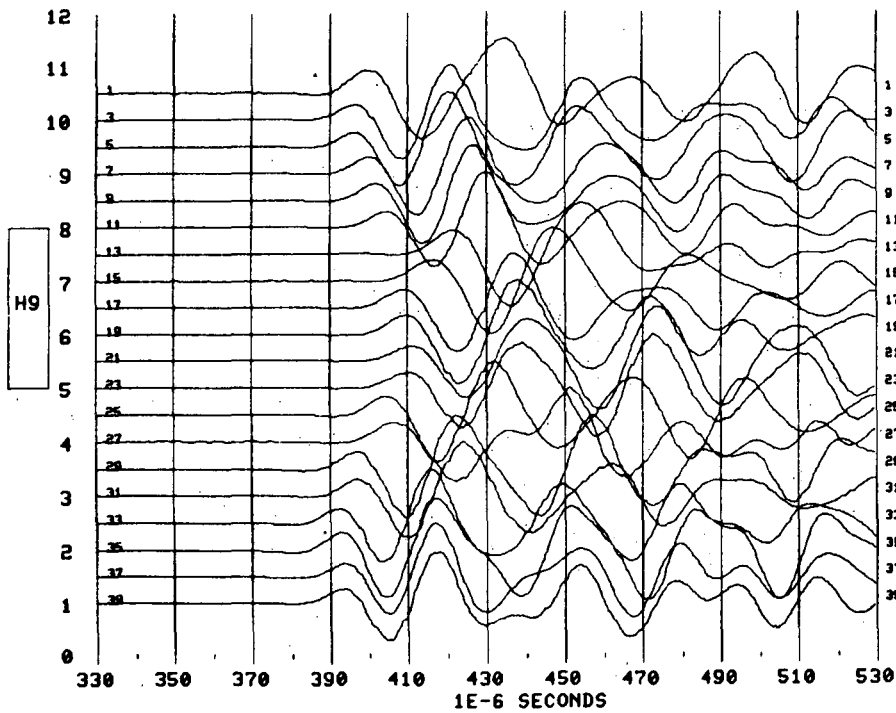
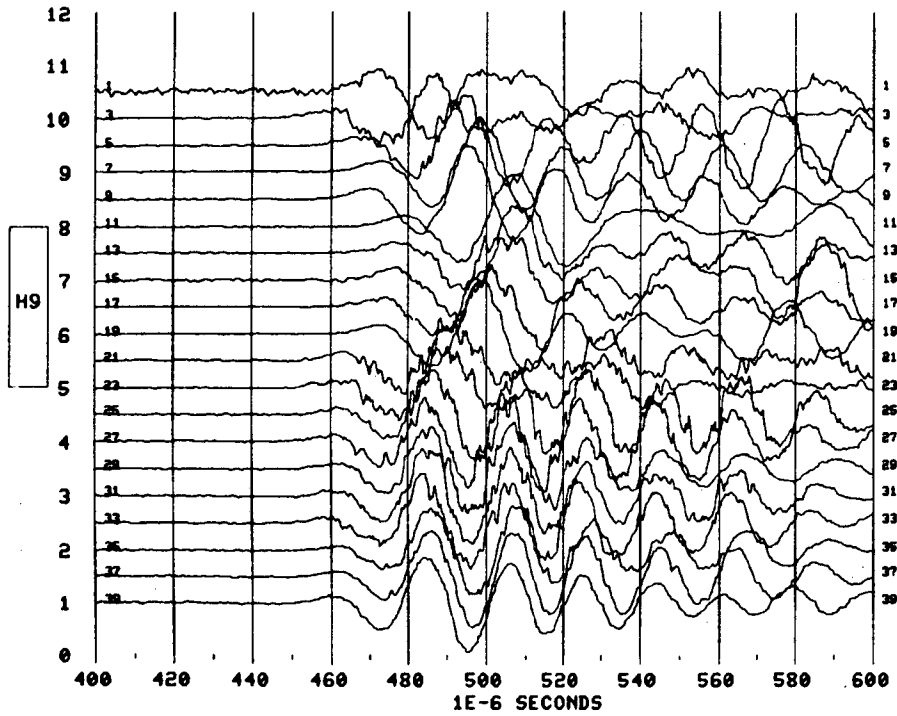


Fig. C.4.1c P waves for survey # 3 in cross section M7-M6

Fig. C.4.1d P waves for survey # 4 in cross section M7-M6

PROFILE AND FILE NAME : M7-M8, SURUB.1, P-WAVES  
 DATE FOR FIELD WORK : 780713 HEATER DAYS : -44 PLOTDATE : 821117



PROFILE AND FILE NAME : M7-M8, SURUB.2, P-WAVES  
 DATE FOR FIELD WORK : 781214 HEATER DAYS : 112 PLOTDATE : 821117

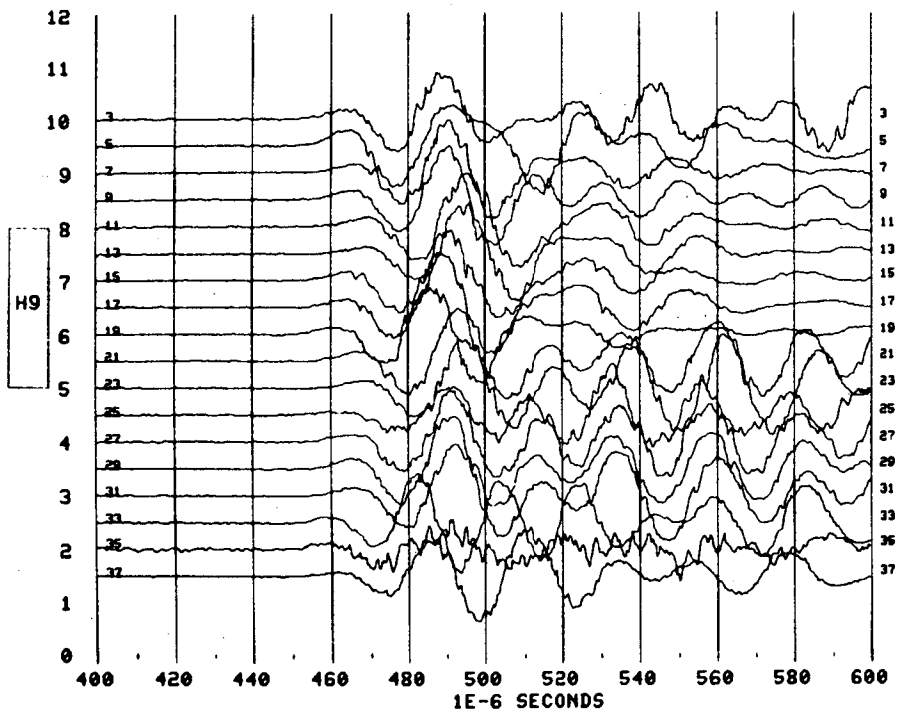
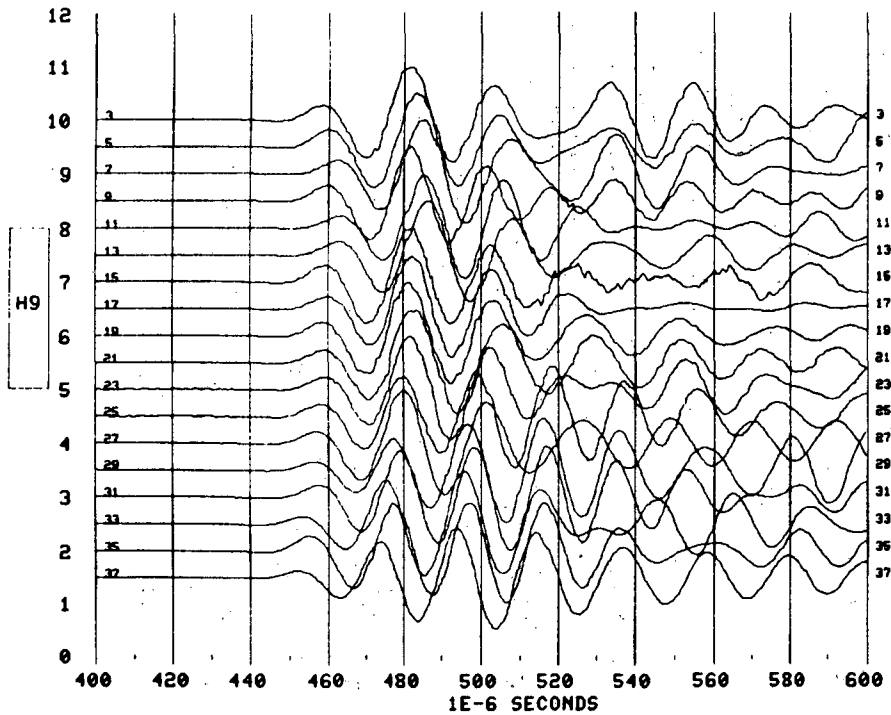


Fig. C:4.2a P waves for survey # 1 in cross section M7-M8

Fig. C:4.2b P waves for survey # 2 in cross section M7-M8

PROFILE AND FILE NAME : M7-M8, SURUB.3, P-WAVES  
 DATE FOR FIELD WORK : 790807 HEATER DAYS : 348 PLOTDATE : 821117



PROFILE AND FILE NAME : M7-M8, SURUB.4, P-WAVES  
 DATE FOR FIELD WORK : 791023 HEATER DAYS : 425 PLOTDATE : 821117

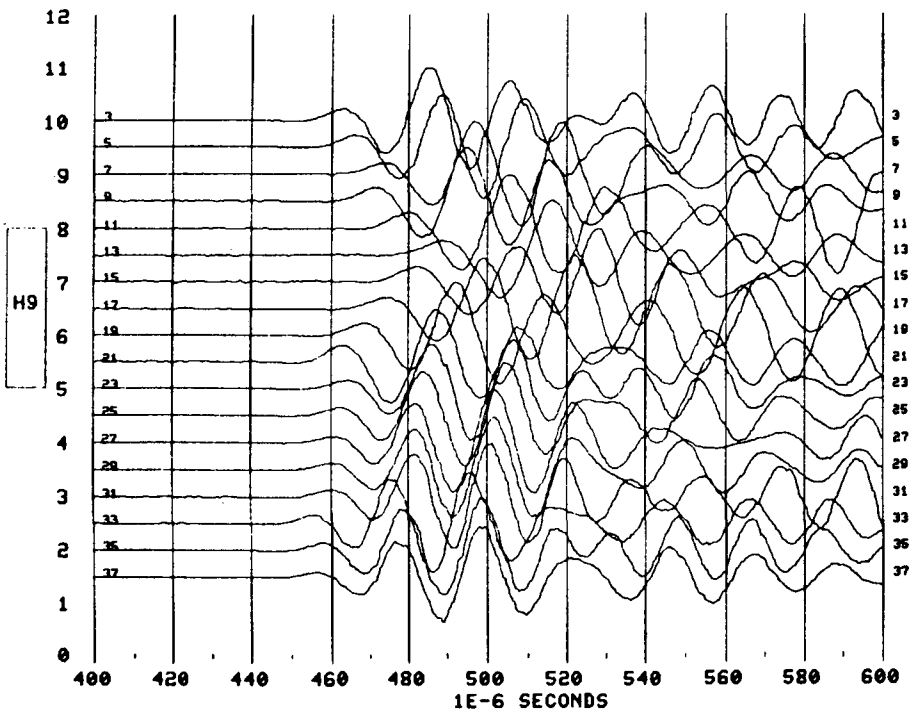


Fig. C:4.2c P waves for survey # 3 in cross section M7-M8

Fig. C:4.2d P waves for survey # 4 in cross section M7-M8

PROFILE AND FILE NAME : M7-M8, SURUB.5, P-WAVES  
DATE FOR FIELD WORK : 800801 HEATER DAYS : 708 PLOTDATE : 821117

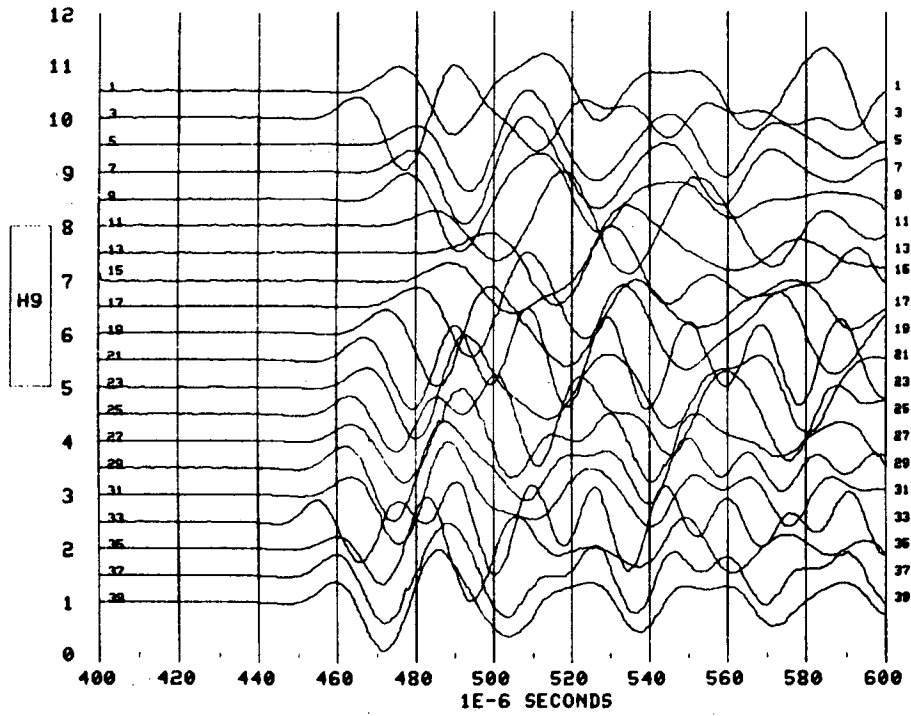
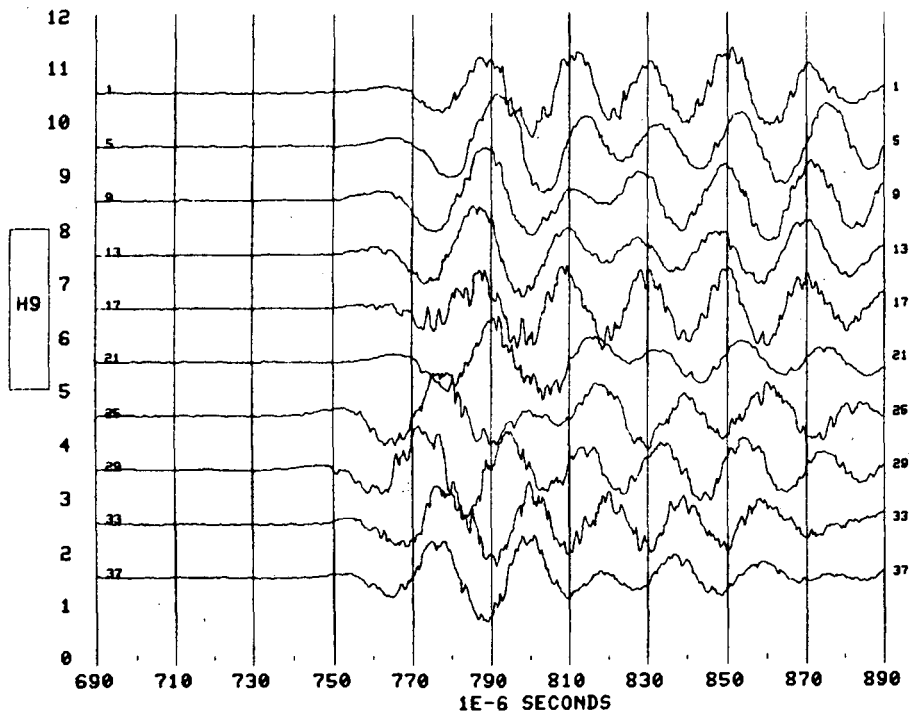


Fig. C.4.2e P waves for survey # 5 in cross section M7-M8

PROFILE AND FILE NAME : M8-M9, SURUC.1, P-WAVES  
DATE FOR FIELD WORK : 780713 HEATER DAYS : -42 PLOTDATE : 821117



PROFILE AND FILE NAME : M8-M9, SURUC.2, P-WAVES  
DATE FOR FIELD WORK : 781220 HEATER DAYS : 118 PLOTDATE : 821117

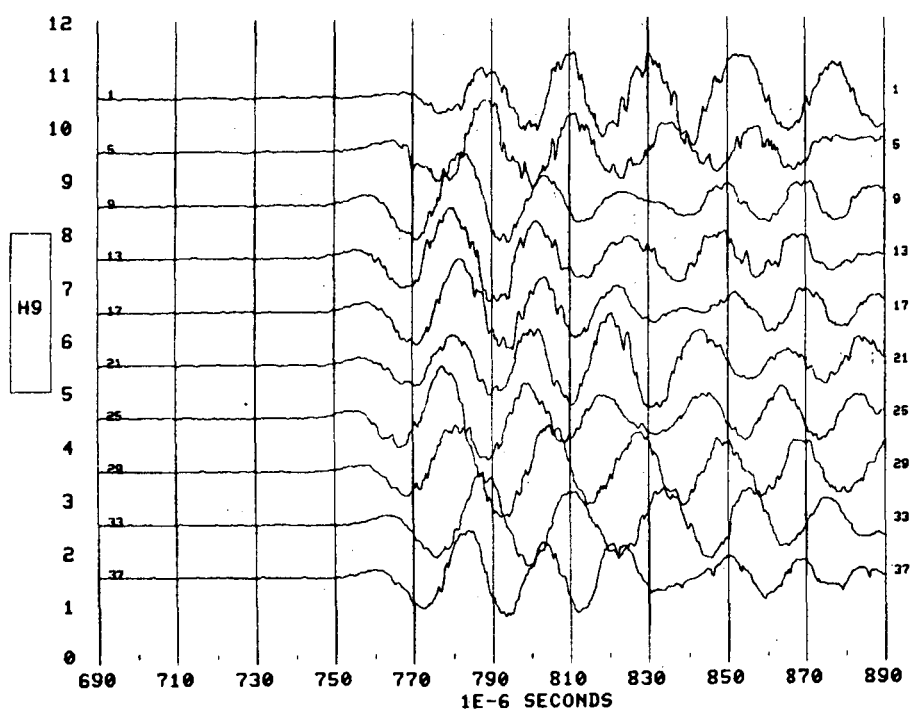
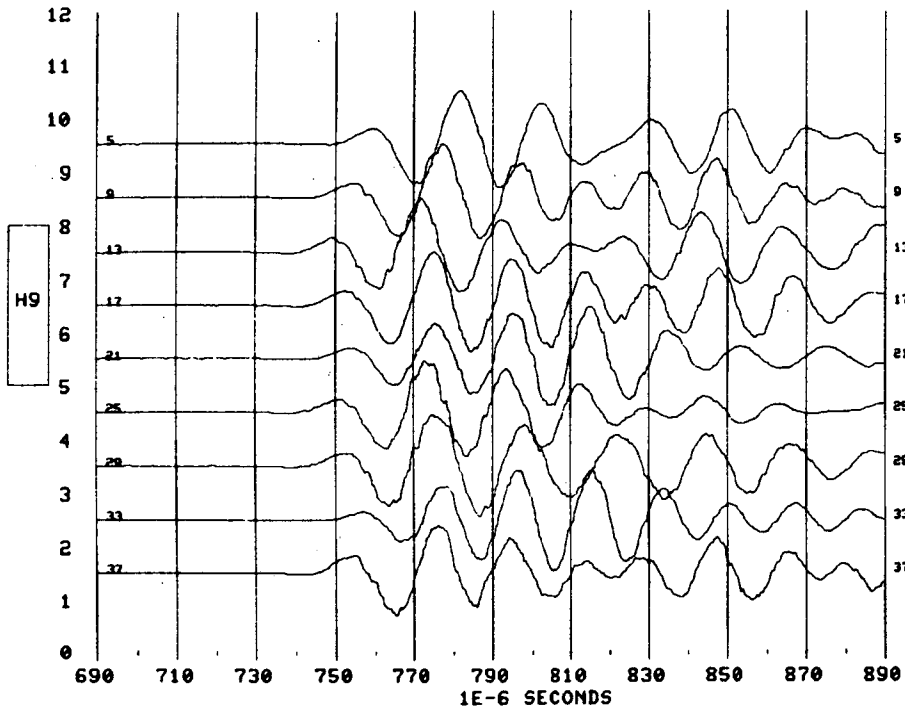


Fig. C:4.3a P waves for survey # 1 in cross section M8-M9

Fig. C:4.3b P waves for survey # 2 in cross section M8-M9

PROFILE AND FILE NAME : M8-M9, SURUC.3, P-WAVES  
 DATE FOR FIELD WORK : 790802 HEATER DAYS : 343 PLOTDATE : 821117



PROFILE AND FILE NAME : M8-M9, SURUC.4, P-WAVES  
 DATE FOR FIELD WORK : 791023 HEATER DAYS : 425 PLOTDATE : 821117

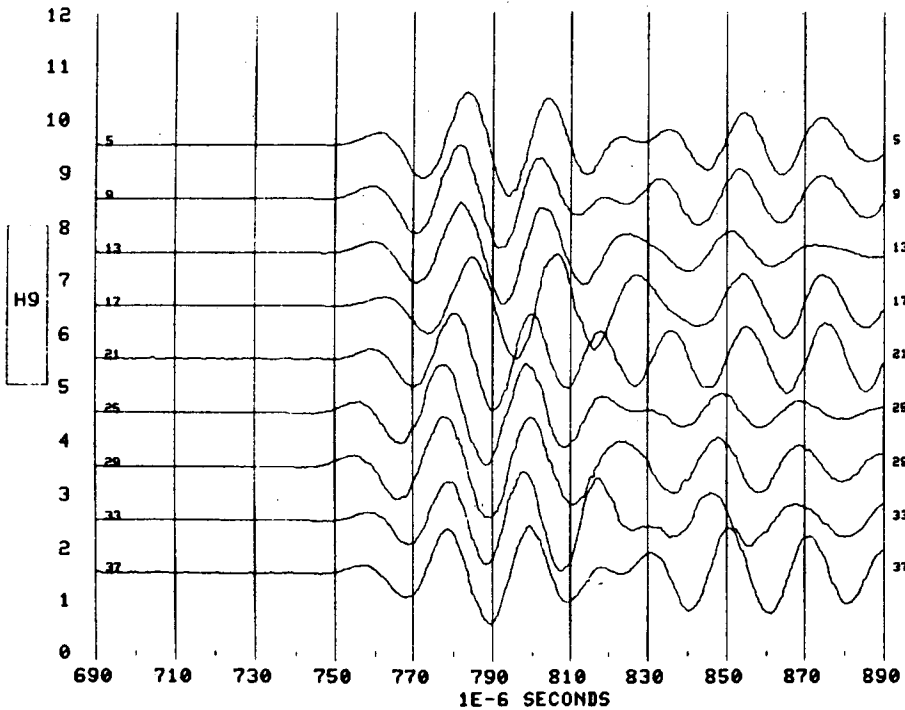


Fig. C:4.3c P waves for survey # 3 in cross section M8-M9

Fig. C:4.3d P waves for survey # 4 in cross section M8-M9

PROFILE AND FILE NAME : M8-M9, SURUC.5, P-WAVES  
DATE FOR FIELD WORK : 800805 HEATER DAYS : 711 PLOTDATE : 821117

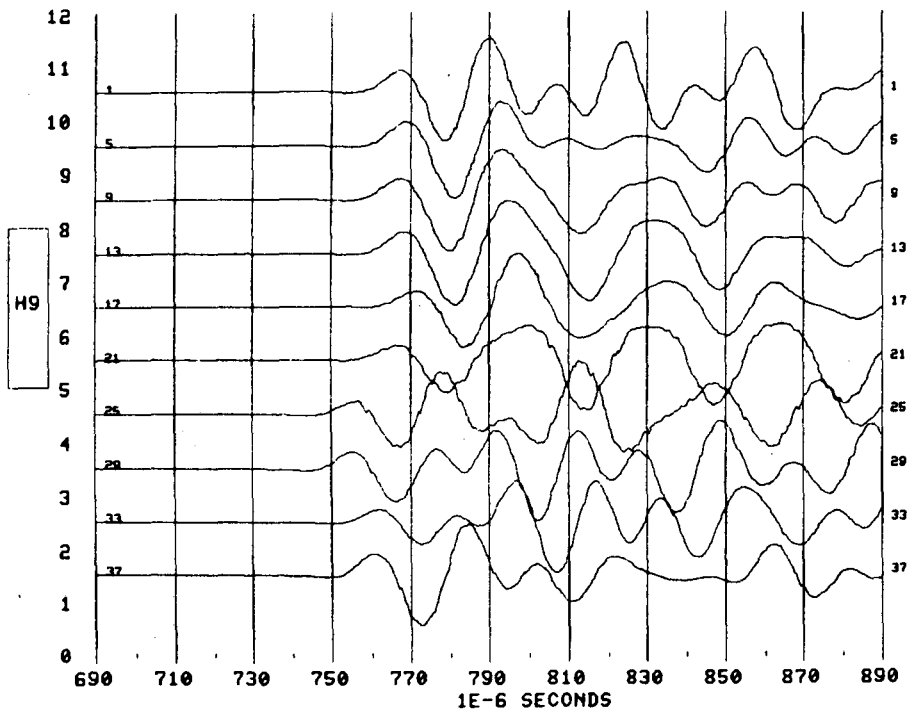
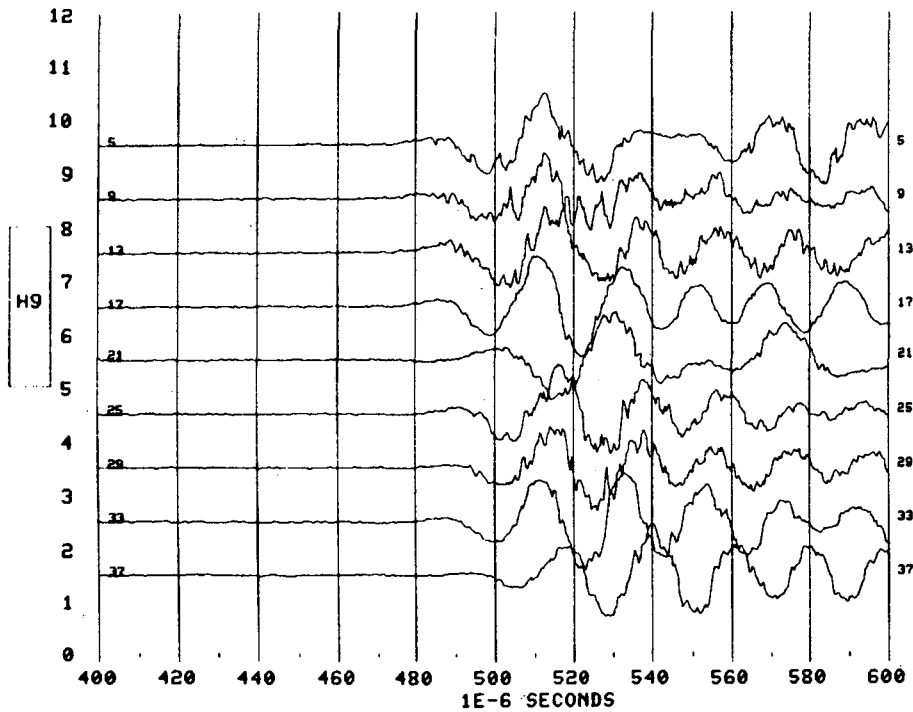


Fig. C:4.3e P waves for survey # 5 in cross section M8-M9

PROFILE AND FILE NAME : M6-M9, SURUD.1, P-WAVES  
 DATE FOR FIELD WORK : 780713 HEATER DAYS : -42 PLOTDATE : 821117



PROFILE AND FILE NAME : M6-M9, SURUD.2, P-WAVES  
 DATE FOR FIELD WORK : 781221 HEATER DAYS : 119 PLOTDATE : 821117

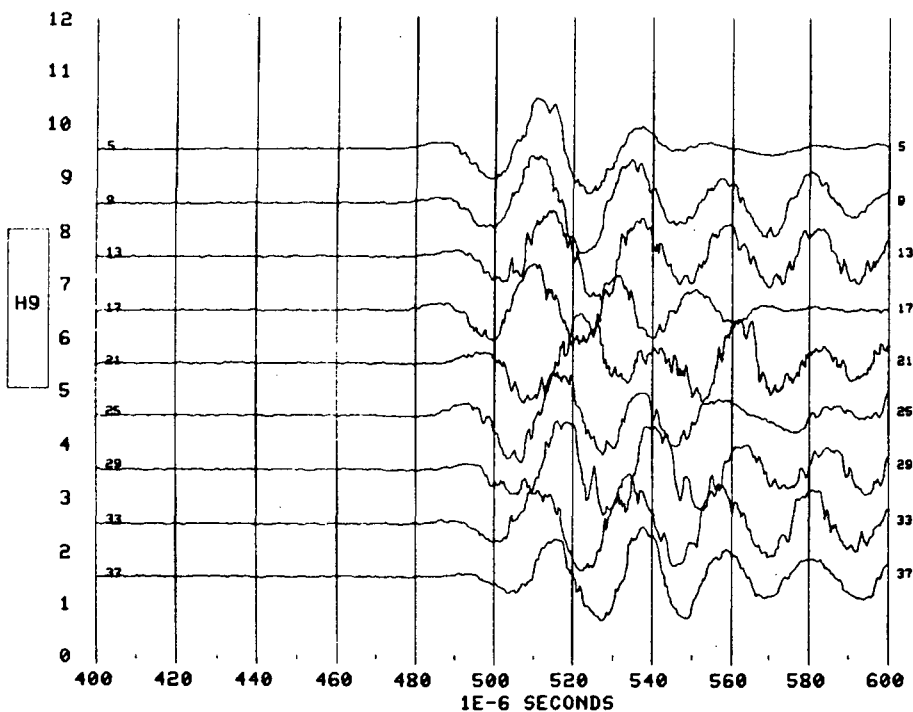
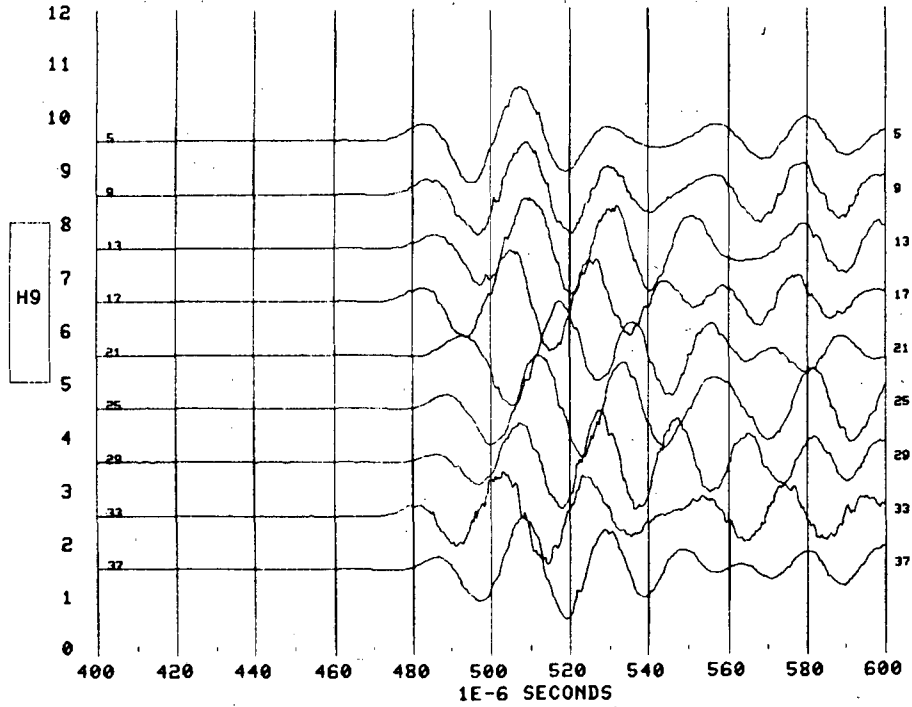


Fig. C:4.4a P waves for survey # 1 in cross section M6-M9

Fig. C:4.4b P waves for survey # 2 in cross section M6-M9



PROFILE AND FILE NAME : M6-M9, SURUD.3, P-WAVES  
DATE FOR FIELD WORK : 790802 HEATER DAYS : 343 PLOTDATE : 821117



PROFILE AND FILE NAME : M6-M9, SURUD.4, P-WAVES  
DATE FOR FIELD WORK : 791024 HEATER DAYS : 426 PLOTDATE : 821117

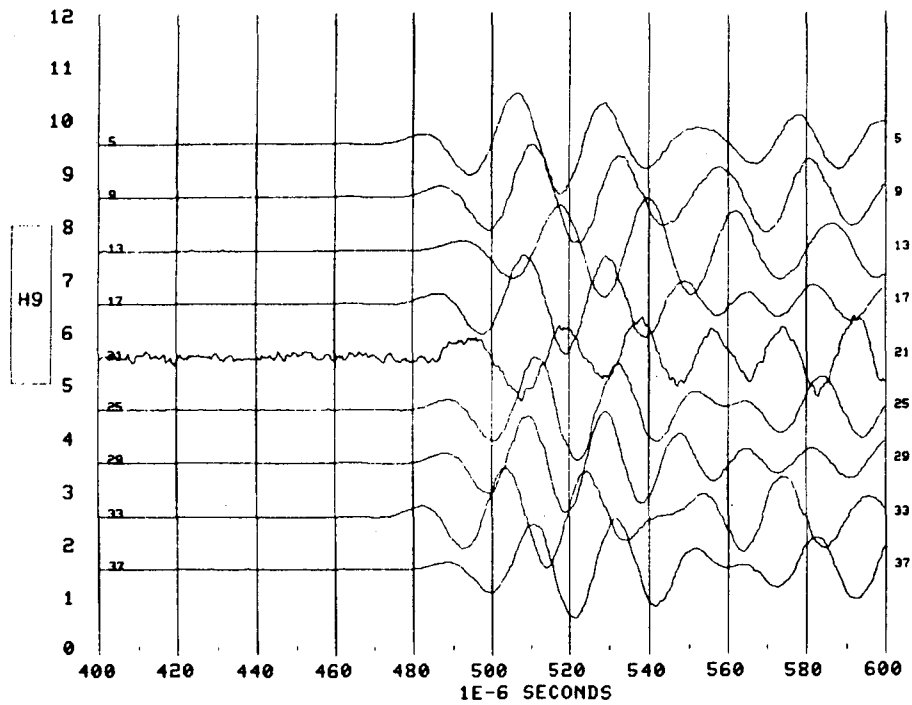


Fig. C:4.4c P waves for survey # 3 in cross section M6-M9

Fig. C:4.4d P waves for survey # 4 in cross section M6-M9

PROFILE AND FILE NAME : M6-M9, SURUD.5, P-WAVES  
DATE FOR FIELD WORK : 80083 HEATER DAYS : 710 PLOTDATE : 821117

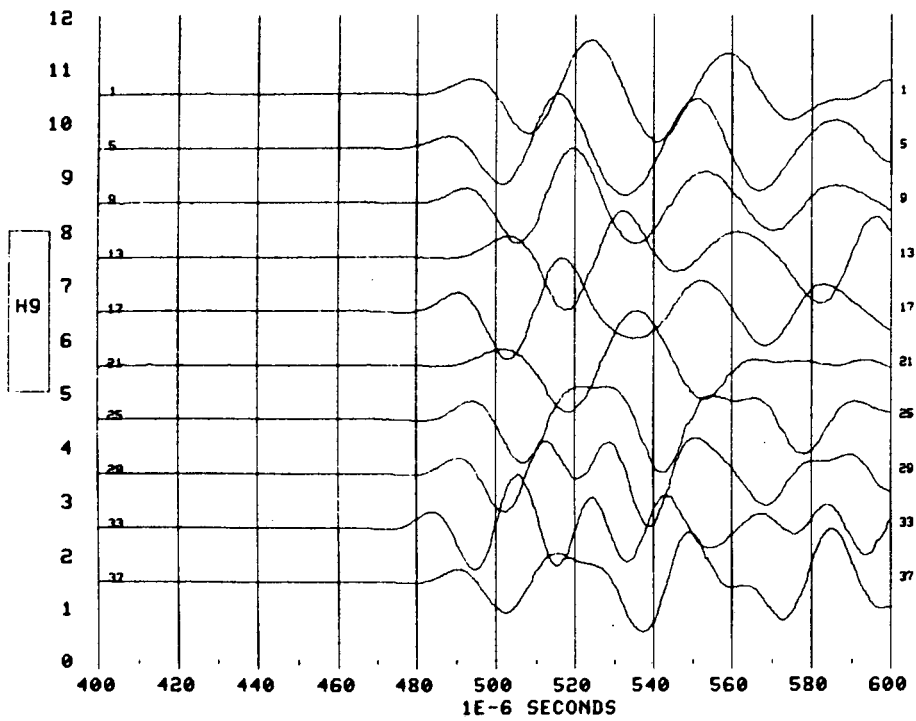
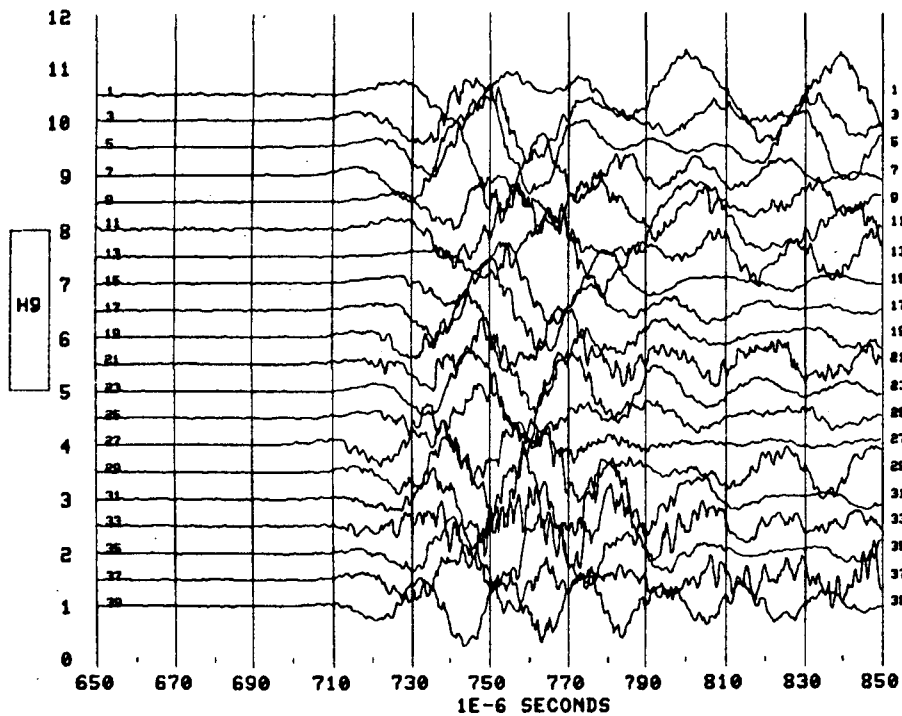


Fig. C:4.4e P waves for survey # 5 in cross section M6-M9

PROFILE AND FILE NAME : M8-M6, SURVE.1  
 DATE FOR FIELD WORK : 780711 HEATER DAYS : -44 PLOTDATE : 821115



PROFILE AND FILE NAME : M8-M6, SURVE.2  
 DATE FOR FIELD WORK : 780817 HEATER DAYS : -7 PLOTDATE : 821115

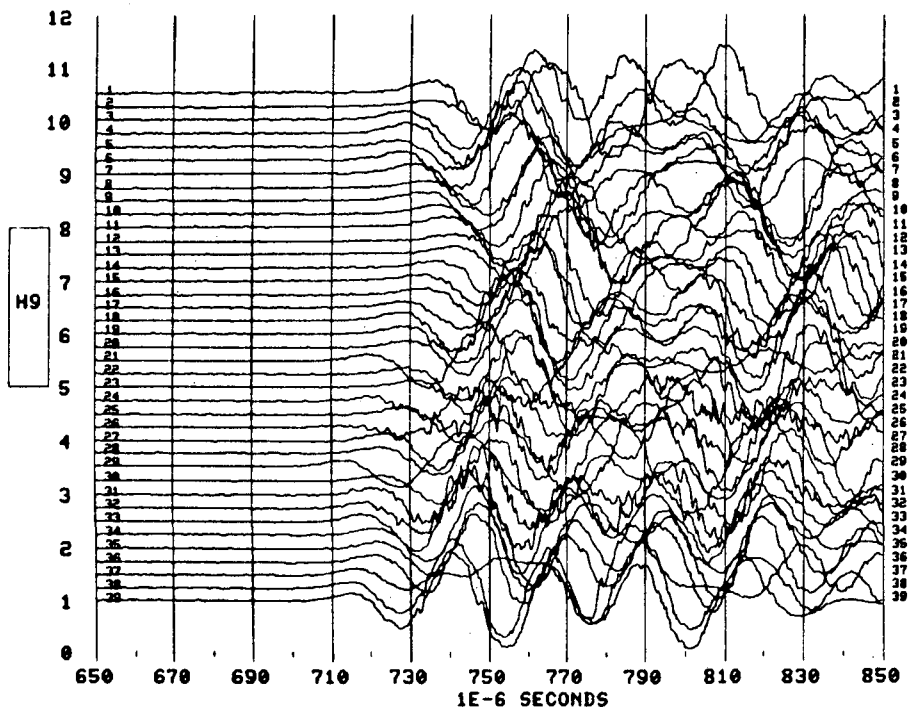
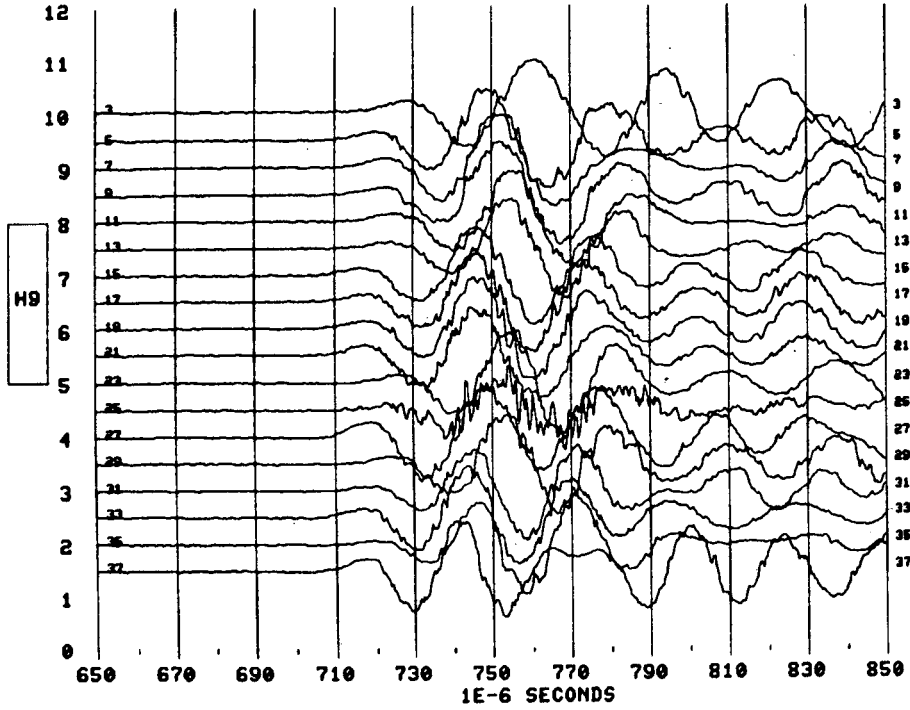


Fig. C:4.5a P waves for survey # 1 in cross section M8-M6

Fig. C:4.5b P waves for survey # 2 in cross section M8-M6

PROFILE AND FILE NAME : M8-M6, SURVE.5  
 DATE FOR FIELD WORK : 780913 HEATER DAYS : 20 PLOTDATE : 821115



PROFILE AND FILE NAME : M8-M6, SURVE.6  
 DATE FOR FIELD WORK : 781213 HEATER DAYS : 111 PLOTDATE : 821115

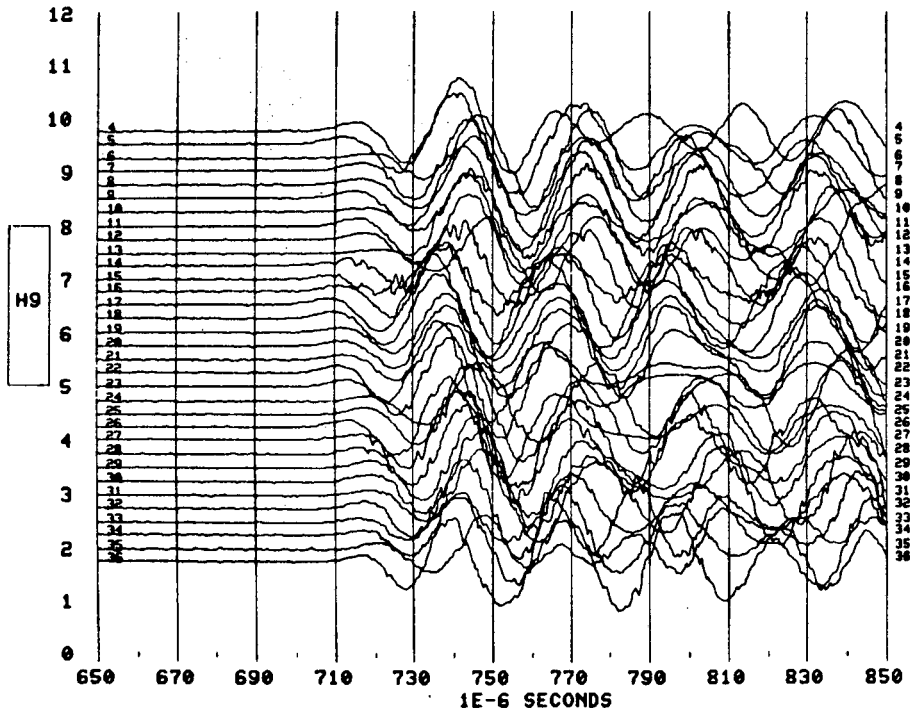
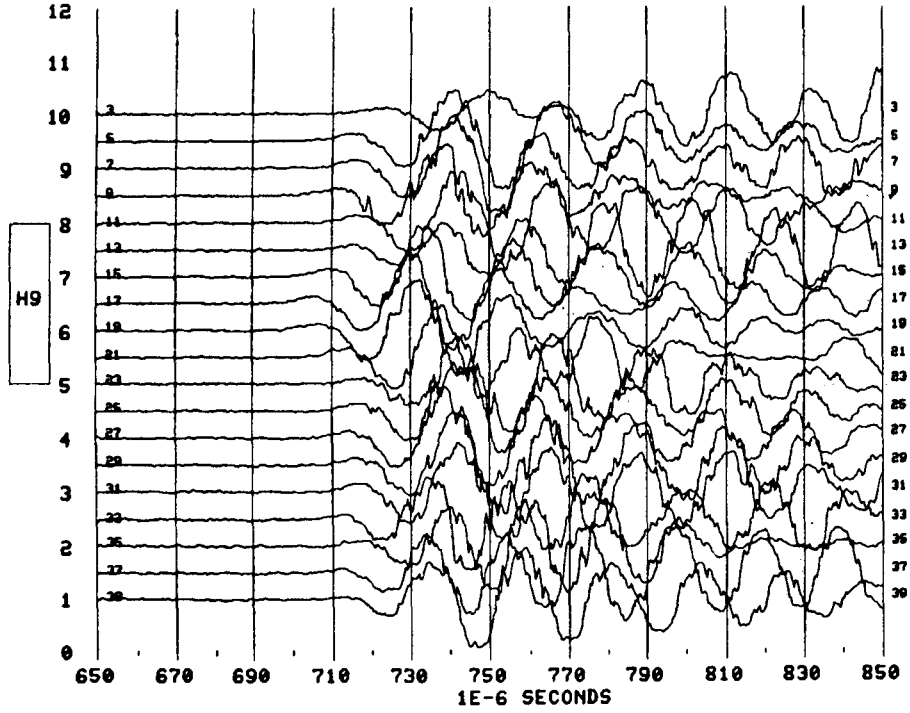


Fig. C:4.5c P waves for survey # 5 in cross section M8-M6

Fig. C:4.5d P waves for survey # 6 in cross section M8-M6

PROFILE AND FILE NAME : M8-M6, SURVE.7  
DATE FOR FIELD WORK : 781220 HEATER DAYS : 118 PLOTDATE : 821115



PROFILE AND FILE NAME : M8-M6, SURVE.8  
DATE FOR FIELD WORK : 790712 HEATER DAYS : 341 PLOTDATE : 821115

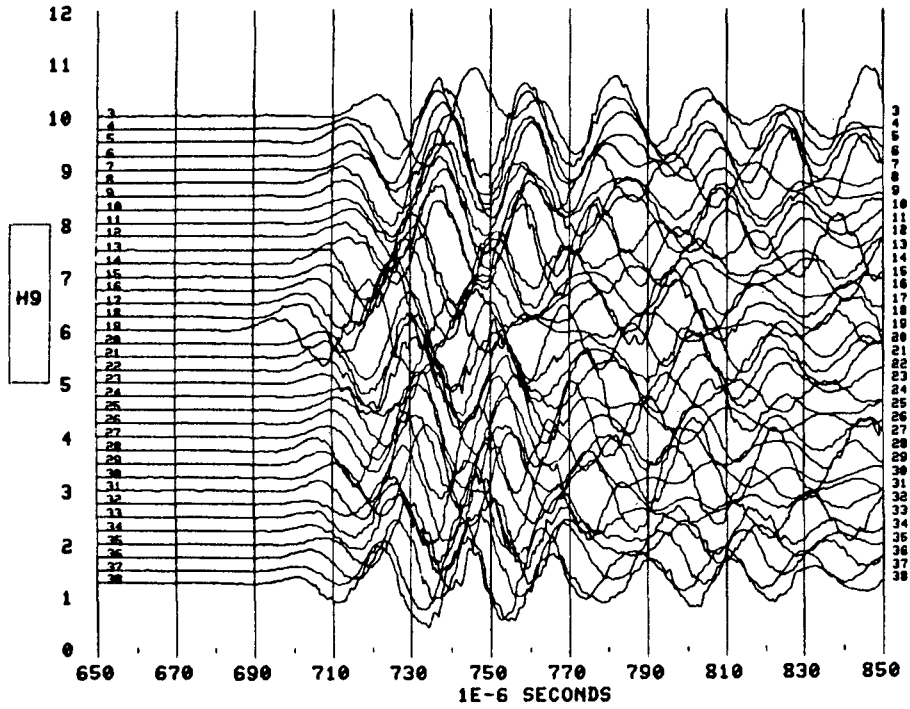
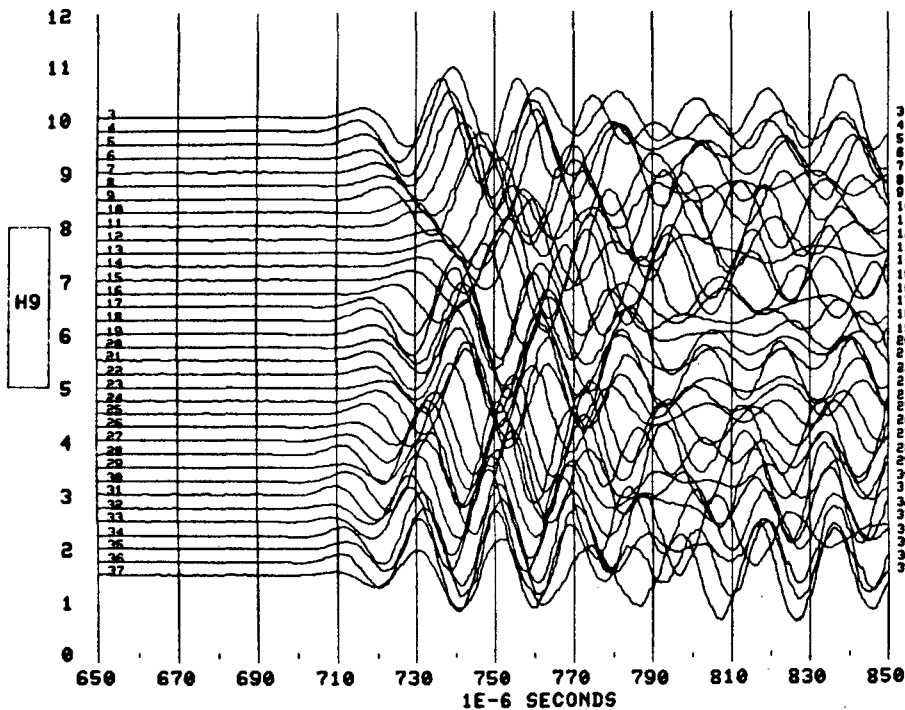


Fig. C:4.5e P waves for survey # 7 in cross section M8-M6

Fig. C:4.5f P-waves for survey # 8 in cross section M8-M6

PROFILE AND FILE NAME : M8-M6, SURVE.9  
DATE FOR FIELD WORK : 791018 HEATER DAYS : 420 PLOTDATE : 821115



PROFILE AND FILE NAME : M8-M6, SURVE.10  
DATE FOR FIELD WORK : 800728 HEATER DAYS : 704 PLOTDATE : 821115

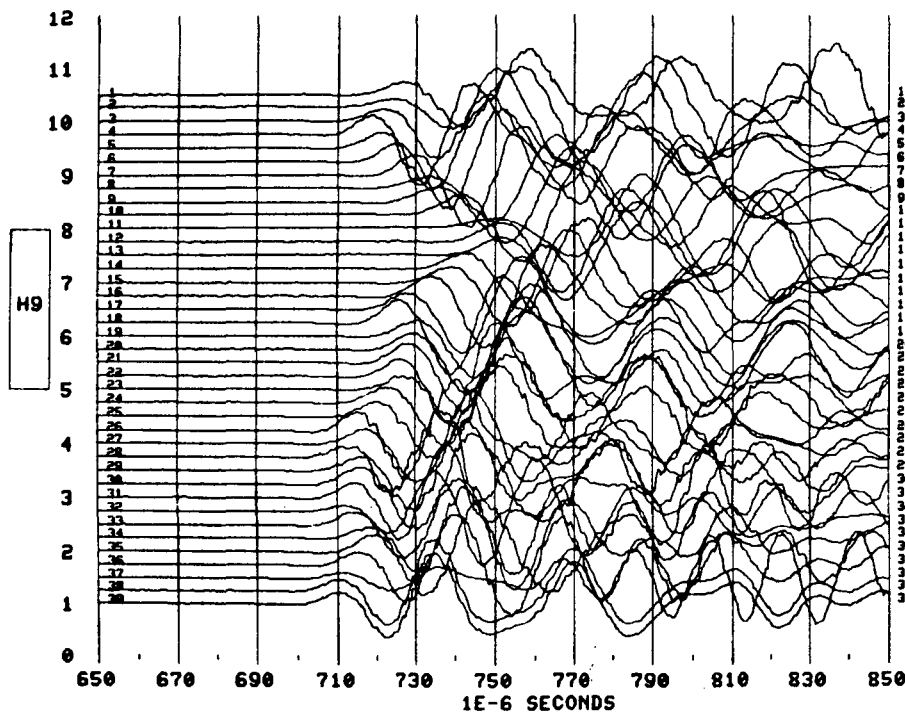
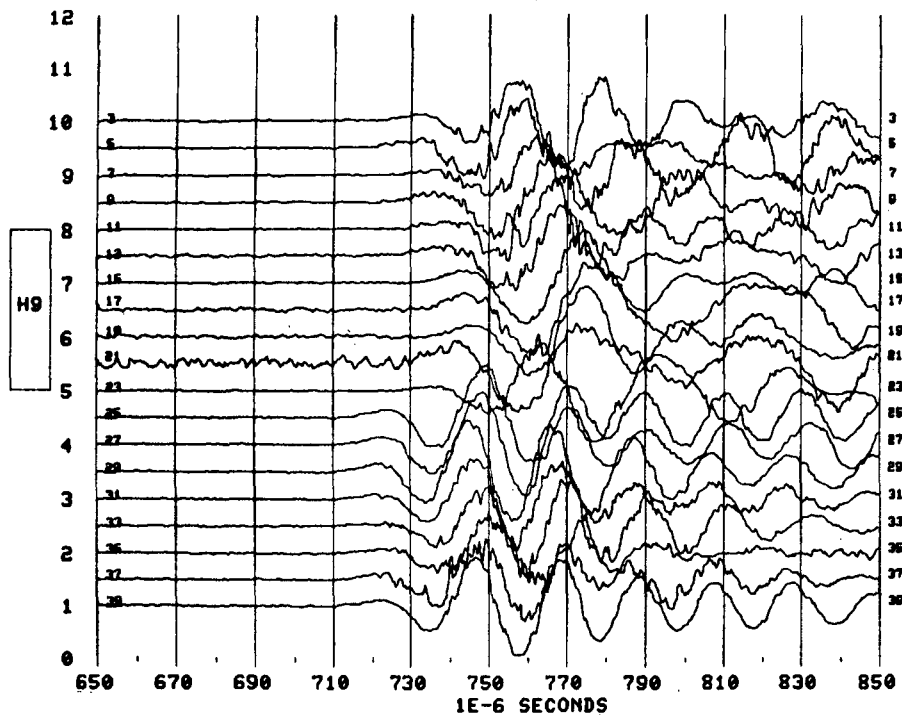


Fig. C:4.5g P waves for survey # 9 in cross section M8-M6

Fig. C:4.5h P waves for survey # 10 in cross section M8-M6

PROFILE AND FILE NAME : M7-M9, SURUF.1  
 DATE FOR FIELD WORK : 780712 HEATER DAYS : -43 PLOTDATE : 821115



PROFILE AND FILE NAME : M7-M9, SURUF.2  
 DATE FOR FIELD WORK : 780823 HEATER DAYS : 0 PLOTDATE : 821115

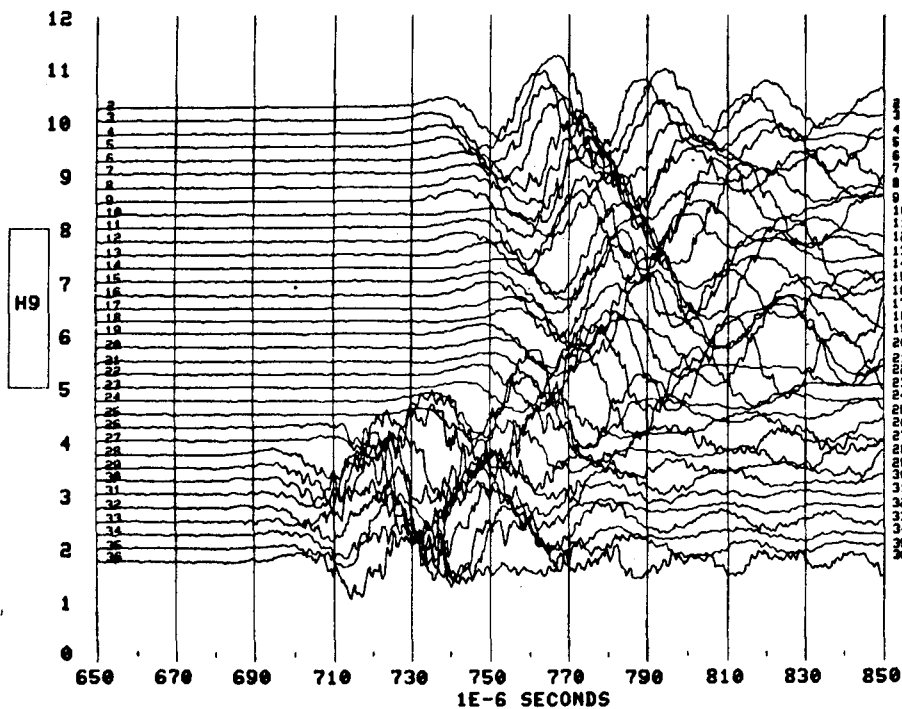
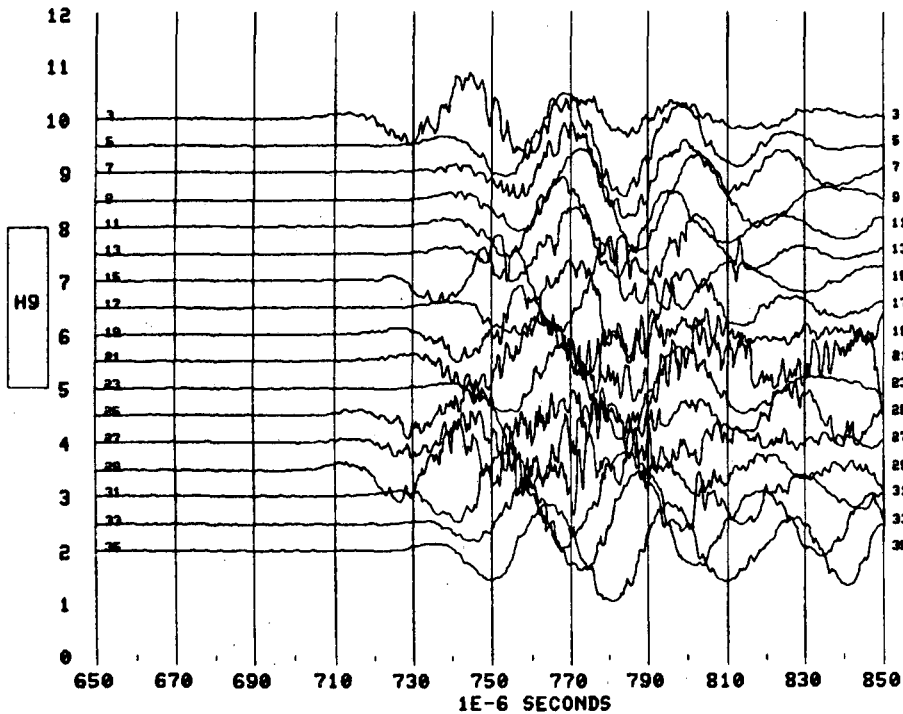


Fig. C-4.6a P waves for survey # 1 in cross section M7-M9

Fig. C-4.6b P waves for survey # 2 in cross section M7-M9 Lines 28-36 were digitized with a delay error of 20  $\mu$ s.

PROFILE AND FILE NAME : M7-M9, SURUF.4  
 DATE FOR FIELD WORK : 780907 HEATER DAYS : 13 PLOTDATE : 821115



PROFILE AND FILE NAME : M7-M9, SURUF.5  
 DATE FOR FIELD WORK : 780914 HEATER DAYS : 20 PLOTDATE : 821115

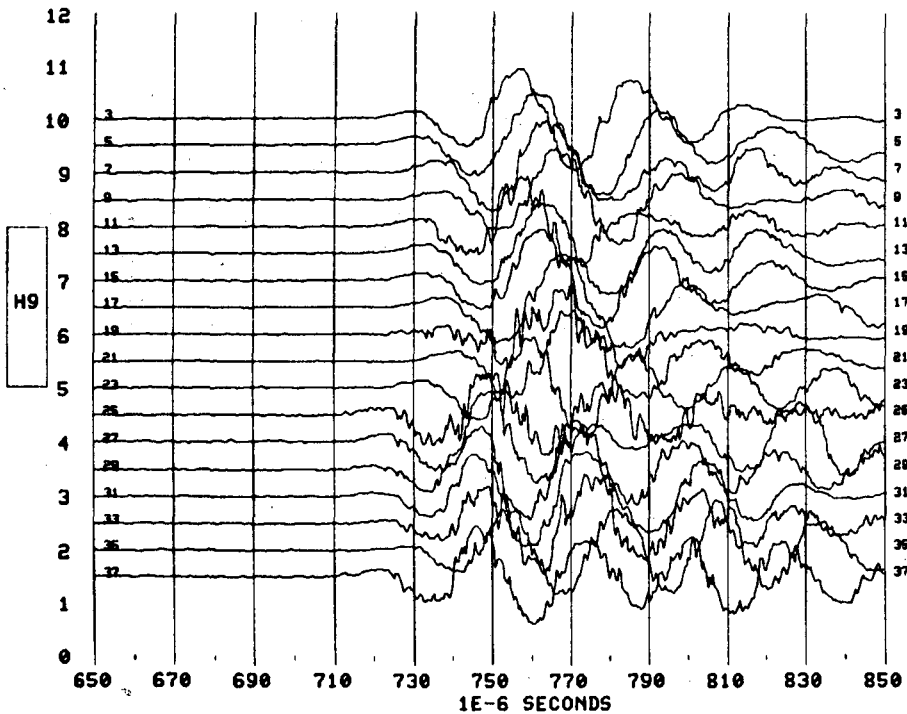
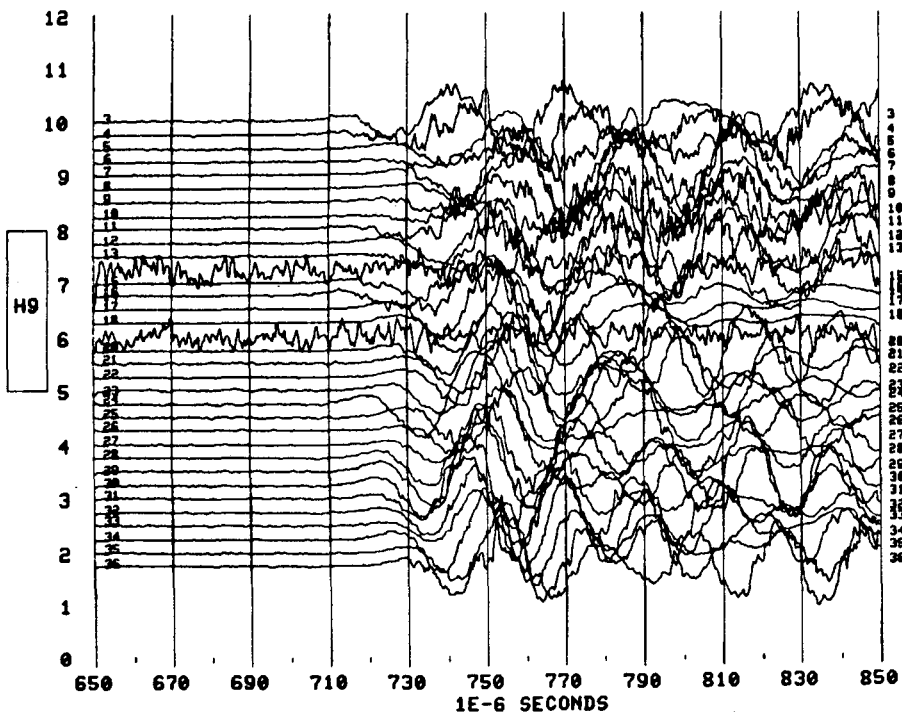


Fig. C:4.6c P waves for survey # 4 in cross section M7-M9

Fig. C:4.6d P waves for survey # 5 in cross section M7-M9



PROFILE AND FILE NAME : M7-M9, SURUF.6  
DATE FOR FIELD WORK : 781213 HEATER DAYS : 111 PLOTDATE : 821115



PROFILE AND FILE NAME : M7-M9, SURUF.9  
DATE FOR FIELD WORK : 790808 HEATER DAYS : 349 PLOTDATE : 821115

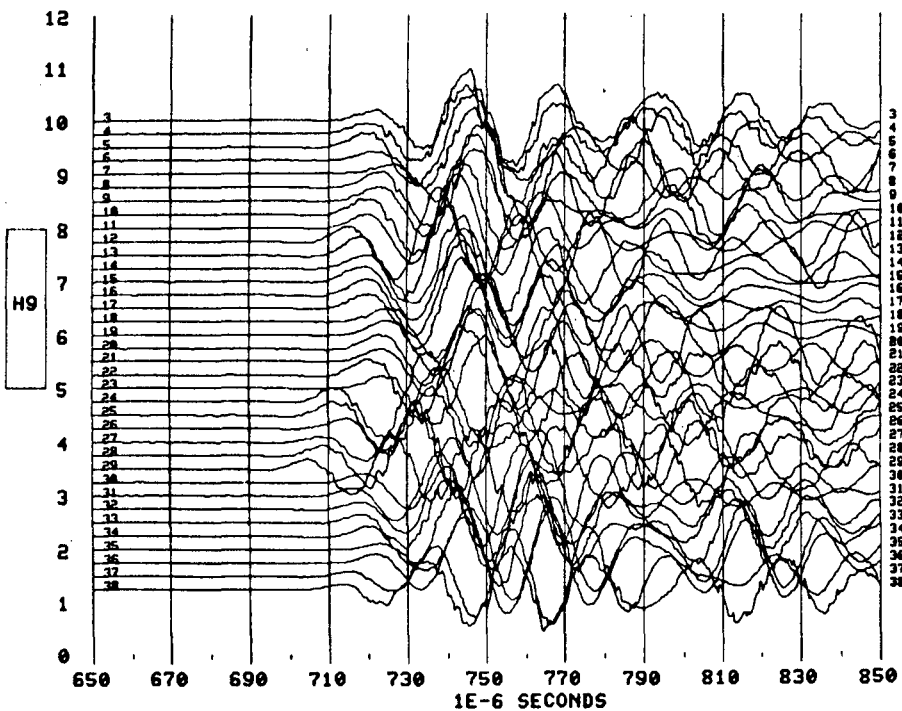


Fig. C:4.6e P waves for survey # 6 in cross section M7-M9

Fig. C:4.6f P waves for survey # 9 in cross section M7-M9

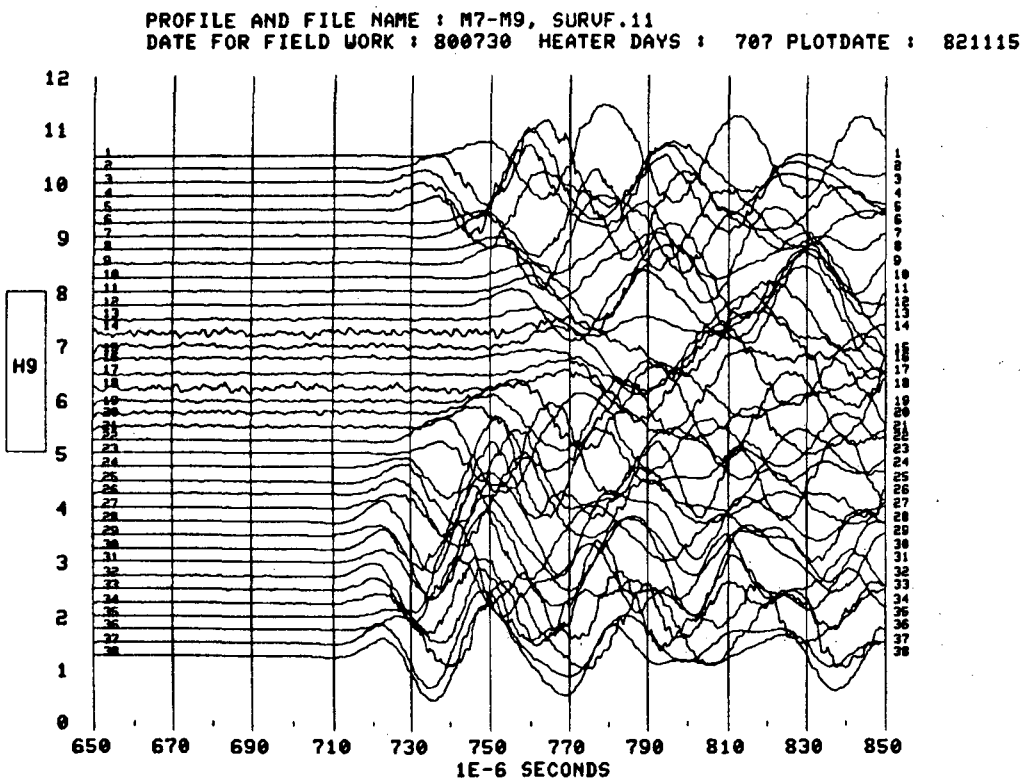
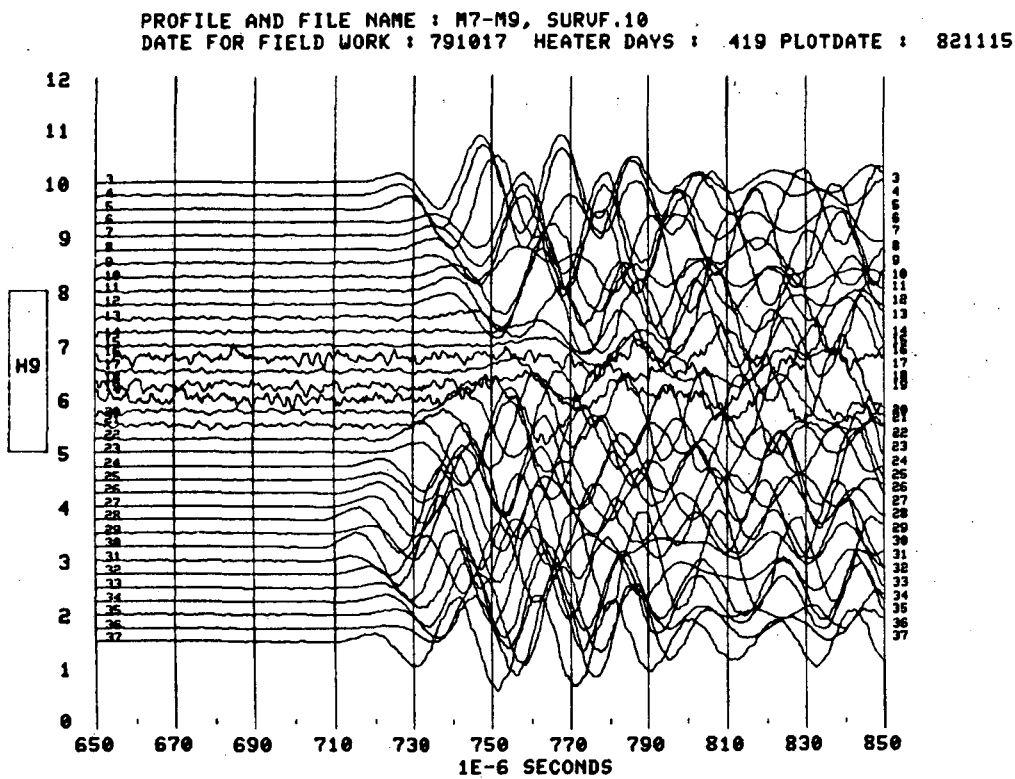


Fig. C:4.6g P waves for survey # 10 in cross section M7-M9

Fig. C:4.6h P waves for survey # 11 in cross section M7-M9

## Appendix D:1 - Tables and figures for Q-values in monitor and reference line.

In this appendix the Q values are presented in table form as well as being graphed with the one graph for each monitor line. By plotting all the Q - values in one graph the individual curve is obscured.

D:1.1

D:1.2

M7-M6 #	DAY #	Q-VALUE	VELOCITY	M8-M9 #	DAY #	Q-VALUE	VELOCITY
1	-44	15.2641	5686	1	-42	18.6588	5868
2	21	15.7293	5919	2	21	16.1526	5980
3	50	15.4482	5816	3	50	15.1934	5929
4	57	12.8249	5800	4	57	14.9519	5924
5	64	12.6778	5814	5	64	15.2511	5924
6	78	12.596	5851	6	78	15.8434	5951
7	91	12.8576	5877	7	91	16.0861	5940
8	110	15.1213	5871	8	110	16.4754	5952
9	133	18.2563	5859	9	118	17.9671	5952
10	159	18.9314	5905	10	133	19.2328	5952
11	176	18.5777	5902	11	159	19.6448	5946
12	195	17.3833	5895	12	176	19.6618	5939
13	210	16.0394	5900	13	195	19.3708	5948
14	222	16.1951	5912	14	210	19.5192	5943
15	238	19.1306	5919	15	222	20.5464	5940
16	252	19.6692	5914	16	238	21.8127	5955
17	267	19.6398	5888	17	252	21.5677	5946
18	286	18.9133	5888	18	267	20.4	5965
19	330	18.7944	5859	19	271	20.2256	5940
20	333	18.6473	5903	20	306	20.9197	5949
21	334	18.6072	5874	21	330	21.8735	5944
22	335	19.3996	5868	22	333	23.2744	5938
23	337	20.2391	5858	23	334	24.1594	5938
24	344	21.4915	5855	24	335	24.2568	5936
25	351	22.494	5853	25	337	22.7834	5935
26	382	26.2496	585	26	343	21.8134	5938
27	376	19.2781	5861	27	344	21.8464	5927
28	383	19.793	5872	28	351	21.4849	5928
29	398	20.8559	5852	29	362	19.8819	5925
30	399	21.3549	5854	30	376	19.3347	5936
31	399	21.2555	5854	31	383	21.6552	5928
32	400	20.0328	5845	32	398	25.2971	5934
33	400	18.3844	5845	33	399	26.9816	5940
34	403	17.5155	5866	34	399	27.4349	5940
35	403	17.4477	5886	35	400	27.4782	5940
36	404	18.4264	5785	36	400	27.5732	5940
37	405	19.4224	5779	37	403	27.9491	5932
38	406	19.3061	5894	38	403	28.0737	5932
39	410	19.3907	5754	39	404	27.3523	5926
40	411	19.4741	5761	40	404	26.8834	5926
41	412	18.2052	5745	41	405	26.6337	5925
42	413	18.6786	5778	42	405	26.5324	5925
43	414	18.3372	5768	43	406	26.5886	5917
44	417	18.3888	5754	44	410	26.1485	5905
45	417	18.6618	5754	45	411	25.5346	5905
46	418	19.0446	5748	46	412	24.9778	5904
47	419	19.1694	5762	47	413	24.5354	5900
48	420	19.2796	5737	48	414	24.4917	5908
49	424	19.2844	5742	49	417	24.6886	5890
50	426	19.3937	5734	50	417	24.2943	5890
51	428	19.5554	5727	51	418	22.9553	5878
52	431	19.5999	5727	52	419	21.9965	5886
53	433	19.461	5739	53	420	22.2061	5883
54	436	18.856	5739	54	424	22.4261	5883
55	438	19.1135	5739	55	425	23.383	5883
56	440	19.852	5735	56	426	23.351	5861
57	442	18.9537	5737	57	428	23.544	5859
58	447	18.7412	5737	58	431	23.6557	5856
59	449	18.54	5739	59	433	23.8268	5853
60	452	18.3707	5737	60	435	23.8631	5853
61	454	18.2583	5739	61	438	23.781	5850
62	456	18.1662	5737	62	440	23.752	5854
63	459	18.4652	5746	63	442	23.8268	5850
64	462	18.0473	5746	64	447	23.9822	5844
65	466	18.0662	5749	65	449	23.9009	5846
66	469	18.0124	5743	66	452	23.8932	5846
67	473	17.9867	5737	67	454	24.0577	5843
68	476	18.1189	5746	68	456	24.0112	5842
69	480	18.2663	5743	69	459	23.9	5836
70	483	18.2804	5739	70	462	24.0003	5839
71	497	18.1871	5756	71	466	24.2739	5836
72	501	18.1368	5758	72	469	24.3477	5837
73	503	18.1406	5759	73	473	24.7808	5835
74	505	18.1405	5759	74	476	26.4532	5831
75	508	18.1453	5746	75	480	27.3797	5836
76	510	18.0721	5743	76	483	25.9669	5816
77	512	17.9642	5755	77	497	24.8523	5809
78	515	17.8639	5751	78	501	24.1611	5809
79	518	17.802	5756	79	503	23.8919	5809
80	522	17.7323	5755	80	505	23.8142	5812
81	526	17.6859	5761	81	508	23.6575	5814
82	530	17.6919	5746	82	510	23.4811	5816
83	533	17.7351	5746	83	512	23.0689	5819
84	536	17.747	5745	84	515	22.6866	5816
85	539	17.6833	5748	85	518	22.4445	5815
86	543	17.6508	5759	86	522	22.2281	5816
87	546	17.5994	5756	87	526	22.0883	5818
88	550	17.5878	5754	88	530	21.9239	5816
89	557	17.6526	5755	89	533	21.821	5813
90	564	17.6016	5748	90	536	21.5814	5816
91	571	17.5426	5752	91	539	21.5528	5818
92	575	17.4804	5754	92	543	21.6762	5818
93	585	16.1109	5751	93	546	21.7292	5818
94	701	13.6585	5793	94	550	21.7806	5820
				95	557	21.8135	5817
				96	564	21.6424	5830
				97	571	21.4917	5812
				98	575	21.105	5817
				99	586	18.6896	5826
				100	711	14.0665	6055

Table D:1.1 record#, day#,  $Q_{\alpha}$ , and  $V_p$  for line M7-M6 in H9 heater mid-plane.

Table D:1.2 record#, day#,  $Q_{\alpha}$ , and  $V_p$  for line M8-M9 in H9 heater mid-plane.

D:1.3

D:1.4

M8-M6 #	DAY #	Q-VALUE	VELOCITY	M7-M9 #	DAY #	Q-VALUE	VELOCITY
1	-43	13.0743	5030	1	-43	11.5706	5748
2	-7	13.0785	5030	2	0	11.5721	5731
3	6	12.853	5060	3	6	12.5487	5826
4	15	12.5853	5063	4	8	13.0837	5862
5	18	12.8404	5085	5	11	13.0739	5873
6	21	13.718	5095	6	12	13.0473	5889
7	50	14.169	5098	7	13	13.1027	5882
8	57	13.7777	5094	8	14	12.9454	5889
9	64	13.6316	5095	9	15	12.5177	5897
10	78	13.8629	6012	10	21	12.3072	5874
11	91	14.2955	6008	11	50	12.4728	5896
12	110	15.55	6014	12	57	12.5117	5899
13	118	18.1984	6016	13	64	12.7595	5888
14	133	19.7645	6029	14	78	13.1631	5909
15	159	18.9549	6029	15	91	13.2464	5919
16	176	18.2471	6030	16	110	13.387	5918
17	195	16.9597	6025	17	112	16.1214	5917
18	210	15.2528	6032	18	133	17.7509	5917
19	222	15.835	6029	19	159	17.0542	5924
20	238	17.1513	6035	20	176	16.4894	5933
21	252	18.2717	6024	21	195	15.4826	5931
22	267	18.2173	6026	22	210	14.1966	5931
23	306	17.6789	6026	23	222	14.415	5918
24	330	17.4725	6025	24	235	15.8244	5918
25	333	17.6274	6025	25	252	16.5826	5918
26	334	18.0652	6025	26	267	17.0264	5918
27	335	18.9677	6030	27	271	17.3689	5918
28	337	19.3969	6022	28	306	17.5397	5918
29	341	19.1715	6019	29	330	18.2226	5918
30	342	19.2472	6023	30	333	19.1584	5930
31	344	19.6601	6023	31	334	19.5519	5930
32	351	19.7242	6023	32	335	19.7446	5930
33	362	18.7091	6023	33	337	19.2337	5916
34	376	17.9754	6023	34	344	18.8705	5916
35	383	18.2582	6023	35	349	19.502	5915
36	398	19.332	6023	36	351	19.7961	5919
37	399	20.2423	6021	37	362	18.4511	5919
38	399	20.4756	6021	38	376	17.9207	5923
39	400	20.4398	6017	39	383	19.6472	5919
40	400	20.4569	6017	40	398	22.4818	5918
41	403	20.375	5998	41	399	23.0658	5909
42	403	20.1624	5998	42	399	22.896	5909
43	404	19.9789	5988	43	400	22.8042	5857
44	404	19.9595	5988	44	400	18.7836	5847
45	405	19.8632	5985	45	403	16.7147	5837
46	405	19.6763	5985	46	403	15.7244	5827
47	406	19.4844	5982	47	404	15.3812	5817
48	410	19.2245	5960	48	405	14.9522	5807
49	411	19.9501	5962	49	406	13.8352	5797
50	412	18.6795	5957	50	410	12.8268	5787
51	413	18.3816	5955	51	411	12.2795	5777
52	414	18.0005	5951	52	412	11.9258	5767
53	417	17.9965	5946	53	413	11.6727	5757
54	417	18.2138	5946	54	414	11.5406	5747
55	418	18.427	5945	55	417	11.5518	5737
56	419	18.085	5941	56	417	11.6059	5727
57	420	18.6271	5939	57	418	11.8851	5717
58	424	18.7673	5924	58	419	11.8548	5697
59	426	18.7562	5927	59	420	11.9136	5687
60	428	18.7161	5925	60	424	11.9155	5677
61	431	18.749	5924	61	426	11.8328	5667
62	433	18.7863	5921	62	428	11.885	5657
63	435	18.7663	5923	63	431	11.9812	5669
64	438	18.7426	5920	64	433	12.0295	5694
65	440	18.7581	5919	65	435	12.0756	5665
66	442	18.8028	5914	66	438	12.1477	5642
67	447	18.76	5911	67	440	12.2994	5644
68	449	18.6601	5914	68	442	12.4869	5658
69	452	18.7111	5911	69	447	12.6414	5645
70	454	18.8566	5914	70	449	12.7833	5644
71	456	18.8886	5912	71	452	12.7482	5648
72	459	18.7883	5911	72	454	12.8007	5648
73	462	18.6737	5911	73	456	12.8801	5646
74	466	18.6822	5911	74	459	12.9647	5643
75	469	18.7938	5908	75	462	13.0221	5644
76	473	19.207	5907	76	466	13.0281	5681
77	476	19.178	5904	77	469	13.008	5675
78	480	20.7551	5897	78	473	13.0363	5684
79	483	20.1529	5896	79	476	13.0936	5683
80	497	19.8087	5898	80	480	13.1406	5688
81	501	19.6024	5898	81	483	13.1206	5687
82	503	19.3721	5896	82	497	13.0036	5686
83	505	19.2106	5899	83	501	12.8958	5684
84	508	19.1788	5900	84	503	12.8475	5691
85	510	19.1045	5899	85	505	12.789	5693
86	512	18.935	5898	86	508	12.7894	5695
87	515	18.6863	5899	87	510	12.8151	5688
88	518	18.4958	5899	88	512	12.7672	5719
89	522	18.3816	5899	89	515	12.7027	5691
90	526	18.1492	5903	90	518	12.6773	5699
91	530	18.0327	5901	91	522	12.6776	5702
92	533	18.2182	5902	92	526	12.7279	5705
93	536	18.2039	5900	93	530	12.7468	5694
94	539	18.095	5901	94	533	12.7225	5699
95	543	18.0293	5900	95	536	12.7166	5703
96	546	18.0521	5903	96	539	12.7288	5705
97	550	18.098	5904	97	543	12.7489	5700
98	557	18.1019	5908	98	546	12.7681	5703
99	564	17.8696	5905	99	550	12.7592	5741
100	571	17.5239	5907	100	557	12.8637	5737
101	575	17.232	6008	101	564	13.0502	5717
102	585	15.813	5897	102	571	13.2454	5697
103	704	12.7685	5915	103	575	13.1028	5677
				104	585	11.7721	5657
				106	706	9.27960	5634

Table D:1.3 record# , day# ,  $Q_{\alpha}$  , and  $V_p$  for line M8-M6 in H9 heater mid-plane

Table D:1.4 record# , day# ,  $Q_{\alpha}$  , and  $V_p$  for line M7-M9 in H9 heater mid-plane

REF. PROFILE #	DAY #	Q-VALUE	VELOCITY
1	-1	13.8103	5899
2	0	13.6996	5904
3	5	13.7487	5901
4	6	14.2449	5904
5	19	14.9722	5907
6	20	14.8304	5925
7	20	14.5709	5922
8	20	14.4236	5902
9	20	14.6662	5921
10	110	14.9062	5920
11	110	15.3871	5920
12	110	15.8174	5920
13	110	15.7541	5920
14	113	15.8345	5935
15	116	16.3211	5931
16	118	17.1964	5930
17	118	17.6242	5925
18	119	18.1332	5926
19	119	19.4953	5930
20	132	19.576	5933
21	223	18.6976	5931
22	223	20.2825	5942
23	336	21.8044	5928
24	336	22.3349	5928
25	337	21.4985	5928
26	343	20.3429	5930
27	344	19.7895	5930
28	344	19.5316	5932
29	348	19.8896	5931
30	349	20.1955	5931
31	349	19.9104	5922
32	350	20.0203	5926
33	350	19.9703	5922
34	354	19.6531	5927
35	354	19.4805	5923
36	355	19.8436	5925
37	355	20.5802	5930
38	356	21.4677	5931
39	356	21.8541	5923
40	357	22.0288	5931
41	357	21.7568	5922
42	358	20.5656	5926
43	362	19.0721	5923
44	375	18.94	5925
45	375	20.183	5925
46	398	22.404	5918
47	398	23.6175	5918
48	419	25.2602	5922
49	420	25.4031	5921
50	424	24.5421	5920
51	424	23.5603	5920
52	424	23.0662	5927
53	425	22.6485	5917
54	425	22.8159	5920
55	425	22.7973	5918
56	426	22.3379	5927
57	566	22.2393	5926
58	566	20.633	5903
59	699	17.4113	5921
60	701	15.5963	5913
61	706	14.8511	5912
62	708	14.5821	5909
63	710	14.5494	5912
64	712	14.585	5912
65	712	14.6856	5907
66	712	14.7267	5907
67	712	14.5705	5909
68	750	14.5132	5912

Table D:1.5 record#, day#,  $Q_{\alpha}$ , and  $V_n$  for reference line M9-M6 1 m below ground surface

MONITORING Q FOR P-WAVES IN HEATER MIDPLANE  
STANDARD FILE : M79PA.42  
STANDARD Q : 50  
STANDARD VEL : 5900  
STANDARD LINE LENGTH : 4.202 M.  
SMOOTHING OF Q PLOT: 2x3 POINT RUNNING

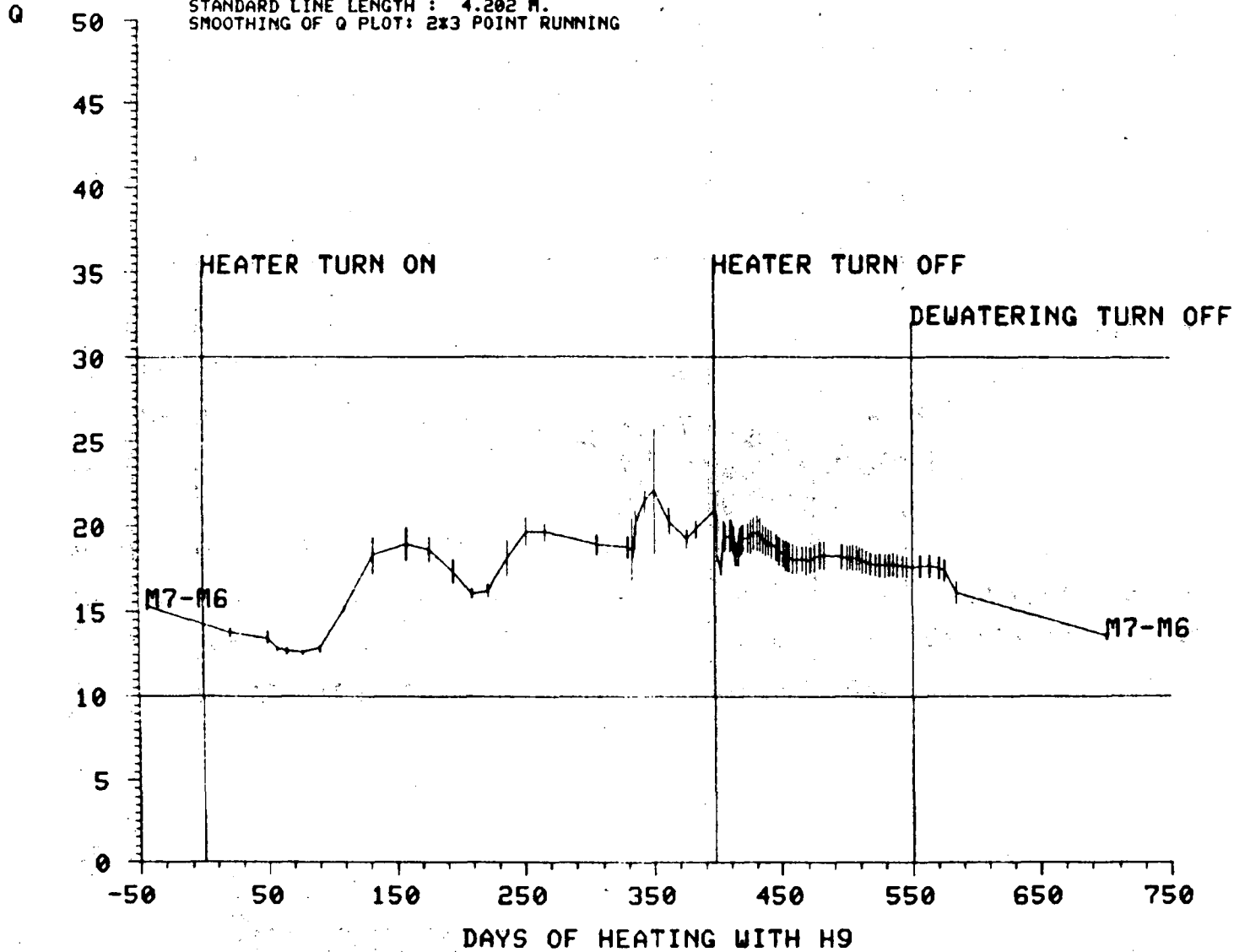
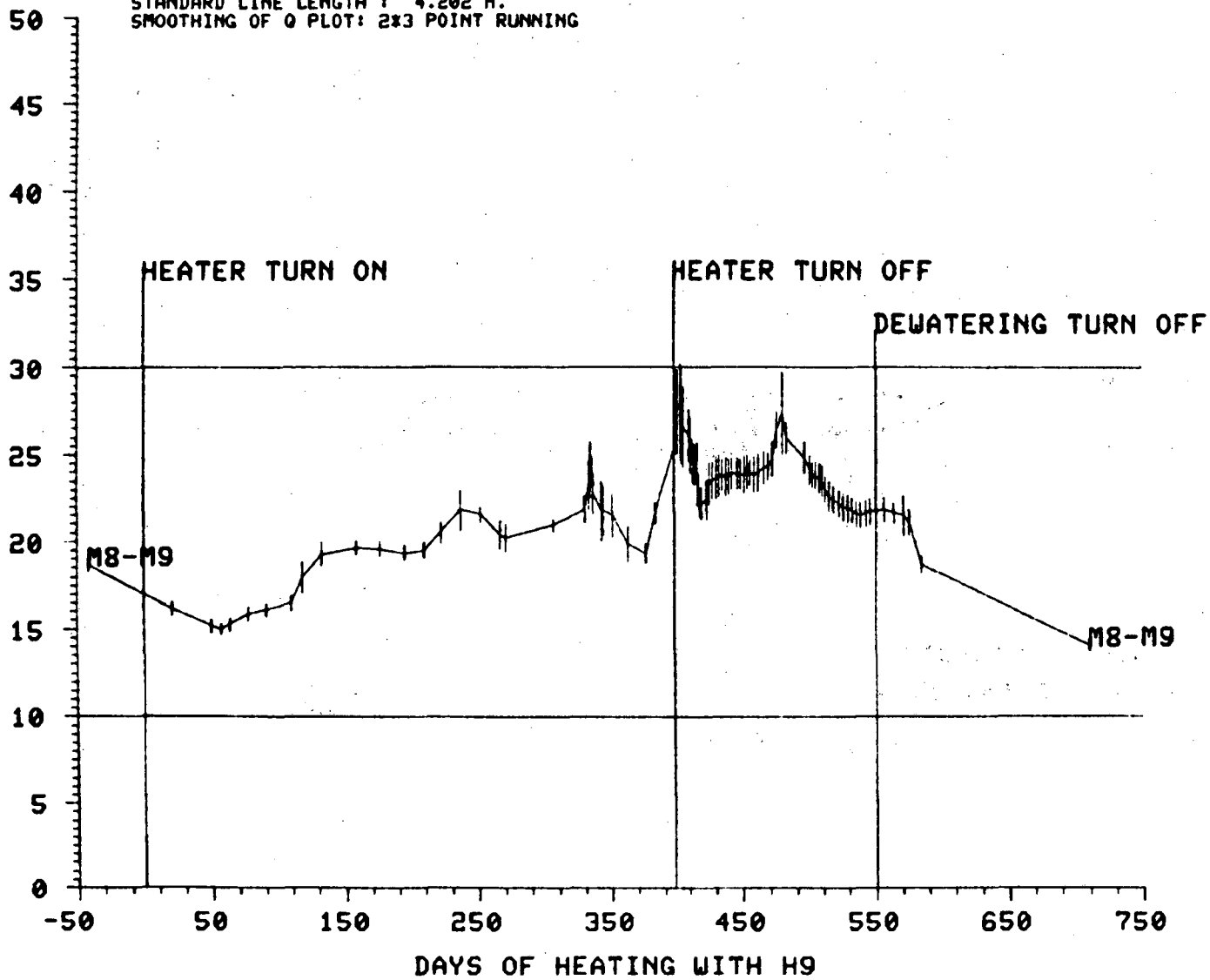


Fig. D.1.1  $Q_{\alpha}$  for monitor signals in heater midplane in line M7-M6

MONITORING Q FOR P-WAVES IN HEATER MIDPLANE  
STANDARD FILE : M79PA.42  
STANDARD Q : 50  
STANDARD VEL : 5900  
STANDARD LINE LENGTH : 4.202 M.  
SMOOTHING OF Q PLOT: 2x3 POINT RUNNING

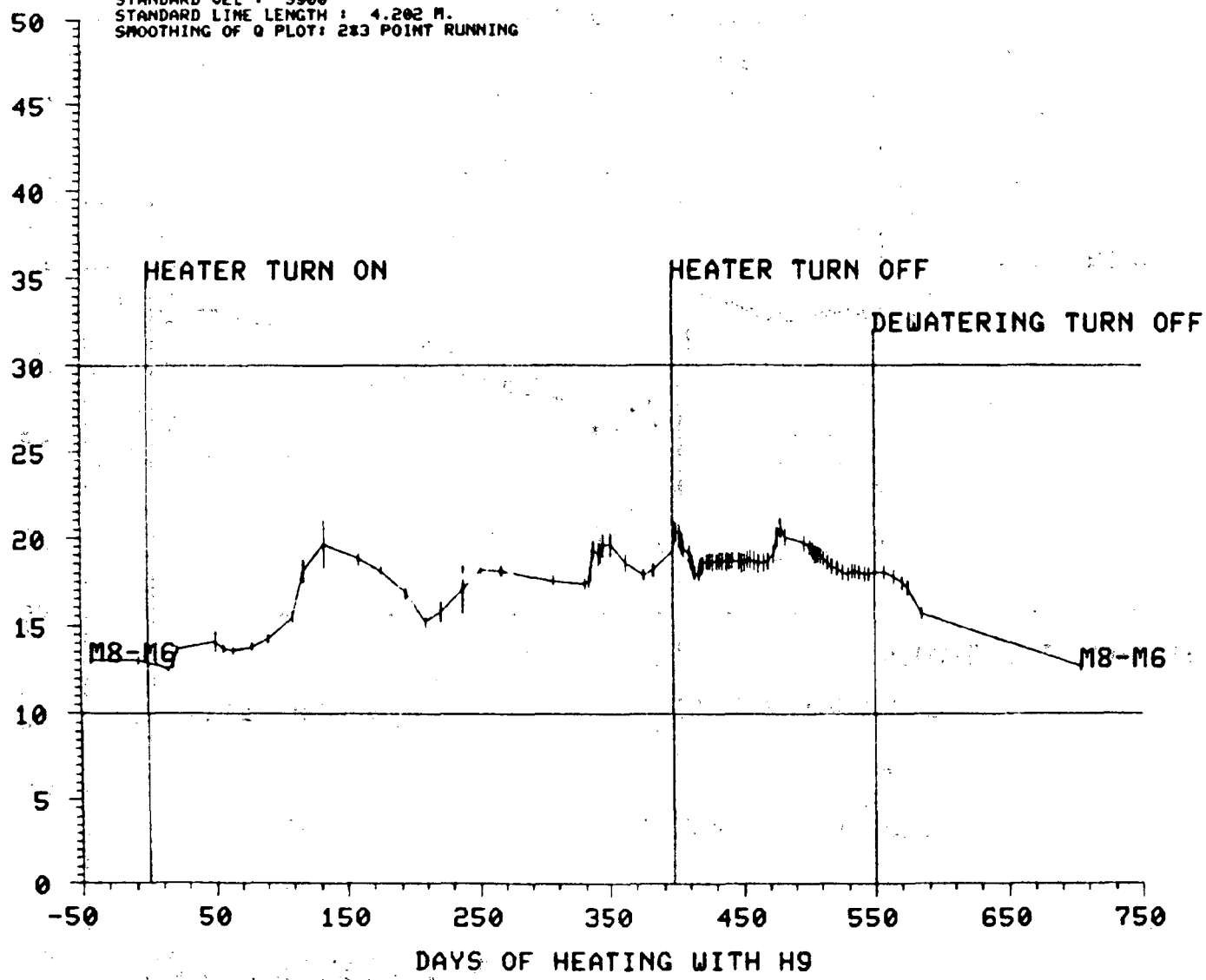
Fig. D.1.2  $Q_a$  for monitor signals in heater midplane in line M8-M9.





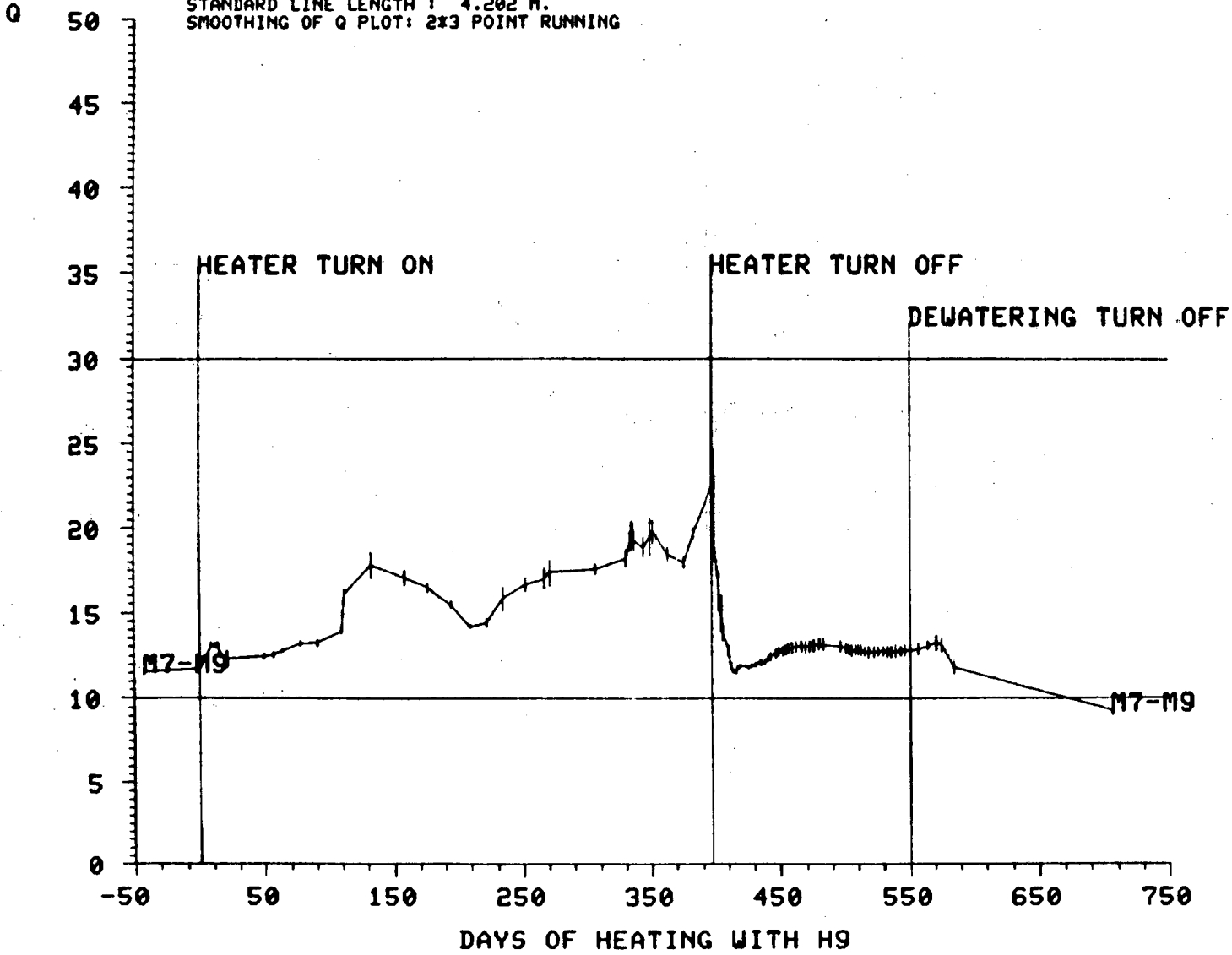
MONITORING Q-VALUES IN HEATER MIDPLANE  
STANDARD FILE : M79PA.42  
STANDARD Q : 50  
STANDARD UEL : 5900  
STANDARD LINE LENGTH : 4.202 M.  
SMOOTHING OF Q PLOT: 283 POINT RUNNING

Fig. D.1.3  $Q_{\alpha}$  for monitor signals in heater midplane in line M8-M6.



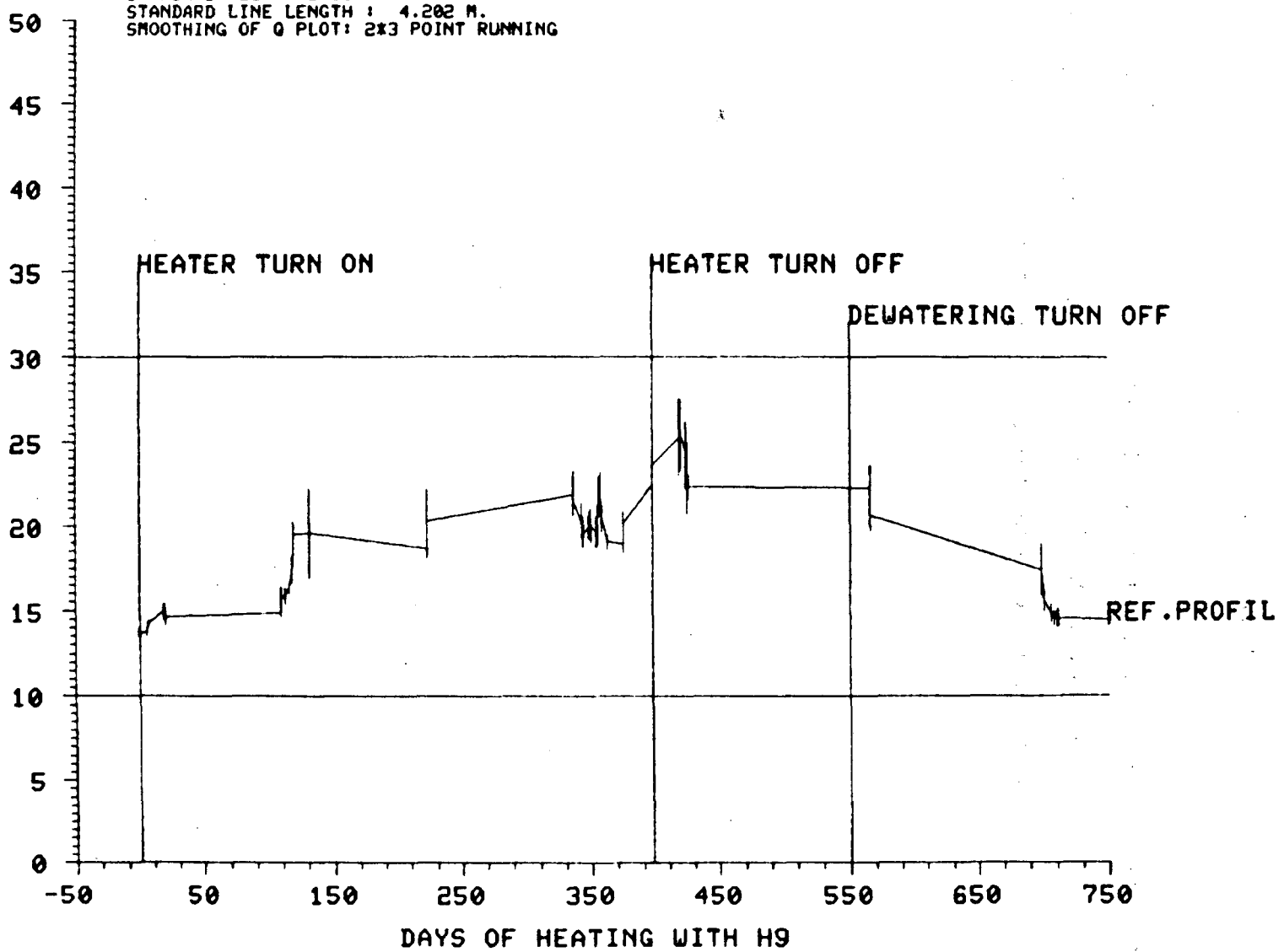
MONITORING Q FOR P-WAVES IN HEATER MIDPLANE  
STANDARD FILE : M79PA.42  
STANDARD Q : 50  
STANDARD VEL : 5900  
STANDARD LINE LENGTH : 4.202 M.  
SMOOTHING OF Q PLOT : 2x3 POINT RUNNING

Fig. D:1.4  $Q_a$  for monitor signals in heater midplane in line M7-M9.



MONITORING Q FOR P-WAVES IN HEATER MIDPLANE  
STANDARD FILE : M79PA.42  
STANDARD Q : 50  
STANDARD VEL : 5900  
STANDARD LINE LENGTH : 4.202 M.  
SMOOTHING OF Q PLOT: 2\*3 POINT RUNNING

Fig. D.1.5  $Q_a$  for reference signals between boreholes M6-M9.



## **Appendix D:2 - Amplitude spectra from seismic waves in the monitor and reference lines**

The Fourier amplitude spectra from the ultra sonic cross holes signals are presented in this appendix. The amplitude spectra are obtained by Fourier transformation of the cross hole signals in Appendix D:2.

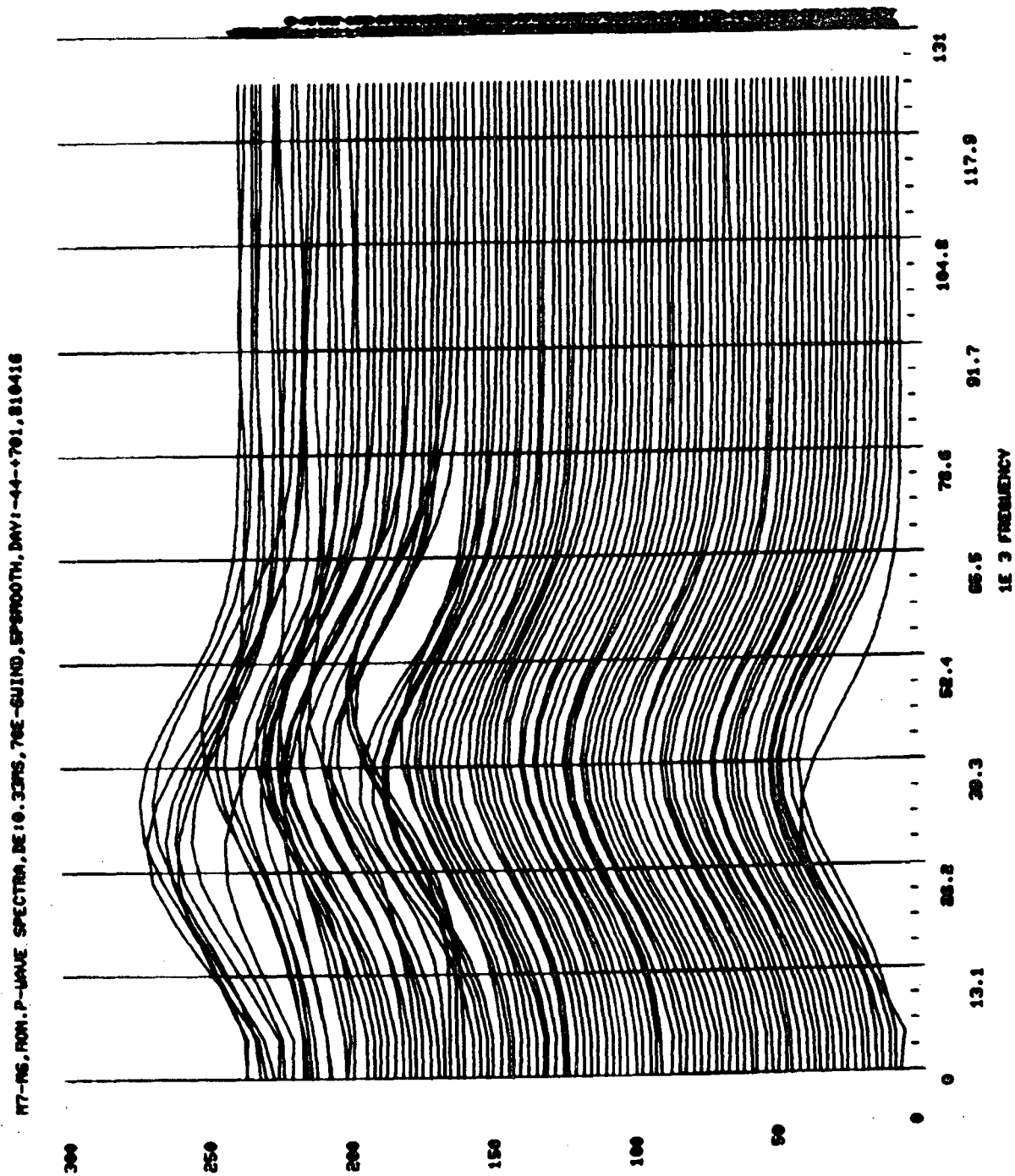


Fig. D:2.1 P wave amplitude spectra from monitor line M7-M6

THIS FIGURE HAS BEEN DELETED

Fig. D:2.2

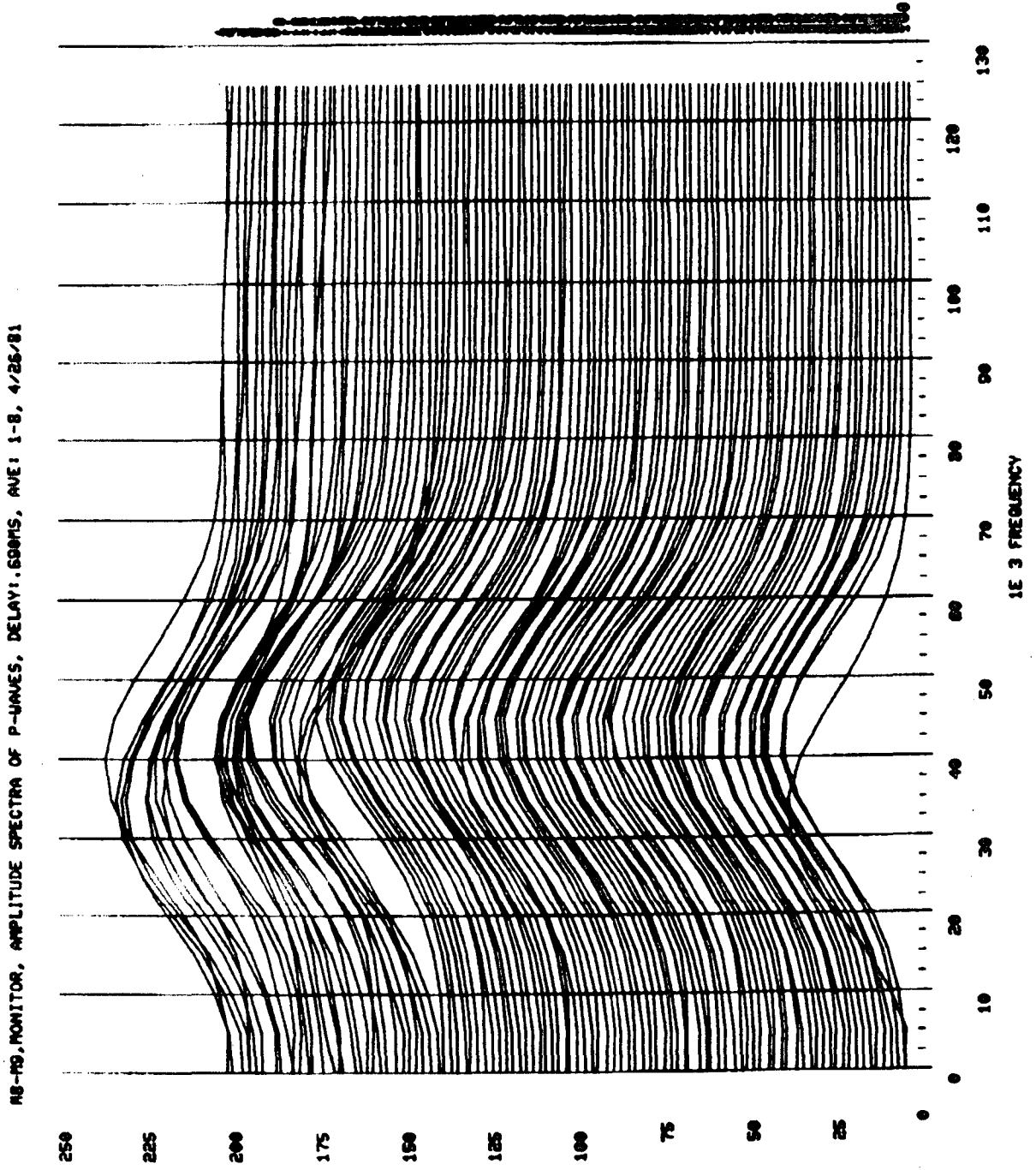


Fig. D:2.3 P wave amplitude spectra from monitor line M8-M9

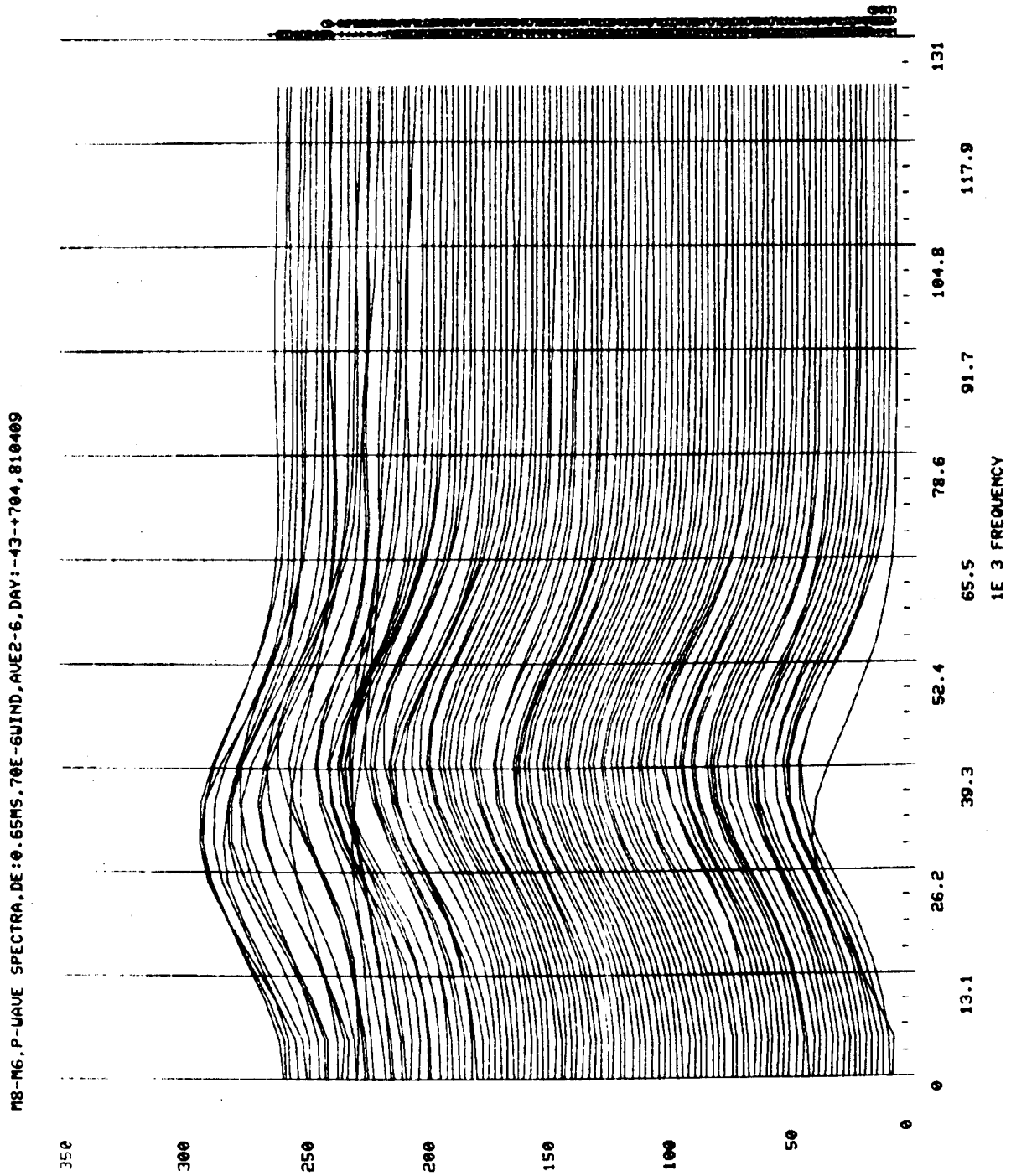


Fig. D:2.4 P wave amplitude spectra from monitor line M8-M6



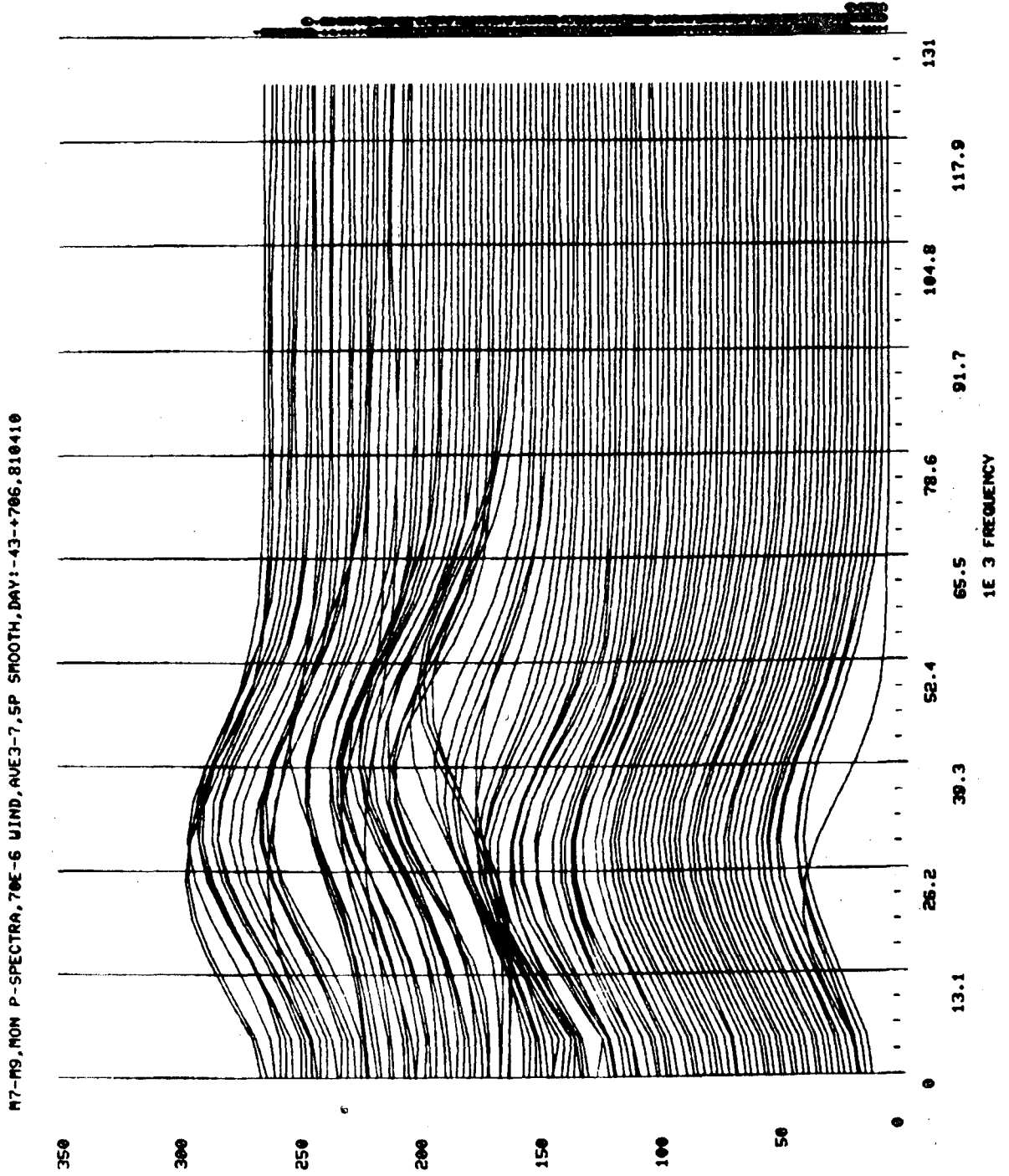


Fig. D:2.5 P wave amplitude spectra from monitor line M7-M9

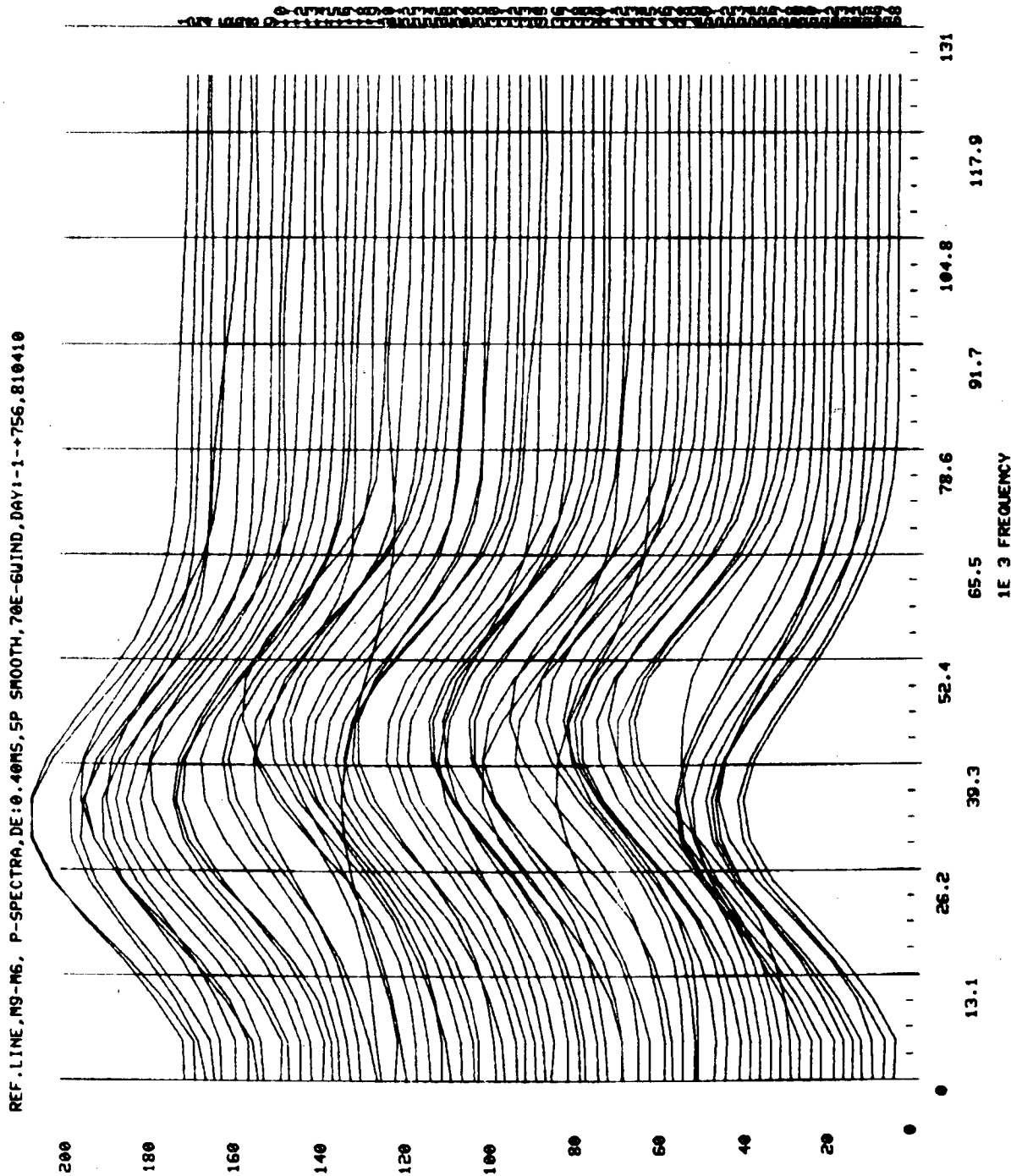


Fig. D:2.6 P wave amplitude spectra from reference line M9-M6

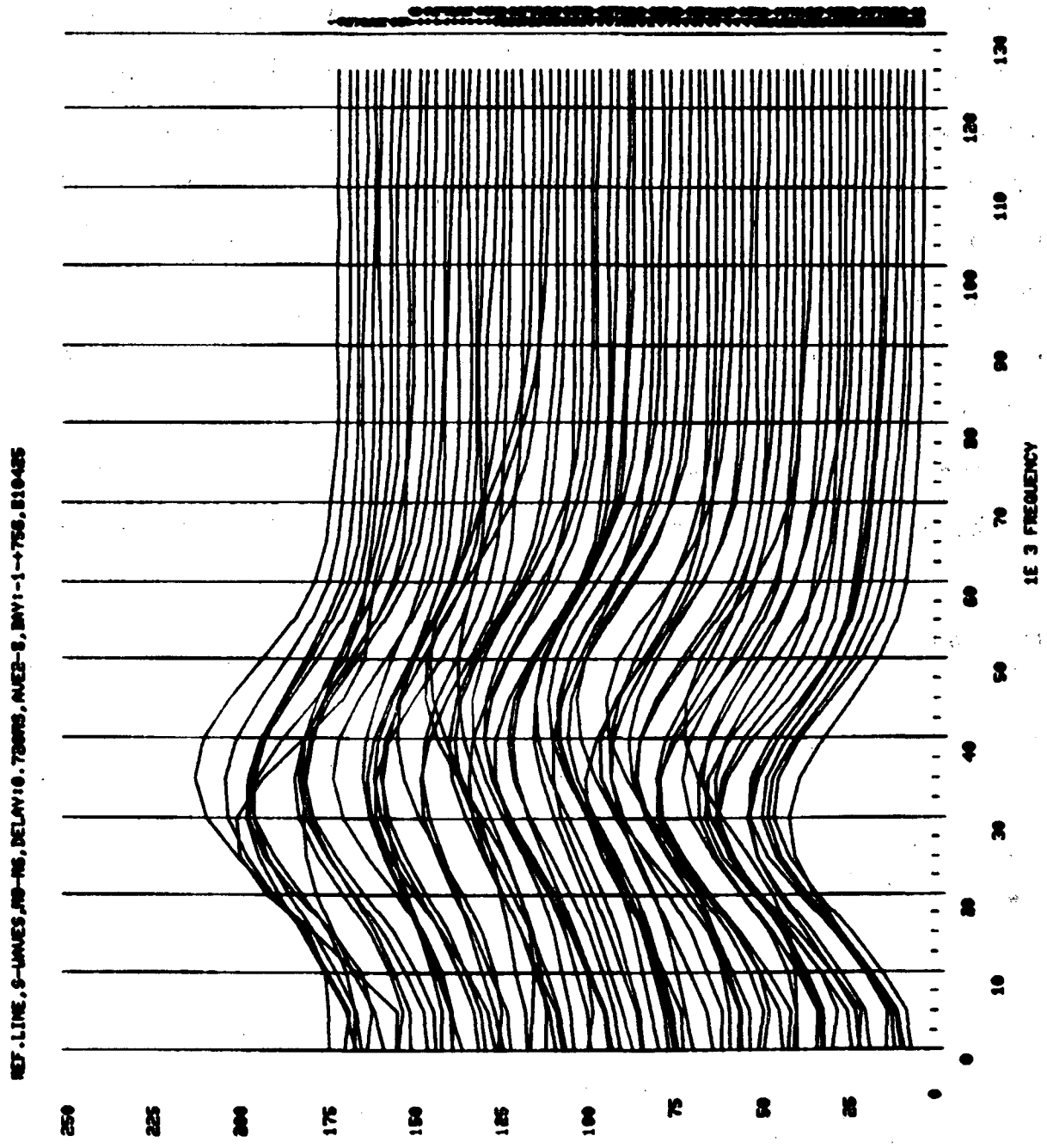


Fig. D:2.7 S wave amplitude spectra from reference line M9-m6

### Appendix D:3 - P wave amplitude spectra for cross hole surveys in six sections.

The P wave amplitude spectra for the surveys between the four monitor holes in the H9 area are presented in this appendix. The order of presentation is the same as before starting with cross section M7-M6. In this cross section four surveys were performed. In cross section M7-M8 which follows, and in cross section M8-M9 as well as in cross section M6-M9 five surveys were performed during the course of the H9 heater experiment. The two main cross sections M8-M6 and M7-M9 follow both with 8 surveys, out of 10 and 11 respectively, presented.

The data is presented so the distance between two consecutive numbers represent a vertical distance of 0.25 m. Using this convention the heater shown in each figure is placed on the right level relative to the p wave signals.

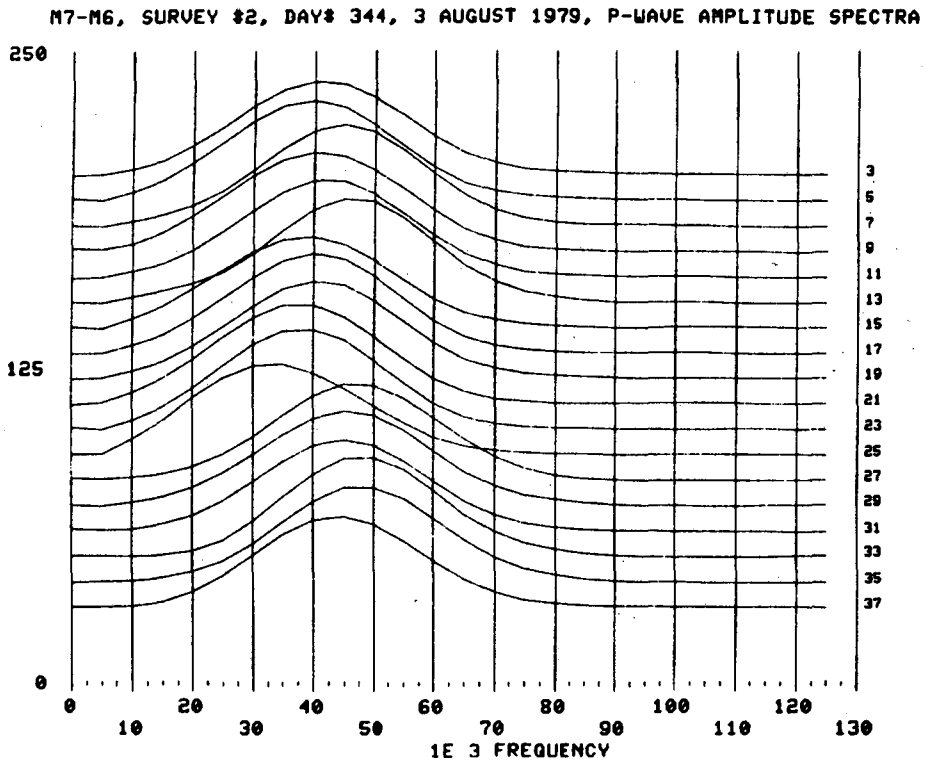
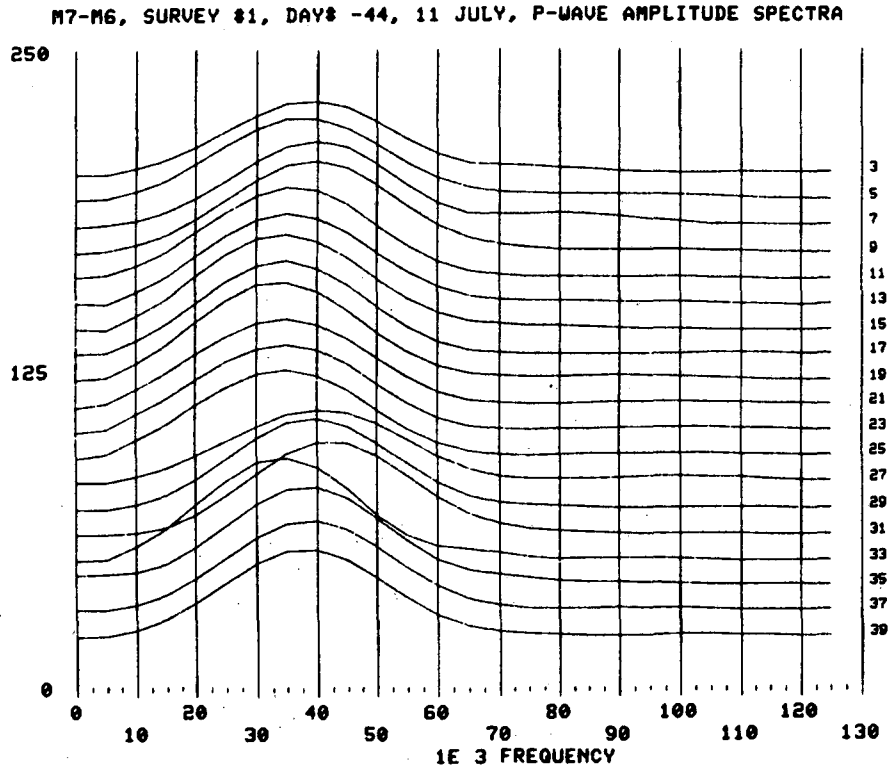


Fig. D:3.1a P wave amplitude spectra for survey # 1 in cross section M7-

M6

Fig. D:3.1b P wave amplitude spectra for survey # 2 in cross section M7-M6

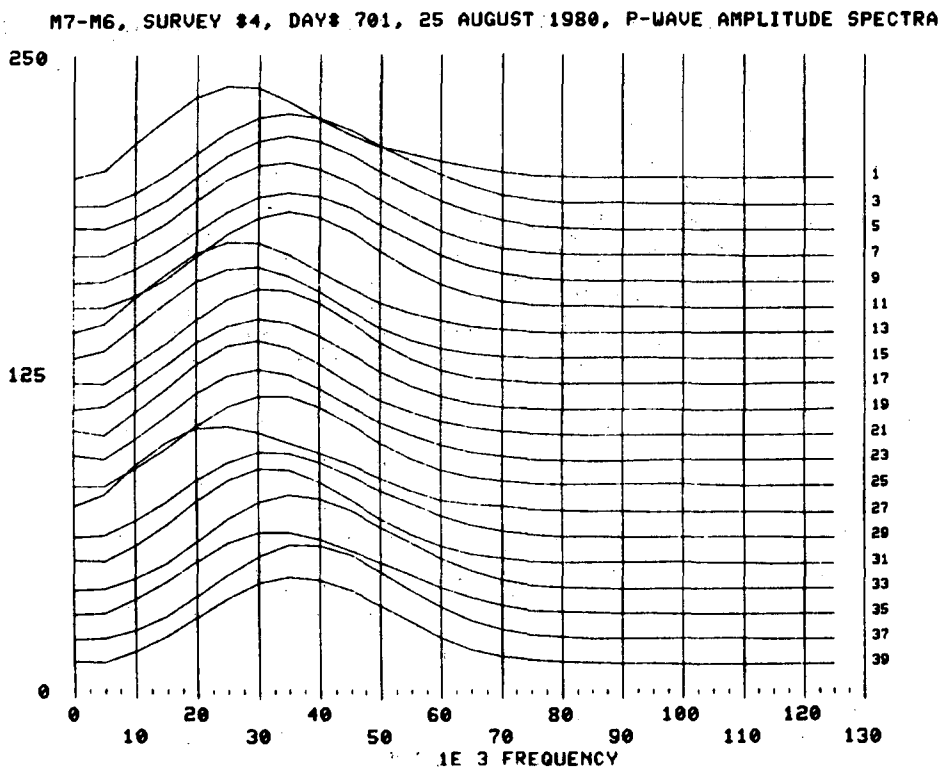
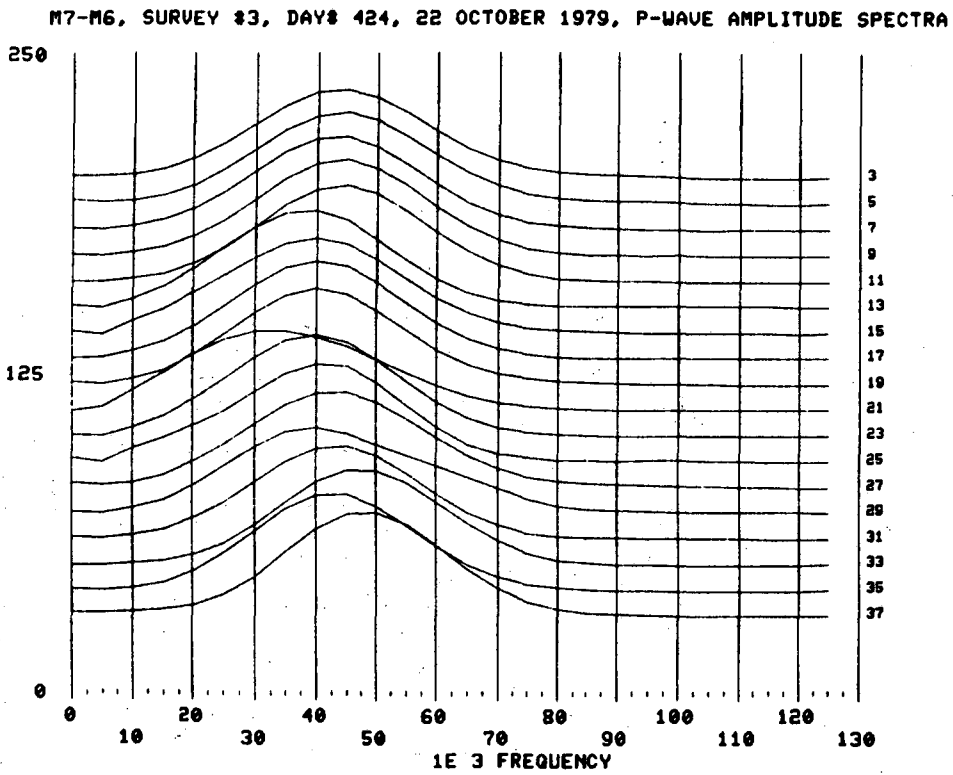


Fig. D:3.1c P wave amplitude spectra for survey # 3 in cross section M7-

M6

Fig. D:3.1d P wave amplitude spectra for survey # 4 in cross section M7-M6

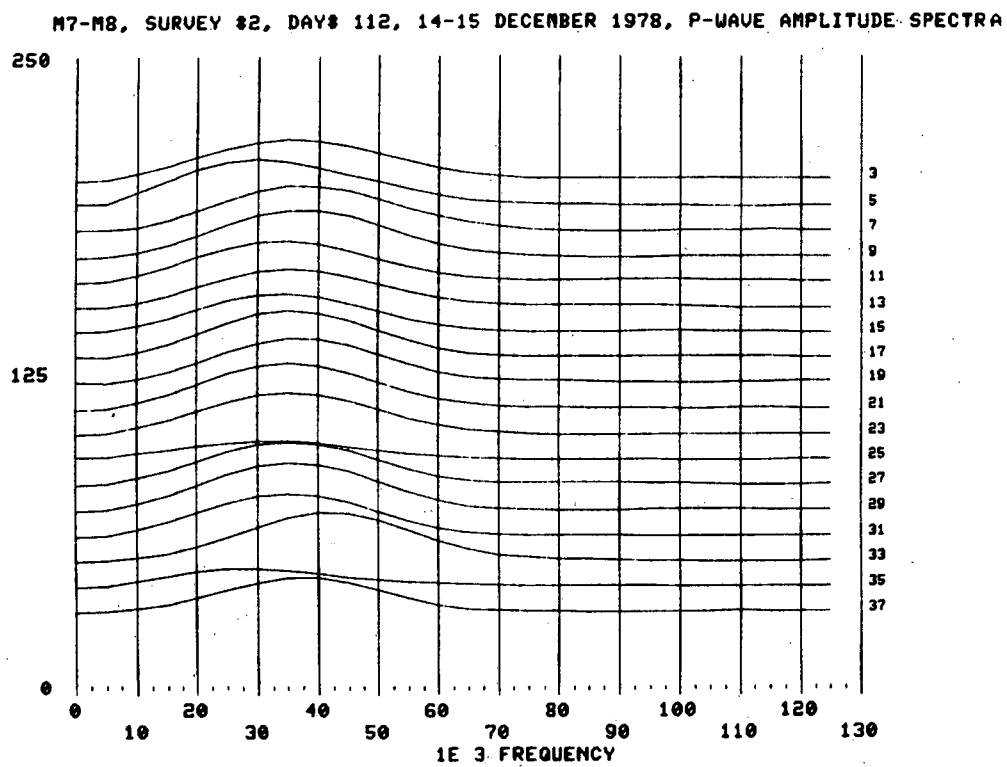
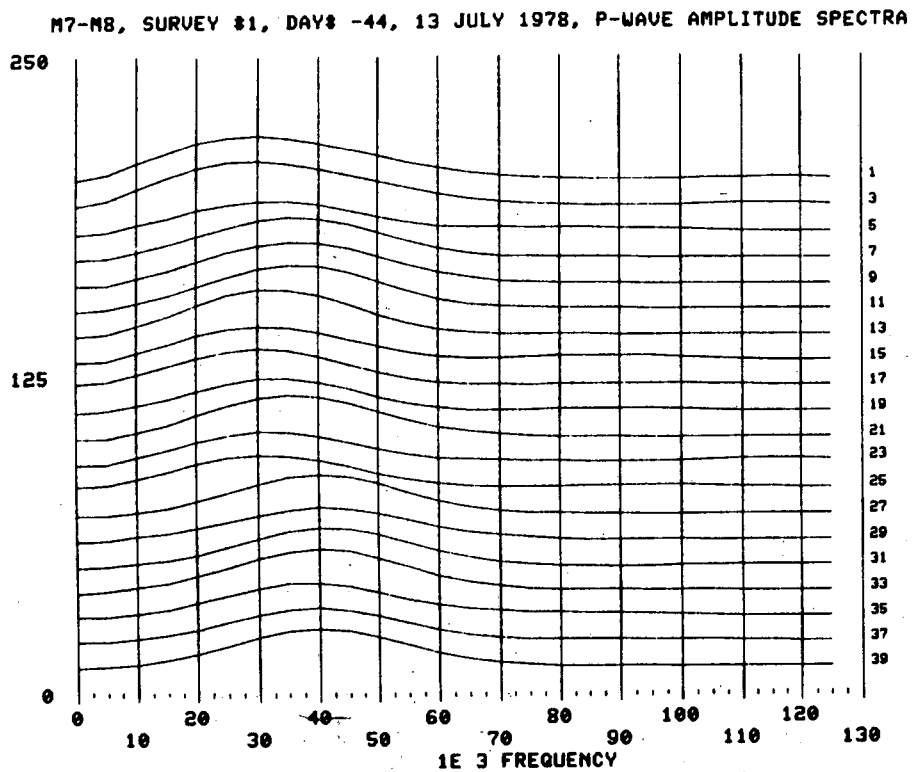


Fig. D:3.2a P wave amplitude spectra for survey # 1 in cross section M7-

M8

Fig. D:3.2b P wave amplitude spectra for survey # 2 in cross section M7-M8

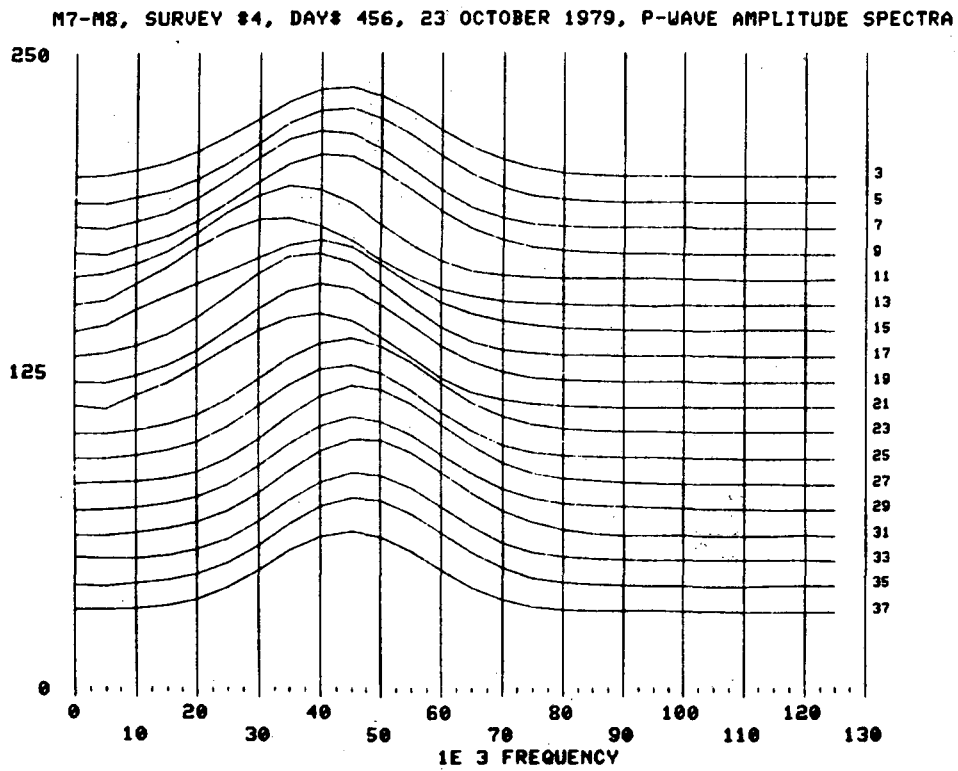
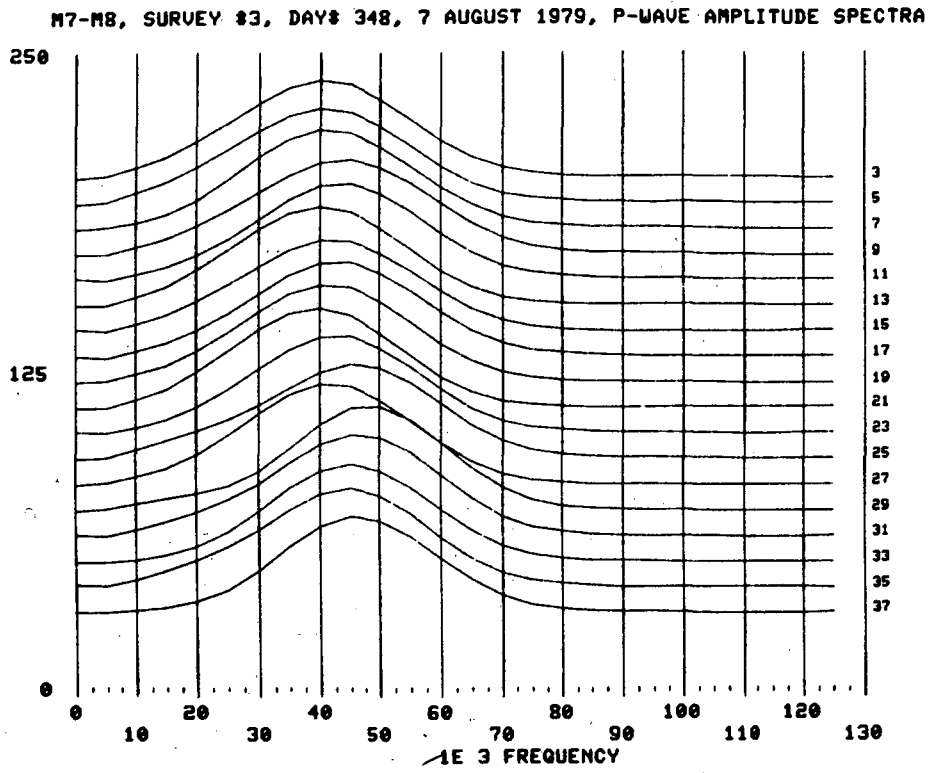


Fig. D:3.2c P wave amplitude spectra for survey # 3 in cross section M7-

M8

Fig. D:3.2d P wave amplitude spectra for survey # 4 in cross section M7-  
M8



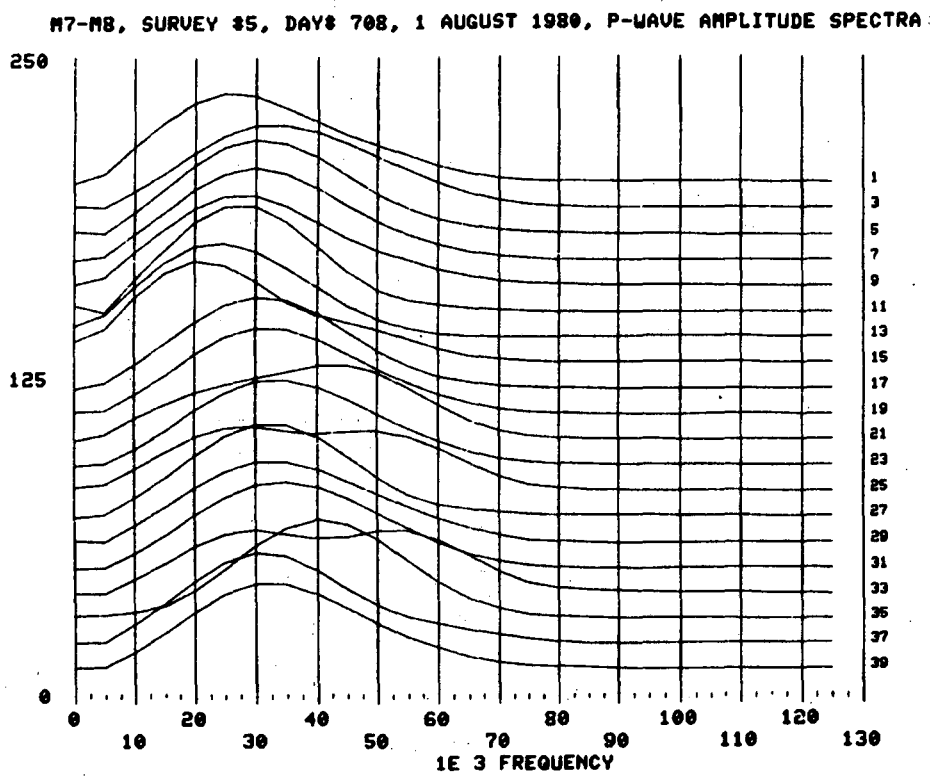


Fig. D:3.2e P wave amplitude spectra for survey # 5 in cross section M7-M8

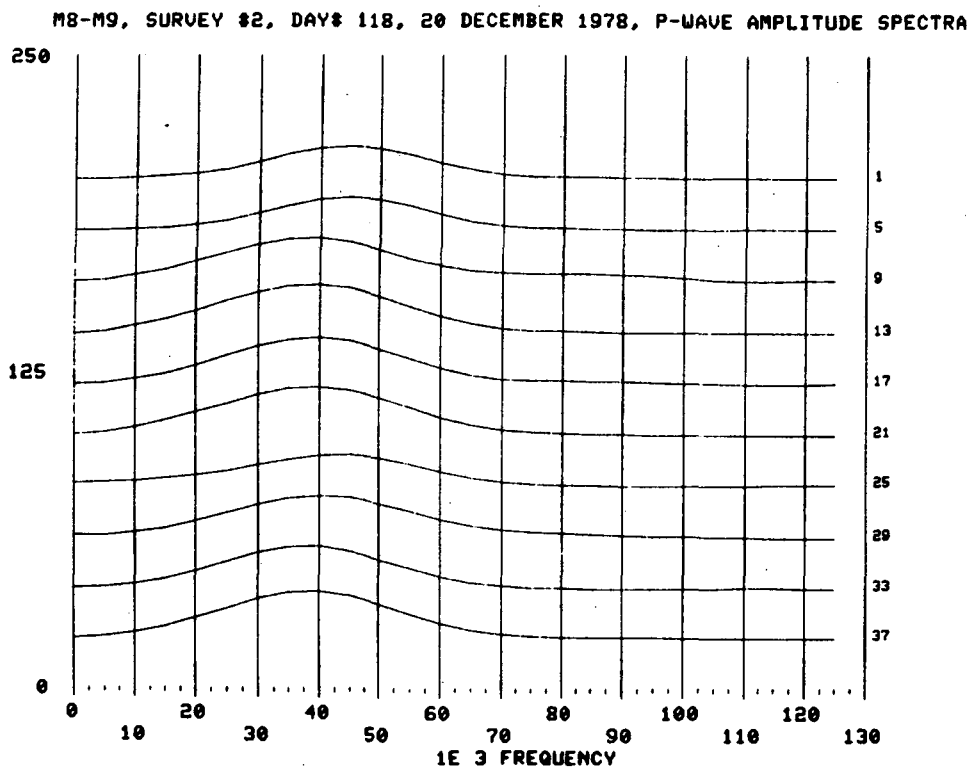
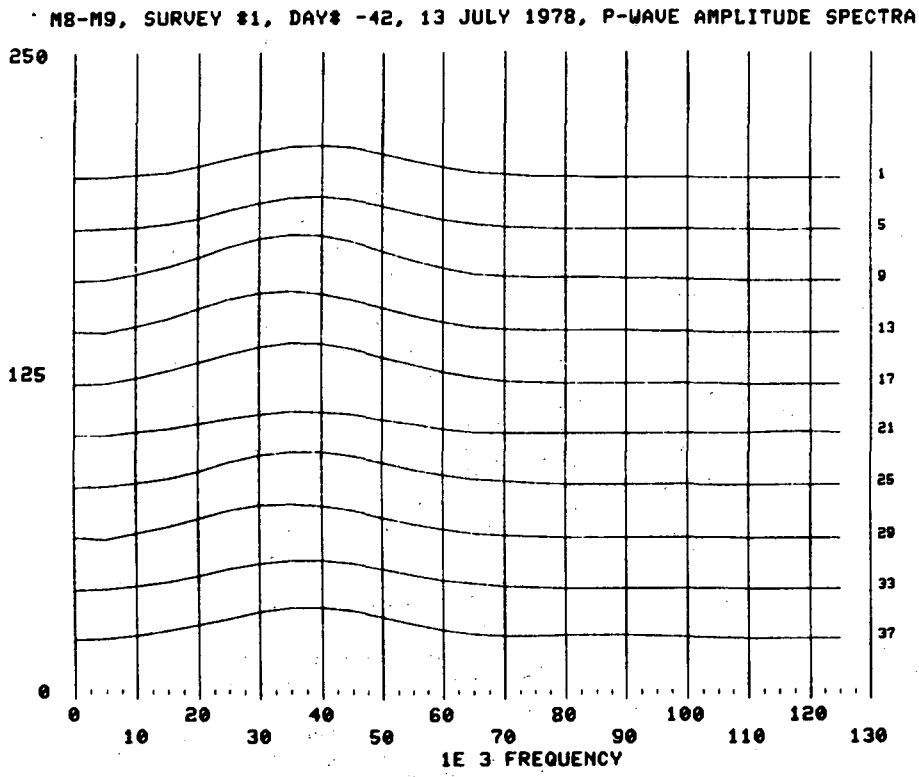


Fig. D:3.3a P wave amplitude spectra for survey # 1 in cross section M8-

M9

Fig. D:3.3b P wave amplitude spectra for survey # 2 in cross section M8-M9

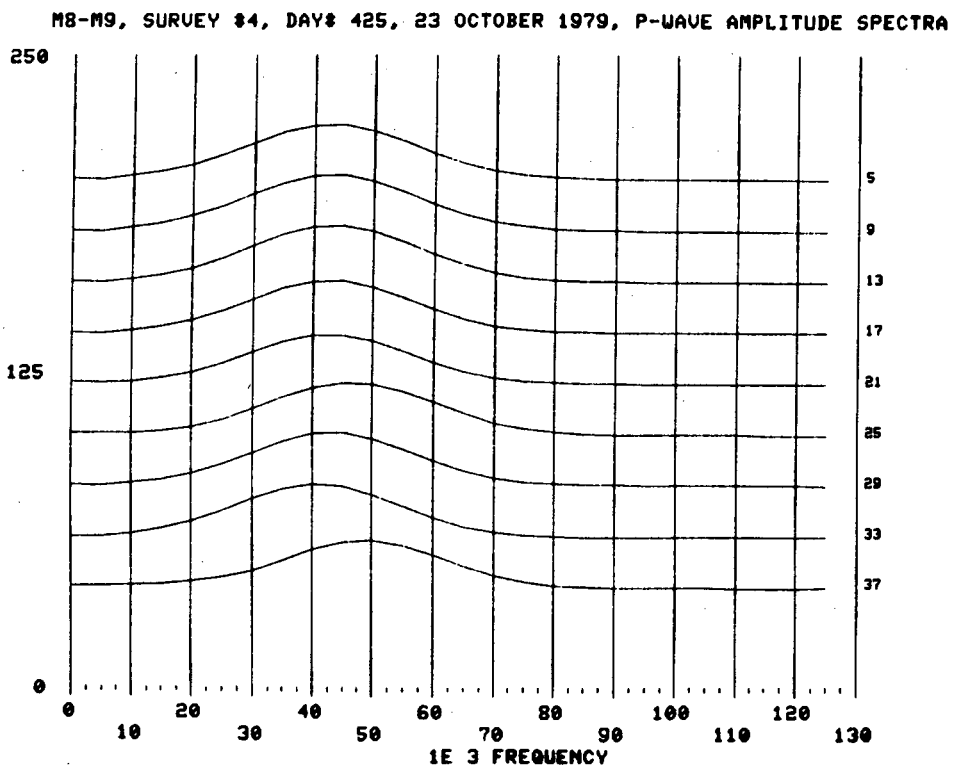
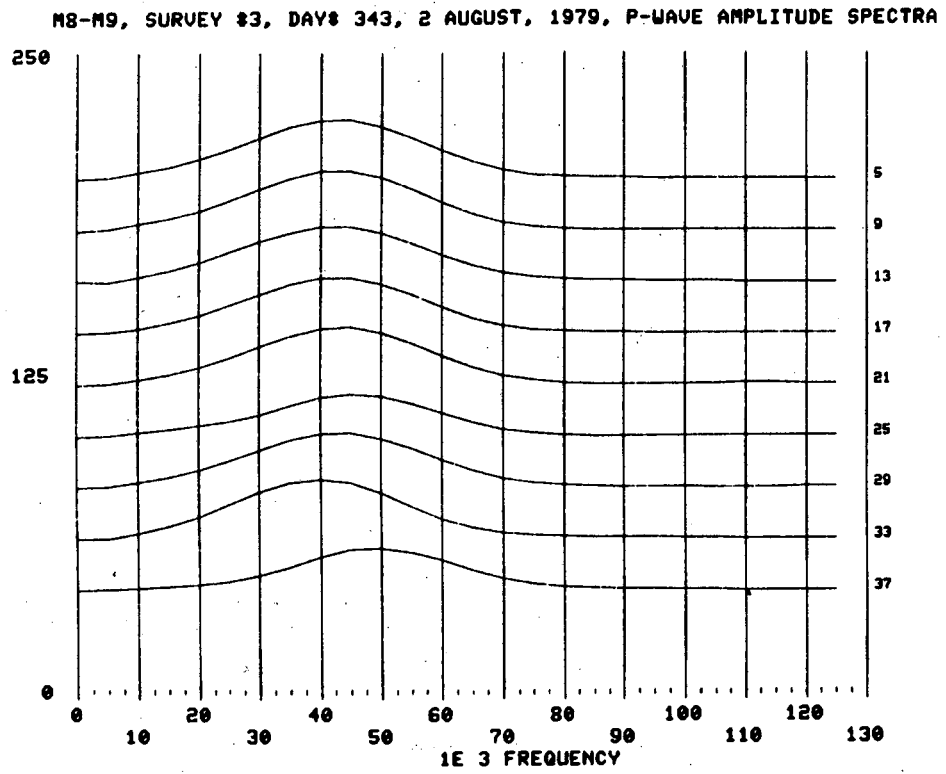


Fig. D:3.3c P wave amplitude spectra for survey # 3 in cross section M8-M9

Fig. D:3.3d P wave amplitude spectra for survey # 4 in cross section M8-M9

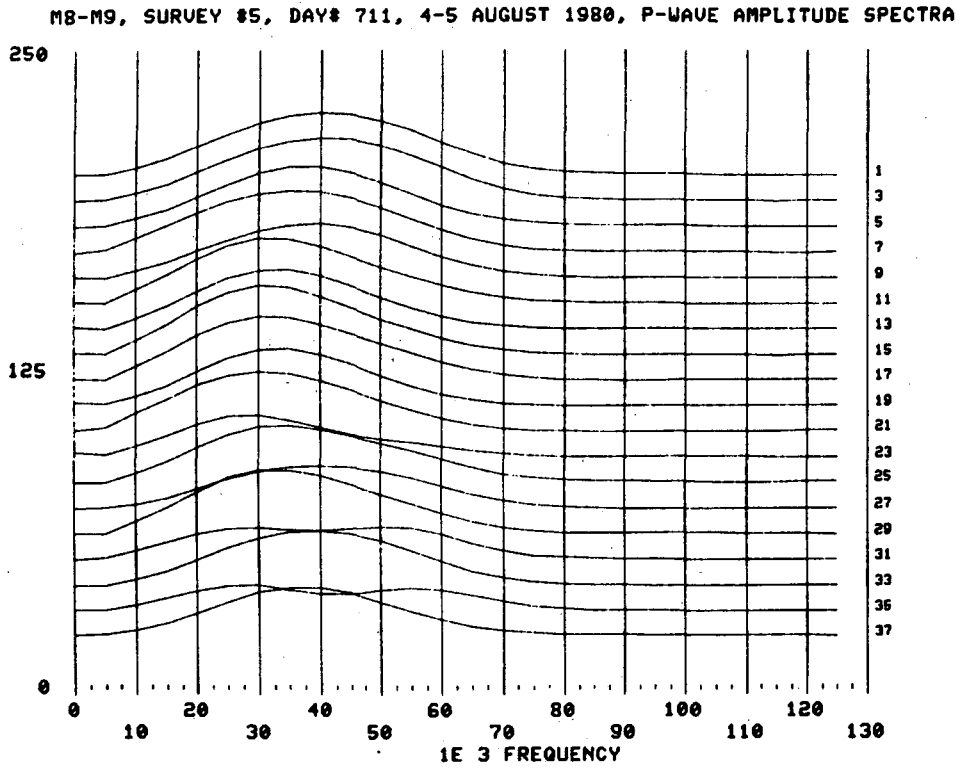


Fig. D:3.3e P wave amplitude spectra for survey # 5 in cross section M8-M9

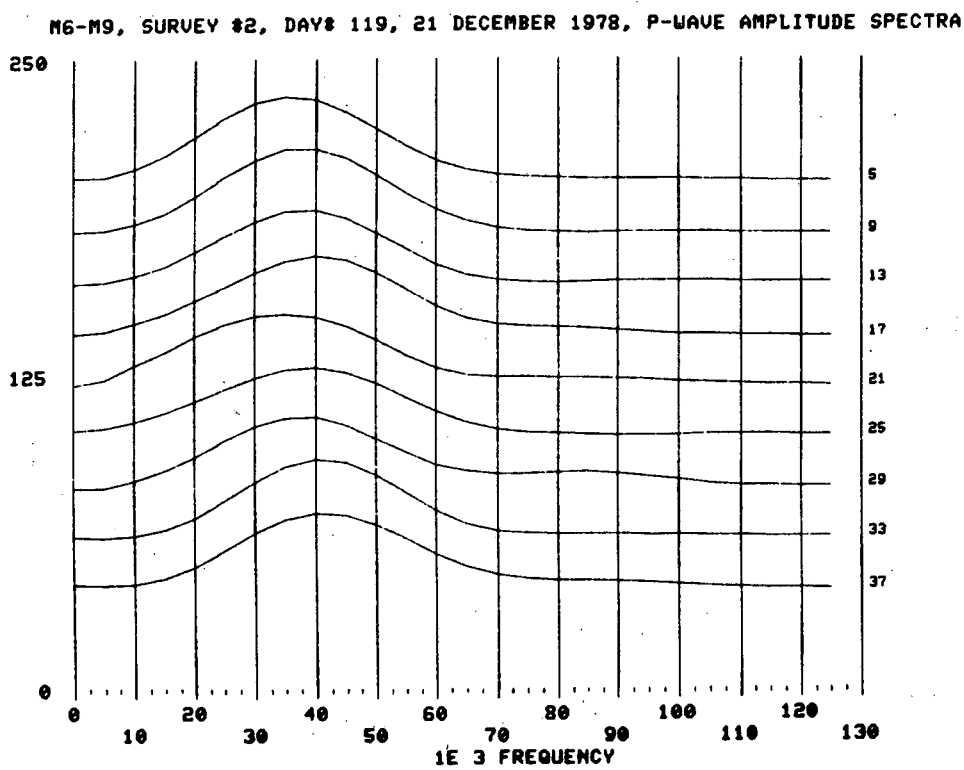
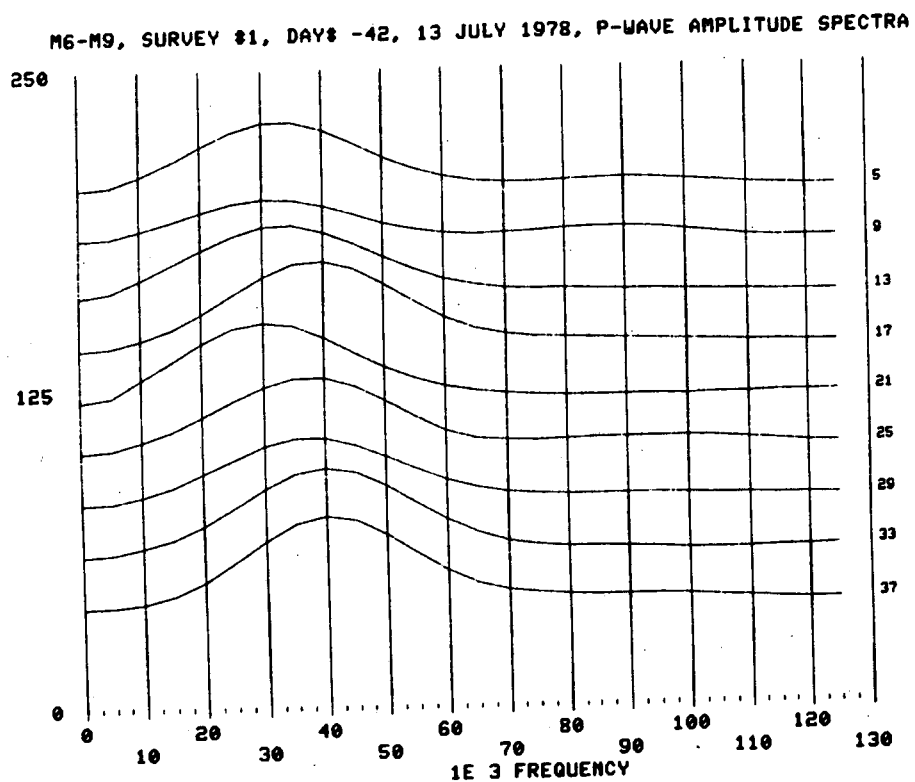


Fig. D:3.4a P wave amplitude spectra for survey # 1 in cross section M6-

M9

Fig. D:3.4b P wave amplitude spectra for survey # 2 in cross section M6-M9

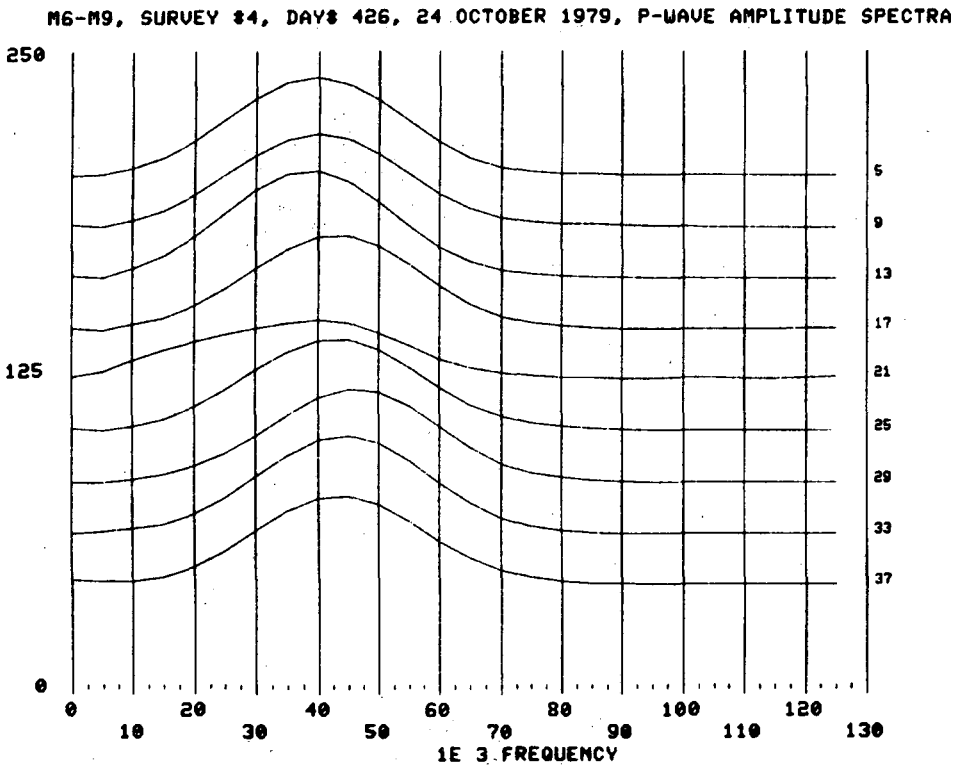
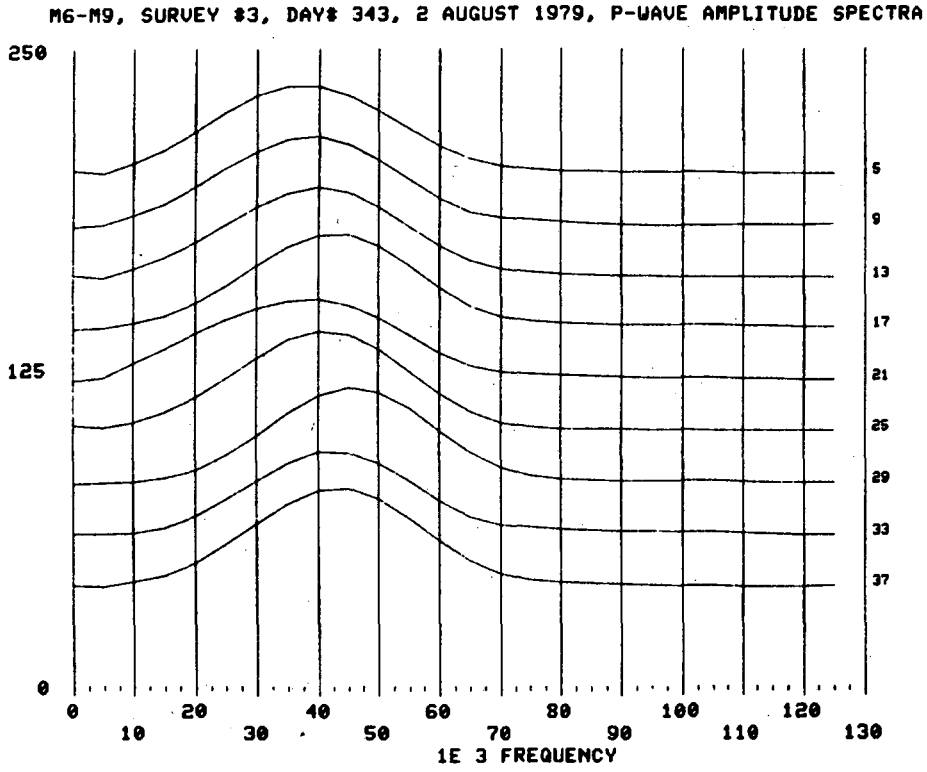


Fig. D:3.4c P wave amplitude spectra for survey # 3 in cross section M6-

M9

Fig. D:3.4d P wave amplitude spectra for survey # 4 in cross section M6-  
M9

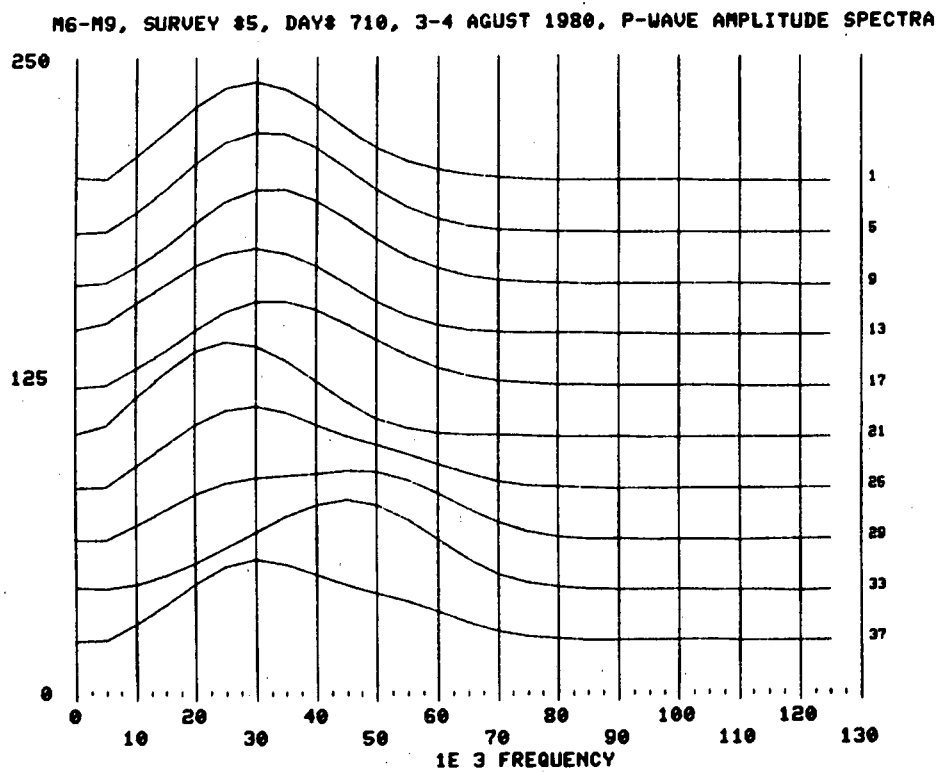


Fig. D:3.4e P wave amplitude spectra for survey # 5 in cross section M6-M9

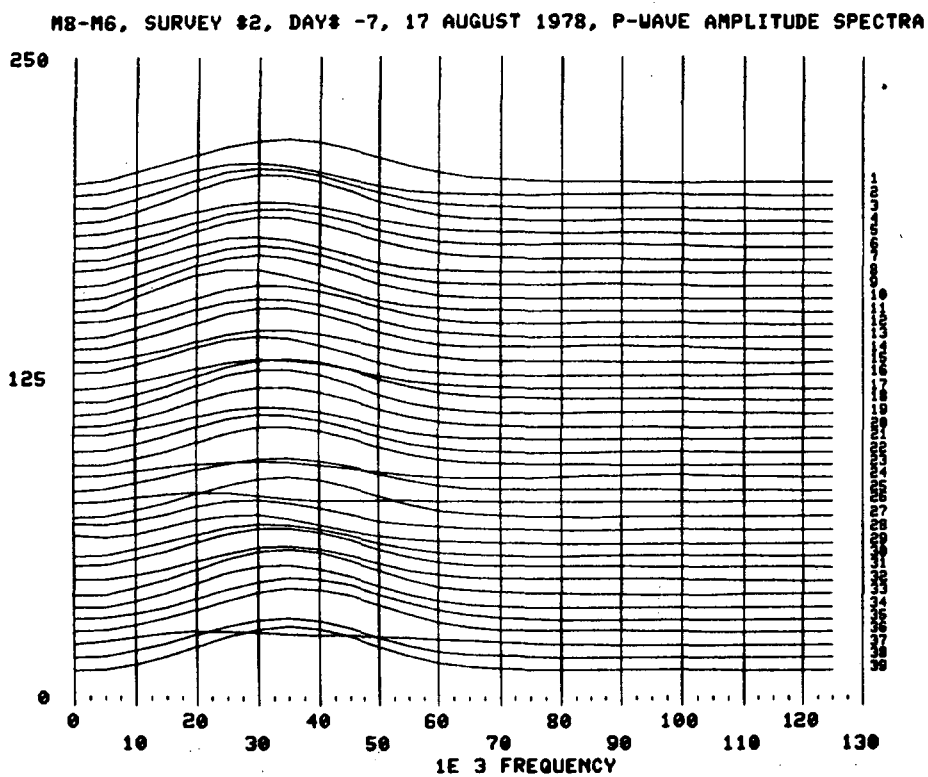
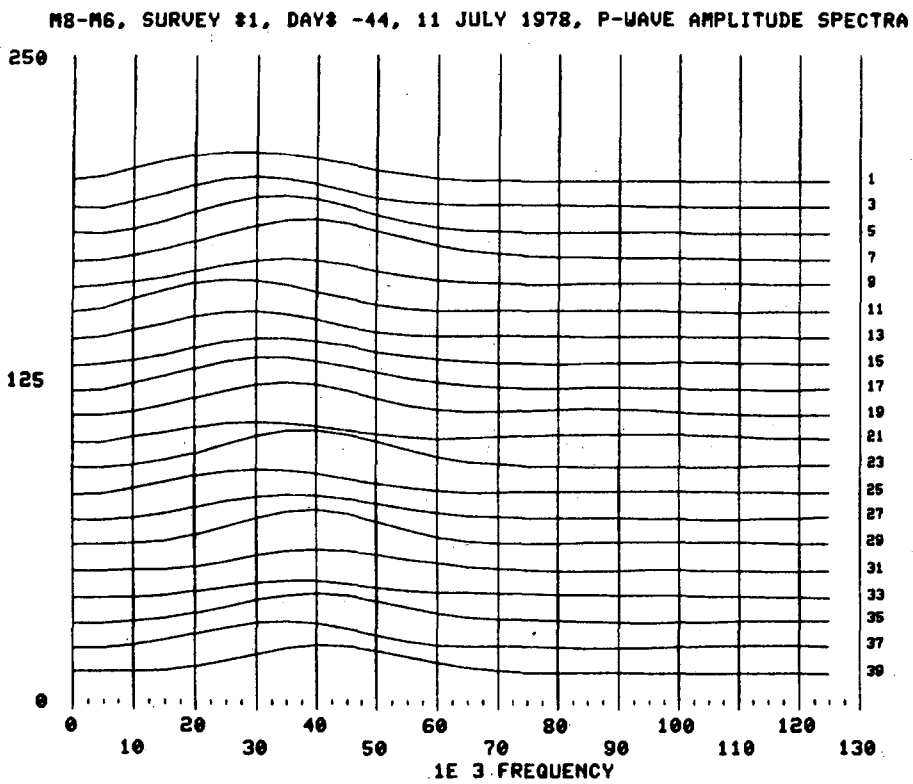


Fig. D:3.5a P wave amplitude spectra for survey # 1 in cross section M8-

M6

Fig. D:3.5b P wave amplitude spectra for survey # 2 in cross section M8-M6



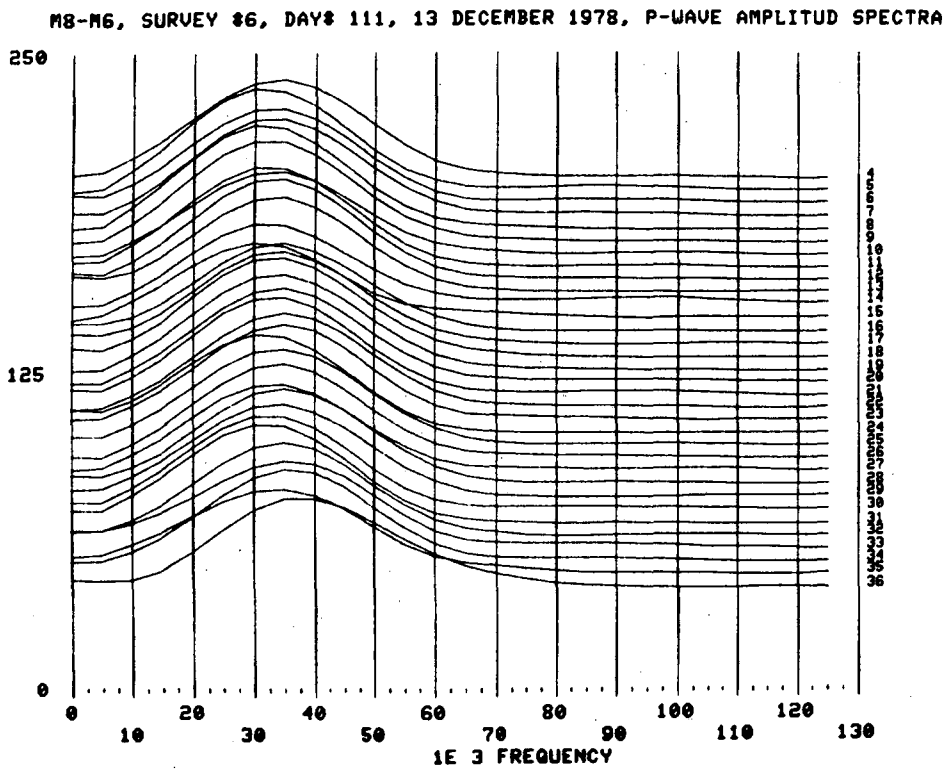
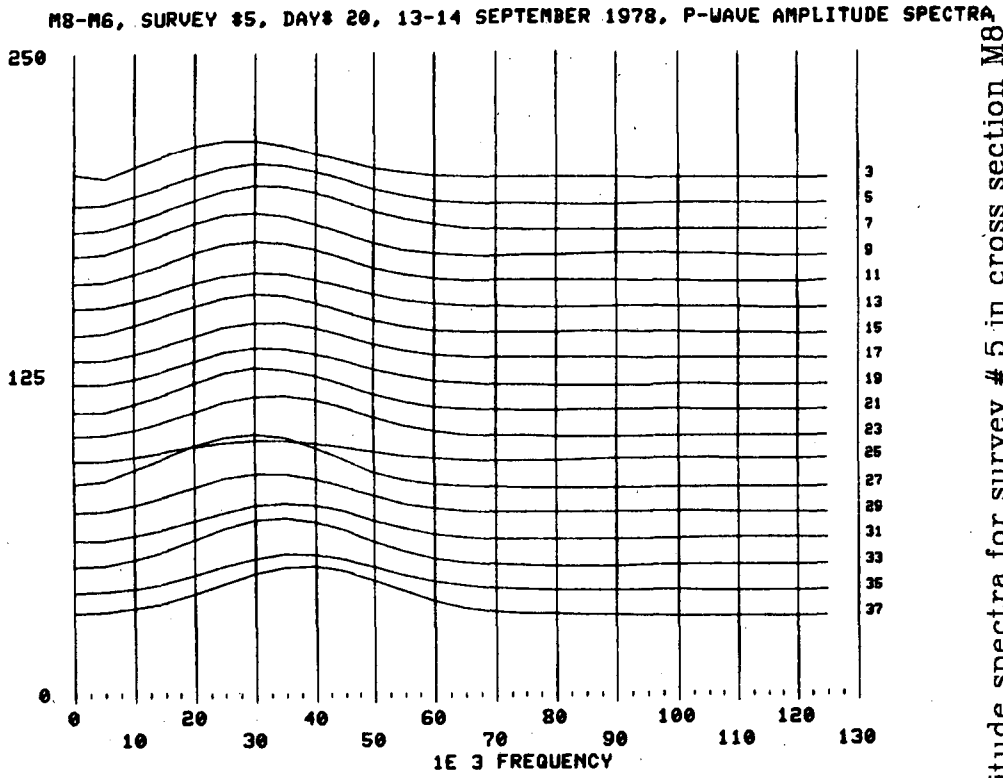


Fig. D:3.5c P wave amplitude spectra for survey # 5 in cross section M8-

M6

Fig. D:3.5d P wave amplitude spectra for survey # 6 in cross section M8-M6

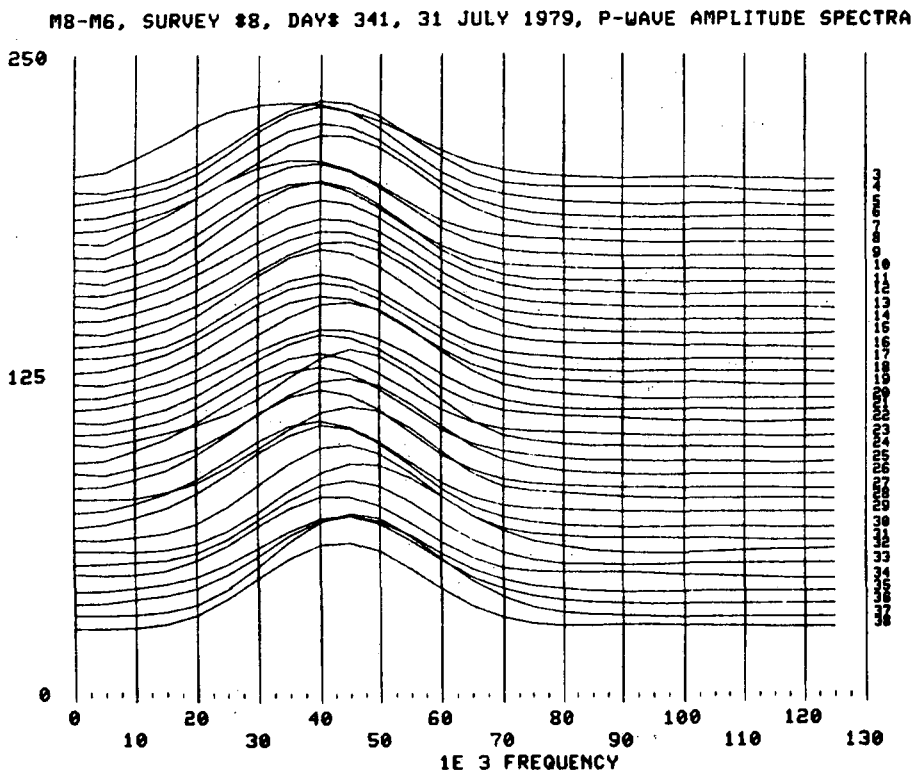
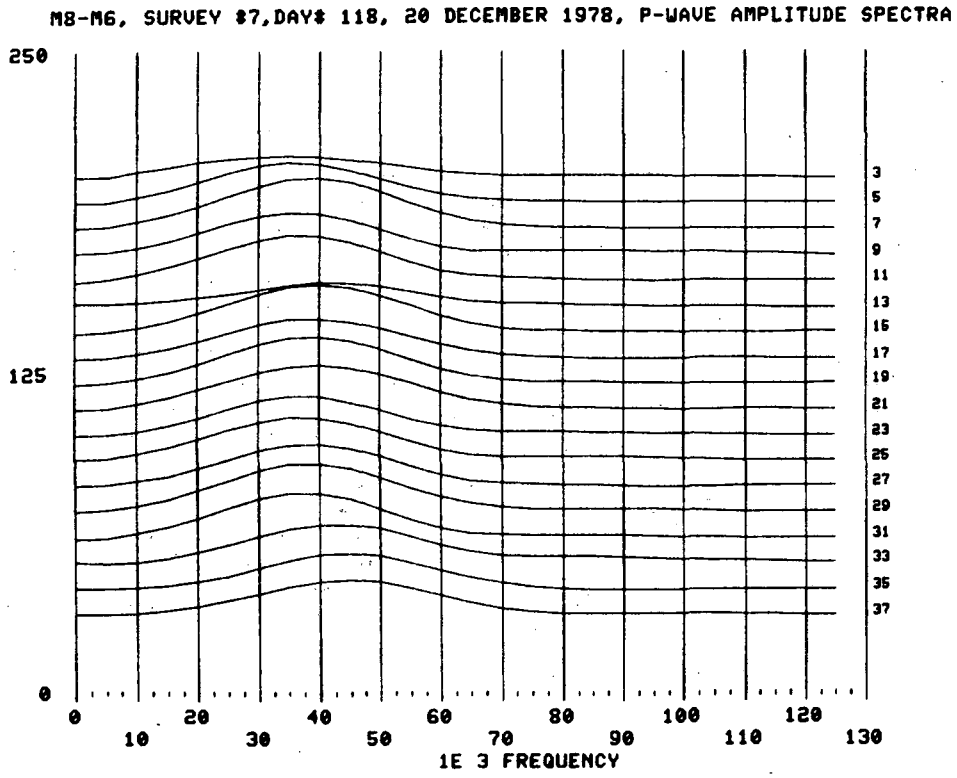


Fig. D:3.5e P wave amplitude spectra for survey # 7 in cross section M8-

M6

Fig. D:3.5f P-wave amplitude spectra for survey # 8 in cross section M8-M6

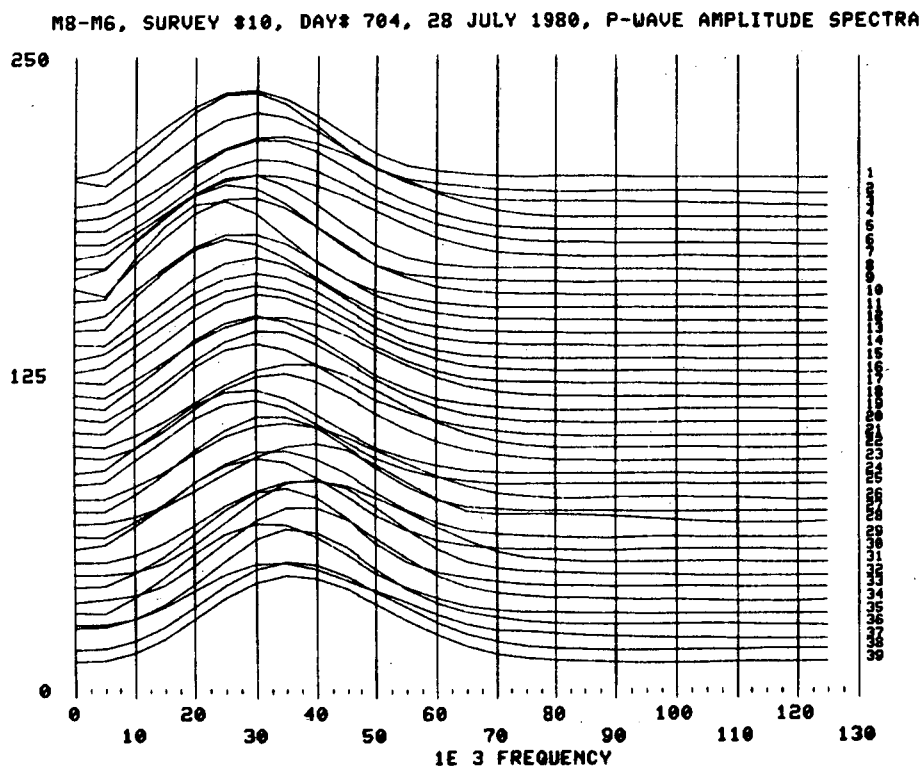
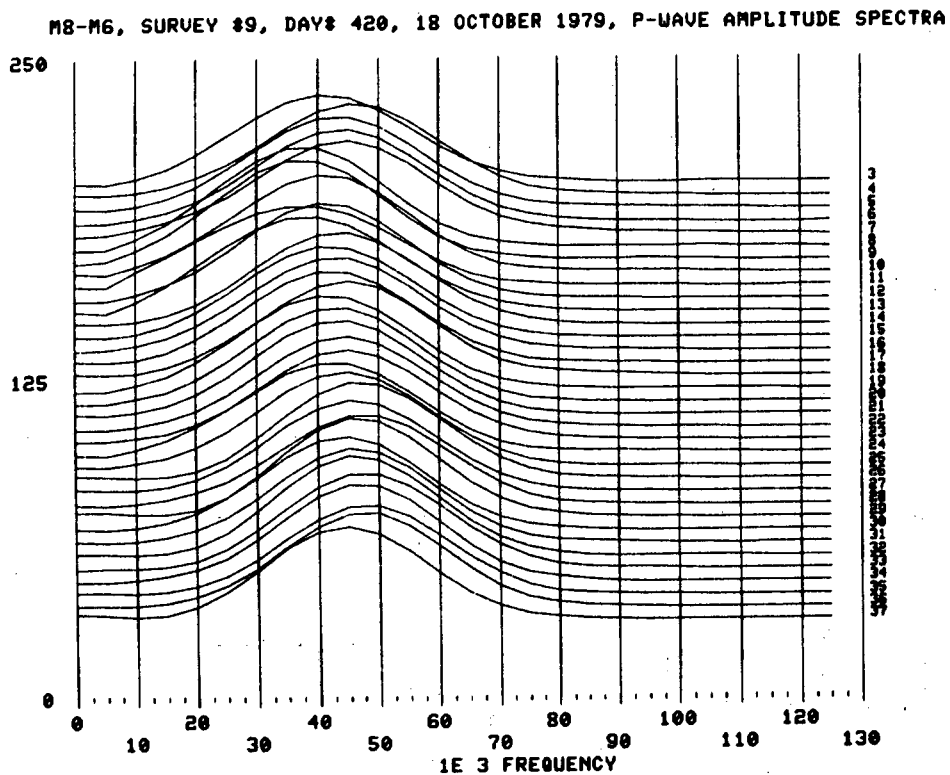


Fig. D:3.5g P wave amplitude spectra for survey # 9 in cross section M8-

M6

Fig. D:3.5h P wave amplitude spectra for survey # 10 in cross section M8-M6

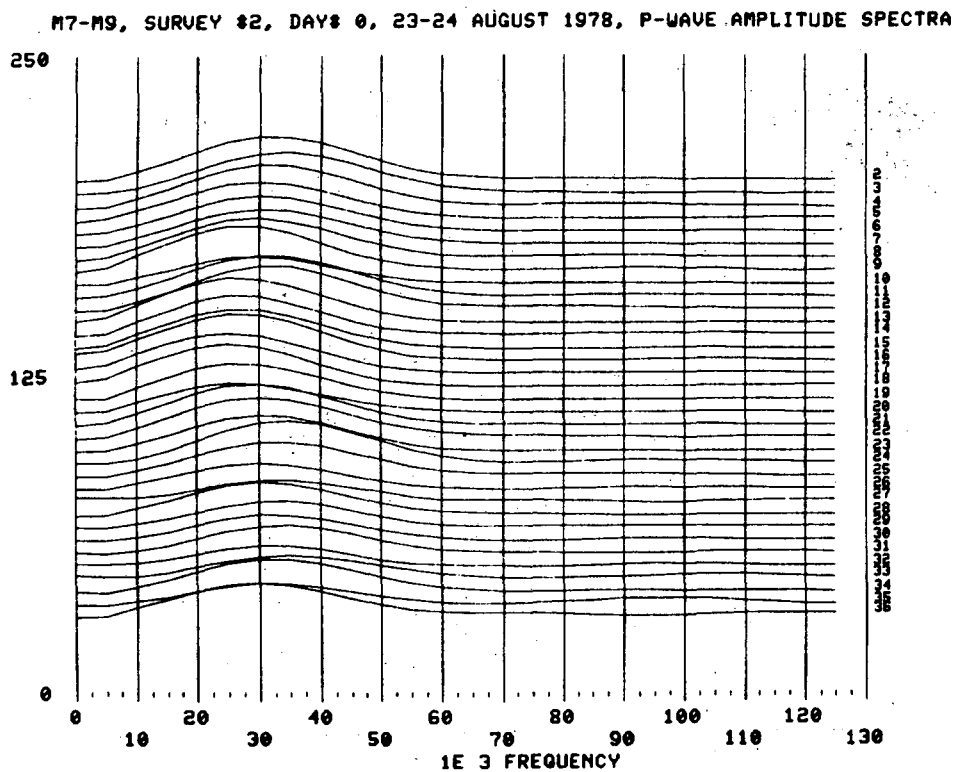
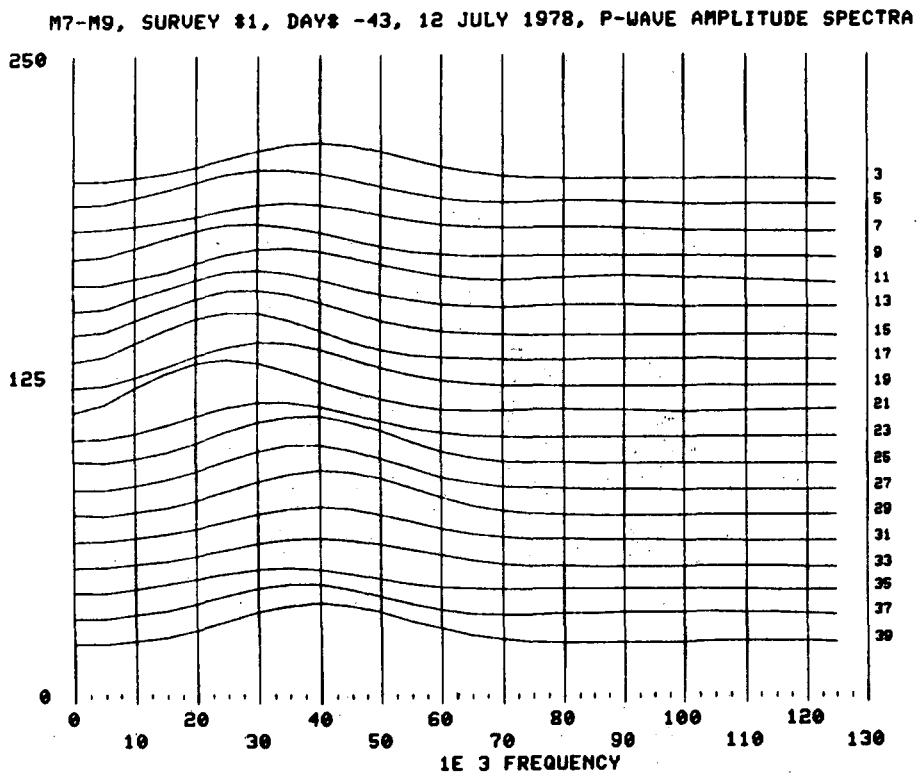


Fig. D:3.6a P wave amplitude spectra for survey # 1 in cross section M7-

M9

Fig. D:3.6b P wave amplitude spectra for survey # 2 in cross section M7-M9

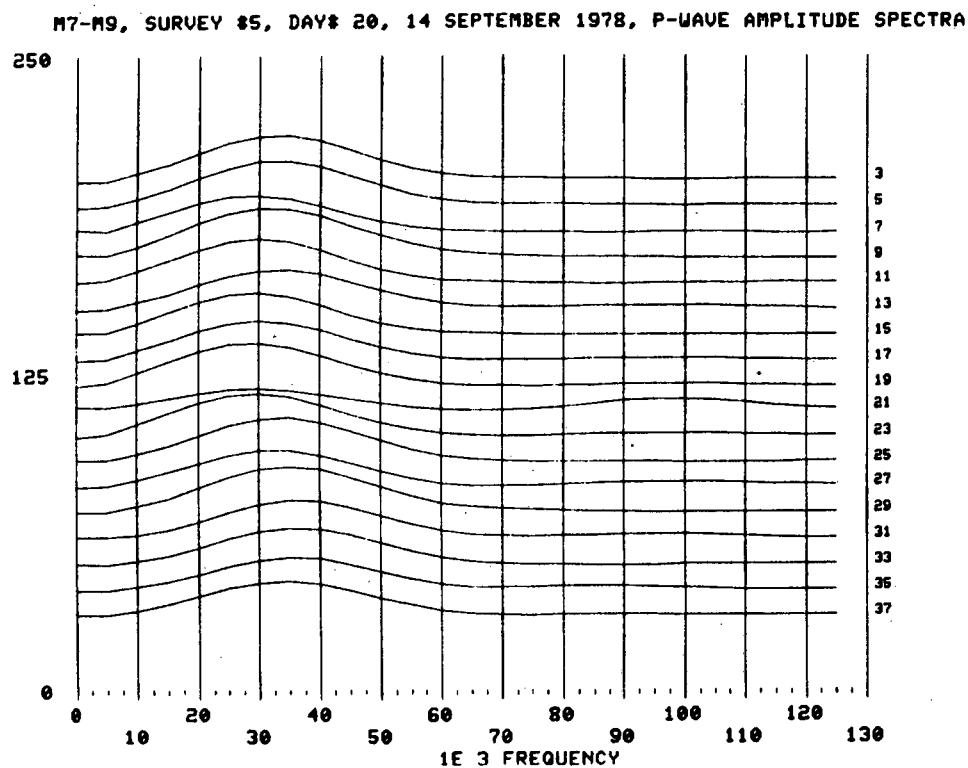
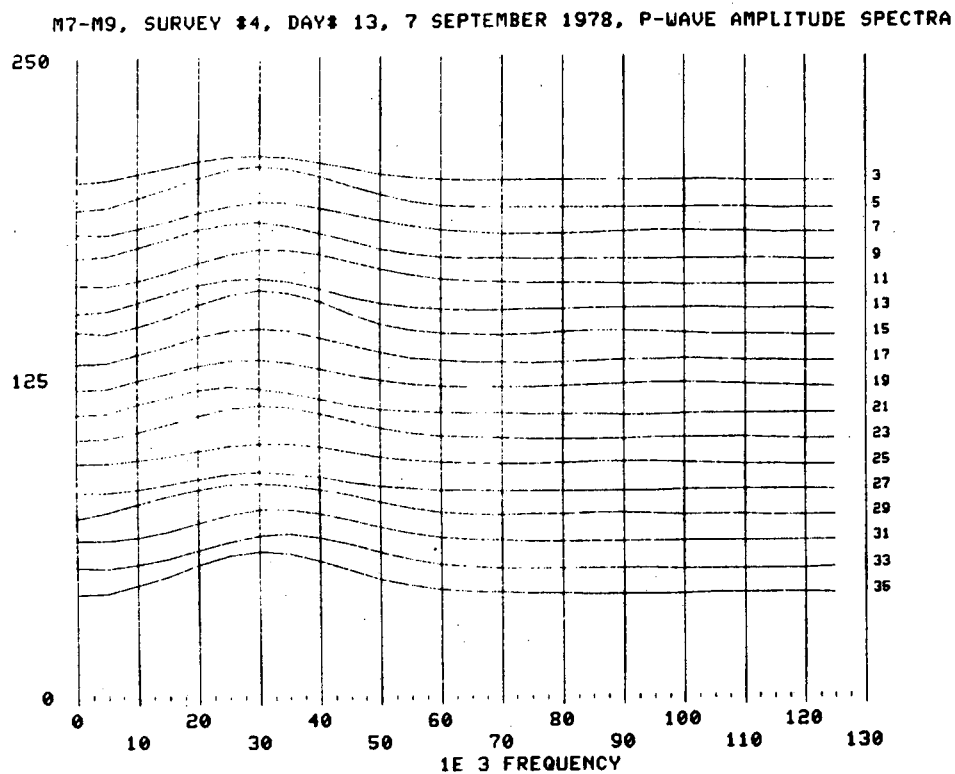


Fig. D:3.6c P wave amplitude spectra for survey # 4 in cross section M7-

M9

Fig. D:3.6d P wave amplitude spectra for survey # 5 in cross section M7-  
M9

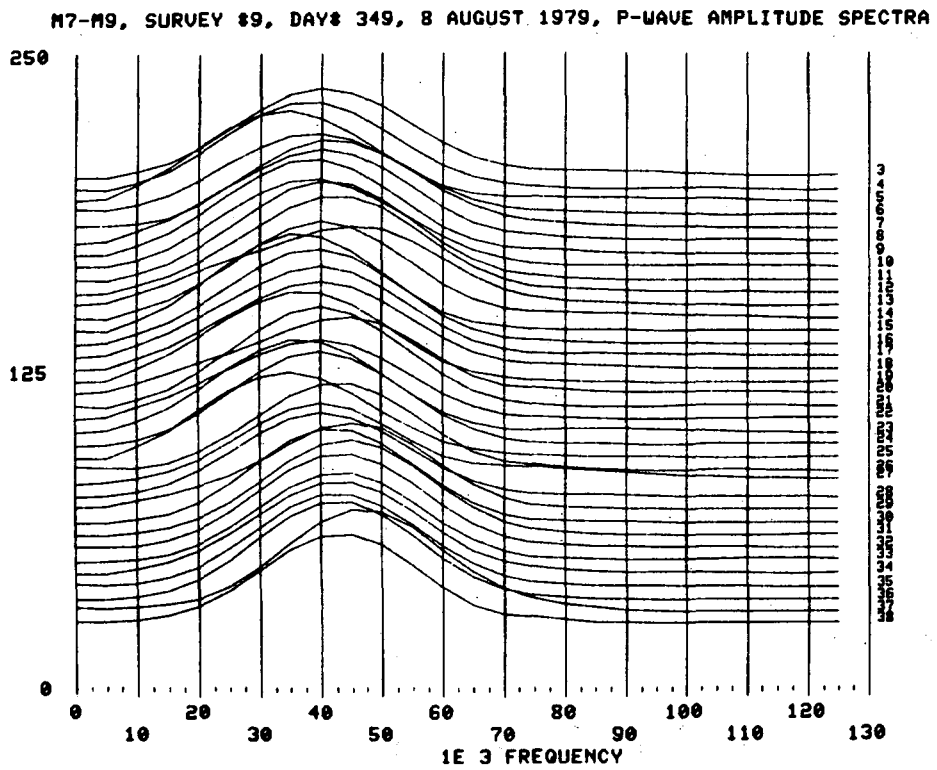
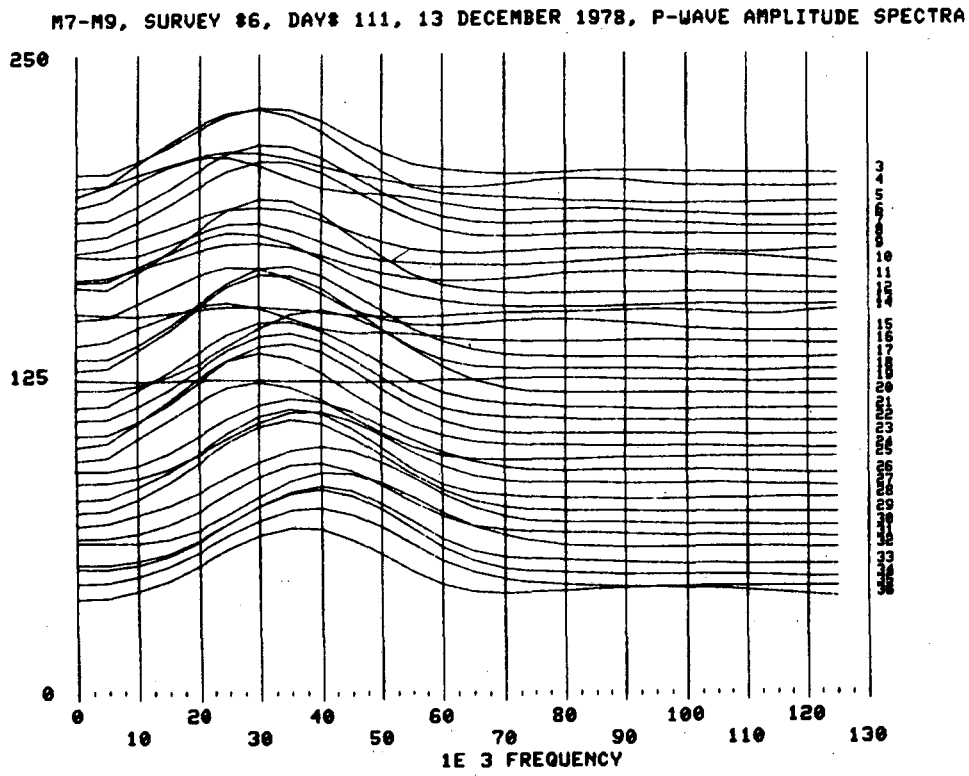


Fig. D:3.6e P wave amplitude spectra for survey # 6 in cross section M7-

M9

Fig. D:3.6f P wave amplitude spectra for survey # 9 in cross section M7-M9

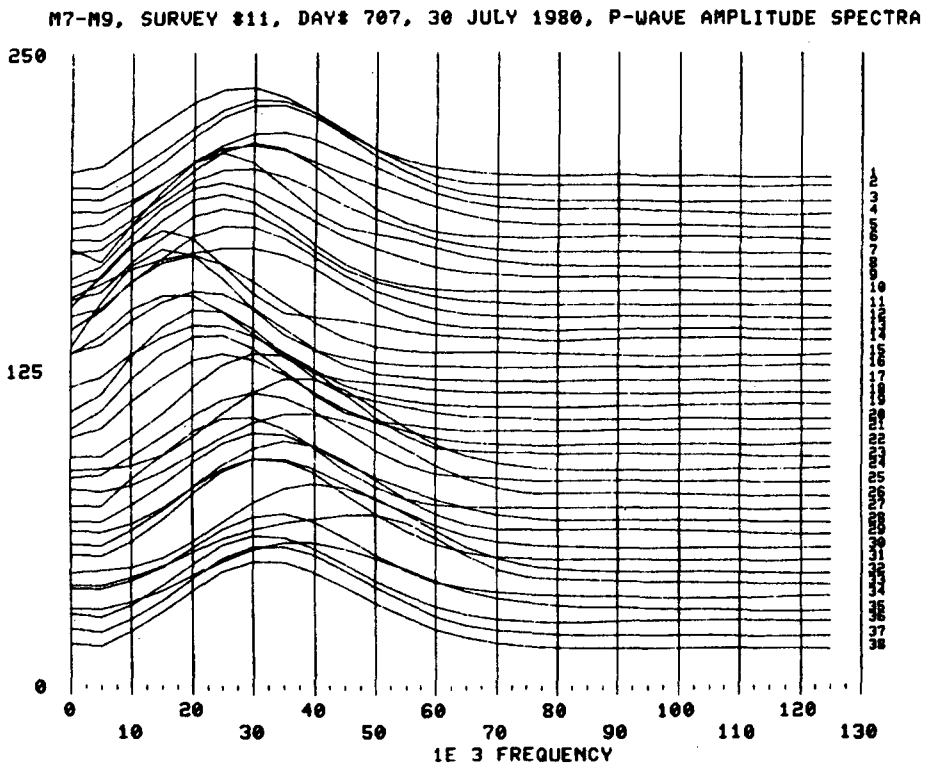
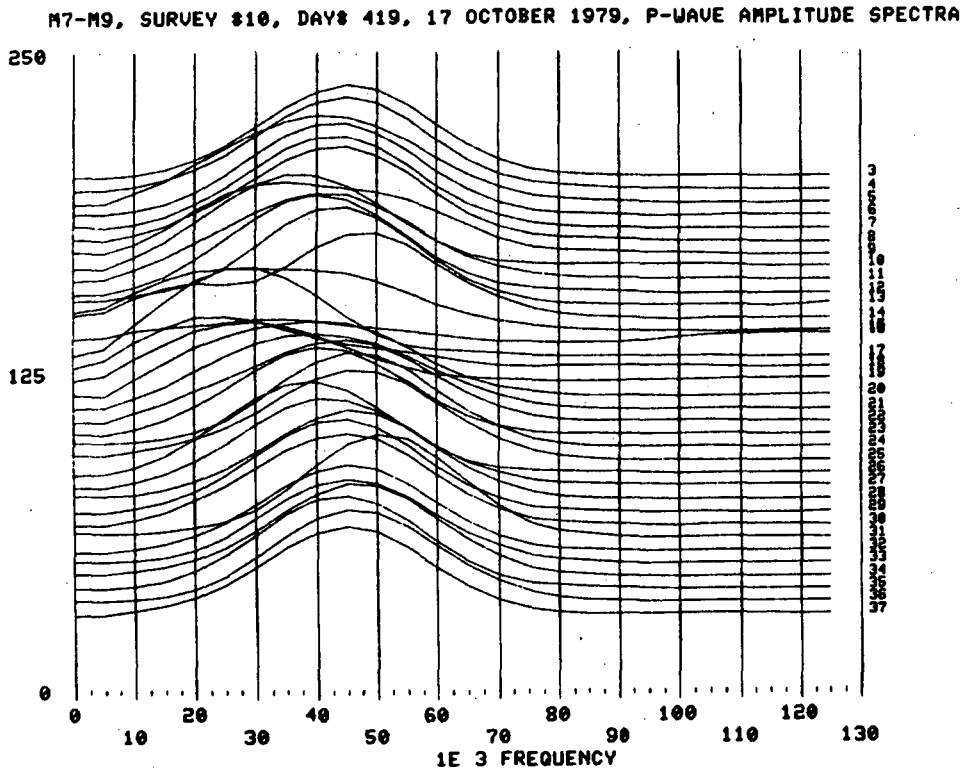


Fig. D:3.6g P wave amplitude spectra for survey # 10 in cross section

M7-M9

Fig. D:3.6h P wave amplitude spectra for survey # 11 in cross section

M7-M9

## Appendix E:1 - Tables for laboratory test of Stripa quartz monzonite.

In this appendix the tables for testing of the 11 core specimens from the full scale drift are presented. The first column shows the load in metric tons the specimen were subjected to in the laboratory press. In the second column the pressure is shown. In the third and fourth columns the  $V_p$  and  $V_s$  are presented. In the remaining columns the dynamic moduli and Poissons ratio is shown calculated from the seismic velocities in column three and four.



Table E:1.1a Specimen # 1, dry, from borehole E21, H9 area

DATE :29 OCTOBER, 1982

LENGTH OF SPECIMEN : .079045 METER.

DIAMETER OF SPECIMEN : 5.1791 CENTIMETER

NUMBER OF LOADS : 16

DENSITY OF SPECIMEN : 2605 KG/M<sup>3</sup>

LOAD (TONS)	PRESSURE (MPA)	P-WAVE VEL (M/S)	S-WAVE VEL (M/S)	YOUNGS M (GPA)	BULK M (GPA)	SHEAR M (GPA)	PO. RA
.5	2.32751	5574.4	3346.53	71.0828	42.0489	29.1741	.218253
1	4.65503	5590.17	3347.95	71.2659	42.4746	29.1988	.220358
2	9.31005	5566.55	3353.63	71.2011	41.6558	29.298	.215121
3	13.9651	5598.09	3357.9	71.6105	42.4734	29.3727	.218999
4	18.6201	5650.11	3377.99	72.6402	43.5277	29.7252	.221862
5	23.2751	5686.69	3395.4	73.4591	44.1984	30.0324	.222995
6	27.9302	5723.75	3415.95	74.3749	44.814	30.3969	.223394
7	32.5852	5752.91	3432.26	75.1037	45.2977	30.688	.223666
9	41.8952	5790.84	3456.27	76.1369	45.8638	31.1189	.223323
11	51.2053	5820.69	3476.03	76.9796	46.291	31.4757	.222842
9	41.8952	5799.34	3460.81	76.3453	46.0113	31.2007	.223455
7	32.5852	5765.5	3439.73	75.4316	45.4972	30.8217	.223677
5	23.2751	5711.34	3401.25	73.8466	44.7925	30.1359	.225227
3	13.9651	5638.02	3360.76	72.0514	43.5755	29.4227	.22442
1	4.65503	5582.27	3350.78	71.2709	42.1787	29.2483	.218377
.5	2.32751	5562.63	3345.11	70.9355	41.7404	29.1494	.216759

Table E:1.1b Specimen # 1, saturated.

DATE :3 SEPTEMBER, 1982

LENGTH OF SPECIMEN : .079045 METER.

DIAMETER OF SPECIMEN : 5.1791 CENTIMETER

NUMBER OF LOADS : 16

DENSITY OF SPECIMEN : 2811 KG/M<sup>3</sup>

LOAD (TONS)	PRESSURE (MPA)	P-WAVE VEL (M/S)	S-WAVE VEL (M/S)	YOUNGS M (GPA)	BULK M (GPA)	SHEAR M (GPA)	PO. RA
.5	2.32751	5970.17	3483.69	78.7026	50.8137	31.6874	.241859
1	4.65503	5970.17	3483.69	78.7026	50.8137	31.6874	.241859
2	9.31005	5970.17	3485.23	78.7501	50.7764	31.7154	.241514
3	13.9651	5974.68	3489.85	78.8305	50.8051	31.7994	.241068
4	18.6201	5979.2	3513.11	79.6844	50.3780	32.2248	.236383
5	23.2751	5982.8	3541.44	80.6674	50.1002	32.7467	.231689
6	27.9302	5982.8	3554.18	81.0521	49.7938	32.9827	.228706
7	32.5852	5997.35	3570.24	81.5756	49.5378	33.2813	.225544
9	41.8952	6001.9	3562.19	81.377	49.8802	33.1315	.228092
11	51.2053	6001.9	3562.19	81.377	49.8802	33.1315	.228092
9	41.8952	6001.9	3563.8	81.4253	49.8403	33.1614	.227713
7	32.5852	5997.35	3558.98	81.2384	49.817	33.0718	.228211
5	23.2751	5979.2	3509.99	79.5889	50.4552	32.1676	.237097
3	13.9651	5965.86	3494.47	78.997	50.4114	31.8838	.238826
1	4.65503	5907.7	3480.63	78.0772	48.9507	31.8316	.234164
.5	2.32751	5898.88	3474.51	77.8166	48.8271	31.5205	.234381

Table E.1.2a Specimen # 2, dry, from borehole E24, H9 area

DATE : 13 SEPTEMBER, 1982

LENGTH OF SPECIMEN : .081928 METER.

DIAMETER OF SPECIMEN : 5.1689 CENTIMETER

NUMBER OF LOADS : 16

DENSITY OF SPECIMEN : 2605 KG/M<sup>3</sup>

LOAD (TONS)	PRESSURE (MPA)	P-WAVE VEL (M/S)	S-WAVE VEL (M/S)	YOUNGS M (GPA)	BULK M (GPA)	SHEAR M (GPA)	PO. RA
.5	2.33671	4989.52	3180.43	61.0168	29.7191	26.35	.157813
1	4.67342	5017.02	3189.1	61.5182	30.2441	26.4938	.160991
2	9.34683	5032.43	3217.91	62.2657	30.0064	26.9746	.154153
3	14.0203	5114.11	3264.06	64.1848	31.1261	27.754	.156318
4	18.6937	5245.07	3325	67.05	33.2656	28.7999	.164068
5	23.3671	5379.38	3378.47	69.834	35.7379	29.7337	.174323
6	28.0405	5469.16	3419.37	71.8278	37.3095	30.4578	.179136
7	32.7139	5550.68	3458.34	73.6999	38.7187	31.156	.182755
9	42.0607	5661.92	3511.7	76.2908	40.6761	32.125	.187405
11	51.4076	5733.24	3542.07	77.8731	42.0492	32.6829	.191342
9	42.0607	5701.32	3522.27	77.0065	41.5842	32.3186	.191363
7	32.7139	5600	3480.37	74.8045	39.6203	31.5544	.185327
5	23.3671	5461.87	3405.15	71.411	37.4388	30.2052	.182099
3	14.0203	5235.02	3303.55	66.4755	33.485	28.4295	.169128
1	4.67342	5020.1	3189.1	61.555	30.3245	26.4938	.161687
.5	2.33671	4977.4	3174.27	60.7507	29.5403	26.248	.157244

Table E.1.2b Specimen # 2, saturated.

DATE : 31 AUGUST, 1982

LENGTH OF SPECIMEN : .081928 METER.

DIAMETER OF SPECIMEN : 5.1689 CENTIMETER

NUMBER OF LOADS : 16

DENSITY OF SPECIMEN : 2811 KG/M<sup>3</sup>

LOAD (TONS)	PRESSURE (MPA)	P-WAVE VEL (M/S)	S-WAVE VEL (M/S)	YOUNGS M (GPA)	BULK M (GPA)	SHEAR M (GPA)	PO. RA
.5	2.33671	5814.62	3423.65	75.5731	47.4713	30.6046	.234671
1	4.67342	5835.33	3422.22	75.7058	48.1353	30.579	.237871
2	9.34683	5864.57	3430.82	76.2083	48.8233	30.7328	.23985
3	14.0203	5877.19	3439.46	76.5748	49.0036	30.8879	.239561
4	18.6937	5894.1	3462.72	77.4207	48.9645	31.307	.236474
5	23.3671	5902.59	3480.37	78.025	48.7994	31.627	.233518
6	28.0405	5923.93	3490.75	78.5239	49.2065	31.816	.234033
7	32.7139	5932.51	3514.71	79.3189	48.8877	32.2542	.229588
9	42.0607	5949.75	3542.07	80.2906	48.7504	32.7582	.225504
11	51.4076	5967.08	3571.4	81.3204	48.5632	33.3031	.220912
9	42.0607	5958.4	3551.28	80.6446	48.792	32.9288	.224529
7	32.7139	5932.51	3516.22	79.3639	48.8508	32.2819	.22923
5	23.3671	5856.18	3486.3	77.7833	47.2309	31.7348	.225521
3	14.0203	5697.36	3440.91	74.991	43.5343	30.9138	.212904
1	4.67342	5502.22	3359.08	70.8789	39.765	29.461	.202926
.5	2.33671	5513.32	3359.08	70.9909	40.0845	29.461	.204828

Table E.1.3a Specimen # 3, dry, from borehole E29, H10 area

DATE : 13 SEPTEMBER, 1982

LENGTH OF SPECIMEN : .081178 METER.

DIAMETER OF SPECIMEN : 5.1867 CENTIMETER

NUMBER OF LOADS : 16

DENSITY OF SPECIMEN : 2605 KG/M<sup>3</sup>

LOAD (TONS)	PRESSURE (MPA)	P-WAVE VEL (M/S)	S-WAVE VEL (M/S)	YOUNGS M (GPA)	BULK M (GPA)	SHEAR M (GPA)	PO. RA
.5	2.3207	5586.92	3307.99	70.1295	43.3038	28.5059	.230087
1	4.6414	5586.92	3318.81	70.4322	43.0548	28.6927	.227354
2	9.28279	5629.54	3354.46	71.8003	43.4736	29.3126	.224736
3	13.9242	5680.76	3373.98	72.8019	44.5263	29.6547	.227495
4	18.5656	5716.76	3392.31	73.6404	45.1646	29.9777	.228252
5	23.207	5749.15	3416.58	74.6223	45.558	30.4083	.227006
6	27.8484	5773.68	3429.57	75.2147	45.9855	30.6399	.227397
7	32.4898	5798.43	3444.12	75.8566	46.3841	30.9005	.227433
9	41.7726	5827.57	3461.75	76.6301	46.8438	31.2175	.227356
11	51.0553	5848.56	3470.63	77.0783	47.2685	31.3779	.228225
9	41.7726	5835.95	3460.27	76.6623	47.1339	31.1909	.22892
7	32.4898	5802.57	3444.12	75.8937	46.5093	30.9005	.228034
5	23.207	5777.79	3413.71	74.791	46.4863	30.3571	.231853
3	13.9242	5712.74	3371.18	72.9981	45.5412	29.6064	.23285
1	4.6414	5625.64	3332.43	71.1478	43.8709	28.8288	.229708
.5	2.3207	5598.48	3313.39	70.3794	43.5164	28.5991	.230449

Table E:1.3b Specimen # 3, saturated.

DATE : 12 SEPTEMBER, 1982

LENGTH OF SPECIMEN : .081178 METER.

DIAMETER OF SPECIMEN : 5.1867 CENTIMETER

NUMBER OF LOADS : 16

DENSITY OF SPECIMEN : 2811 KG/M<sup>3</sup>

LOAD (TONS)	PRESSURE (MPA)	P-WAVE VEL (M/S)	S-WAVE VEL (M/S)	YOUNGS M (GPA)	BULK M (GPA)	SHEAR M (GPA)	PO. RA
.5	2.3207	5865.46	3472.11	77.4511	47.8585	31.4771	.230278
1	4.6414	5891	3475.09	77.7651	48.5705	31.531	.233154
2	9.28279	5921.08	3481.05	78.206	49.3538	31.6393	.2359
3	13.9242	5934.06	3490.03	78.5901	49.5379	31.8027	.235589
4	18.5656	5942.75	3503.58	79.0762	49.4772	32.0503	.233628
5	23.207	5947.11	3512.68	79.389	49.3902	32.2169	.232103
6	27.8484	5955.83	3518.77	79.6504	49.5123	32.3287	.231884
7	32.4898	5960.21	3524.88	79.8737	49.4985	32.4411	.231057
9	41.7726	5964.58	3530.71	80.3285	49.2947	32.6962	.228408
11	51.0553	5968.97	3538.71	80.3687	49.4314	32.6962	.229023
9	41.7726	5968.97	3535.63	80.2762	49.5073	32.6392	.22975
7	32.4898	5955.83	3523.35	79.7883	49.4	32.4129	.230809
5	23.207	5951.47	3506.61	79.2443	49.674	32.1056	.234119
3	13.9242	5934.06	3488.53	78.5447	49.5743	31.7754	.235936
1	4.6414	5882.46	3458.8	77.2029	48.7012	31.2361	.235794
.5	2.3207	5865.46	3449.98	76.7925	48.3919	31.0771	.235519

Table E:1.4a Specimen # 4, dry, from borehole DBEX-1, H10 area

DATE : 3 SEPTEMBER, 1982

LENGTH OF SPECIMEN : .077775 METER.

DIAMETER OF SPECIMEN : 5.2095 CENTIMETER

NUMBER OF LOADS : 16

DENSITY OF SPECIMEN : 2605 KG/M<sup>3</sup>

LOAD (TONS)	PRESSURE (MPA)	P-WAVE VEL (M/S)	S-WAVE VEL (M/S)	YOUNGS M (GPA)	BULK M (GPA)	SHEAR M (GPA)	PO. RA
.5	2.30043	5555.36	3421.69	72.855	39.7299	30.4982	.194374
1	4.60086	5571.28	3436.81	73.4061	39.8311	30.7694	.192844
2	9.20171	5623.65	3441.37	74.0838	41.2493	30.8511	.204666
3	13.8026	5672.87	3459.74	75.0777	42.2574	31.1814	.203888
4	18.4034	5710.35	3473.65	75.8343	43.0341	31.4325	.206302
5	23.0043	5744.09	3489.23	76.5996	43.6639	31.7152	.207617
6	27.6051	5773.94	3498.65	77.1599	44.331	31.8866	.20991
7	32.206	5799.78	3504.96	77.5938	44.9565	32.0017	.212338
9	41.4077	5838.96	3508.12	78.0685	46.0676	32.0595	.217558
11	50.6094	5856.55	3514.46	78.4192	46.4488	32.1755	.218618
9	41.4077	5838.96	3509.7	78.1134	46.029	32.0884	.217159
7	32.206	5812.78	3498.65	77.5463	45.5033	31.8866	.215968
5	23.0043	5765.38	3484.54	76.6864	44.4159	31.63	.212241
3	13.8026	5693.63	3472.1	75.6202	42.5748	31.4045	.203971
1	4.60086	5591.3	3450.53	73.9691	40.0851	31.0156	.19245
.5	2.30043	5563.3	3435.29	73.2808	39.6361	30.7422	.19186

Table E:1.4b Specimen # 4, saturated.

DATE : 2 SEPTEMBER, 1982

LENGTH OF SPECIMEN : .077775 METER.

DIAMETER OF SPECIMEN : 5.2095 CENTIMETER

NUMBER OF LOADS : 16

DENSITY OF SPECIMEN : 2611 KG/M<sup>3</sup>

LOAD (TONS)	PRESSURE (MPA)	P-WAVE VEL (M/S)	S-WAVE VEL (M/S)	YOUNGS M (GPA)	BULK M (GPA)	SHEAR M (GPA)	PO. RA
.5	2.30043	5869.81	3449	76.8004	48.5486	31.0595	.236345
1	4.60086	5887.59	3452.06	77.0434	49.0207	31.1146	.238058
2	9.20171	5909.96	3456.67	77.3709	49.599	31.1976	.240012
3	13.8026	5914.45	3465.91	77.6901	49.515	31.3647	.238496
4	18.4034	5923.46	3473.65	78.0019	49.6065	31.5049	.237931
5	23.0043	5927.97	3478.31	78.1821	49.6334	31.5895	.237468
6	27.6051	5932.49	3484.54	78.4103	49.6223	31.7029	.236643
7	32.206	5941.56	3493.94	78.7737	49.6752	31.874	.235704
9	41.4077	5950.65	3503.38	79.1393	49.7274	32.0465	.234756
11	50.6094	5959.77	3504.96	79.2668	49.9725	32.0754	.235632
9	41.4077	5946.1	3503.38	79.0995	49.5862	32.0465	.234135
7	32.206	5937.02	3497.08	78.8293	49.458	31.9314	.234356
5	23.0043	5923.46	3472.1	77.9547	49.644	31.4768	.238288
3	13.8026	5896.51	3450.53	77.0719	49.3321	31.087	.239616
1	4.60086	5852.15	3432.28	76.148	48.4089	30.7586	.237831
.5	2.30043	5812.78	3417.18	75.3655	47.5696	30.489	.235947

Table E:1.5a Specimen # 5, dry, from borehole DBEX-1, H10 area

DATE : 13 SEPTEMBER, 1982

LENGTH OF SPECIMEN : .078943 METER.

DIAMETER OF SPECIMEN : 5.1956 CENTIMETER

NUMBER OF LOADS : 16

DENSITY OF SPECIMEN : 2605 KG/M<sup>3</sup>

LOAD (TONS)	PRESSURE (MPA)	P-WAVE VEL (M/S)	S-WAVE VEL (M/S)	YOUNGS M (GPA)	BULK M (GPA)	SHEAR M (GPA)	PO. RA
.5	2.31275	5539.86	3259.41	68.3727	43.0477	27.6749	.235283
1	4.62551	5555.45	3268.86	68.7659	43.2842	27.8356	.235215
2	9.25101	5567.21	3296.16	69.6312	43.0023	28.3024	.230126
3	13.8765	5610.73	3312.78	70.4648	43.8886	28.5882	.23241
4	18.502	5654.94	3372.19	72.5223	43.8061	29.6232	.224078
5	23.1275	5691.64	3404.18	73.7501	44.1377	30.1879	.221515
6	27.753	5728.81	3429.32	74.7982	44.6469	30.6355	.220779
7	32.3786	5753.86	3448.8	75.58	44.931	30.9844	.219644
8	41.6296	5791.86	3470.02	76.5375	45.5637	31.3669	.220035
9	50.8806	5821.76	3479.2	77.0803	46.2468	31.5331	.222214
10	41.6296	5808.9	3468.5	76.6539	46.1156	31.3394	.222965
11	32.3786	5766.47	3450.31	75.7408	45.2733	31.0115	.221172
12	23.1275	5724.66	3413.01	74.3001	44.9105	30.3448	.224266
13	13.8765	5642.82	3340.8	71.5317	44.1812	29.0742	.230158
14	4.62551	5551.55	3321.12	70.184	41.975	28.7327	.221326
15	2.31275	5532.1	3263.46	68.4231	42.7321	27.7436	.233132

Table E:1.5b Specimen # 5, saturated.

DATE : 13 SEPTEMBER, 1982.

LENGTH OF SPECIMEN : .078943 METER.

DIAMETER OF SPECIMEN : 5.1956 CENTIMETER

NUMBER OF LOADS : 16

DENSITY OF SPECIMEN : 2611 KG/M<sup>3</sup>

LOAD (TONS)	PRESSURE (MPA)	P-WAVE VEL (M/S)	S-WAVE VEL (M/S)	YOUNGS M (GPA)	BULK M (GPA)	SHEAR M (GPA)	PO. RA
.5	2.31275	5900.07	3486.88	78.1975	48.5639	31.7454	.231634
1	4.62551	5900.07	3489.96	78.2894	48.4891	31.8016	.230904
2	9.25101	5908.91	3500.8	78.691	48.4978	31.9993	.229572
3	13.8765	5913.33	3521.1	79.3318	48.1382	32.3715	.225333
4	18.502	5917.77	3532.13	79.697	48.0043	32.5746	.223299
5	23.1275	5922.21	3544.81	80.1096	47.829	32.809	.220847
6	27.753	5931.1	3554.39	80.4742	47.8677	32.9866	.219803
7	32.3786	5940.03	3560.8	80.7476	47.9855	33.1057	.219542
8	41.6296	5944.5	3564.02	80.8847	48.0445	33.1655	.219411
9	50.8806	5953.47	3565.63	81.0191	48.2031	33.1955	.220333
10	41.6296	5944.5	3557.59	80.6975	48.2038	33.046	.220985
11	32.3786	5935.56	3541.63	80.1443	48.321	32.7502	.22357
12	23.1275	5922.21	3532.13	79.7389	48.1416	32.5746	.223943
13	13.8765	5904.49	3508.58	78.8811	48.1716	32.1417	.227083
14	4.62551	5860.65	3493.05	78.0214	47.2035	31.8579	.224521
15	2.31275	5856.31	3479.2	77.5771	47.4068	31.6057	.227265

Table E:1.6a Specimen # 6, dry, from borehole E22, H9 area.

DATE :17 SEPTEMBER, 1982

LENGTH OF SPECIMEN : .07813 METER.

DIAMETER OF SPECIMEN : 5.1742 CENTIMETER

NUMBER OF LOADS : 16

DENSITY OF SPECIMEN : 2606 KG/M<sup>3</sup>

LOAD (TONS)	PRESSURE (MPA)	P-WAVE VEL (M/S)	S-WAVE VEL (M/S)	YOUNGS M (GPA)	BULK M (GPA)	SHEAR M (GPA)	PO. RA
.5	2.33192	5572.75	3495.75	74.8765	38.4695	31.846	.175602
1	4.66385	5608.76	3495.75	75.3089	39.5186	31.846	.182391
2	9.32769	5657.49	3489.5	75.7123	41.1011	31.7323	.192984
3	13.9915	5698.76	3494.19	76.2845	42.2088	31.8175	.198781
4	18.6554	5728.01	3511.46	77.0522	42.6591	32.1329	.198961
5	23.3192	5761.8	3527.31	77.8355	43.2832	32.4237	.200286
6	27.9831	5783.12	3535.29	78.2773	43.729	32.5706	.201657
7	32.6469	5800.3	3549.75	78.8488	43.8915	32.8375	.200592
9	41.9746	5834.95	3574.11	79.8783	44.3394	33.2897	.199746
11	51.3023	5852.44	3593.84	80.5991	44.3805	33.6582	.197318
9	41.9746	5834.95	3579.02	80.0097	44.2173	33.3812	.198422
7	32.6469	5813.24	3552.98	79.0753	44.2037	32.8972	.201852
5	23.3192	5774.58	3528.91	78.0151	43.6283	32.453	.20187
3	13.9915	5702.92	3502.02	76.5334	42.142	31.9603	.197319
1	4.66385	5592.7	3488.39	74.5128	38.3513	31.6757	.176183
.5	2.33192	5560.85	3486.39	74.5128	38.3513	31.6757	.176183

Table E:1.6b Specimen # 6, saturated.

DATE :29 SEPTEMBER, 1982

LENGTH OF SPECIMEN : .07813 METER.

DIAMETER OF SPECIMEN : 5.1742 CENTIMETER

NUMBER OF LOADS : 16

DENSITY OF SPECIMEN : 2611 KG/M<sup>3</sup>

LOAD (TONS)	PRESSURE (MPA)	P-WAVE VEL (M/S)	S-WAVE VEL (M/S)	YOUNGS M (GPA)	BULK M (GPA)	SHEAR M (GPA)	PO. RA
.5	2.33192	5977.81	3506.73	79.4771	50.4915	32.1079	.237655
1	4.66385	5982.39	3505.16	79.4679	50.6729	32.0791	.238624
2	9.32769	5977.81	3514.62	79.7185	50.2987	32.2525	.23585
3	13.9915	5982.39	3530.5	80.2424	50.0521	32.5447	.232804
4	18.6554	5977.81	3538.5	80.4429	49.7125	32.6922	.230306
5	23.3192	5982.39	3551.36	80.8714	49.5378	32.9304	.227914
6	27.9831	5982.39	3554.6	80.9681	49.4579	32.9904	.227148
7	32.6469	5986.97	3561.08	81.2045	49.4406	33.1108	.226256
9	41.9746	5991.56	3561.08	81.2475	49.5842	33.1108	.226904
11	51.3023	5991.56	3562.7	81.296	49.5439	33.141	.226519
9	41.9746	5991.56	3557.83	81.1503	49.6646	33.0505	.227672
7	32.6469	5986.97	3549.75	80.8652	49.721	32.9005	.228936
5	23.3192	5977.81	3544.92	80.6359	49.5541	32.811	.228795
3	13.9915	5968.68	3524.13	79.9271	49.7808	32.4273	.232403
1	4.66385	5941.45	3508.31	79.207	49.3213	32.1368	.232343
.5	2.33192	5932.42	3487.95	78.5129	49.5375	31.7648	.235847

Table E:1.7a Specimen # 7, dry, from borehole E22, H9 area.

DATE :29 SEPTEMBER, 1982

LENGTH OF SPECIMEN : .08255 METER.

DIAMETER OF SPECIMEN : 5.1765 CENTIMETER

NUMBER OF LOADS : 16

DENSITY OF SPECIMEN : 2611 KG/M<sup>3</sup>

LOAD (TONS)	PRESSURE (MPA)	P-WAVE VEL (M/S)	S-WAVE VEL (M/S)	YOUNGS M (GPA)	BULK M (GPA)	SHEAR M (GPA)	PO. RA
.5	2.32985	5960.29	3579.79	81.4985	48.1429	33.4597	.217850
1	4.65971	5964.6	3586.01	81.7217	48.1218	33.5761	.216962
2	9.31941	5973.23	3587.57	81.8529	48.3519	33.6053	.217857
3	13.9791	5968.91	3587.57	81.81	48.2173	33.6053	.217218
4	18.6388	5973.23	3587.57	81.8529	48.3519	33.6053	.217857
5	23.2985	5973.23	3592.25	81.989	48.2349	33.6931	.216702
6	27.9582	5981.88	3600.09	82.303	48.309	33.8402	.216053
7	32.6179	5981.88	3604.8	82.4395	48.1907	33.9289	.214885
9	41.9373	5990.57	3609.53	82.6644	48.3433	34.018	.215009
11	51.2567	5999.27	3607.95	82.7066	48.6556	33.9883	.216694
9	41.9373	5986.22	3607.95	82.5746	48.2471	33.9883	.214751
7	32.6179	5977.55	3603.23	82.35	48.0949	33.8993	.214627
5	23.2985	5977.55	3587.57	81.8958	48.4869	33.6053	.218495
3	13.9791	5973.23	3526.27	80.0324	49.8701	32.4667	.23253
1	4.65971	5938.85	3475.79	78.1974	50.0314	31.5438	.239506
.5	2.32985	5938.85	3475.79	78.1974	50.0314	31.5438	.239506

Table E:1.7b Specimen # 7, saturated.

DATE :17 SEPTEMBER, 1982

LENGTH OF SPECIMEN : .08255 METER.

DIAMETER OF SPECIMEN : 5.1765 CENTIMETER

NUMBER OF LOADS : 16

DENSITY OF SPECIMEN : 2606 KG/M<sup>3</sup>

LOAD (TONS)	PRESSURE (MPA)	P-WAVE VEL (M/S)	S-WAVE VEL (M/S)	YOUNGS M (GPA)	BULK M (GPA)	SHEAR M (GPA)	PO. RA
.5	2.32985	5665.75 ✓	3419.64	73.96	43.0221	30.4743	.21348
1	4.65971	5669.64 ✓	3421.05	74.0363	43.1034	30.4996	.213726
2	9.31941	5681.35	3439.58	74.6538	43.0079	30.8309	.210698
3	13.9791	5716.76	3452.53	75.3555	43.7497	31.0634	.212929
4	18.6388	5752.61	3477.25	76.3882	44.226	31.5099	.21213
5	23.2985	5788.92	3502.33	77.442	44.7098	31.9661	.211316
6	27.9582	5813.38	3533.82	78.5572	44.6796	32.5434	.206961
7	32.6179	5833.92	3552.07	79.271	44.8539	32.8803	.205447
9	41.9373	5867.09	3561.26	79.8716	45.6381	33.0508	.208315
11	51.2567	5888.02	3576.69	80.5181	45.8964	33.3378	.207609
9	41.9373	5875.45	3565.87	80.0865	45.7794	33.1365	.208433
7	32.6179	5842.18	3555.13	79.4417	45.0296	32.937	.205965
5	23.2985	5809.29	3517.26	78.0599	44.9615	32.2391	.210642
3	13.9791	5756.63	3449.65	75.6588	45.0108	31.0115	.21985
1	4.65971	5677.44	3369.39	72.6704	44.553	29.5853	.22815
.5	2.32985	5657.99	3362.53	72.3056	44.1388	29.4649	.226976

Table E:1.8a Specimen # 8, dry from borehole E22, H9 area.

DATE :19 SEPTEMBER, 1982

LENGTH OF SPECIMEN : .080683 METER.

DIAMETER OF SPECIMEN : 5.1841 CENTIMETER

NUMBER OF LOADS : 16

DENSITY OF SPECIMEN : 2606 KG/M<sup>3</sup>

LOAD (TONS)	PRESSURE (MPA)	P-WAVE VEL (M/S)	S-WAVE VEL (M/S)	YOUNGS M (GPA)	BULK M (GPA)	SHEAR M (GPA)	PO. RA
.5	2.32303	5511.13	3283.8	68.8352	41.6824	28.1014	.224763
1	4.64606	5514.9	3282.47	68.8313	41.8212	28.0788	.225692
2	9.2921	5579.74	3316.19	70.3243	42.8224	28.6588	.226933
3	13.9382	5626.43	3343.68	71.4987	43.6499	29.1356	.227
4	18.5842	5665.94	3367.4	72.5133	44.2595	29.5506	.228939
5	23.2303	5697.86	3382.84	73.2356	44.8432	29.8237	.227888
6	27.8763	5738.48	3392.89	73.8748	45.8165	29.9996	.231266
7	32.5224	5783.07	3407.82	74.5032	46.2151	30.2536	.231317
8	41.8145	5796.19	3431.86	75.5096	46.6274	30.6026	.230096
9	51.1066	5821.28	3446.52	76.159	47.0366	30.9554	.230143
9	41.8145	5804.53	3430.4	75.54	46.9143	30.6665	.231638
7	32.5224	5771.32	3415.88	74.8264	46.2577	30.4074	.2304
5	23.2303	5722.2	3381.52	73.4067	45.5981	29.7987	.231693
3	13.9382	5658	3321.86	71.1375	45.0883	28.753	.237044
1	4.64606	5568.19	3291.84	69.545	43.146	28.2392	.231358
.5	2.32303	5552.88	3286.48	69.2661	42.8243	28.1478	.230425

Table E:1.8b Specimen # 8, saturated.

DATE :29 SEPTEMBER, 1982

LENGTH OF SPECIMEN : .080683 METER.

DIAMETER OF SPECIMEN : 5.1841 CENTIMETER

NUMBER OF LOADS : 16

DENSITY OF SPECIMEN : 2611 KG/M<sup>3</sup>

LOAD (TONS)	PRESSURE (MPA)	P-WAVE VEL (M/S)	S-WAVE VEL (M/S)	YOUNGS M (GPA)	BULK M (GPA)	SHEAR M (GPA)	PO. RA
.5	2.32303	5950.07	3439.17	77.1541	51.2613	30.8827	.249148
1	4.64606	5954.46	3477.72	78.3873	50.4697	31.5788	.241141
2	9.2921	5954.46	3491.26	78.8031	50.1411	31.8252	.238062
3	13.9382	5954.46	3503.39	79.1729	49.8458	32.0467	.235274
4	18.5842	5954.46	3506.43	79.2653	49.7715	32.1024	.234569
5	23.2303	5958.86	3521.74	79.767	49.5338	32.3833	.231608
6	27.8763	5963.27	3540.28	80.3633	49.215	32.7252	.22785
7	32.5224	5967.68	3552.75	80.7757	49.0444	32.9562	.225502
8	41.8145	5967.68	3573.21	81.379	48.537	33.3367	.22056
9	51.1066	5976.52	3590.7	81.9767	48.3765	33.6639	.217574
9	41.8145	5967.68	3576.37	81.4717	48.4582	33.3959	.219787
7	32.5224	5967.68	3560.59	81.0079	48.8503	33.1018	.223619
5	23.2303	5950.07	3495.78	76.0999	52.057	30.2859	.256357
3	13.9382	5945.69	3387.2	75.4752	52.3603	29.9563	.259757
1	4.64606	5915.18	3394.32	75.4785	51.2472	30.0824	.254528
.5	2.32303	5906.52	3402.91	75.6828	50.7766	30.2349	.251582



Table E:1.9a Specimen # 9, dry, from borehole E25, H9 area.

DATE :20 SEPTEMBER, 1982

LENGTH OF SPECIMEN : .082855 METER.

DIAMETER OF SPECIMEN : 5.1638 CENTIMETER

NUMBER OF LOADS : 16

DENSITY OF SPECIMEN : 2606 KG/M<sup>3</sup>

LOAD (TONS)	PRESSURE (MPA)	P-WAVE VEL (M/S)	S-WAVE VEL (M/S)	YOUNGS M (GPA)	BULK M (GPA)	SHEAR M (GPA)	PO. RA
.5	2.34133	5478.21	3486.59	72.1062	37.353	30.5884	.178268
1	4.68265	5476.21	3433.69	72.2792	37.1837	30.7254	.176067
2	9.36531	5549.56	3472.55	74.0523	38.3582	31.4247	.17825
3	14.048	5617.29	3506.35	75.6655	39.5103	32.0394	.18082
4	18.7306	5671.12	3528.75	76.8489	40.5462	32.4501	.18411
5	23.4133	5725.98	3554.48	78.1334	41.5425	32.8251	.186532
6	28.0959	5753.82	3563.66	78.6898	42.1484	33.0953	.188838
7	32.7786	5777.89	3572.88	79.204	42.6432	33.2667	.190439
9	42.1439	5814.39	3593.02	80.145	43.2441	33.6429	.191114
11	51.5092	5834.86	3607.1	80.7474	43.5134	33.907	.190718
9	42.1439	5822.56	3593.02	80.2391	43.4919	33.6429	.192513
7	32.7786	5794.06	3580.6	79.5892	42.9387	33.4107	.191074
5	23.4133	5749.83	3563.66	78.6433	42.0287	33.0953	.188136
3	14.048	5682.79	3521.25	76.7987	41.0752	32.3123	.188382
1	4.68265	5560.74	3446.55	73.558	39.3078	30.8559	.188111
.5	2.34133	5479.83	3411.07	71.7842	37.8251	30.3219	.183791

Table E:1.9b Specimen # 9, saturated.

DATE :30 SEPTEMBER, 1982

LENGTH OF SPECIMEN : .082855 METER.

DIAMETER OF SPECIMEN : 5.1638 CENTIMETER

NUMBER OF LOADS : 16

DENSITY OF SPECIMEN : 2611 KG/M<sup>3</sup>

LOAD (TONS)	PRESSURE (MPA)	P-WAVE VEL (M/S)	S-WAVE VEL (M/S)	YOUNGS M (GPA)	BULK M (GPA)	SHEAR M (GPA)	PO. RA
.5	2.34133	5905.56	3510.81	78.9567	48.1502	32.1825	.2267
1	4.68265	5913.99	3510.81	79.0341	48.4104	32.1825	.227903
2	9.36531	5913.99	3516.77	79.2102	48.2646	32.2919	.226472
3	14.048	5918.21	3548.39	80.1749	47.6171	32.8754	.219377
4	18.7306	5918.21	3616.54	82.0978	45.9173	34.1503	.202008
5	23.4133	5926.68	3622.87	82.3645	46.0197	34.2698	.201706
6	28.0959	5926.68	3627.63	82.4948	45.8996	34.3599	.200452
7	32.7786	5930.92	3629.22	82.5854	45.9908	34.39	.200718
9	42.1439	5935.17	3638.78	82.8939	45.8805	34.5715	.198877
11	51.5092	5947.95	3645.18	83.2122	46.1147	34.6933	.199256
9	42.1439	5939.43	3641.98	83.0289	45.9313	34.6323	.198721
7	32.7786	5935.17	3635.59	82.8069	45.9613	34.5108	.199723
5	23.4133	5926.68	3633.99	82.6683	45.7387	34.4806	.198766
3	14.048	5918.21	3611.81	81.9678	46.0363	34.061	.203249
1	4.68265	5872.08	3500.42	78.3421	47.374	31.9925	.224384
.5	2.34133	5863.76	3491.57	78.007	47.3347	31.8309	.225336

Table E:1.10a Specimen # 10, dry, from borehole E25, H9 area.

DATE :29 SEPTEMBER, 1982

LENGTH OF SPECIMEN : .080289 METER.

DIAMETER OF SPECIMEN : 5.174 CENTIMETER

NUMBER OF LOADS : 16

DENSITY OF SPECIMEN : 2608 KG/M<sup>3</sup>

LOAD (TONS)	PRESSURE (MPA)	P-WAVE VEL (M/S)	S-WAVE VEL (M/S)	YOUNGS M (GPA)	BULK M (GPA)	SHEAR M (GPA)	PO. RA
.5	2.3321	5341.98	3386.29	69.5735	34.521	29.883	.164101
1	4.66421	5392.14	3397.76	70.4438	35.6558	30.0856	.170723
2	9.32842	5503.02	3437.03	72.6656	37.8712	30.7851	.180207
3	13.9926	5587.27	3469.71	74.4262	39.5219	31.3733	.186139
4	18.6568	5646.2	3489.31	75.5812	40.7732	31.7288	.191051
5	23.321	5698.3	3509.13	76.6664	41.8312	32.0903	.194541
6	27.9853	5734.93	3524.54	77.4697	42.5462	32.3727	.196527
7	32.6495	5755.48	3541.64	78.1425	42.7418	32.6876	.195292
9	41.9779	5805.42	3555.78	79.0649	43.8982	32.9487	.199817
11	51.3063	5830.72	3569.99	79.7215	44.313	33.213	.200157
9	41.9779	5809.62	3558.91	79.1948	43.9474	33.0072	.199661
7	32.6495	5772.04	3538.52	78.2431	43.3158	32.63	.198943
5	23.321	5722.67	3510.67	76.9736	42.5191	32.1184	.198278
3	13.9926	5622.48	3468.21	74.7856	40.5867	31.3462	.192898
1	4.66421	5439.63	3422.38	71.5714	36.4129	30.5232	.172408
.5	2.3321	5388.52	3387.72	70.1769	35.7907	29.9022	.173207

Table E:1.10b Specimen # 10, saturated.

DATE :30 SEPTEMBER, 1982

LENGTH OF SPECIMEN : .080289 METER.

DIAMETER OF SPECIMEN : 5.174 CENTIMETER

NUMBER OF LOADS : 16

DENSITY OF SPECIMEN : 2611 KG/M<sup>3</sup>

LOAD (TONS)	PRESSURE (MPA)	P-WAVE VEL (M/S)	S-WAVE VEL (M/S)	YOUNGS M (GPA)	BULK M (GPA)	SHEAR M (GPA)	PO. RA
.5	2.3321	5942.93	3527.64	79.7991	48.8939	32.4919	.227986
1	4.66421	5942.93	3533.85	79.9836	48.7413	32.6064	.226503
2	9.32842	5942.93	3543.2	80.2602	48.5107	32.7793	.224253
3	13.9926	5942.93	3557.33	80.6746	48.1615	33.0412	.220819
4	18.6568	5942.93	3571.57	81.0883	47.808	33.3063	.217313
5	23.321	5942.93	3579.54	81.3178	47.6098	33.455	.215333
6	27.9853	5951.74	3589.14	81.6824	47.6439	33.6346	.214261
7	32.6495	5951.74	3595.57	81.8665	47.4831	33.7553	.212647
9	41.9779	5960.58	3605.25	82.2338	47.5151	33.9374	.211552
11	51.3063	5960.58	3603.64	82.1877	47.5557	33.9069	.21196
9	41.9779	5956.16	3602.02	82.0959	47.4586	33.8765	.211693
7	32.6495	5951.74	3592.35	81.7745	47.5636	33.6949	.213456
5	23.321	5951.74	3577.94	81.36	47.9233	33.4251	.217048
3	13.9926	5942.93	3544.77	80.3063	48.4721	32.8082	.223875
1	4.66421	5916.65	3495.39	78.5988	48.8688	31.9005	.231939
.5	2.3321	5894.93	3466.71	77.548	48.894	31.3792	.235659

Table E:1.11a Specimen # 11, dry, from borehole E25, H9 area.

DATE :20 SEPTEMBER, 1982

LENGTH OF SPECIMEN : .080213 METER.

DIAMETER OF SPECIMEN : 5.1791 CENTIMETER

NUMBER OF LOADS : 16

DENSITY OF SPECIMEN : 2606 KG/M<sup>3</sup>

LOAD (TONS)	PRESSURE (MPA)	P-WAVE VEL (M/S)	S-WAVE VEL (M/S)	YOUNGS M (MPA)	BULK M (MPA)	SHEAR M (MPA)	PO. RA
.5	8.32751	5434.49	3403.18	71.0737	36.7823	30.1818	.177427
1	4.65503	5501.58	3423.52	72.329	38.152	30.5436	.184031
2	9.31005	5597.56	3467.92	74.4996	39.8649	31.341	.188533
3	13.9651	5676.79	3504.28	76.3027	41.3118	32.0017	.192168
4	18.6201	5729.5	3535.17	77.684	42.1232	32.5683	.192632
5	23.2751	5774.88	3566.61	79.0081	42.7078	33.1501	.191672
6	27.9302	5804.12	3584.14	79.7966	43.1548	33.4768	.19182
7	32.5852	5833.67	3611.57	80.8494	43.3651	33.9912	.189268
9	41.8952	5863.58	3622.99	81.4951	43.988	34.2065	.191222
11	51.2053	5889.35	3637.78	82.1839	44.406	34.4863	.191544
9	41.8952	5872.11	3618.00	81.4655	44.3739	34.114	.194019
7	32.5852	5842.17	3598.61	80.6098	43.9484	33.7477	.194301
5	23.2751	5804.12	3563.44	79.2546	43.6689	33.0912	.197517
3	13.9651	5725.41	3510.42	76.9968	42.6072	32.1138	.198811
1	4.65503	5558.77	3441.14	73.4032	39.38	30.8588	.189338
.5	8.32751	5509.13	3419.14	72.3098	38.4729	30.4656	.18675

Table E:1.11b Specimen # 11, saturated.

DATE :30 SEPTEMBER, 1982

LENGTH OF SPECIMEN : .080213 METER.

DIAMETER OF SPECIMEN : 5.1791 CENTIMETER

NUMBER OF LOADS : 16

DENSITY OF SPECIMEN : 2611 KG/M<sup>3</sup>

LOAD (TONS)	PRESSURE (MPA)	P-WAVE VEL (M/S)	S-WAVE VEL (M/S)	YOUNGS M (MPA)	BULK M (MPA)	SHEAR M (MPA)	PO. RA
.5	2.32751	5986.05	3576.15	81.6433	49.0371	33.3916	.222512
1	4.65503	5986.05	3577.74	81.6904	48.9974	33.4214	.222126
2	9.31005	5986.05	3582.54	81.8317	48.8779	33.5111	.220965
3	13.9651	5986.05	3609.95	82.6303	48.1915	34.0258	.21423
4	18.6201	5990.52	3627.91	83.1918	47.8788	34.3652	.210408
5	23.2751	5994.99	3624.63	83.1448	48.1017	34.3031	.211913
6	27.9302	5994.99	3629.55	83.2857	47.9774	34.3963	.210678
7	32.5852	5994.99	3627.91	83.2387	48.0189	34.3652	.211091
9	41.8952	6003.97	3627.91	83.3322	48.3001	34.3652	.21245
11	51.2053	6008.47	3629.55	83.4261	48.3997	34.3963	.212718
9	41.8952	5999.48	3626.27	83.2384	48.2008	34.3341	.212182
7	32.5852	5994.99	3624.63	83.1448	48.1017	34.3031	.211913
5	23.2751	5994.99	3624.63	83.1448	48.1017	34.3031	.211913
3	13.9651	5994.99	3619.72	83.0038	48.2254	34.2103	.21314
1	4.65503	5981.58	3571.37	81.4593	49.0165	33.3025	.223021
.5	2.32751	5941.7	3541.41	80.1958	48.5168	32.7461	.224509

## Appendix E:2 - Velocity plots for laboratory test.

In this appendix the  $V_p$  and  $V_s$  are plotted as function of the uniaxial stress  $\sigma_{ua}$ . The dry velocities are shown in figures a and b and the saturated in figures c and d. The saturated velocities have many times a considerable hysteresis on the unloading part of the curve. This is interpreted to be an effect of the saturation which is assumed to be partial during the unloading because the pore fluid were forced out of the fractures during the loading of the specimen.

In Table 7.2 the location of the specimen are shown.

**Figure captions for Appendix E:2**

Fig. E:2.1a P wave velocity as function of uniaxial stress for the dry specimen # 1

Fig. E:2.1b S wave velocity as function of uniaxial stress for the dry specimen # 1

Fig. E:2.1c P wave velocity as function of uniaxial stress for the saturated specimen # 1

Fig. E:2.1d S wave velocity as function of uniaxial stress for the saturated specimen # 1

Fig. E:2.2a P wave velocity as function of uniaxial stress for the dry specimen # 2

Fig. E:2.2b S wave velocity as function of uniaxial stress for the dry specimen # 2

Fig. E:2.2c P wave velocity as function of uniaxial stress for the saturated specimen # 2

Fig. E:2.2d S wave velocity as function of uniaxial stress for the saturated specimen # 2

Fig. E:2.3a P wave velocity as function of uniaxial stress for the dry specimen # 3

Fig. E:2.3b S wave velocity as function of uniaxial stress for the dry specimen # 3

Fig. E:2.3c P wave velocity as function of uniaxial stress for the saturated specimen # 3

Fig. E:2.3d S wave velocity as function of uniaxial stress for the saturated specimen # 3

Fig. E:2.4a P wave velocity as function of uniaxial stress for the dry specimen # 4

Fig. E:2.4b S wave velocity as function of uniaxial stress for the dry specimen # 4

Fig. E:2.4c P wave velocity as function of uniaxial stress for the saturated specimen # 4

Fig. E:2.4d S wave velocity as function of uniaxial stress for the saturated specimen # 4

Fig. E:2.5a P wave velocity as function of uniaxial stress for the dry specimen # 5

Fig. E:2.5b S wave velocity as function of uniaxial stress for the dry specimen # 5

Fig. E:2.5c P wave velocity as function of uniaxial stress for the saturated specimen # 5

Fig. E:2.5d S wave velocity as function of uniaxial stress for the saturated specimen # 5

Fig. E:2.6a P wave velocity as function of uniaxial stress for the dry specimen # 6

Fig. E:2.6b S wave velocity as function of uniaxial stress for the dry specimen # 6

Fig. E:2.6c P wave velocity as function of uniaxial stress for the saturated specimen # 6

Fig. E:2.6d S wave velocity as function of uniaxial stress for the saturated specimen # 6

Fig. E:2.7a P wave velocity as function of uniaxial stress for the dry specimen # 7

Fig. E:2.7b S wave velocity as function of uniaxial stress for the dry specimen # 7

Fig. E:2.7c P wave velocity as function of uniaxial stress for the saturated specimen # 7

Fig. E:2.7d S wave velocity as function of uniaxial stress for the saturated specimen # 7

Fig. E:2.8a P wave velocity as function of uniaxial stress for the dry specimen # 8

Fig. E:2.8b S wave velocity as function of uniaxial stress for the dry specimen # 8

Fig. E:2.8c P wave velocity as function of uniaxial stress for the saturated specimen # 8

Fig. E:2.8d S wave velocity as function of uniaxial stress for the saturated specimen # 8

Fig. E:2.9a P wave velocity as function of uniaxial stress for the dry specimen # 9

Fig. E:2.9b S wave velocity as function of uniaxial stress for the dry specimen # 9



Fig. E:2.9c P wave velocity as function of uniaxial stress for the saturated specimen # 9

Fig. E:2.9d S wave velocity as function of uniaxial stress for the saturated specimen # 9

Fig. E:2.10a P wave velocity as function of uniaxial stress for the dry specimen # 10

Fig. E:2.10b S wave velocity as function of uniaxial stress for the dry specimen # 10

Fig. E:2.10c P wave velocity as function of uniaxial stress for the saturated specimen # 10

Fig. E:2.10d S wave velocity as function of uniaxial stress for the saturated specimen # 10

Fig. E:2.11a P wave velocity as function of uniaxial stress for the dry specimen # 11

Fig. E:2.11b S wave velocity as function of uniaxial stress for the dry specimen # 11

Fig. E:2.11c P wave velocity as function of uniaxial stress for the saturated specimen # 11

Fig. E:2.11d S wave velocity as function of uniaxial stress for the saturated specimen # 11

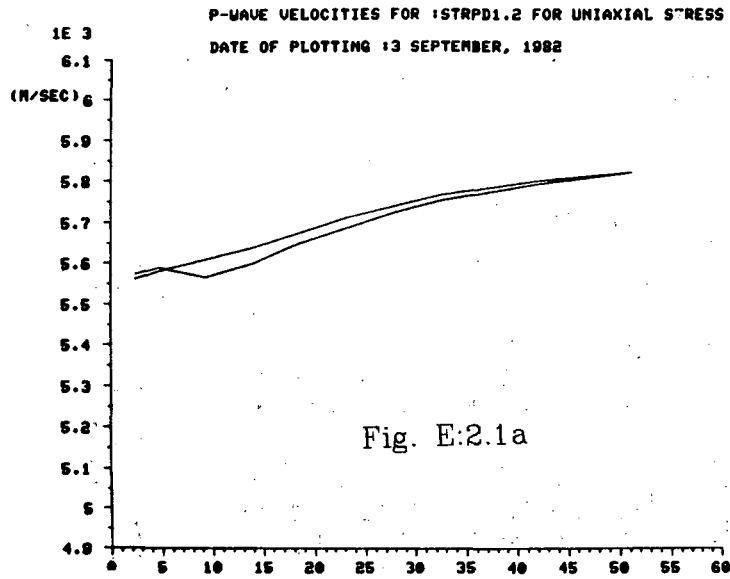


Fig. E:2.1a

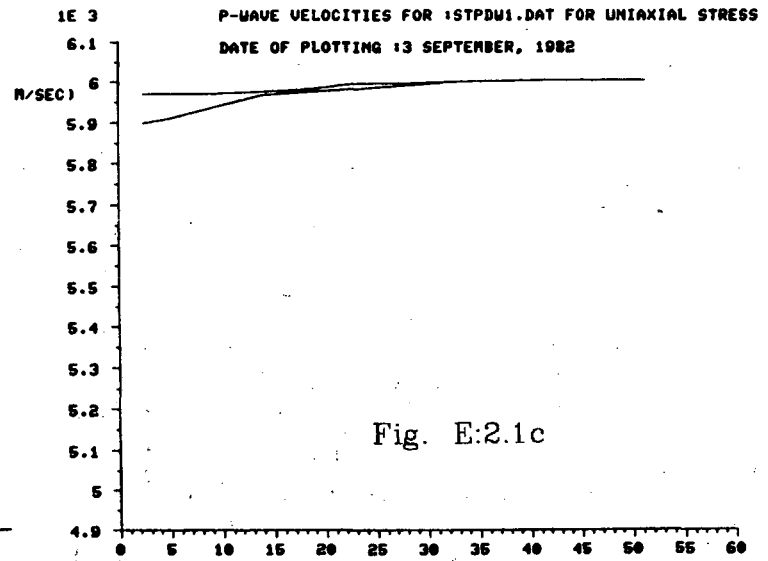


Fig. E:2.1c

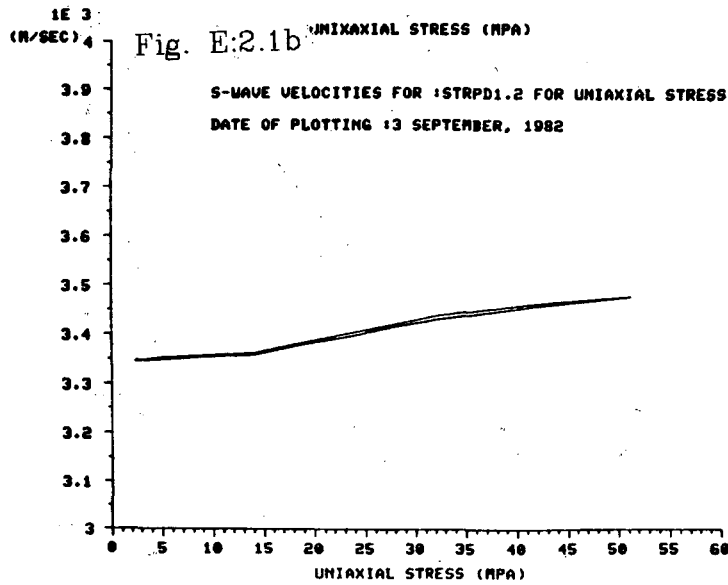


Fig. E:2.1b

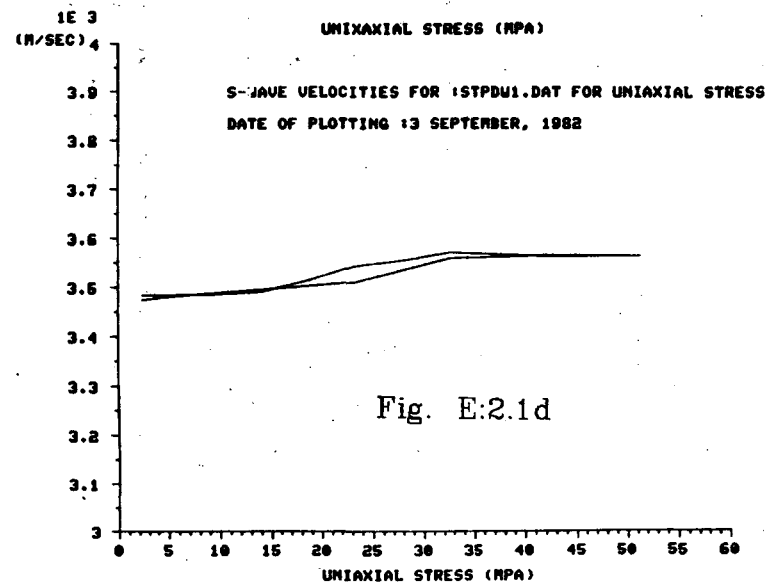
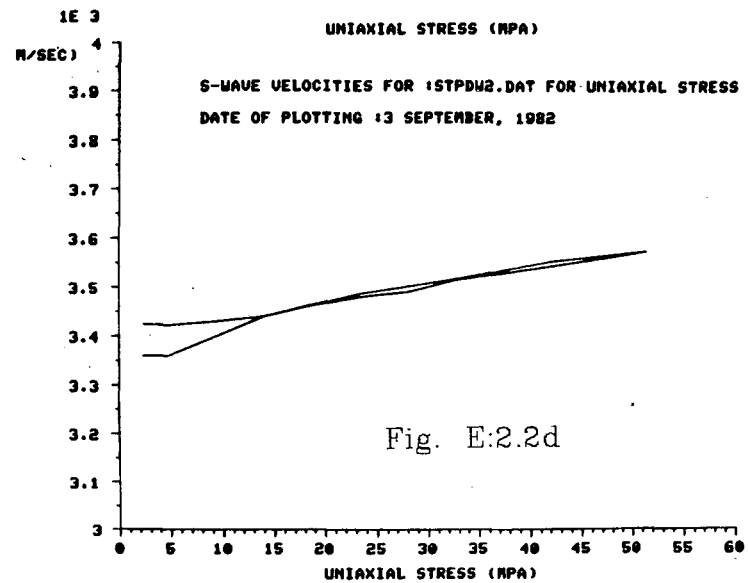
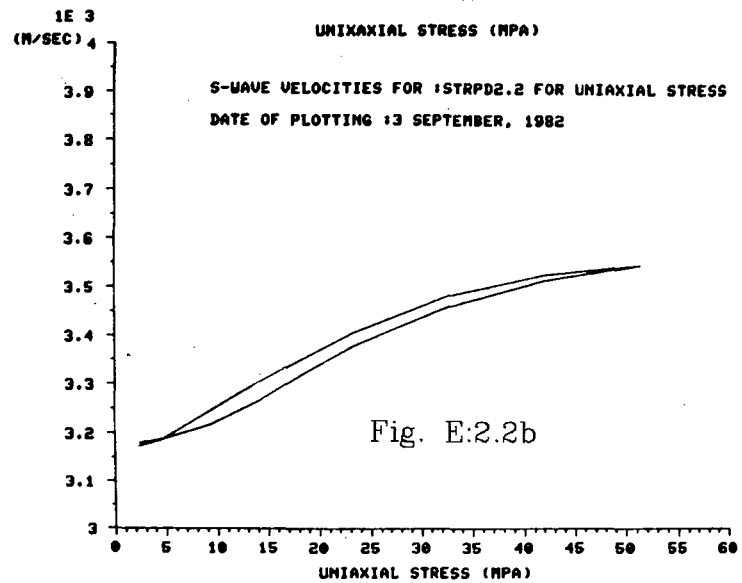
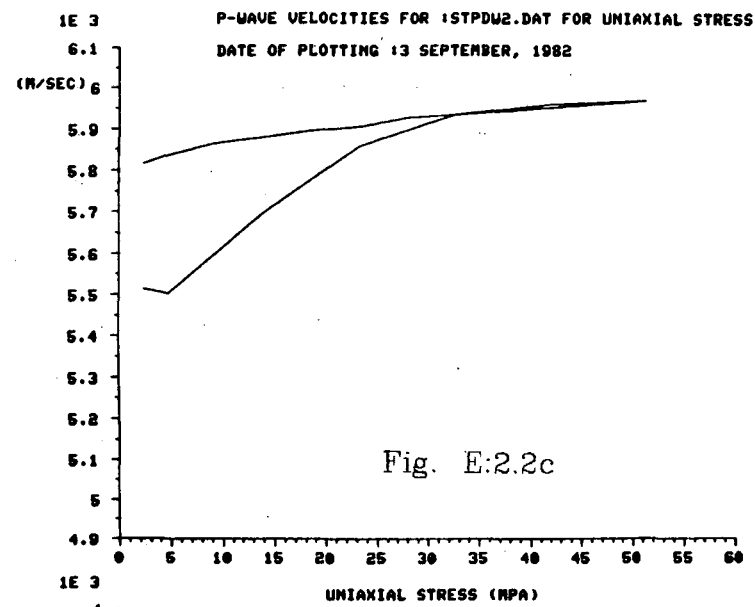
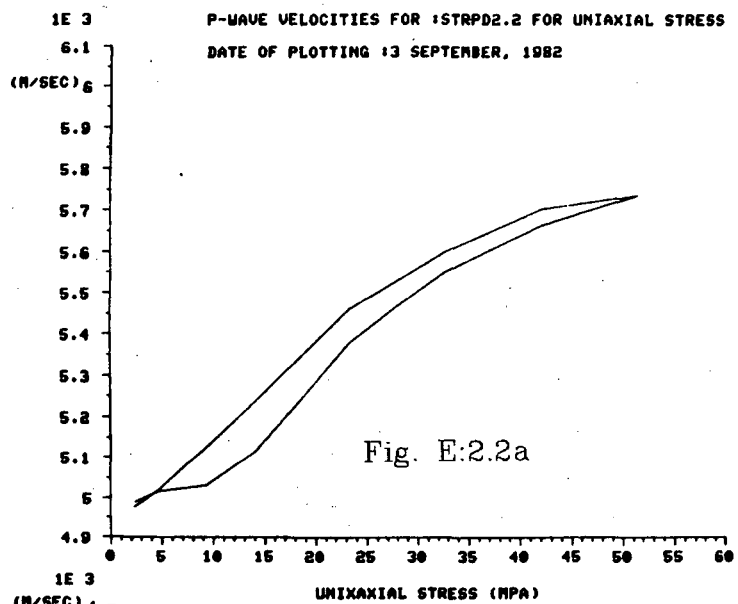
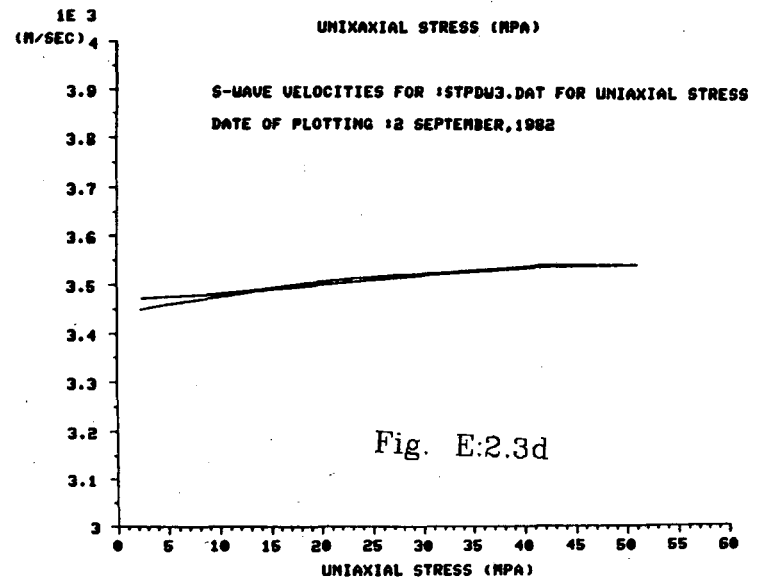
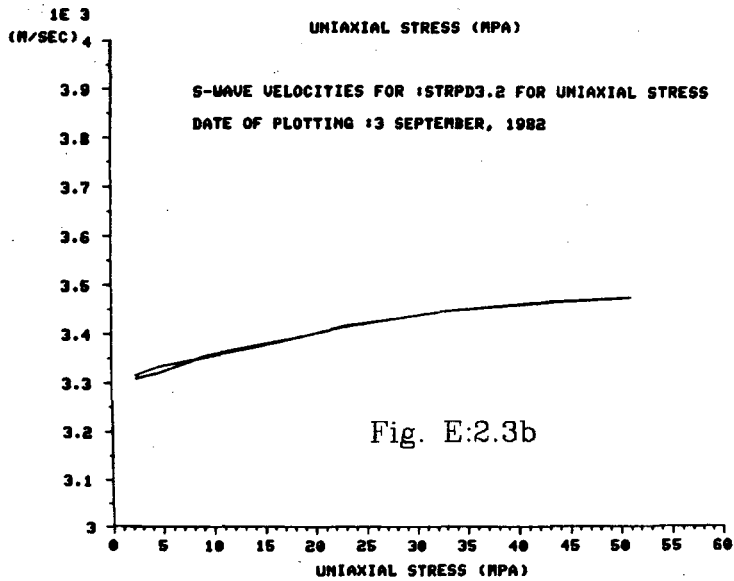
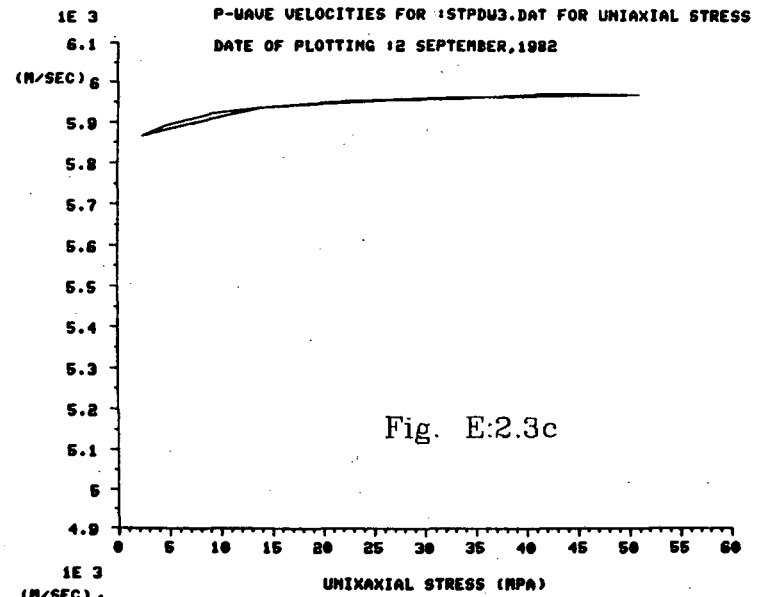
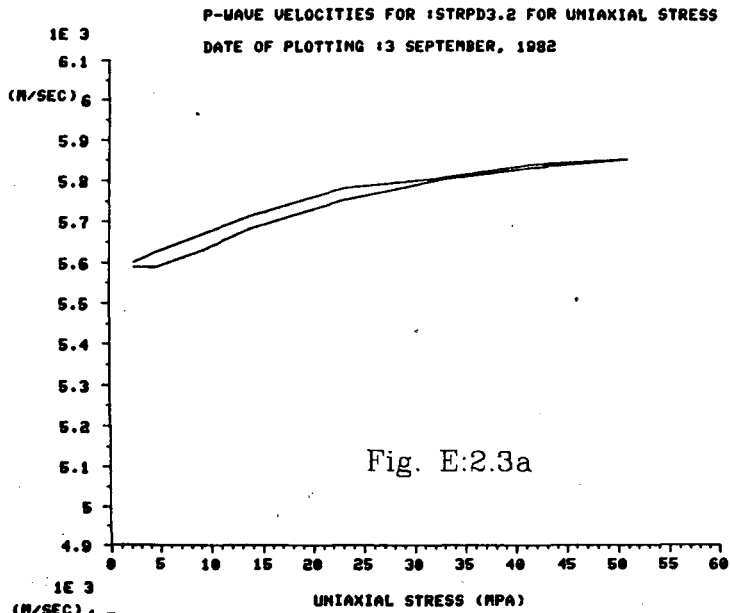
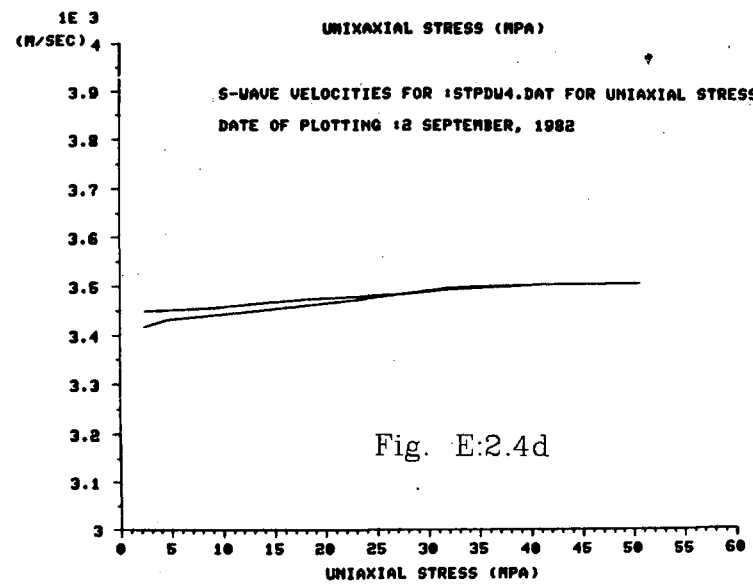
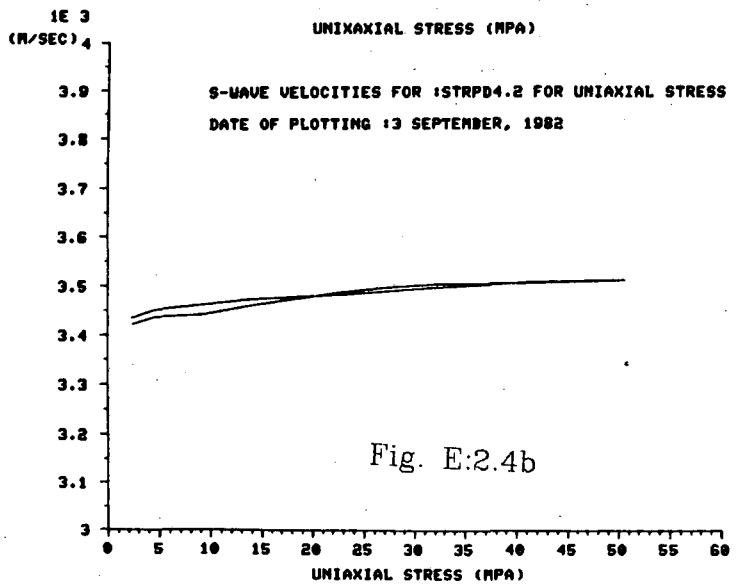
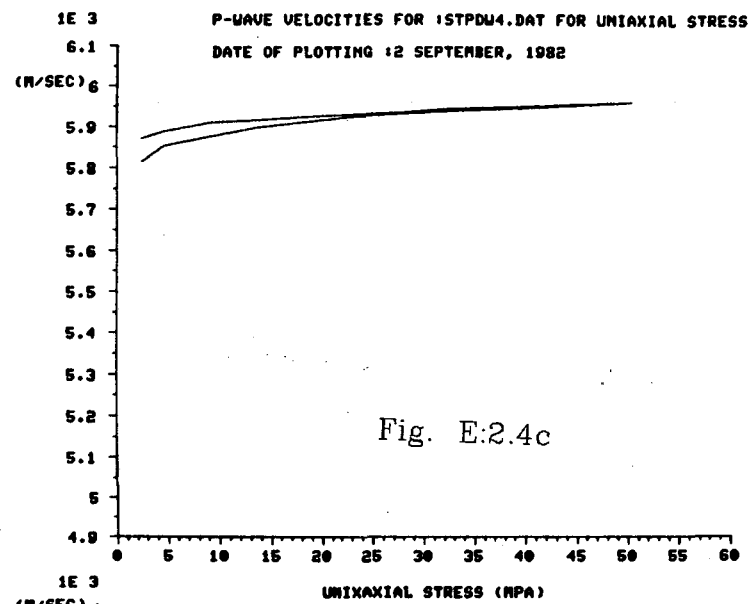
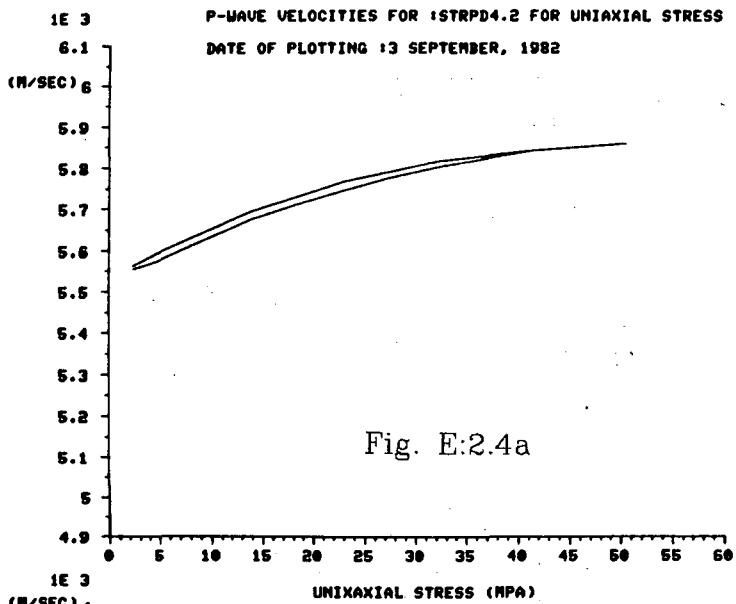
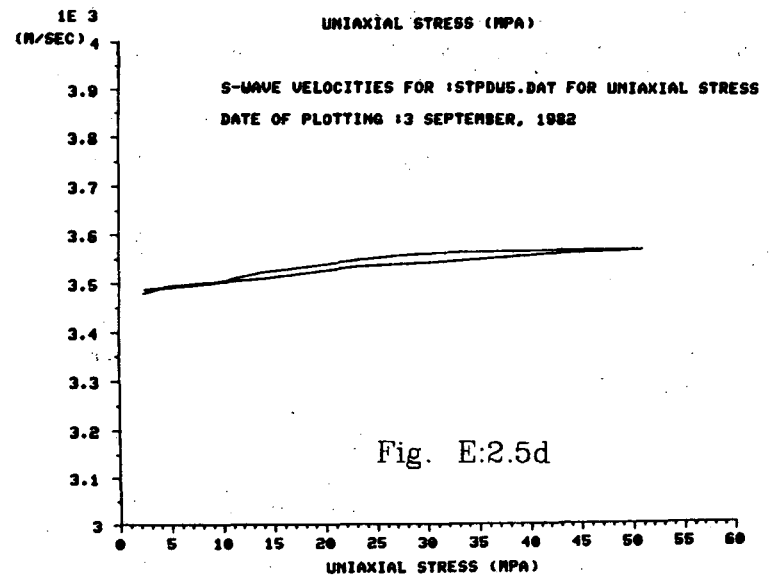
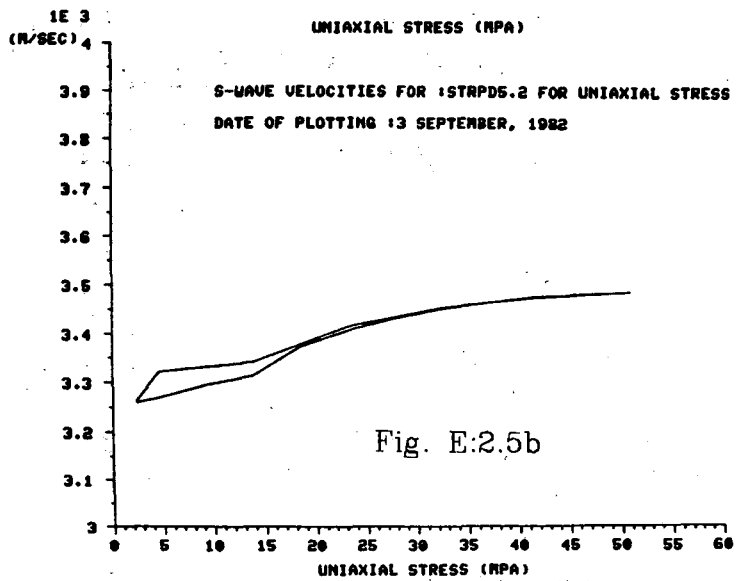
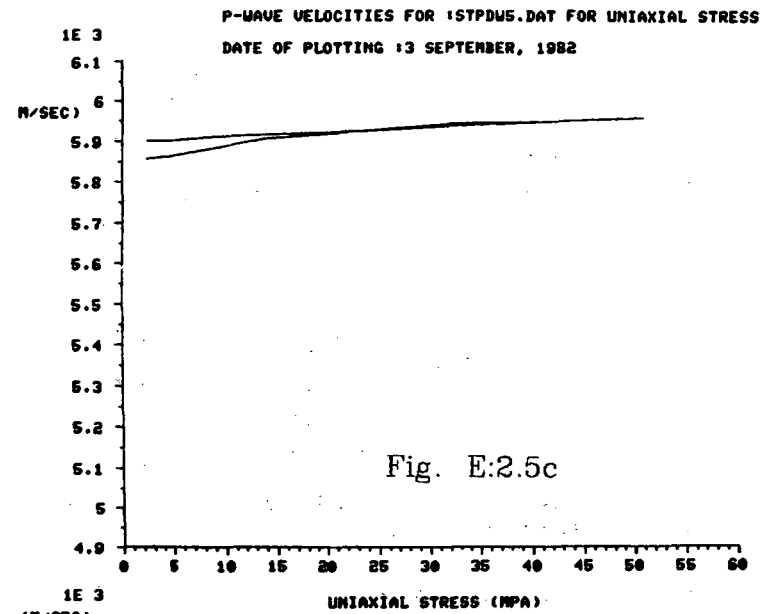
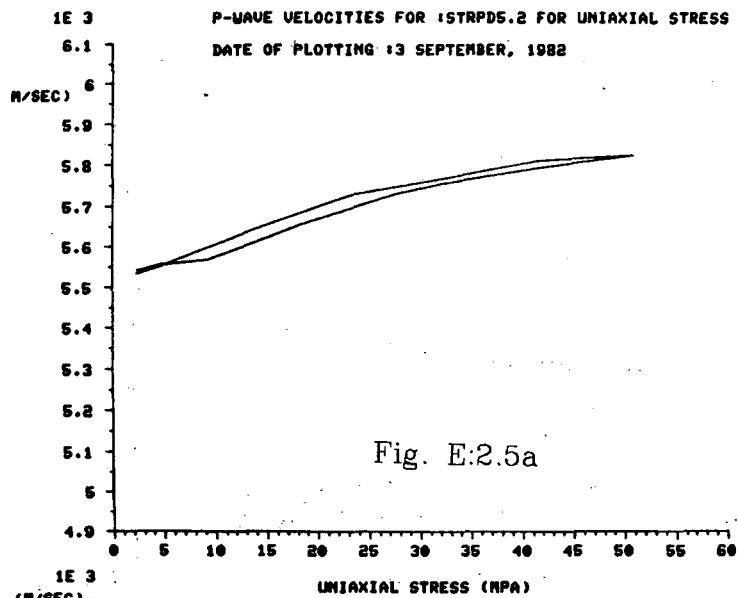


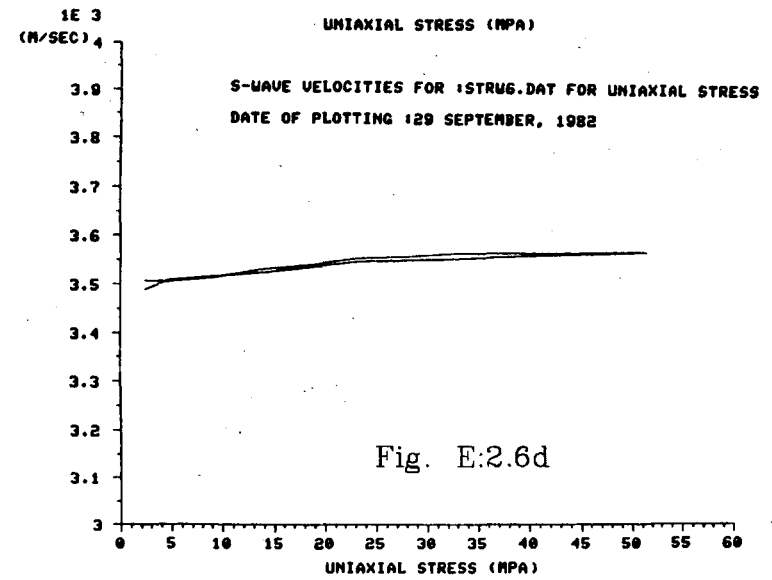
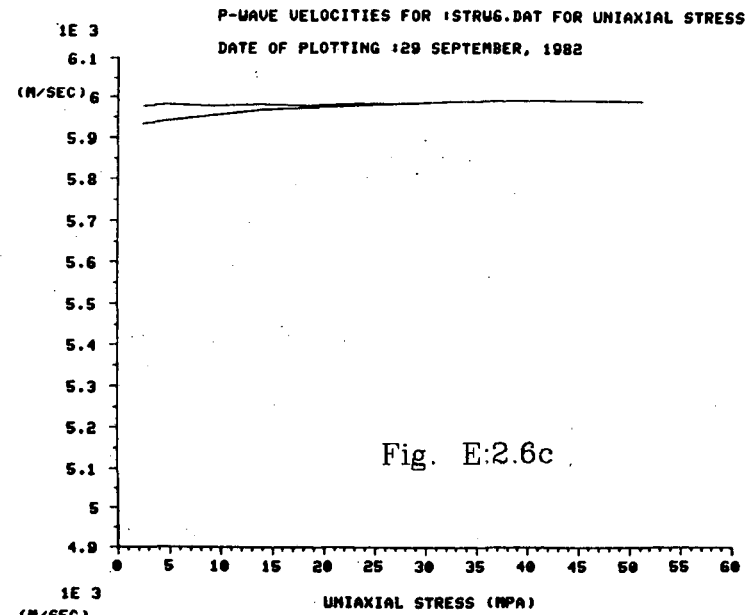
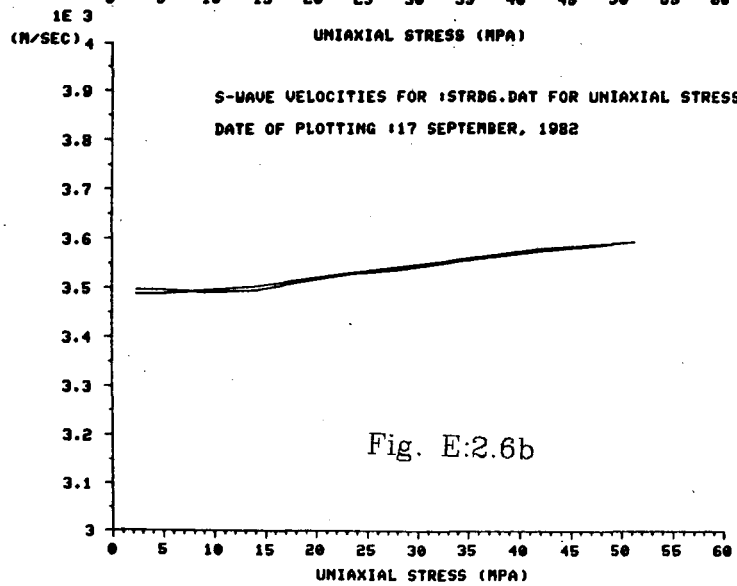
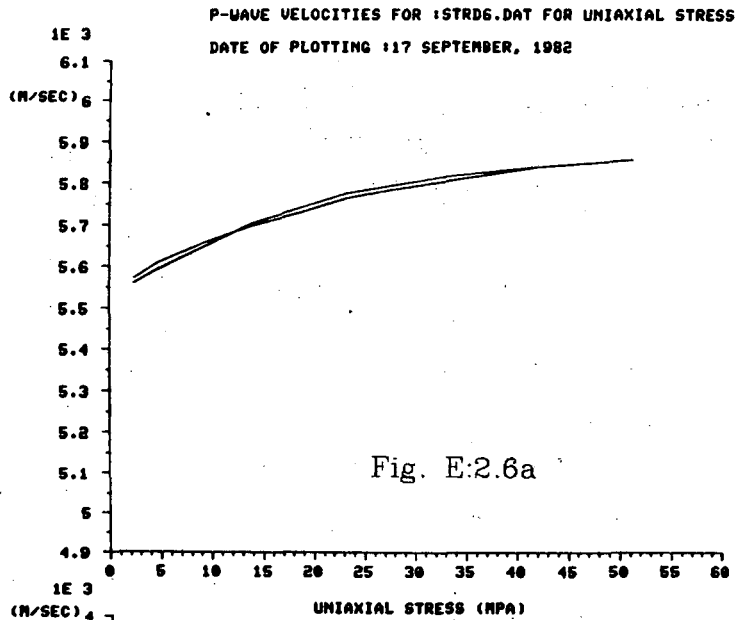
Fig. E:2.1d



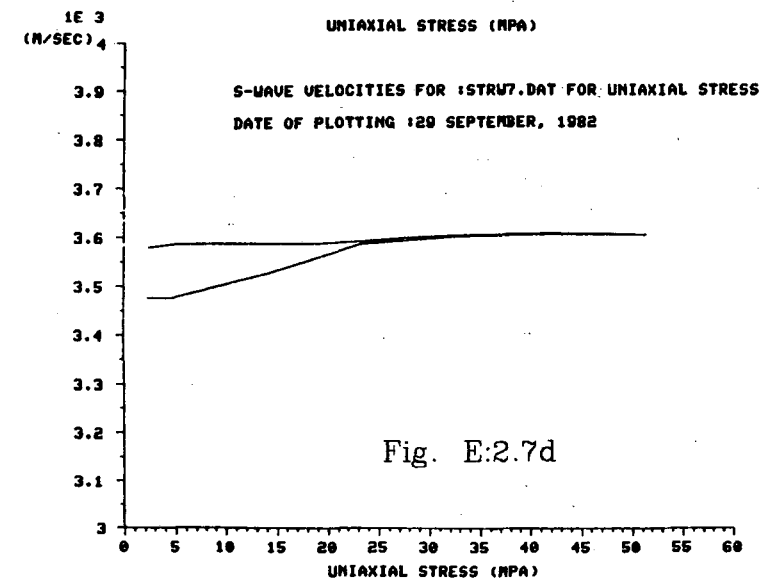
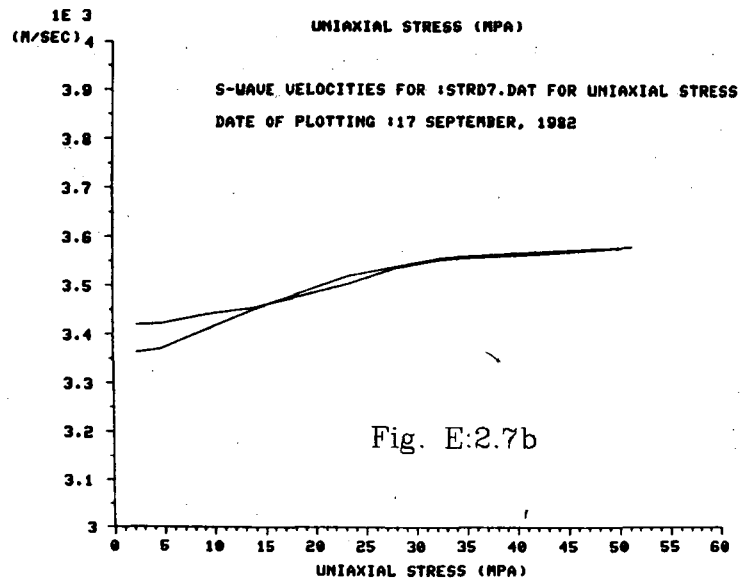
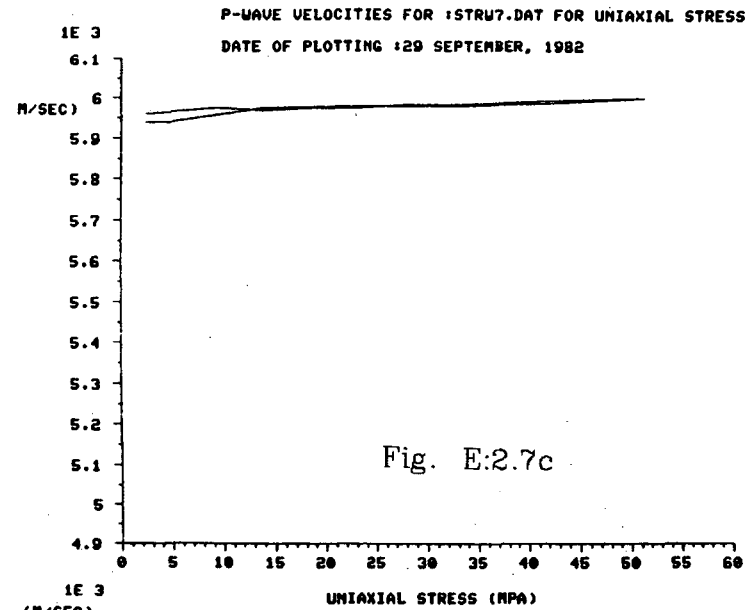
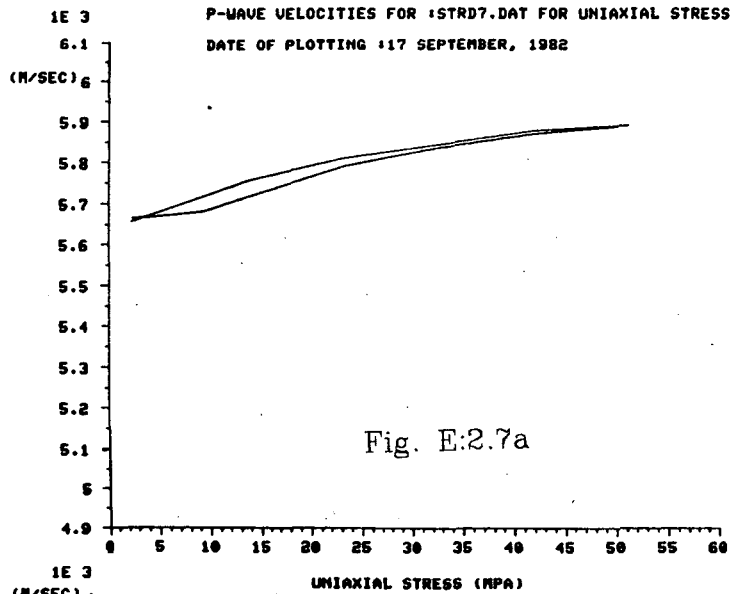


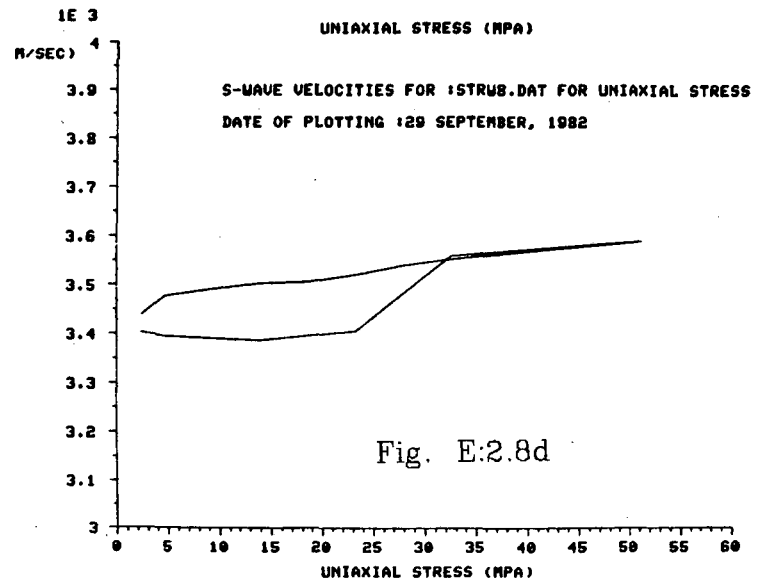
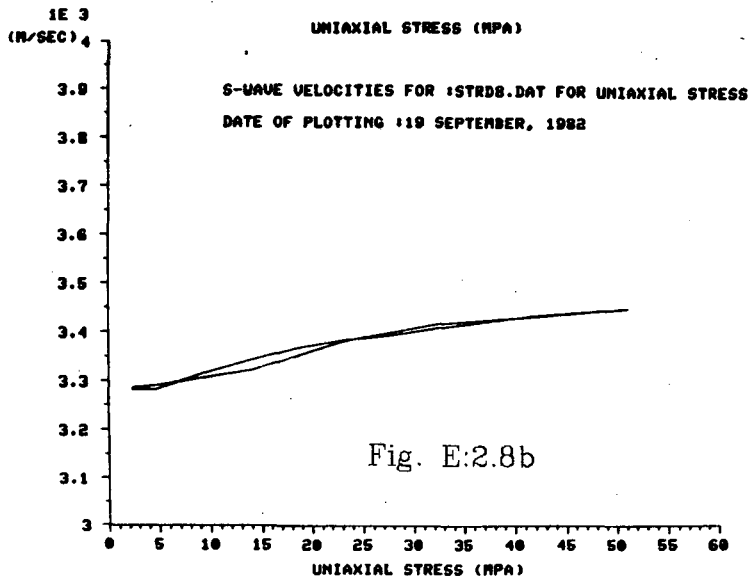
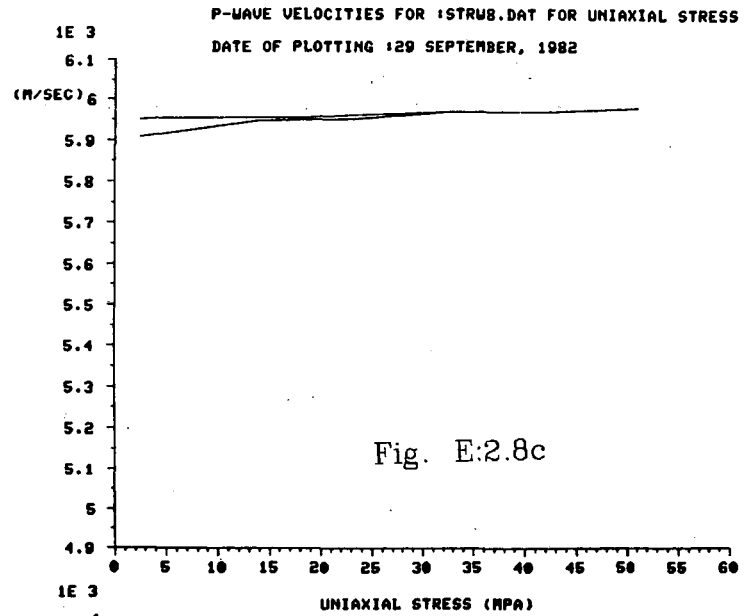
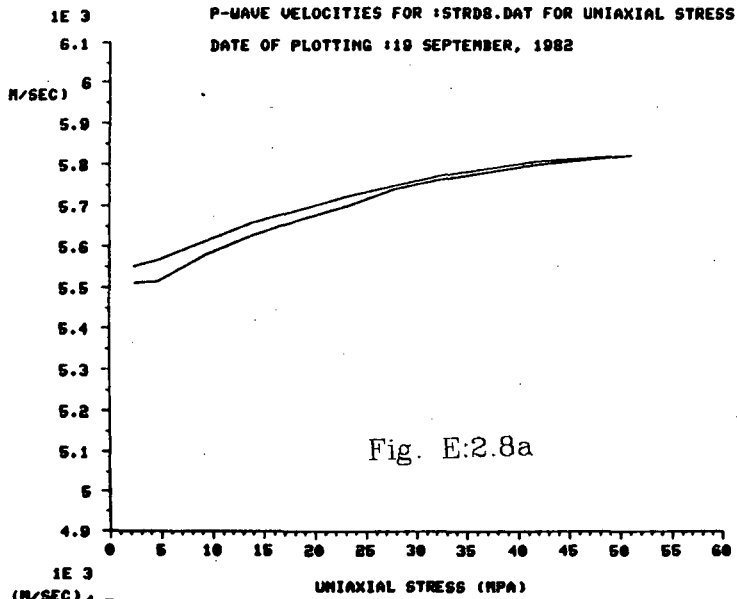


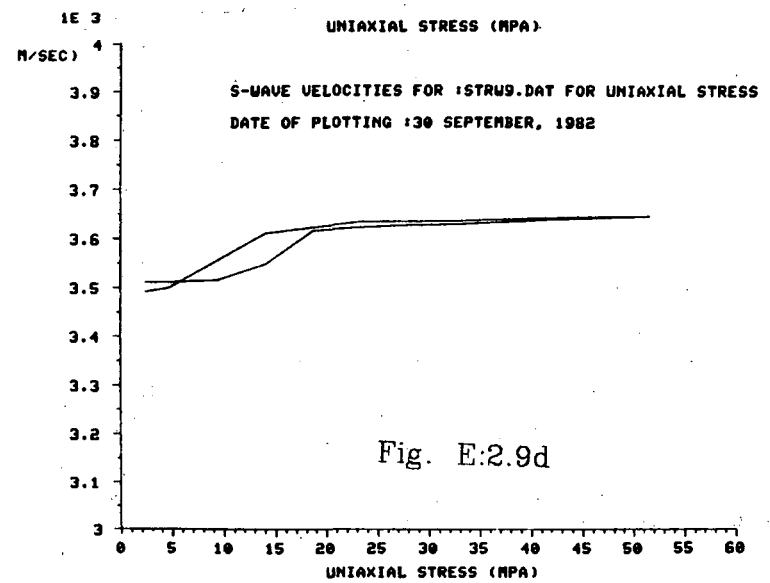
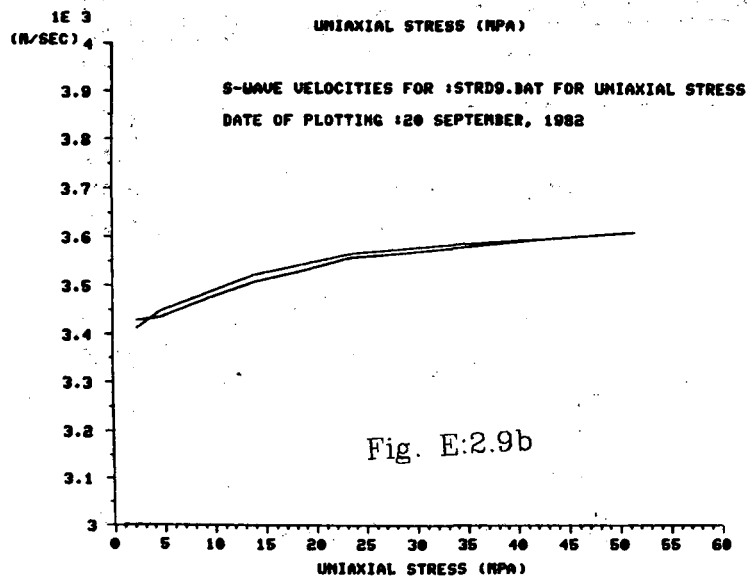
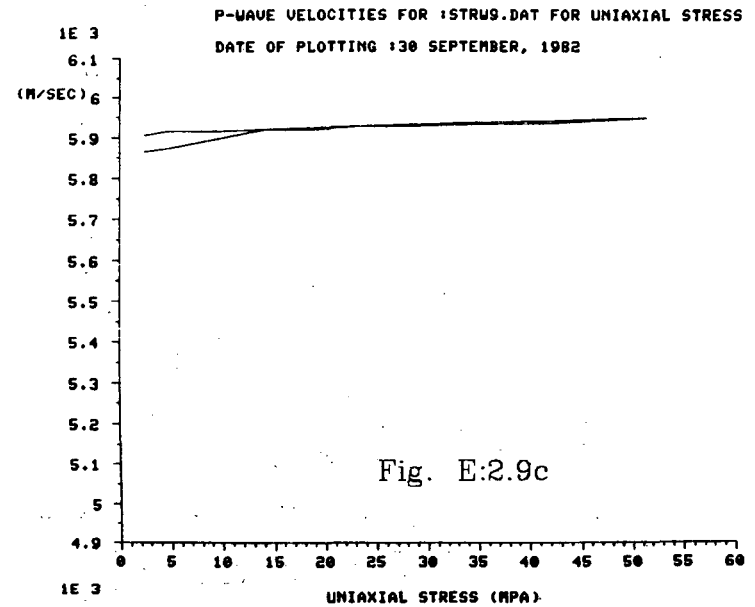
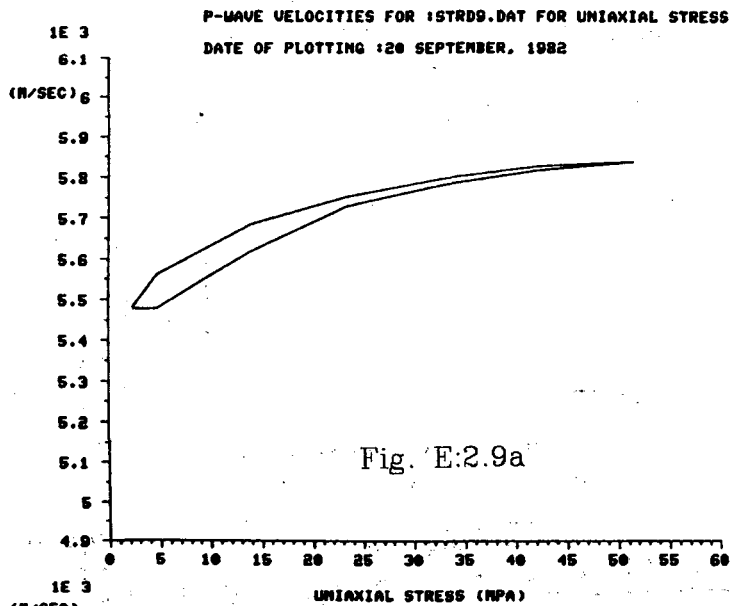


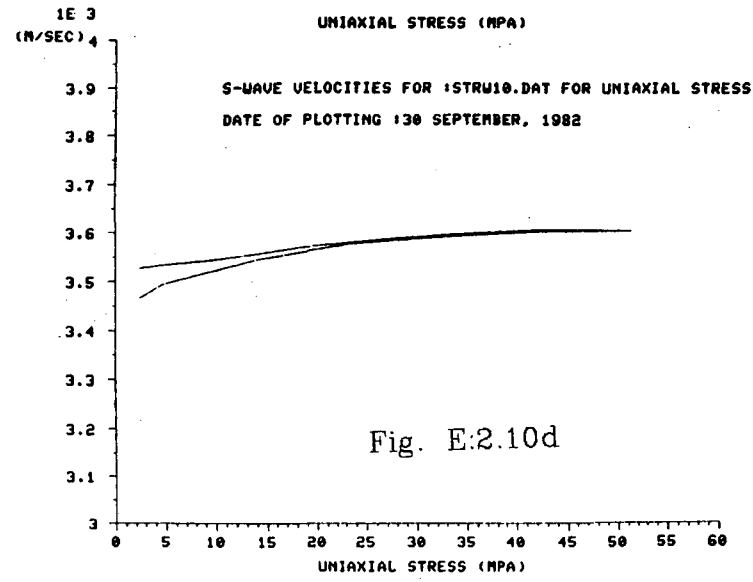
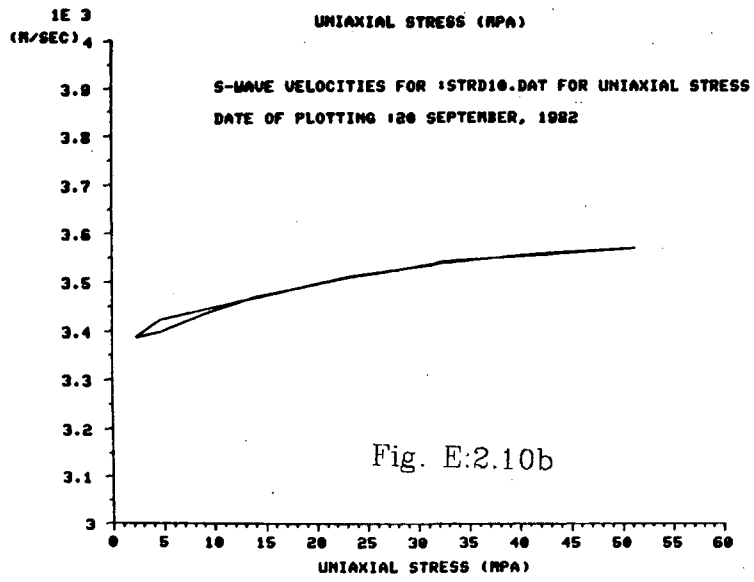
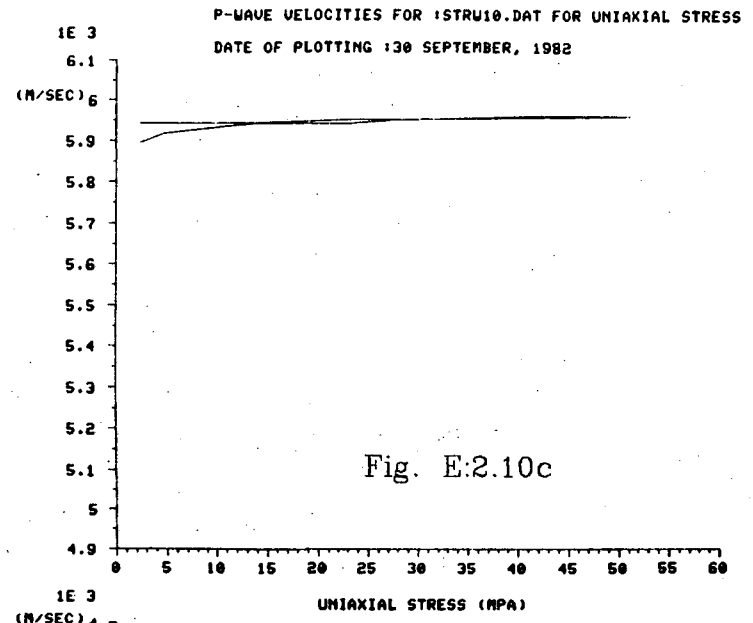
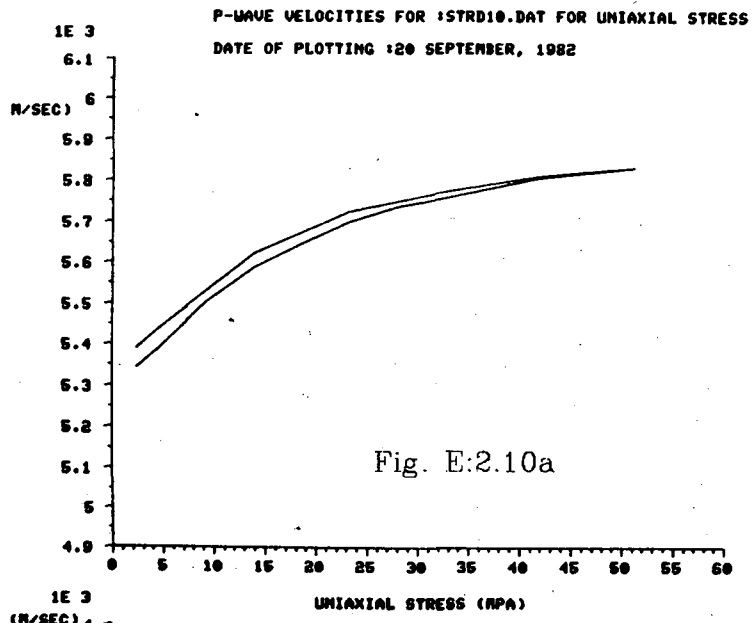


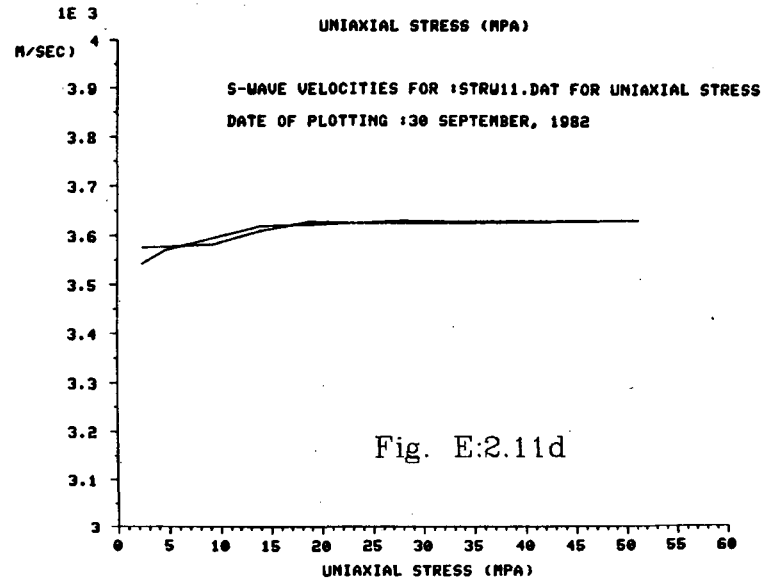
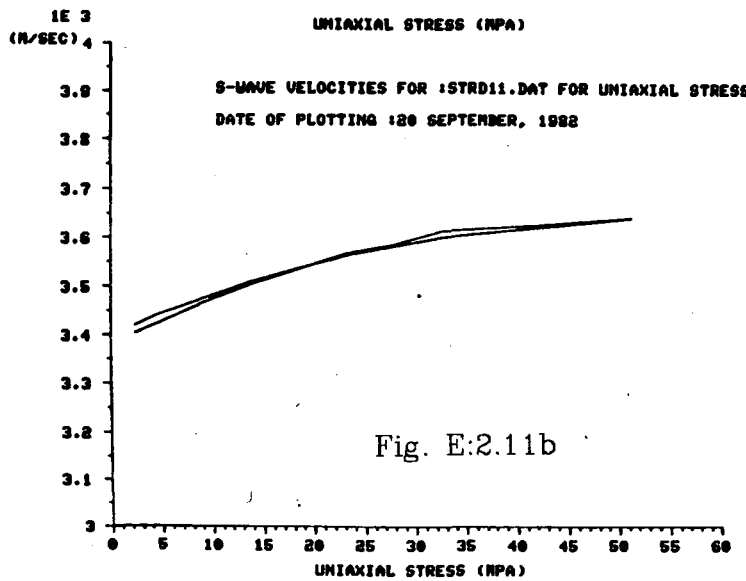
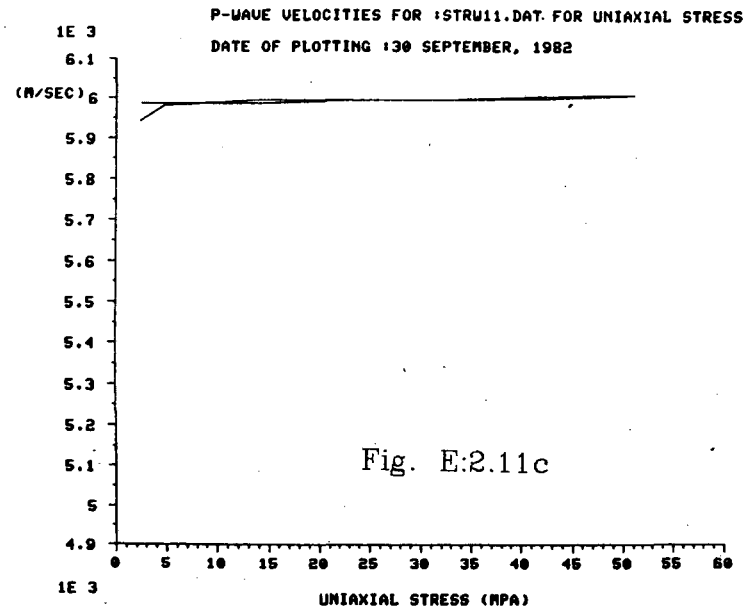
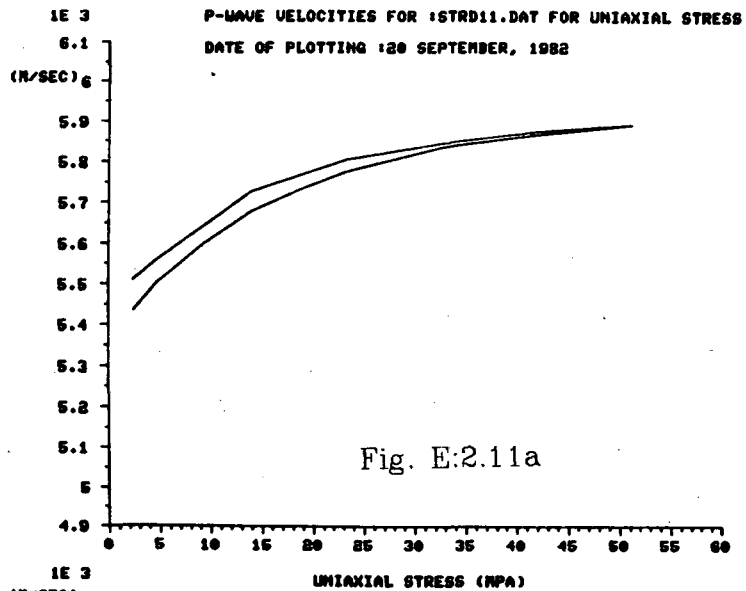












### Appendix E:3 - P and S waveforms from laboratory test

In this appendix the  $V_p$  and  $V_s$  are plotted as function of the uniaxial stress  $\sigma_{uu}$ . The dry velocities are shown in figures a and b and the saturated in figures c and d. The saturated velocities have many times a considerable hysteresis on the unloading part of the curve. This is interpreted to be an effect of the saturation which is assumed to be partial during the unloading because the pore fluid were forced out of the fractures during the loading of the specimen.

In Table 7.2 the location of the specimen are shown.

**Figure captions for Appendix E:3**

Fig. E:3.1a P wave velocity as function of uniaxial stress for the dry specimen # 1

Fig. E:3.1b P waveform as function of uniaxial stress for the saturated specimen # 1

Fig. E:3.1c S waveform as function of uniaxial stress for the dry specimen # 1

Fig. E:3.1d S waveform as function of uniaxial stress for the saturated specimen # 1

Fig. E:3.2a P wave velocity as function of uniaxial stress for the dry specimen # 2

Fig. E:3.2b P waveform as function of uniaxial stress for the saturated specimen # 2

Fig. E:3.2c S waveform as function of uniaxial stress for the dry specimen # 2

Fig. E:3.2d S waveform as function of uniaxial stress for the saturated specimen # 2

Fig. E:3.3a P wave velocity as function of uniaxial stress for the dry specimen # 3

Fig. E:3.3b P waveform as function of uniaxial stress for the saturated specimen # 3

Fig. E:3.3c S waveform as function of uniaxial stress for the dry specimen # 3

Fig. E:3.3d S waveform as function of uniaxial stress for the saturated specimen # 3

Fig. E:3.4a P wave velocity as function of uniaxial stress for the dry specimen # 4

Fig. E:3.4b P waveform as function of uniaxial stress for the saturated specimen # 4

Fig. E:3.4c S waveform as function of uniaxial stress for the dry specimen # 4

Fig. E:3.4d S waveform as function of uniaxial stress for the saturated specimen # 4



Fig. E:3.5a P wave velocity as function of uniaxial stress for the dry specimen # 5

Fig. E:3.5b P waveform as function of uniaxial stress for the saturated specimen # 5

Fig. E:3.5c S waveform as function of uniaxial stress for the dry specimen # 5

Fig. E:3.5d S waveform as function of uniaxial stress for the saturated specimen # 5

Fig. E:3.6a P wave velocity as function of uniaxial stress for the dry specimen # 6

Fig. E:3.6b P waveform as function of uniaxial stress for the saturated specimen # 6

Fig. E:3.6c S waveform as function of uniaxial stress for the dry specimen # 6

Fig. E:3.6d S waveform as function of uniaxial stress for the saturated specimen # 6

Fig. E:3.7a P wave velocity as function of uniaxial stress for the dry specimen # 7

Fig. E:3.7b P waveform as function of uniaxial stress for the saturated specimen # 7

Fig. E:3.7c S waveform as function of uniaxial stress for the dry specimen # 7

Fig. E:3.7d S waveform as function of uniaxial stress for the saturated specimen # 7

Fig. E:3.8a P wave velocity as function of uniaxial stress for the dry specimen # 8

Fig. E:3.8b P waveform as function of uniaxial stress for the saturated specimen # 8

Fig. E:3.8c S waveform as function of uniaxial stress for the dry specimen # 8

Fig. E:3.8d S waveform as function of uniaxial stress for the saturated specimen # 8

Fig. E:3.9a P wave velocity as function of uniaxial stress for the dry specimen # 9

Fig. E:3.9b P waveform as function of uniaxial stress for the saturated specimen # 9

Fig. E:3.9c S waveform as function of uniaxial stress for the dry specimen # 9

Fig. E:3.9d S waveform as function of uniaxial stress for the saturated specimen # 9

Fig. E:3.10a P wave velocity as function of uniaxial stress for the dry specimen # 10

Fig. E:3.10b P waveform as function of uniaxial stress for the saturated specimen # 10

Fig. E:3.10c S waveform as function of uniaxial stress for the dry specimen # 10

Fig. E:3.10d S waveform as function of uniaxial stress for the saturated specimen # 10

Fig. E:3.11a P wave velocity as function of uniaxial stress for the dry specimen # 11

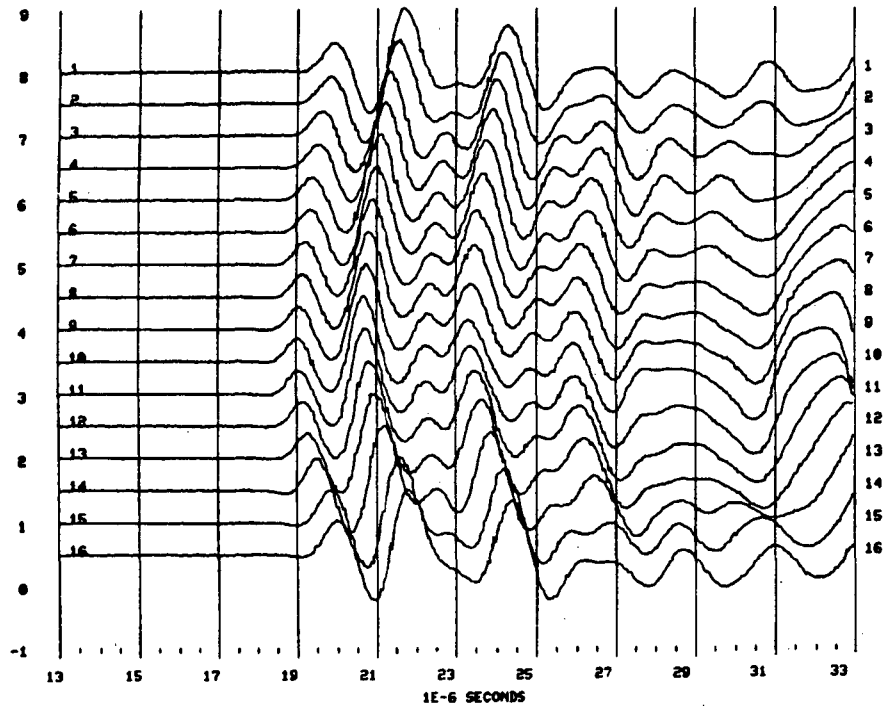
Fig. E:3.11b P waveform as function of uniaxial stress for the saturated specimen # 11

Fig. E:3.11c S waveform as function of uniaxial stress for the dry specimen # 11

Fig. E:3.11d S waveform as function of uniaxial stress for the saturated specimen # 11

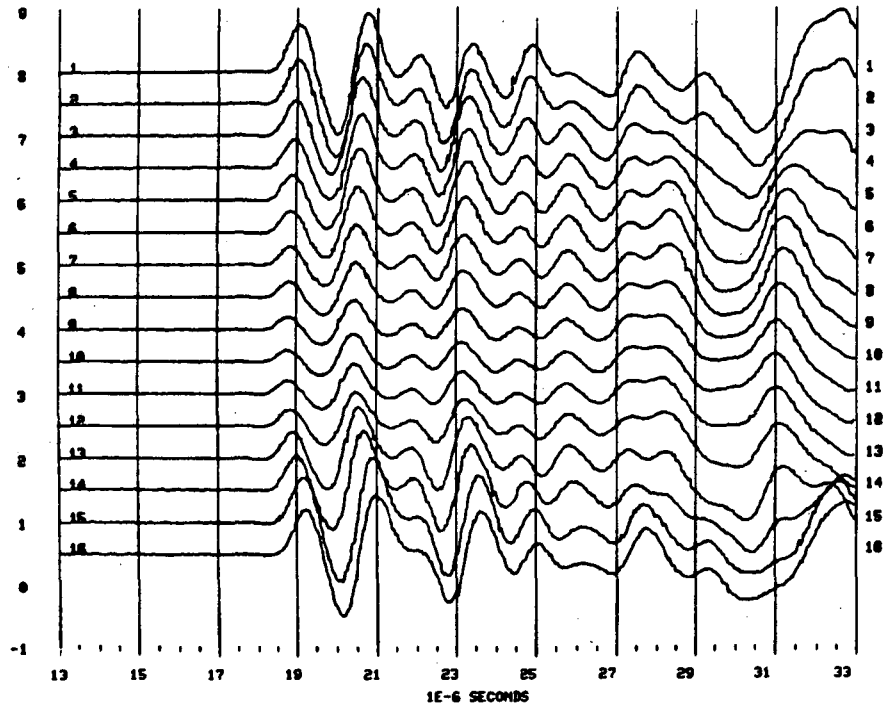
STRIPA 01, DRY, P-WAVES, FB-76, 820007

Fig. E:3.1a



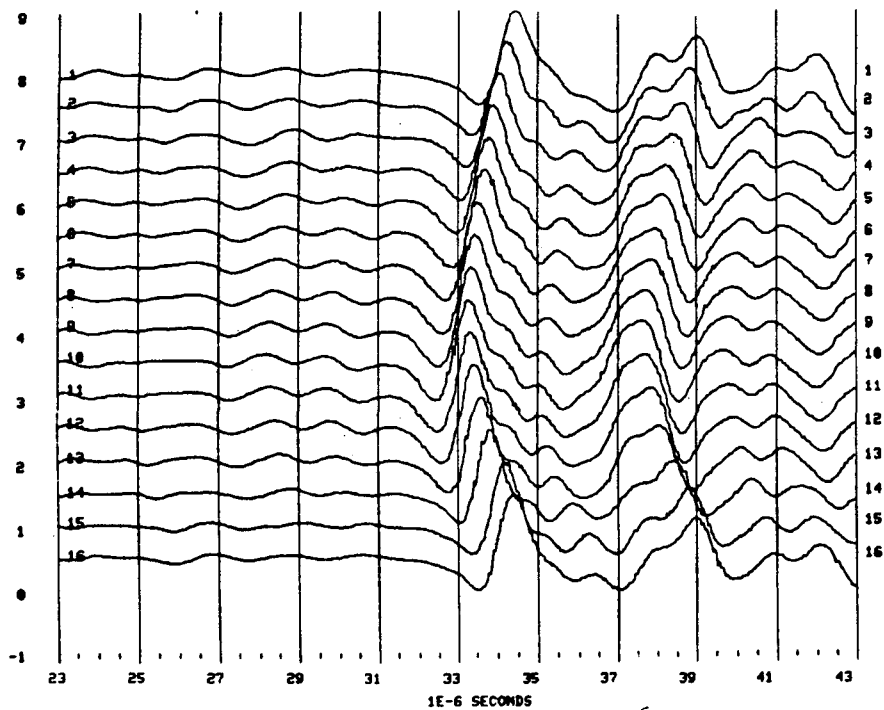
STRIPA SPECIMEN 01, SATURATED, P-WAVES, 820031

Fig. E:3.1b



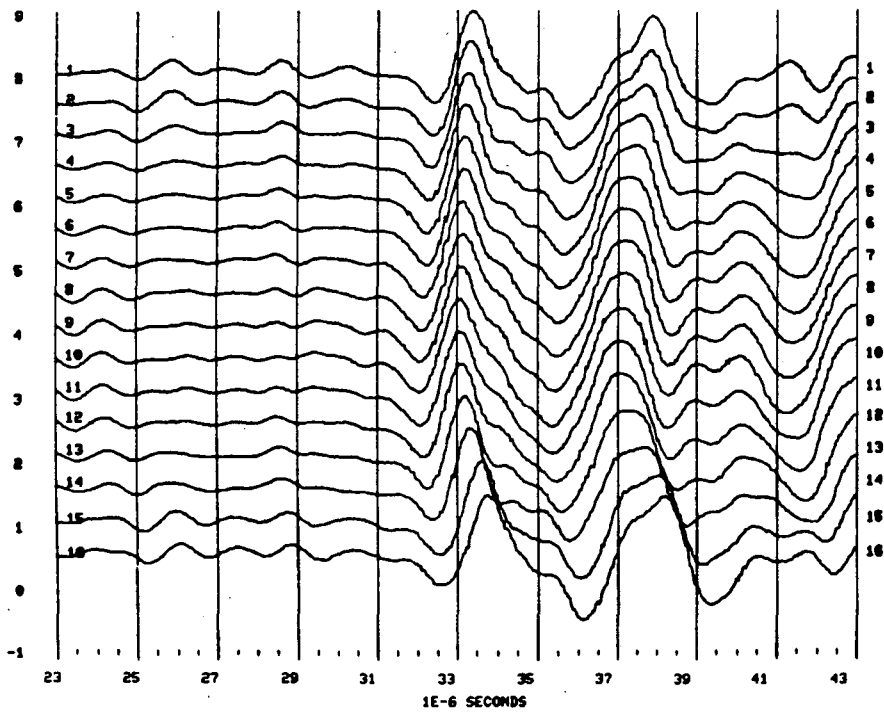
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Fig. E:3.1c



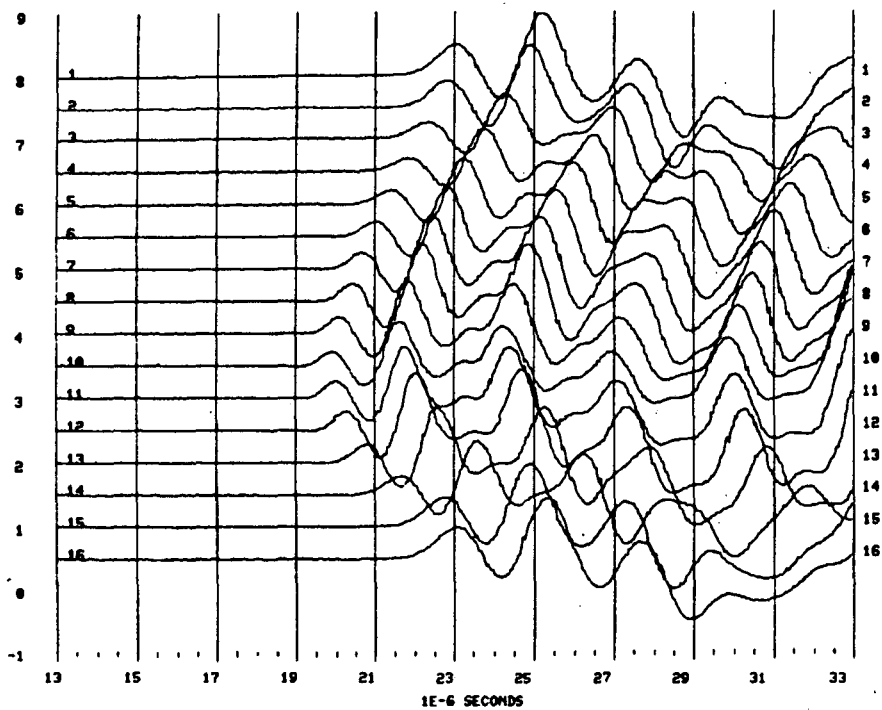
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Fig. E:3.1d



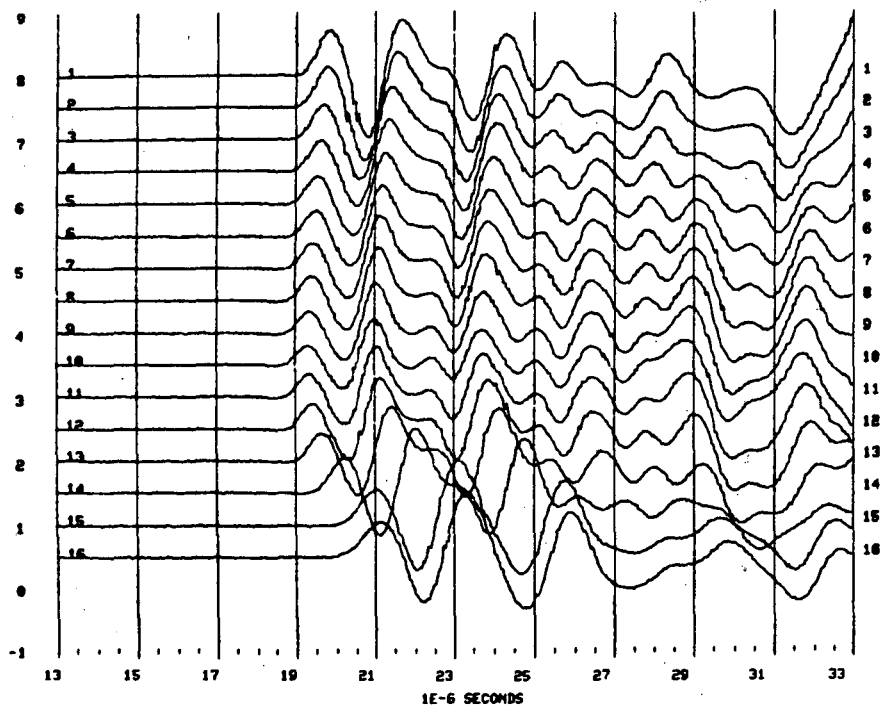
STRIPA 82, DRY, N7-ND, 820007

Fig. E:3.2a



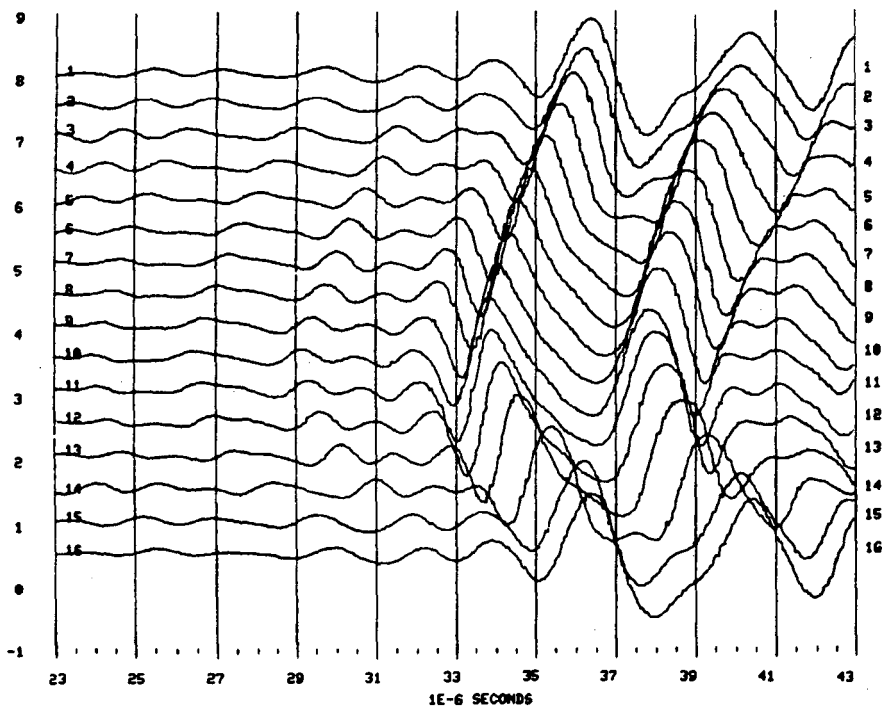
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Fig. E:3.2b



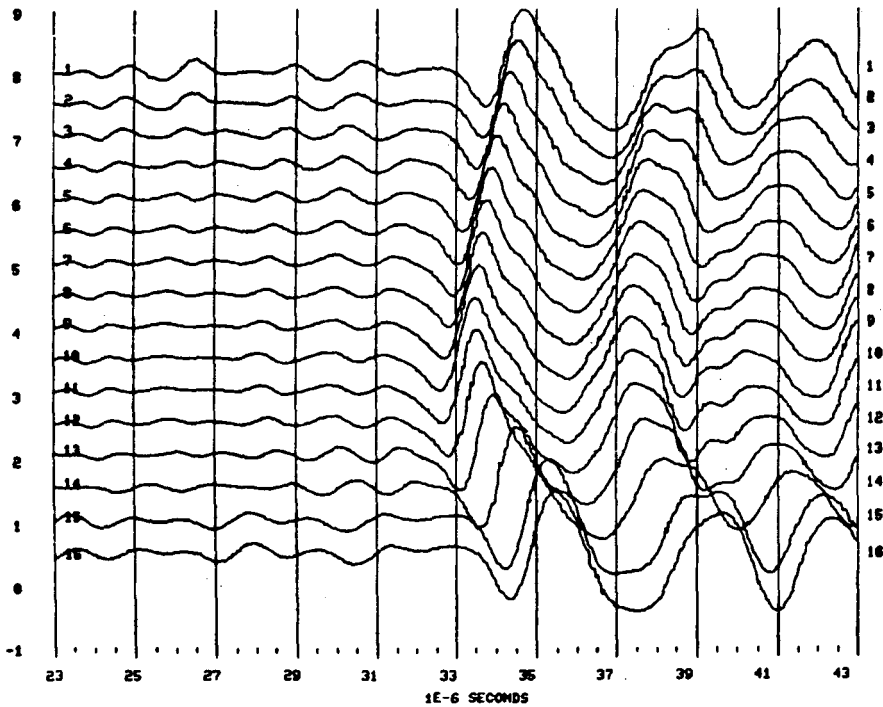
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Fig. E:3.2c

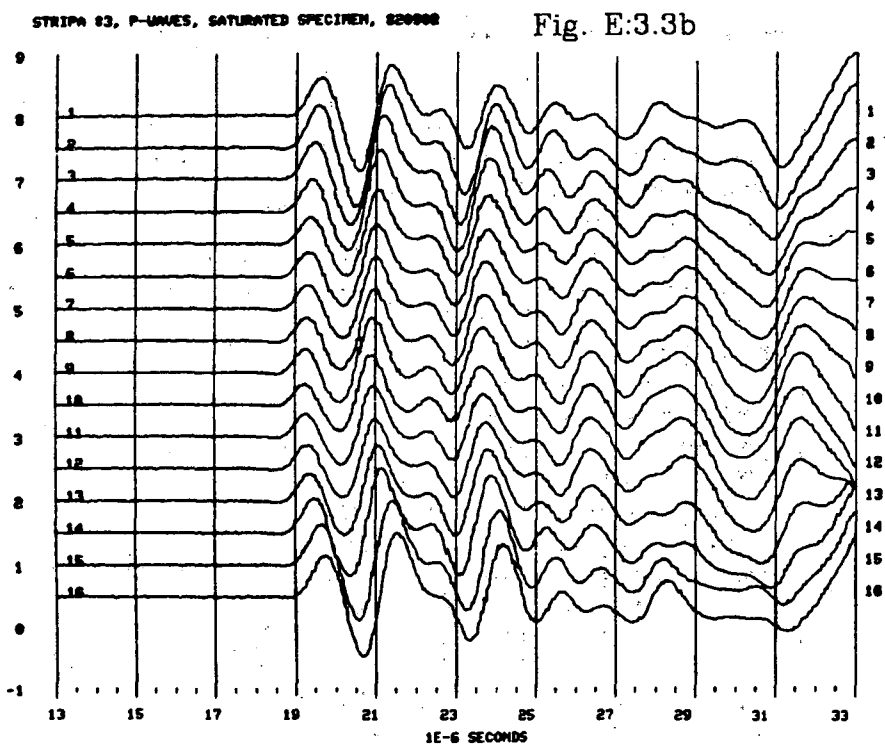
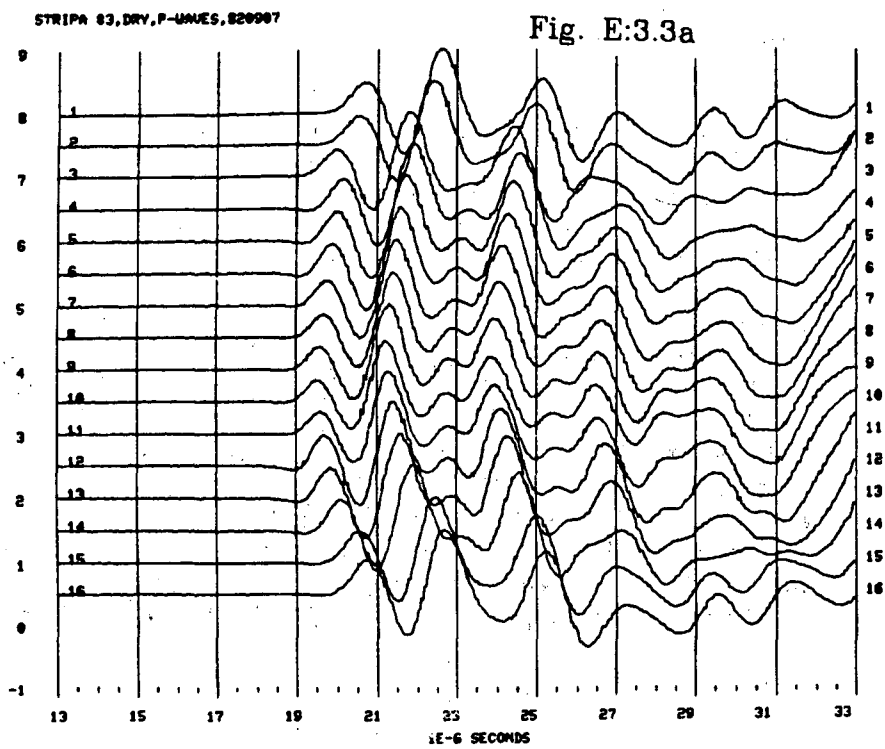


STRIPA #2, SATURATED, S-UMUES, 820931

Fig. E:3.2d

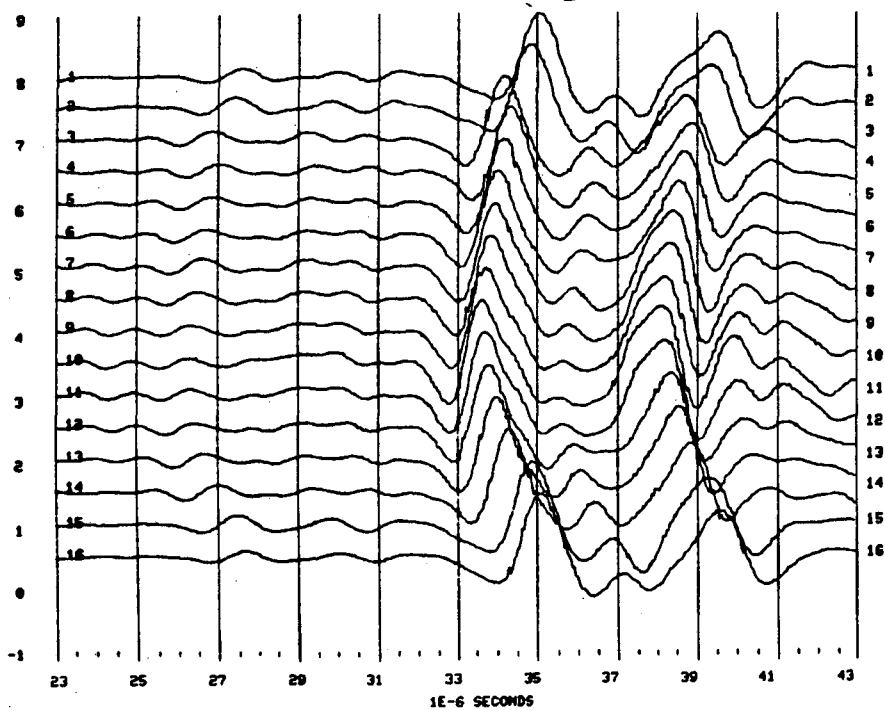






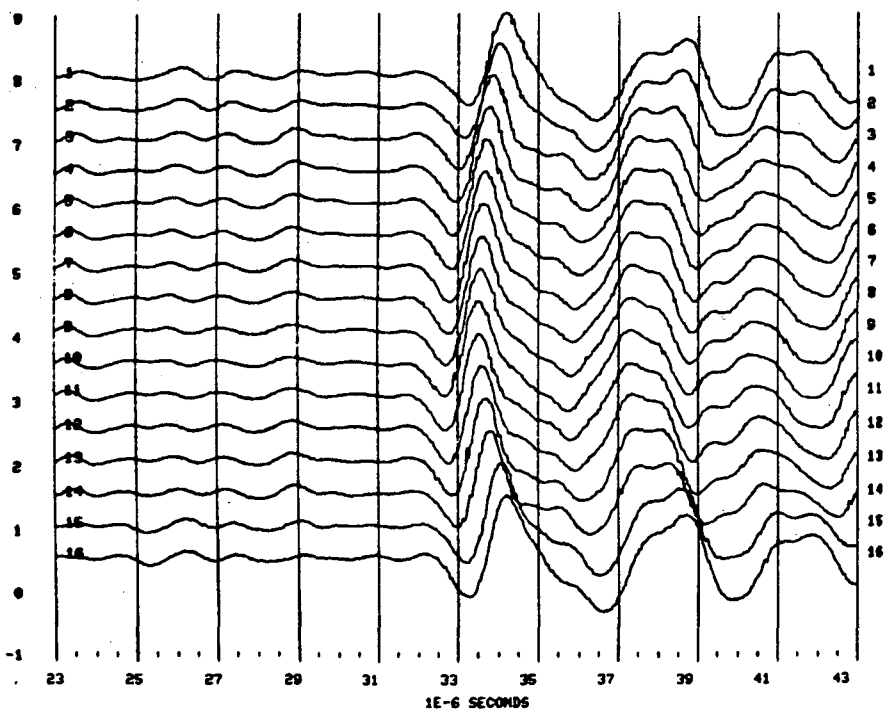
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Fig. E:3.3c



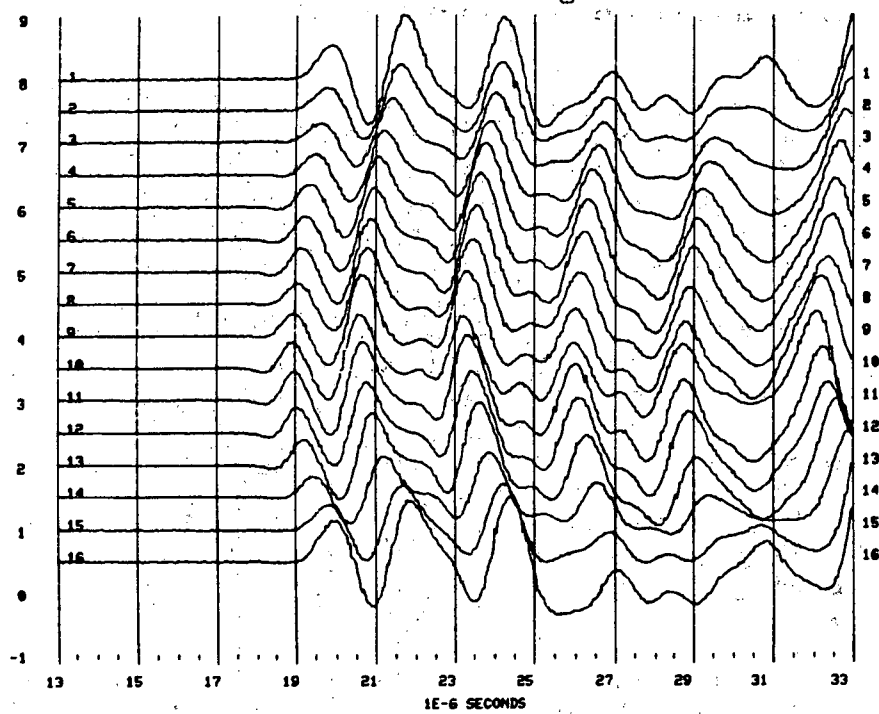
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Fig. E:3.3d



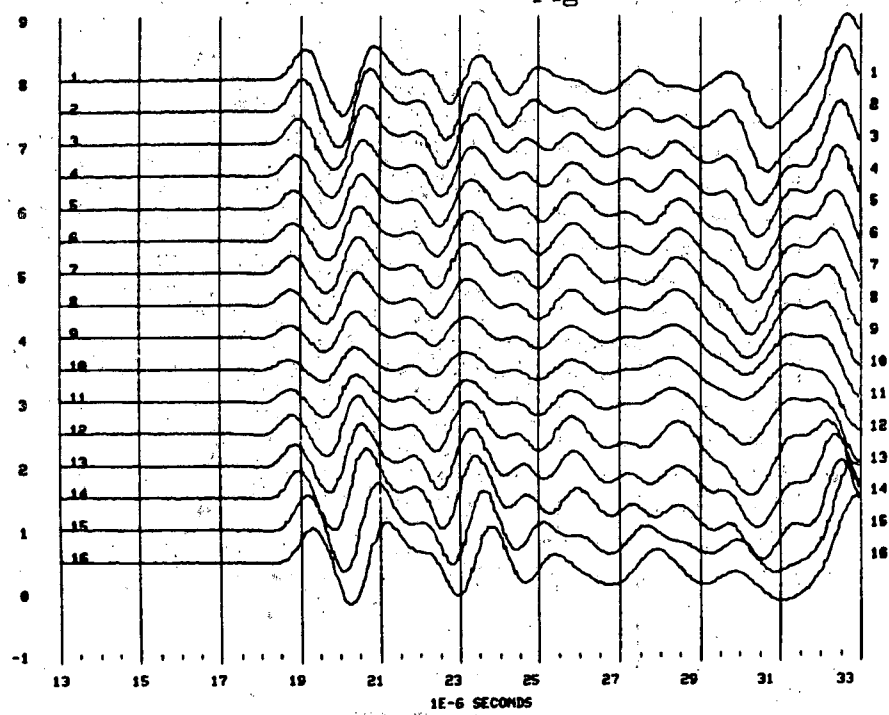
STRIPA 04, DRY, P-WAVES, DRILLBACK 1.45 F.H10, 829907

Fig. E:3.4a



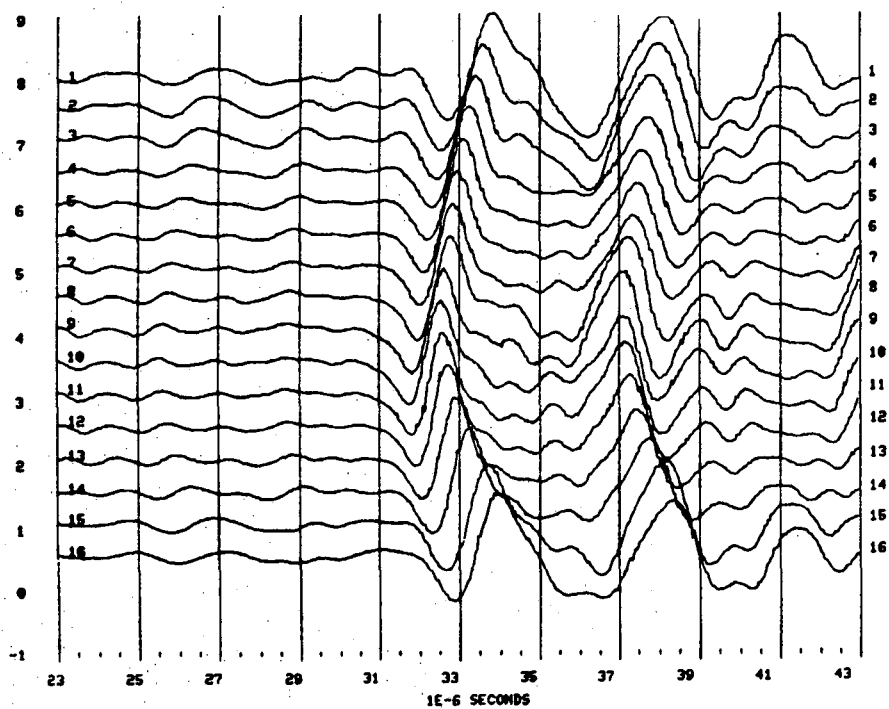
STRIPA 04, P-WAVES, SATURATED, 829902

Fig. E:3.4b



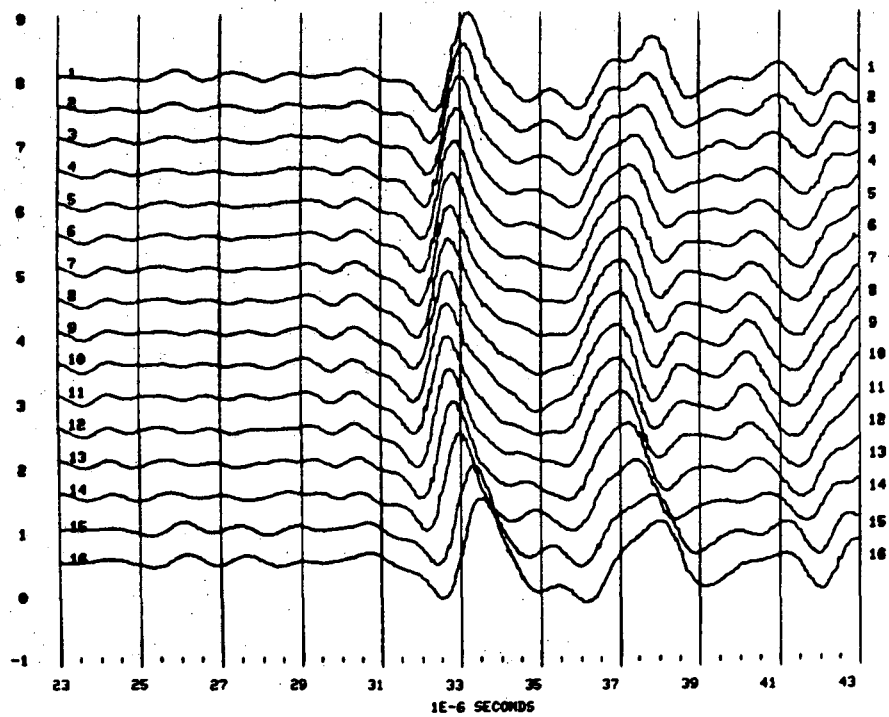
STRIPA 04, S-WAVES, DRILLBACK 1.45R F. H10, DRY, 820007

Fig. E.3.4c

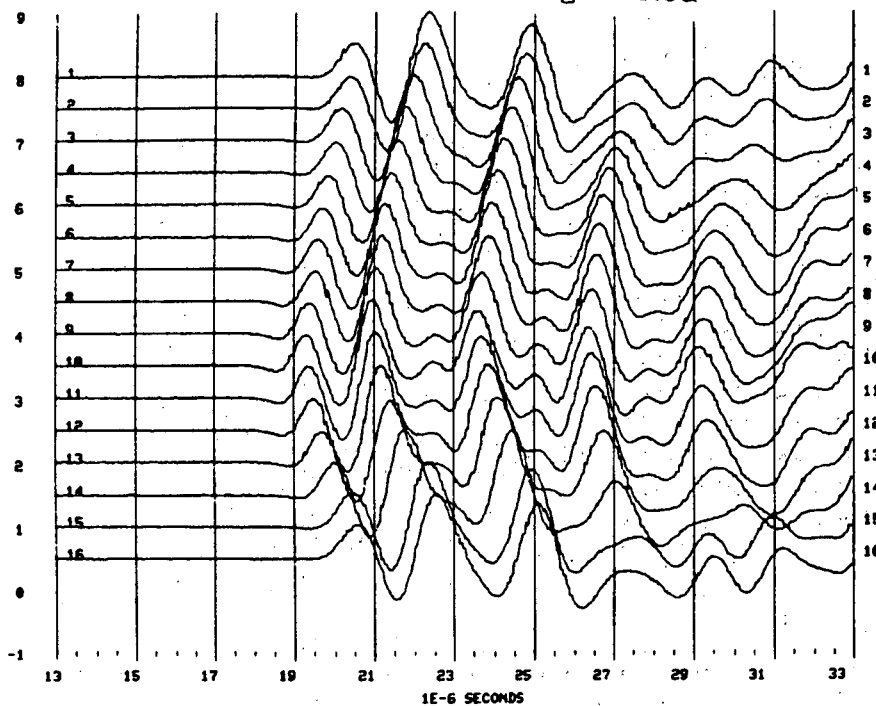


STRIPA 04, S-WAVES, SATURATED, 820003

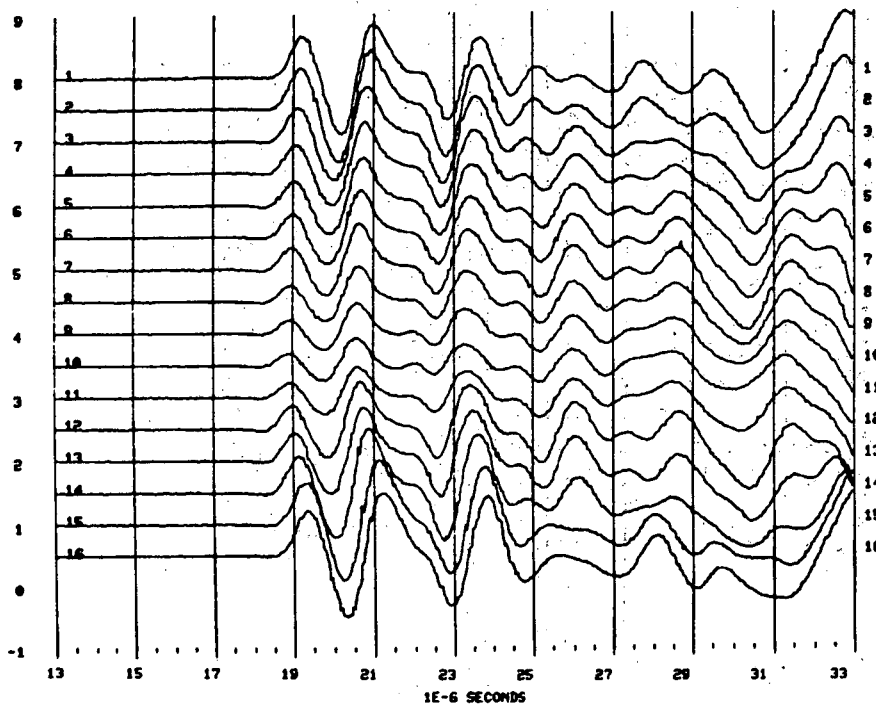
Fig. E.3.4d



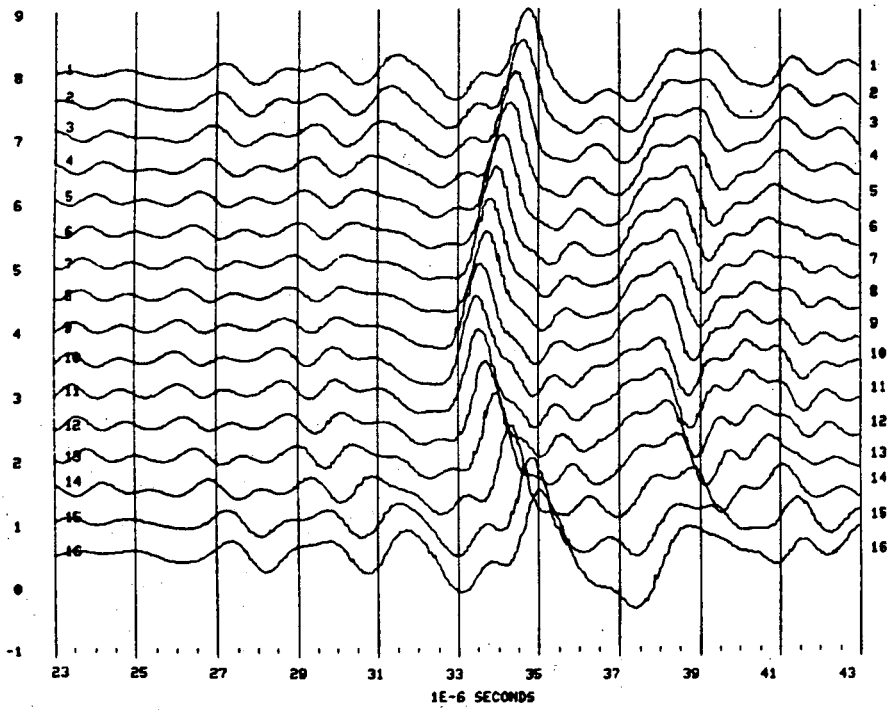
STRIPA 85, P-UNES, DRY, DRILLBACK 0.75 FROM H10, 820007 Fig. E:3.5a



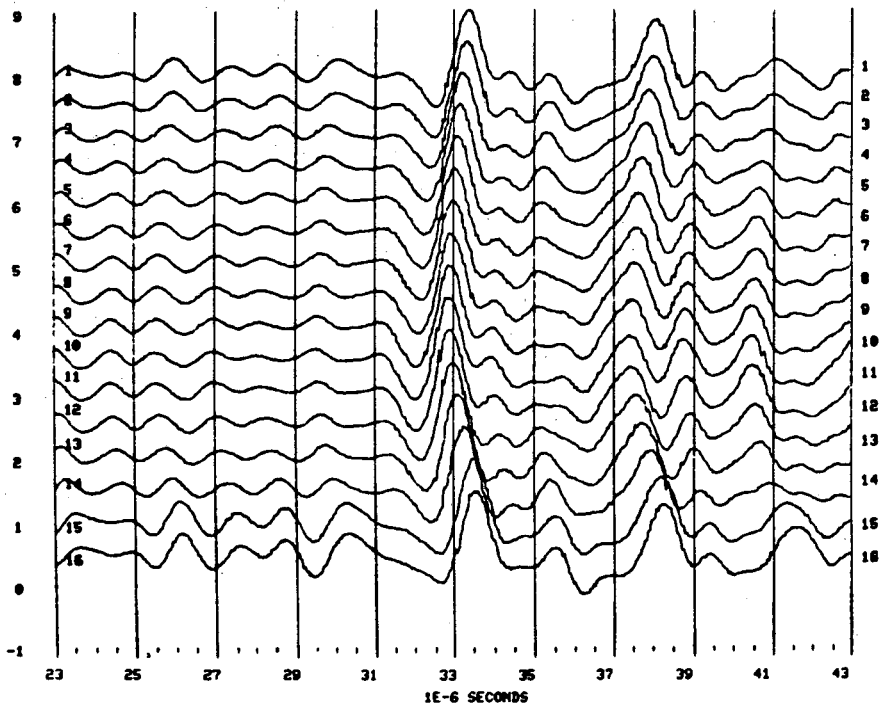
STRIPA 85, DRILLBACK 0.75 G. H10, SATURATED P-UNES, 820003 Fig. E:3.5b



STRIPA 85, DRY, 5-UNES, DRILLBACK 0.75R FROM H10, 820001 Fig. E:3.5c

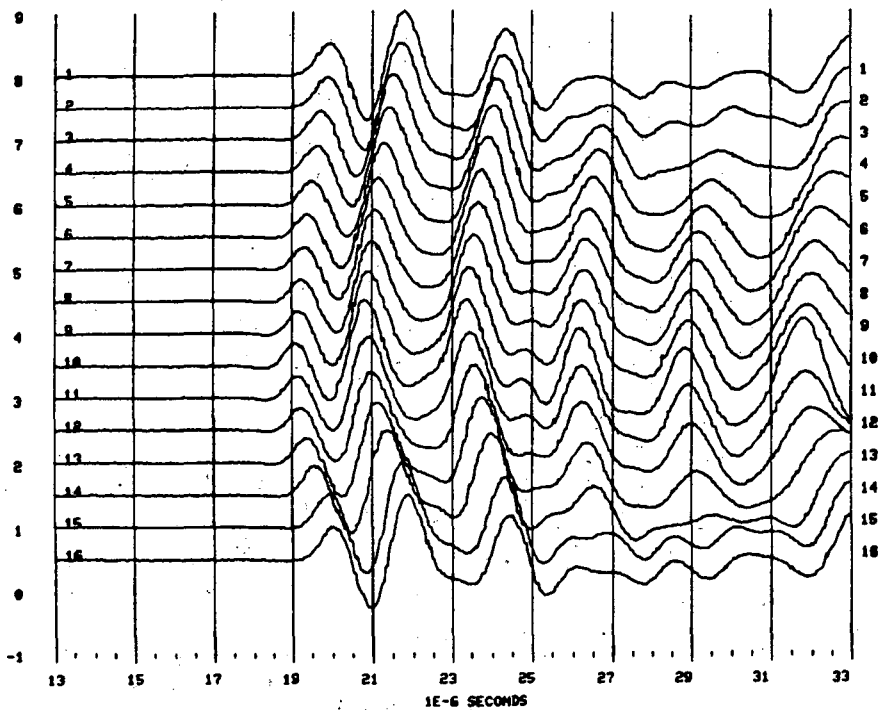


STRIPA 85, SATURATED, DRILLBACK 0.75R FROM H10, 5-UNES, 820003 Fig. E:3.5d



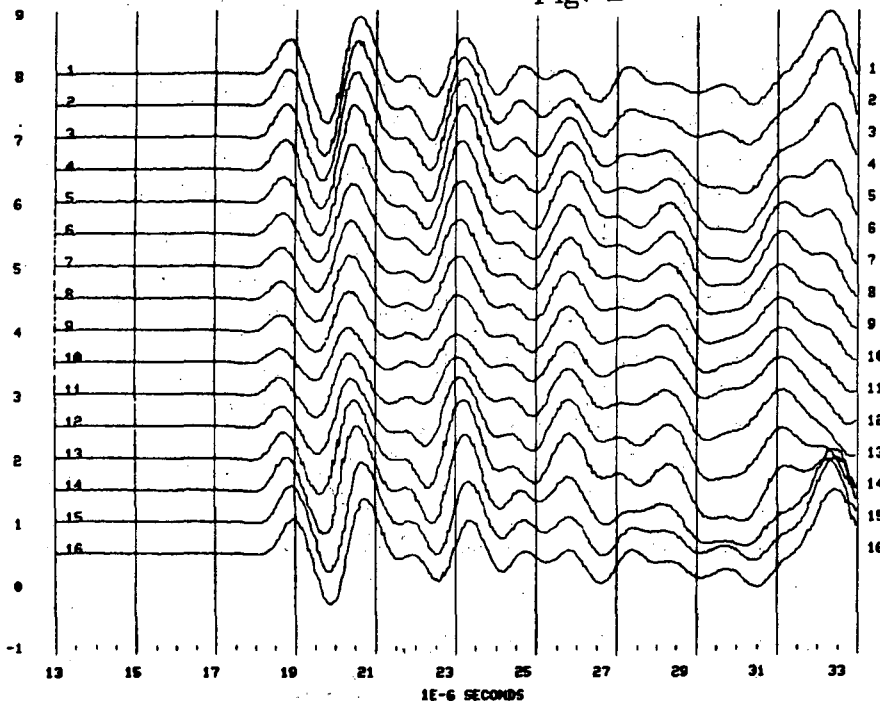
STRIPA 86, E22, DRY, P-WAVES, 820916

Fig. E:3.6a



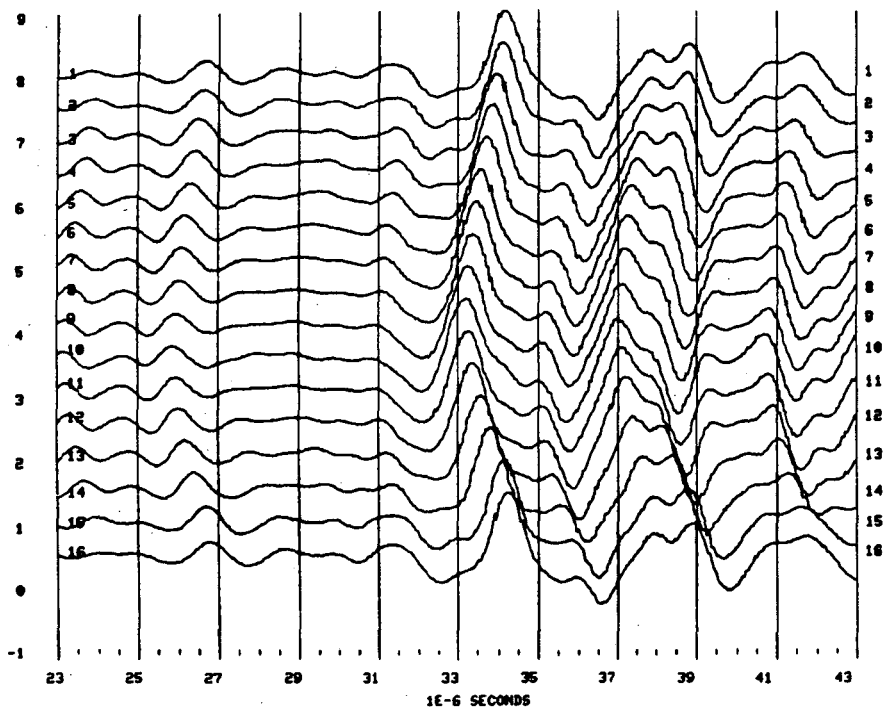
STRIPA 86, P-WAVES, SATURATED, MS-MG, 820929

Fig. E:3.6b



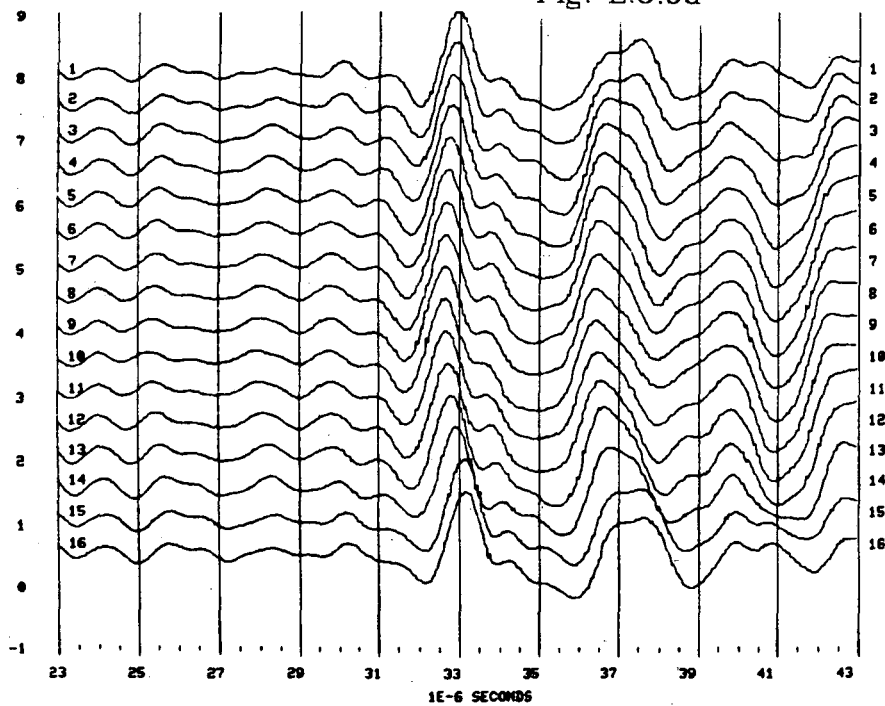
STRIPA 86, E22, RB-R6, S-WAVES, DRY, 820917

Fig. E:3.6c



STRIPA 86, S-WAVES, SATURATED, RB-R6, 820929

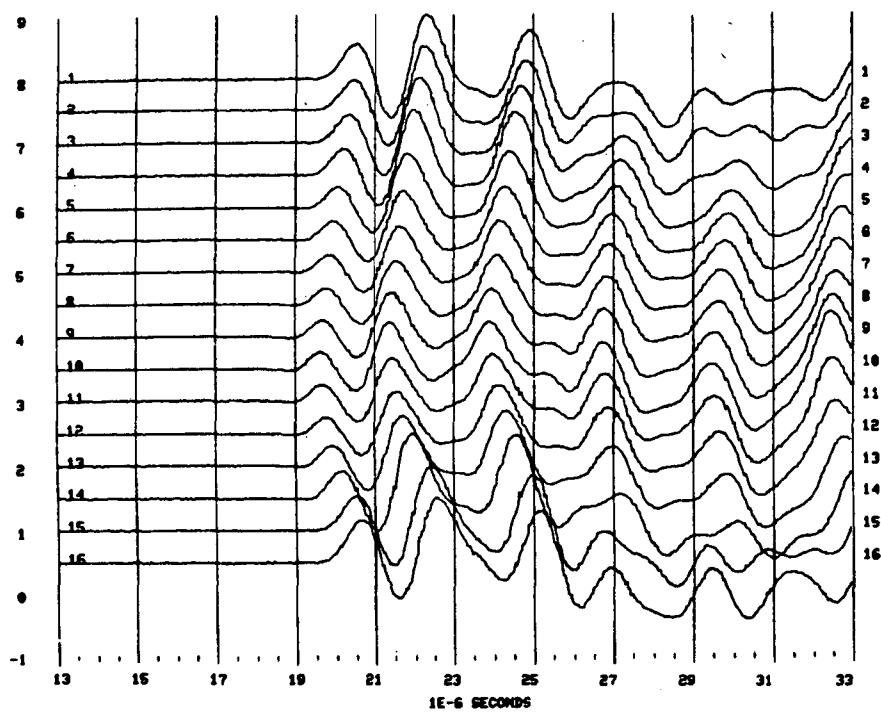
Fig. E:3.6d





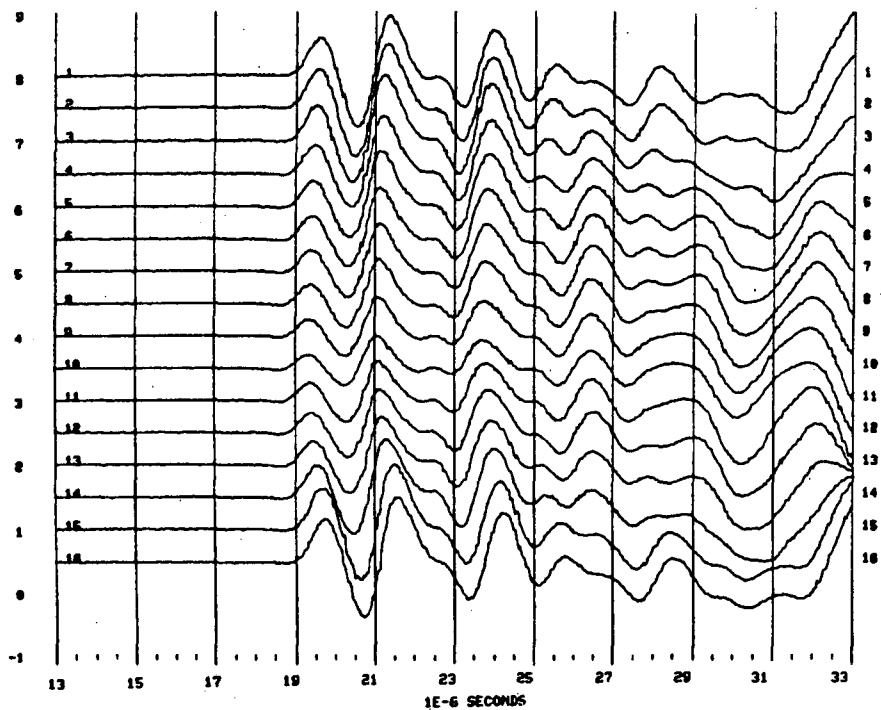
STRIPA 87, DRY, P-WAVES, 820917

Fig. E:3.7a



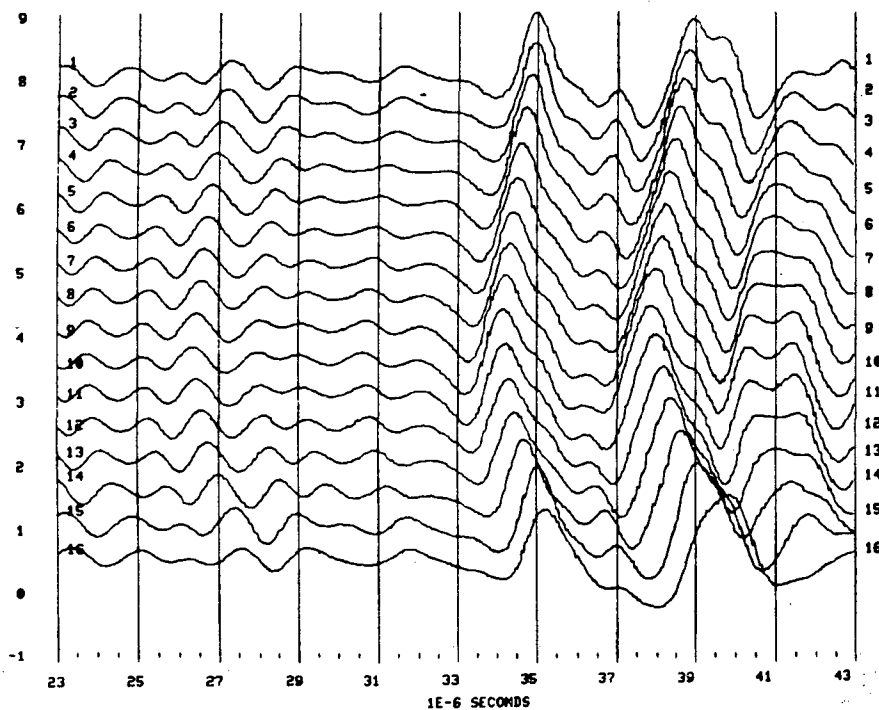
STRIPA 87, P-WAVES, SATURATED, NO-MS, 820909

Fig. E:3.7b



STRIPA 87, DRY, S-WAVES, 820917

Fig. E:3.7c



STRIPA 87, S-WAVES, SATURATED, 820920

Fig. E:3.7d

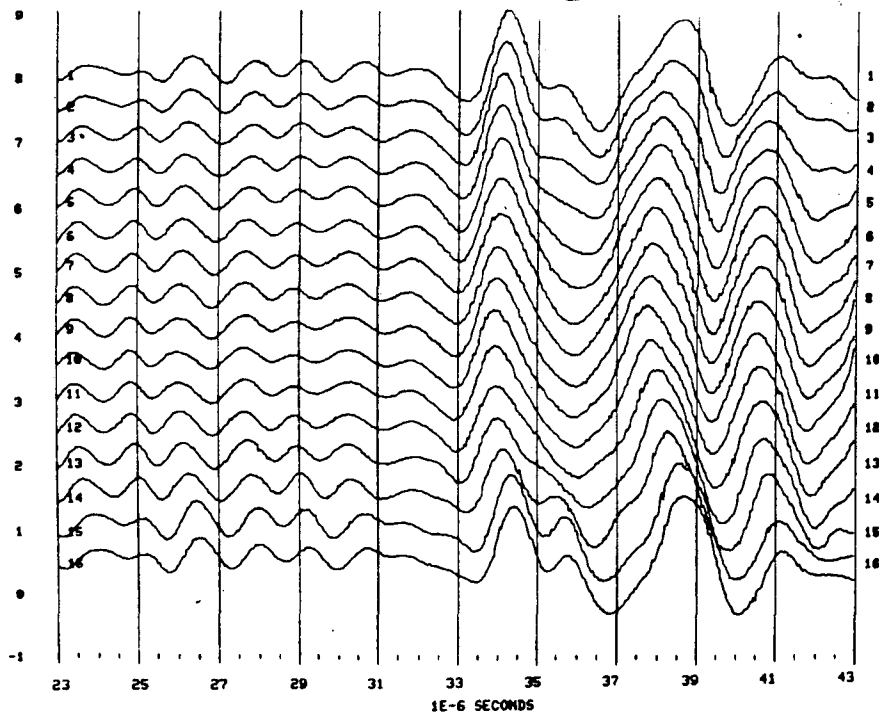


Fig. E:3.8a

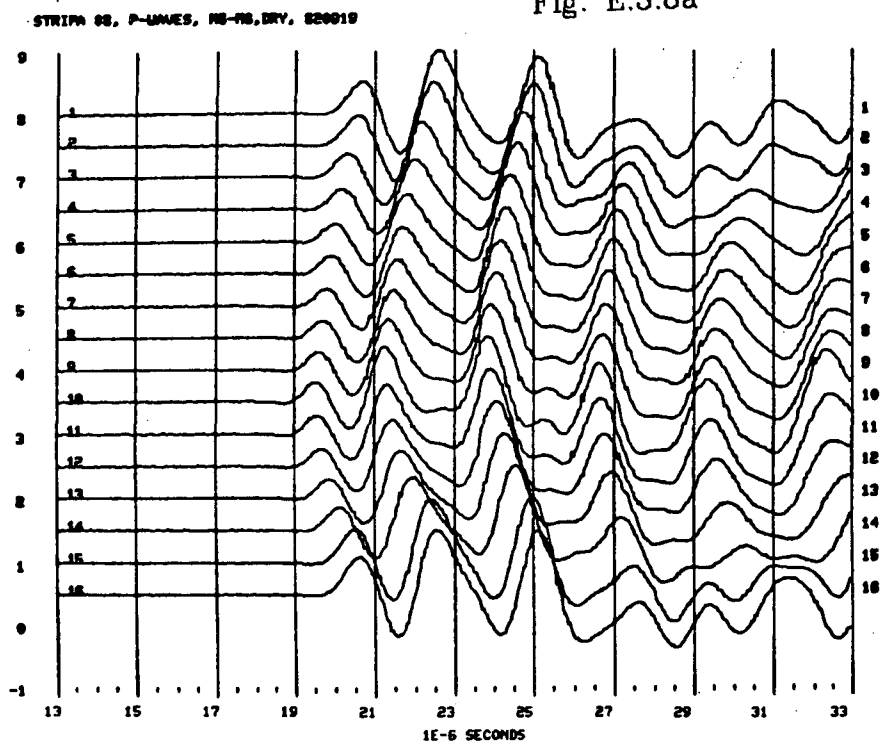
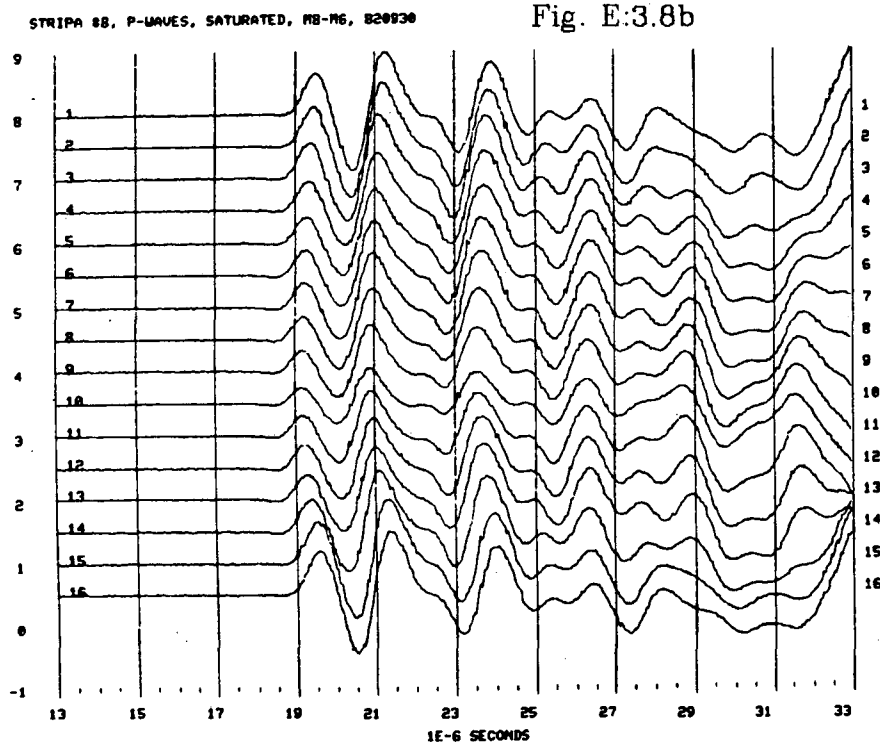
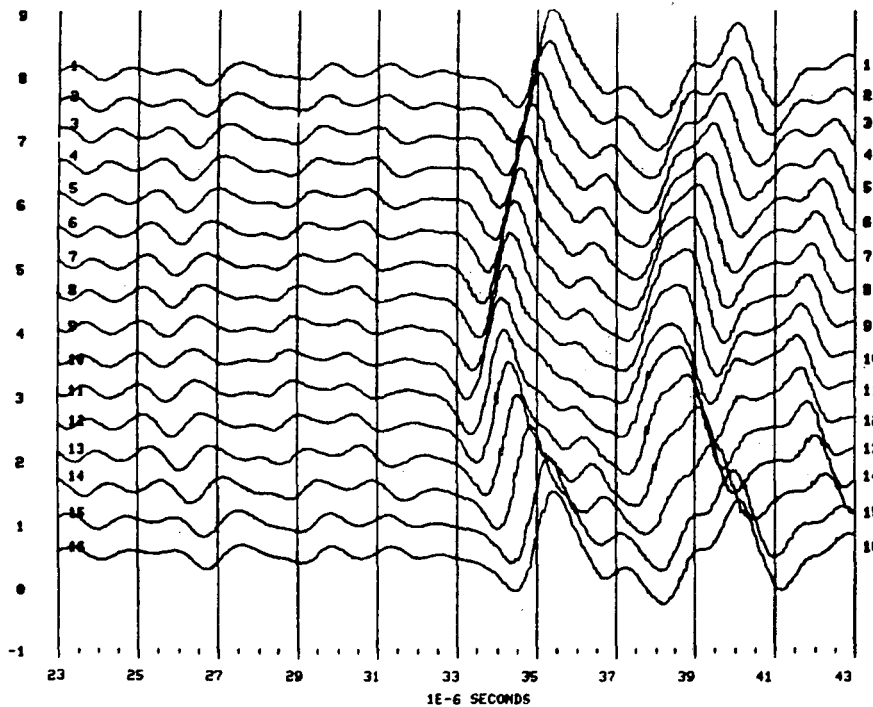


Fig. E:3.8b



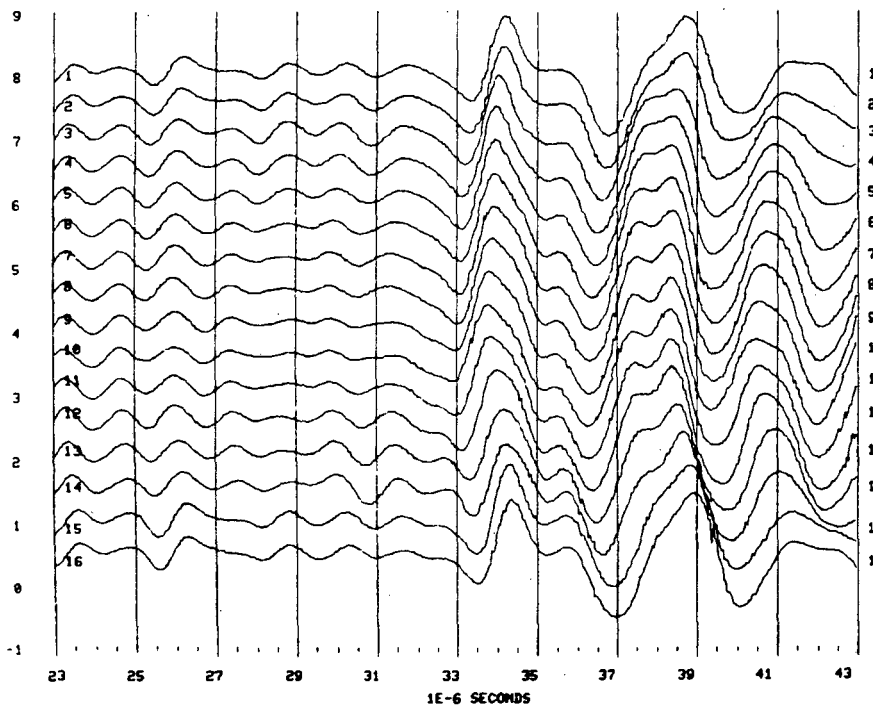
STRIPA 88, S-WAVES, NB-FR, DRY, 820919

Fig. E:3.8c



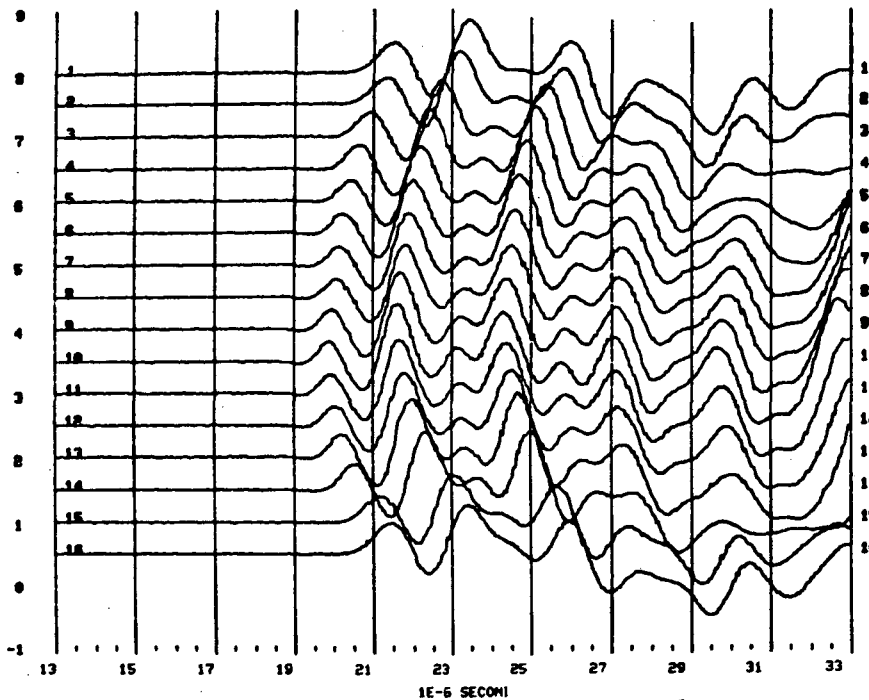
STRIPA 88, S-WAVES, SATURATED, NB-P6, 820930

Fig. E:3.8d



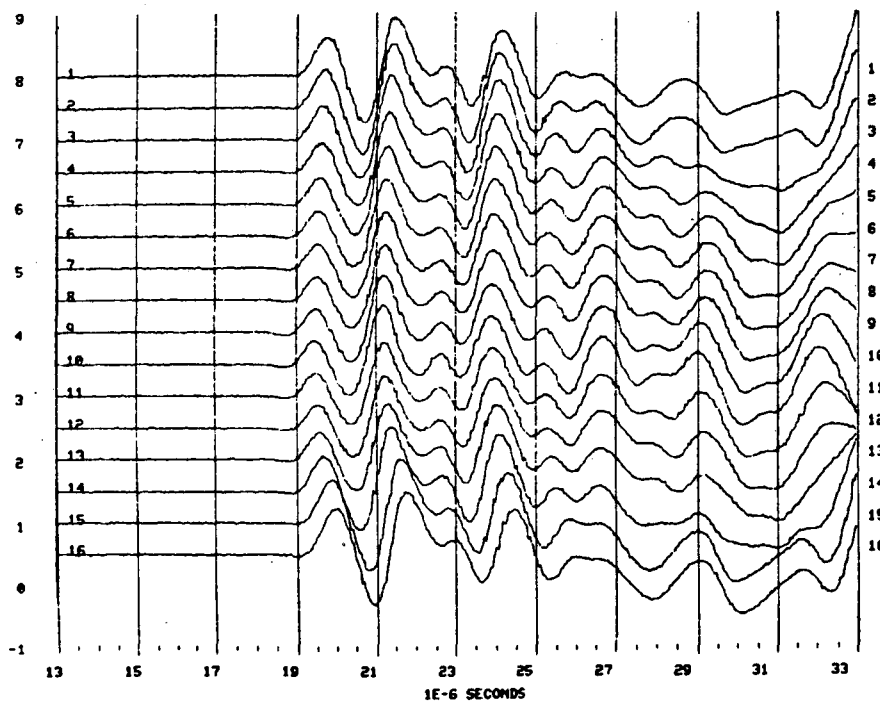
STRIPA 89, P-WAVES, DRY, RB-RS, 820928

Fig. E:3.9a



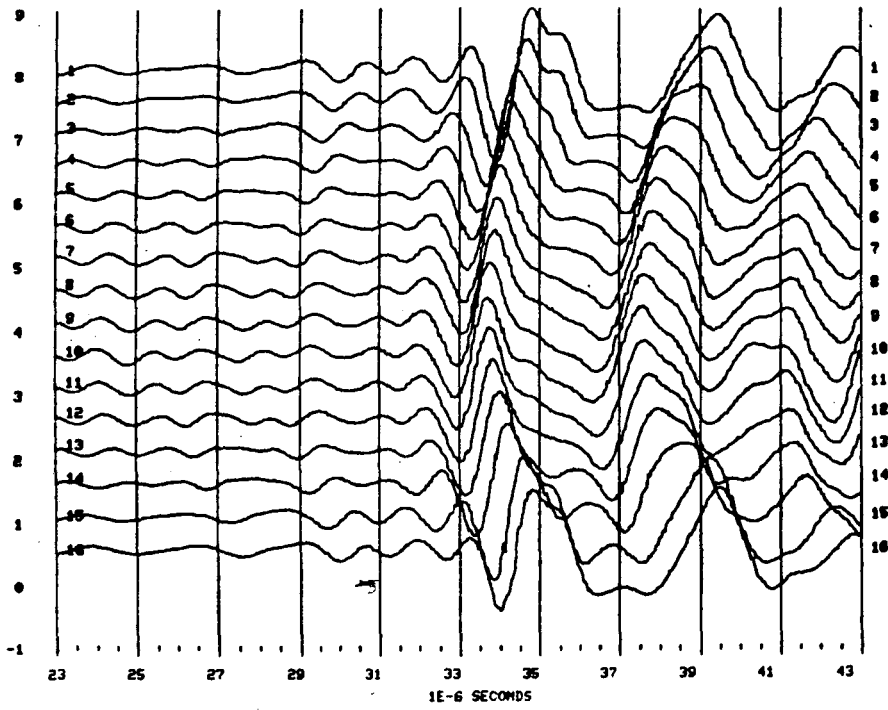
STRIPA 89, P-WAVES, SATURATED, 820930

Fig. E:3.9b



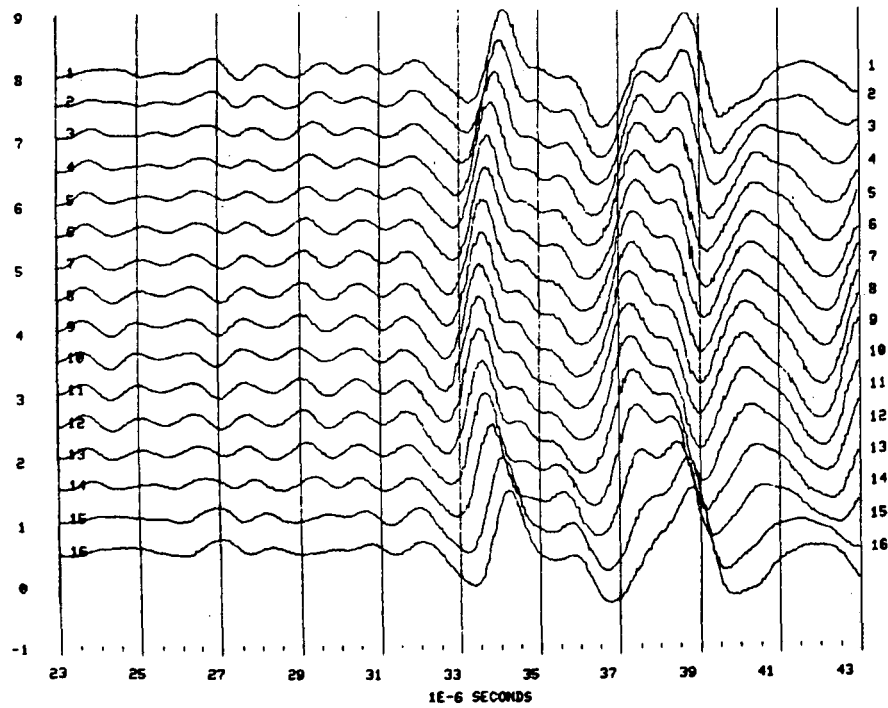
STRIPA 89, S-WAVES, DRY, 820928

Fig. E:3.9c



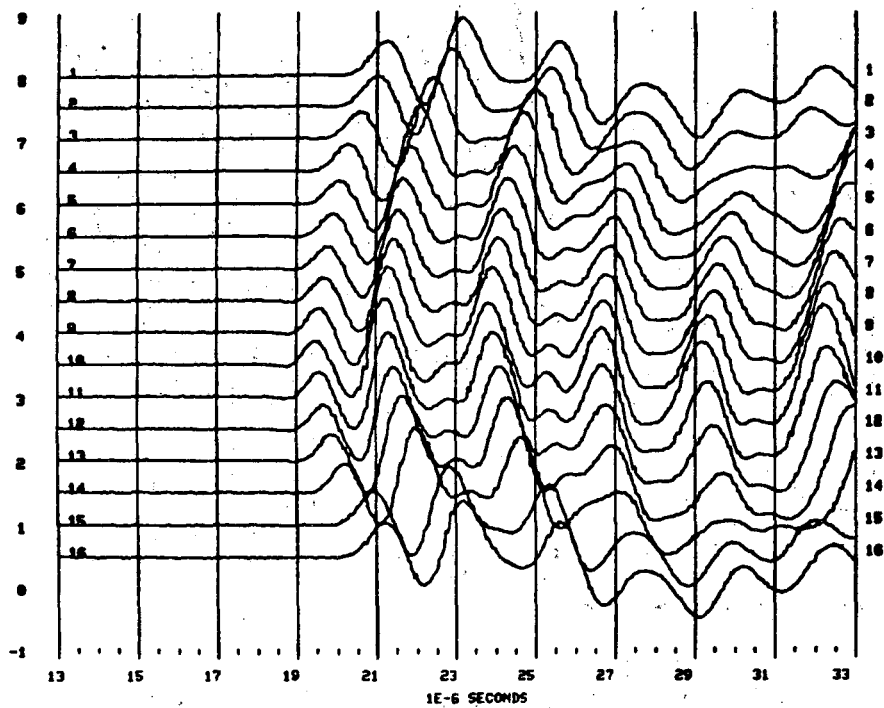
STRIPA 89, S-WAVES, SATURATED, 820930

Fig. E:3.9d



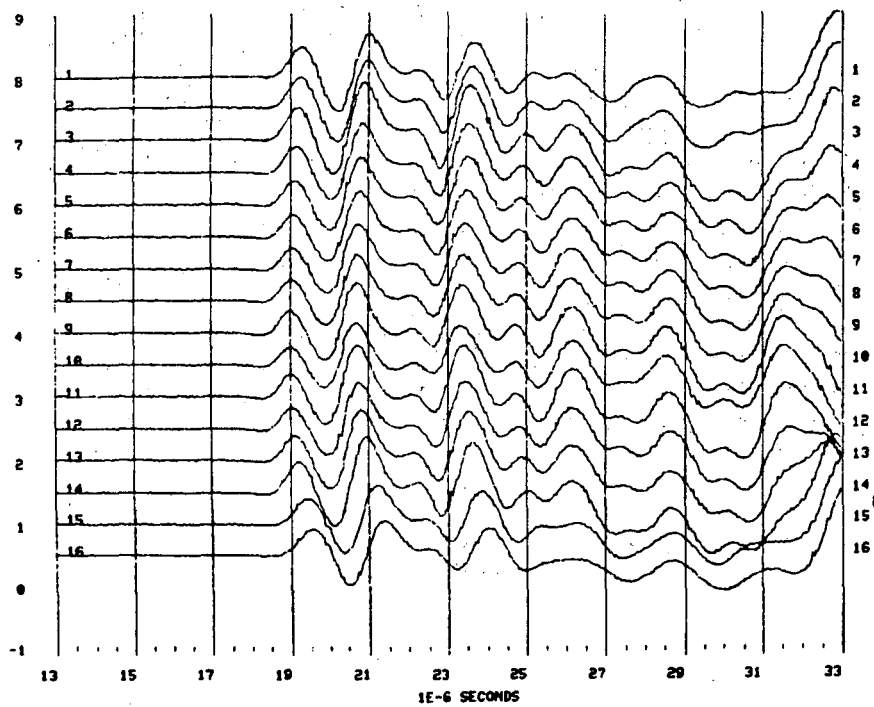
STRIPA #10, P-WAVES, DRY, 87-10, 829928

Fig. E:3.10a



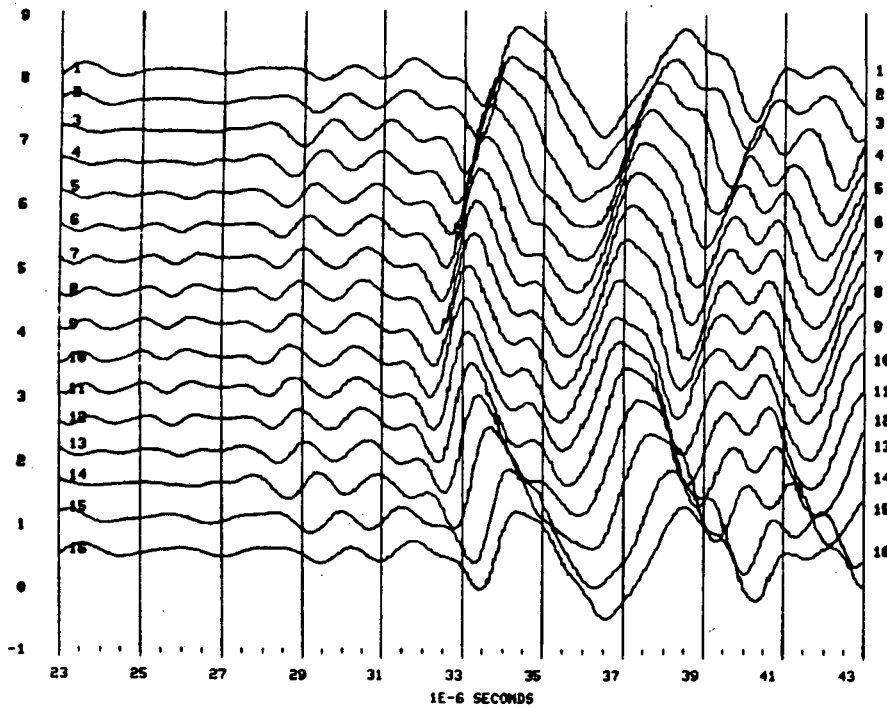
STRIPA #10, P-WAVES, SATURATED, 829930

Fig. E:3.10b



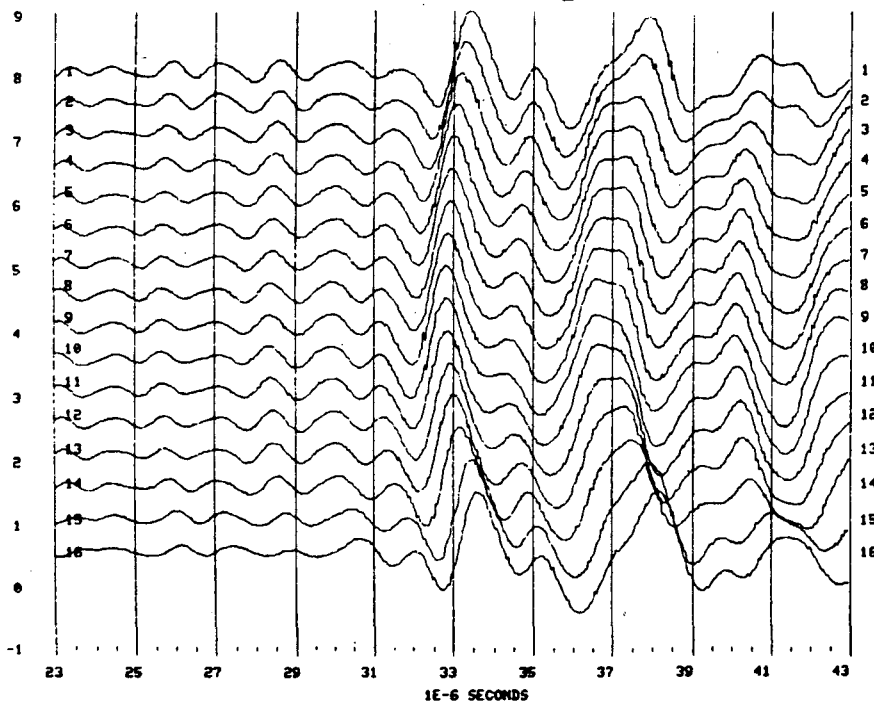
STRIPA #10, 5-WAVES, DRY, #7-79, 820920

Fig. E:3.10c



STRIPA #10, 5-WAVES, SATURATED, 820930

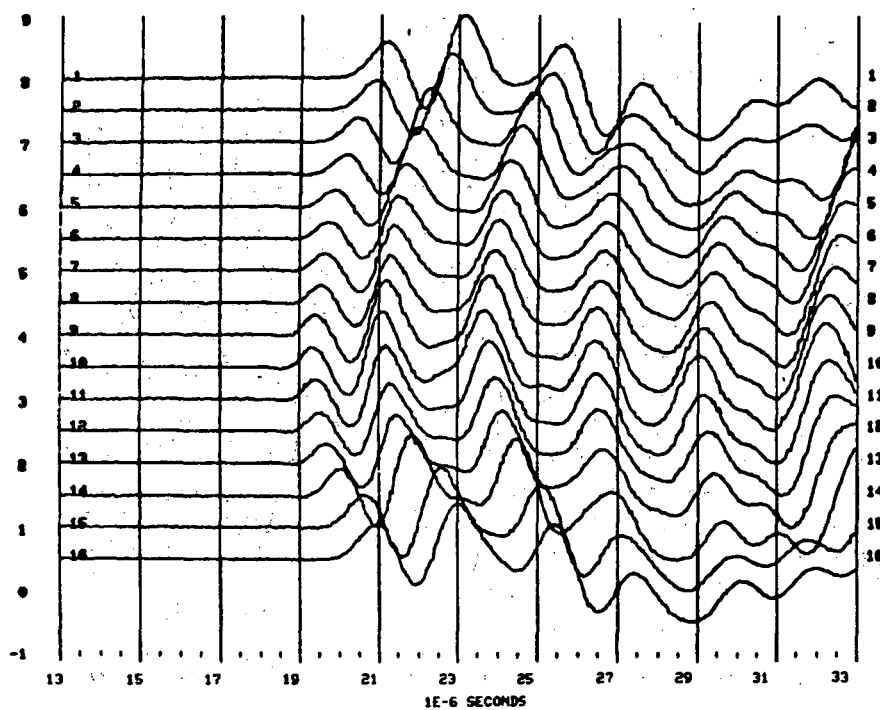
Fig. E:3.10d





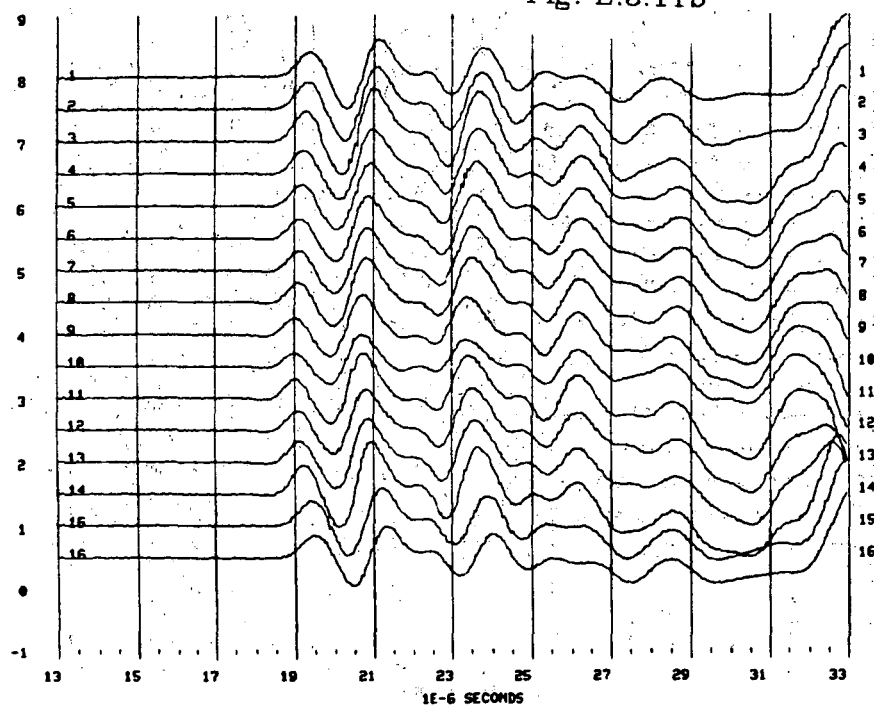
STRIPA 811, P-WAVES, DRY, NT-NO, 820929

Fig. E:3.11a



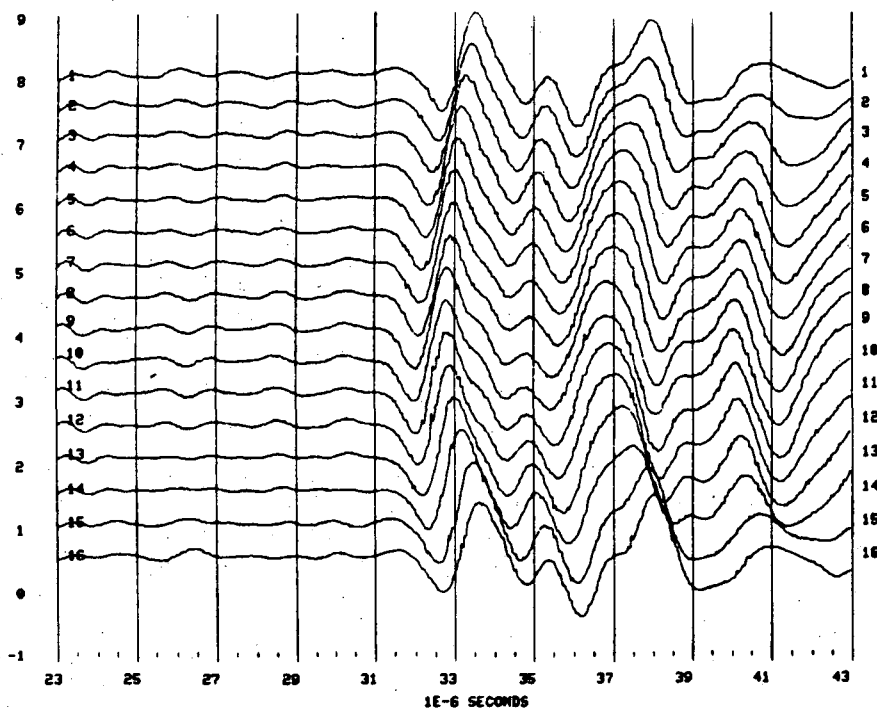
STRIPA 811, P-WAVES, SATURATED, 820930

Fig. E:3.11b



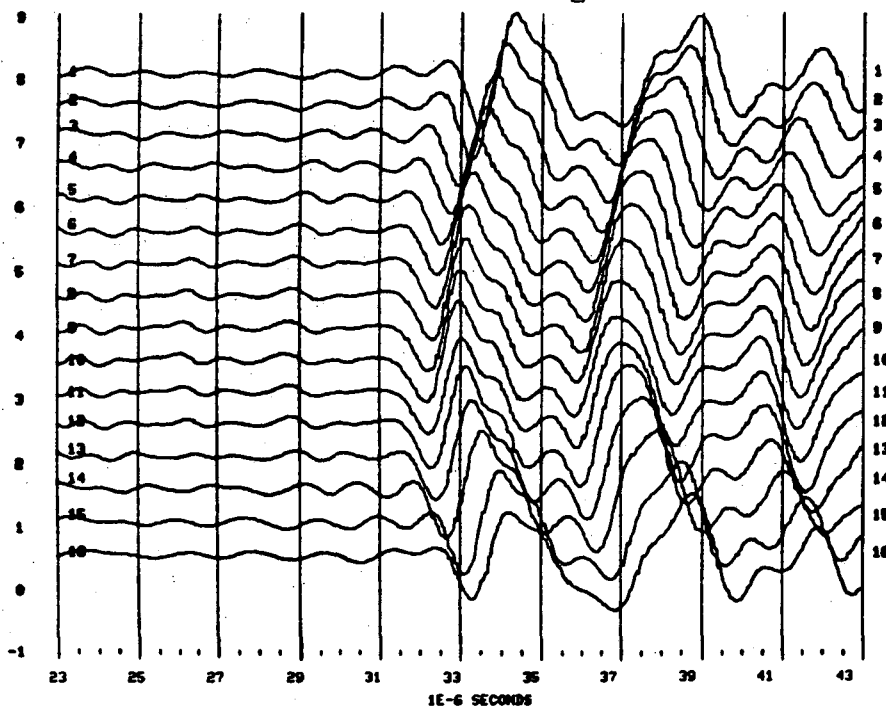
STRIPA 811, S-WAVES, SATURATED, 820930

Fig. E:3.11c



STRIPA 811, S-WAVES, DRY, 87-80, 880000

Fig. E:3.11d



## Appendix E:4 - Truncated P and S waveforms from the laboratory test.

In this appendix the P and S waveforms after truncation are shown. The P waves were truncated with a  $4 \times 10^{-6}$  s long half cos window and the S waves were truncated with a  $3 \times 10^{-6}$  s cos window.

**Figure captions for Appendix E:4**

Fig. E:4.1a Truncated P waveforms as function of uniaxial stress for the dry specimen # 1

Fig. E:4.1b Truncated P waveforms as function of uniaxial stress for the saturated specimen # 1

Fig. E:4.1c Truncated S waveforms as function of uniaxial stress for the dry specimen # 1

Fig. E:4.1d Truncated S waveforms as function of uniaxial stress for the saturated specimen # 1

Fig. E:4.2a Truncated P waveforms as function of uniaxial stress for the dry specimen # 2

Fig. E:4.2b Truncated P waveforms as function of uniaxial stress for the saturated specimen # 2

Fig. E:4.2c Truncated S waveforms as function of uniaxial stress for the dry specimen # 2

Fig. E:4.2d Truncated S waveforms as function of uniaxial stress for the saturated specimen # 2

Fig. E:4.3a Truncated P waveforms as function of uniaxial stress for the dry specimen # 3

Fig. E:4.3b Truncated P waveforms as function of uniaxial stress for the saturated specimen # 3

Fig. E:4.3c Truncated S waveforms as function of uniaxial stress for the dry specimen # 3

Fig. E:4.3d Truncated S waveforms as function of uniaxial stress for the saturated specimen # 3

Fig. E:4.4a Truncated P waveforms as function of uniaxial stress for the dry specimen # 4

Fig. E:4.4b Truncated P waveforms as function of uniaxial stress for the saturated specimen # 4

Fig. E:4.4c Truncated S waveforms as function of uniaxial stress for the dry specimen # 4

Fig. E:4.4d Truncated S waveforms as function of uniaxial stress for the saturated specimen # 4

Fig. E:4.5a Truncated P waveforms as function of uniaxial stress for the dry specimen # 5

Fig. E:4.5b Truncated P waveforms as function of uniaxial stress for the saturated specimen # 5

Fig. E:4.5c Truncated S waveforms as function of uniaxial stress for the dry specimen # 5

Fig. E:4.5d Truncated S waveforms as function of uniaxial stress for the saturated specimen # 5

Fig. E:4.6a Truncated P waveforms as function of uniaxial stress for the dry specimen # 6

Fig. E:4.6b Truncated P waveforms as function of uniaxial stress for the saturated specimen # 6

Fig. E:4.6c Truncated S waveforms as function of uniaxial stress for the dry specimen # 6

Fig. E:4.6d Truncated S waveforms as function of uniaxial stress for the saturated specimen # 6

Fig. E:4.7a Truncated P waveforms as function of uniaxial stress for the dry specimen # 7

Fig. E:4.7b Truncated P waveforms as function of uniaxial stress for the saturated specimen # 7

Fig. E:4.7c Truncated S waveforms as function of uniaxial stress for the dry specimen # 7

Fig. E:4.7d Truncated S waveforms as function of uniaxial stress for the saturated specimen # 7

Fig. E:4.8a Truncated P waveforms as function of uniaxial stress for the dry specimen # 8

Fig. E:4.8b Truncated P waveforms as function of uniaxial stress for the saturated specimen # 8

Fig. E:4.8c Truncated S waveforms as function of uniaxial stress for the dry specimen # 8

Fig. E:4.8d Truncated S waveforms as function of uniaxial stress for the saturated specimen # 8

Fig. E:4.9a Truncated P waveforms as function of uniaxial stress for the dry specimen # 9

Fig. E:4.9b Truncated P waveforms as function of uniaxial stress for the saturated specimen # 9

Fig. E:4.9c Truncated S waveforms as function of uniaxial stress for the dry specimen # 9

Fig. E:4.9d Truncated S waveforms as function of uniaxial stress for the saturated specimen # 9

Fig. E:4.10a Truncated P waveforms as function of uniaxial stress for the dry specimen # 10

Fig. E:4.10b Truncated P waveforms as function of uniaxial stress for the saturated specimen # 10

Fig. E:4.10c Truncated S waveforms as function of uniaxial stress for the dry specimen # 10

Fig. E:4.10d Truncated S waveforms as function of uniaxial stress for the saturated specimen # 10

Fig. E:4.11a Truncated P waveforms as function of uniaxial stress for the dry specimen # 11

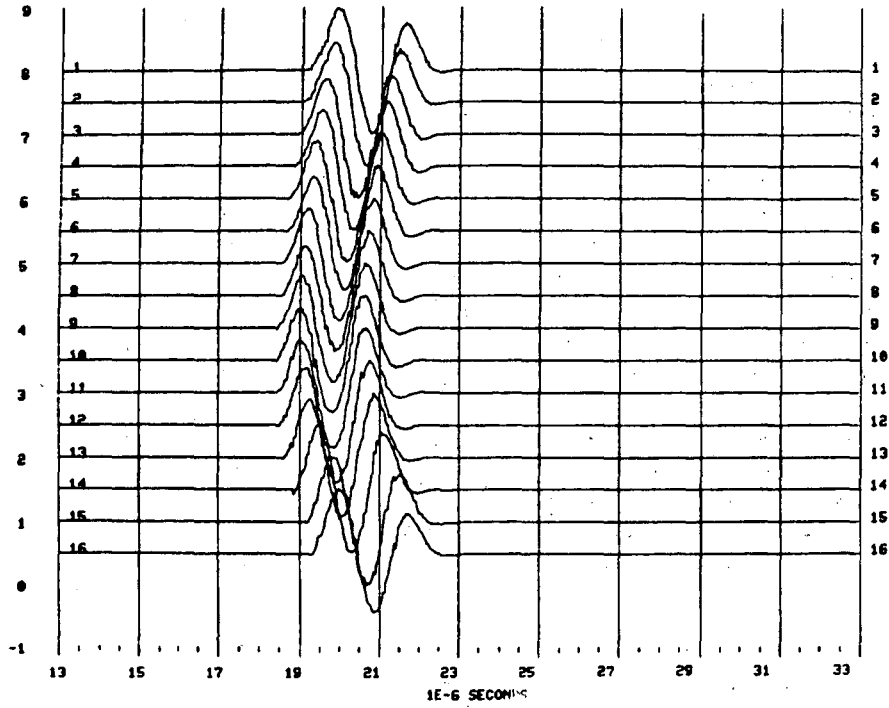
Fig. E:4.11b Truncated P waveforms as function of uniaxial stress for the saturated specimen # 11

Fig. E:4.11c Truncated S waveforms as function of uniaxial stress for the dry specimen # 11

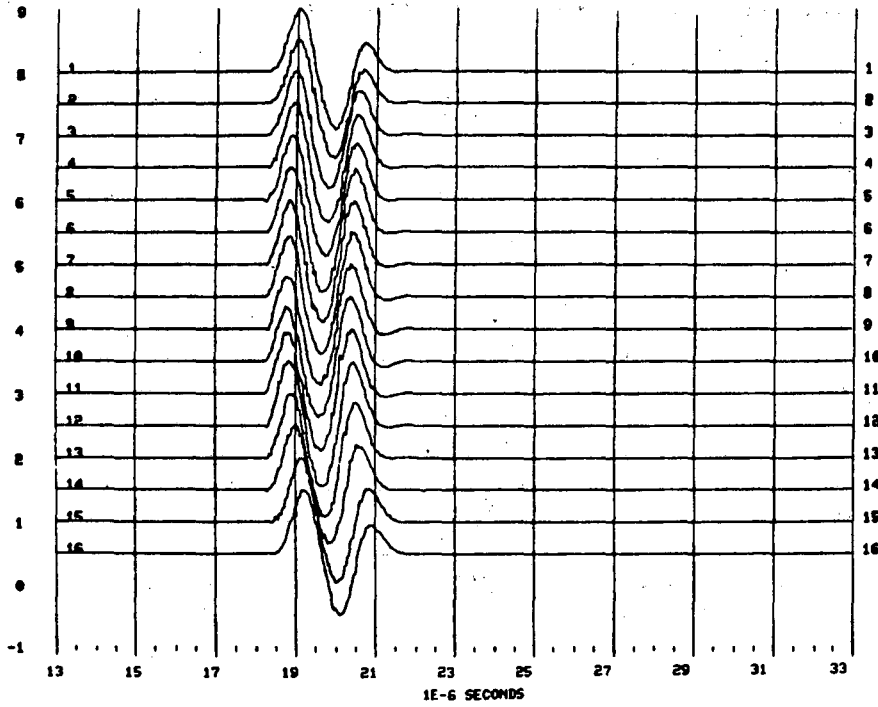
Fig. E:4.11d Truncated S waveforms as function of uniaxial stress for the saturated specimen # 11



STRIPA 81, P-WAVES TRUNCATED WITH 4E-6 SEC TAPER, NS-NS, 820822 Fig. E:4.1a



STRIPA 81, TRUNCATED WITH 4E-6, SATURATED, 820831 Fig. E:4.1b



STRIPA 81, TRUNCATED S-WAVES WITH  $1 \times 10^{-6}$  SEC WIND, DRY, RB-R6, 821019

Fig. E:4.1c

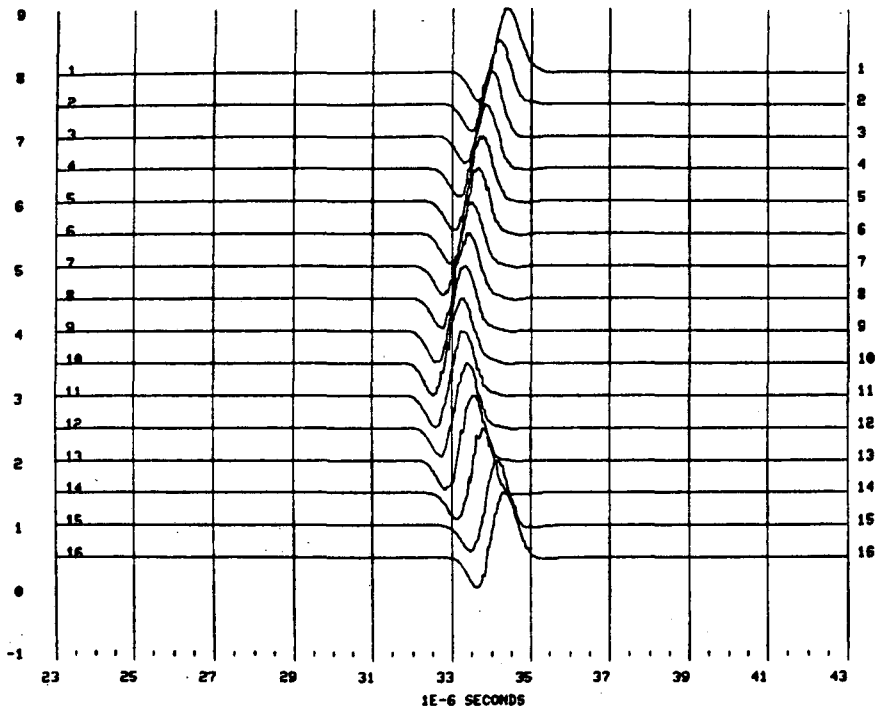
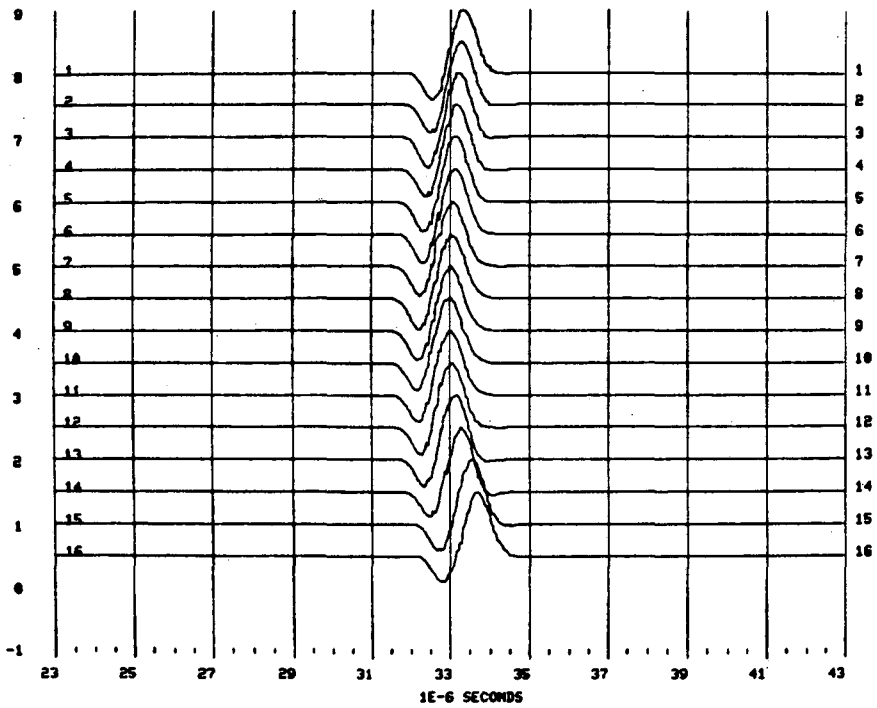
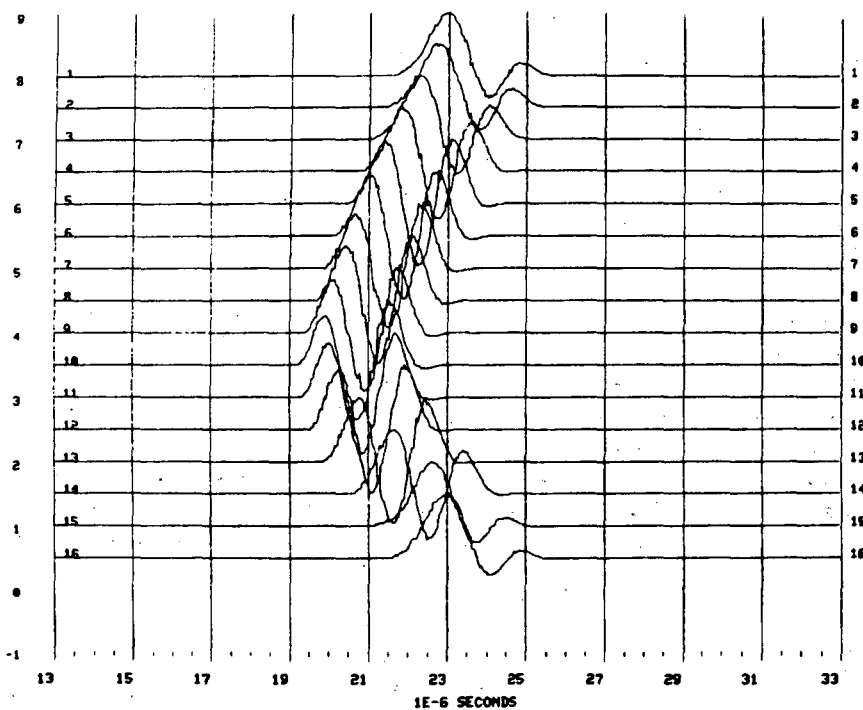
STRIPA 81, S-WAVES TRUNCATED WITH  $1 \times 10^{-6}$  SEC WIND, SATURATED, RB-R6, 821019

Fig. E:4.1d



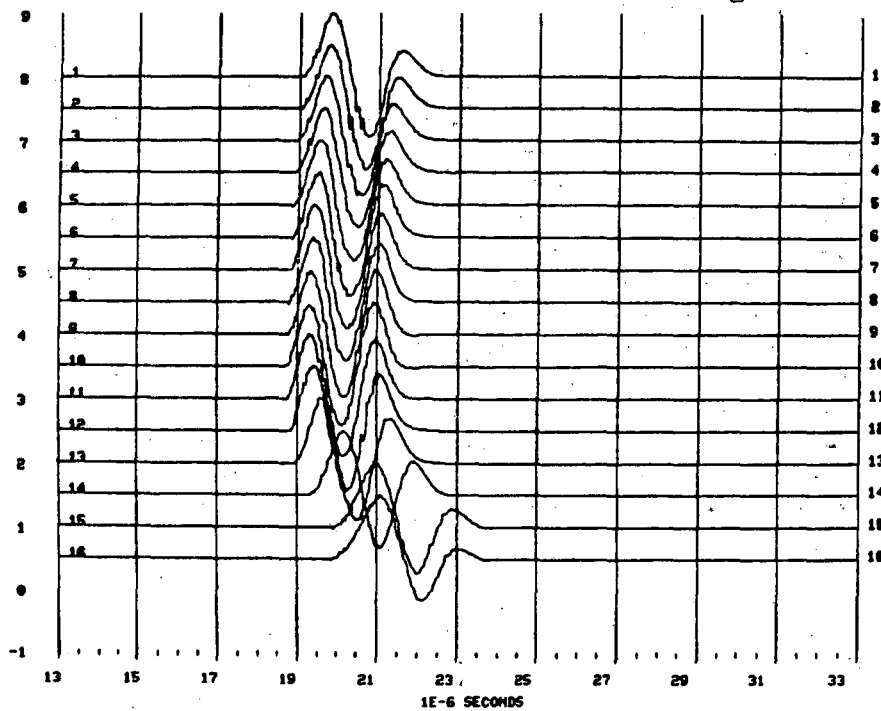
STRIPA 82, P-WAVES TRUNCATED WITH  $4E-6$  SEC. DRY SPECIMEN, 821827

Fig. E:4.2a



STRIPA 82, TRUNCATED P-WAVES, SATURATED SPECIMEN, 820831

Fig. E:4.2b



STRIPA 82, S-WAVES TRUNCATED WITH  $1 \times 10^{-6}$  SEC WIND, DRY, M7-ND, 821029

Fig. E:4.2c

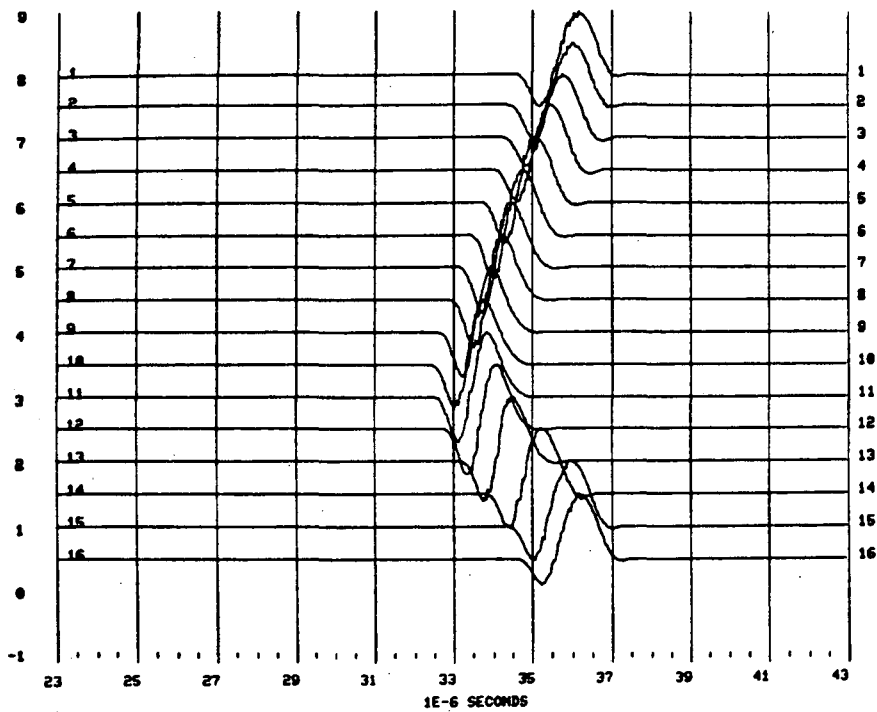
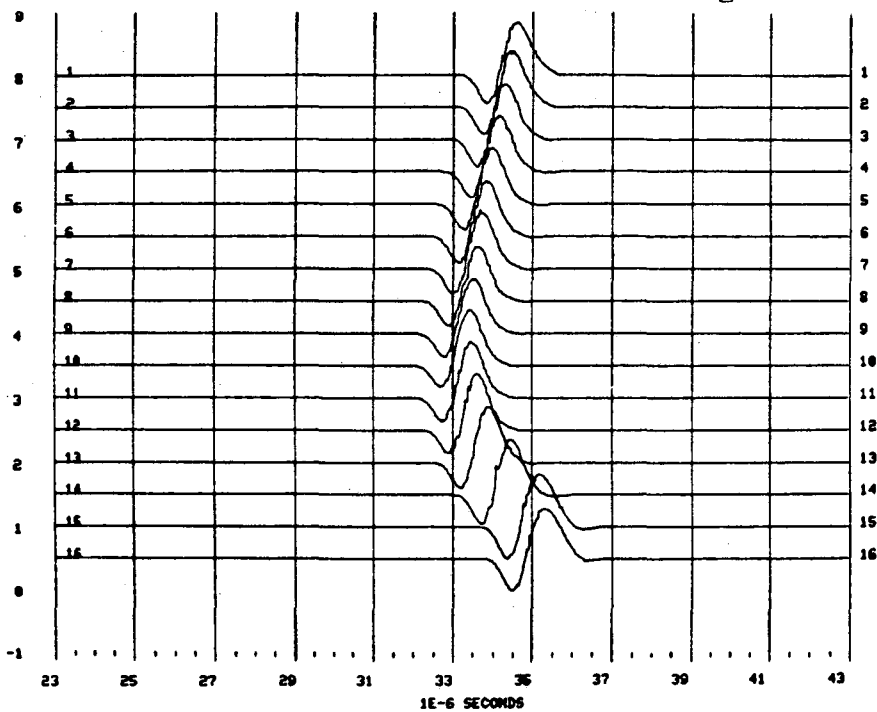
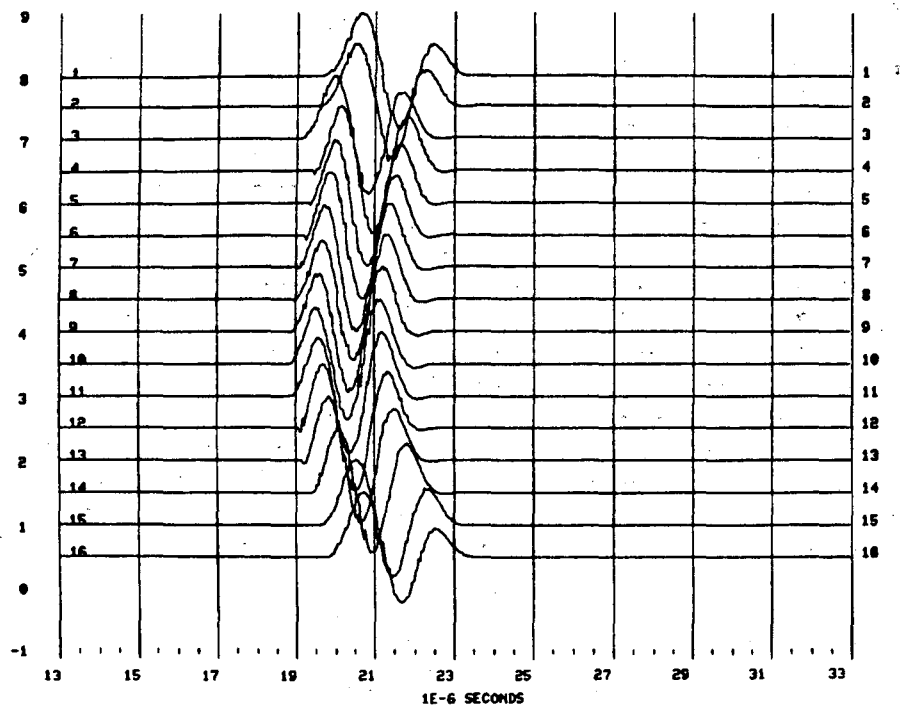
STRIPA 82, S-WAVES TRUNCATED WITH  $1 \times 10^{-6}$  SEC WIND, SATURATED, 821019

Fig. E:4.2d



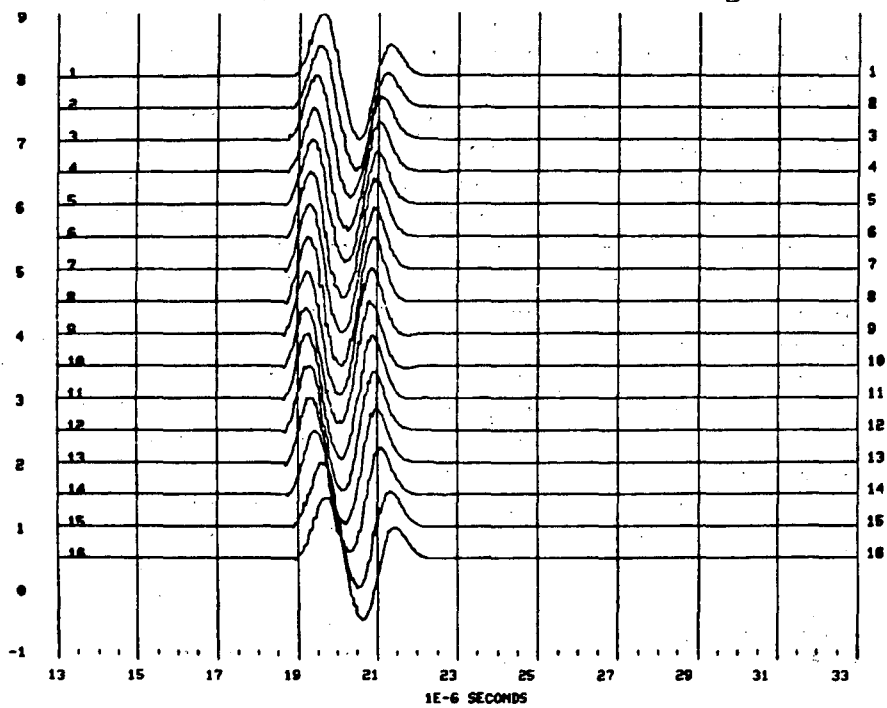
STRIPA SPECIMEN 83, M18, E29, DRY

Fig. E:4.3a



STRIPA 83, TRUNCATED P-WAVES, 4E-6 SEC WINDOW, SATURATED, 828802

Fig. E:4.3b



STRIPA 03, S-WAVES TRUNCATED WITH  $1 \times 10^{-6}$  SEC WIND, E29/H10, 821019

Fig. E:4.3c

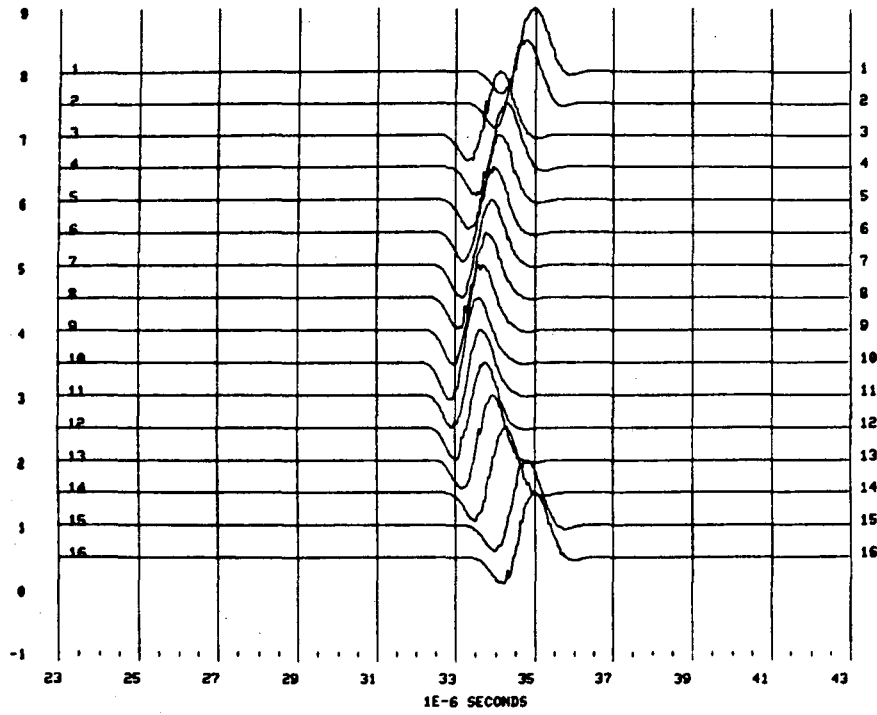
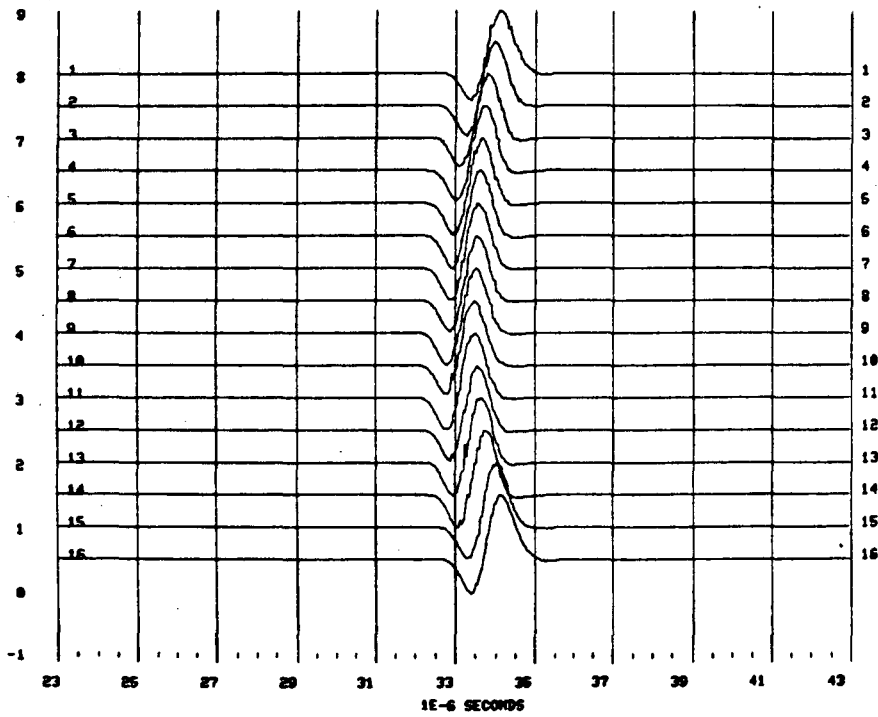
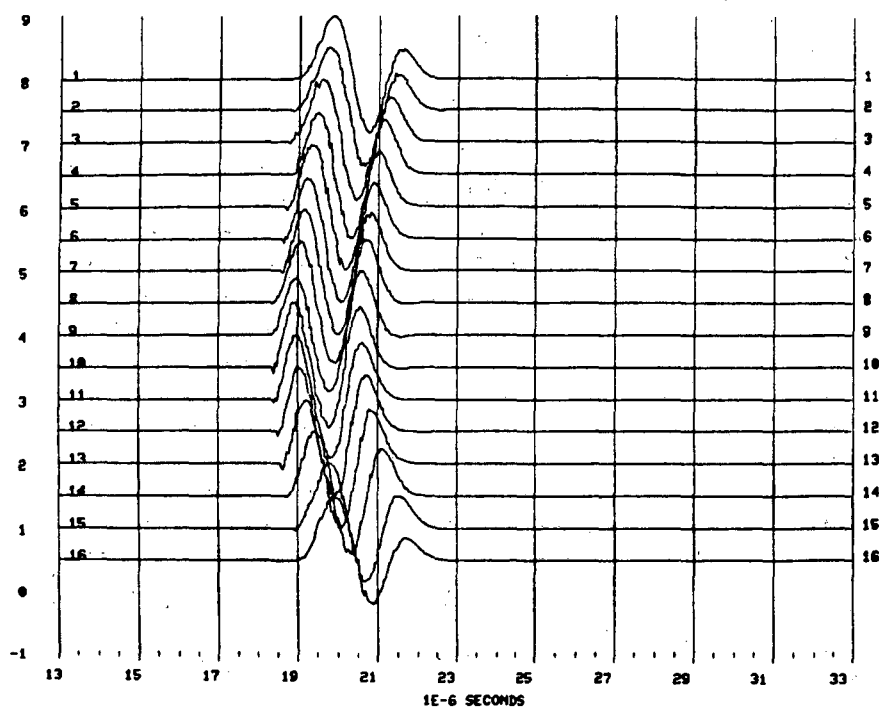
STRIPA 03, S-WAVES TRUNCATED WITH  $1 \times 10^{-6}$  SEC WIND, SATURATED, H10/E29, 821020

Fig. E:4.3d



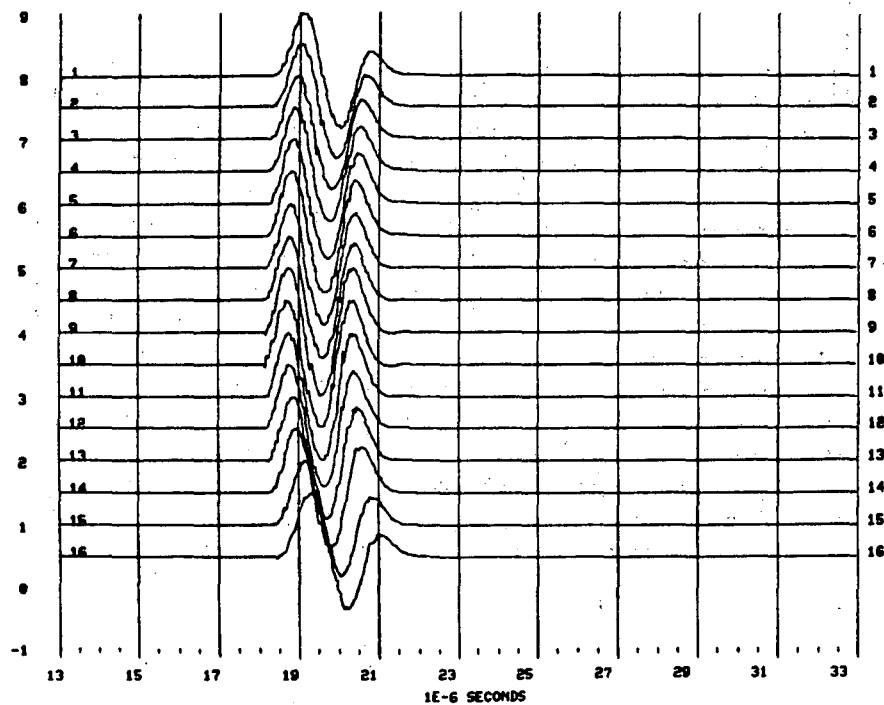
STRIPA #4, DRILLBACK 1.45 F H10, DRY

Fig. E:4.4a

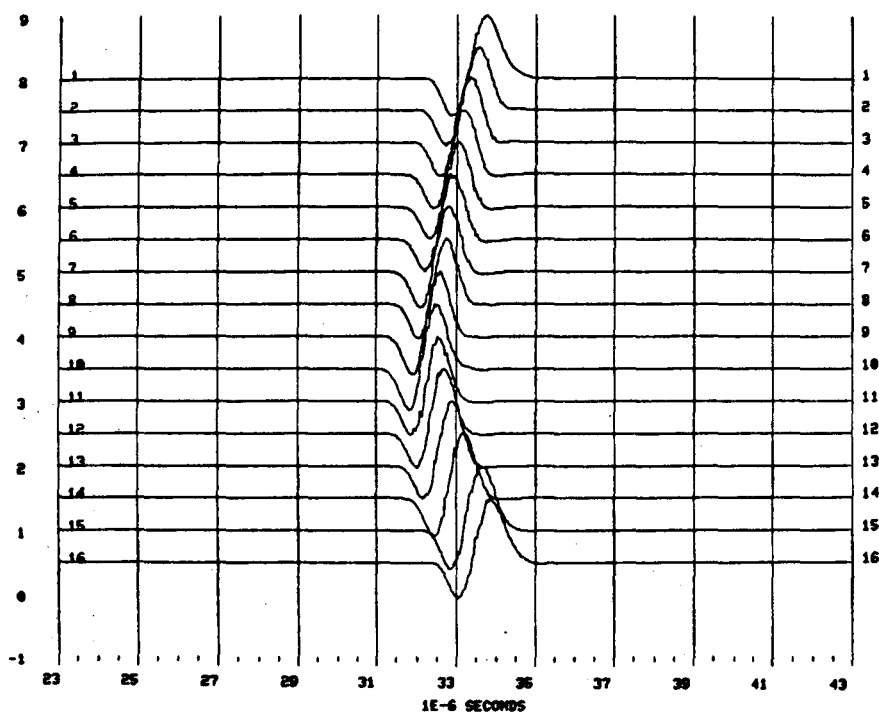


STRIPA #4, P-WAVES, TRUNCATED WITH 4E-6 SEC COS. 820902

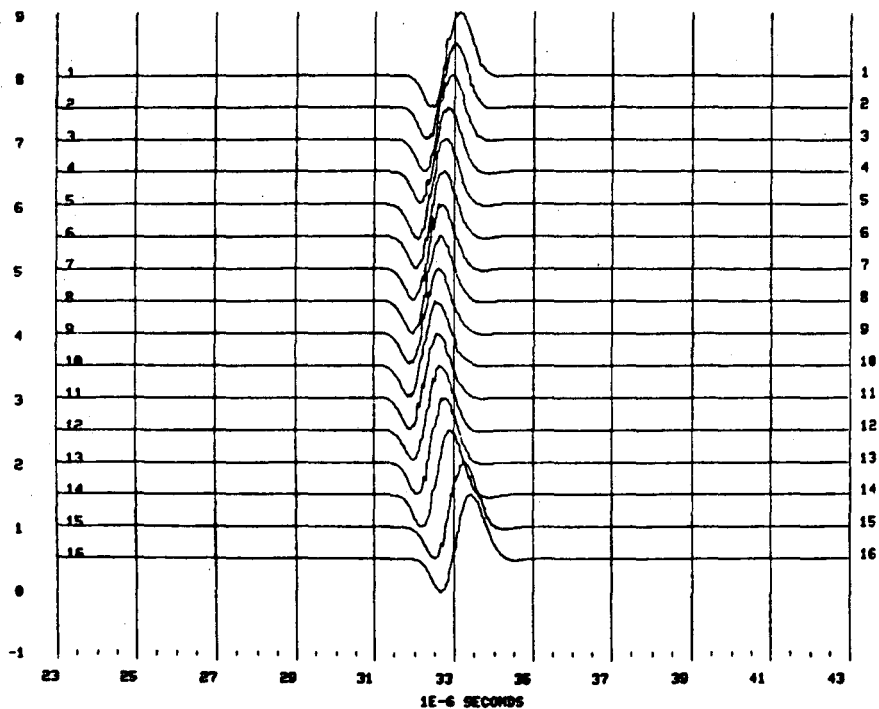
Fig. E:4.4b



STRIPA 04, S-WAVES TRUNC. WITH 1+2E-6 SEC WIND, DBEX-1 1.45 M FROM H10, 130 C Fig. E:4.4c



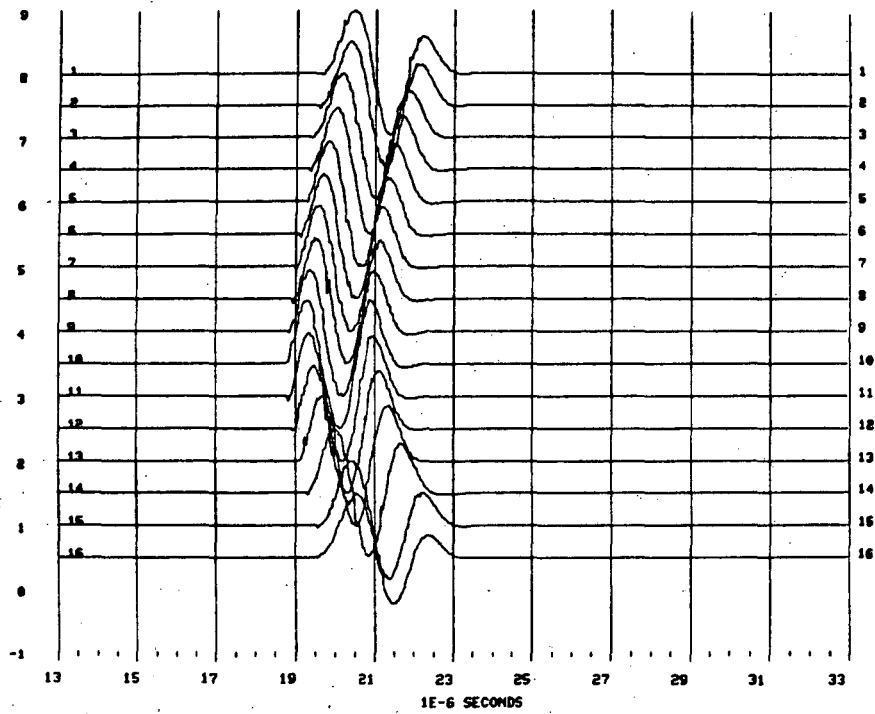
STRIPA 04, S-WAVES TRUNC. WITH 1+2E-6 SEC WIND, SATURATED, DBEX-1 1.45 F. H10, 130 Fig. E:4.4d





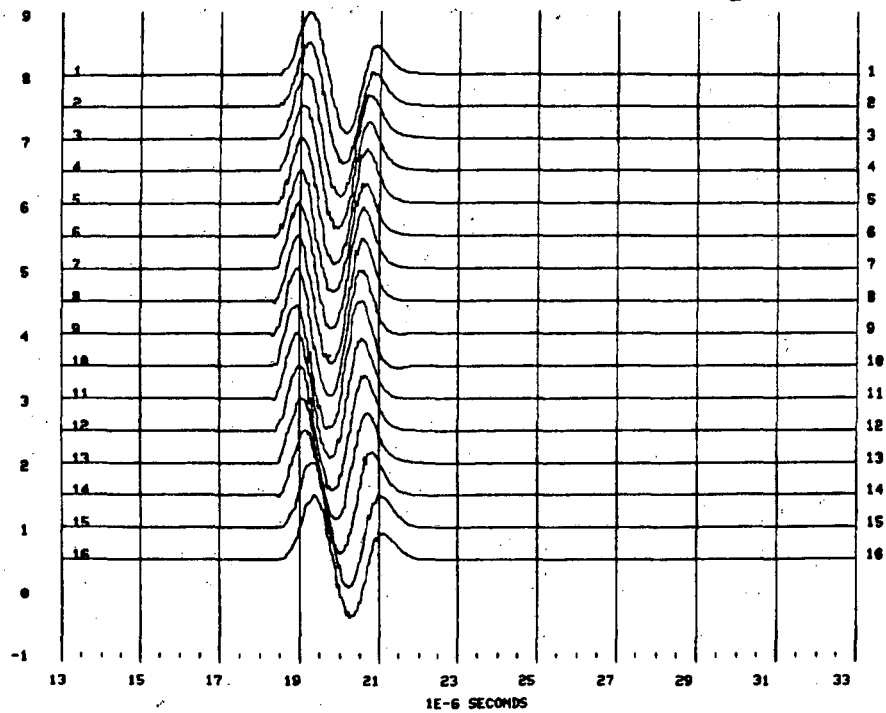
STRIPA 05, TRUNCATED P-WAVES WITH 4E-6 SEC, DRILLBACK 1 0.75 M FROM H10, 800C, 821025

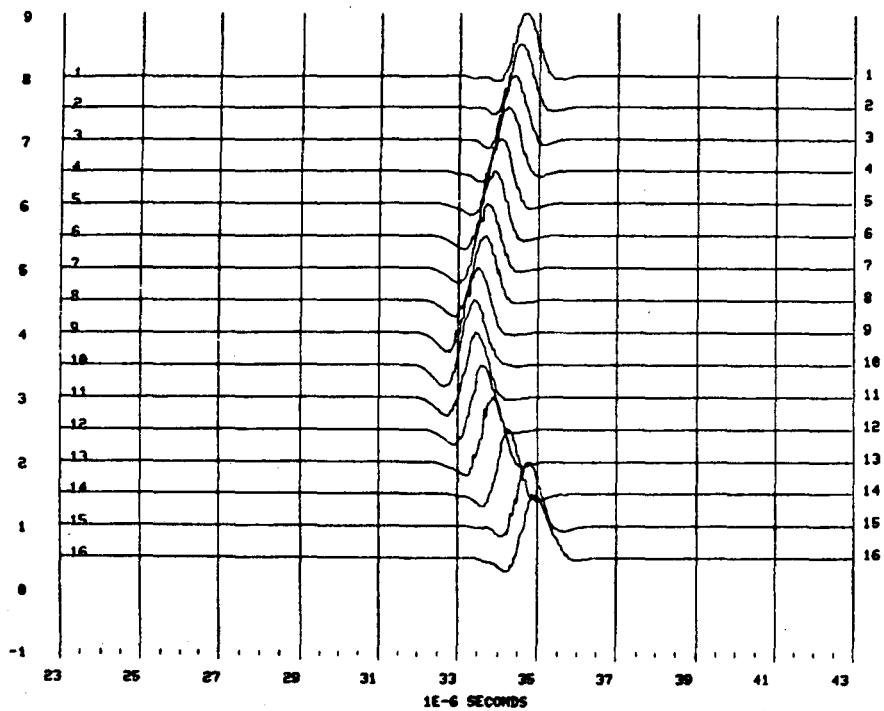
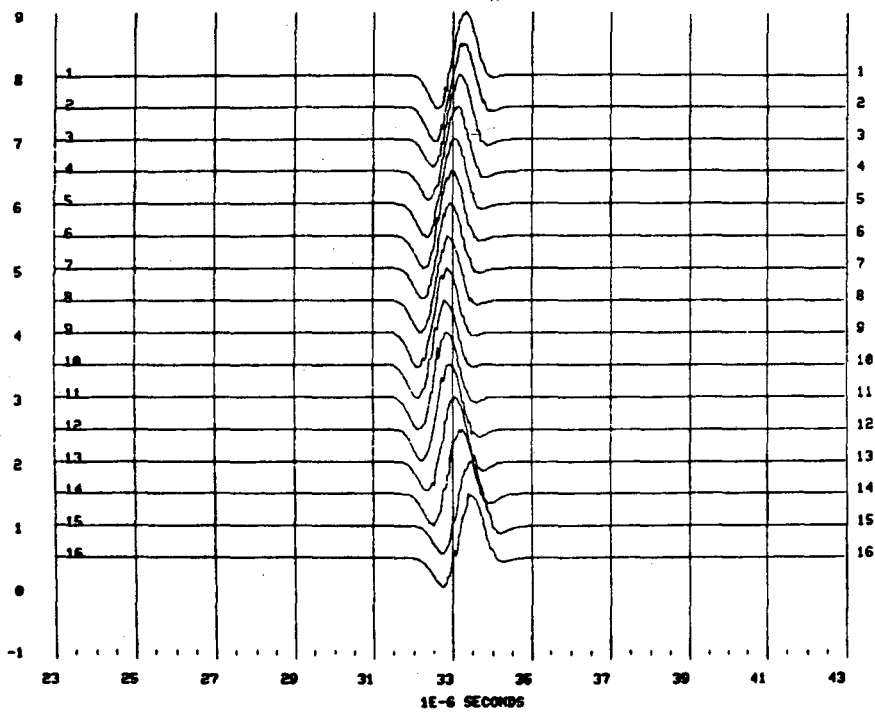
Fig. E:4.5a



STRIPA 05, TRUNCATED P-WAVES WITH 4E-6 SEC, DRILLBACK 0.75M FROM H10, 82000

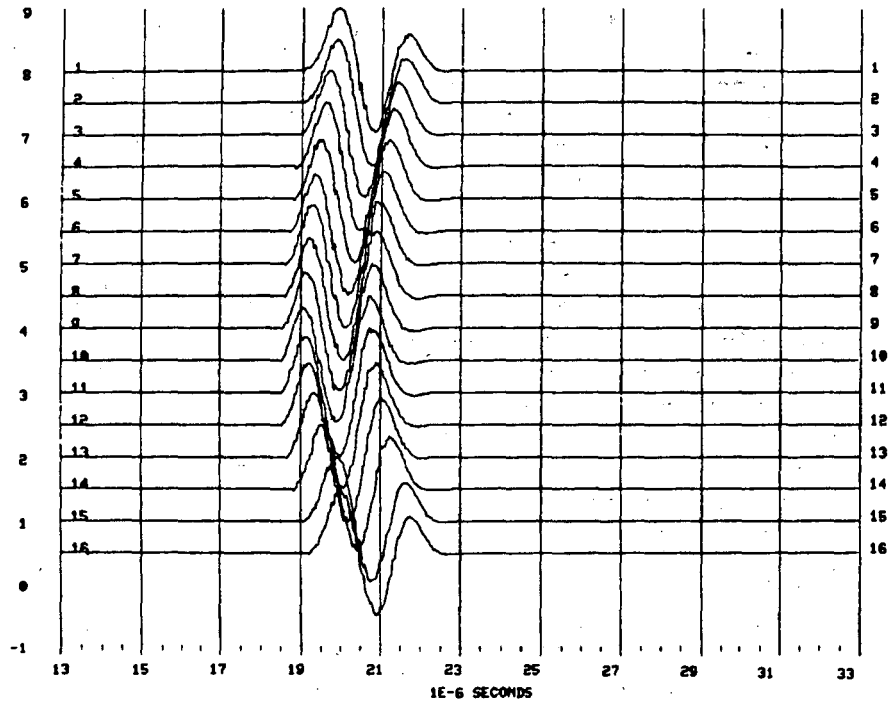
Fig. E:4.5b



STRIPA 85, S-WAVES TRUNCATED WITH  $1 \times 10^{-6}$  SEC WIND, DBEX-1 0.75 M FROM H10, DRY Fig. E:4.5cSTRIPA 85, S-WAVES TRUNCATED WITH  $1 \times 10^{-6}$  SEC WIND, DBEX-1 0.75 F. H10, 200 C Fig. E:4.5d

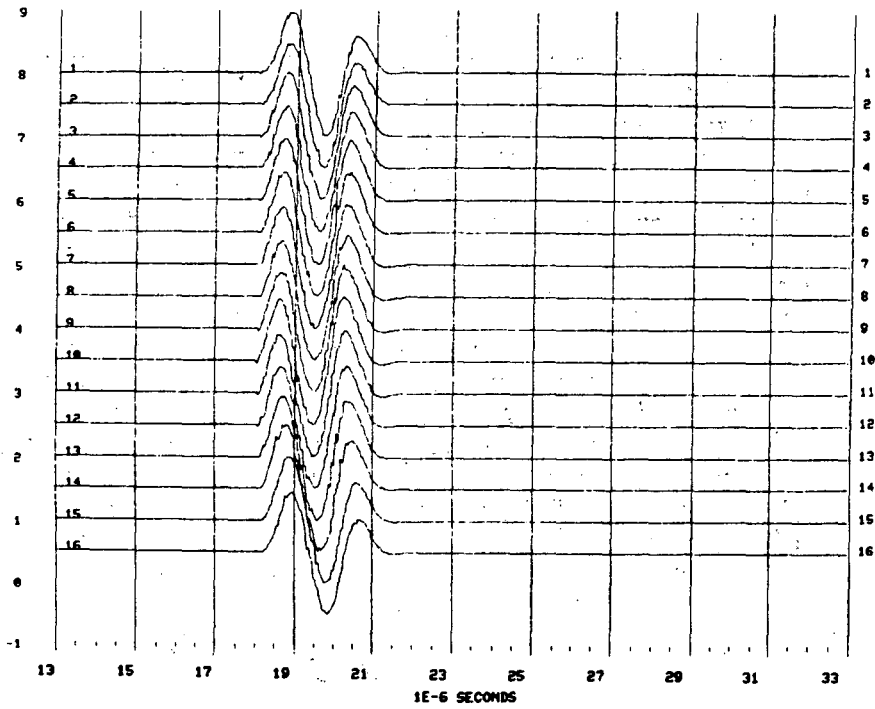
STRIPA 86, P-WAVES TRUNCATED WITH 4E-6, MB-M6, 820922

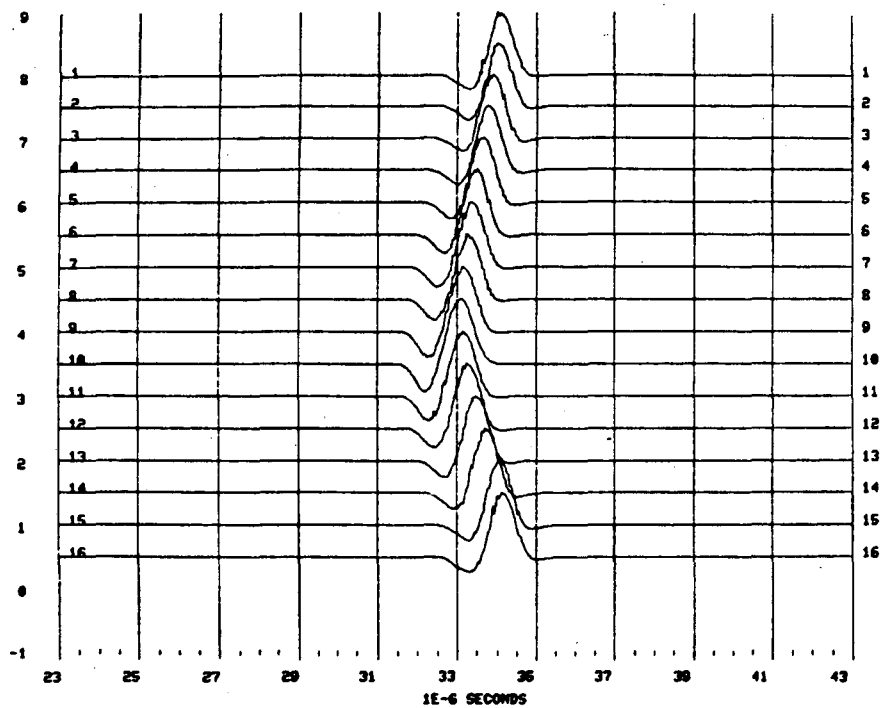
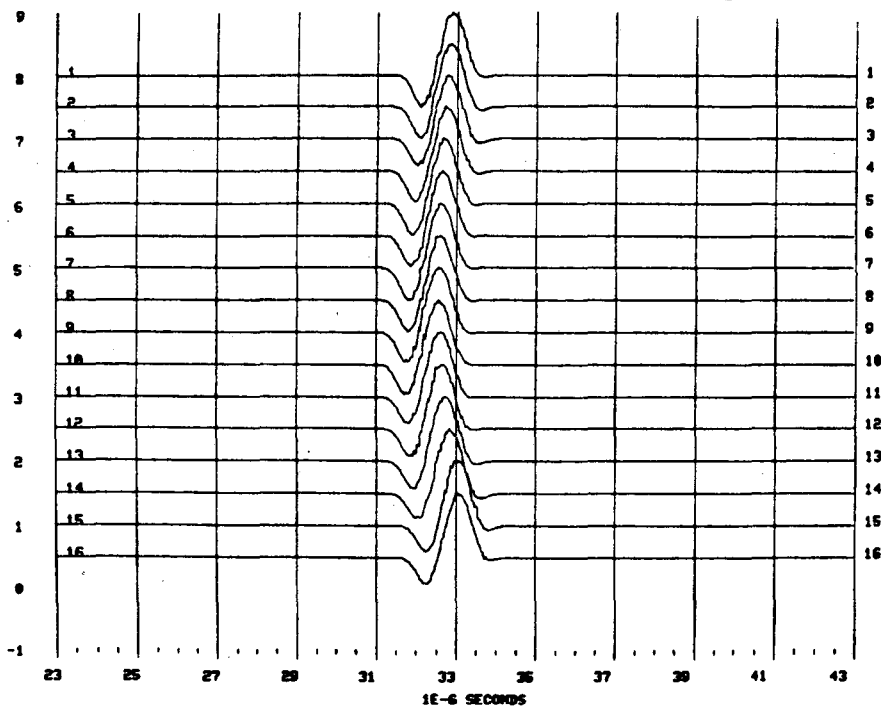
Fig. E:4.6a



STRIPA 86, P-WAVES, SATURATED, TRUNCATED WITH 4E-6, 821001

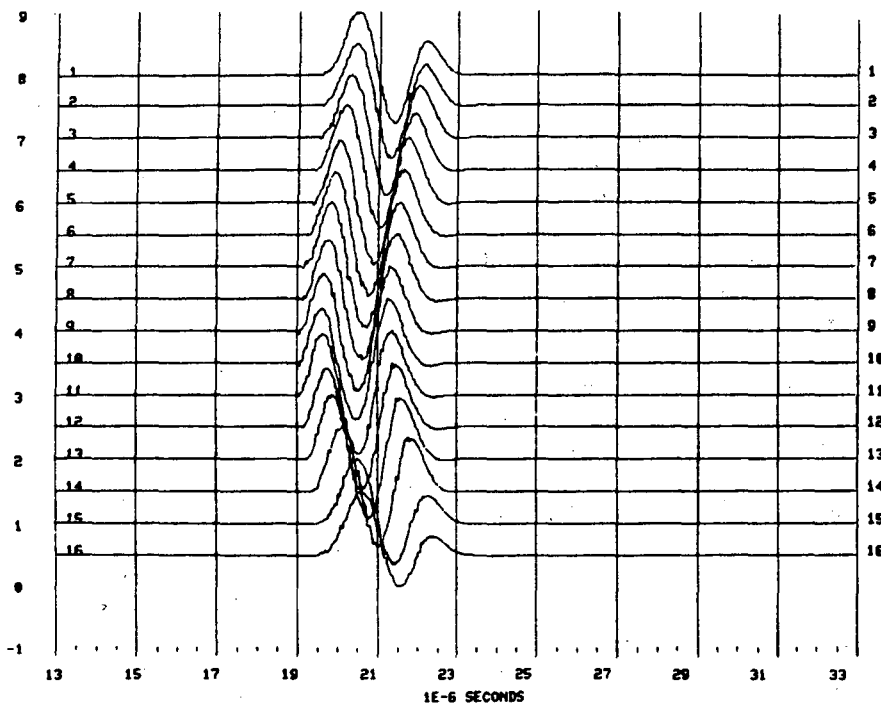
Fig. E:4.6b



STRIPA 86, S-WAVES TRUNCATED WITH  $1 \times 10^{-6}$  SEC WINDOW, E22, M8-46, DRY, 821020 Fig. E:4.6cSTRIPA 86, TRUNCATED S-WAVES WITH  $1 \times 10^{-6}$  SEC WINDOW, SATURATED, 821003 Fig. E:4.6d

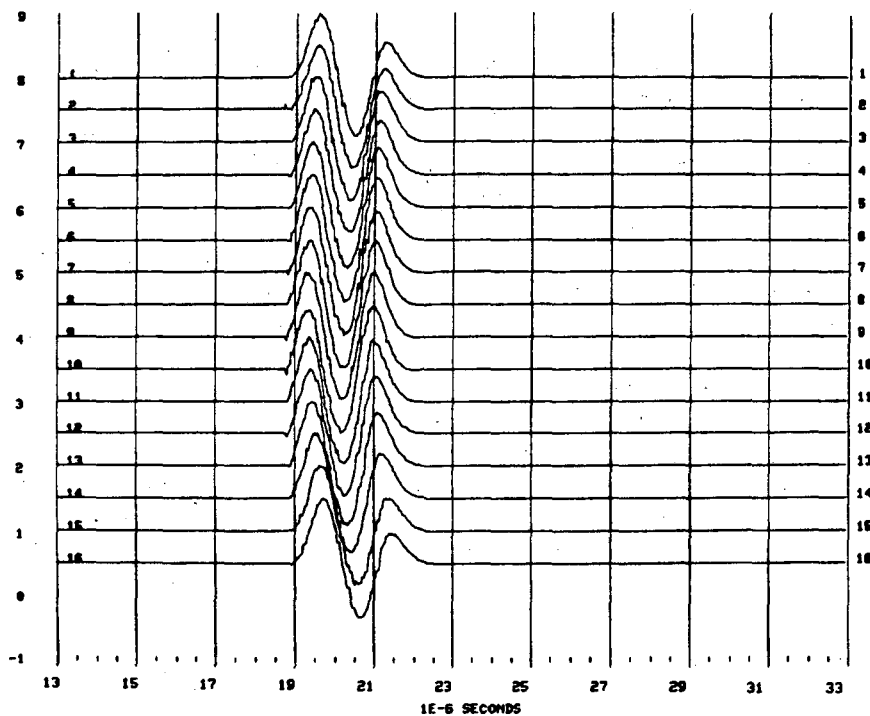
STRIPA 97, P-WAVES, DRY, NB-N6, TRUNCATED WITH 4E-6 SEC. 820981

Fig. E:4.7a



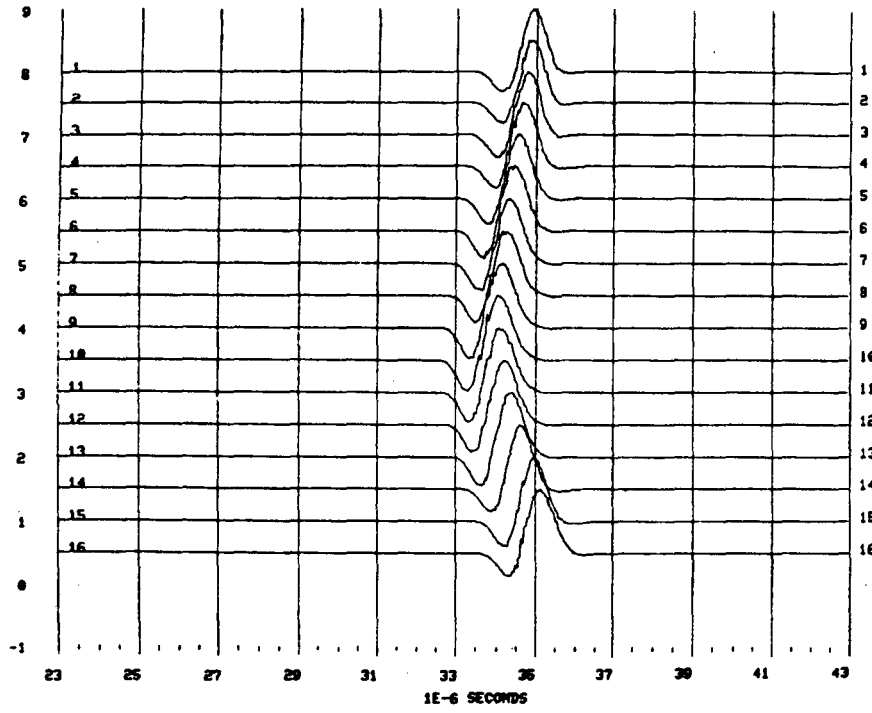
STRIPA 97, TRUNCATED P-WAVES WITH 4E-6 SEC WIND, NB-N6, 821003

Fig. E:4.7b



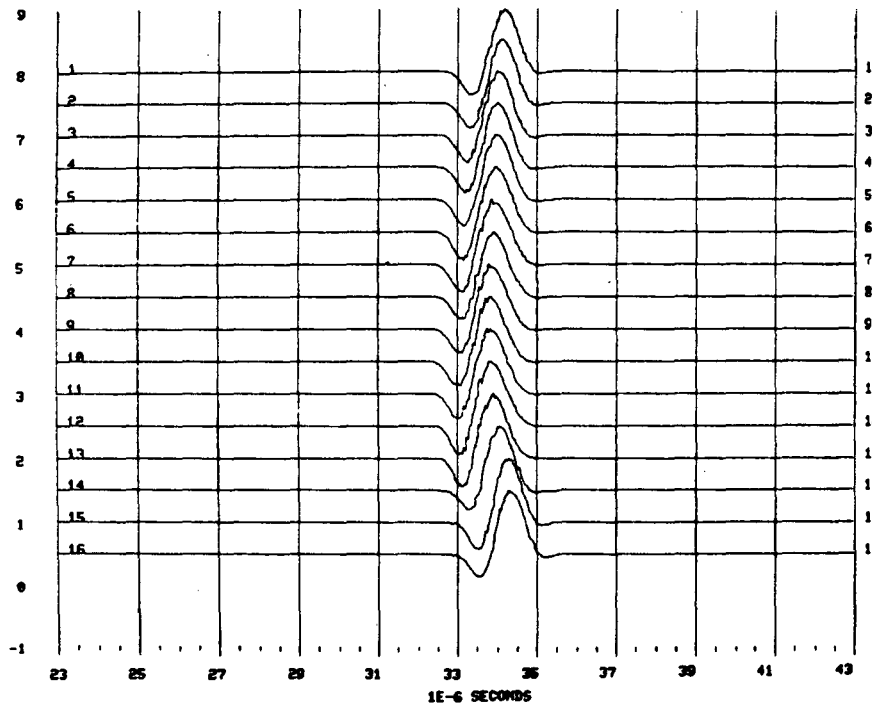
STRIPA 87, S-WAVES TRUNC. WITH 1+2E-6 SEC WIND, DRY, E22, R8-R6, 821020

Fig. E:4.7c



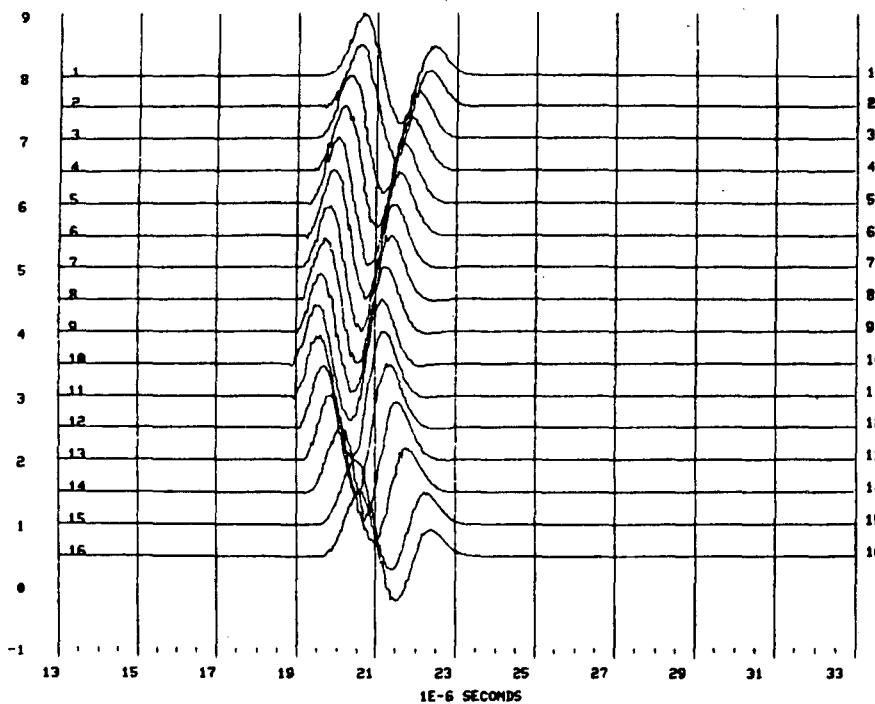
STRIPA 87, TRUNCATED S-WAVES WITH 1+2E-6 SEC WIND., SATURATED, 821003

Fig. E:4.7d



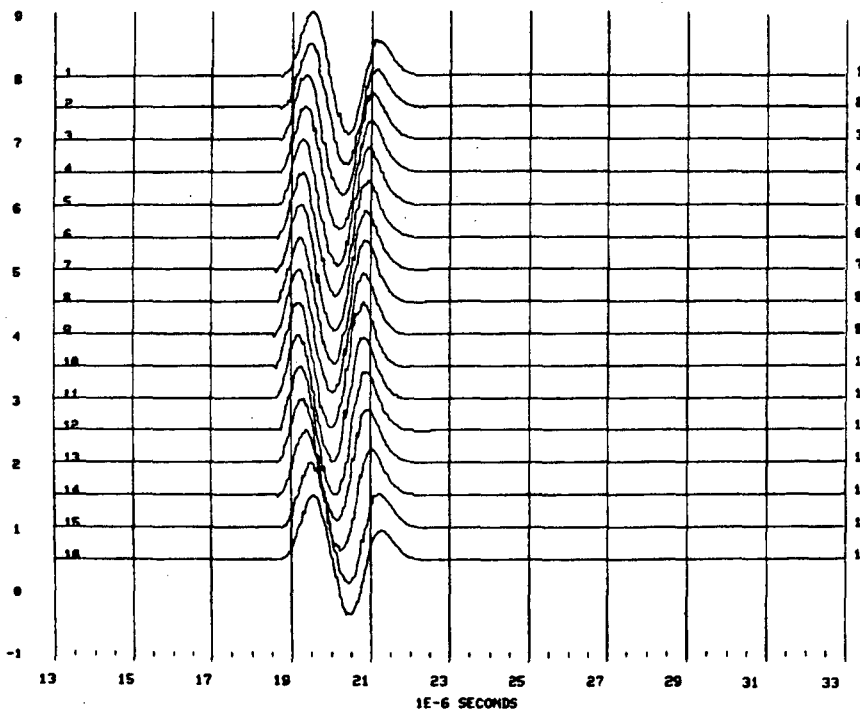
STRIPA 88, TRUNCATED P-WAVES 4E-6 SEC, DRY, 820921

Fig. E:4.8a



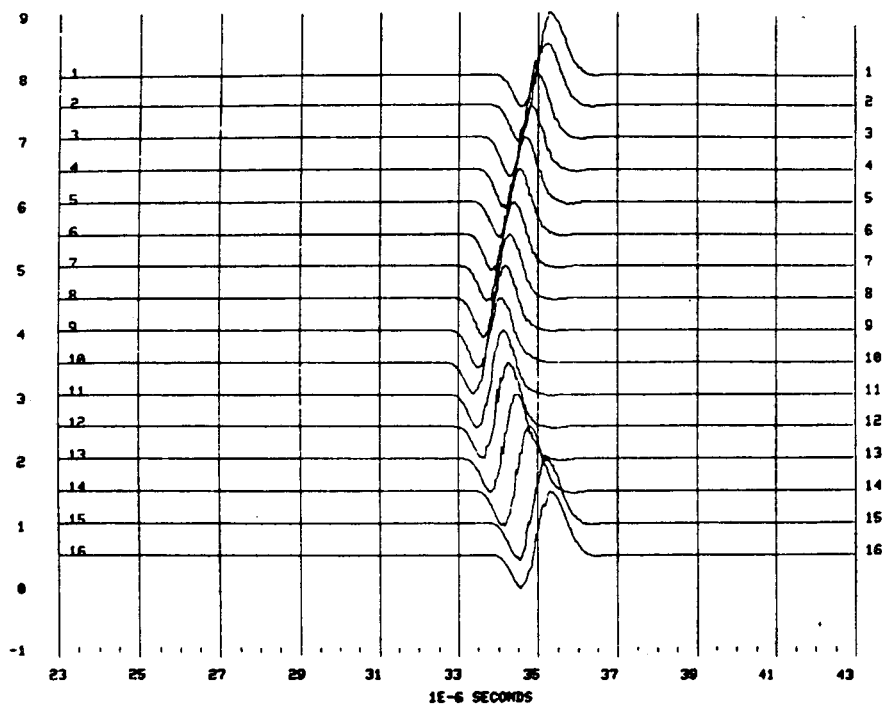
STRIPA 88, SATURATED, TRUNCATED P-WAVES WITH 4E-6 SEC WIND, 821003

Fig. E:4.8b



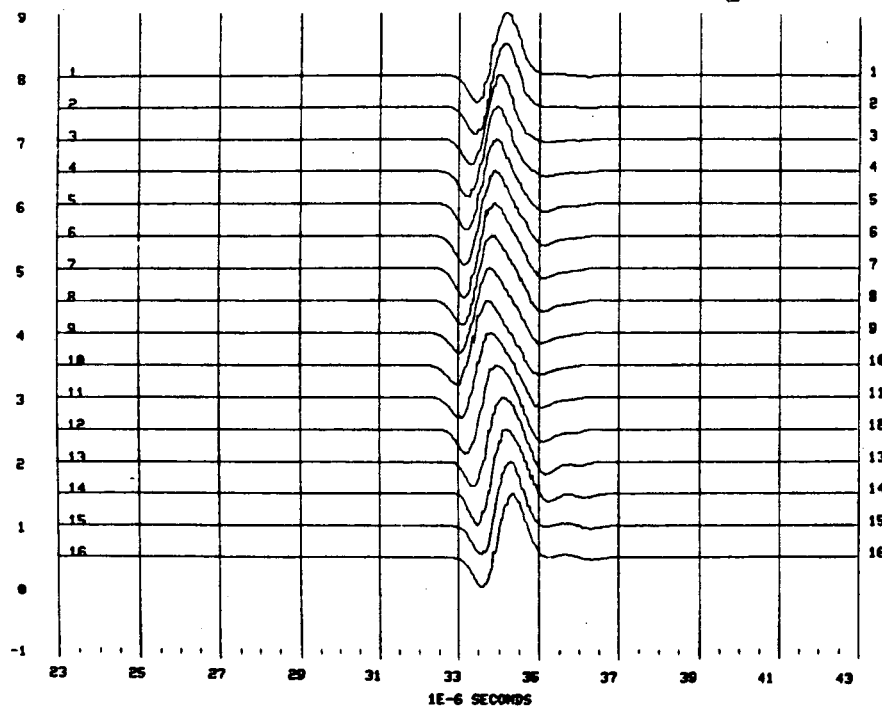
STRIPA 88, S-WAVES TRUNCATED WITH 1+2E-6 SEC, DRY, E22, M8-M6, 821020

Fig. E:4.8c



SSTRIPA 88, S-WAVES TRUNCATED WITH 1+2E-6 SEC WIND, SATURATED 8201003

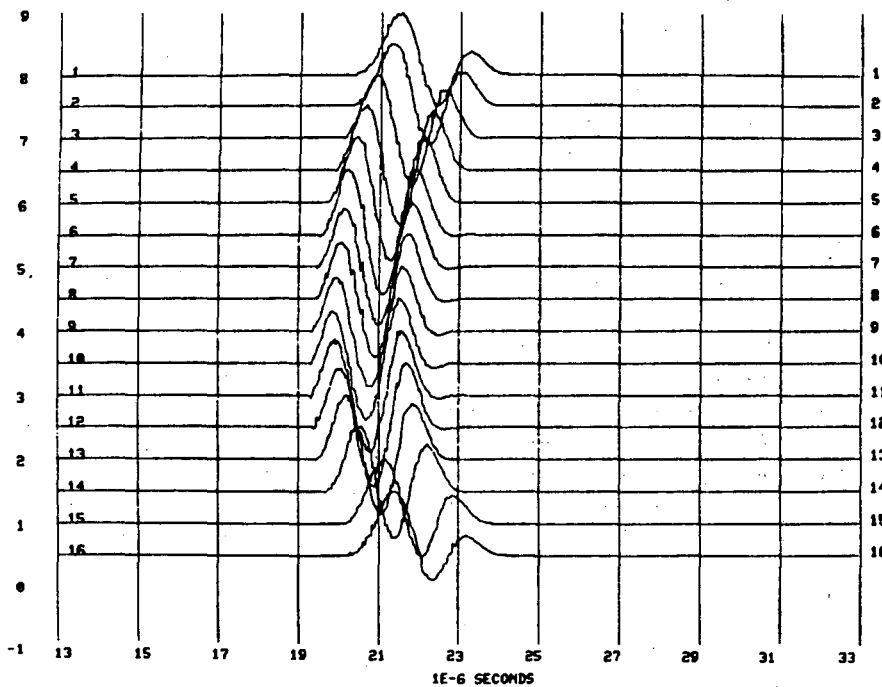
Fig. E:4.8d





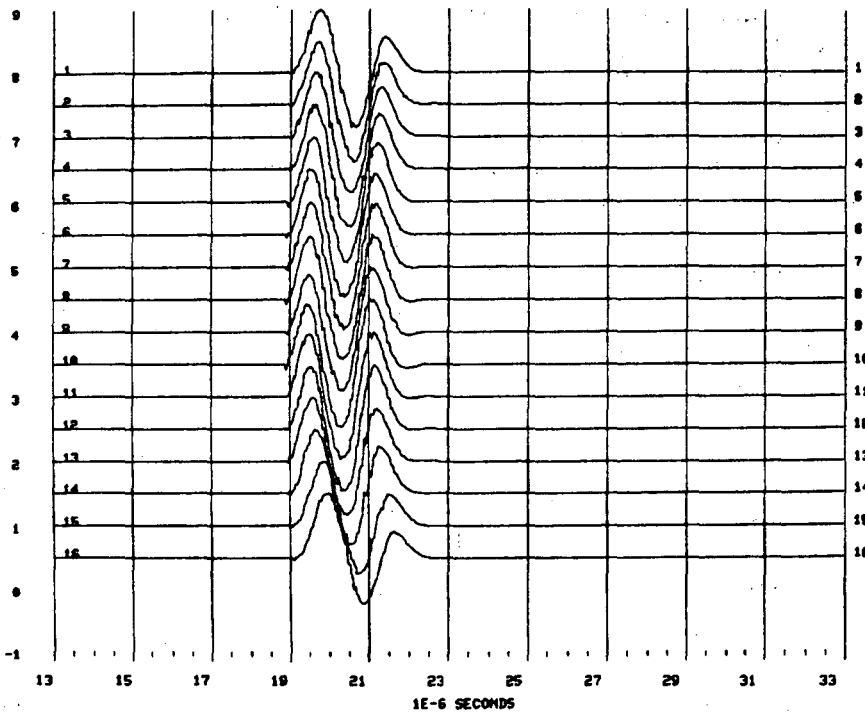
STRIPA 89, TRUNCATED P-WAVES WITH 4E-6 SEC. DRY, 820021

Fig. E:4.9a



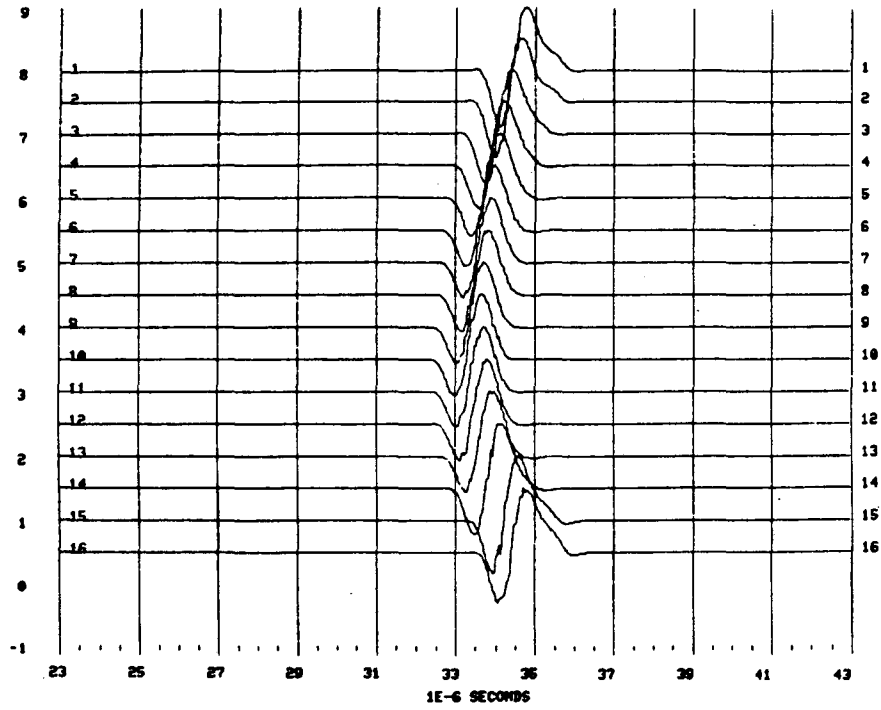
STRIPA 89, TRUNCATED P-WAVES WITH 4E-6 SEC WIND, SATURATED, 87-NO. 821003

Fig. E:4.9b



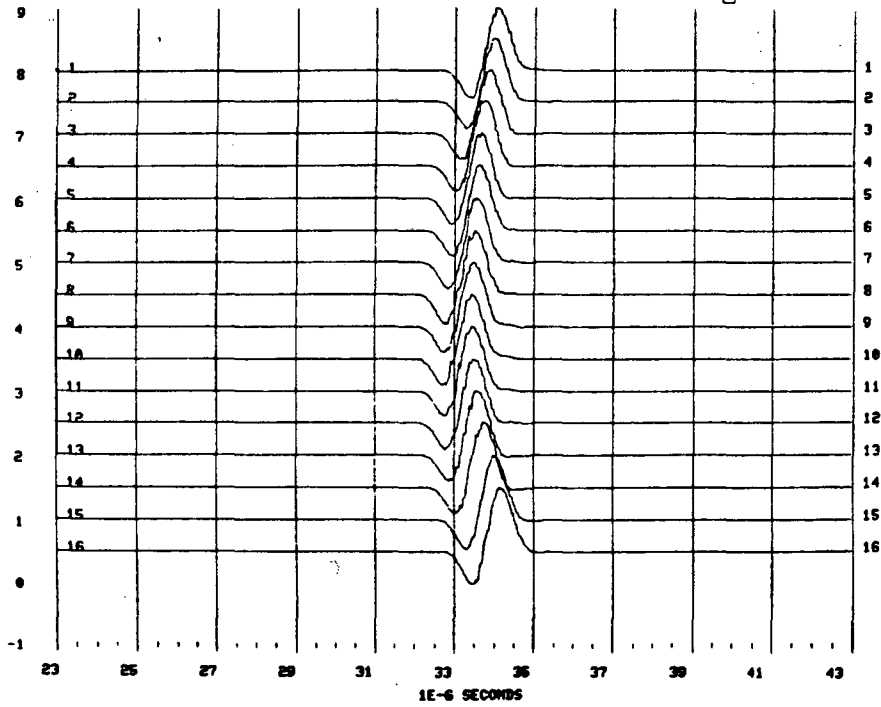
STRIPA 89, S-WAVES TRUNCATED WITH  $1.2E-6$  SEC WIND, DRY, E25, R7-R9

Fig. E:4.9c



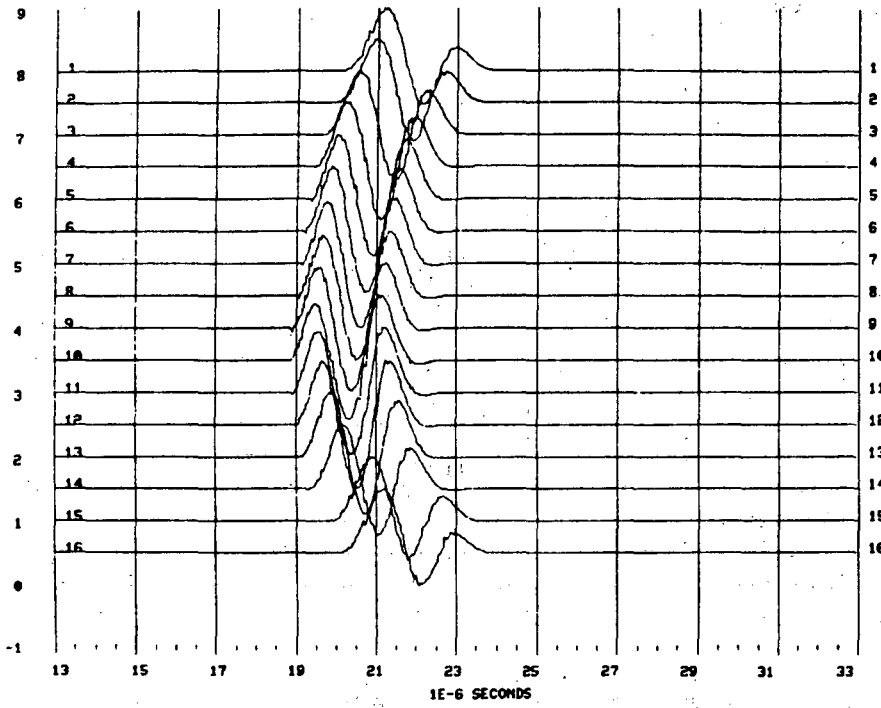
STRIPA 89, S-WAVES TRUNCATED WITH  $1.2E-6$  SEC WIND, SATURATED, 821003

Fig. E:4.9d



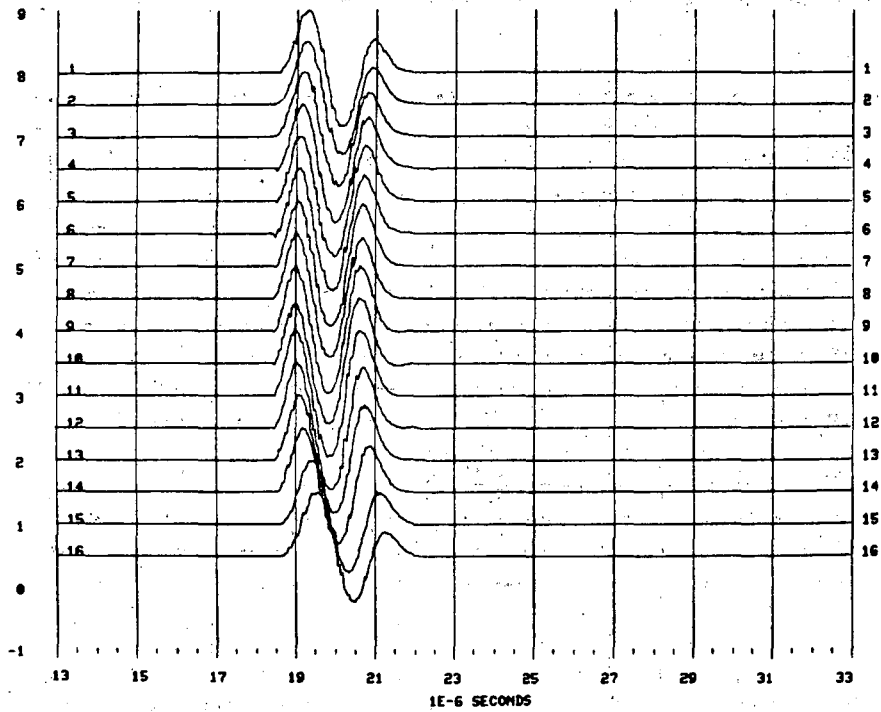
STRIPA 810, TRUNCATED P-WAVES 4E-6 SEC, N7-M9, 820921

Fig. E:4.10a



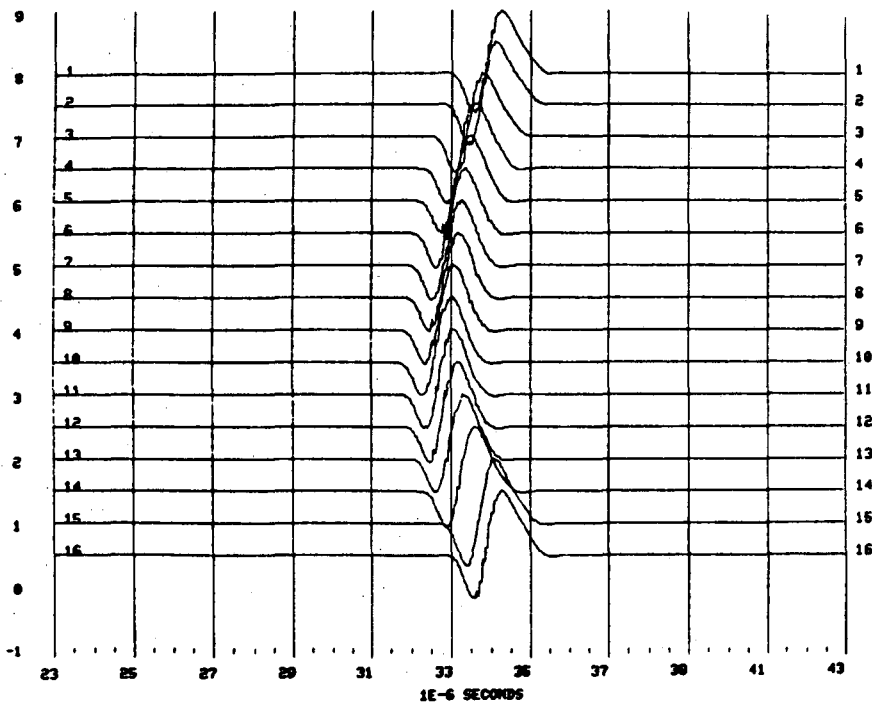
STRIPA 810, TRUNCATED P-WAVES WITH 4E-6 SEC WIND., SATURATED, N7-M9, 821003

Fig. E:4.10b



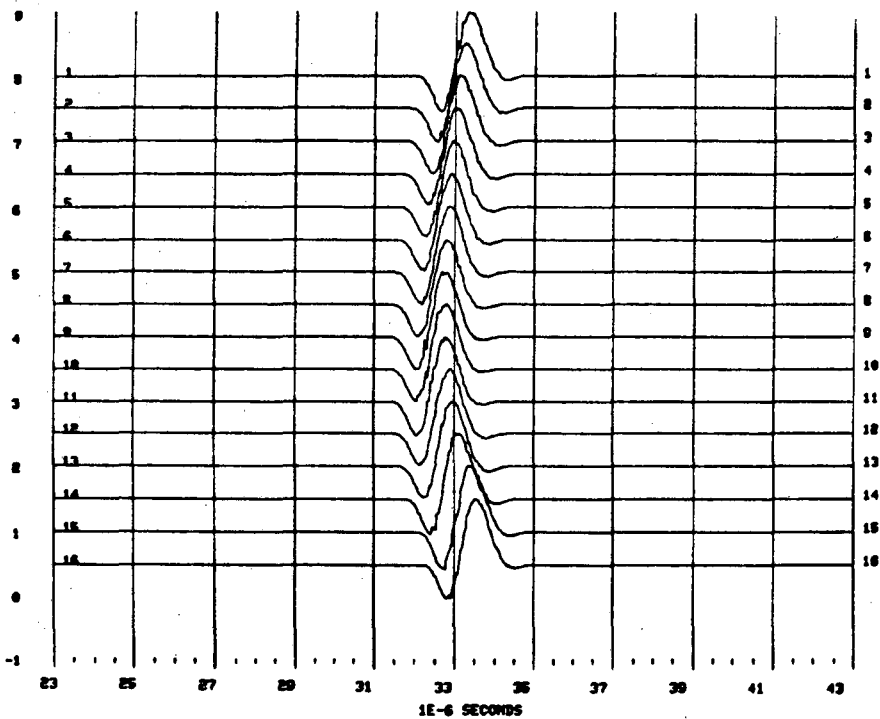
STRIPA 810, S-WAVES TRUNCATED WITH 1\*2E-6 SEC WIND, DRY, E25, 821020

Fig. E:4.10c



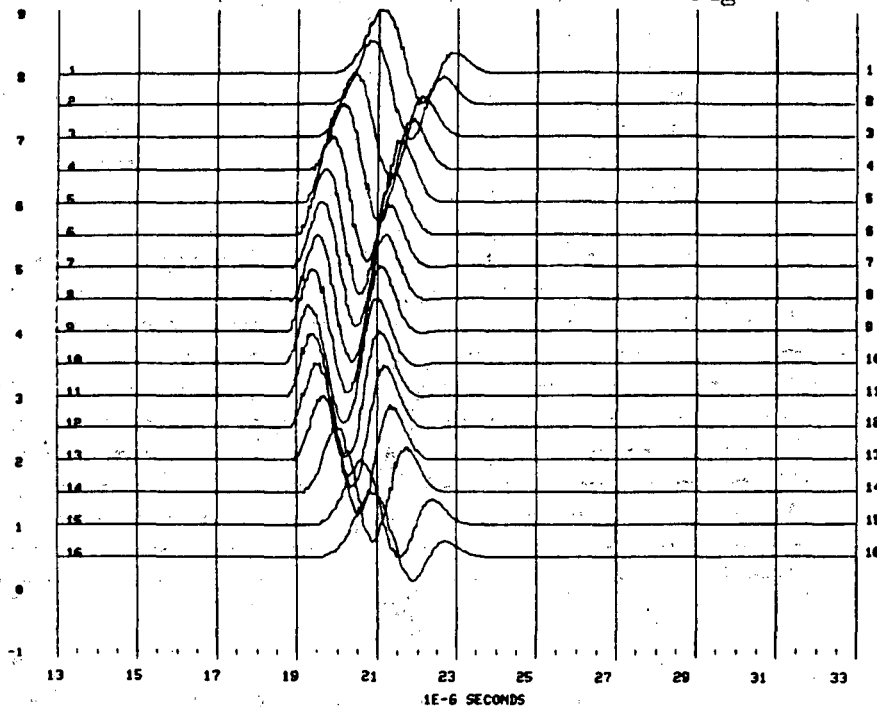
STRIPA 810, S-WAVES TRUNCATED WITH 1\*2E-6 SEC WIND, SATURATED, 821003

Fig. E:4.10d



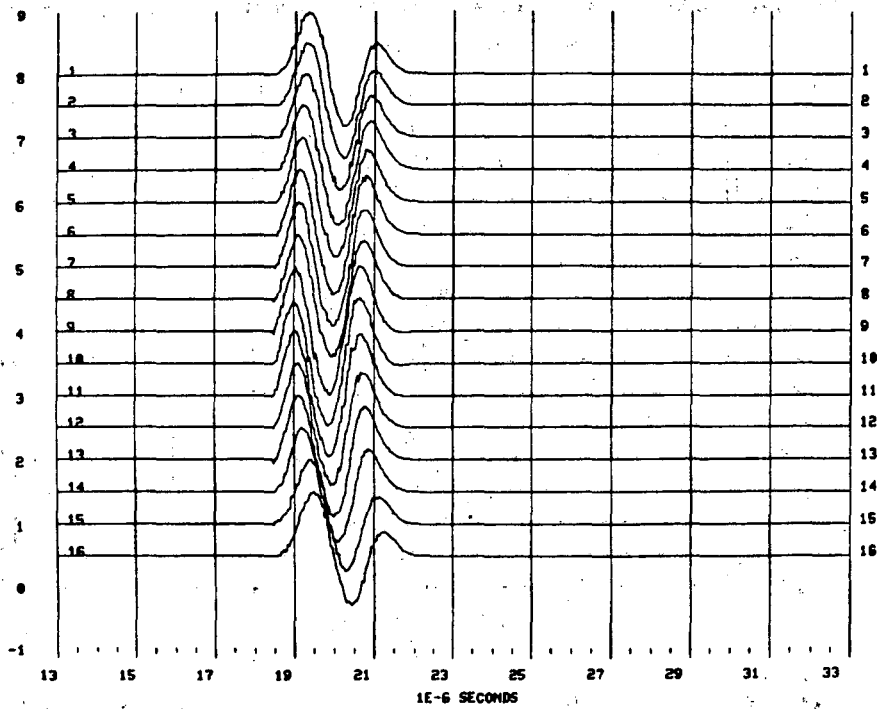
STRIPA 811, TRUNCATED P-WAVES WITH 4E-6, N7-ND, 880081

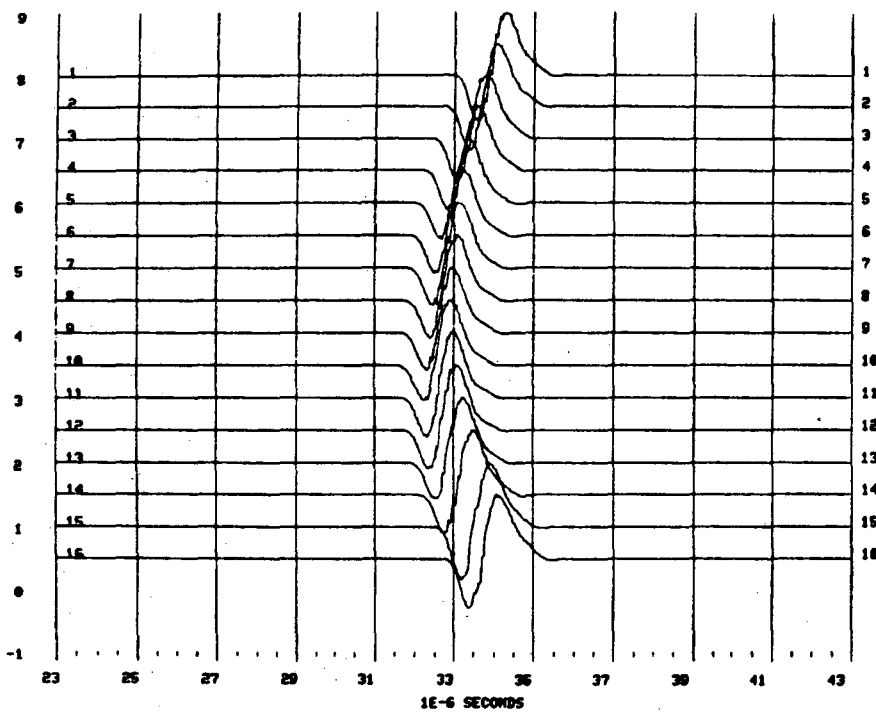
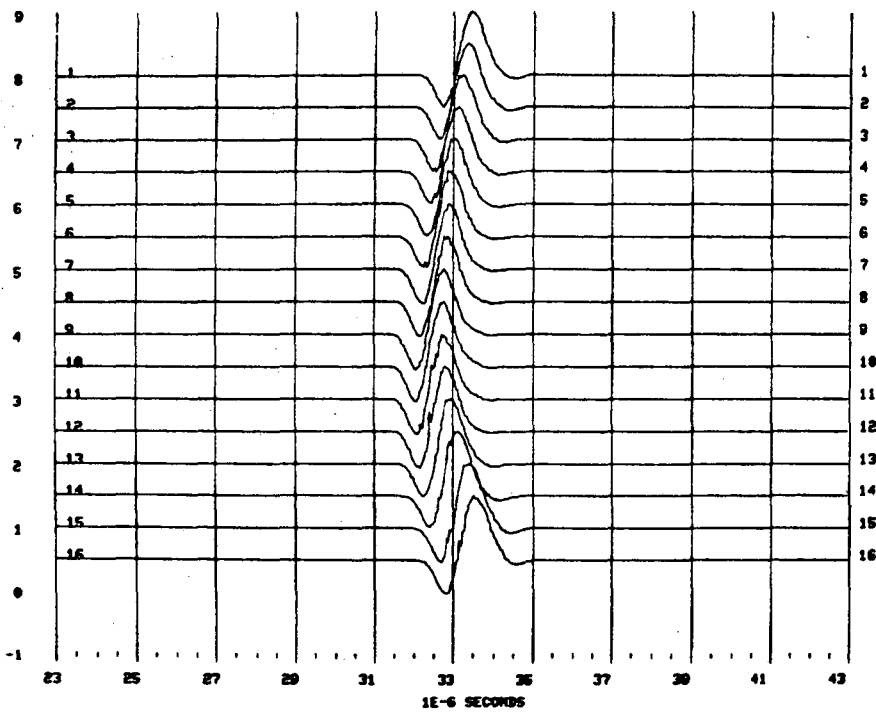
Fig. E:4.11a



STRIPA 811, TRUNCATED P-WAVES WITH 4E-6 SEC WIND., SATURATED, N7-ND, 821003

Fig. E:4.11b



STRIPA 811, N7-M9, 5-WAVES TRUNCATED WITH  $1+2E-6$  SEC AT CROSSOVER, 820923 Fig. E:4.11cSTRIPA 811, 5-WAVES TRUNCATED WITH  $1+2E-6$  SEC WIND, SATURATED, 821003 Fig. E:4.11d

## Appendix E:5 - Fourier Amplitude spectra for P and S waves from laboratory test.

In this appendix the Fourier amplitude spectra for the truncated P and S waveforms in Appendix 4 are shown.

**Figure captions for Appendix E:5**

Fig. E:5.1a Amplitude spectra for P waves as function of uniaxial stress for the dry specimen # 1

Fig. E:5.1b Amplitude spectra for P waves as function of uniaxial stress for the saturated specimen # 1

Fig. E:5.1c Amplitude spectra for S waves as function of uniaxial stress for the dry specimen # 1

Fig. E:5.1d Amplitude spectra for S waves as function of uniaxial stress for the saturated specimen # 1

Fig. E:5.2a Amplitude spectra for P waves as function of uniaxial stress for the dry specimen # 2

Fig. E:5.2b Amplitude spectra for P waves as function of uniaxial stress for the saturated specimen # 2

Fig. E:5.2c Amplitude spectra for S waves as function of uniaxial stress for the dry specimen # 2

Fig. E:5.2d Amplitude spectra for S waves as function of uniaxial stress for the saturated specimen # 2



Fig. E:5.3a Amplitude spectra for P waves as function of uniaxial stress for the dry specimen # 3

Fig. E:5.3b Amplitude spectra for P waves as function of uniaxial stress for the saturated specimen # 3

Fig. E:5.3c Amplitude spectra for S waves as function of uniaxial stress for the dry specimen # 3

Fig. E:5.3d Amplitude spectra for S waves as function of uniaxial stress for the saturated specimen # 3

Fig. E:5.4a Amplitude spectra for P waves as function of uniaxial stress for the dry specimen # 4

Fig. E:5.4b Amplitude spectra for P waves as function of uniaxial stress for the saturated specimen # 4

Fig. E:5.4c Amplitude spectra for S waves as function of uniaxial stress for the dry specimen # 4

Fig. E:5.4d Amplitude spectra for S waves as function of uniaxial stress for the saturated specimen # 4

Fig. E:5.5a Amplitude spectra for P waves as function of uniaxial stress for the dry specimen # 5

Fig. E:5.5b Amplitude spectra for P waves as function of uniaxial stress for the saturated specimen # 5

Fig. E:5.5c Amplitude spectra for S waves as function of uniaxial stress for the dry specimen # 5

Fig. E:5.5d Amplitude spectra for S waves as function of uniaxial stress for the saturated specimen # 5

Fig. E:5.6a Amplitude spectra for P waves as function of uniaxial stress for the dry specimen # 6

Fig. E:5.6b Amplitude spectra for P waves as function of uniaxial stress for the saturated specimen # 6

Fig. E:5.6c Amplitude spectra for S waves as function of uniaxial stress for the dry specimen # 6

Fig. E:5.6d Amplitude spectra for S waves as function of uniaxial stress for the saturated specimen # 6

Fig. E:5.7a Amplitude spectra for P waves as function of uniaxial stress for the dry specimen # 7

Fig. E:5.7b Amplitude spectra for P waves as function of uniaxial stress for the saturated specimen # 7

Fig. E:5.7c Amplitude spectra for S waves as function of uniaxial stress for the dry specimen # 7

Fig. E:5.7d Amplitude spectra for S waves as function of uniaxial stress for the saturated specimen # 7

Fig. E:5.8a Amplitude spectra for P waves as function of uniaxial stress for the dry specimen # 8

Fig. E:5.8b Amplitude spectra for P waves as function of uniaxial stress for the saturated specimen # 8

Fig. E:5.8c Amplitude spectra for S waves as function of uniaxial stress for the dry specimen # 8

Fig. E:5.8d Amplitude spectra for S waves as function of uniaxial stress for the saturated specimen # 8

Fig. E:5.9a Amplitude spectra for P waves as function of uniaxial stress for the dry specimen # 9

Fig. E:5.9b Amplitude spectra for P waves as function of uniaxial stress for the saturated specimen # 9

Fig. E:5.9c Amplitude spectra for S waves as function of uniaxial stress for the dry specimen # 9

Fig. E:5.9d Amplitude spectra for S waves as function of uniaxial stress for the saturated specimen # 9

Fig. E:5.10a Amplitude spectra for P waves as function of uniaxial stress for the dry specimen # 10

Fig. E:5.10b Amplitude spectra for P waves as function of uniaxial stress for the saturated specimen # 10

Fig. E:5.10c Amplitude spectra for S waves as function of uniaxial stress for the dry specimen # 10

Fig. E:5.10d Amplitude spectra for S waves as function of uniaxial stress for the saturated specimen # 10

Fig. E:5.11a Amplitude spectra for P waves as function of uniaxial stress for the dry specimen # 11

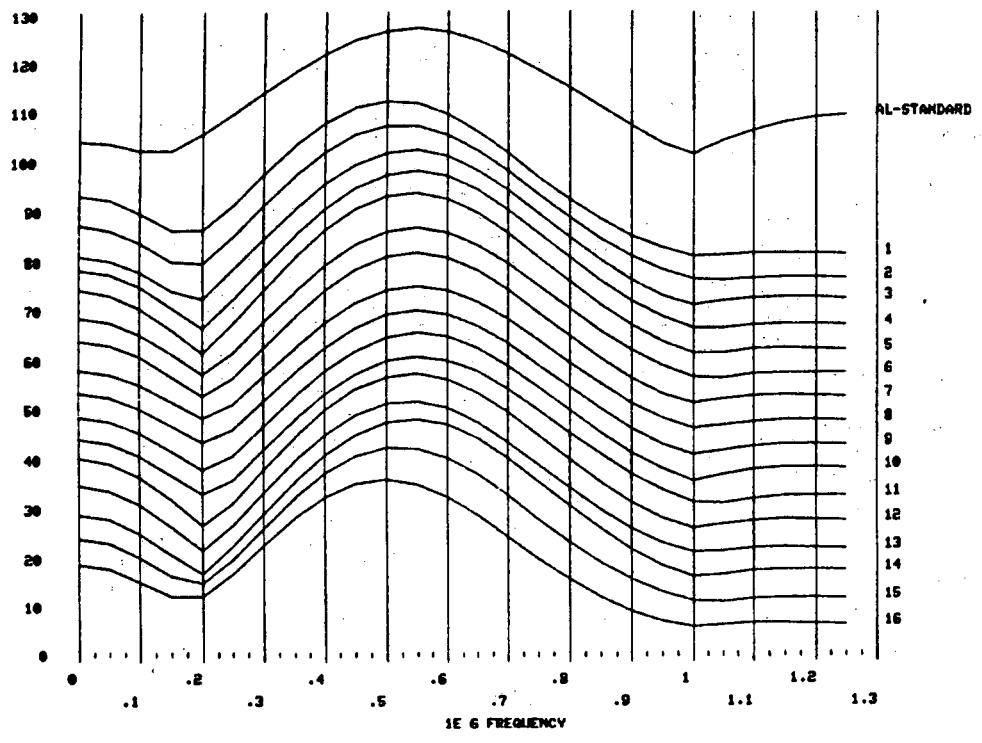
Fig. E:5.11b Amplitude spectra for P waves as function of uniaxial stress for the saturated specimen # 11

Fig. E:5.11c Amplitude spectra for S waves as function of uniaxial stress for the dry specimen # 11

Fig. E:5.11d Amplitude spectra for S waves as function of uniaxial stress for the saturated specimen # 11

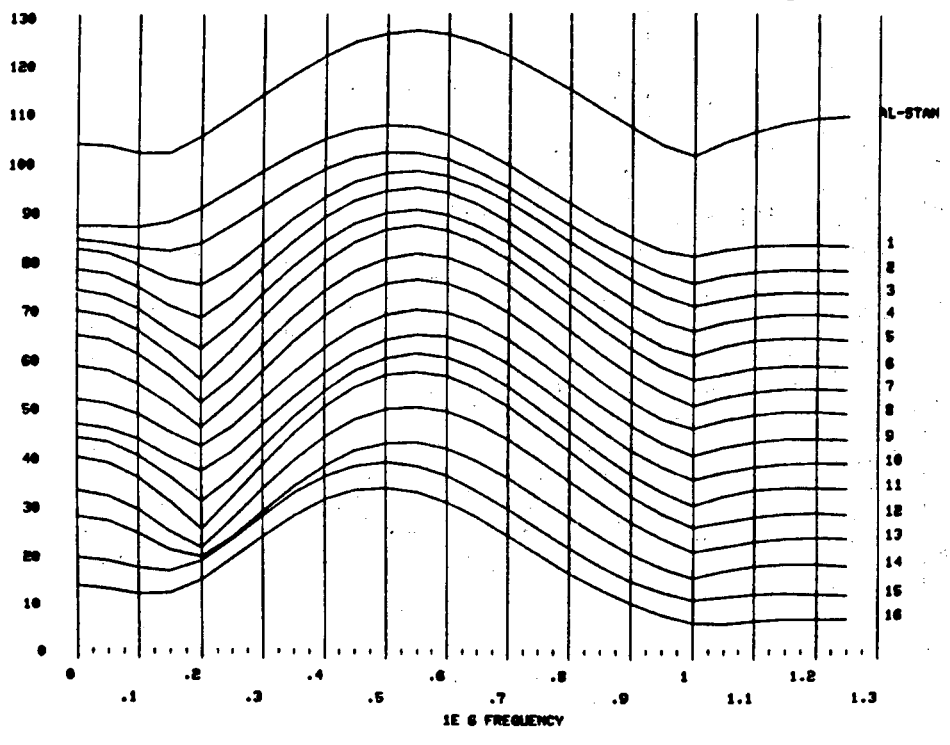
SPECIMEN : STRIPA 81, DRY, NS-NS CONDITION : DRY WINDOW : 4E-6  
SMOOTH : 0 FILE : STRPA1.  
P-WAVES DATE : 7 SEPTEMBER, 1982

Fig. E:5.1a



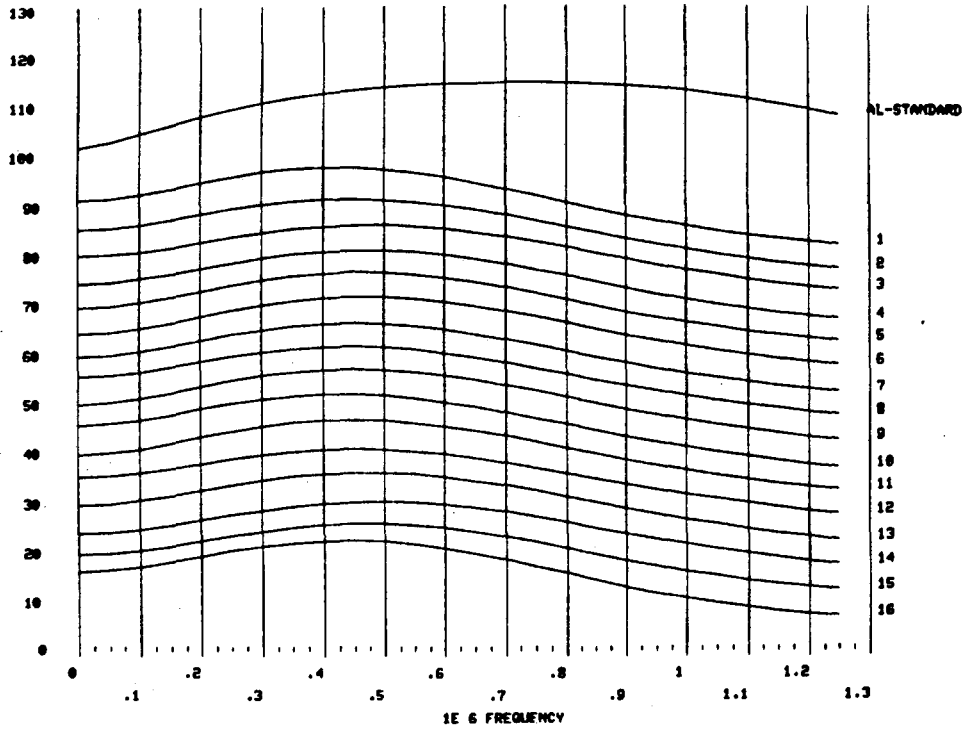
SPECIMEN : STRIPA 81 CONDITION : SATURATED WINDOW : 4E-6  
SMOOTH : 0 FILE : STPA11.  
P-WAVES DATE : 31 AUGUST 1982

Fig. E:5.1b



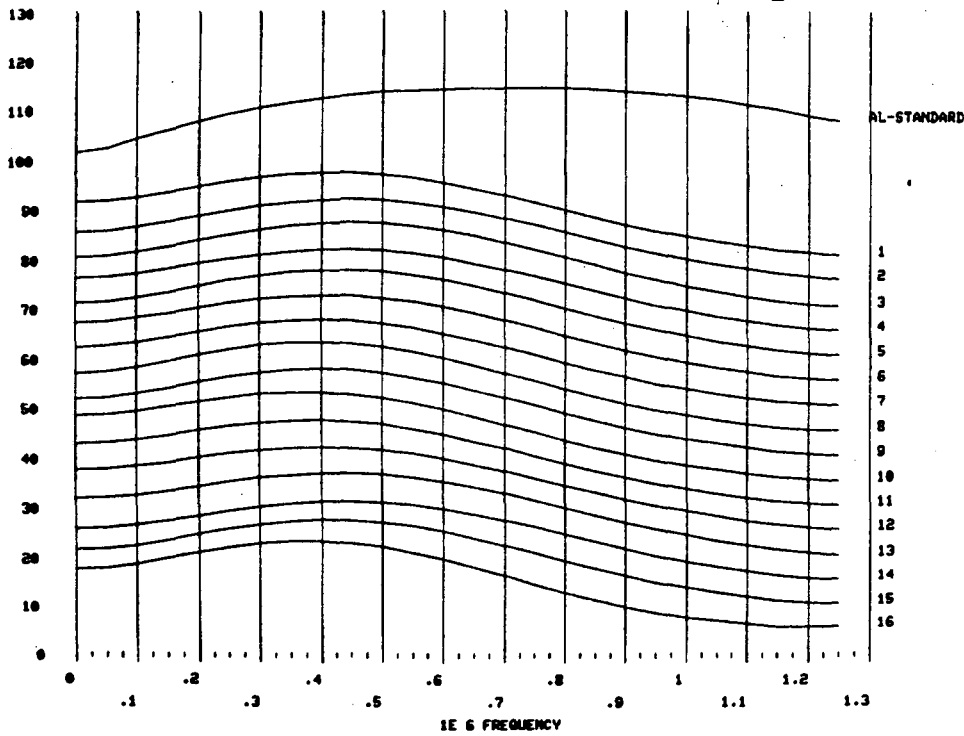
SPECIMEN : STRIPA 01, RB-R6, E21    CONDITION : DRY    WINDOW : 1+2E-6 SEC WIND  
SMOOTH : 0    FILE : STSA01.  
S-WAVES    DATE : 19 OCTOBER, 1982

Fig. E:5.1c



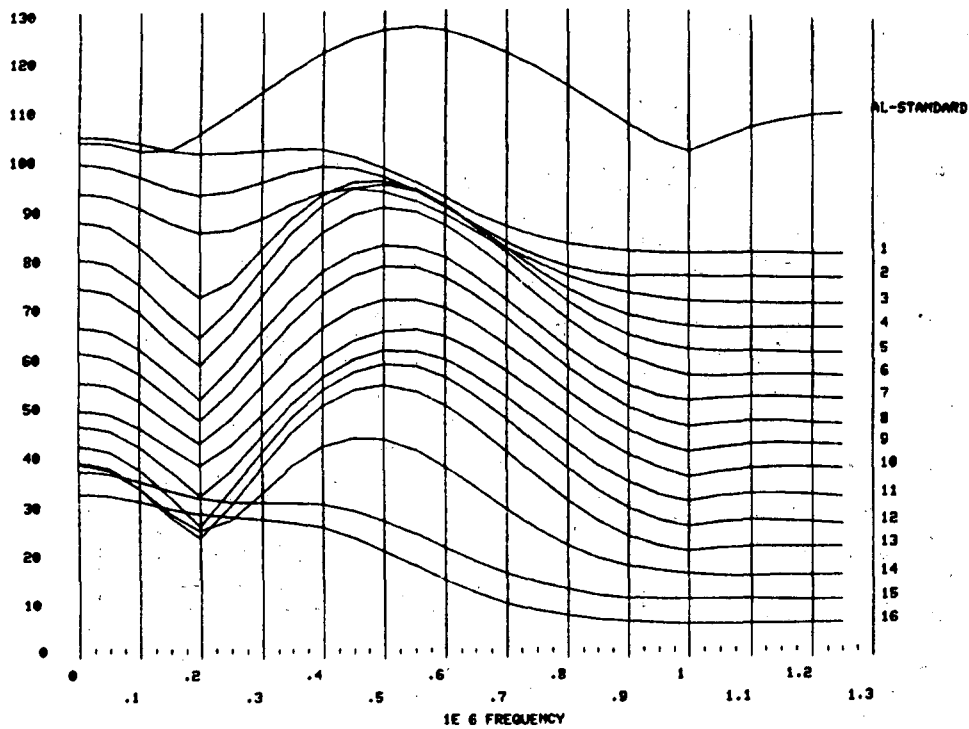
SPECIMEN : STRIPA 01, RB-R6    CONDITION : SATURATED    WINDOW : 1+2E-6 SEC WIND  
SMOOTH : 0    FILE : STSA01.  
S-WAVES    DATE : 19 OCTOBER, 1982

Fig. E:5.1d



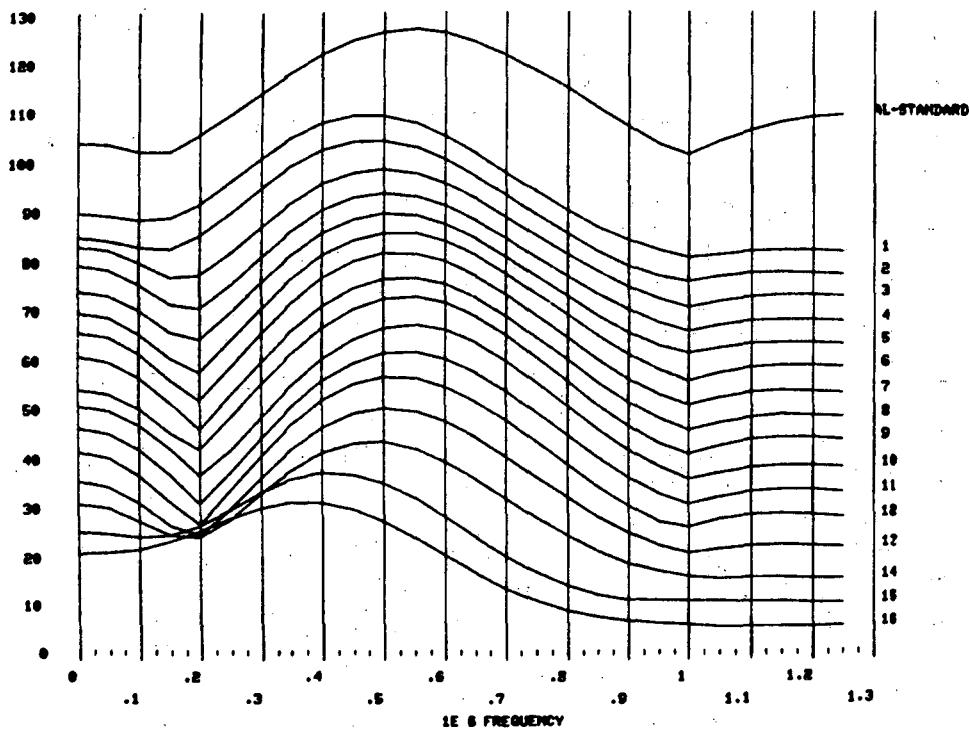
SPECIMEN : STRIPA 82, P-WAVES, WIND: 4E-6 SEC CONDITION : DRY WINDOW : 4E-6  
 SMOOTH : 0 FILE : STRPA2  
 P-WAVES DATE : 7 SEPTEMBER, 1982

Fig. E:5.2a



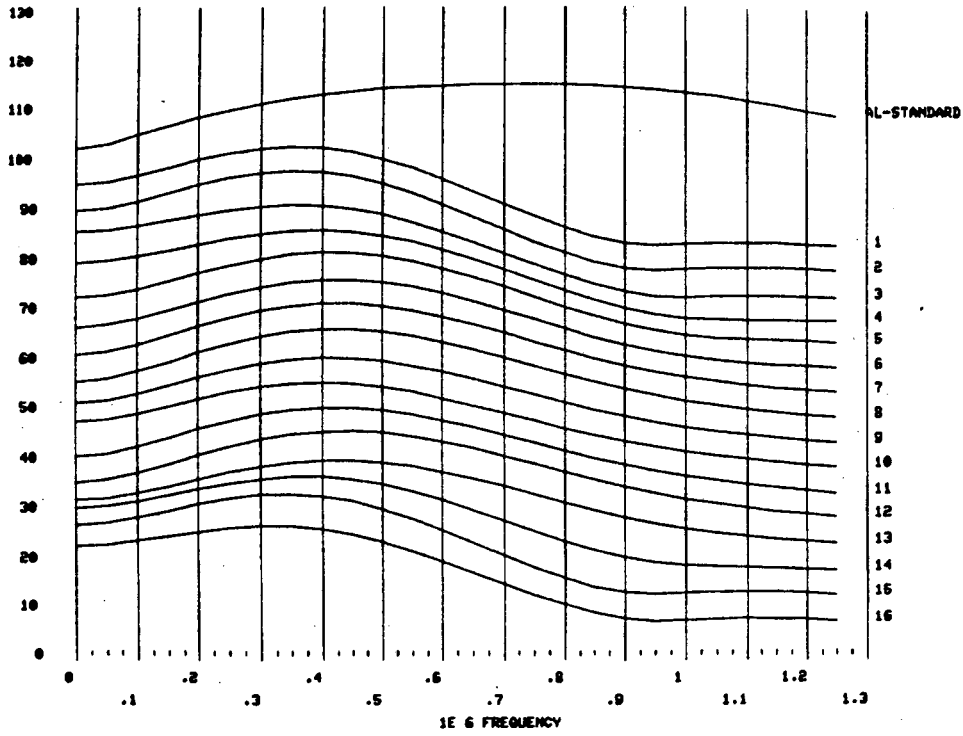
SPECIMEN : STRIPA 82 CONDITION : SATURATED WINDOW : 4E-6 SEC  
 SMOOTH : 0 FILE : STRPA2  
 P-WAVES DATE : 31 AUGUST, 1982

Fig. E:5.2b



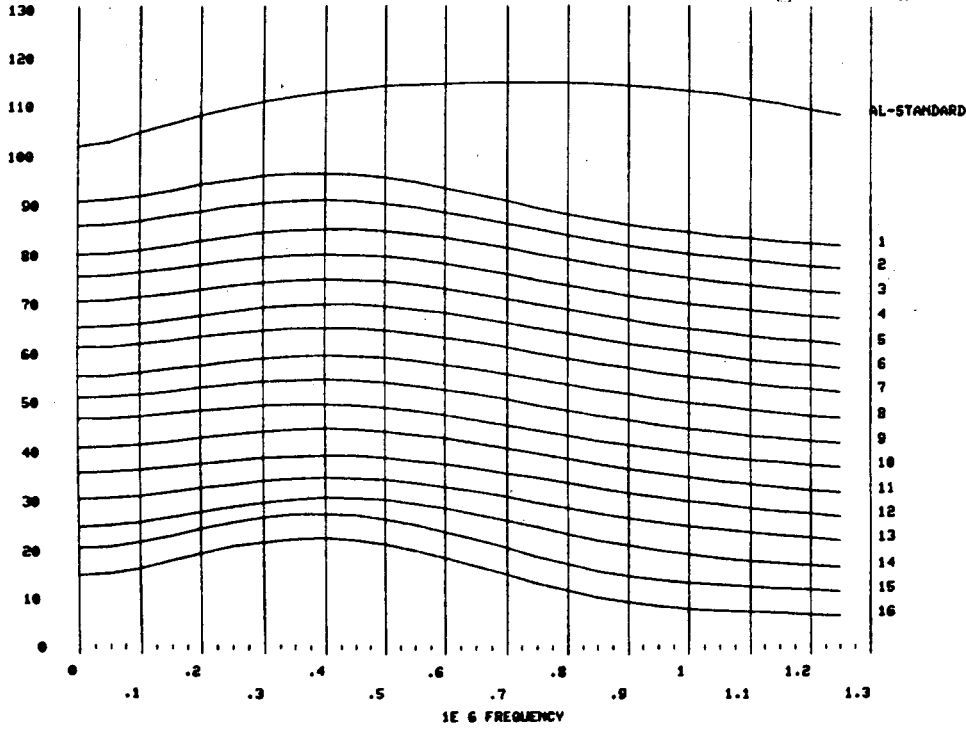
SPECIMEN : STRIPA 82, N7-R9 CONDITION : DRY WINDOW : 1+2E-6 SEC WIND  
 SMOOTH : 0 FILE : STSAD2  
 S-WAVES DATE : 19 OCTOBER, 1982

Fig. E:5.2c



SPECIMEN : STRIPA 82, N7-R9, E24 CONDITION : SATURATED WINDOW : 1+2E-6 SEC WIND  
 SMOOTH : 0 FILE : STSAD2  
 S-WAVES DATE : 19 OCTOBER, 1982

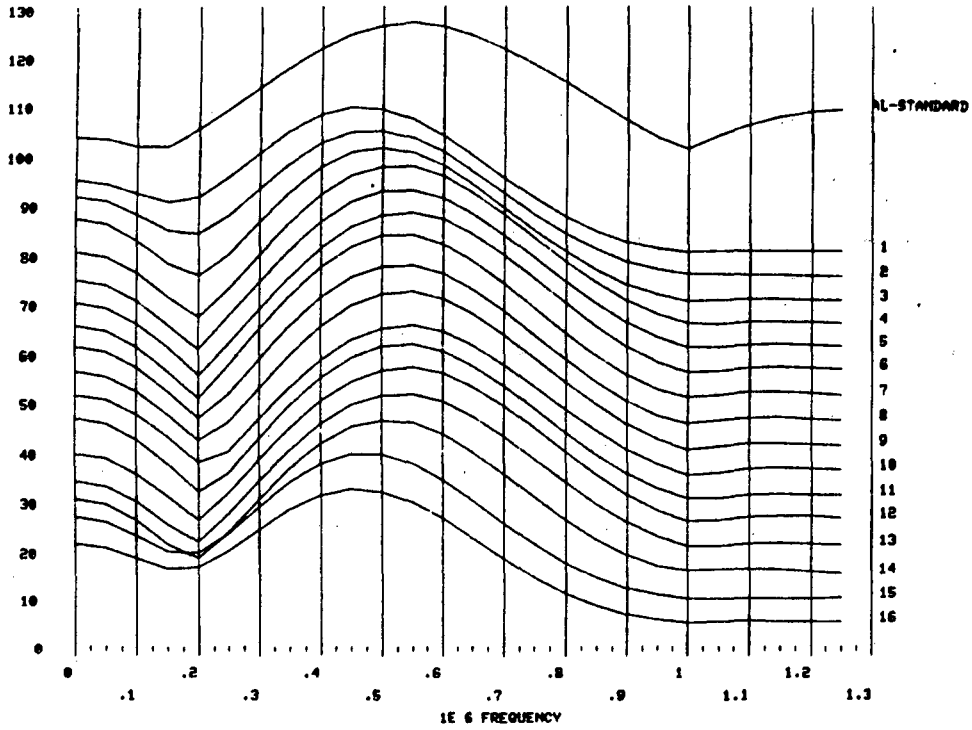
Fig. E:5.2d





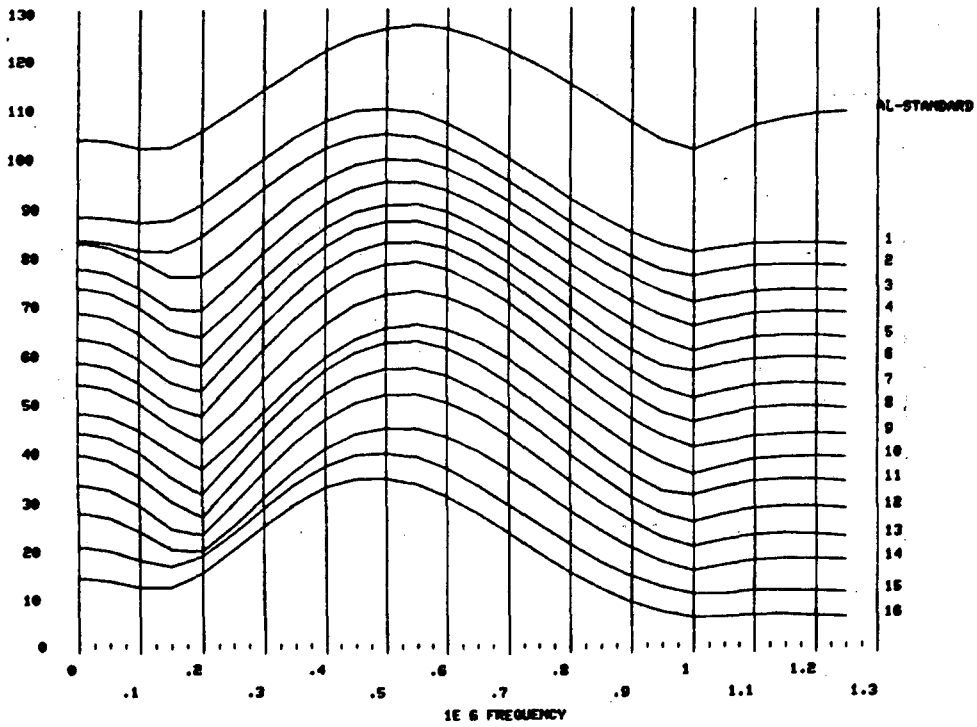
SPECIMEN : STRIPA 03, E29,M10    CONDITION : DRY    WINDOW : 4E-6  
SMOOTH : 0    FILE : STRPA3.  
P-WAVES    DATE : 7 SEPTEMBER, 1982

Fig. E:5.3a



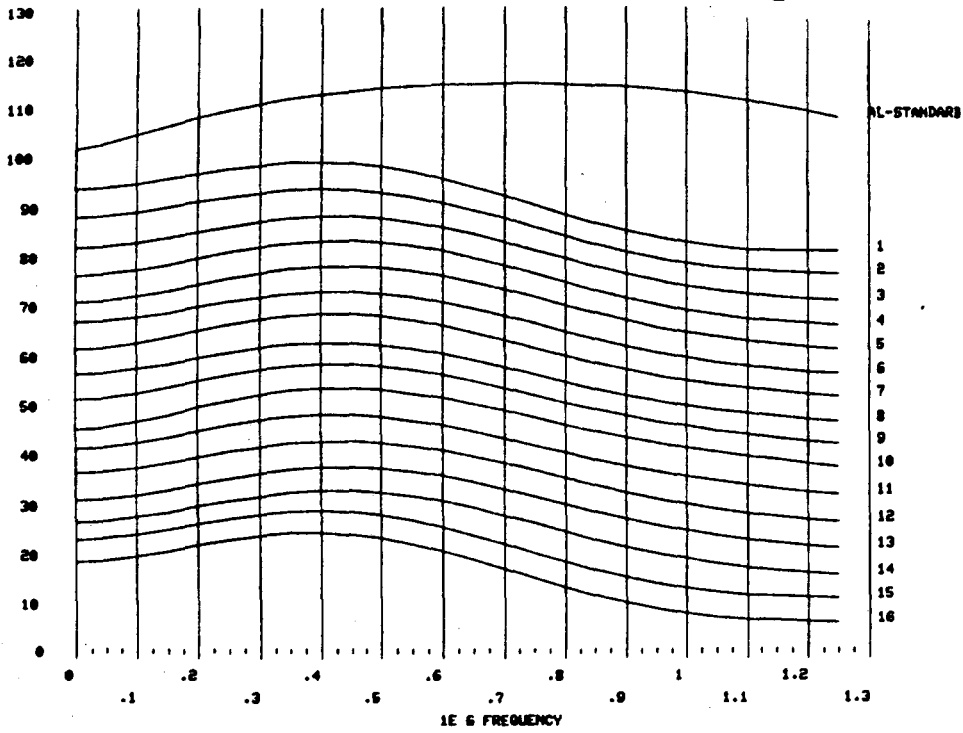
SPECIMEN : STRIPA 03    CONDITION : SATURATED    WINDOW : 4E-6  
SMOOTH : 0    FILE : STRPA3.  
P-WAVES    DATE : 2 SEPTEMBER, 1982

Fig. E:5.3b



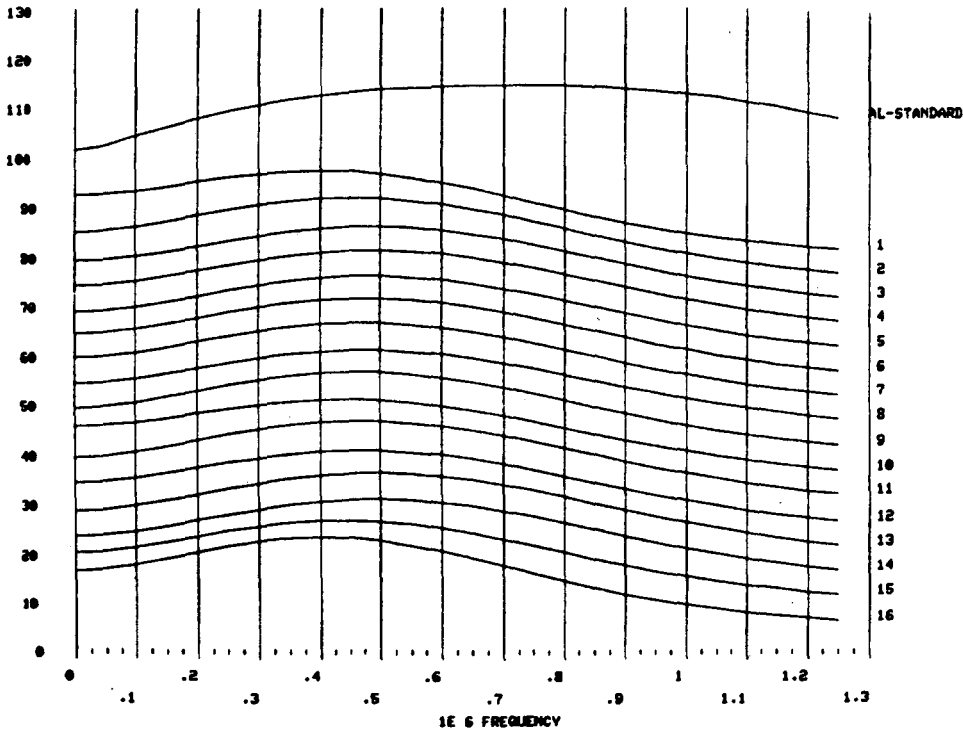
SPECIMEN : STRIPA 83, E28/M10    CONDITION : DRY    WINDOW : 1+2E-6 SEC WIND  
SMOOTH : 0    FILE : ST5AD3.  
S-WAVES    DATE : 19 OCTOBER, 1982

Fig. E:5.3c



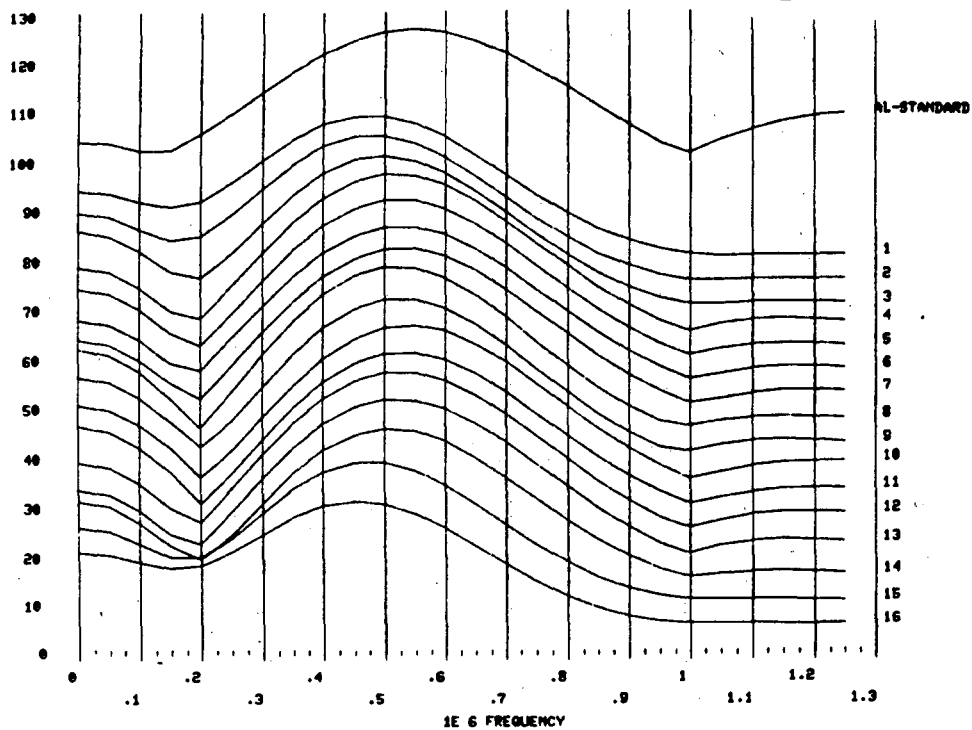
SPECIMEN : STRIPA 83, M10-E28    CONDITION : SATURATED    WINDOW : 1+2E-6 SEC WIND  
SMOOTH : 0    FILE : ST5AM3.  
S-WAVES    DATE : 20 OCTOBER, 1982

Fig. E:5.3d



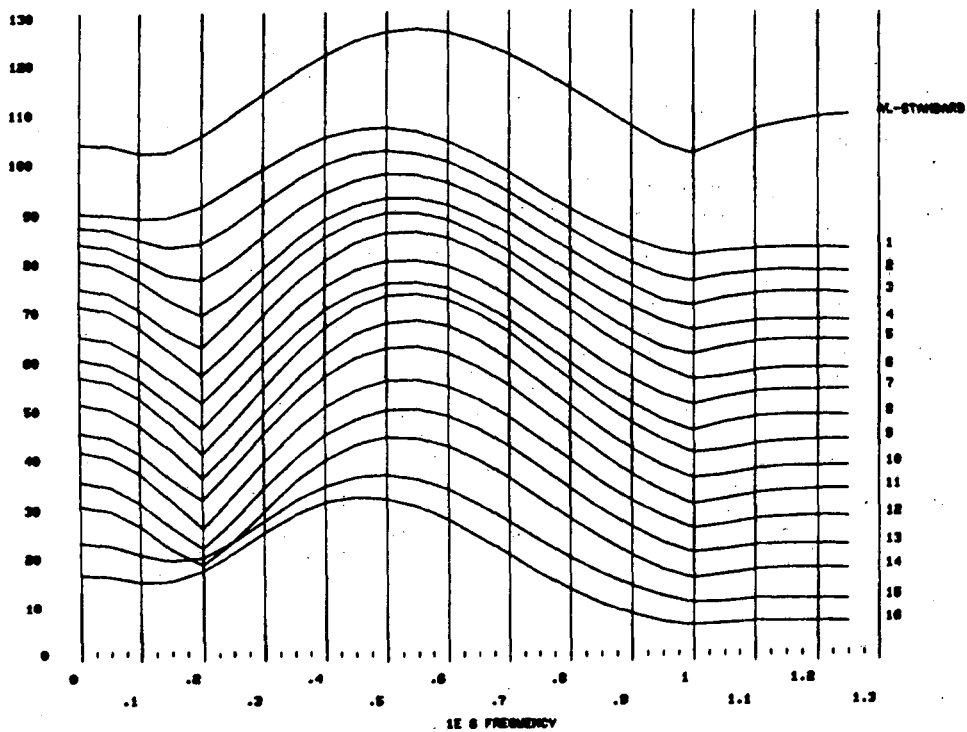
SPECIMEN : STRIPA 04, E29, H10    CONDITION : DRY    WINDOW : 4E-6 SEC  
 SMOOTH : 0    FILE : STRPA4.  
 P-WAVES    DATE : 7 SEPTEMBER, 1982

Fig. E:5.4a



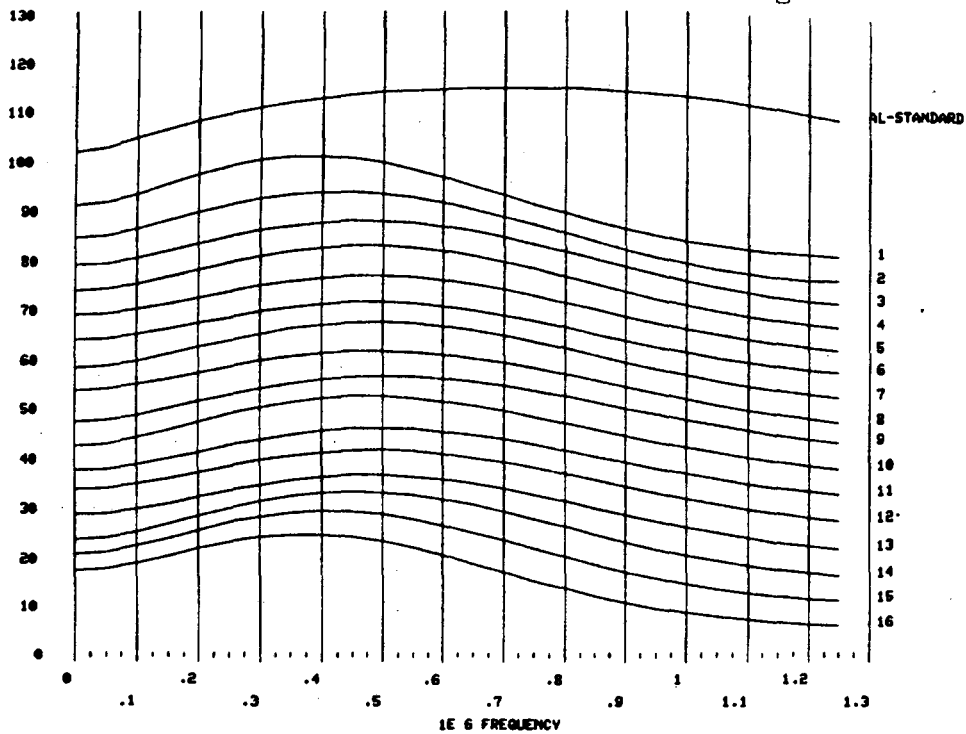
SPECIMEN : STRIPA 04    CONDITION : SATURATED    WINDOW : 4E-6  
 SMOOTH : 0    FILE : STRPA4.  
 P-WAVES    DATE : 3 SEPTEMBER, 1982

Fig. E:5.4b



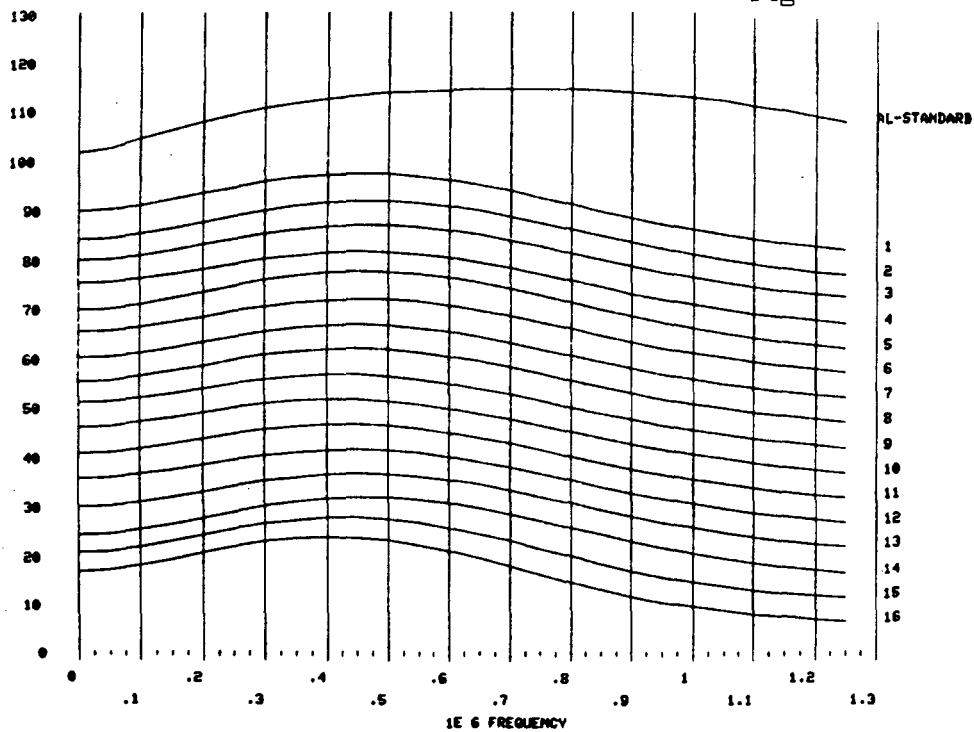
SPECIMEN : STRIPA 84, DBEX-1, 1.45 FROM M10, 130 C CONDITION : DRY. WINDOW : 1+2E-6 SEC  
 SMOOTH : 0 FILE : STSAD4.  
 5-WAVES DATE : 20 OCTOBER, 1982

Fig. E:5.4c



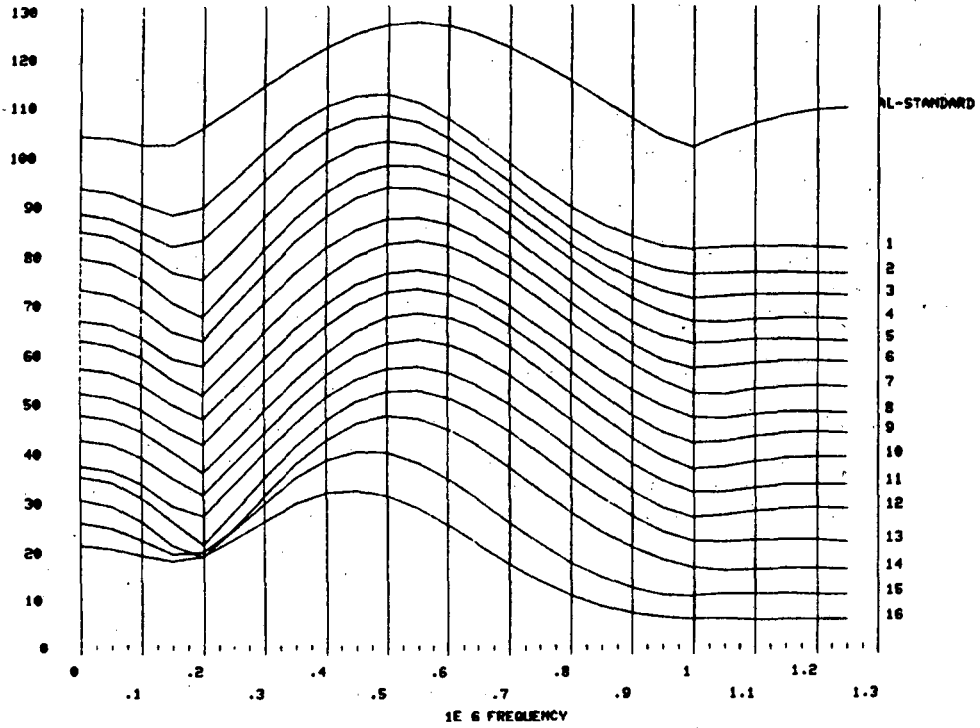
SPECIMEN : STRIPA 84, DBEX-1 1.45 F. M10, 130 C CONDITION : SATURATED WINDOW : 1+2E-6 SEC  
 SMOOTH : 0 FILE : STSAU4.  
 5-WAVES DATE : 20 OCTOBER, 1982

Fig. E:5.4d



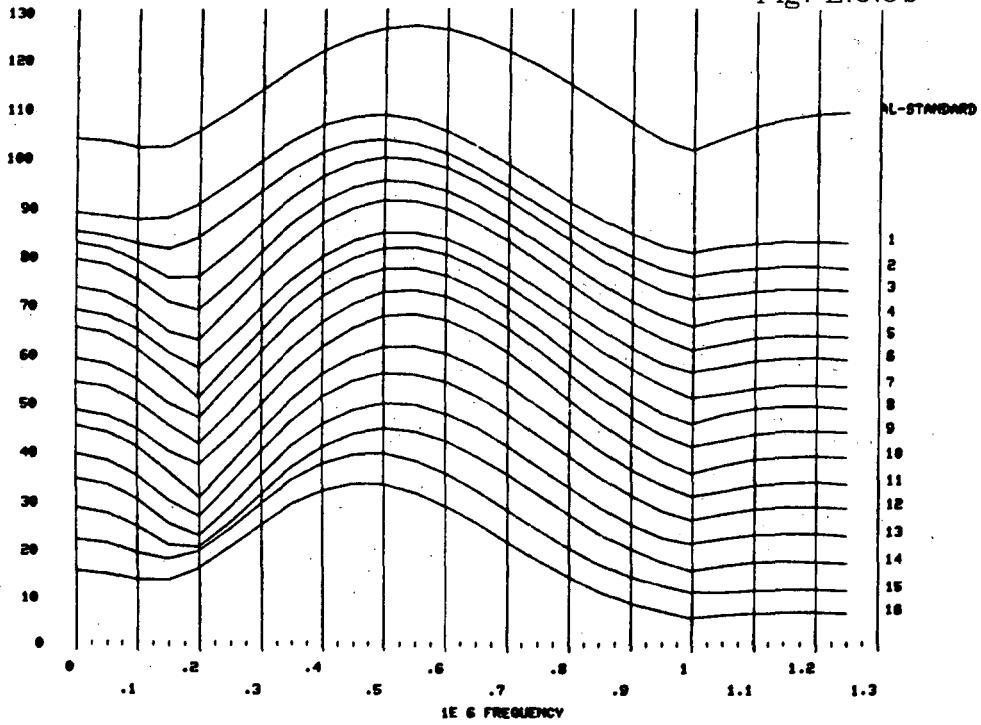
SPECIMEN : STRIPA 95, DRY, DRILLBACK 0.75H FROM M10, B29907    CONDITION : DRY    WINDOW : 4-6 SEC  
 SMOOTH : 0    FILE : STRPA5.  
 P-WAVES    DATE : 7 SEPTEMBER, 1982

Fig. E:5.5a



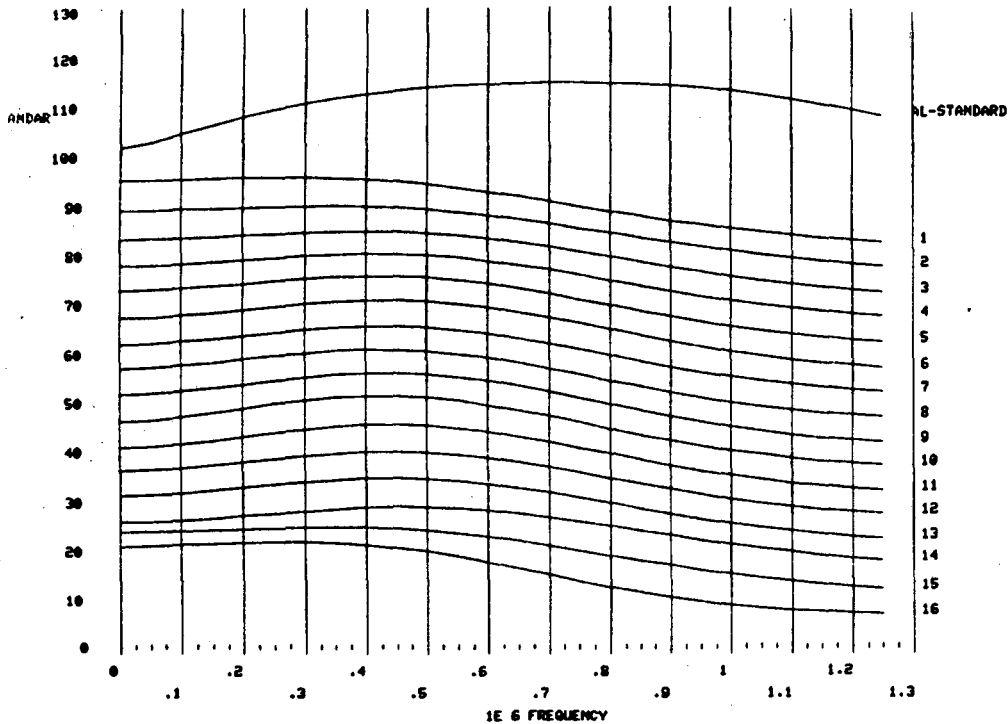
SPECIMEN : STRIPA 95, DRILLBACK 0.75 M10    CONDITION : SATURATED    WINDOW : 4E-8  
 SMOOTH : 0    FILE : STRPA5.  
 P-WAVES    DATE : 3 SEPTEMBER, 1982

Fig. E:5.5b



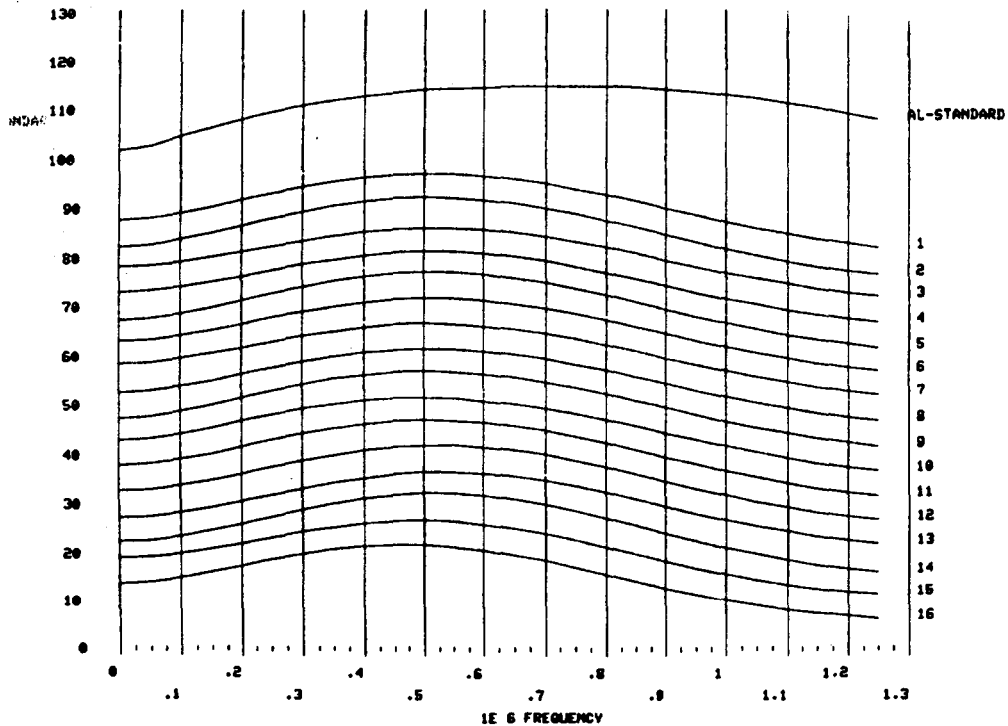
SPECIMEN : STRIPA 85, DBEX-1, 0.75 FROM H10, 200C CONDITION : DRY WINDOW : 1+2E-6 SEC  
 SMOOTH : 0 FILE : STSADS.  
 S-WAVES DATE : 20 OCTOBER, 1982

Fig. E:5.5c



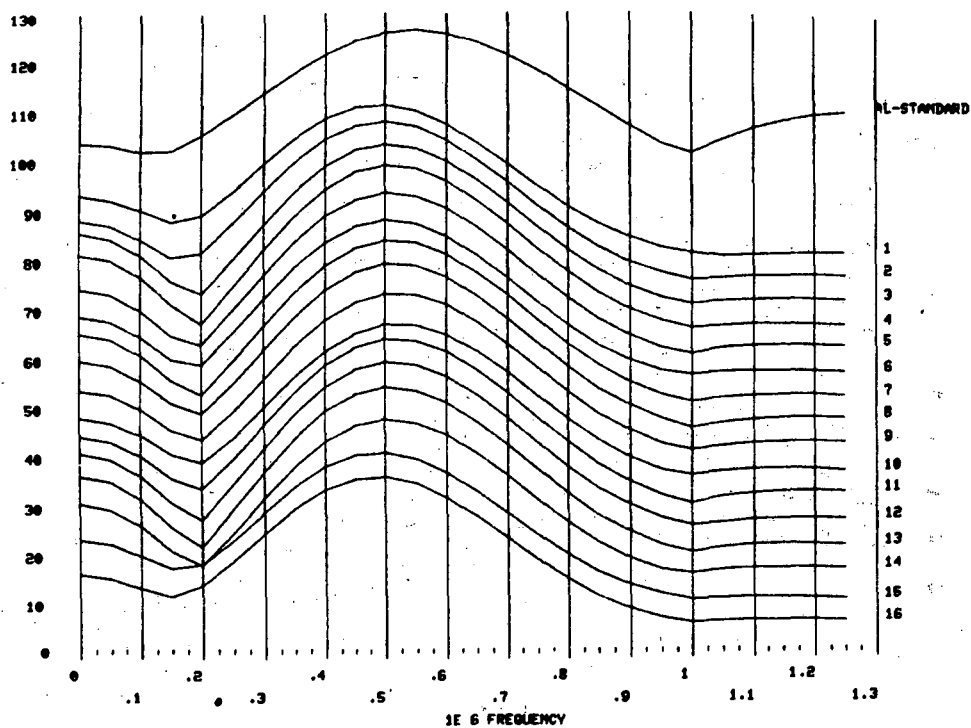
SEC W) SPECIMEN : STRIPA 85, DBEX-1 0.75 FROM H10, 200 C CONDITION : SATURATED WINDOW : 1+2E-6 SEC WIND  
 SMOOTH : 0 FILE : STSAMS.  
 S-WAVES DATE : 20 OCTOBER 1982

Fig. E:5.5d



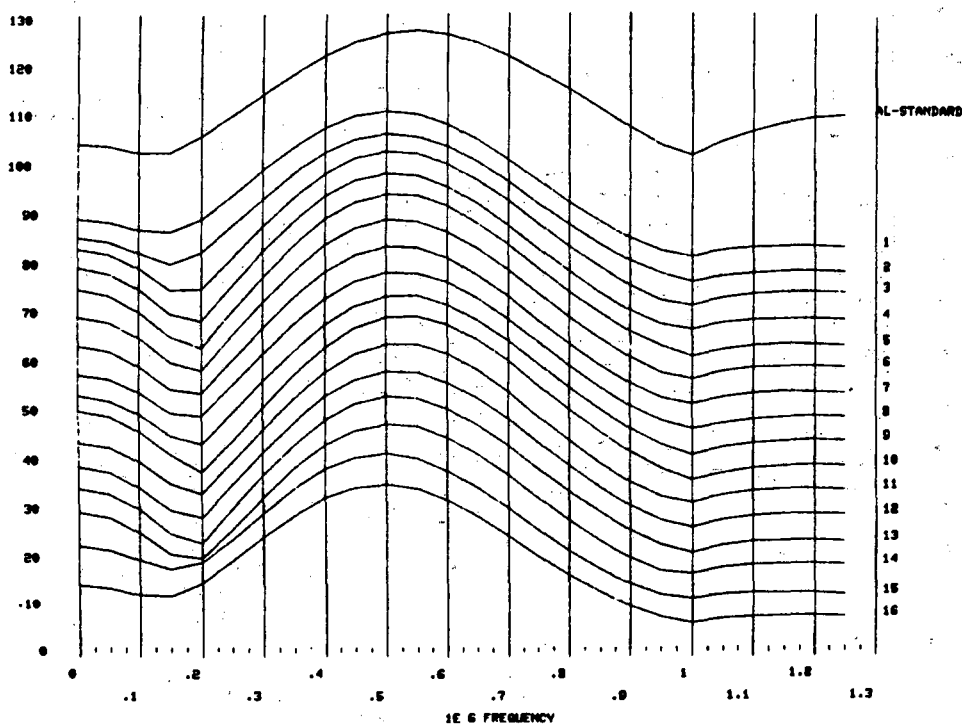
SPECIMEN : STRIP# 86, R8-R6 CONDITION : DRY WINDOW : 4E-6  
 SMOOTH : 0 FILE : STRPADG.  
 P-WAVES DATE : 22 SEPTEMBER, 1982

Fig. E:5.6a



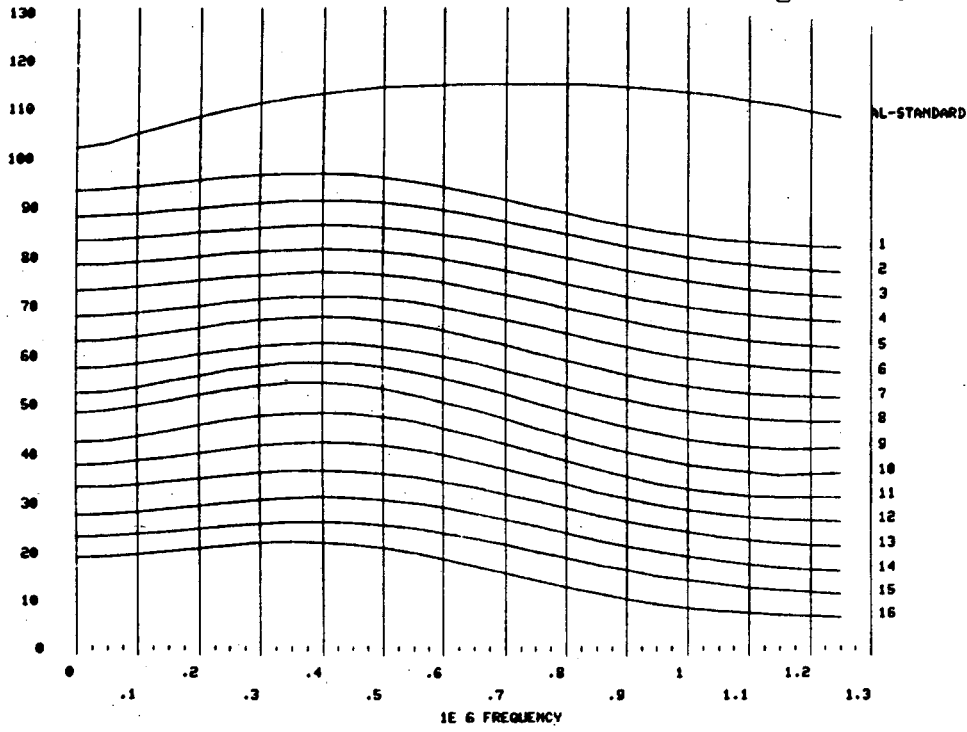
SPECIMEN : STRIP# 86, R8-R6 CONDITION : SATURATED WINDOW : 4E-6 SEC.  
 SMOOTH : 0 FILE : STRPADG.  
 P-WAVES DATE : 30 SEPTEMBER, 1982

Fig. E:5.6b



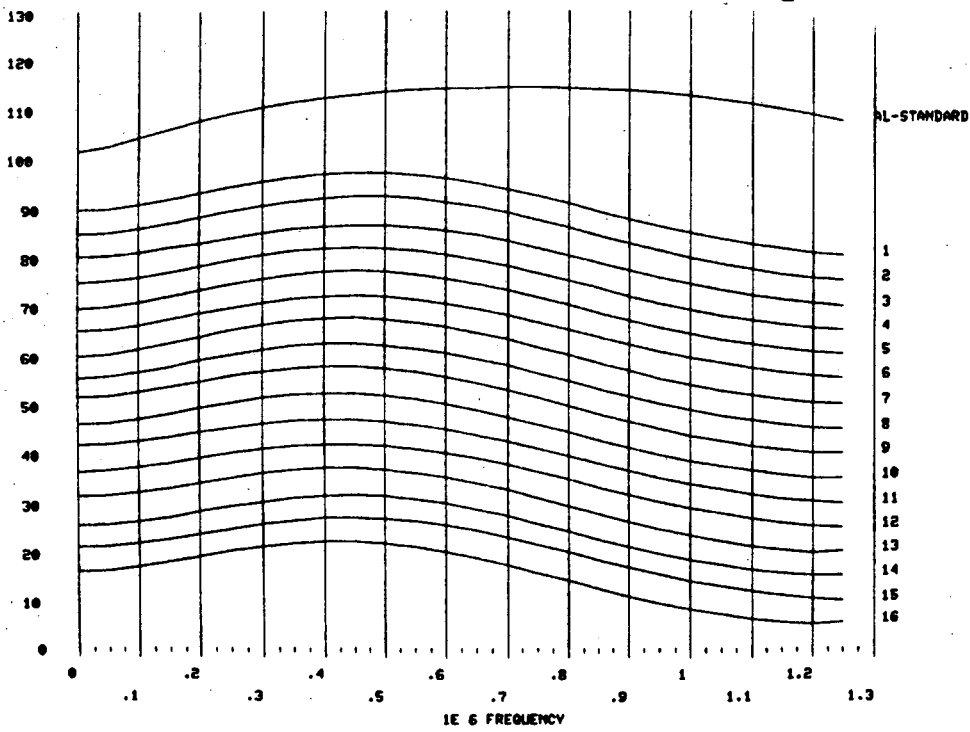
SPECIMEN : STRIPA 86, E22, RB-N6 CONDITION : DRY WINDOW : 1+2E-6 SEC  
SMOOTH : 0 FILE : STSAD6.  
5-WAVES DATE : 20 OCTOBER, 1982

Fig. E:5.6c



SPECIMEN : STRIPA 86, RB-N6 CONDITION : SATURATED WINDOW : 1+2E-6  
SMOOTH : 0 FILE : STSAM6.  
5-WAVES DATE : 3 OCTOBER, 1982

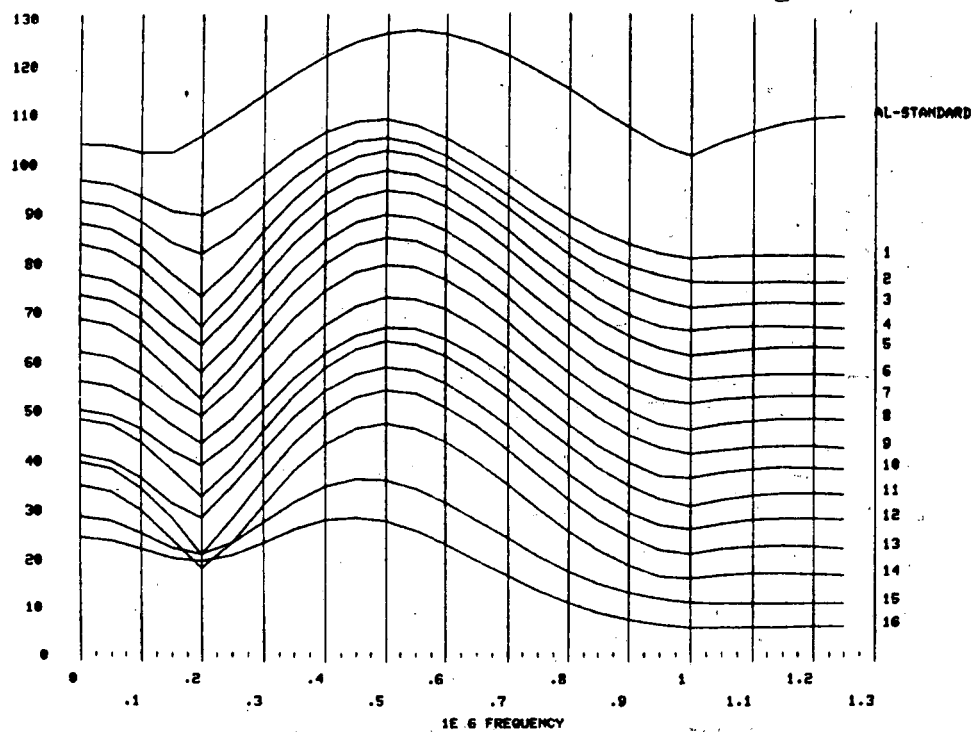
Fig. E:5.6d





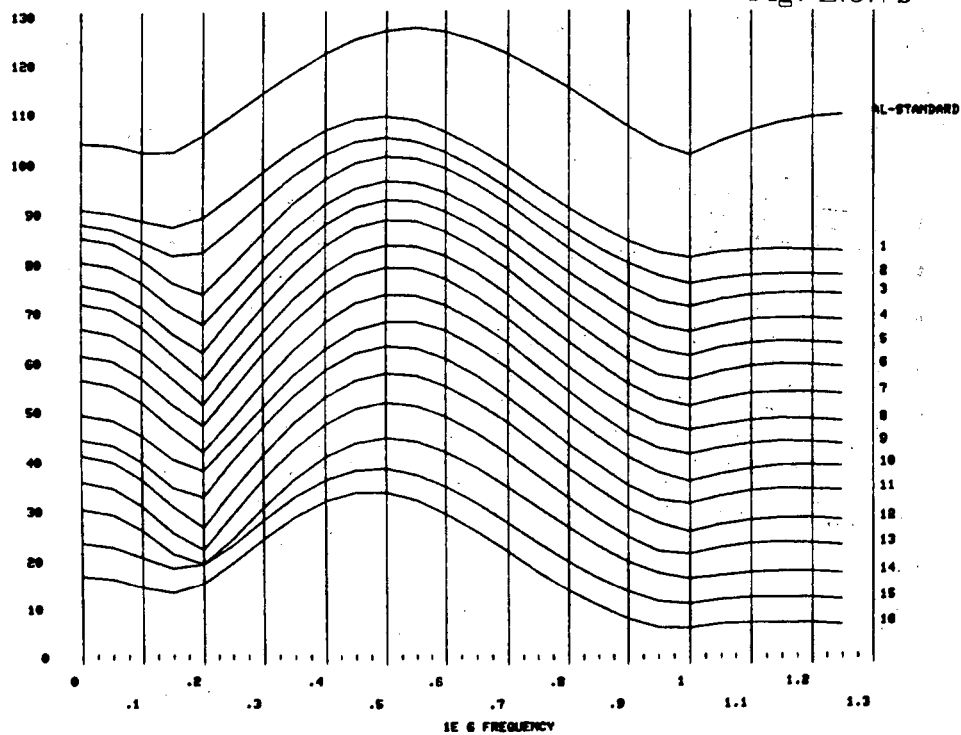
SPECIMEN : STRIPA 97, NS-NS CONDITION : DRY WINDOW : 4E-6  
 SMOOTH : 0 FILE : STPAD7.  
 P-WAVES DATE : 22 SEPTEMBER, 1982

Fig. E:5.7a



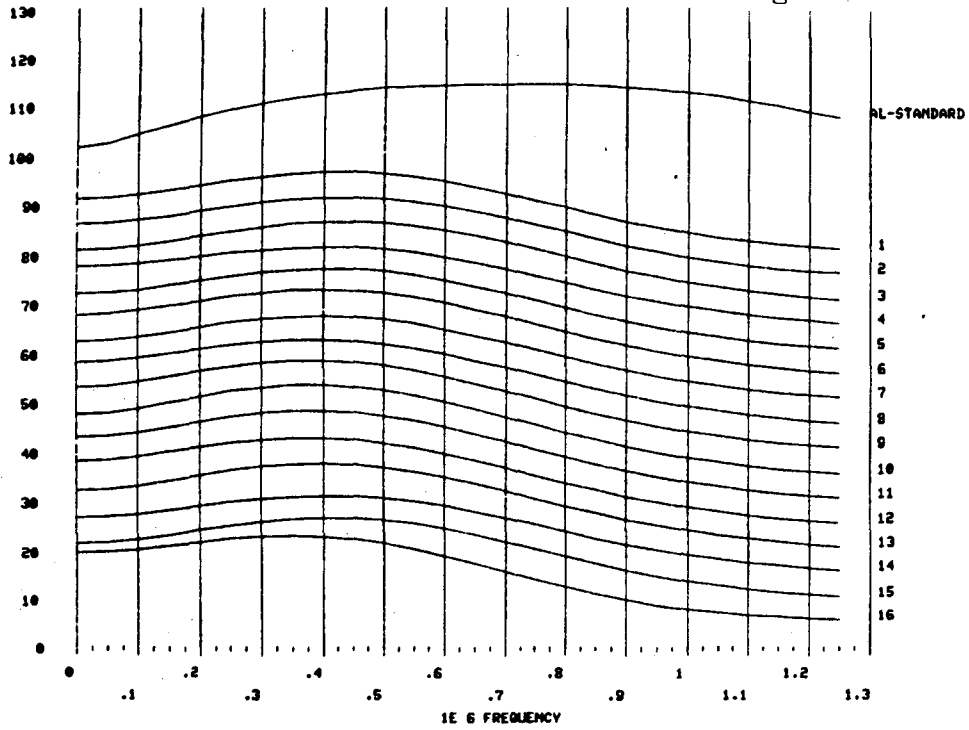
SPECIMEN : STRIPA 97, NS-NS CONDITION : SATURATED WINDOW : 4E-6  
 SMOOTH : 0 FILE : STPAD7.  
 P-WAVES DATE : 3 OCTOBER, 1982

Fig. E:5.7b



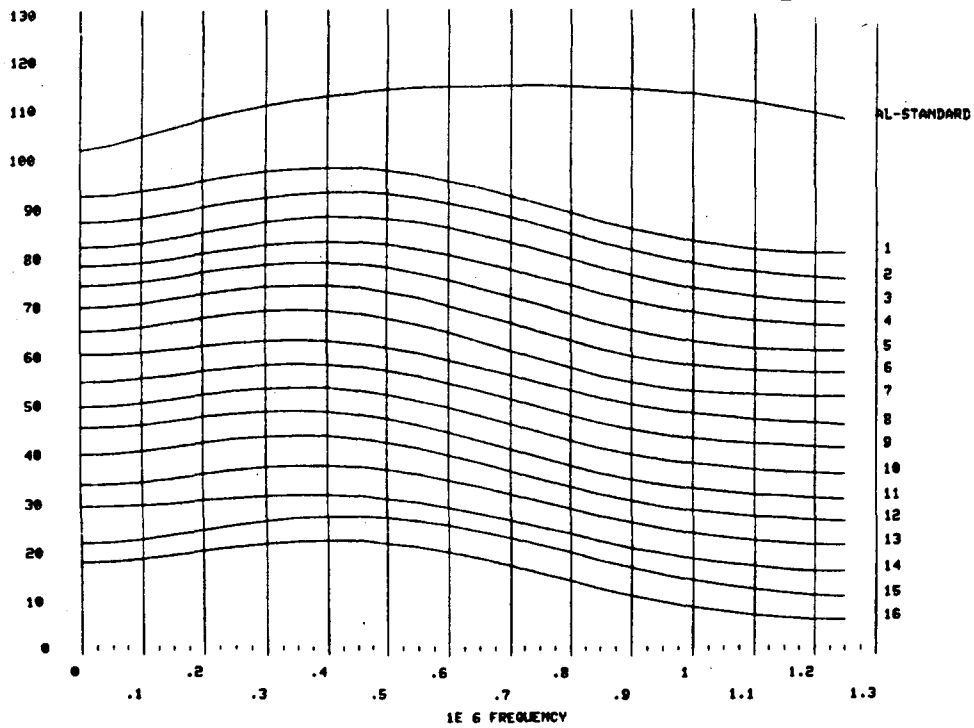
SPECIMEN : STRIPA 07, E22, RB-R6 CONDITION : DRY WINDOW : 1+2E-6 SEC  
 SMOOTH : 0 FILE : ST5AD7.  
 S-WAVES DATE : 20 OCTOBER, 1982

Fig. E:5.7c



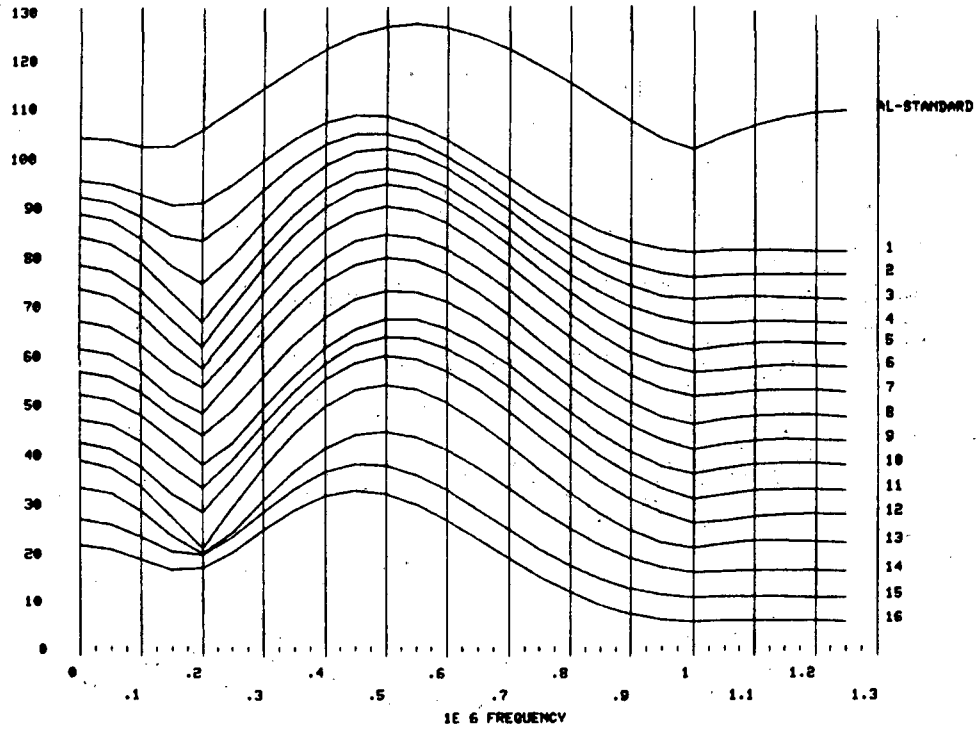
SPECIMEN : STRIPA 07, RB-R6 CONDITION : SATURATED WINDOW : 1+2E-6 SEC  
 SMOOTH : 0 FILE : ST5AU7.  
 S-WAVES DATE : 3 OCTOBER, 1982

Fig. E:5.7d



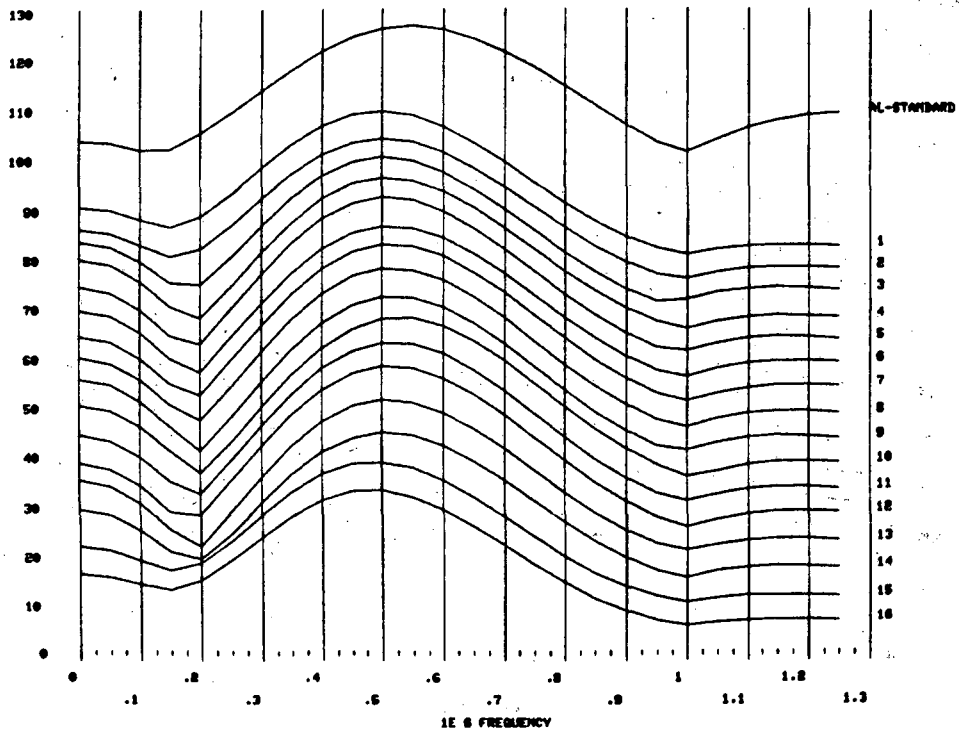
SPECIMEN : STRIPA 88, PB-RG CONDITION : DRY WINDOW : 4E-6  
SMOOTH : 0 FILE : STPAD8.  
P-WAVES DATE : 22 SEPTEMBER, 1982

Fig. E:5.8a



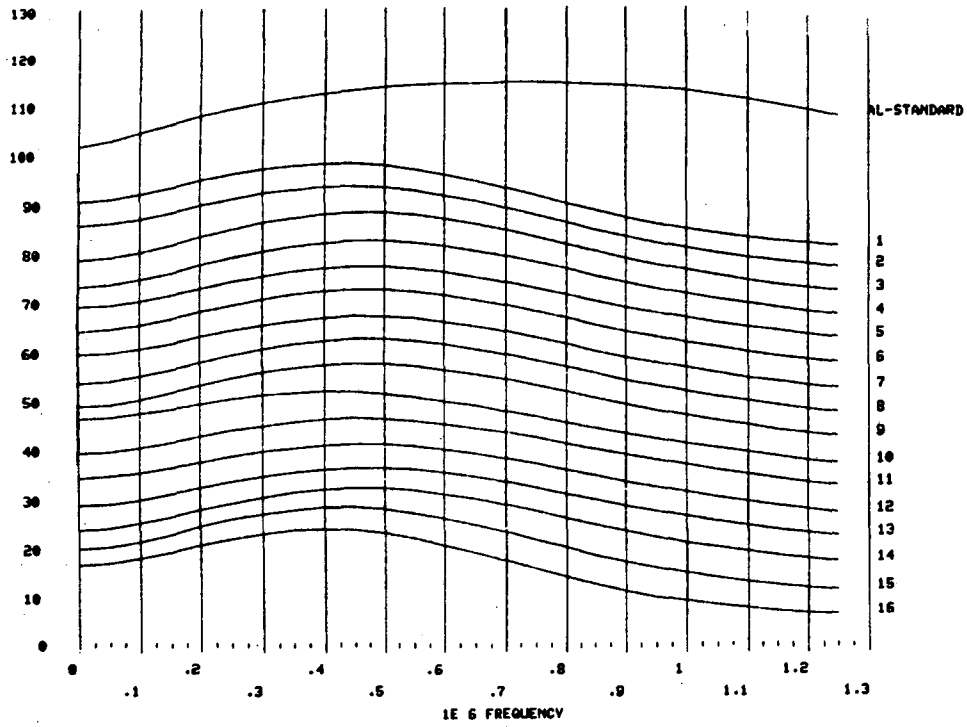
SPECIMEN : STRIPA 88, PB-RG CONDITION : SATURATED WINDOW : 4E-6 SEC  
SMOOTH : 0 FILE : STPAD8.  
P-WAVES DATE : 3 OCTOBER, 1982

Fig. E:5.8b



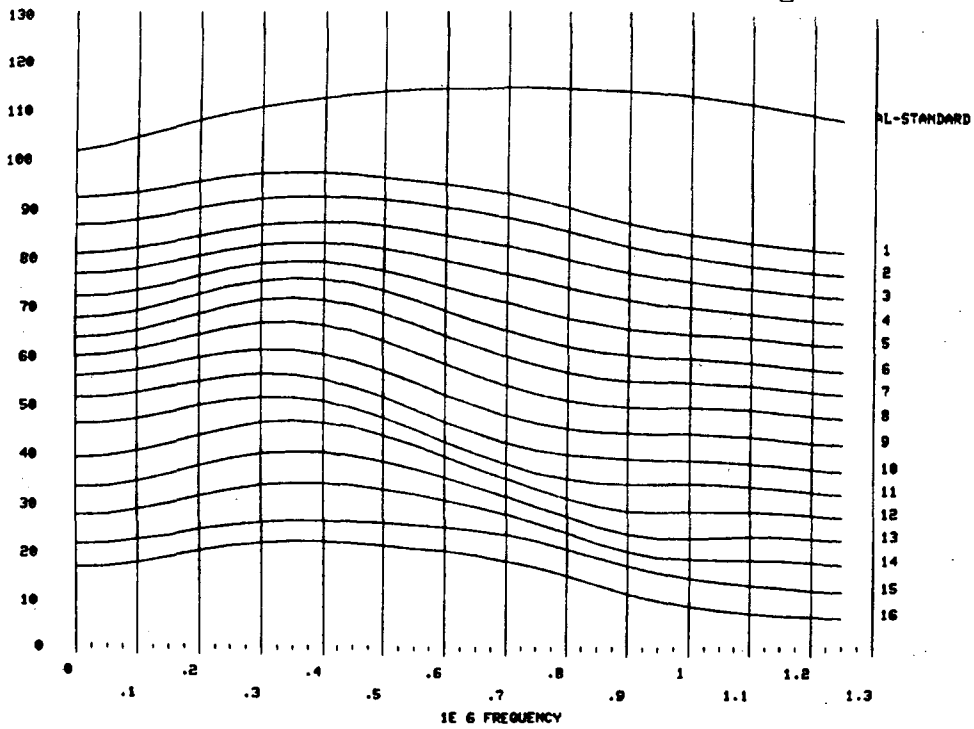
SPECIMEN : STRIPA 88, E22, RB-R6 CONDITION : DRY WINDOW : 1\*2E-6 SEC  
SMOOTH : 0 FILE : STSAD8.  
5-WAVES DATE : 20 OCTOBER, 1982

Fig. E:5.8c



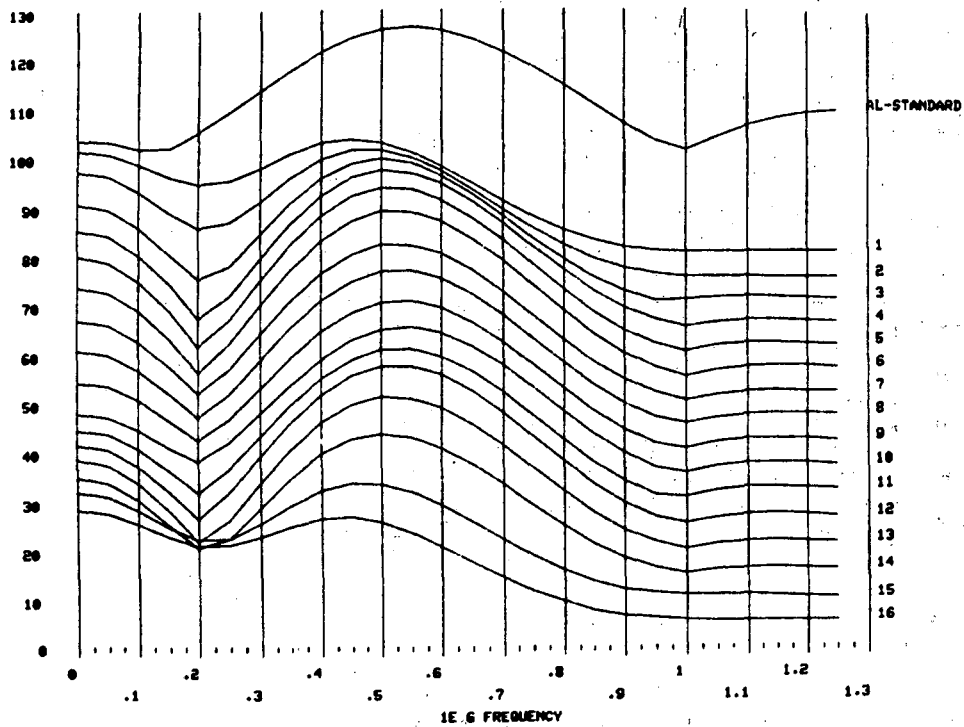
SPECIMEN : STRIPA 88, RB-R6 CONDITION : SATURATED WINDOW : 1\*2E-6 SEC  
SMOOTH : 0 FILE : STSAMB.  
5-WAVES DATE : 3 OCTOBER, 1982

Fig. E:5.8d



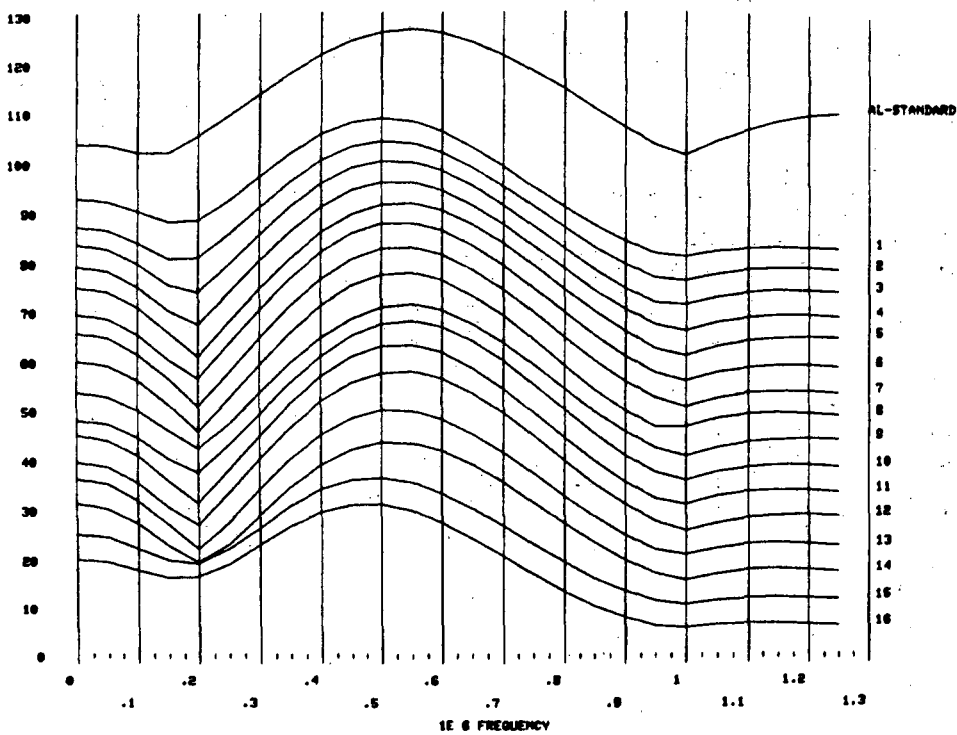
SPECIMEN : STRIPA 89, E25, M7-M9 CONDITION : DRY WINDOW : 4E-6 SEC  
 SMOOTH : 0 FILE : STPAD9.  
 P-WAVES DATE : 20 OCTOBER, 1982

Fig. E:5.9a



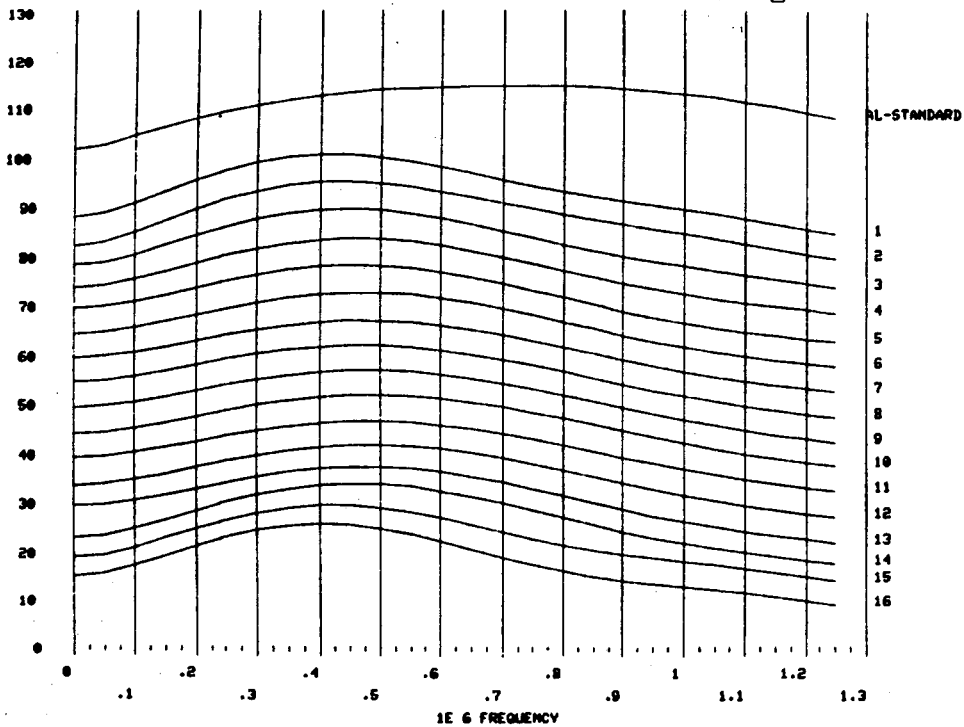
SPECIMEN : STRIPA 89, M7-M9 CONDITION : SATURATED WINDOW : 4E-6  
 SMOOTH : 0 FILE : STPAD9.  
 P-WAVES DATE : 3 OCTOBER, 1982

Fig. E:5.9b



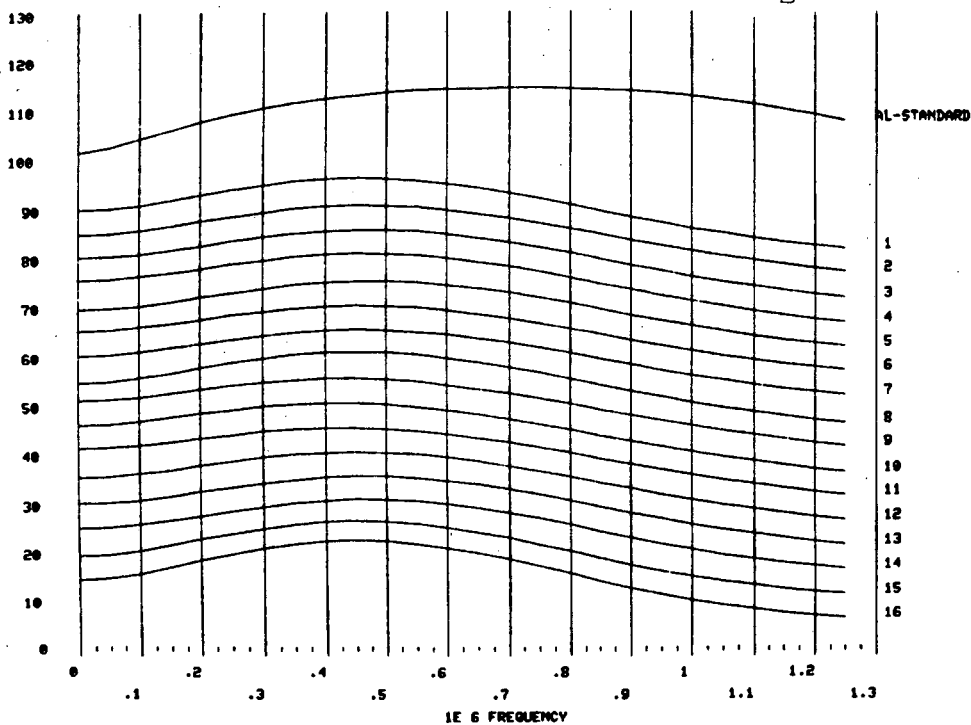
SPECIMEN : STRIPA 89, E-25, M7-M9    CONDITION : DRY    WINDOW : 1+2E-6 SEC  
SMOOTH : 0    FILE : STSAD9.  
S-WAVES    DATE : 20 OCTOBER, 1982

Fig. E:5.9c



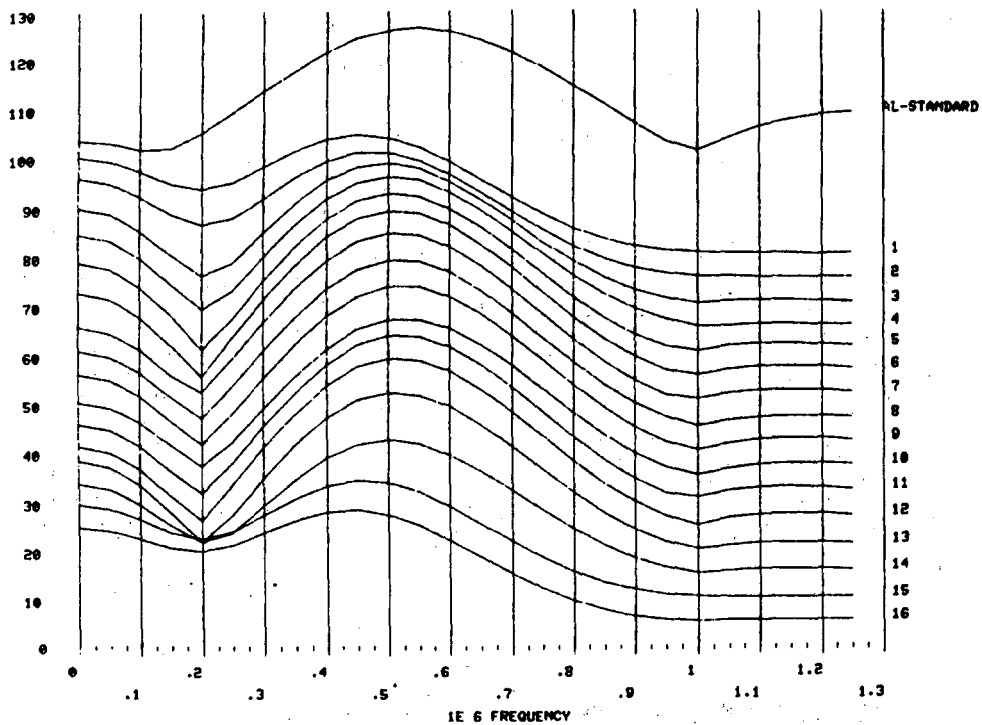
SPECIMEN : STRIPA 89, M7-M9    CONDITION : SATURATED    WINDOW : 1+2E-6 SEC  
SMOOTH : 0    FILE : STSAM9.  
S-WAVES    DATE : 3 OCTOBER, 1982

Fig. E:5.9d



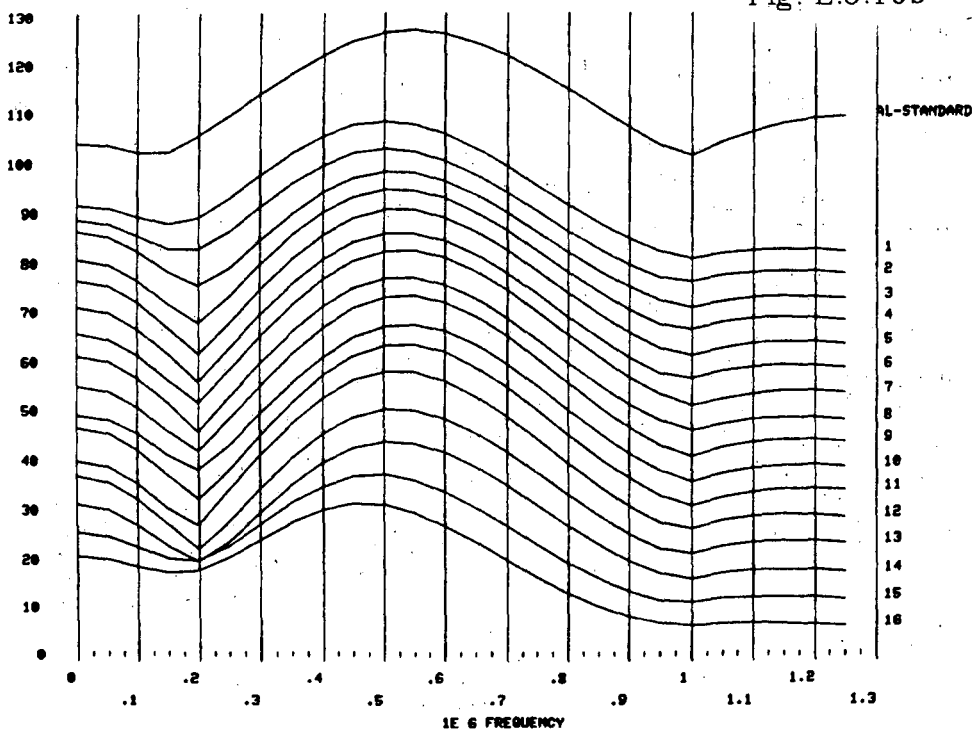
SPECIMEN : STRIPA 010 CONDITION : DRY WINDOW : 4E-6  
 SMOOTH : 0 FILE : SPAD10.  
 P-WAVES DATE : 21 SEPTEMBER, 1982

Fig. E:5.10a



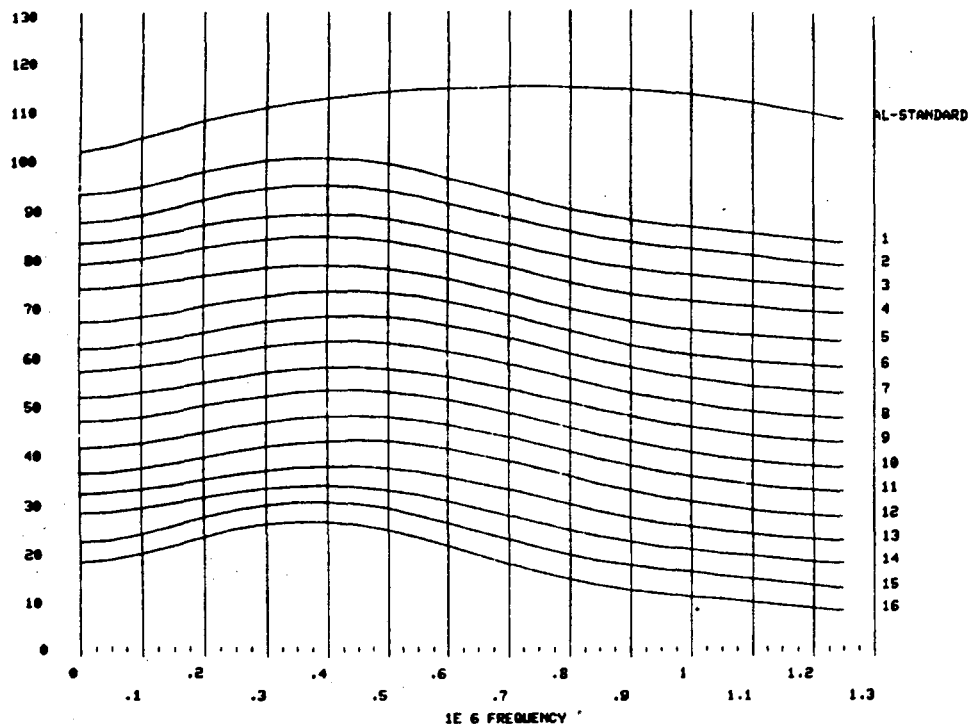
SPECIMEN : STRIPA 010, H7-R0 CONDITION : SATURATED WINDOW : 4EE-6  
 SMOOTH : 0 FILE : SPAD10.  
 P-WAVES DATE : 3 OCTOBER, 1982

Fig. E:5.10b



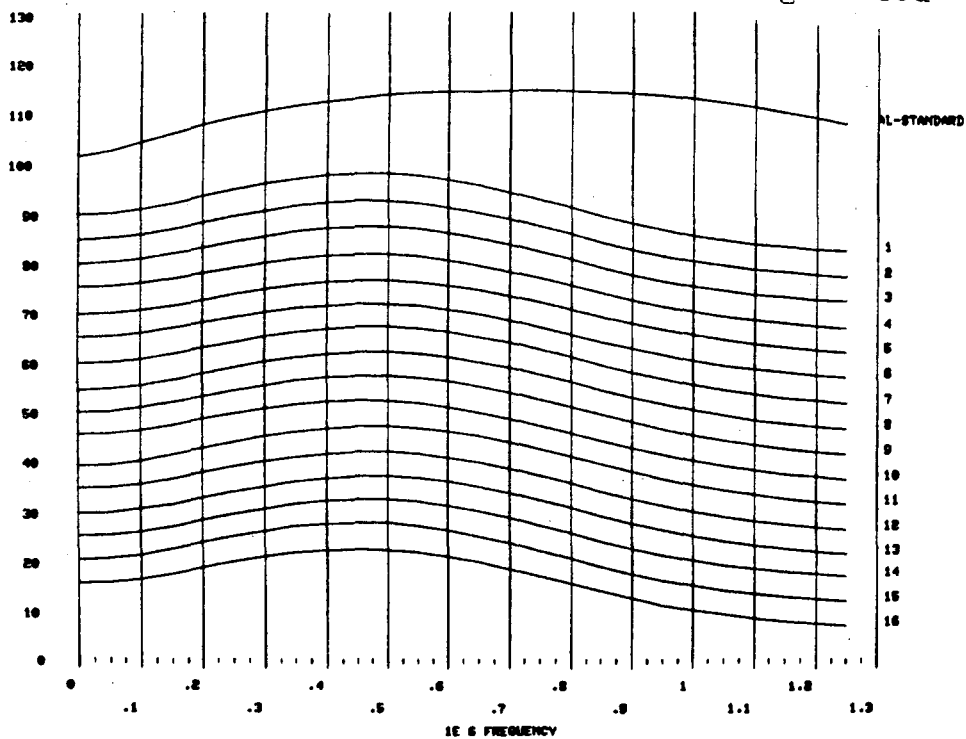
SPECIMEN : STRIPA 010, E25, N7-ND    CONDITION : DRY    WINDOW : 1+2E-6 SEC  
SMOOTH : 0    FILE : SSAD10.  
S-WAVES    DATE : 20 OCTOBER, 1982

Fig. E:5.10c



SPECIMEN : STRIPA 010, N7-ND    CONDITION : SATURATED    WINDOW : 1+2E-6 SEC  
SMOOTH : 0    FILE : SSAM10.  
S-WAVES    DATE : 3 OCTOBER, 1982

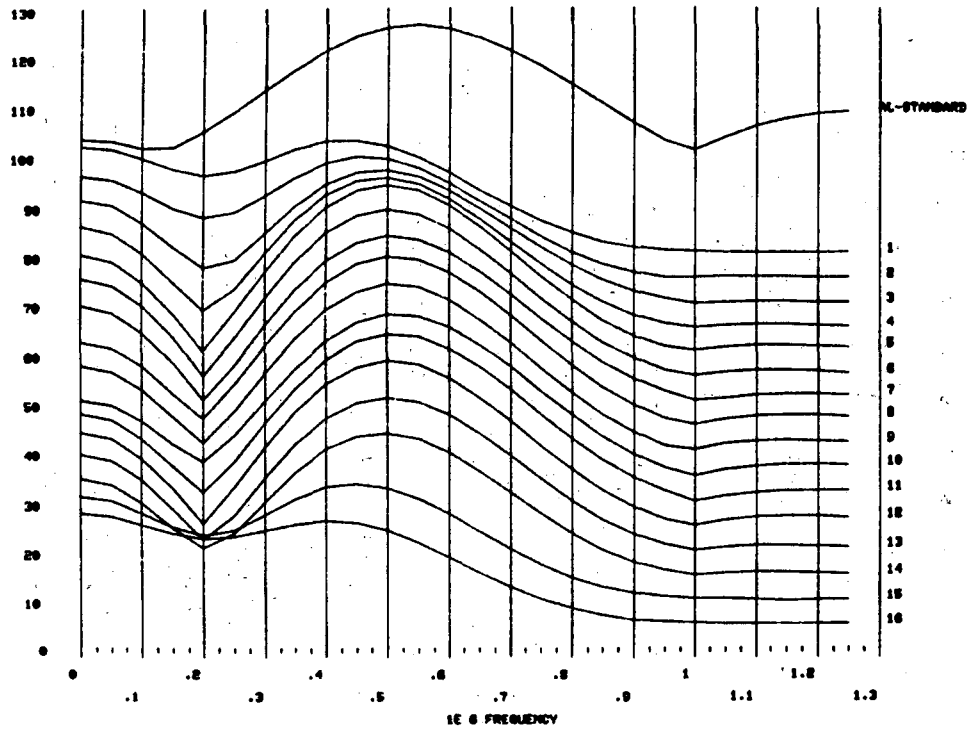
Fig. E:5.10d





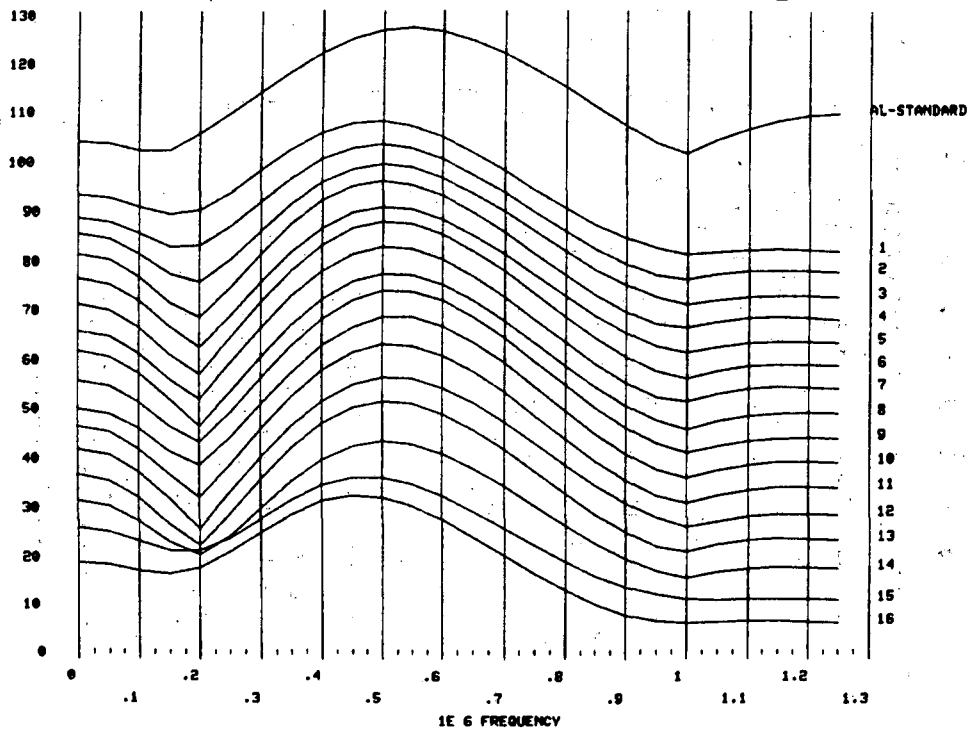
SPECIMEN : STRIPA 811, R7-R8 CONDITION : DRY WINDOW : 4E-6  
SMOOTH : 0 FILE : SPAN11.  
P-WAVES DATE : 21 SEPTEMBER, 1982

Fig. E:5.11a



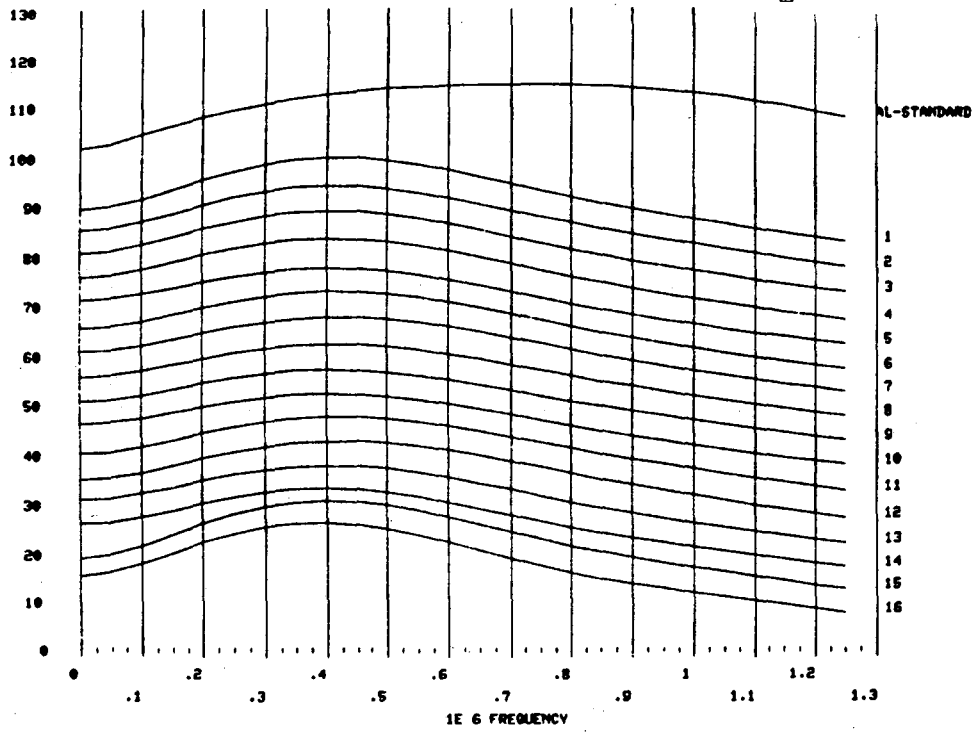
SPECIMEN : STRIPA 811, R7-R8 CONDITION : SATURATED WINDOW : 4E-6  
SMOOTH : 0 FILE : SPAN11.  
P-WAVES DATE : 3 OCTOBER, 1982

Fig. E:5.11b



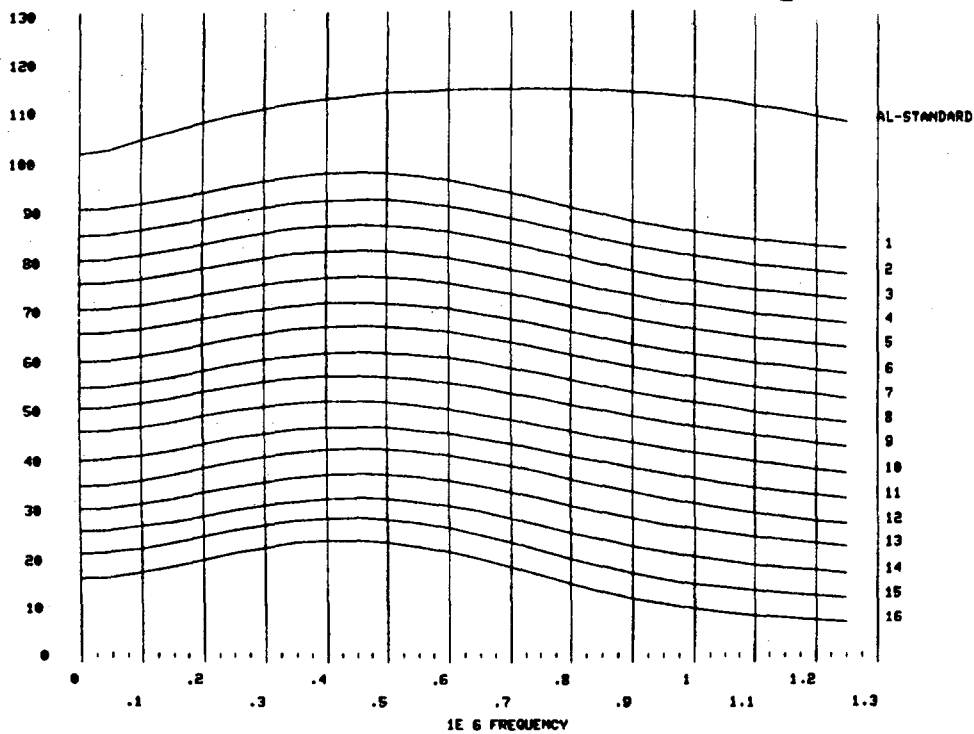
SPECIMEN : STRIPA #11, #7-RD    CONDITION : DRY    WINDOW : 1+2E-6 AT CROSSOVER  
SMOOTH : 0    FILE : SSAD11.  
5-WAVES    DATE : 23 SEPTEMBER, 1982

Fig. E:5.11c



SPECIMEN : STRIPA #11, #7-RD    CONDITION : SATURATED    WINDOW : 1+2E-6 SEC  
SMOOTH : 0    FILE : SSAM11.  
5-WAVES    DATE : 3 OCTOBER, 1982

Fig. E:5.11d



**Appendix E:6 -  $Q_\alpha$  and  $Q_\beta$  from laboratory  
test of Stripa core specimen.**

In this appendix the  $Q_\alpha$  and  $Q_\beta$  are graphed as function of  $\sigma_{ua}$  for 11 core specimens both under a saturated as well as dry state.

**Figure captions for Appendix E:6**

Fig. E:6.1a  $Q_\alpha$  as function of uniaxial stress for the dry specimen # 1

Fig. E:6.1b  $Q_\alpha$  as function of uniaxial stress for the saturated specimen # 1

Fig. E:6.1c  $Q_\beta$  as function of uniaxial stress for the dry specimen # 1

Fig. E:6.1d  $Q_\beta$  as function of uniaxial stress for the saturated specimen # 1

Fig. E:6.2a  $Q_\alpha$  as function of uniaxial stress for the dry specimen # 2

Fig. E:6.2b  $Q_\alpha$  as function of uniaxial stress for the saturated specimen # 2

Fig. E:6.2c  $Q_\beta$  as function of uniaxial stress for the dry specimen # 2

Fig. E:6.2d  $Q_\beta$  as function of uniaxial stress for the saturated specimen # 2

Fig. E:6.3a  $Q_\alpha$  as function of uniaxial stress for the dry specimen # 3

Fig. E:6.3b  $Q_\alpha$  as function of uniaxial stress for the saturated specimen # 3

Fig. E:6.3c  $Q_\beta$  as function of uniaxial stress for the dry specimen # 3

Fig. E:6.3d  $Q_\beta$  as function of uniaxial stress for the saturated specimen # 3

Fig. E:6.4a  $Q_\alpha$  as function of uniaxial stress for the dry specimen # 4

Fig. E:6.4b  $Q_\alpha$  as function of uniaxial stress for the saturated specimen # 4

Fig. E:6.4c  $Q_\beta$  as function of uniaxial stress for the dry specimen # 4

Fig. E:6.4d  $Q_\beta$  as function of uniaxial stress for the saturated specimen # 4

Fig. E:6.5a  $Q_\alpha$  as function of uniaxial stress for the dry specimen # 5

Fig. E:6.5b  $Q_\alpha$  as function of uniaxial stress for the saturated specimen # 5

Fig. E:6.5c  $Q_\beta$  as function of uniaxial stress for the dry specimen # 5

Fig. E:6.5d  $Q_\beta$  as function of uniaxial stress for the saturated specimen # 5

Fig. E:6.6a  $Q_\alpha$  as function of uniaxial stress for the dry specimen # 6

Fig. E:6.6b  $Q_\alpha$  as function of uniaxial stress for the saturated specimen # 6

Fig. E:6.6c  $Q_\beta$  as function of uniaxial stress for the dry specimen # 6

Fig. E:6.6d  $Q_\beta$  as function of uniaxial stress for the saturated specimen # 6

Fig. E:6.7a  $Q_\alpha$  as function of uniaxial stress for the dry specimen # 7

Fig. E:6.7b  $Q_\alpha$  as function of uniaxial stress for the saturated specimen # 7

Fig. E:6.7c  $Q_\beta$  as function of uniaxial stress for the dry specimen # 7

Fig. E:6.7d  $Q_\beta$  as function of uniaxial stress for the saturated specimen # 7

Fig. E:6.8a  $Q_\alpha$  as function of uniaxial stress for the dry specimen # 8

Fig. E:6.8b  $Q_\alpha$  as function of uniaxial stress for the saturated specimen # 8

Fig. E:6.8c  $Q_\beta$  as function of uniaxial stress for the dry specimen # 8

Fig. E:6.8d  $Q_\beta$  as function of uniaxial stress for the saturated specimen # 8

Fig. E:6.9a  $Q_\alpha$  as function of uniaxial stress for the dry specimen # 9

Fig. E:6.9b  $Q_\alpha$  as function of uniaxial stress for the saturated specimen # 9

Fig. E:6.9c  $Q_\beta$  as function of uniaxial stress for the dry specimen # 9

Fig. E:6.9d  $Q_\beta$  as function of uniaxial stress for the saturated specimen # 9

Fig. E:6.10a  $Q_\alpha$  as function of uniaxial stress for the dry specimen # 10

Fig. E:6.10b  $Q_\alpha$  as function of uniaxial stress for the saturated specimen # 10

Fig. E:6.10c  $Q_\beta$  as function of uniaxial stress for the dry specimen # 10

Fig. E:6.10d  $Q_\beta$  as function of uniaxial stress for the saturated specimen  
# 10

Fig. E:6.11a  $Q_\alpha$  as function of uniaxial stress for the dry specimen # 11

Fig. E:6.11b  $Q_\alpha$  as function of uniaxial stress for the saturated specimen  
# 11

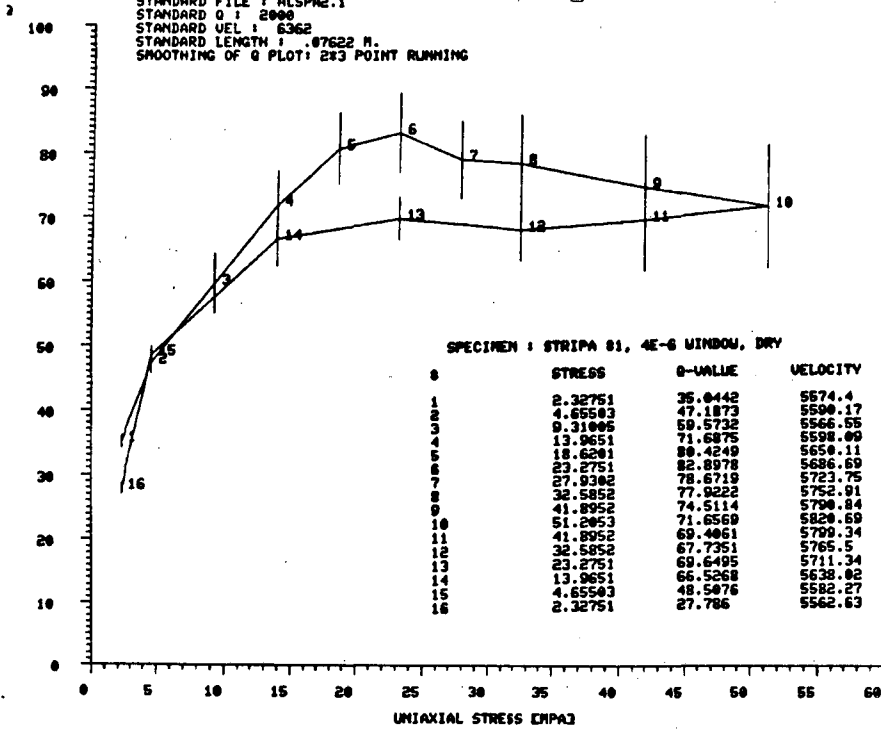
Fig. E:6.11c  $Q_\beta$  as function of uniaxial stress for the dry specimen # 11

Fig. E:6.11d  $Q_\beta$  as function of uniaxial stress for the saturated specimen  
# 11



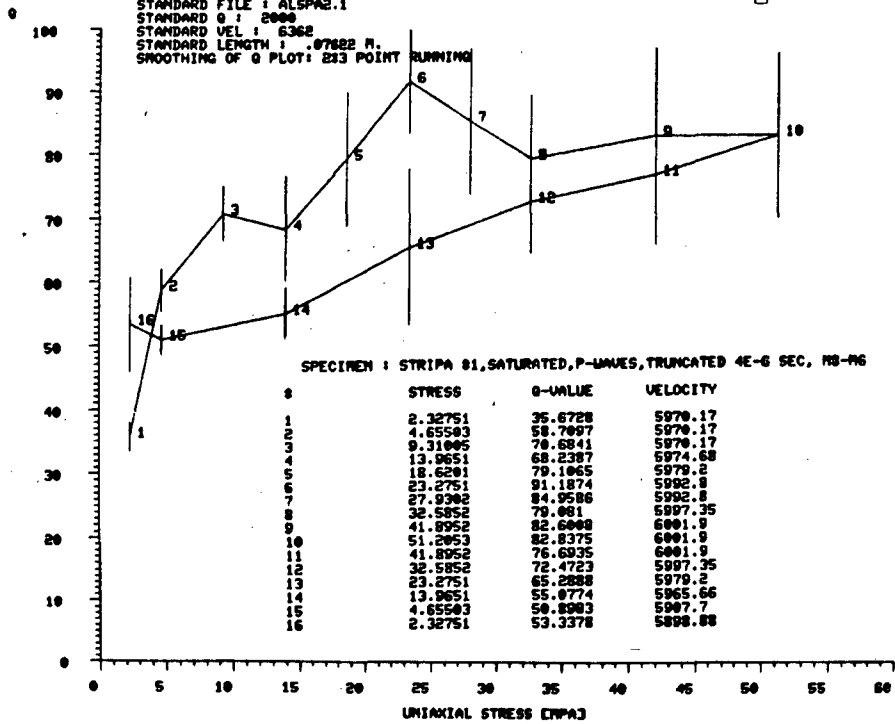
Q FOR UNIAXIAL STRESS ON CORE  
 SPECIMEN FILE : STP001.1  
 SPECIMEN : STRIPA 01, 4E-6 WINDOW, DRY  
 STANDARD FILE : ALSPAZ.1  
 STANDARD Q : 2000  
 STANDARD VEL : 6362  
 STANDARD LENGTH : .07622 M.  
 SMOOTHING OF Q PLOT: 233 POINT RUNNING

Fig. E:6.1a



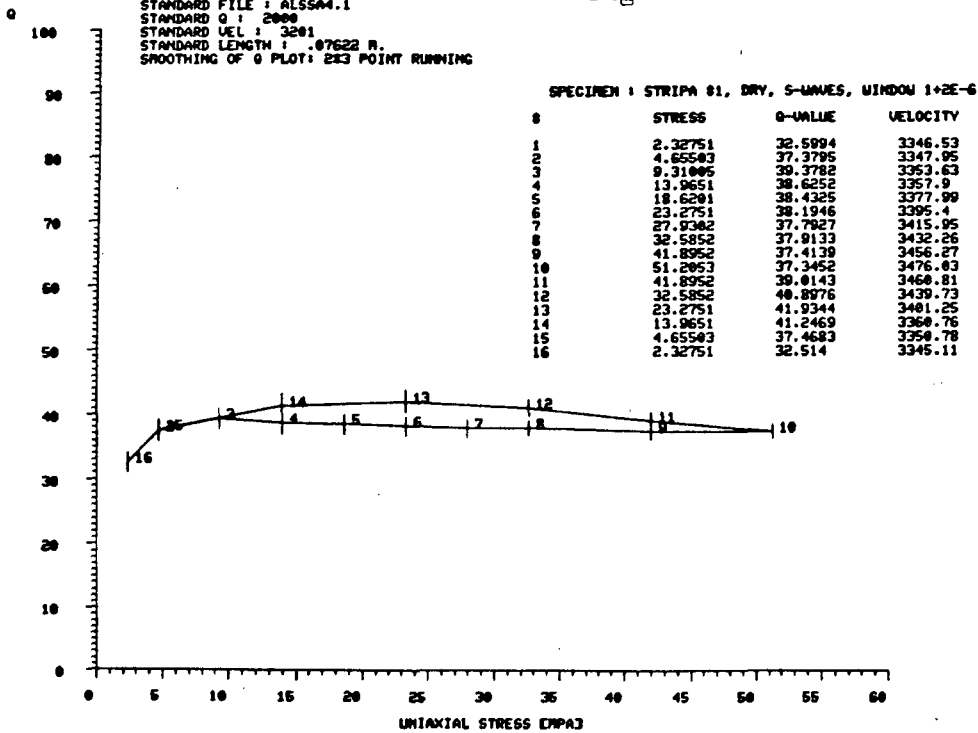
Q FOR UNIAXIAL STRESS ON CORE  
 SPECIMEN FILE : STP001.43  
 SPECIMEN : STRIPA 01, SATURATED, P-WAVES, TRUNCATED 4E-6 SEC, RB-R6  
 STANDARD FILE : ALSPAZ.1  
 STANDARD Q : 2000  
 STANDARD VEL : 6362  
 STANDARD LENGTH : .07622 M.  
 SMOOTHING OF Q PLOT: 233 POINT RUNNING

Fig. E:6.1b



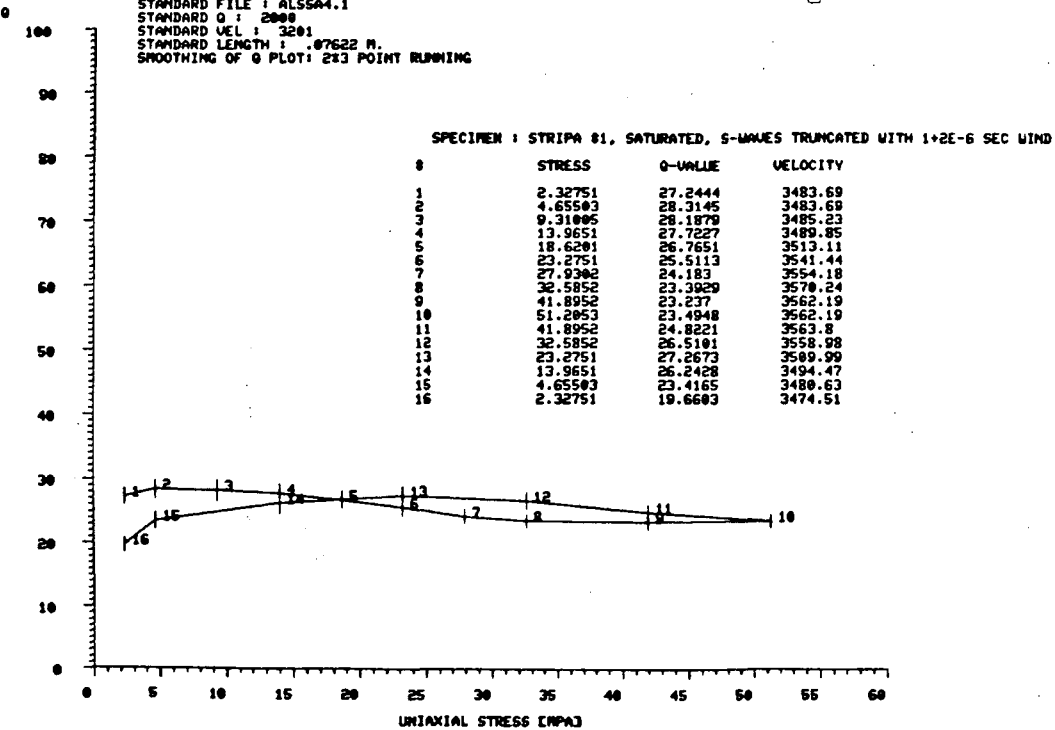
Q FOR UNIAXIAL STRESS ON CORE  
 SPECIMEN FILE : STSQD1.3  
 SPECIMEN : STRIPA #1, DRY, S-WAVES, WINDOW 1+2E-6  
 STANDARD FILE : ALLSSA4.1  
 STANDARD Q : 2000  
 STANDARD VEL : 3201  
 STANDARD LENGTH : .07622 M.  
 SMOOTHING OF Q PLOT: 2x3 POINT RUNNING

Fig. E:6.1c



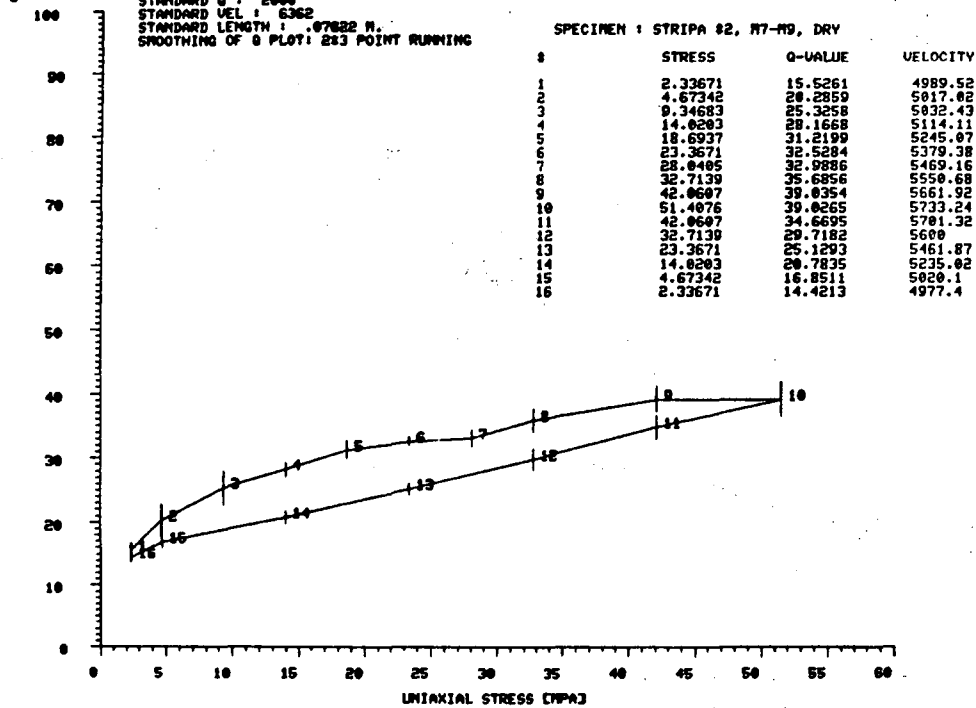
Q FOR UNIAXIAL STRESS ON CORE  
 SPECIMEN FILE : STSQM1.3  
 SPECIMEN : STRIPA #1, SATURATED, S-WAVES TRUNCATED WITH 1+2E-6 SEC WIND  
 STANDARD FILE : ALLSSA4.1  
 STANDARD Q : 2000  
 STANDARD VEL : 3201  
 STANDARD LENGTH : .07622 M.  
 SMOOTHING OF Q PLOT: 2x3 POINT RUNNING

Fig. E:6.1d



Q FOR UNIAXIAL STRESS ON CORE  
 SPECIMEN FILE : STPODE.U1  
 SPECIMEN : STRIPA #2, N7-M9, DRY  
 STANDARD FILE : ALSPAR.1  
 STANDARD Q : 2000  
 STANDARD VEL : 6362  
 STANDARD LENGTH : .07822 M.  
 SMOOTHING OF Q PLOT: 2x3 POINT RUNNING

Fig. E:6.2a

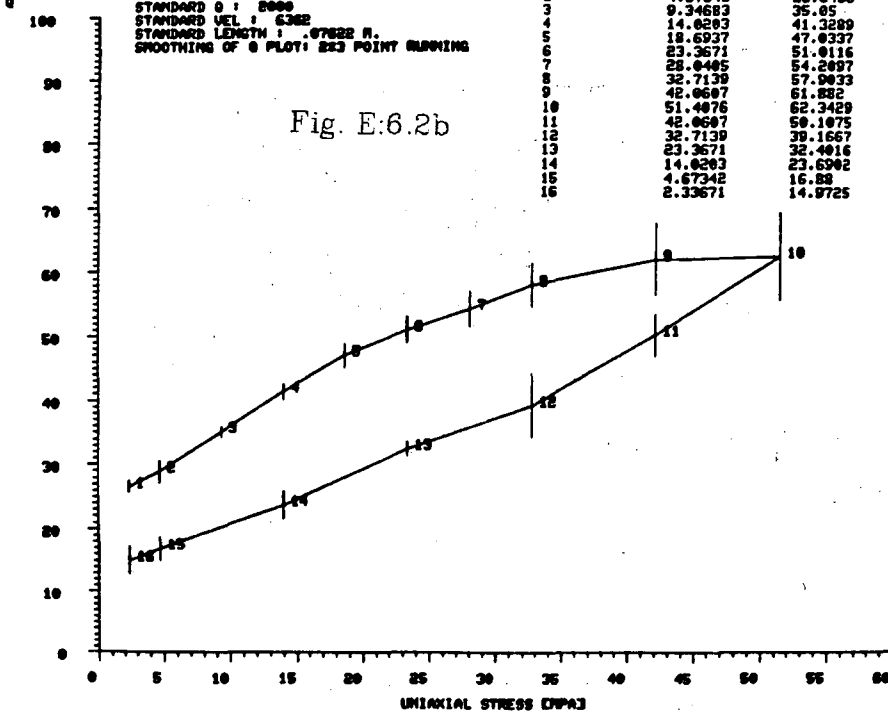


Q FOR UNIAXIAL STRESS ON CORE  
 SPECIMEN FILE : STPODE.U1  
 SPECIMEN : STRIPA #2, SATURATED  
 STANDARD FILE : ALSPAR.1  
 STANDARD Q : 2000  
 STANDARD VEL : 6362  
 STANDARD LENGTH : .07822 M.  
 SMOOTHING OF Q PLOT: 2x3 POINT RUNNING

SPECIMEN : STRIPA #2, SATURATED

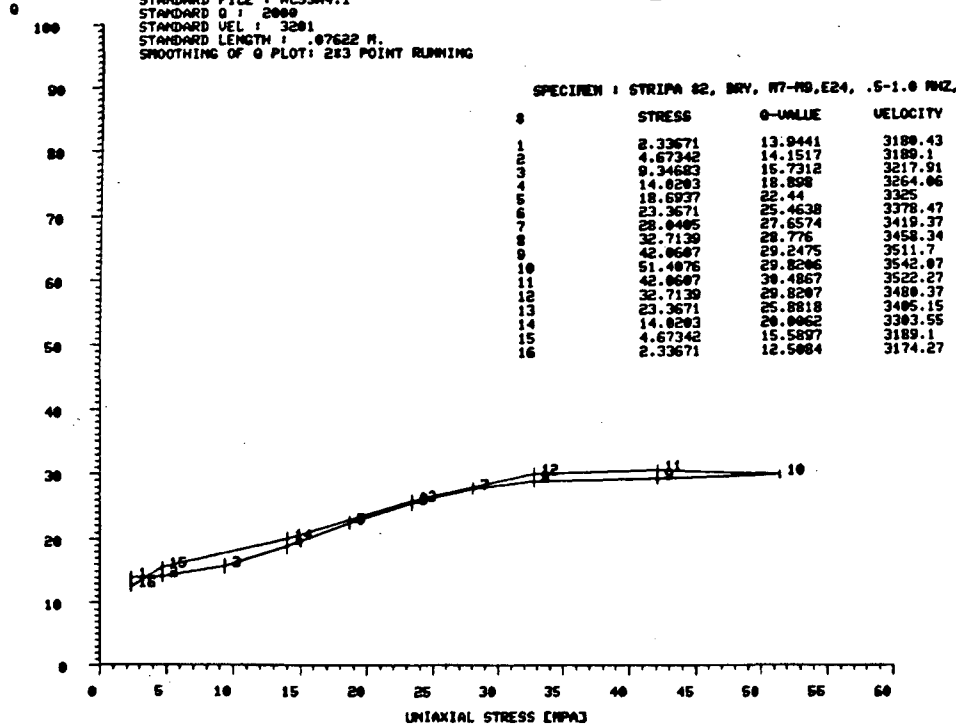
#	STRESS	Q-VALUE	VELOCITY
1	2.33671	26.5204	5914.62
2	4.67342	28.8483	5935.33
3	9.34683	35.05	5954.57
4	14.0203	41.3289	5877.19
5	18.6937	47.0337	5994.1
6	23.3671	51.0116	5922.59
7	28.0405	54.2087	5923.83
8	32.7139	57.9033	5932.51
9	42.0607	61.882	5949.75
10	51.4076	62.3429	5967.08
11	42.0607	50.1075	5958.4
12	32.7139	39.1667	5932.51
13	23.3671	32.4016	5856.18
14	14.0203	23.6902	5697.36
15	4.67342	16.88	5502.22
16	2.33671	14.9725	5513.32

Fig. E:6.2b



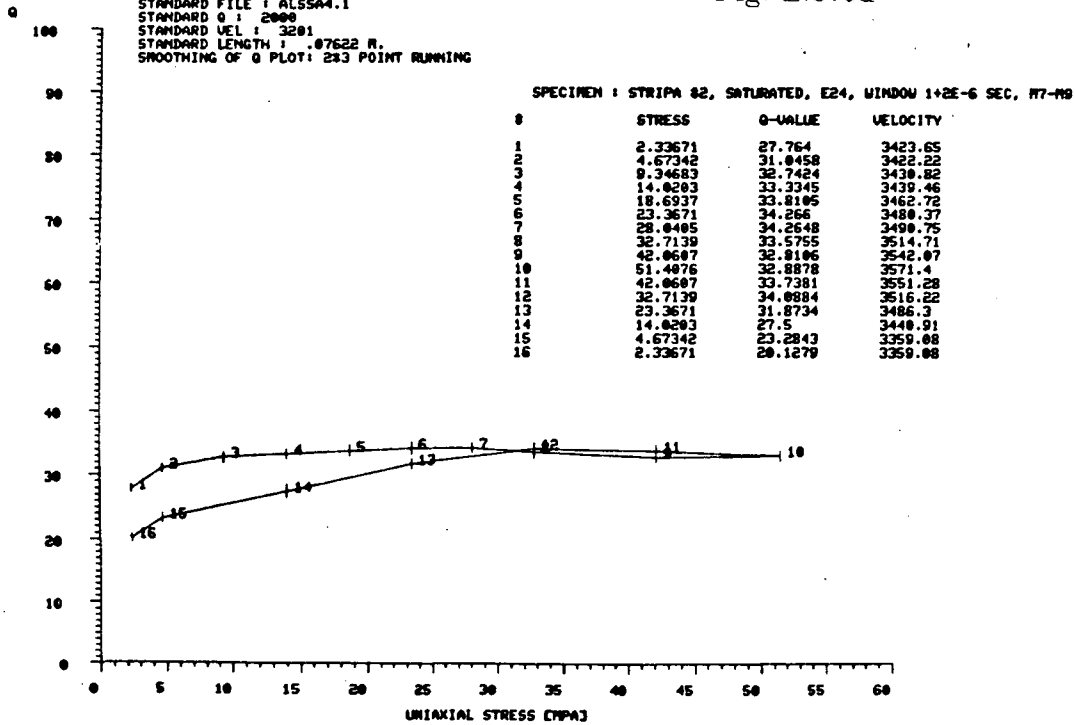
Q FOR UNIAXIAL STRESS ON CORE  
 SPECIMEN FILE : STSQD2.3  
 SPECIMEN : STRIPA 82, DRY, N7-R0,E24, .5-1.0 MHZ,  
 STANDARD FILE : ALSSA4.1  
 STANDARD Q : 2000  
 STANDARD VEL : 3201  
 STANDARD LENGTH : .07622 M.  
 SMOOTHING OF Q PLOT: 283 POINT RUNNING

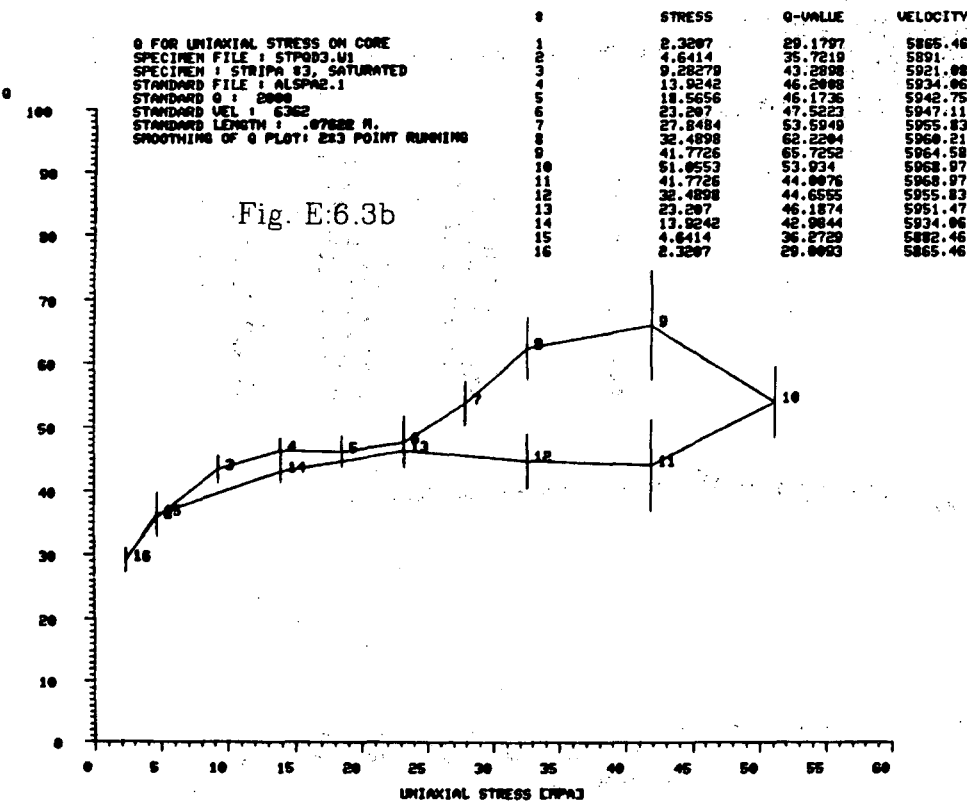
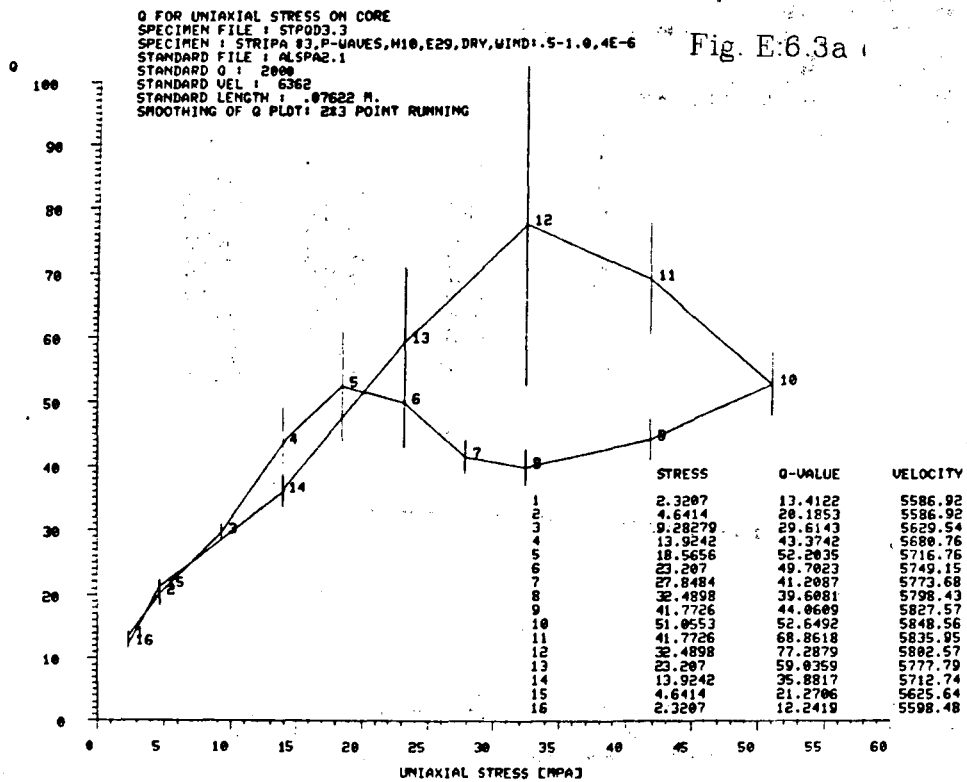
Fig. E:6.2c



Q FOR UNIAXIAL STRESS ON CORE  
 SPECIMEN FILE : STSQM2.3  
 SPECIMEN : STRIPA 82, SATURATED, E24, WINDOW 1+2E-6 SEC, N7-R0  
 STANDARD FILE : ALSSA4.1  
 STANDARD Q : 2000  
 STANDARD VEL : 3201  
 STANDARD LENGTH : .07622 M.  
 SMOOTHING OF Q PLOT: 283 POINT RUNNING

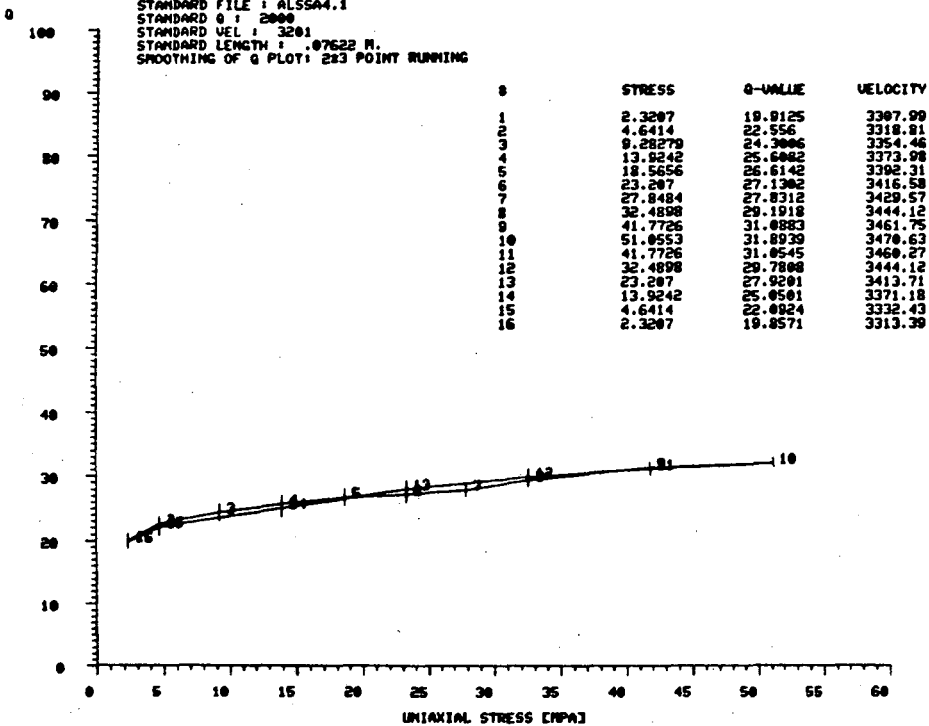
Fig. E:6.2d





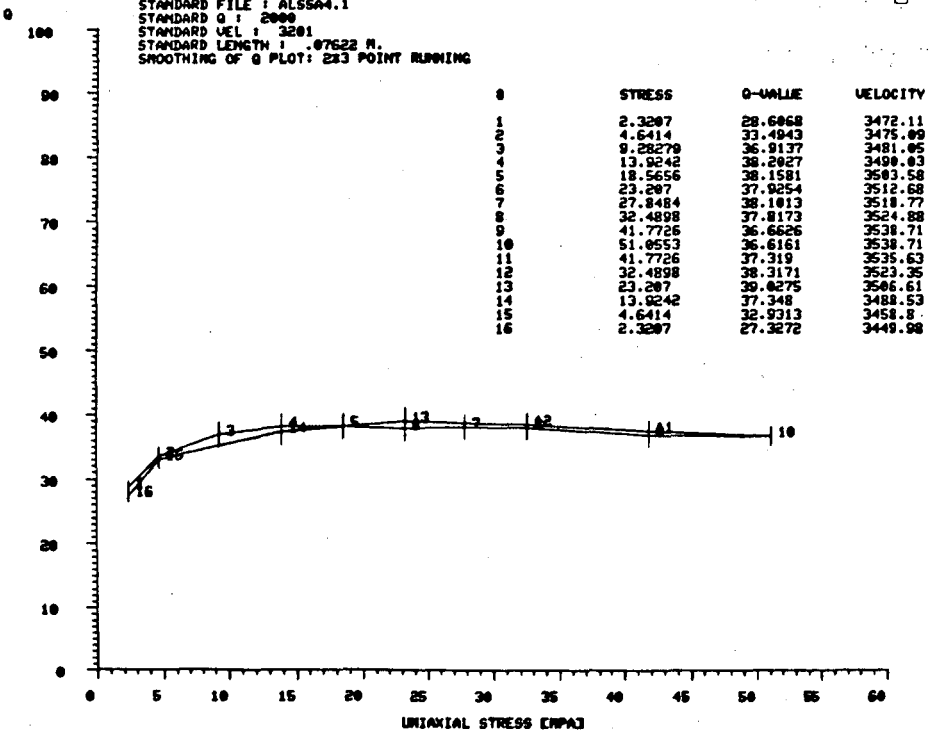
Q FOR UNIAXIAL STRESS ON CORE  
 SPECIMEN FILE : ST5003.3  
 SPECIMEN : STRIPA 83, S-WAVES TRUNCATED WITH 1+2E-6 SEC WIND, E29/M10, 821019  
 STANDARD FILE : ALSSA4.1  
 STANDARD Q : 2000  
 STANDARD VEL : 3201  
 STANDARD LENGTH : .07622 M.  
 SMOOTHING OF Q PLOT: 2x3 POINT RUNNING

Fig. E:6.3c



Q FOR UNIAXIAL STRESS ON CORE  
 SPECIMEN FILE : ST5003.3  
 SPECIMEN : STRIPA 83, S-WAVES TRUNCATED WITH 1+2E-6 SEC WIND, SATURATED, M10/E29  
 STANDARD FILE : ALSSA4.1  
 STANDARD Q : 2000  
 STANDARD VEL : 3201  
 STANDARD LENGTH : .07622 M.  
 SMOOTHING OF Q PLOT: 2x3 POINT RUNNING

Fig. E:6.3d



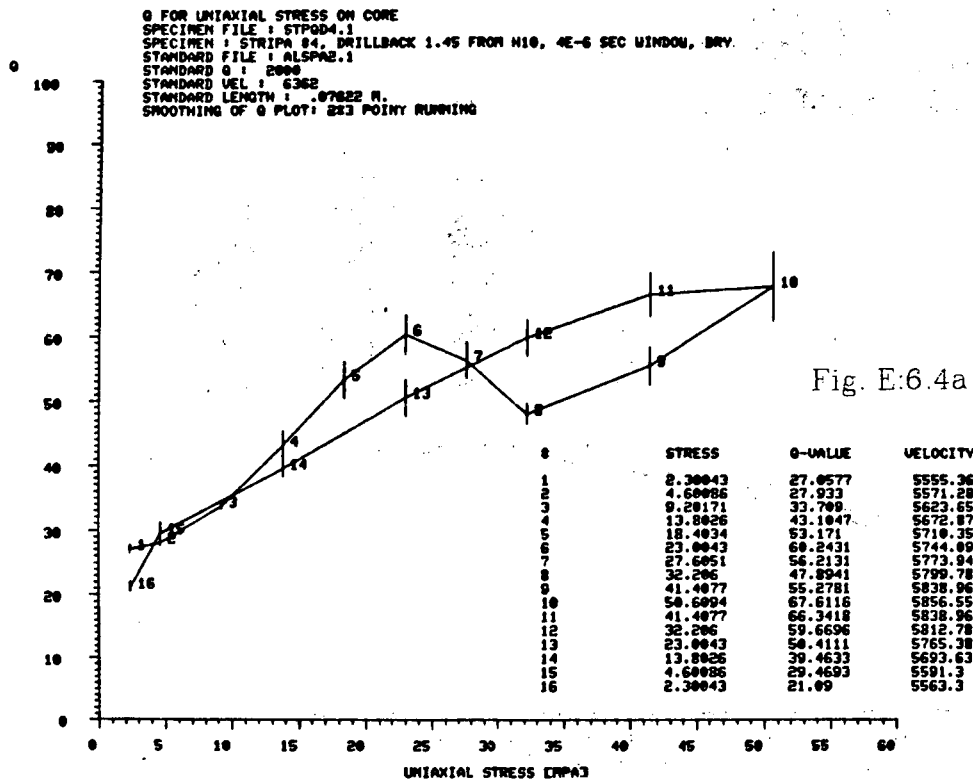


Fig. E:6.4a

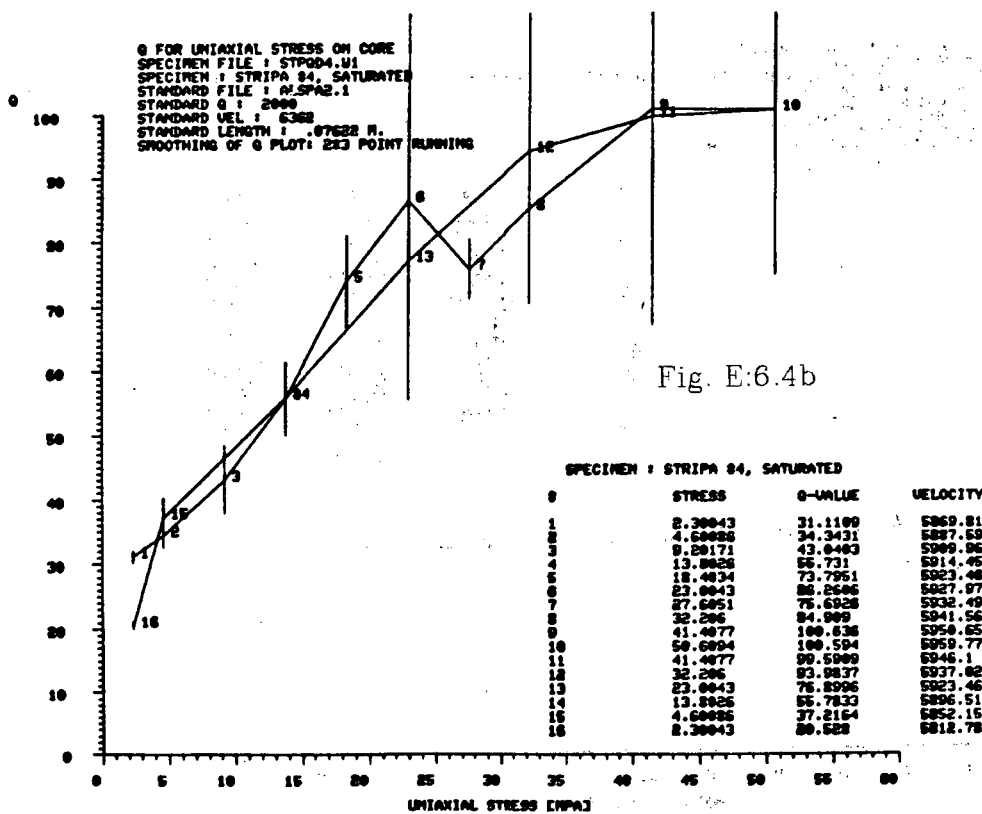
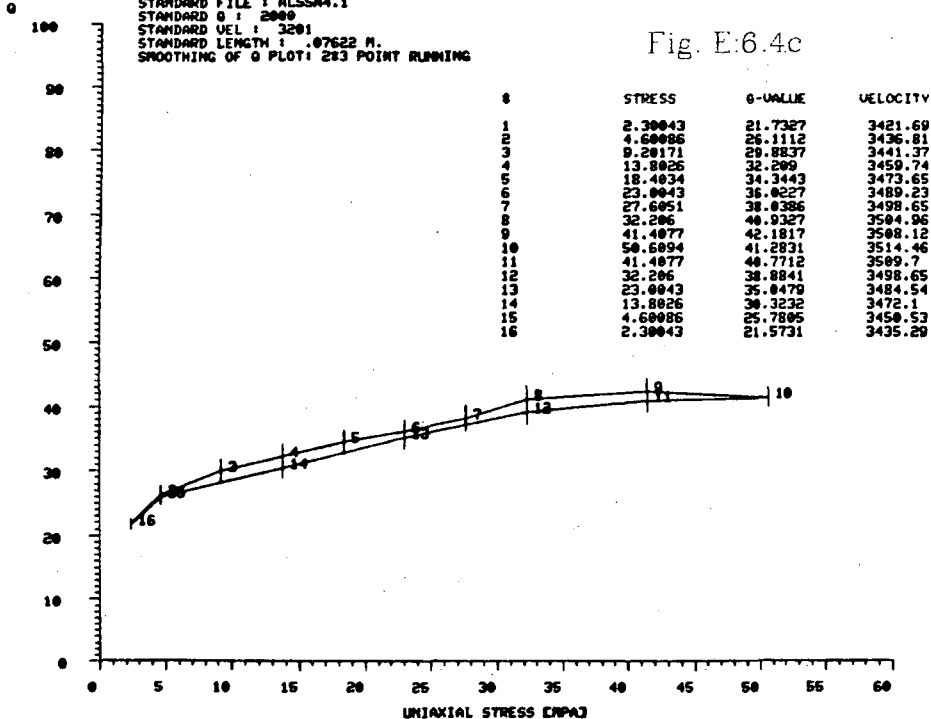


Fig. E:6.4b

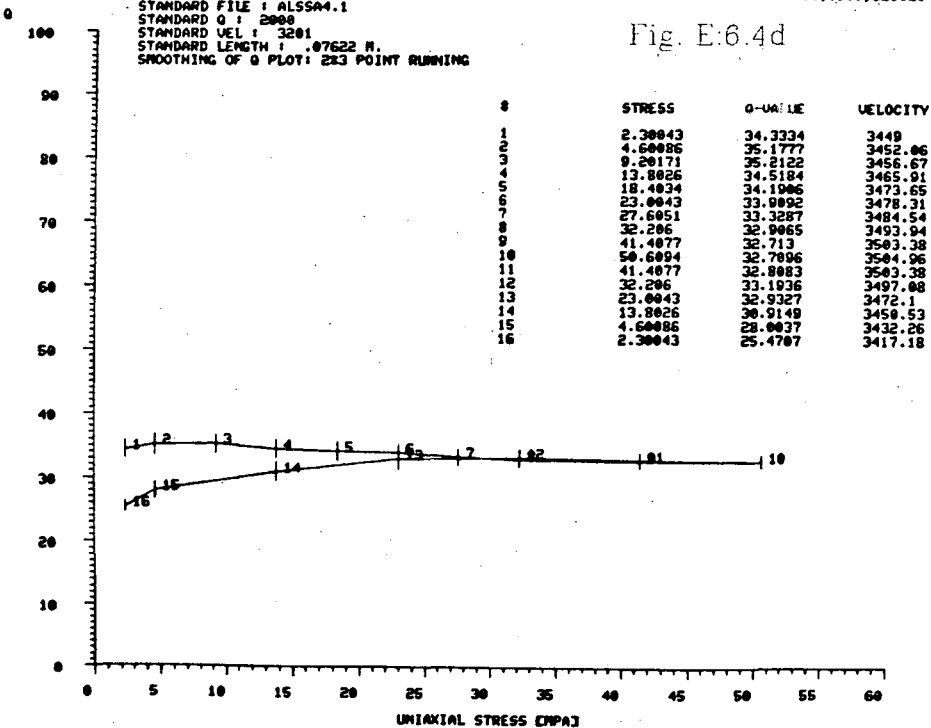
0 FOR UNIAXIAL STRESS ON CORE  
 SPECIMEN FILE : STSQM4.3  
 SPECIMEN : STRIPA 84, 5-WAVES TRUNCATED WITH 1+2E-6 SEC WIND, DBEX-1 1.45 FROM H10,130 C  
 STANDARD FILE : ALSSM4.1  
 STANDARD Q : 2000  
 STANDARD VEL : 3201  
 STANDARD LENGTH : .07622 M.  
 SMOOTHING OF Q PLOT: 283 POINT RUNNING

Fig. E:6.4c



0 FOR UNIAXIAL STRESS ON CORE  
 SPECIMEN FILE : STSQM4.3  
 SPECIMEN : STRIPA 84, 5-WAVES TRUNC. WITH 1+2E-6 SEC WIND, DBEX-1 1.45 FROM H10,130C,821020  
 STANDARD FILE : ALSSM4.1  
 STANDARD Q : 2000  
 STANDARD VEL : 3201  
 STANDARD LENGTH : .07622 M.  
 SMOOTHING OF Q PLOT: 283 POINT RUNNING

Fig. E:6.4d





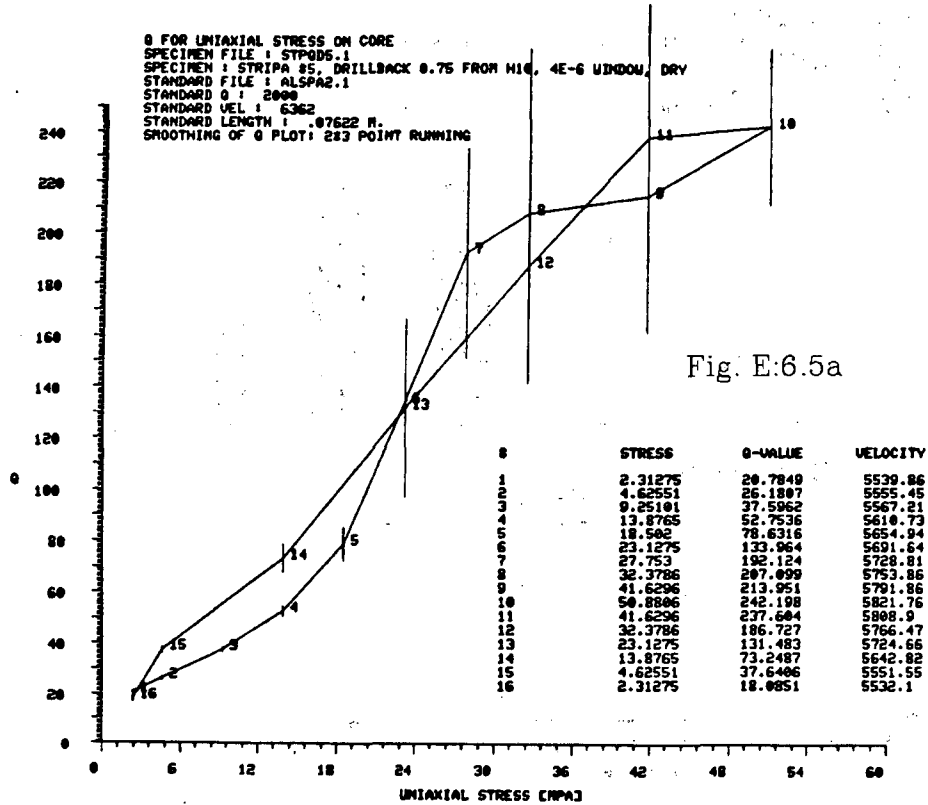


Fig. E:6.5a

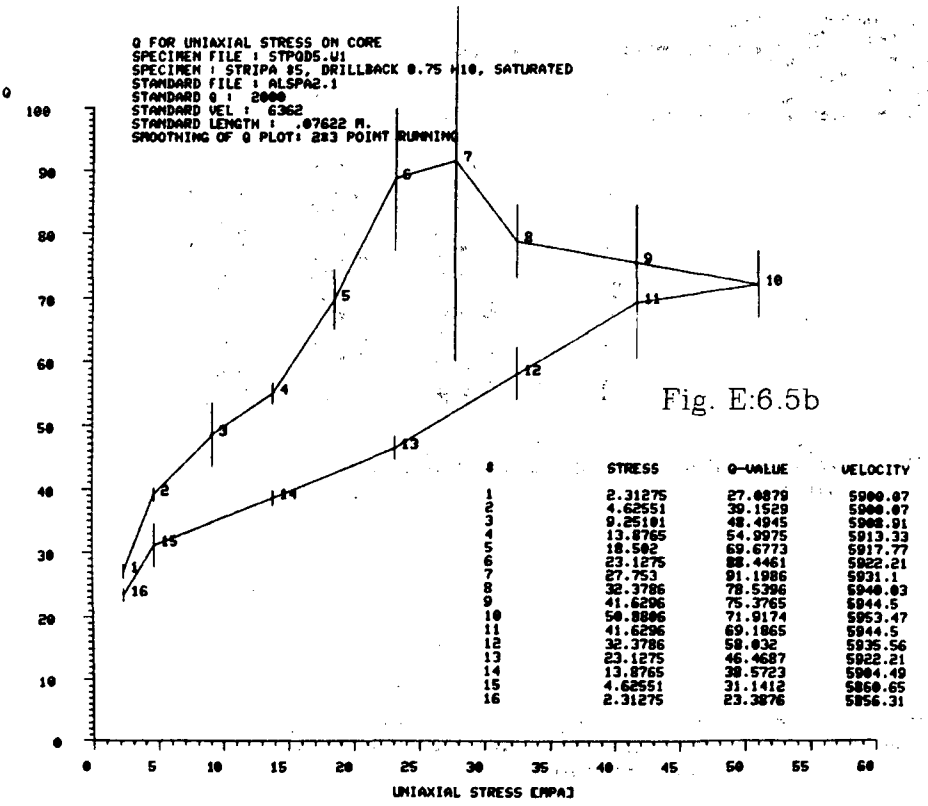
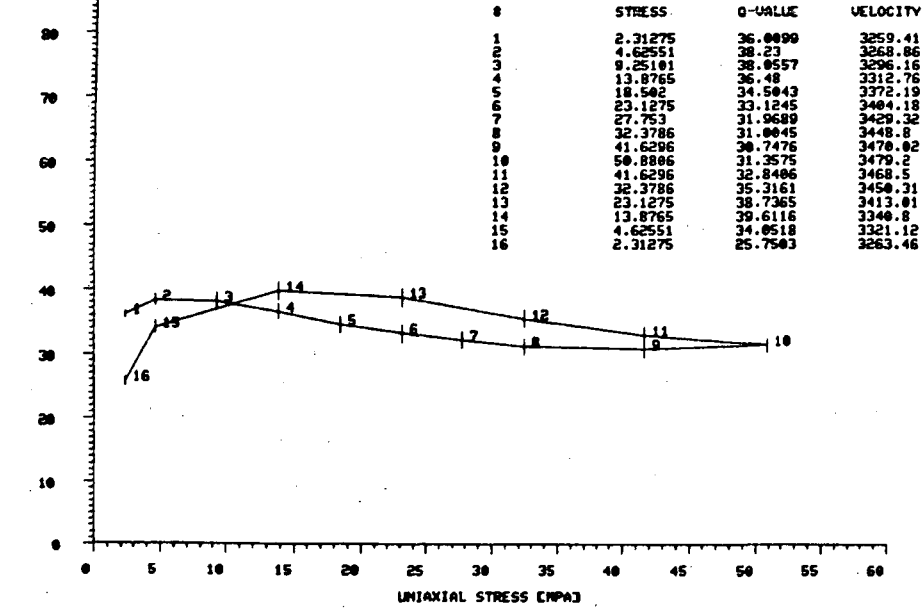


Fig. E:6.5b

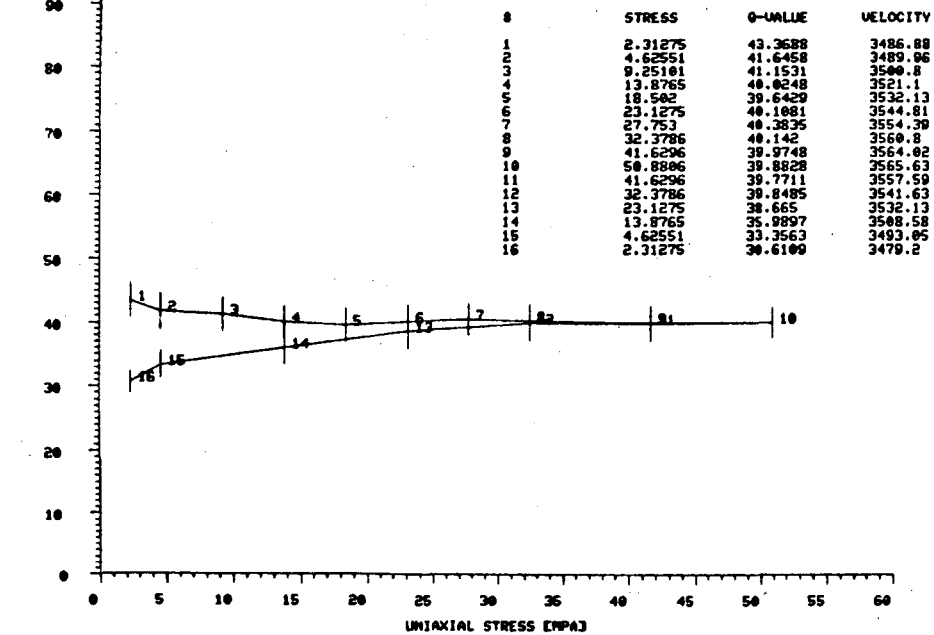
Q FOR UNIAXIAL STRESS ON CORE  
 SPECIMEN FILE : ST5005.3  
 SPECIMEN : STRIPA 85, S-WAVES TRUNC WITH 1+2E-6 SEC, DBEX-1 0.75H F H10, DRY, 200, 821820  
 STANDARD FILE : ALSSA4.1  
 STANDARD Q : 2000  
 STANDARD VEL : 3201  
 STANDARD LENGTH : .07622 M.  
 SMOOTHING OF Q PLOT: 283 POINT RUNNING

Fig. E:6.5c



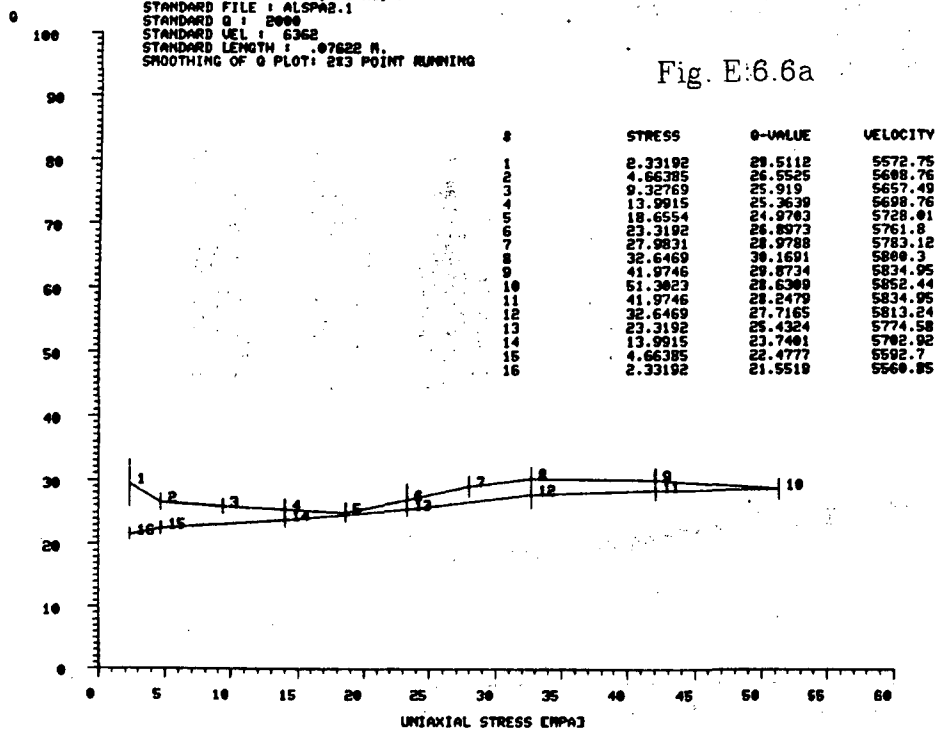
Q FOR UNIAXIAL STRESS ON CORE  
 SPECIMEN FILE : ST5005.3  
 SPECIMEN : STRIPA 85, S-WAVES TRUNCATED WITH 1+2E-6 SEC WIND, DBEX-1 0.75H F. H10, 200 C  
 STANDARD FILE : ALSSA4.1  
 STANDARD Q : 2000  
 STANDARD VEL : 3201  
 STANDARD LENGTH : .07622 M.  
 SMOOTHING OF Q PLOT: 283 POINT RUNNING

Fig. E:6.5d



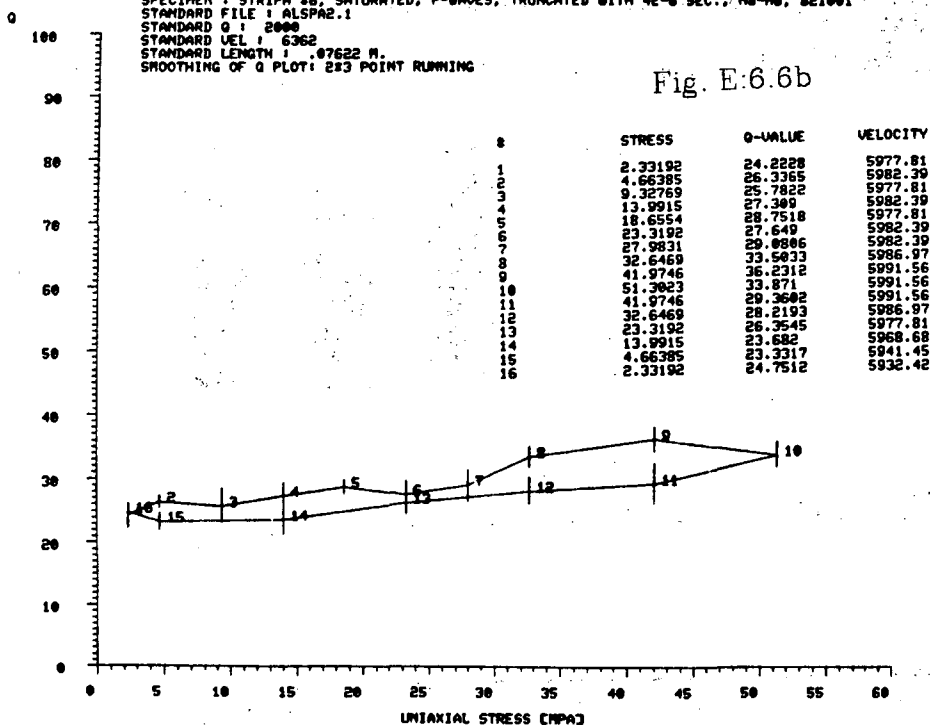
Q FOR UNIAXIAL STRESS ON CORE  
 SPECIMEN FILE : STPDG.01  
 SPECIMEN : STRIPA 86, NS-NG, DRY  
 STANDARD FILE : ALSPA2.1  
 STANDARD Q : 2000  
 STANDARD VEL : 6362  
 STANDARD LENGTH : .07622 M.  
 SMOOTHING OF Q PLOT: 2X3 POINT RUNNING

Fig. E:6.6a



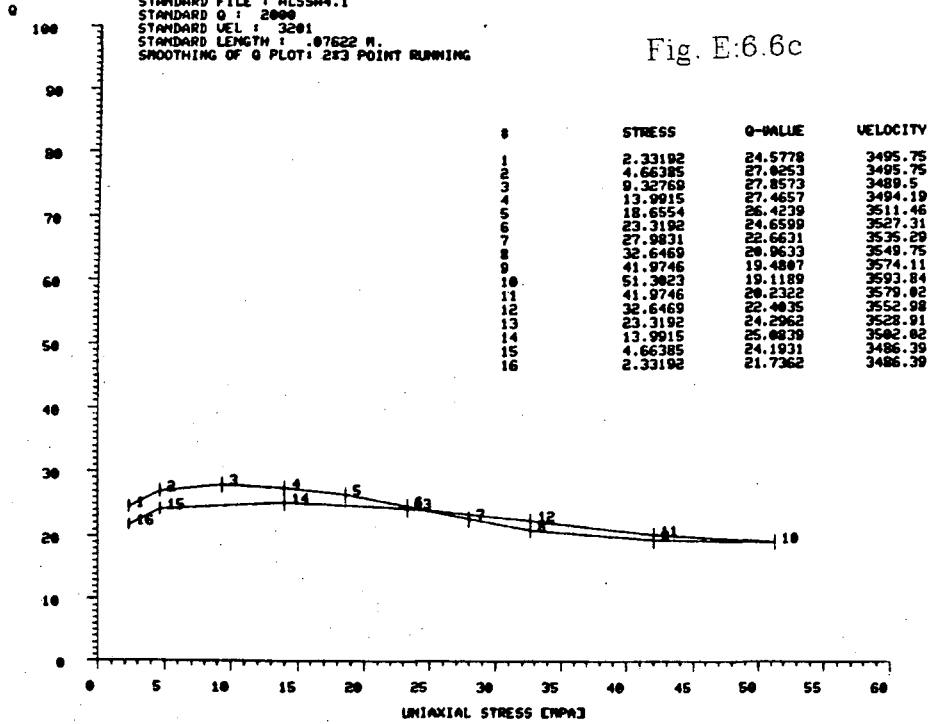
Q FOR UNIAXIAL STRESS ON CORE  
 SPECIMEN FILE : STPDG.01  
 SPECIMEN : STRIPA 86, SATURATED, P-WAVES, TRUNCATED WITH 4E-6 SEC., NS-NG, S21001  
 STANDARD FILE : ALSPA2.1  
 STANDARD Q : 2000  
 STANDARD VEL : 6362  
 STANDARD LENGTH : .07622 M.  
 SMOOTHING OF Q PLOT: 2X3 POINT RUNNING

Fig. E:6.6b



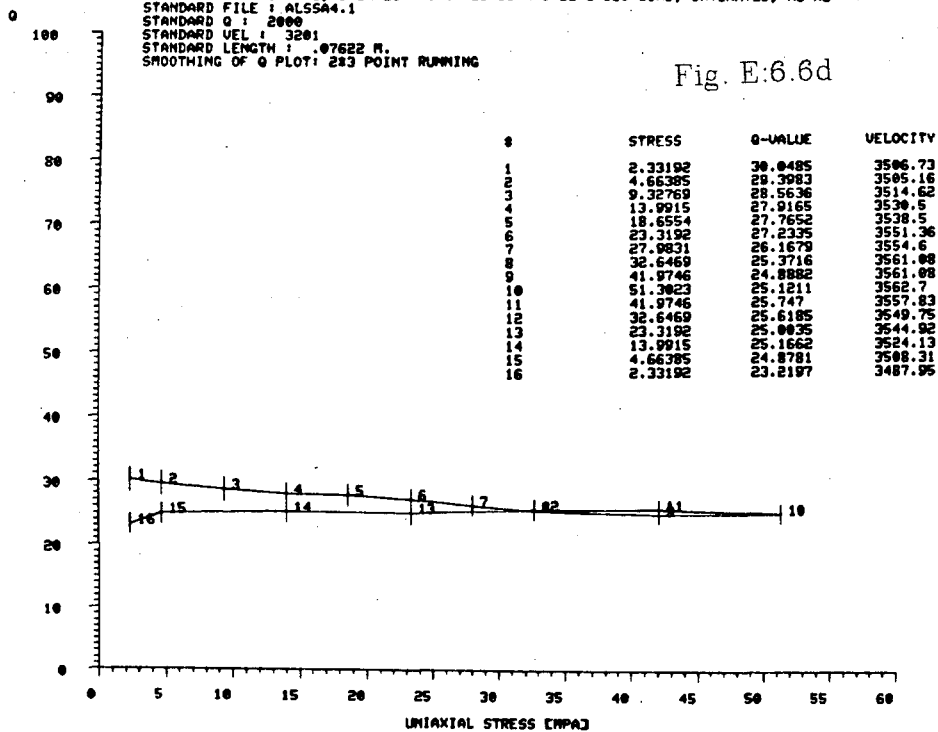
Q FOR UNIAXIAL STRESS ON CORE  
 SPECIMEN FILE : ST50D6.3  
 SPECIMEN : STRIPA 86, S-WAVES TRUNCATED WITH 1+2E-6 SEC WIND, DRY, E22, N8-N6, 821020  
 STANDARD FILE : ALS5A4.1  
 STANDARD Q : 2000  
 STANDARD VEL : 3201  
 STANDARD LENGTH : .07622 M.  
 SMOOTHING OF Q PLOT: 283 POINT RUNNING

Fig. E:6.6c



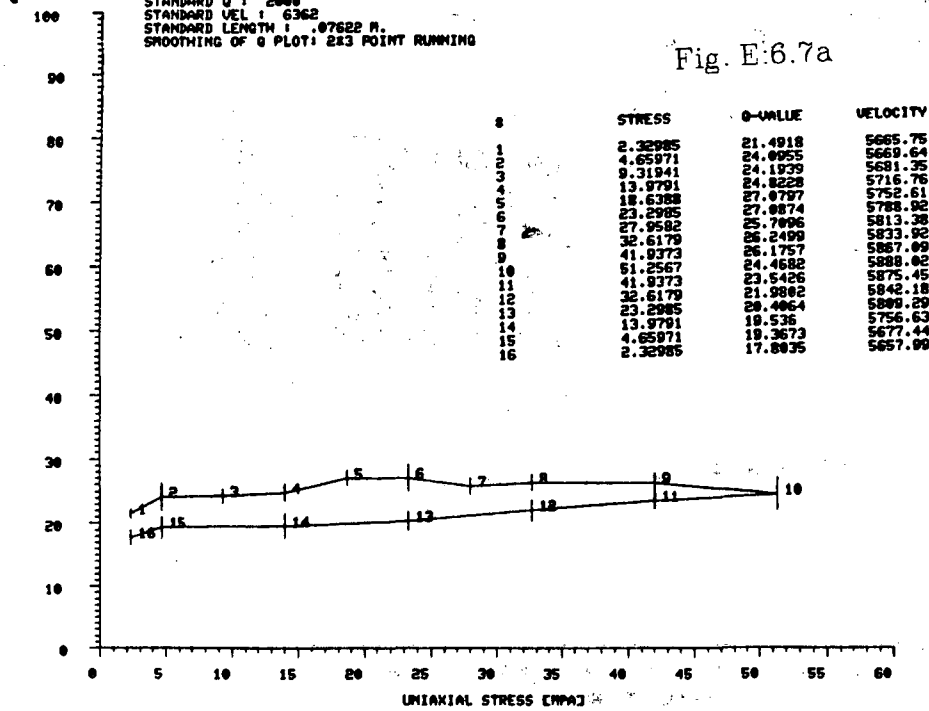
Q FOR UNIAXIAL STRESS ON CORE  
 SPECIMEN FILE : ST50A6.01  
 SPECIMEN : STRIPA 86, S-WAVES TRUNCATED WITH 1+2E-6 SEC WIND, SATURATED, N8-N6  
 STANDARD FILE : ALS5A4.1  
 STANDARD Q : 2000  
 STANDARD VEL : 3201  
 STANDARD LENGTH : .07622 M.  
 SMOOTHING OF Q PLOT: 283 POINT RUNNING

Fig. E:6.6d



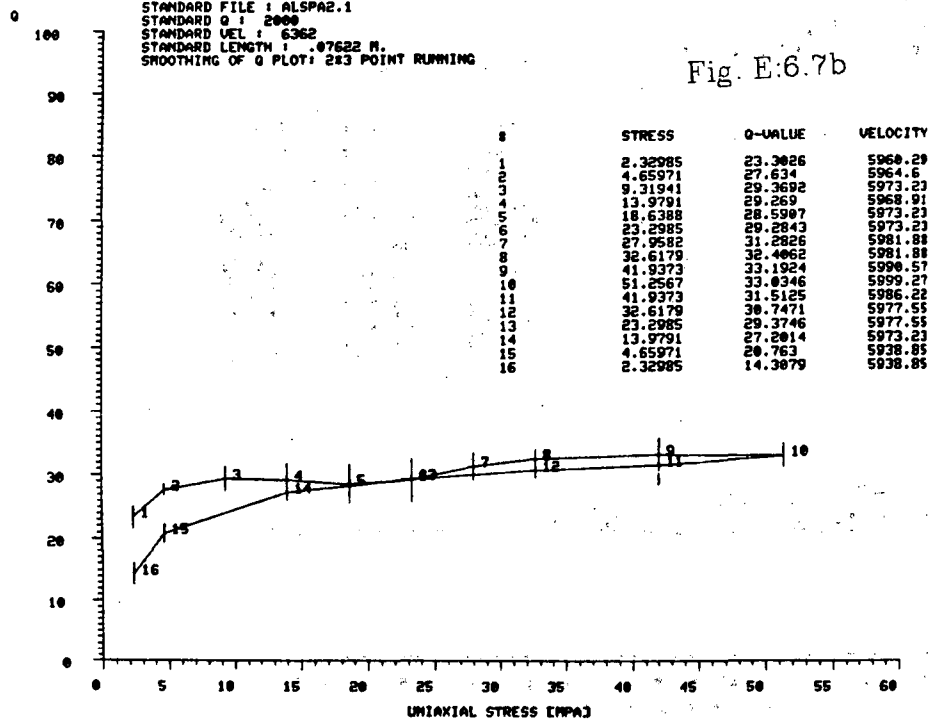
Q FOR UNIAXIAL STRESS ON CORE  
 SPECIMEN FILE : STPAD7.01  
 SPECIMEN : STRIPA #7, RD-RG, DRY  
 STANDARD FILE : ALSPA2.1  
 STANDARD Q : 2000  
 STANDARD VEL : 6362  
 STANDARD LENGTH : .07622 M.  
 SMOOTHING OF Q PLOT: 2x3 POINT RUNNING

Fig. E:6.7a



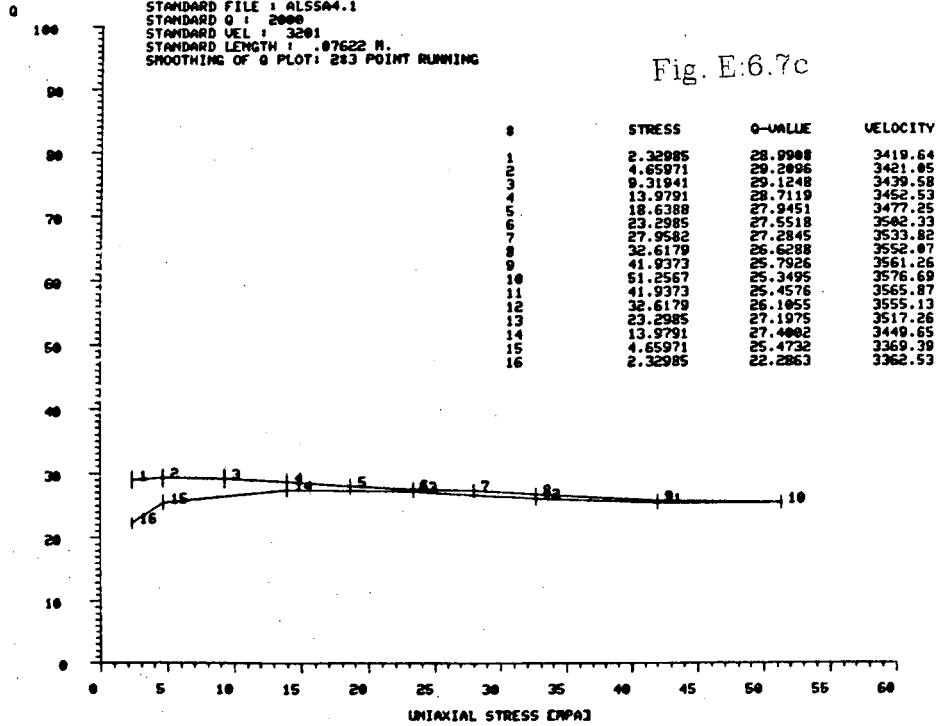
Q FOR UNIAXIAL STRESS ON CORE  
 SPECIMEN FILE : STPDW7.01  
 SPECIMEN : STRIPA #7, P-WAVES, SATURATED, TRUNCATED WITH 4E-6 SEC. RD-RG, 821001  
 STANDARD FILE : ALSPA2.1  
 STANDARD Q : 2000  
 STANDARD VEL : 6362  
 STANDARD LENGTH : .07622 M.  
 SMOOTHING OF Q PLOT: 2x3 POINT RUNNING

Fig. E:6.7b



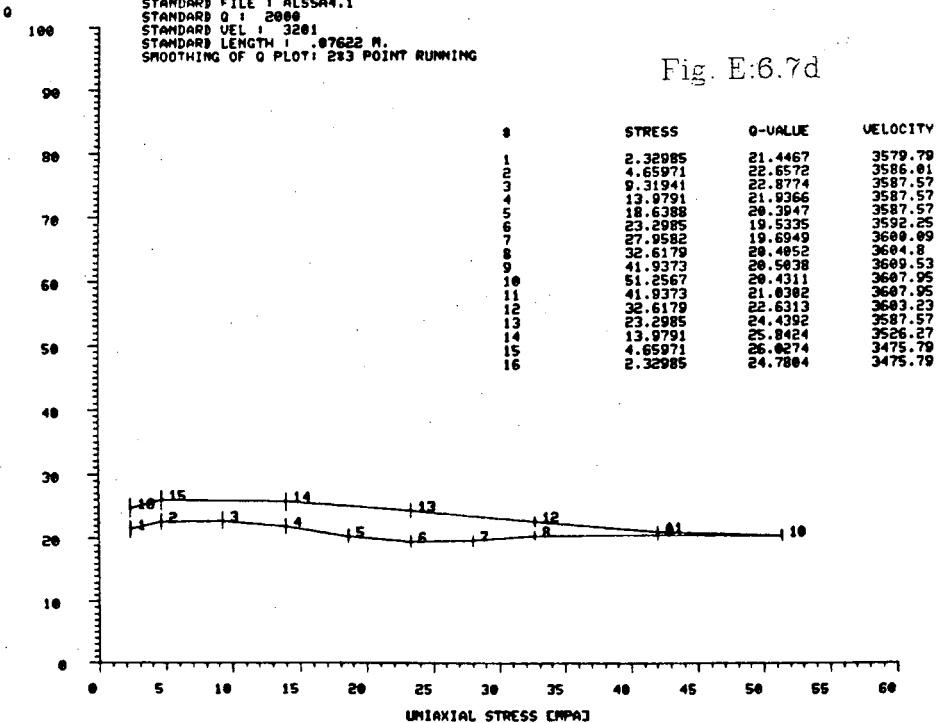
Q FOR UNIAXIAL STRESS ON CORE  
 SPECIMEN FILE : STSQD7.3  
 SPECIMEN : STRIPA 87, 5-WAVES TRUNCATED WITH 1+2E-6 SEC WIND, DRY, E22,FB-N6, 821020  
 STANDARD FILE : ALSSA4.1  
 STANDARD Q : 2000  
 STANDARD VEL : 3201  
 STANDARD LENGTH : .07622 M.  
 SMOOTHING OF Q PLOT: 283 POINT RUNNING

Fig. E:6.7c



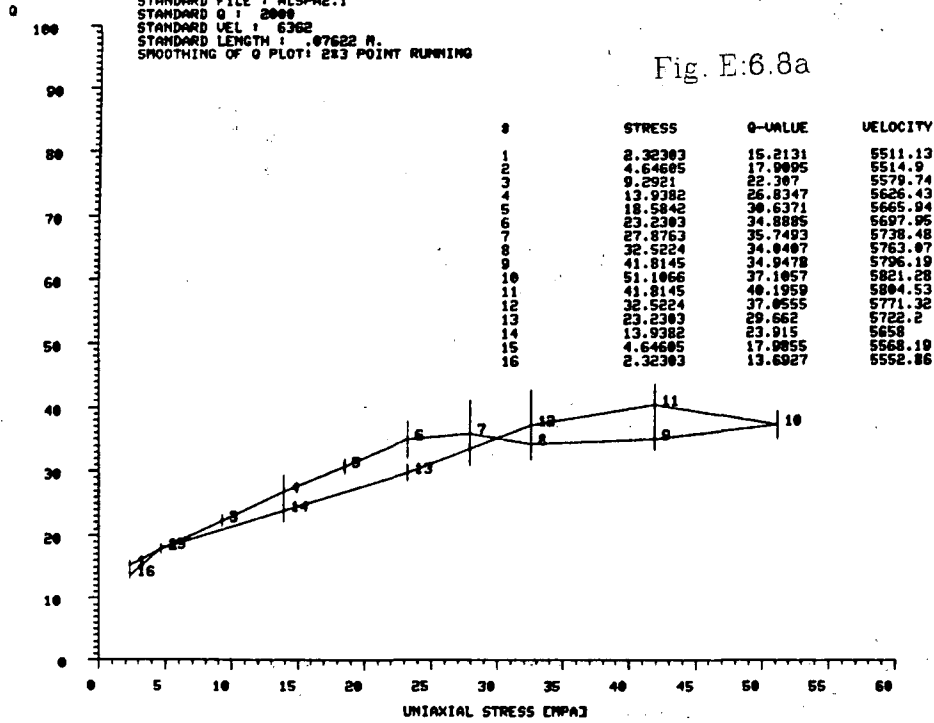
Q FOR UNIAXIAL STRESS ON CORE  
 SPECIMEN FILE : STSQD7.01  
 SPECIMEN : STRIPA 87, SATURATED, TRUNCATED S-WAVES WITH 1+2E-6 SEC WINDOW  
 STANDARD FILE : ALSSA4.1  
 STANDARD Q : 2000  
 STANDARD VEL : 3201  
 STANDARD LENGTH : .07622 M.  
 SMOOTHING OF Q PLOT: 283 POINT RUNNING

Fig. E:6.7d



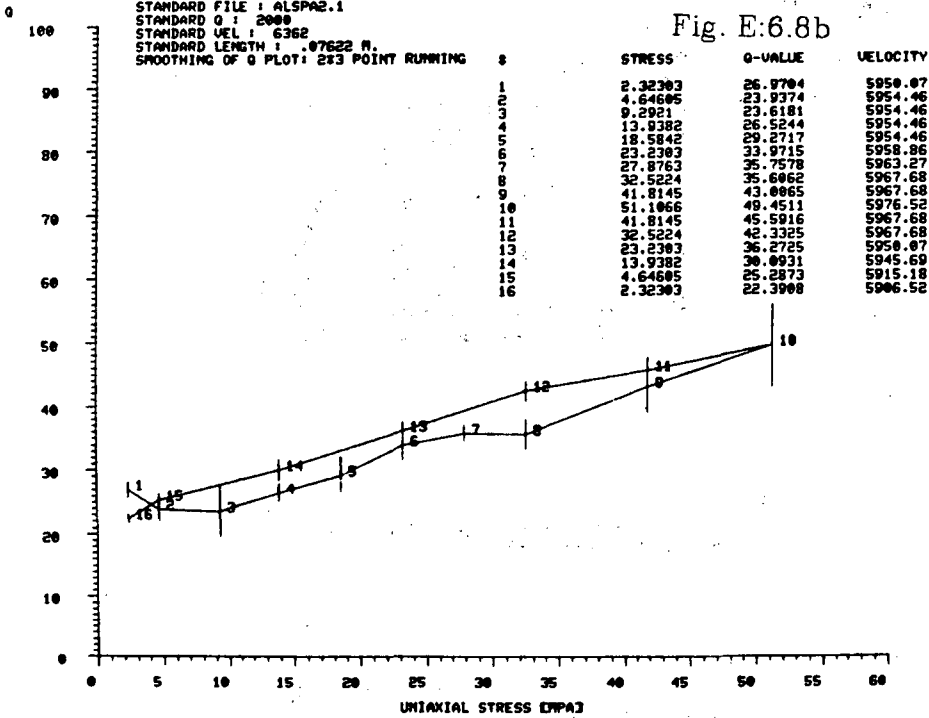
Q FOR UNIAXIAL STRESS ON CORE  
 SPECIMEN FILE : STPO08.01  
 SPECIMEN : STRIPA 8, P8-M6, DRY  
 STANDARD FILE : ALSPA2.1  
 STANDARD Q : 2000  
 STANDARD VEL : 6362  
 STANDARD LENGTH : .07622 M.  
 SMOOTHING OF Q PLOT: 283 POINT RUNNING

Fig. E:6.8a



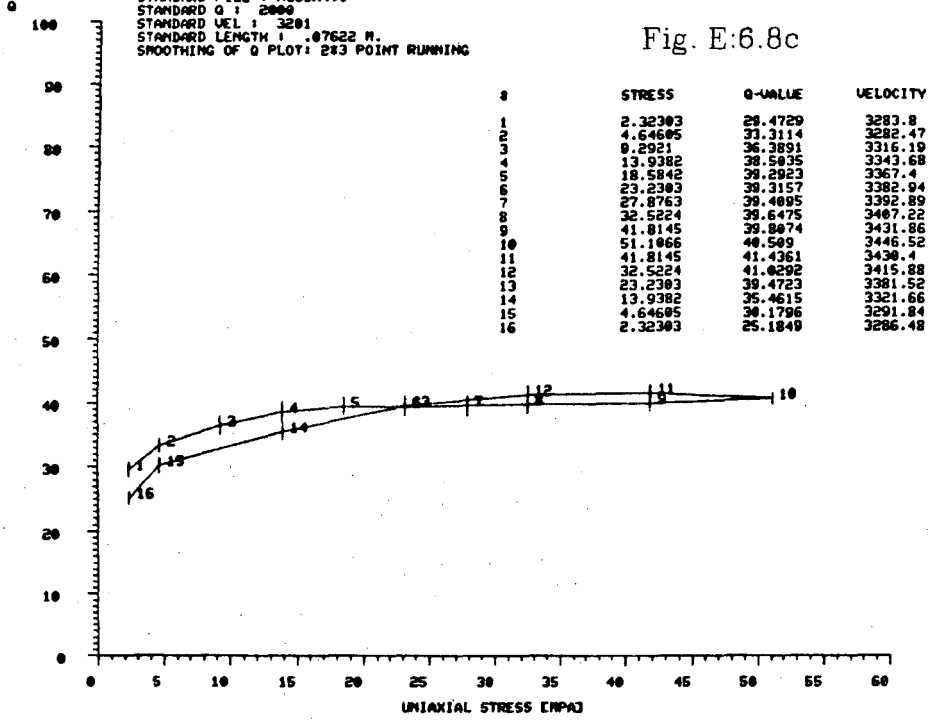
Q FOR UNIAXIAL STRESS ON CORE  
 SPECIMEN FILE : STPO08.01  
 SPECIMEN : STRIPA 8, P-WAVES, SATURATED, TRUNCATED WITH 4E-6 SEC, P8-M6, 821001  
 STANDARD FILE : ALSPA2.1  
 STANDARD Q : 2000  
 STANDARD VEL : 6362  
 STANDARD LENGTH : .07622 M.  
 SMOOTHING OF Q PLOT: 283 POINT RUNNING

Fig. E:6.8b



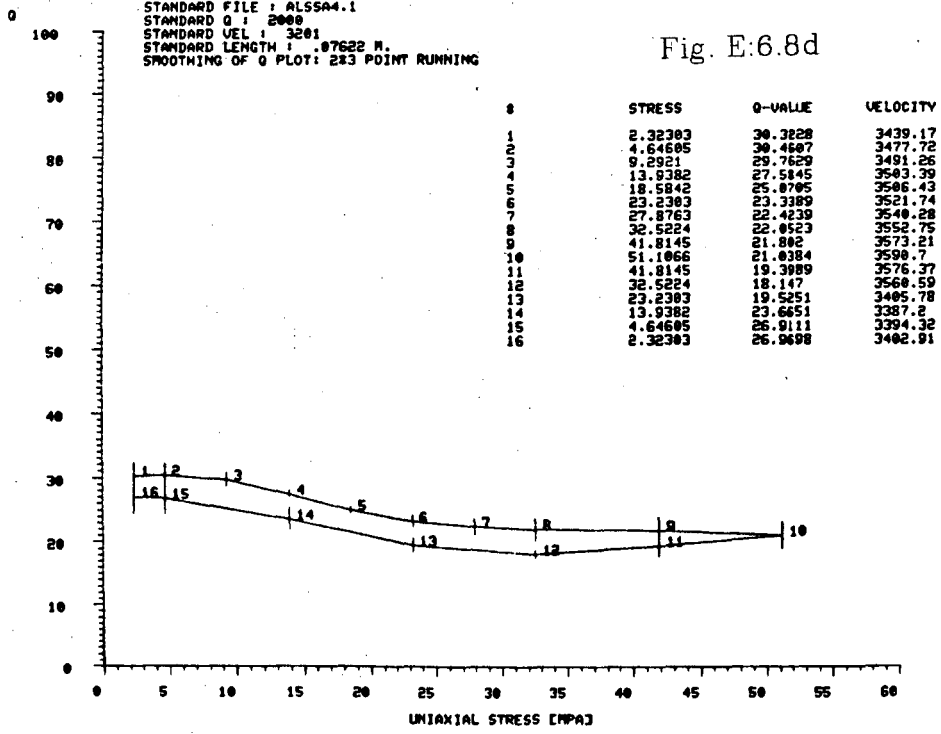
Q FOR UNIAXIAL STRESS ON CORE  
 SPECIMEN FILE : STS0DB.3  
 SPECIMEN : STRIPA 88, S-WAVES TRUNCATED WITH 1+2E-6 SEC, DRY, E22, M8-M6, 821020  
 STANDARD FILE : ALSSA4.1  
 STANDARD Q : 2000  
 STANDARD VEL : 3201  
 STANDARD LENGTH : .07622 M.  
 SMOOTHING OF Q PLOT: 283 POINT RUNNING

Fig. E:6.8c



Q FOR UNIAXIAL STRESS ON CORE  
 SPECIMEN FILE : STS0WB.01  
 SPECIMEN : STRIPA 88, TRUNCATED S-WAVES WITH 1+2E-6 SEC WIND, SATURATED, 821003  
 STANDARD FILE : ALSSA4.1  
 STANDARD Q : 2000  
 STANDARD VEL : 3201  
 STANDARD LENGTH : .07622 M.  
 SMOOTHING OF Q PLOT: 283 POINT RUNNING

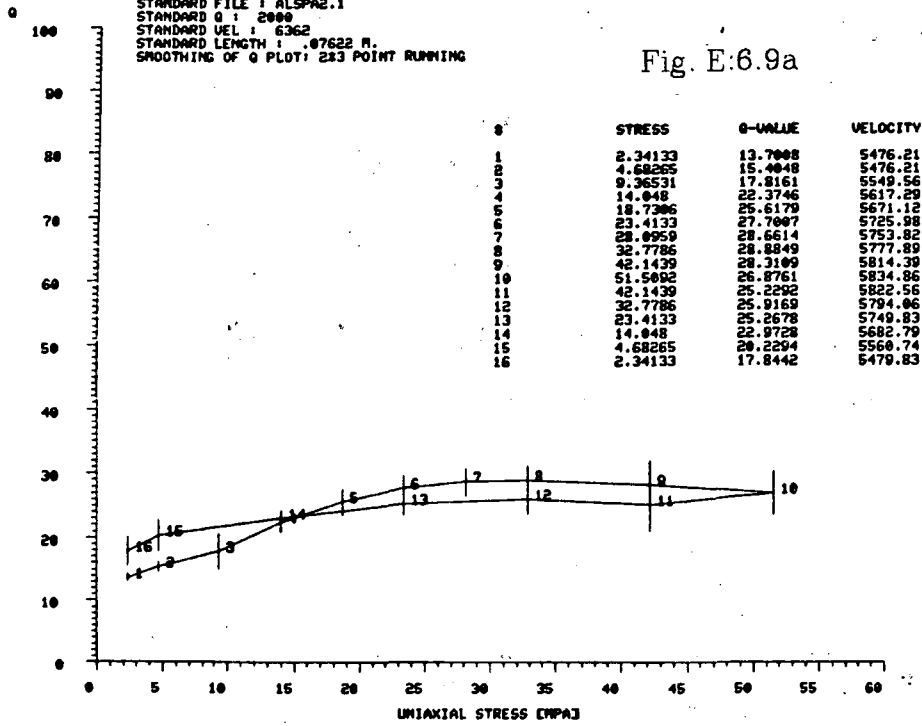
Fig. E:6.8d





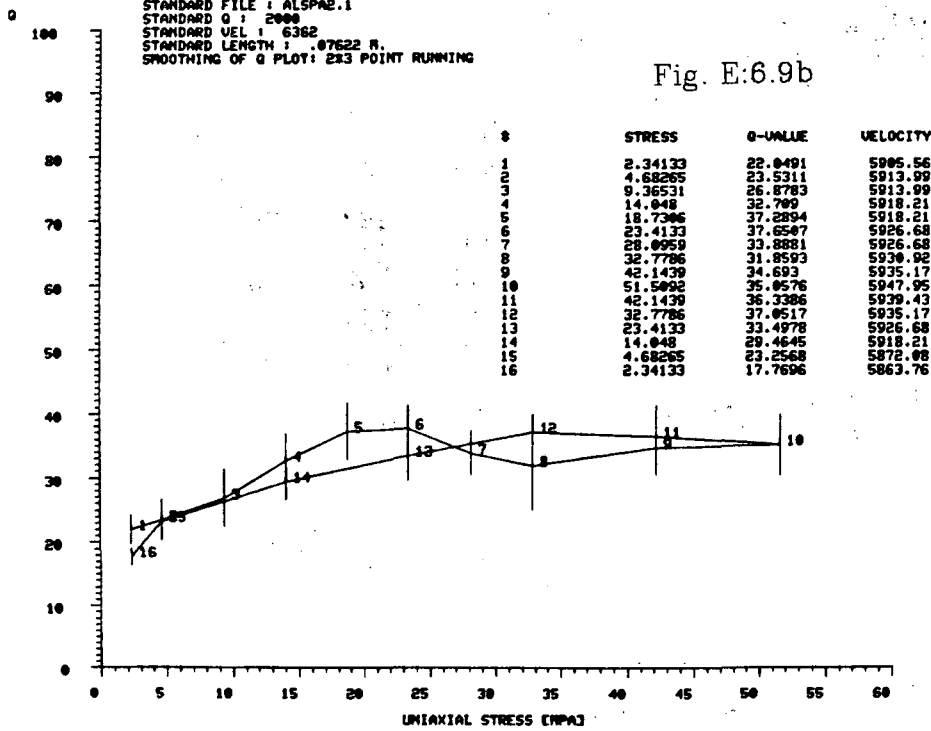
Q FOR UNIAXIAL STRESS ON CORE  
 SPECIMEN FILE : STPQD9.2  
 SPECIMEN : STRIPA 89, P-WAVES TRUNCATED WITH 4E-6 SEC, E25, H7-R9, 821020  
 STANDARD FILE : ALSPA2.1  
 STANDARD Q : 2000  
 STANDARD VEL : 6362  
 STANDARD LENGTH : .07622 M.  
 SMOOTHING OF Q PLOT: 2X3 POINT RUNNING

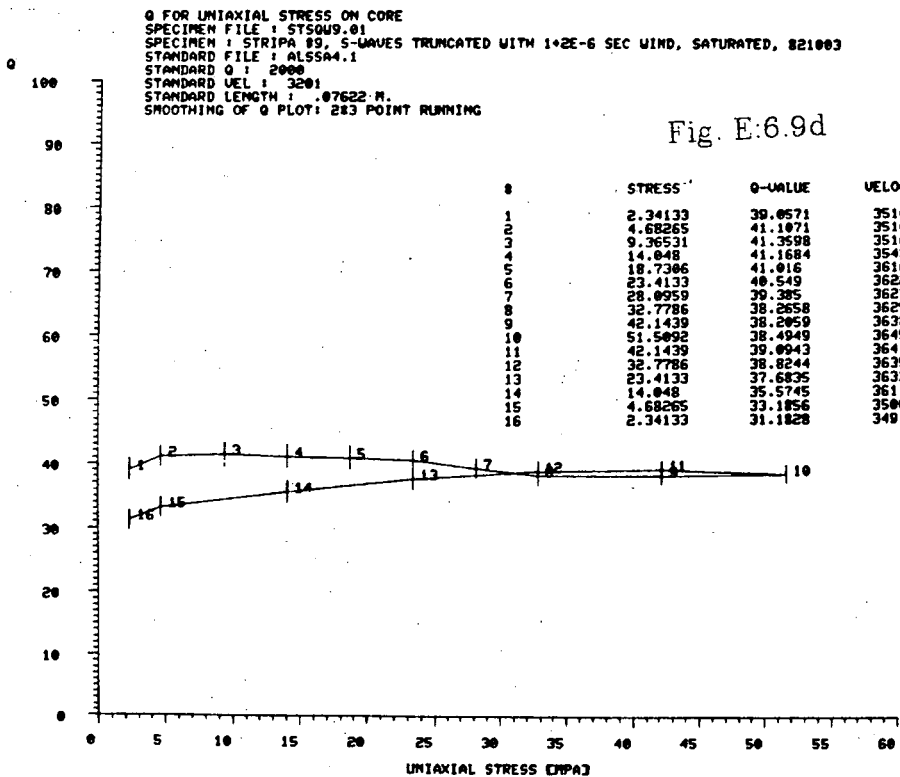
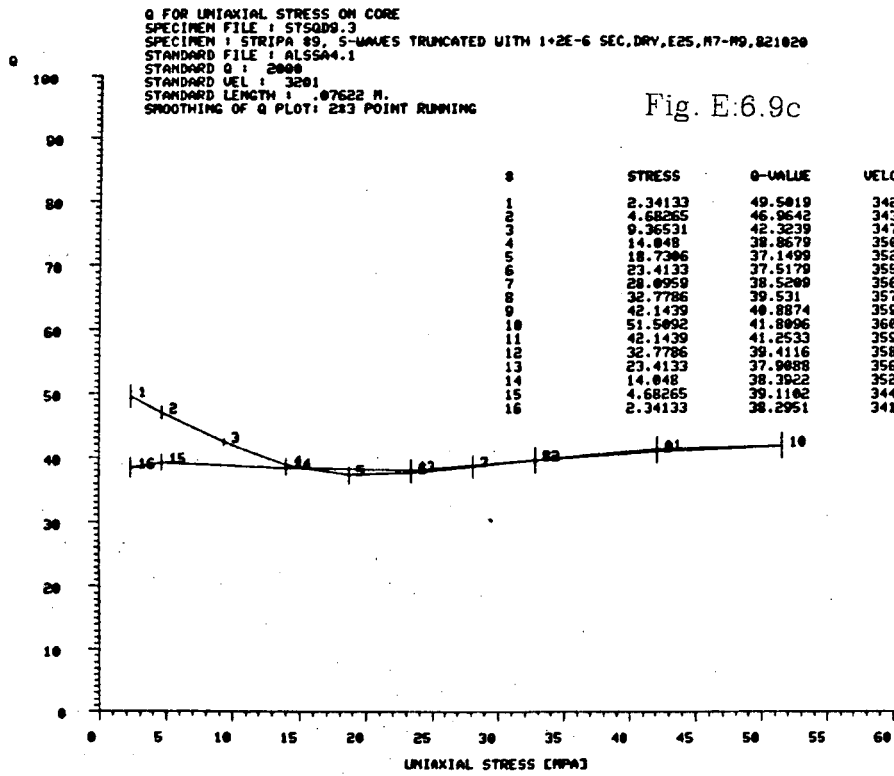
Fig. E:6.9a



Q FOR UNIAXIAL STRESS ON CORE  
 SPECIMEN FILE : STPQD9.01  
 SPECIMEN : STRIPA 89, H7-R9, SATURATED, P-WAVES  
 STANDARD FILE : ALSPA2.1  
 STANDARD Q : 2000  
 STANDARD VEL : 6362  
 STANDARD LENGTH : .07622 M.  
 SMOOTHING OF Q PLOT: 2X3 POINT RUNNING

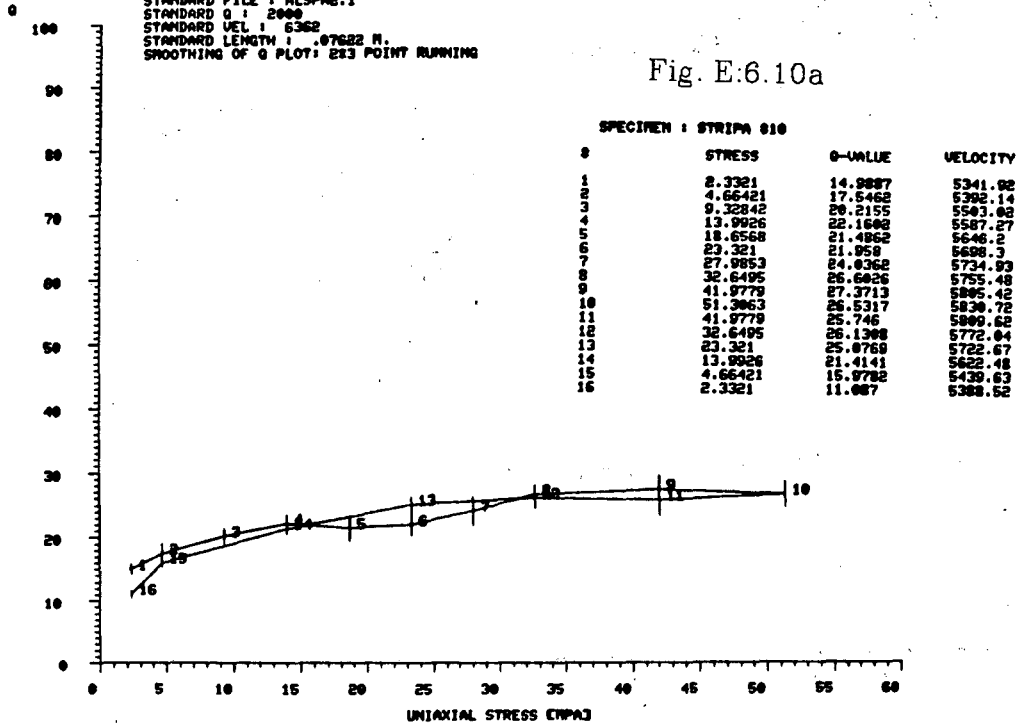
Fig. E:6.9b





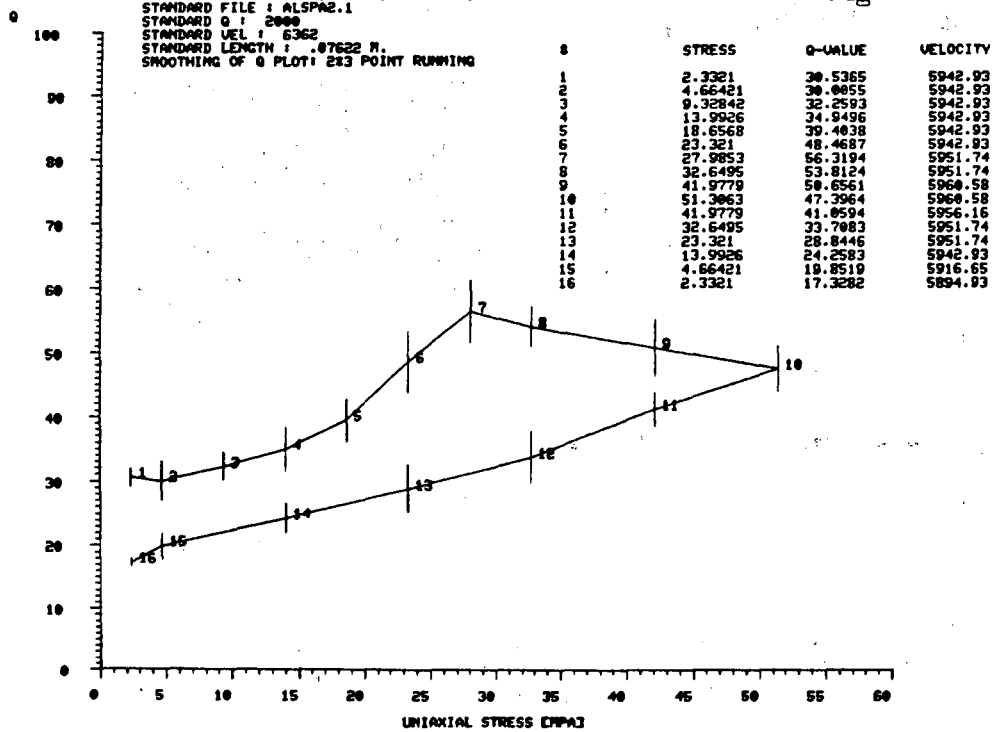
Q FOR UNIAXIAL STRESS ON CORE  
 SPECIMEN FILE : SPOD10.01  
 SPECIMEN : STRIPA 810  
 STANDARD FILE : ALSPAS.1  
 STANDARD Q : 2000  
 STANDARD VEL : 6362  
 STANDARD LENGTH : .07622 M.  
 SMOOTHING OF Q PLOT: 223 POINT RUNNING

Fig. E:6.10a



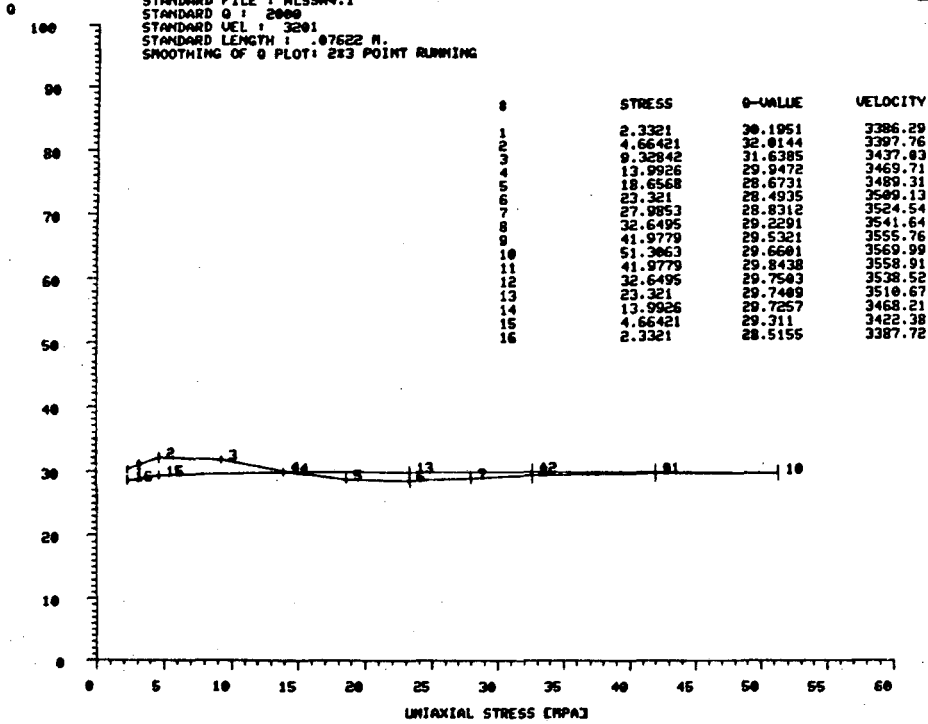
Q FOR UNIAXIAL STRESS ON CORE  
 SPECIMEN FILE : SPOU10.01  
 SPECIMEN : STRIPA 810, M7-M9, SATURATED, P-WAVES TRUNCATED WITH 4E-6 SEC WIND  
 STANDARD FILE : ALSPAS.1  
 STANDARD Q : 2000  
 STANDARD VEL : 6362  
 STANDARD LENGTH : .07622 M.  
 SMOOTHING OF Q PLOT: 223 POINT RUNNING

Fig. E:6.10b



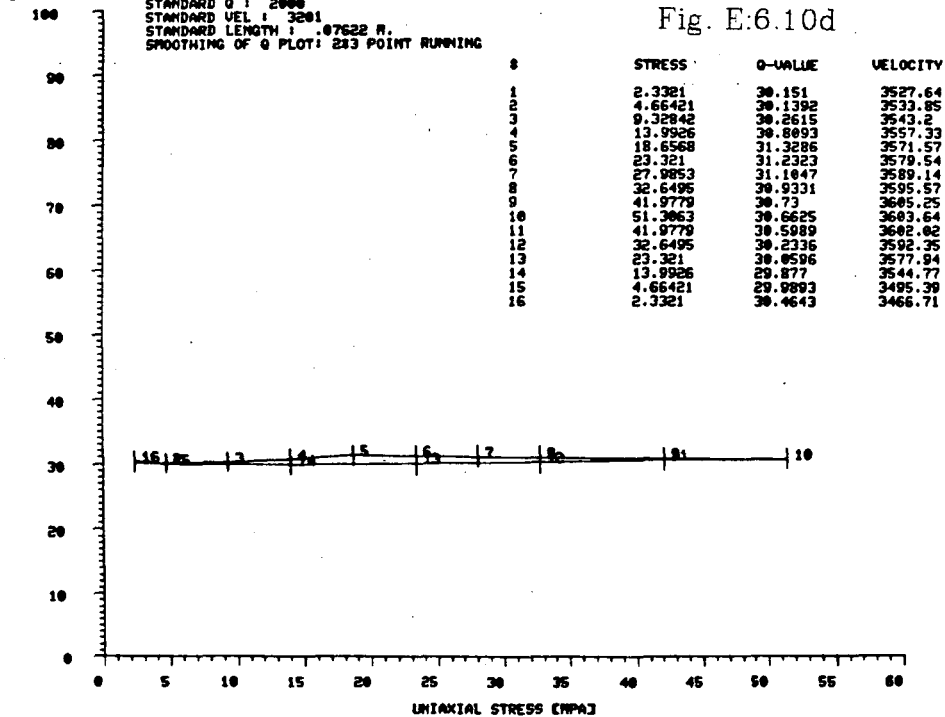
Q FOR UNIAXIAL STRESS ON CORE  
 SPECIMEN FILE : S50D10.3  
 SPECIMEN : STRIPA 810, 5-WAVES TRUNCATED WITH 1+2E-6 SEC WIND, E25, M7-M9, DRY, 821020  
 STANDARD FILE : ALSSA4.1  
 STANDARD Q : 2000  
 STANDARD VEL : 3201  
 STANDARD LENGTH : .07622 M.  
 SMOOTHING OF Q PLOT: 213 POINT RUNNING

Fig. E.6.10c



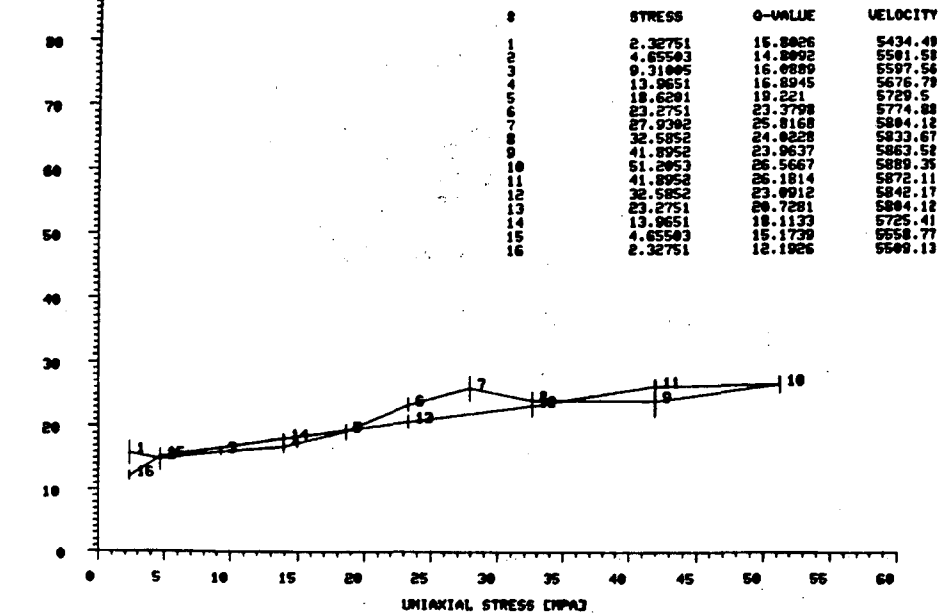
Q FOR UNIAXIAL STRESS ON CORE  
 SPECIMEN FILE : S50W10.01  
 SPECIMEN : STRIPA 810, 5-WAVES TRUNCATED WITH 1+2E-6 SEC WIND, SATURATED, 821003  
 STANDARD FILE : ALSSA4.1  
 STANDARD Q : 2000  
 STANDARD VEL : 3201  
 STANDARD LENGTH : .07622 M.  
 SMOOTHING OF Q PLOT: 213 POINT RUNNING

Fig. E:6.10d



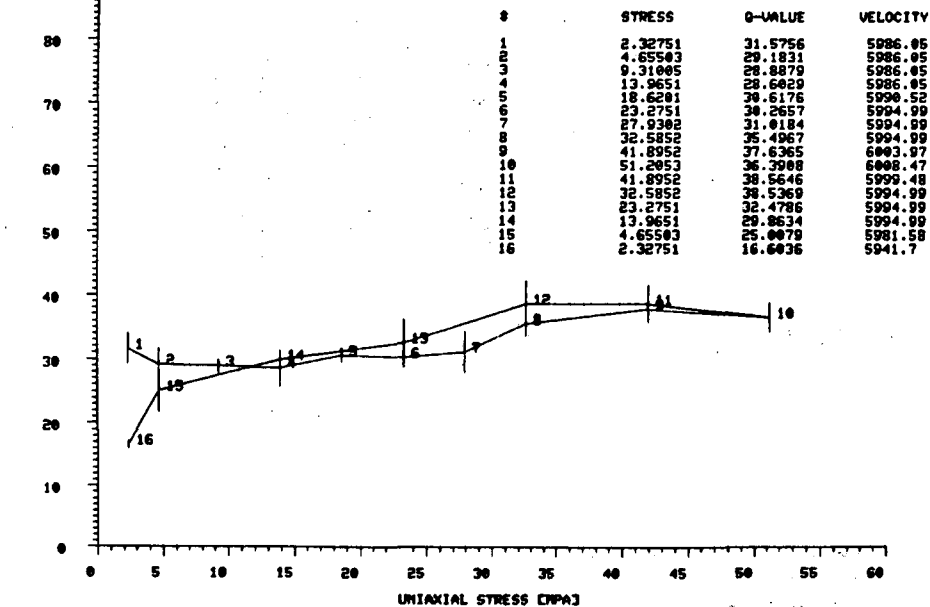
Q FOR UNIAXIAL STRESS ON CORE  
 SPECIMEN FILE : SPOD11.01  
 SPECIMEN : STRIPA 811, N7-ND, DRY  
 STANDARD FILE : ALSPAE.1  
 STANDARD Q : 2000  
 STANDARD VEL : 6362  
 STANDARD LENGTH : .07622 M.  
 SMOOTHING OF Q PLOT: 233 POINT RUNNING

Fig. E:6.11a



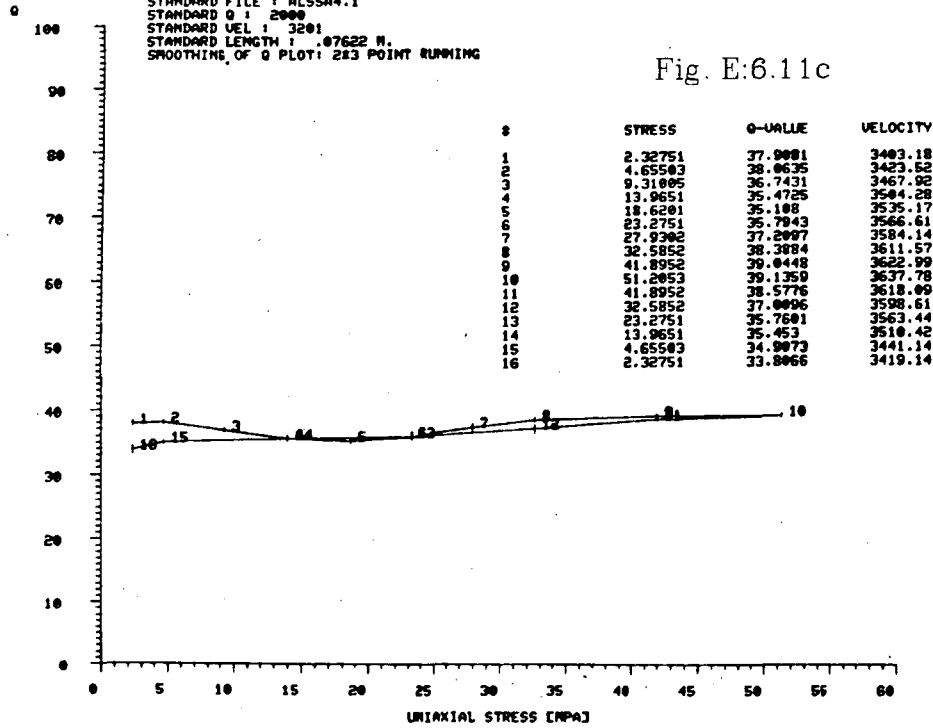
Q FOR UNIAXIAL STRESS ON CORE  
 SPECIMEN FILE : SPQW11.01  
 SPECIMEN : STRIPA 811, TRUNCATED P-WAVES WITH 4E-6 SEC WIND, SATURATED  
 STANDARD FILE : ALSPAE.1  
 STANDARD Q : 2000  
 STANDARD VEL : 6362  
 STANDARD LENGTH : .07622 M.  
 SMOOTHING OF Q PLOT: 233 POINT RUNNING

Fig. E:6.11b



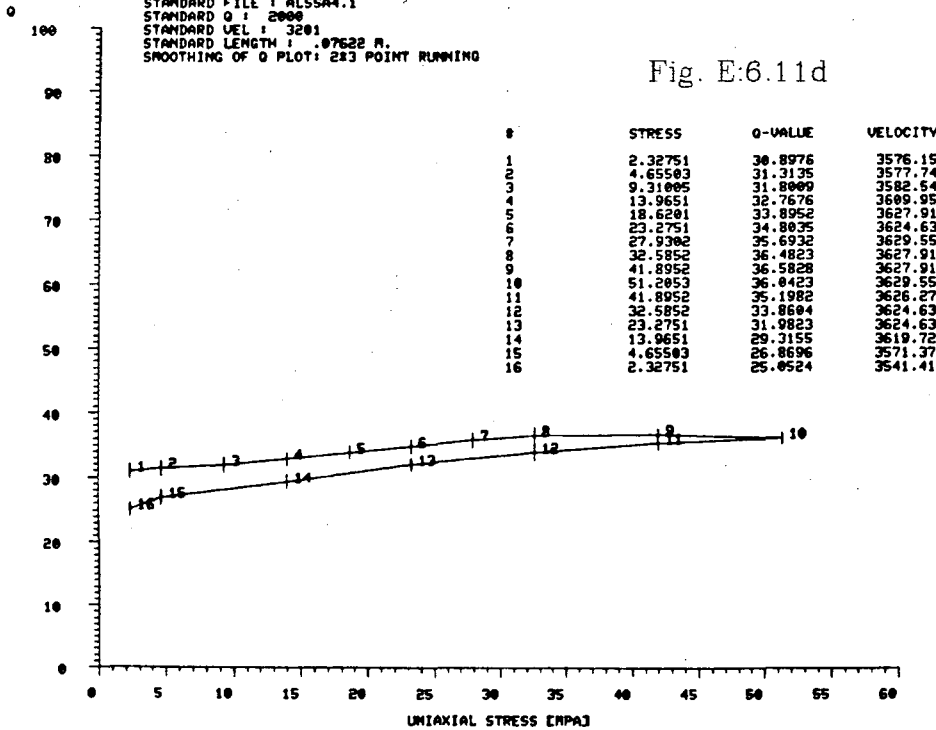
Q FOR UNIAXIAL STRESS ON CORE  
 SPECIMEN FILE : SS0D11.02  
 SPECIMEN : STRIPA 811, TRUNCATED S-WAVES WITH 1+2E-6 AT CROSSOVER, W7-R9, DRY  
 STANDARD FILE : ALSSA4.1  
 STANDARD Q : 2000  
 STANDARD VEL : 3201  
 STANDARD LENGTH : .07622 M.  
 SMOOTHING OF Q PLOT: 243 POINT RUNNING

Fig. E:6.11c



Q FOR UNIAXIAL STRESS ON CORE  
 SPECIMEN FILE : SS0U11.01  
 SPECIMEN : STRIPA 811, S-WAVES TRUNCATED WITH 1+2E-6 SEC WIND, SATURATED, 821003  
 STANDARD FILE : ALSSA4.1  
 STANDARD Q : 2000  
 STANDARD VEL : 3201  
 STANDARD LENGTH : .07622 M.  
 SMOOTHING OF Q PLOT: 243 POINT RUNNING

Fig. E:6.11d



## Appendix E:7 - Saturation experiment for specimen # 1.

In this appendix the data for the saturation experiment from specimen # 1 is presented. For each saturation level the specimen was tested at four different uniaxial stresses. For the presentation of the data the waveforms and the amplitude spectra were assembled in their different stress groups.

SPECIMEN FILE: STDAT2.WET

DATE: 26 OCTOBER, 1982

LENGTH OF SPECIMEN: .070045 METER. DIAMETER OF SPECIMEN: 6.1791 CENTIMETER

NUMBER OF LOADS: 4

DENSITY OF SPECIMEN:

2626	2626	2626	2625	2625
2625	2625	2624	2624	2624
2623	2623			

POROSITY: .897748 %

THE UNIAXIAL STRESS IS: 5 NPA

WEIGHT (GRAMS)	SATURATION (%)	P-WAVE VEL (M/S)	S-WAVE VEL (M/S)	YOUNGS M (GPA)	BULK M (GPA)	SHEAR M (GPA)	PO. RA
437.283	100	5979	3475	79	52	32	.245883
437.243	93	5890	3490	79	48	32	.229525
437.206	86	5778	3459	77	46	31	.220656
437.173	80	5720	3413	75	45	31	.223514
437.162	78	5691	3412	75	44	31	.219588
437.095	67	5625	3375	73	43	30	.218875
437.063	61	5590	3355	72	43	30	.218591
437.023	54	5485	3342	71	40	29	.204772
436.983	47	5501	3344	71	40	29	.206974
436.943	40	5585	3344	71	40	29	.20762
436.743	6	5374	3249	67	39	28	.211822
436.708	0	5385	3241	66	37	28	

THE UNIAXIAL STRESS IS: 9 NPA

WEIGHT (GRAMS)	SATURATION (%)	P-WAVE VEL (M/S)	S-WAVE VEL (M/S)	YOUNGS M (GPA)	BULK M (GPA)	SHEAR M (GPA)	PO. RA
437.283	100	5979	3478	79	52	32	.244404
437.243	93	5903	3512	79	48	32	.226195
437.206	86	5834	3484	78	47	32	.22295
437.173	80	5791	3459	77	46	31	.224919
437.162	78	5757	3438	76	45	31	.222797
437.095	67	5703	3422	75	44	31	.21875
437.063	61	5634	3390	73	43	30	.216353
437.023	54	5590	3390	73	41	30	.202711
436.983	47	5559	3378	72	41	30	.207243
436.943	40	5570	3370	72	41	30	.208891
436.743	6	5448	3289	69	40	28	.213093
436.708	0	5326	3253	67	37	28	.20251

THE UNIAXIAL STRESS IS: 19 NPA

WEIGHT (GRAMS)	SATURATION (%)	P-WAVE VEL (M/S)	S-WAVE VEL (M/S)	YOUNGS M (GPA)	BULK M (GPA)	SHEAR M (GPA)	PO. RA
437.283	100	5979	3504	80	51	32	.238516
437.243	93	5934	3530	80	49	33	.226107
437.206	86	5890	3513	79	48	32	.227909
437.173	80	5864	3485	78	48	32	.226893
437.162	78	5842	3478	78	47	32	.225622
437.095	67	5791	3459	77	46	31	.225569
437.063	61	5728	3435	76	45	31	.218131
437.023	54	5662	3423	75	43	31	.211941
436.983	47	5670	3423	75	43	31	.213239
436.943	40	5670	3422	75	43	31	.213629
436.743	6	5574	3323	71	43	29	.224477
436.708	0	5570	3302	70	43	29	.230365

THE UNIAXIAL STRESS IS: 28 NPA

WEIGHT (GRAMS)	SATURATION (%)	P-WAVE VEL (M/S)	S-WAVE VEL (M/S)	YOUNGS M (GPA)	BULK M (GPA)	SHEAR M (GPA)	PO. RA
437.283	100	5979	3541	81	50	33	.229897
437.243	93	5957	3541	81	49	33	.22564
437.206	86	5925	3534	80	48	33	.224057
437.173	80	5912	3521	80	48	33	.225197
437.162	78	5894	3507	79	48	32	.220659
437.095	67	5851	3486	78	47	32	.22354
437.063	61	5799	3476	77	46	32	.21965
437.023	54	5745	3465	77	45	32	.213956
436.983	47	5753	3468	77	45	32	.214474
436.943	40	5753	3461	76	45	31	.216431
436.743	6	5666	3381	73	44	30	.223593
436.708	0	5602	3337	72	43	29	.225185

Table E:7.1 Data from specimen # 1 during saturation experiment.



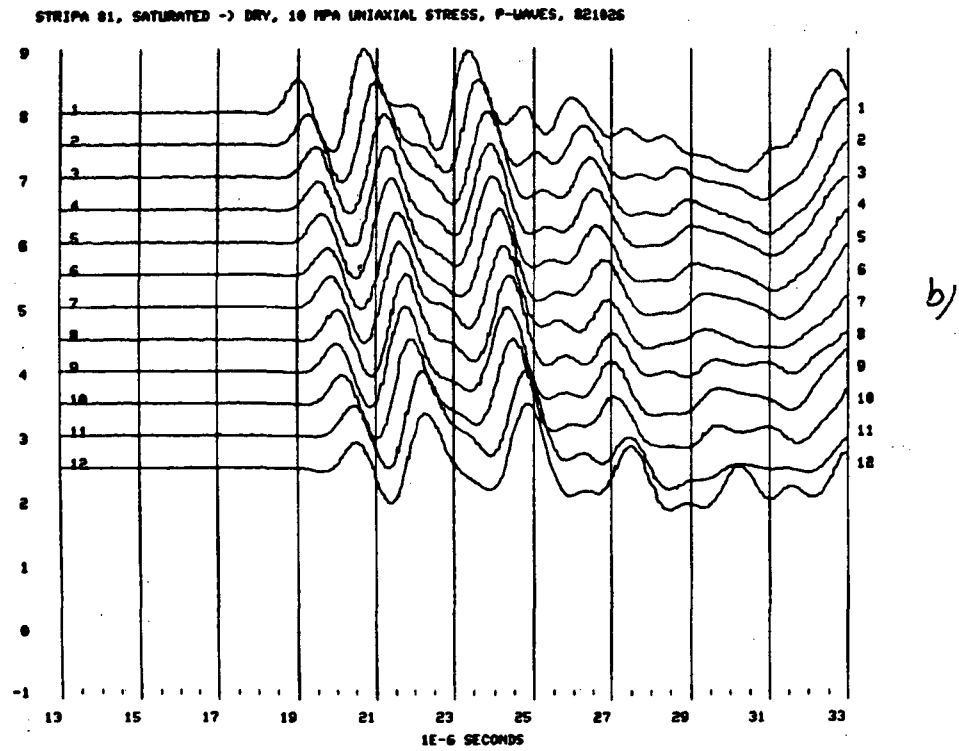
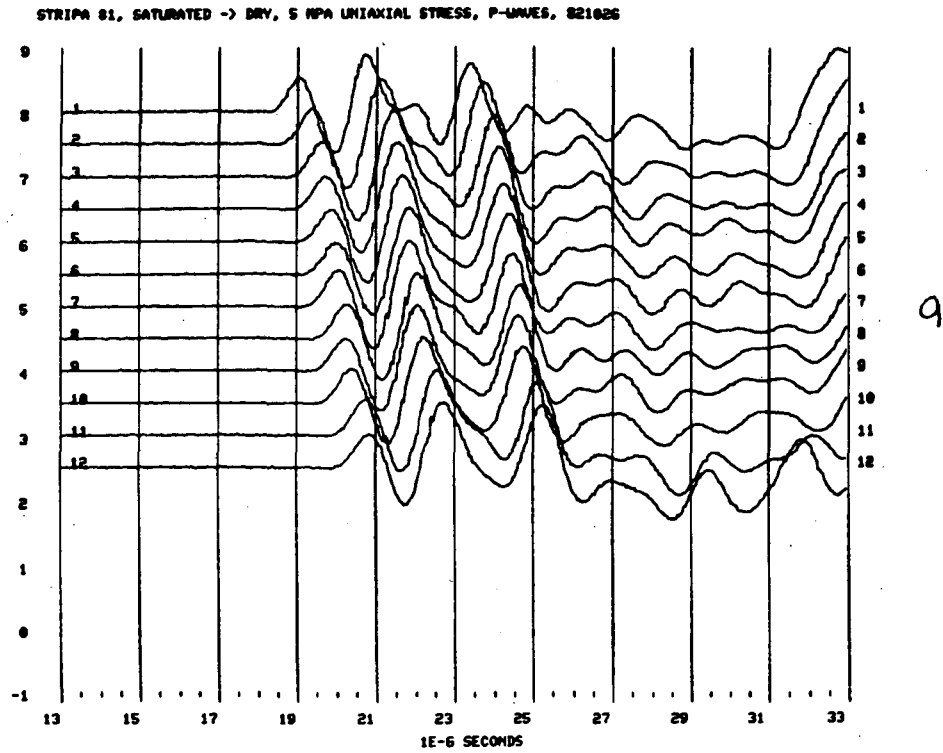
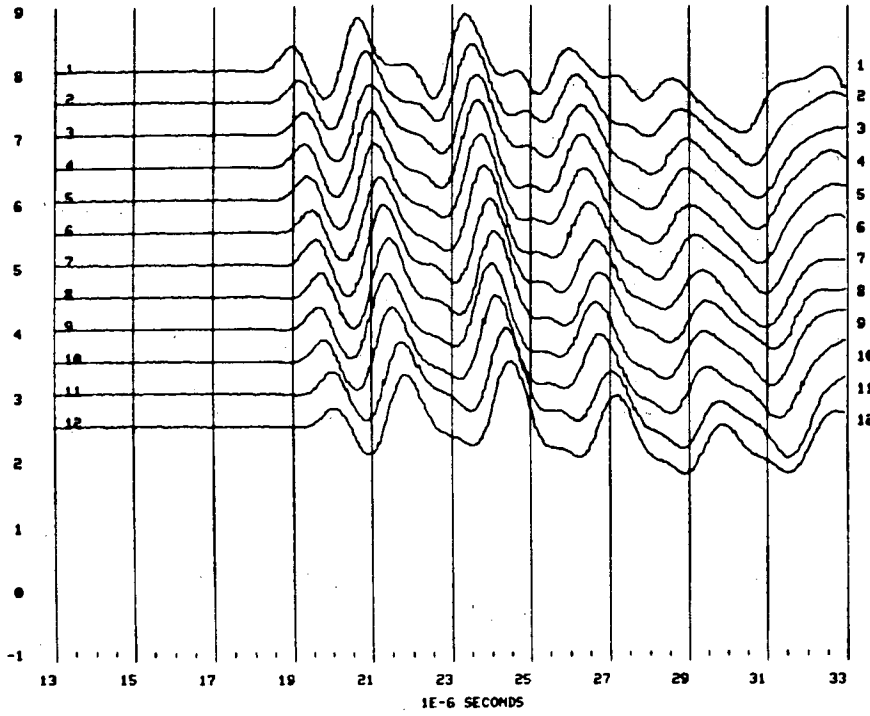
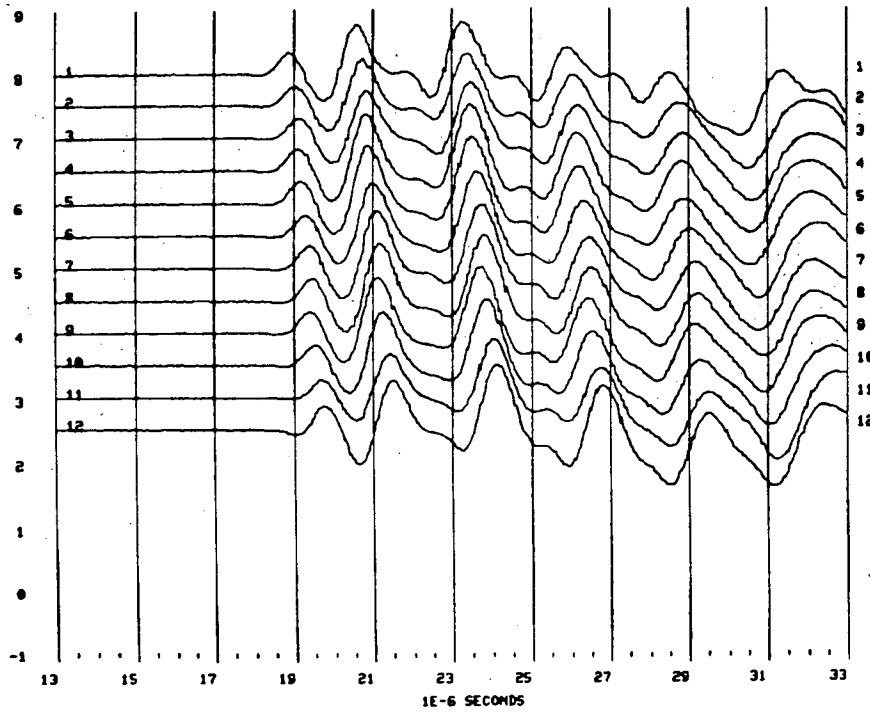


Fig. E:7.1 P waves for 12 saturation conditions under a) 5 MPa, b) 10 MPa, c) 20 MPa, d) 30 MPa uniaxial stress.

STRIPA 01, SATURATED -> DRY, 20 MPa UNIAXIAL STRESS, P-WAVES, 021026



STRIPA 01, SATURATED -> DRY, 30 MPa UNIAXIAL STRESS, P-WAVES, 021026



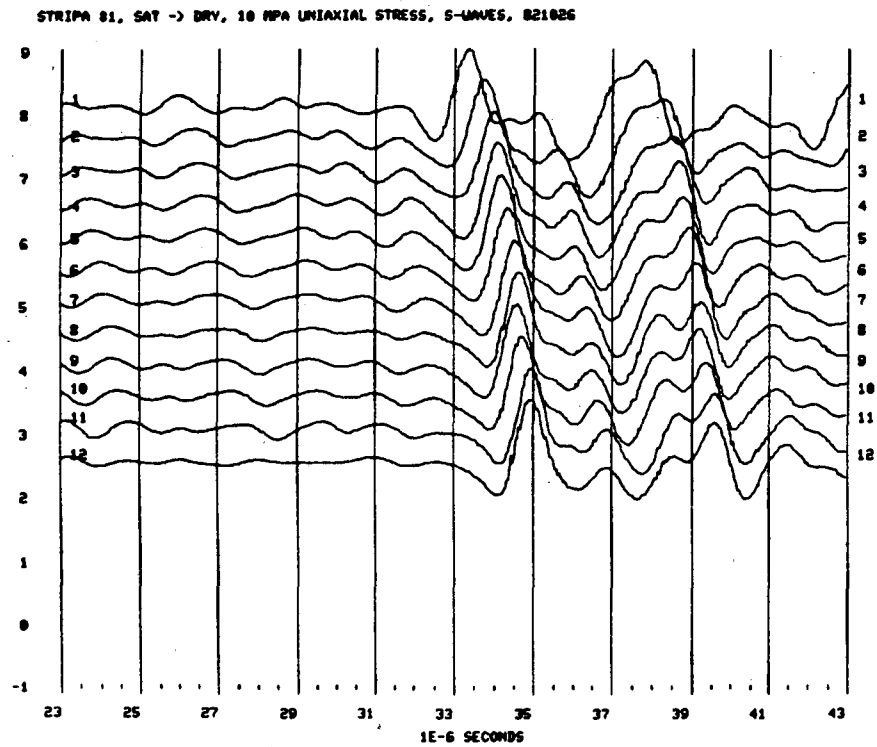
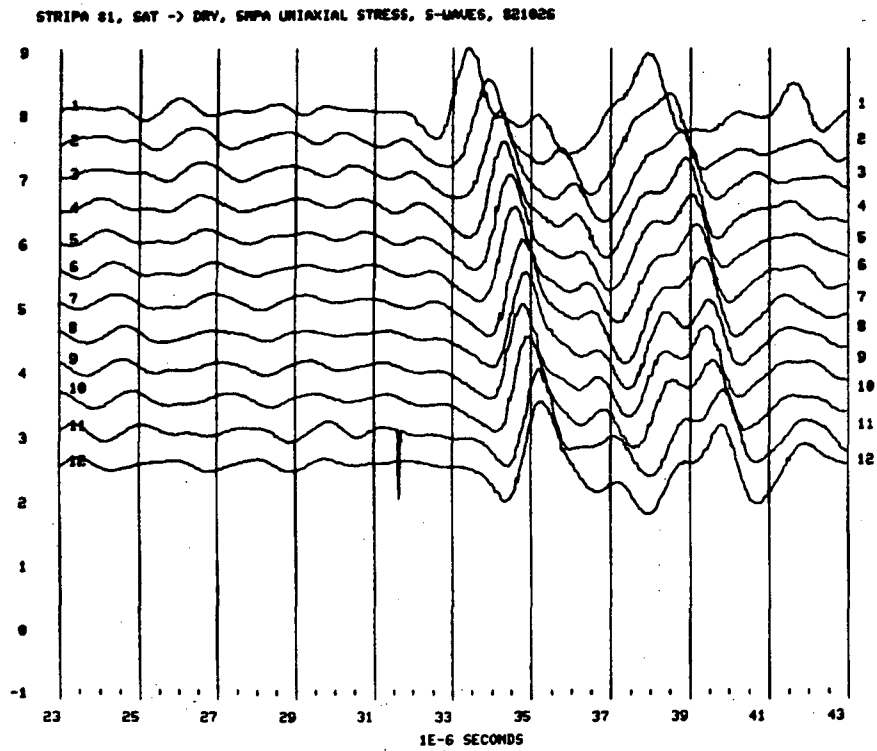
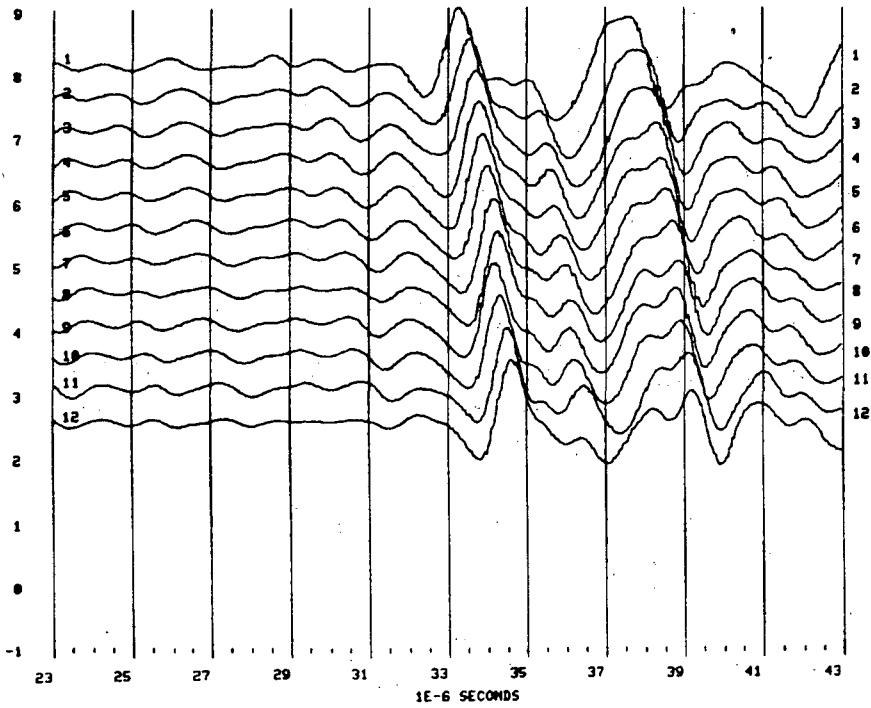
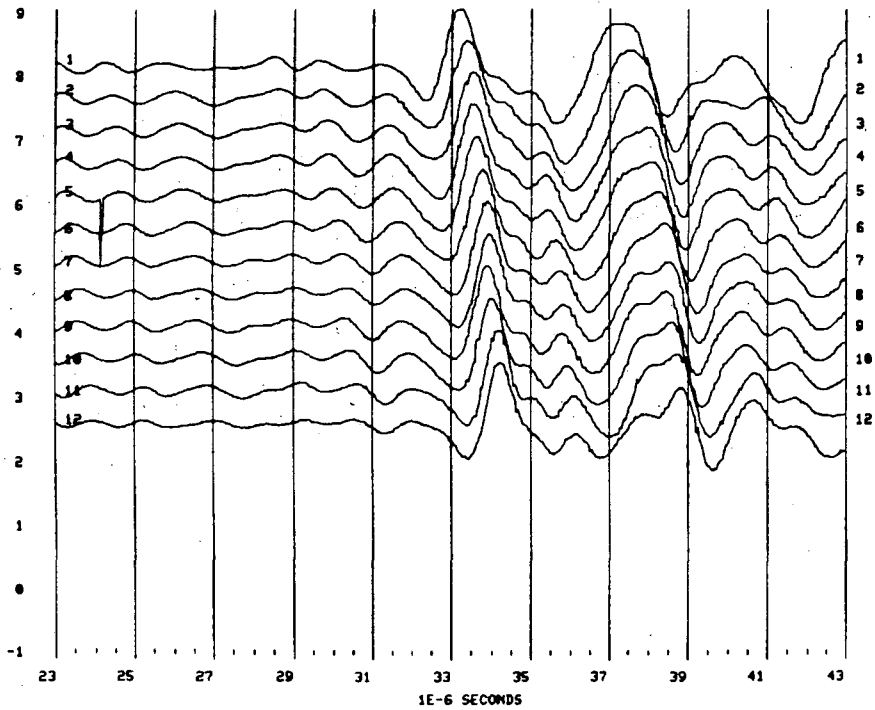


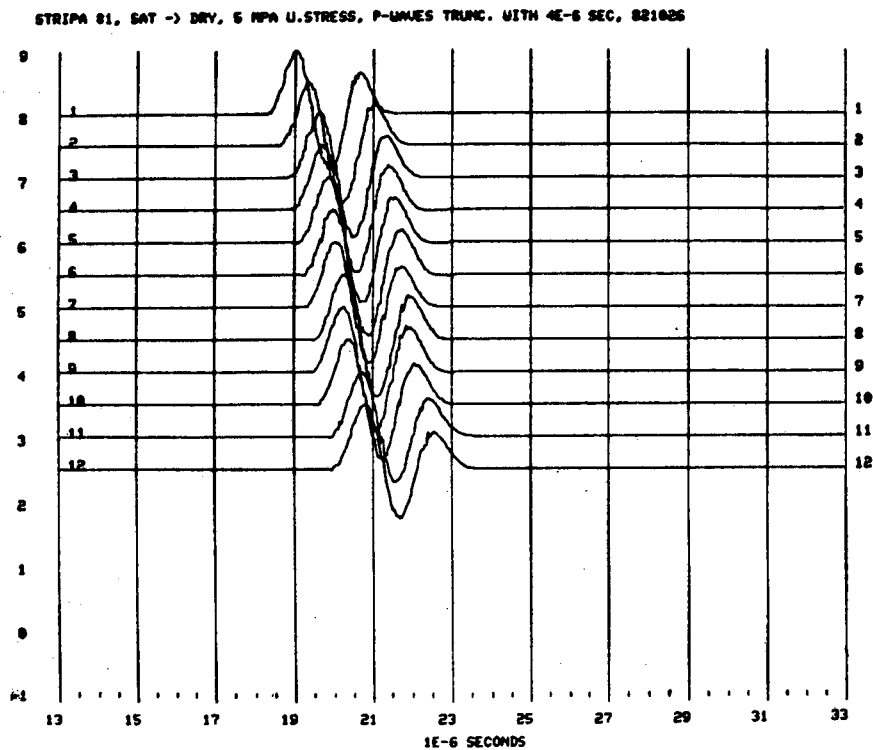
Fig. E:7.2 S waves for 12 saturation conditions under a) 5 MPa, b) 10 MPa, c) 20 MPa, d) 30 MPa uniaxial stress.

STRIPA 81, SAT -> DRY, 20 MPa UNIAXIAL STRESS, S-WAVES, 821026

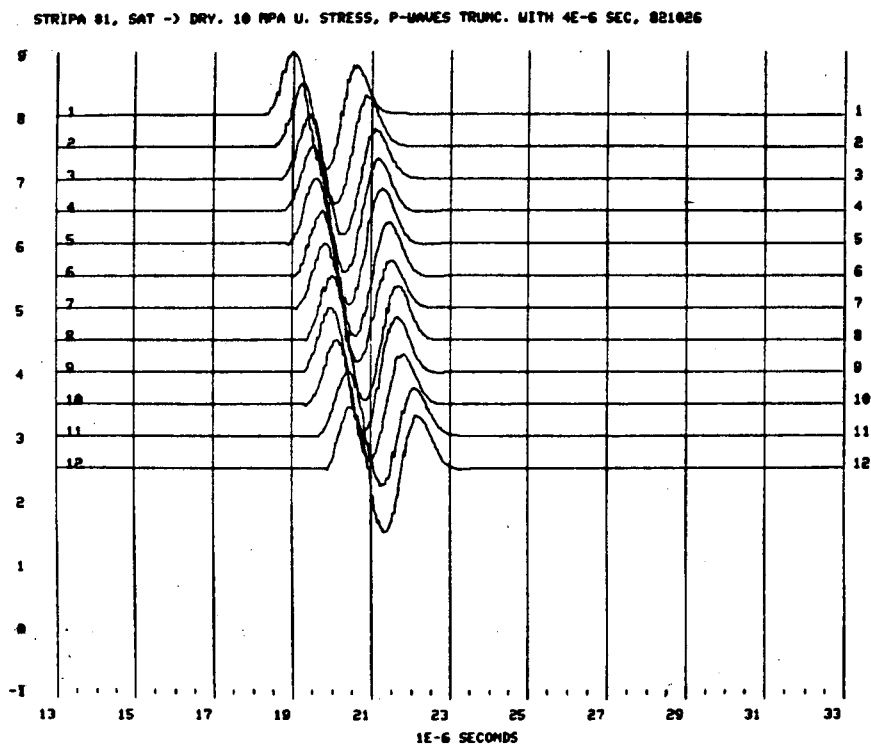


STRIPA 81, SAT -> DRY, 30 MPa UNIAXIAL STRESS, S-WAVES 821026





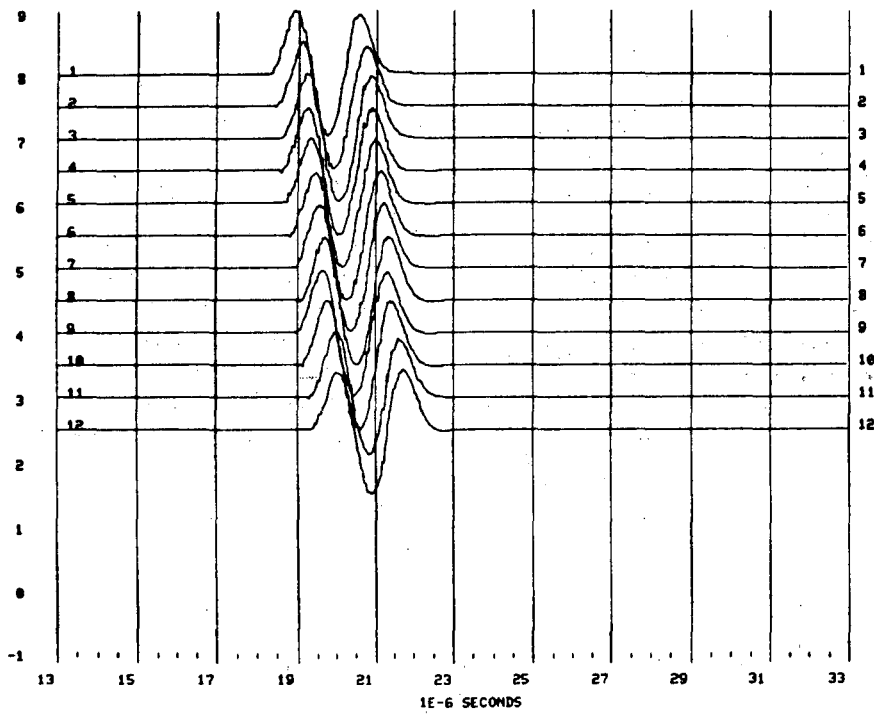
a



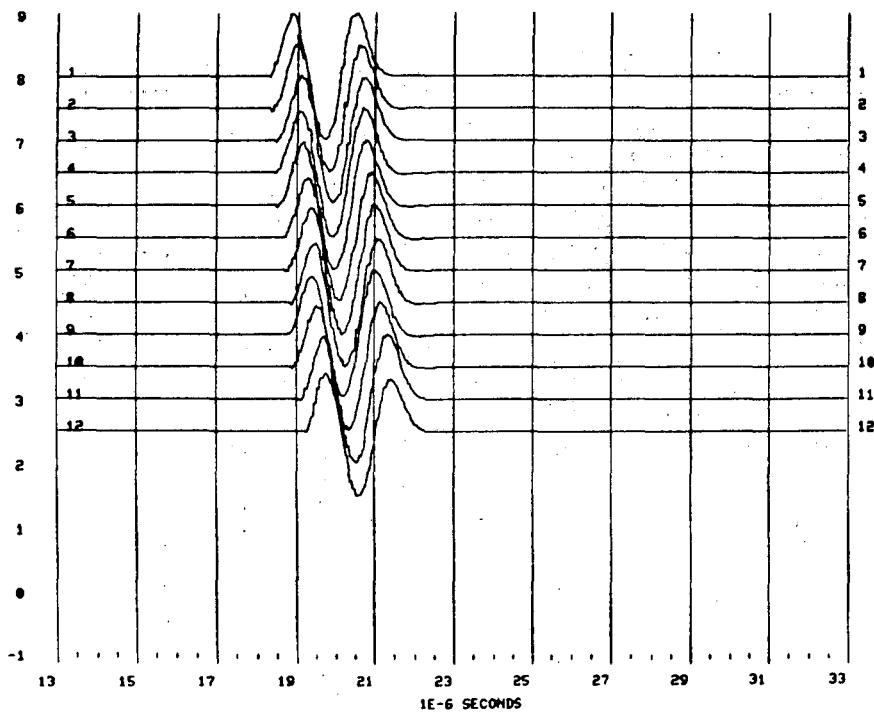
b

Fig. E:7.3 Truncated P waves for 12 saturation conditions under a) 5 MPa, b) 10 MPa, c) 20 MPa, d) 30 MPa uniaxial stress.

STRIPA 81, SAT -> DRY, 20 MPa U-STRESS, P-WAVES TRUNC. WITH 4E-6 SEC, 821026



STRIPA 81, SAT -> DRY, 30 MPa U-STRESS, P-WAVES TRUNC. WITH 4E-6 SEC, 821026



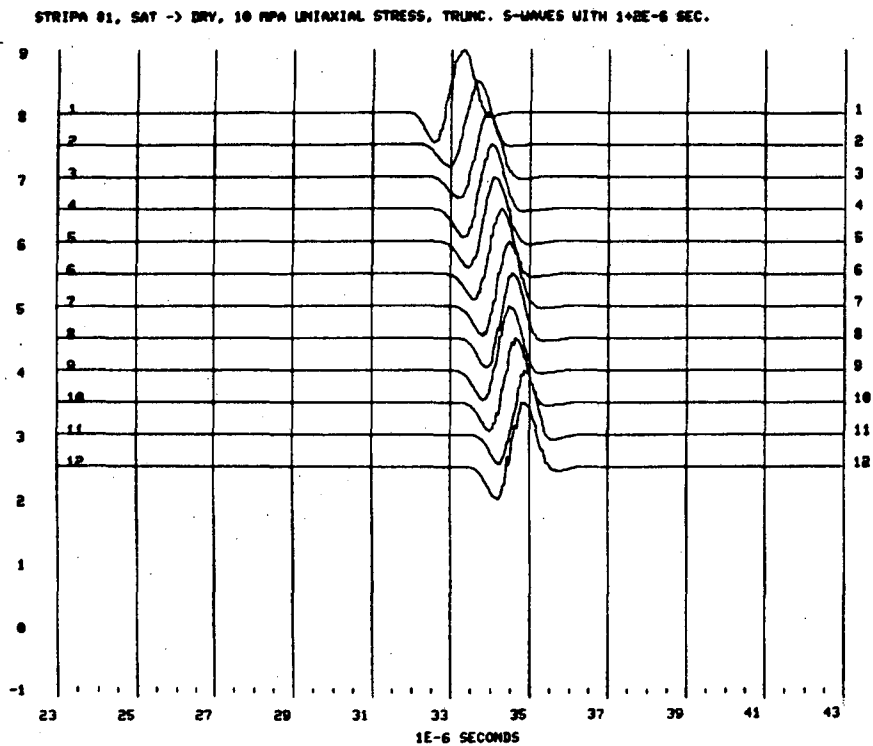
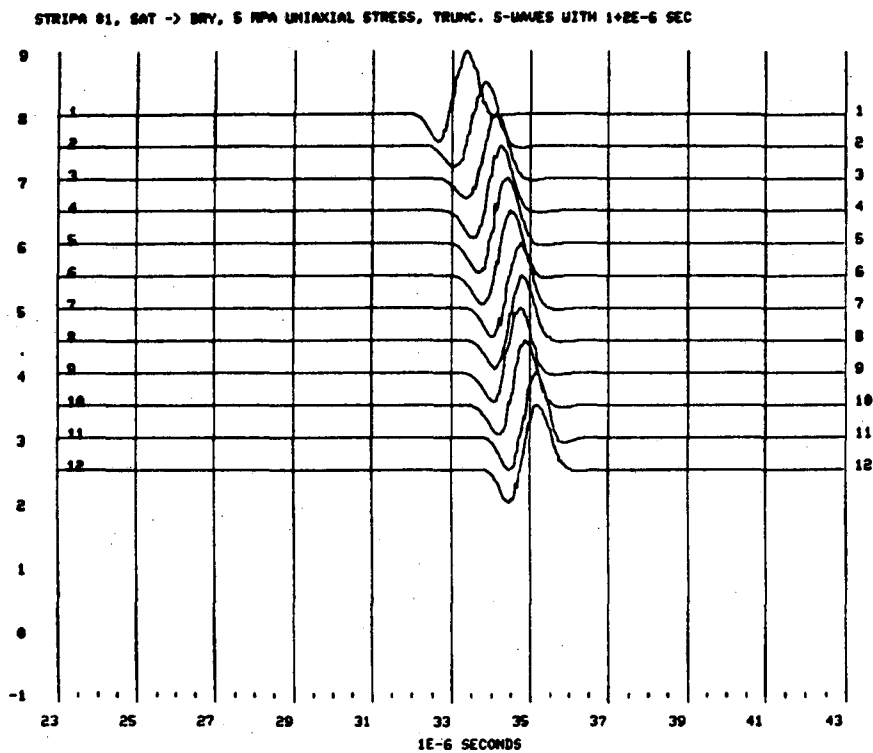
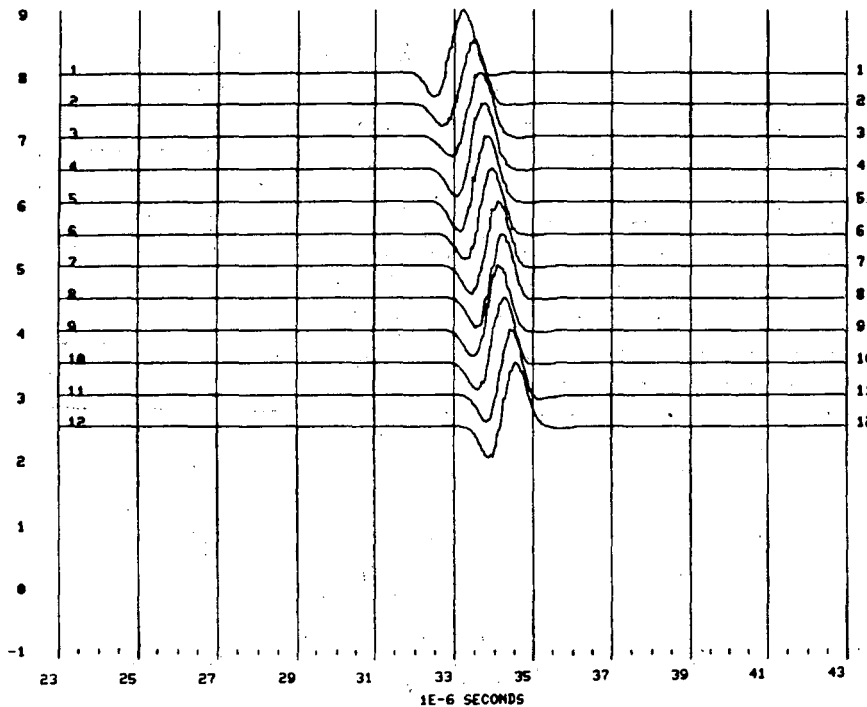
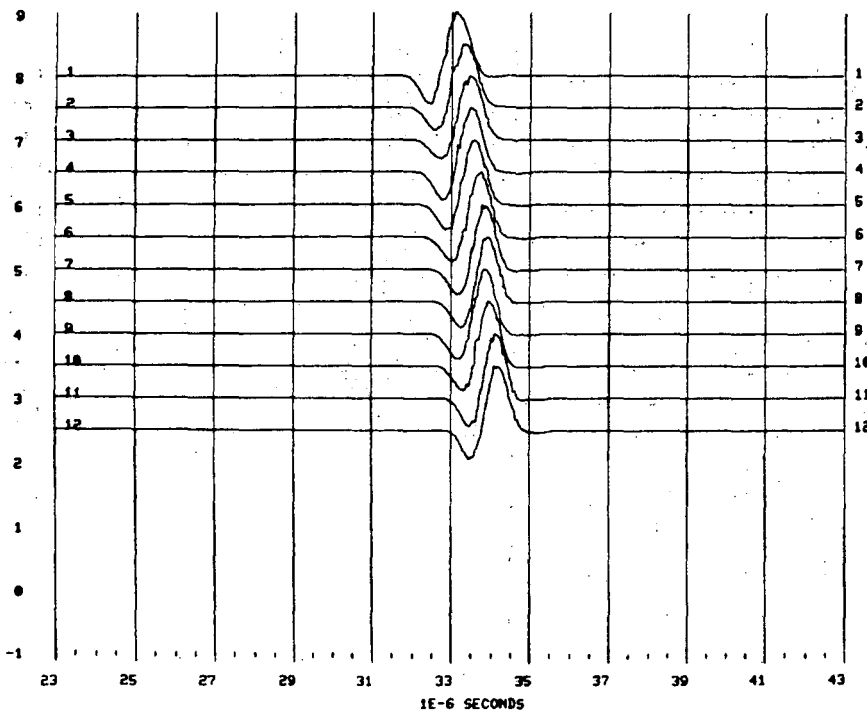


Fig. E:7.4 Truncated S waves for 12 saturation conditions under a) 5 MPa, b) 10 MPa, c) 20 MPa, d) 30 MPa uniaxial stress.

STRIPA 01, SAT -> DRY, 20 MPa UNIAXIAL STRESS, TRUNC. S-WAVES WITH 1+2E-6 SEC.

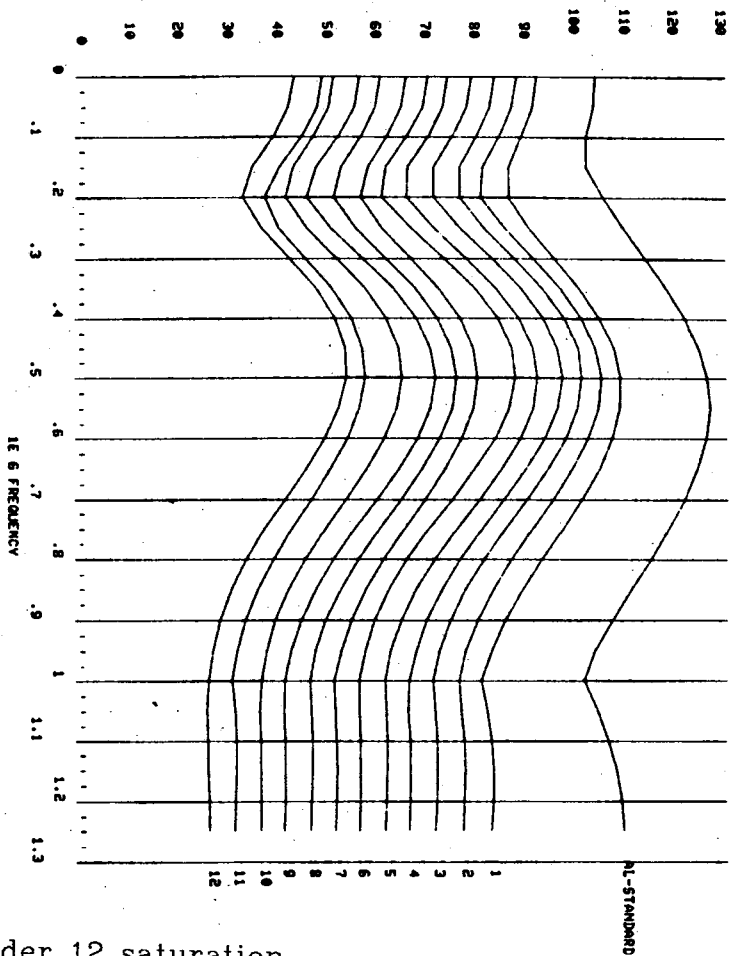


STRIPA 01, SAT -> DRY, 30 MPa UNIAXIAL STRESS, TRUNC. S-WAVES WITH 1+2E-6 SEC.





SPECIMEN : STRIPA 81, E21, NS-NS CONDITION : SAT -> DRY WINDOW : 4E-6 SEC  
 SMOOTH : 0 FILE : STRIP81.P-IMPRES DATE : 27 OCTOBER, 1982



SPECIMEN : STRIPA 81, E21, NS-NS CONDITION : SAT -> DRY WINDOW : 4E-6 SEC  
 SMOOTH : 0 FILE : STRIP10.P-IMPRES DATE : 27 OCTOBER, 1982

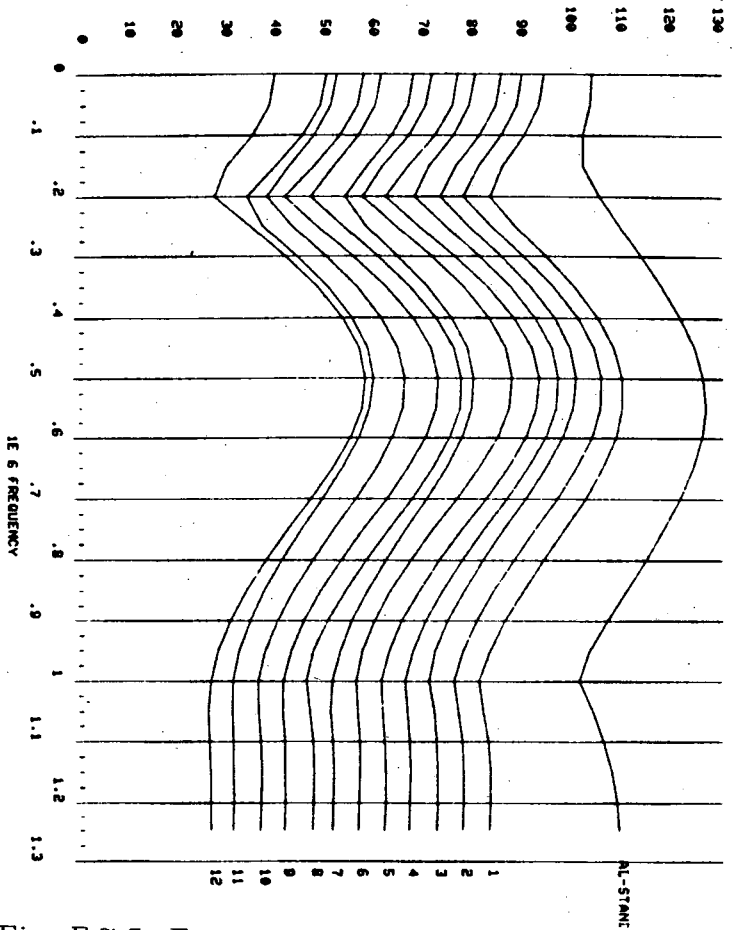
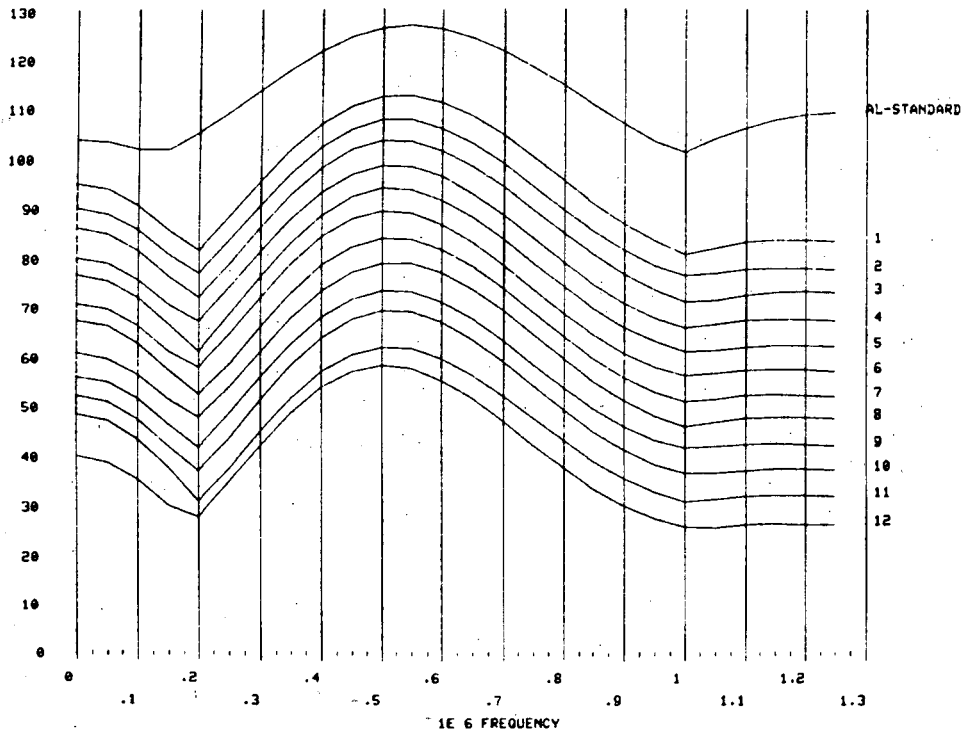
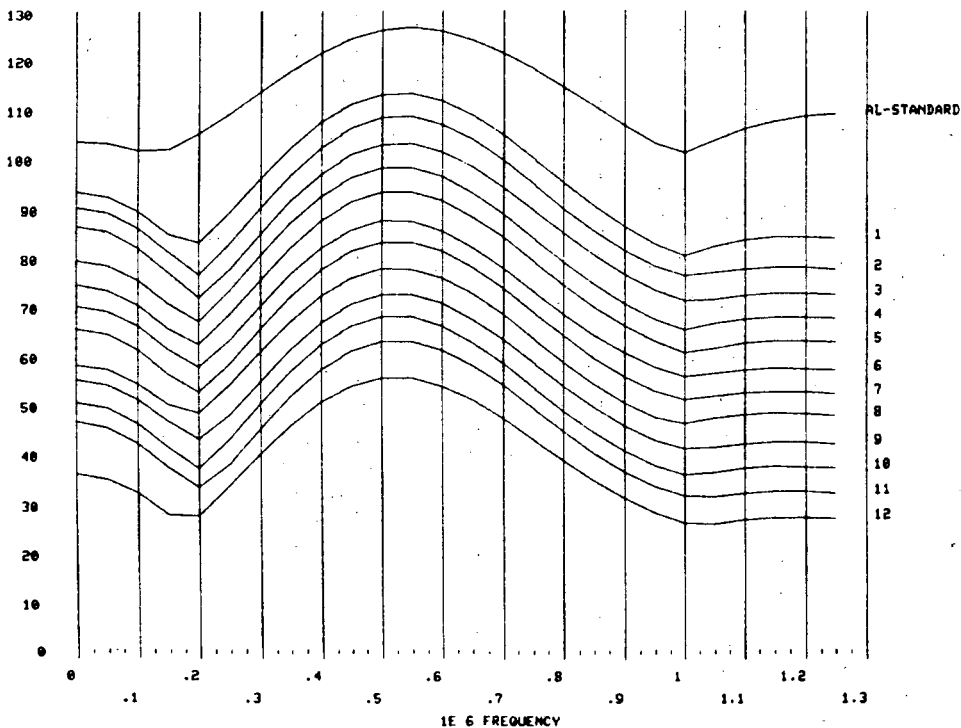


Fig. E:7.5 Fourier amplitude spectra for P waves under 12 saturation conditions under a) 5 MPa, b) 10 MPa, c) 20 MPa, d) 30 MPa uniaxial stress.

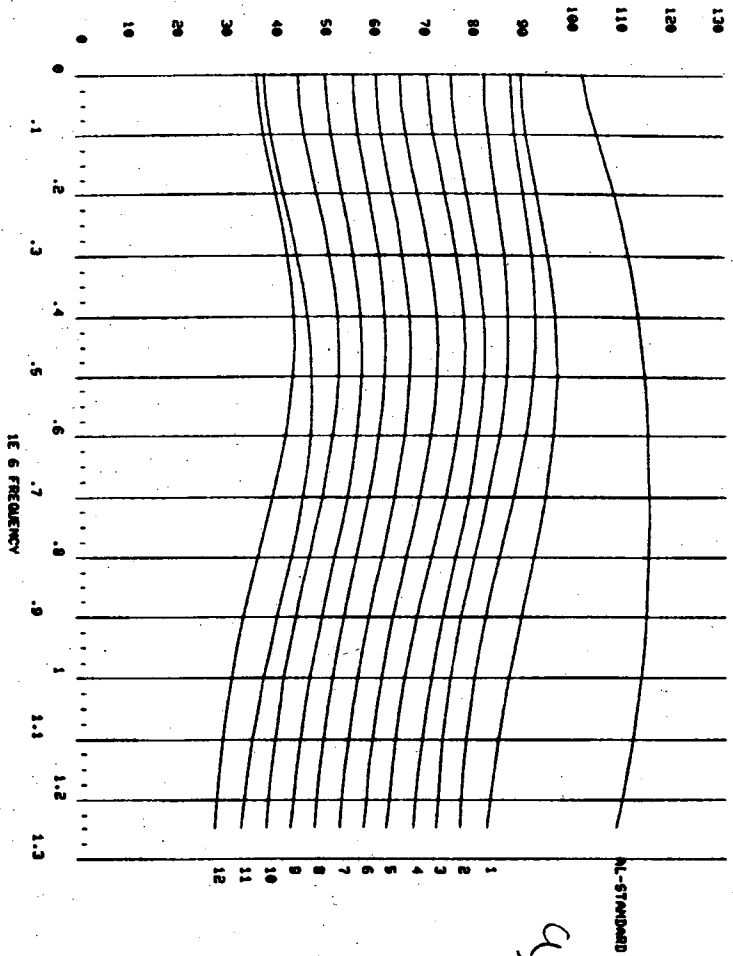
SPECIMEN : STRIPA #1, E21, M8-M6    CONDITION : SAT -> DRY    WINDOW : 4E-6 SEC  
SMOOTH : 0    FILE : STPA28  
P-WAVES    DATE : 27 OCTOBER, 1982



SPECIMEN : STRIPA #1, E21, M8-M6    CONDITION : SAT -> DRY    WINDOW : 4E-6 SEC  
SMOOTH : 0    FILE : STPA30  
P-WAVES    DATE : 27 OCTOBER, 1982



SPECIMEN : STRIPA 01, E21, NB-N6 CONDITION : SAT -> DRY WINDOW : 1+EE-6 SEC  
 SAMPLE : 0 FILE : 57SA10 DATE : 27 OCTOBER, 1982  
 S-WAVES



SPECIMEN : STRIPA 01, E21, NB-N6 CONDITION : SAT -> DRY WINDOW : 1+EE-6 SEC  
 SAMPLE : 0 FILE : 57SA10 DATE : 27 OCTOBER, 1982  
 S-WAVES

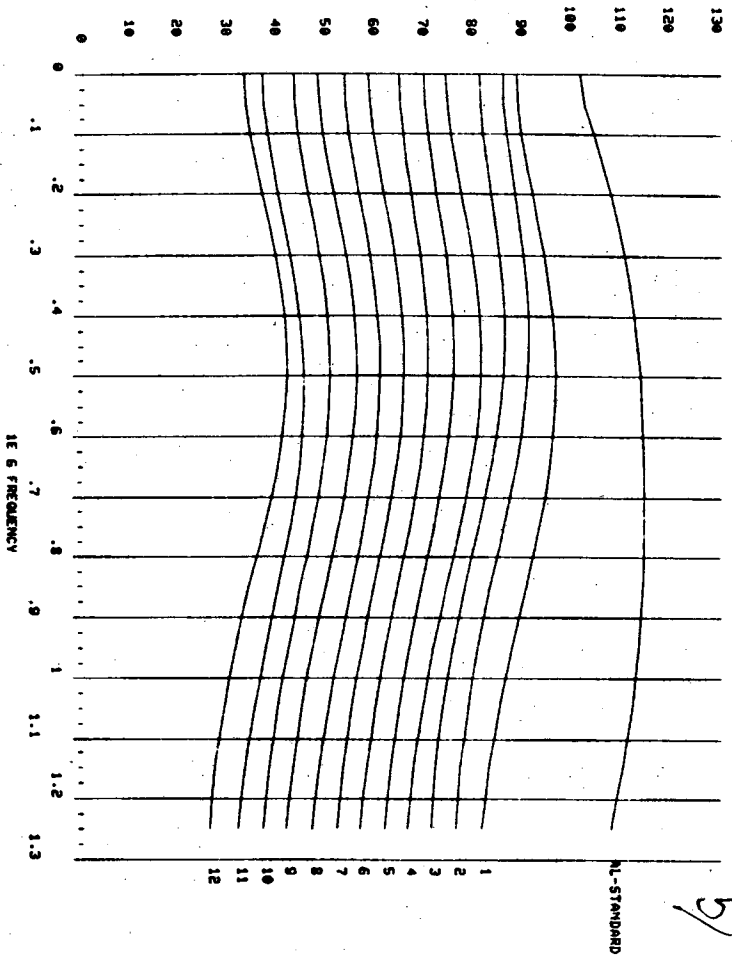
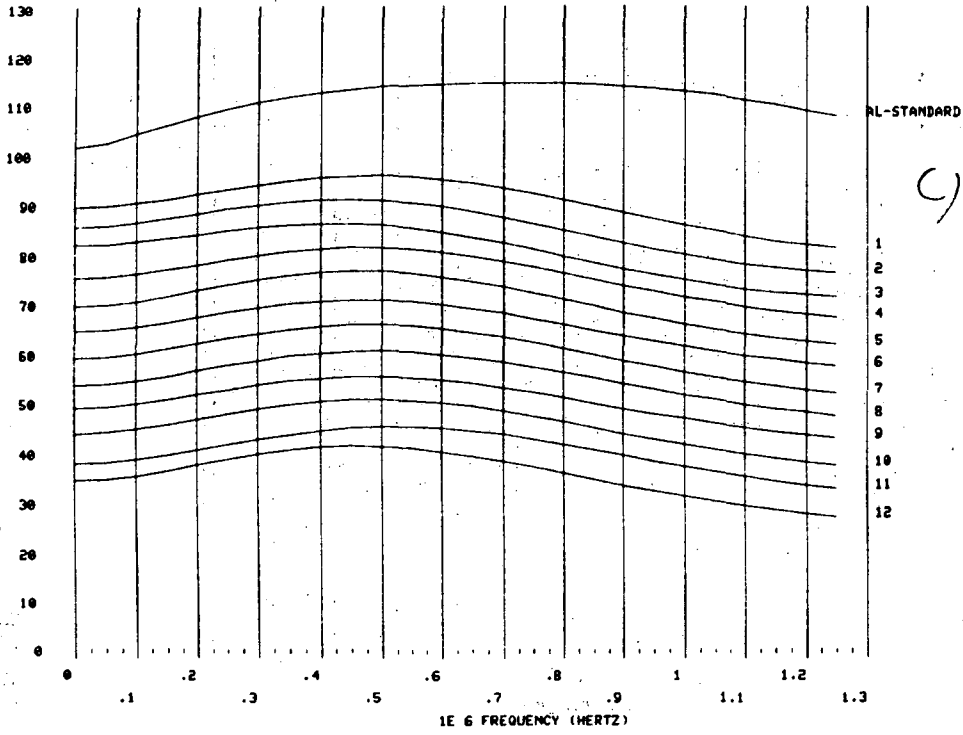
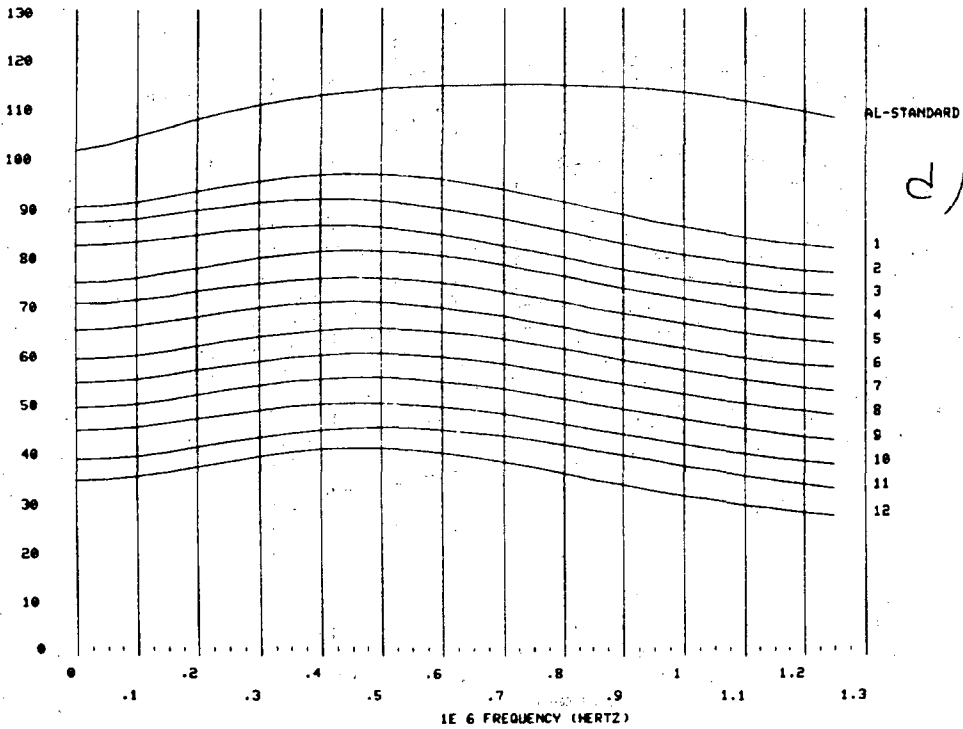


Fig. E:7.6 Fourier amplitude spectra for S waves under 12 saturation conditions under a) 5 MPa, b) 10 MPa, c) 20 MPa, d) 30 MPa uniaxial stress.

SPECIMEN : STRIPA 01, E21, M8-M6 CONDITION : SAT -> DRY WINDOW : 1+2E-6 SEC  
SMOOTH : 0 FILE : 5T5A20.  
S-WAVES DATE : 27 OCTOBER, 1982



SPECIMEN : STRIPA 01, E21, M8-M6 CONDITION : SAT -> DRY WINDOW : 1+2E-6 SEC  
SMOOTH : 0 FILE : 5T5A30.  
S-WAVES DATE : 27 OCTOBER, 1982



## Appendix E:8 - Saturation experiment for specimen # 2.

In this appendix the data for the saturation experiment from specimen # 2 is presented. For each saturation level the specimen was tested at four different uniaxial stresses. For the presentation of the data the waveforms and the amplitude spectra were assembled in their different stress groups.

SPECIMEN FILE 1STDAT2.WET

DATE 127 OCTOBER, 1982

LENGTH OF SPECIMEN : .081928 METER. DIAMETER OF SPECIMEN : 5.1689 CENTIMETER

NUMBER OF LOADS : 4

DENSITY OF SPECIMEN :

2631	2630	2630	2630	2630
2629	2629	2629	2629	2629
2628	2628 KG/M-3			

POROSITY : .949747 %

THE UNIAXIAL STRESS IS : 5 MPa

WEIGHT (GRAMS)	SATURATION (%)	P-WAVE VEL (M/S)	S-WAVE VEL (M/S)	YOUNGS M (GPA)	BULK M (GPA)	SHEAR M (GPA)	PO. RA
452.353	100	5852	3401	76	50	30	.24501
452.218	78	5451	3309	70	40	29	.208256
452.17	70	5252	3292	67	35	28	.176514
452.143	66	5105	3237	64	32	28	.163699
452.121	63	5098	3214	64	32	27	.170181
452.043	50	4974	3195	62	29	27	.140761
452.028	48	4932	3187	61	28	27	.141053
451.953	36	4814	3183	59	25	27	.11155
451.918	30	4752	3182	58	24	27	.0937929
451.871	23	4733	3171	58	24	26	.0929625
451.763	6	4608	3138	55	21	26	.0676624
451.725	0	4552	3116	54	20	26	.0587806

THE UNIAXIAL STRESS IS : 9 MPa

WEIGHT (GRAMS)	SATURATION (%)	P-WAVE VEL (M/S)	S-WAVE VEL (M/S)	YOUNGS M (GPA)	BULK M (GPA)	SHEAR M (GPA)	PO. RA
452.353	100	5865	3422	77	49	31	.241825
452.218	78	5510	3337	71	41	29	.210266
452.17	70	5369	3293	68	38	29	.190473
452.143	66	5212	3252	66	34	28	.18107
452.121	63	5215	3269	66	34	28	.176279
452.043	50	5101	3246	64	31	28	.159852
452.028	48	5057	3234	63	31	28	.153927
451.953	36	5054	3228	63	31	27	.155509
451.918	30	4868	3243	61	25	28	.100854
451.871	23	4845	3248	60	25	28	.0957026
451.763	6	4772	3194	59	24	27	.0940541
451.725	0	4696	3176	57	23	26	.0784116

THE UNIAXIAL STRESS IS : 19 MPa

WEIGHT (GRAMS)	SATURATION (%)	P-WAVE VEL (M/S)	S-WAVE VEL (M/S)	YOUNGS M (GPA)	BULK M (GPA)	SHEAR M (GPA)	PO. RA
452.353	100	5890	3461	78	49	32	.236235
452.218	78	5733	3441	76	45	31	.218504
452.17	70	5642	3400	74	43	30	.215078
452.143	66	5510	3369	72	40	30	.201472
452.121	63	5499	3355	71	40	30	.203454
452.043	50	5481	3322	69	38	29	.195586
452.028	48	5330	3321	69	36	29	.182794
451.953	36	5317	3298	68	36	29	.187178
451.918	30	5215	3275	66	34	28	.174569
451.871	23	5215	3268	66	34	28	.176705
451.763	6	5086	3238	64	31	28	.159011
451.725	0	5076	3234	64	31	27	.158235

THE UNIAXIAL STRESS IS : 28 MPa

WEIGHT (GRAMS)	SATURATION (%)	P-WAVE VEL (M/S)	S-WAVE VEL (M/S)	YOUNGS M (GPA)	BULK M (GPA)	SHEAR M (GPA)	PO. RA
452.353	100	5920	3489	79	49	32	.233791
452.218	78	5865	3533	80	47	33	.215189
452.17	70	5802	3503	78	46	32	.21331
452.143	66	5713	3473	77	44	32	.206949
452.121	63	5693	3463	76	43	32	.206467
452.043	50	5619	3427	74	42	31	.204025
452.028	48	5558	3424	74	40	31	.194314
451.953	36	5543	3392	73	40	30	.20057
451.918	30	5433	3376	71	38	30	.185579
451.871	23	5447	3370	71	38	30	.189943
451.763	6	5337	3326	69	36	29	.182462
451.725	0	5265	3336	68	34	29	.164737

Table E:8.1 Data from specimen # 2 during saturation experiment.

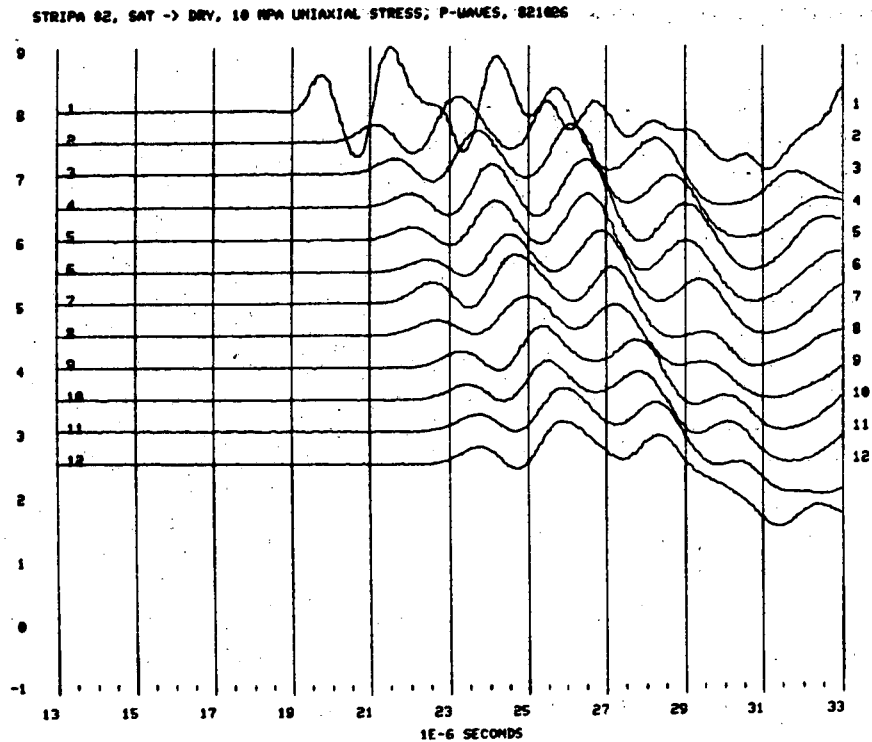
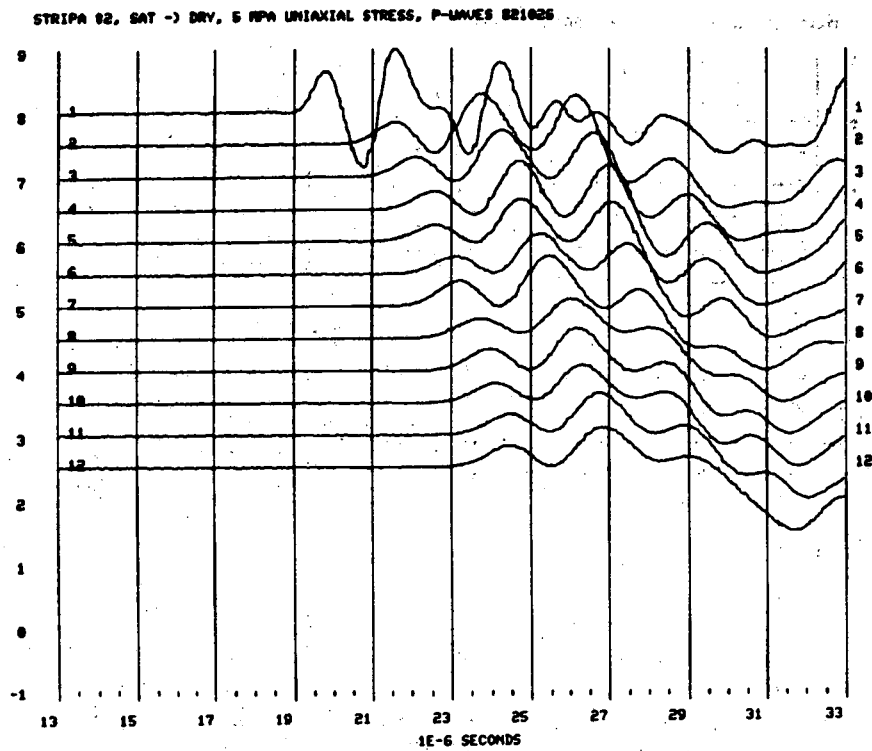
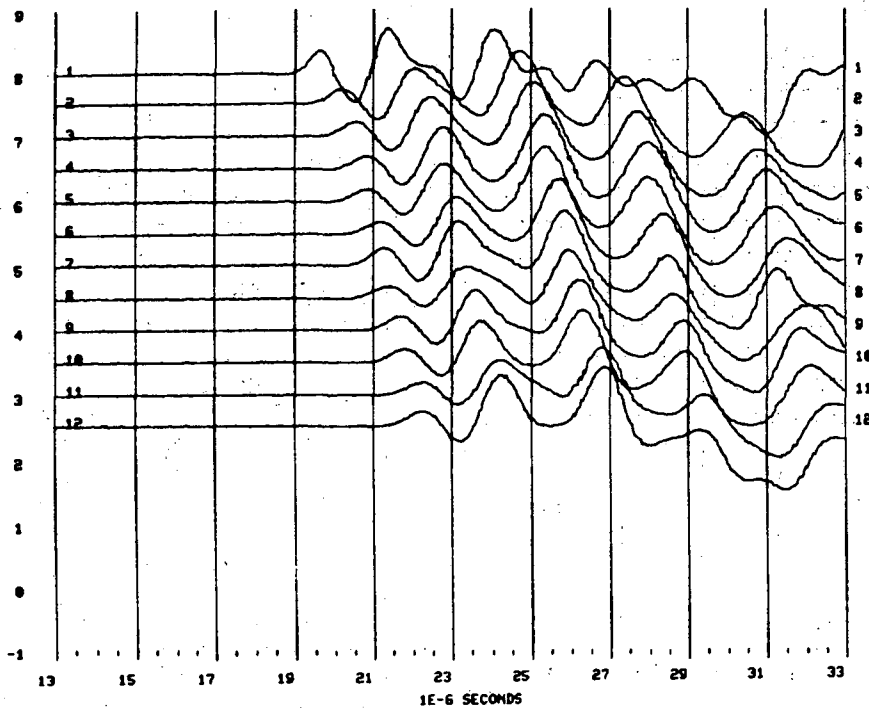
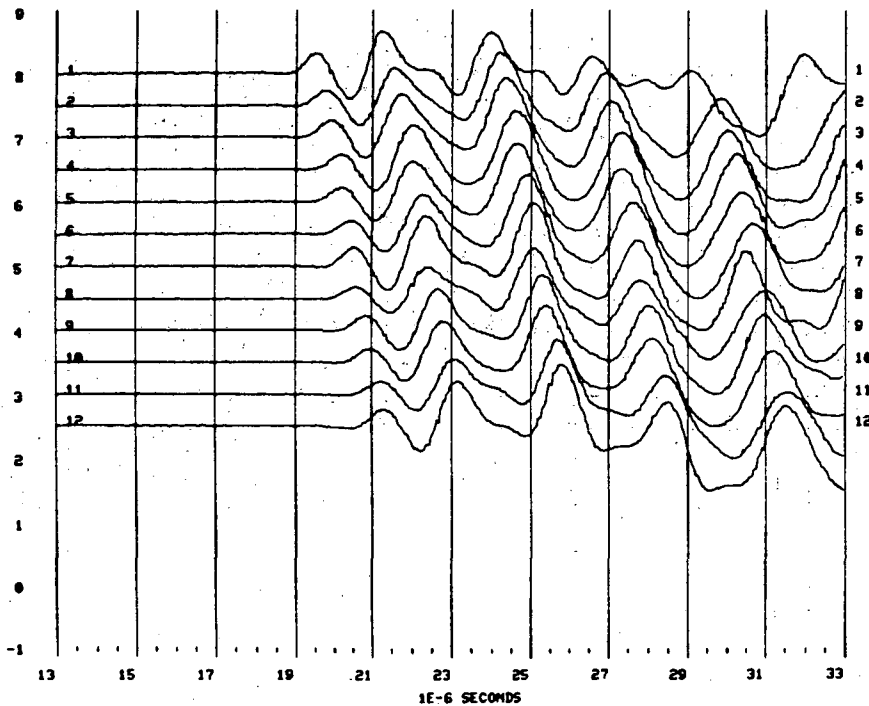


Fig. E.8.1 P waves for 12 saturation conditions under a) 5 MPa, b) 10 MPa, c) 20 MPa, d) 30 MPa uniaxial stress.

STRIPA 82, SAT -> DRY, 20 MPa UNIAXIAL STRESS, P-WAVES, 821026



STRIPA 82, SAT -> DRY, 30 MPa UNIAXIAL STRESS, P-WAVES, 821026





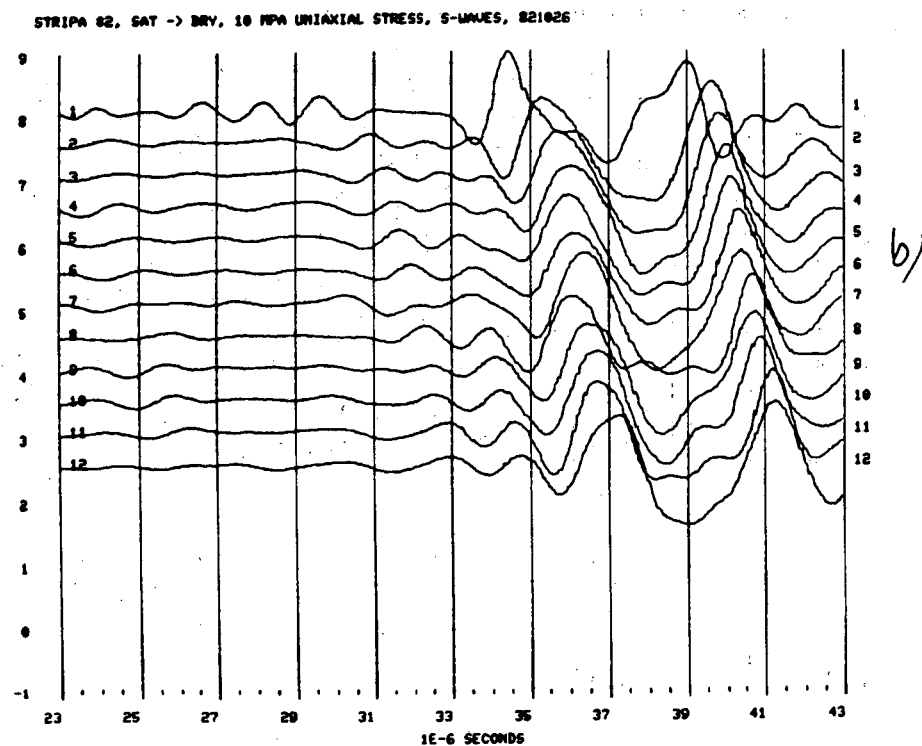
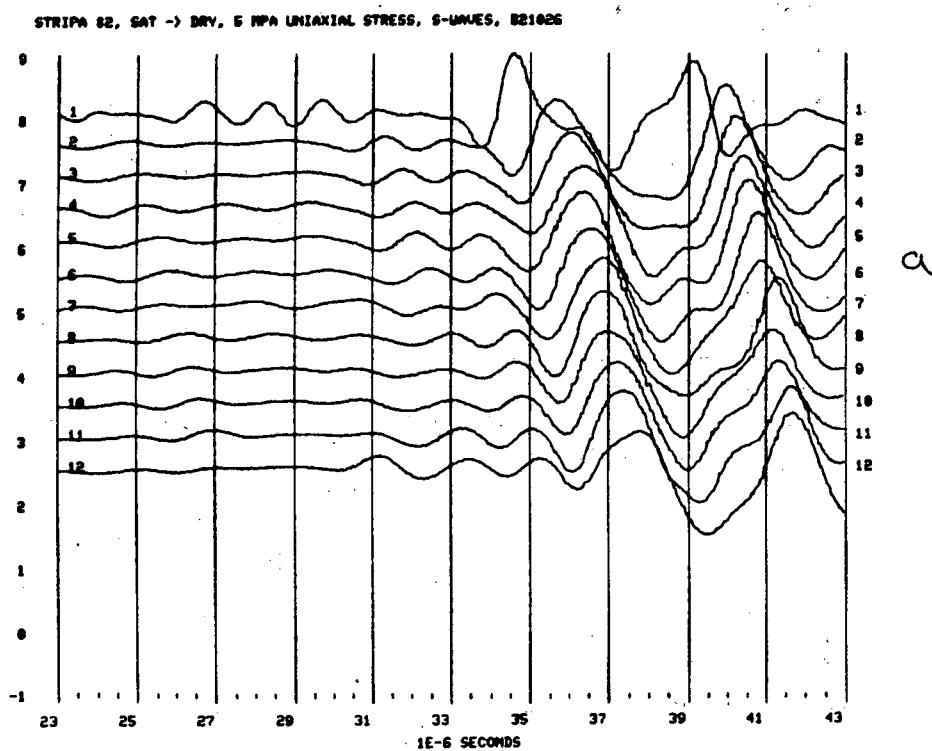
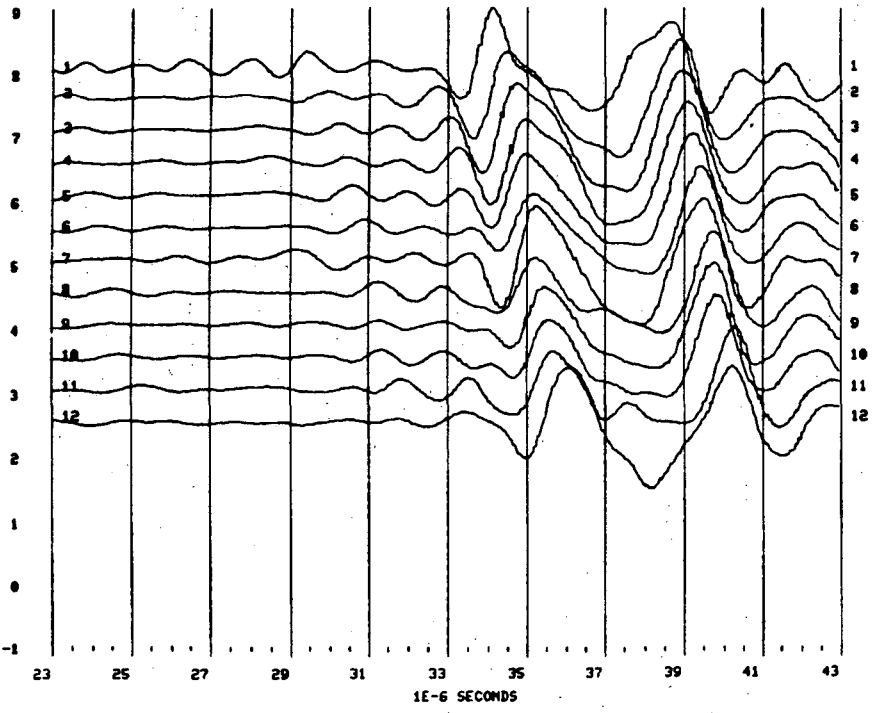
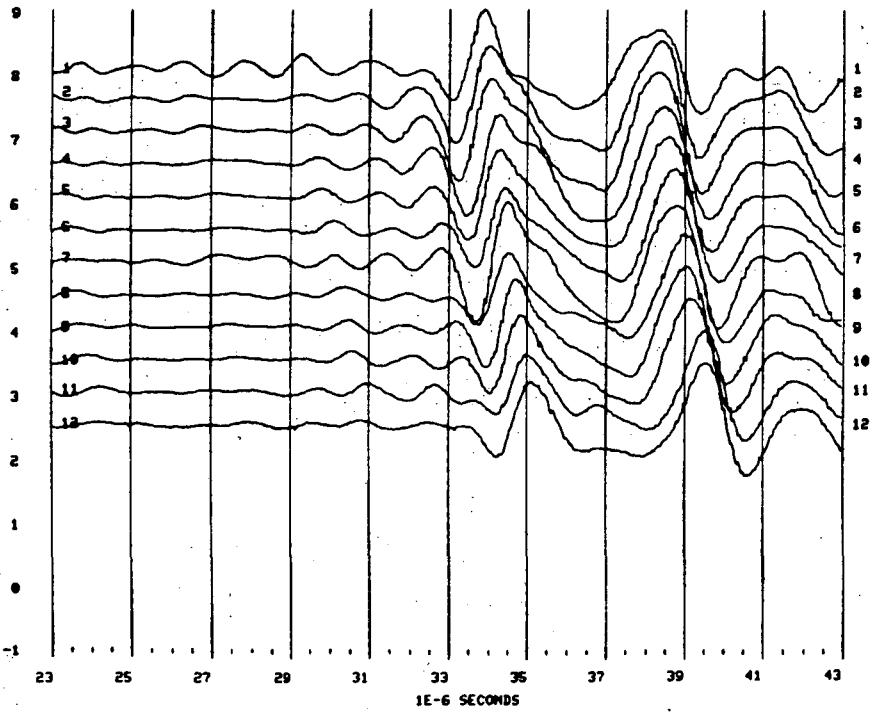


Fig. E:8.2 S waves for 12 saturation conditions under a) 5 MPa, b) 10 MPa, c) 20 MPa, d) 30 MPa uniaxial stress.

STRIPA 82, SAT -> DRY, 20 MPa UNIAXIAL STRESS, S-WAVES, 821026



STRIPA 82, SAT -> DRY, 30 MPa UNIAXIAL STRESS, S-WAVES, 821026



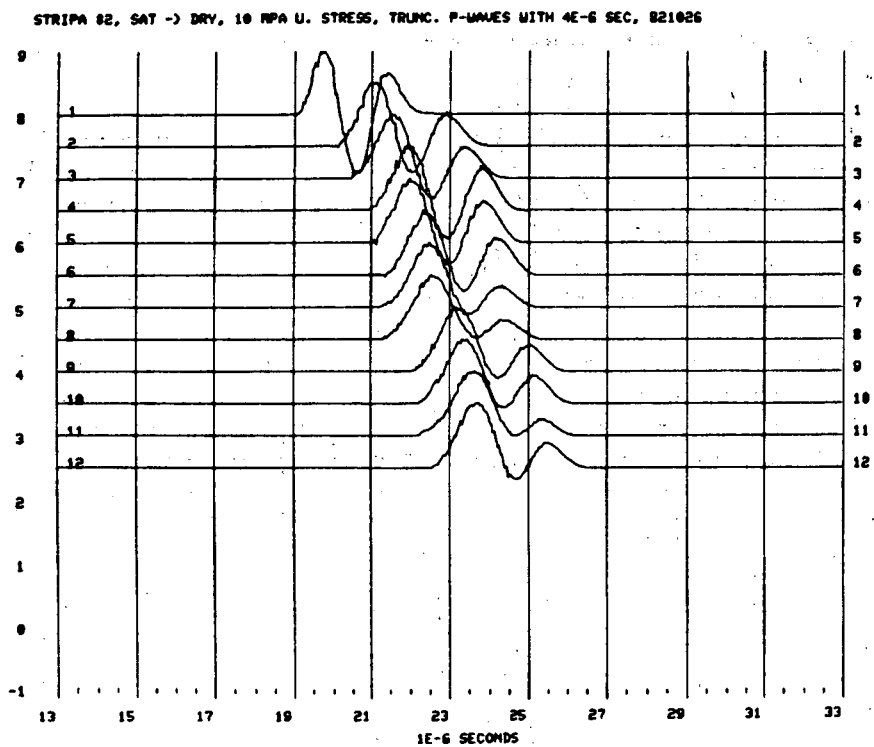
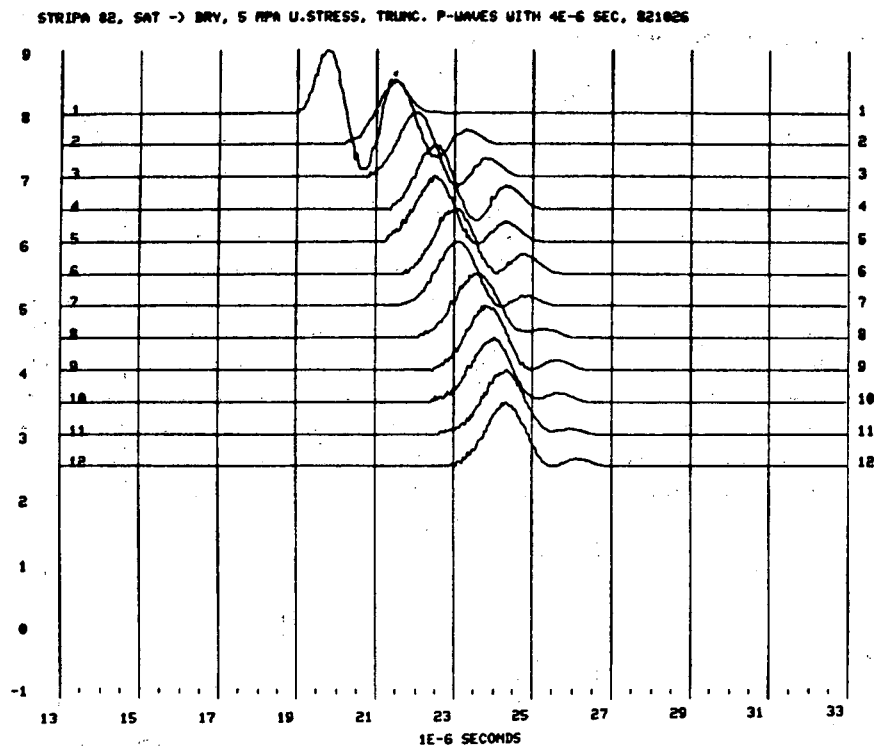
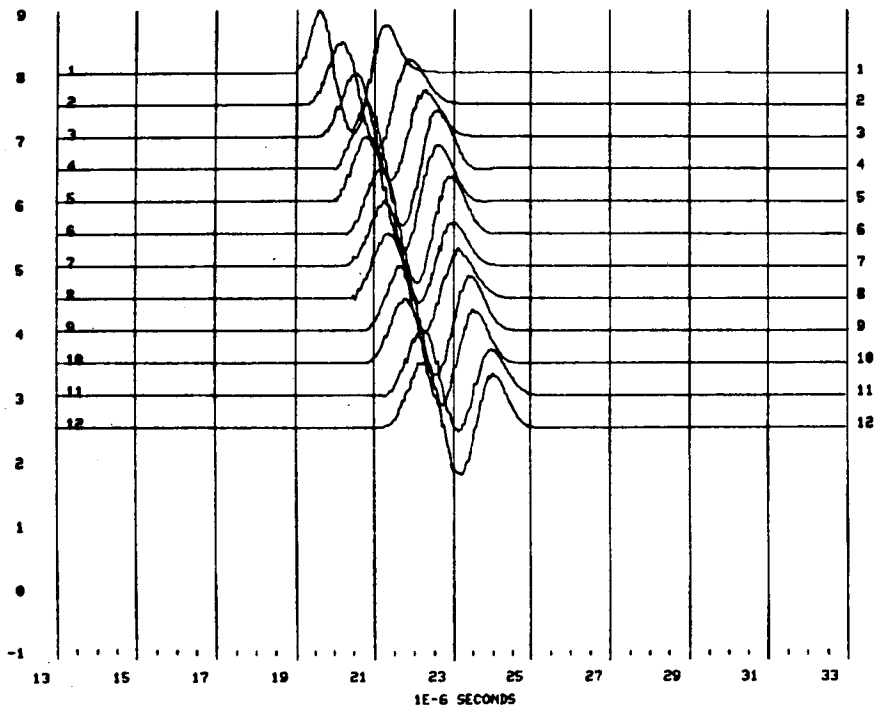
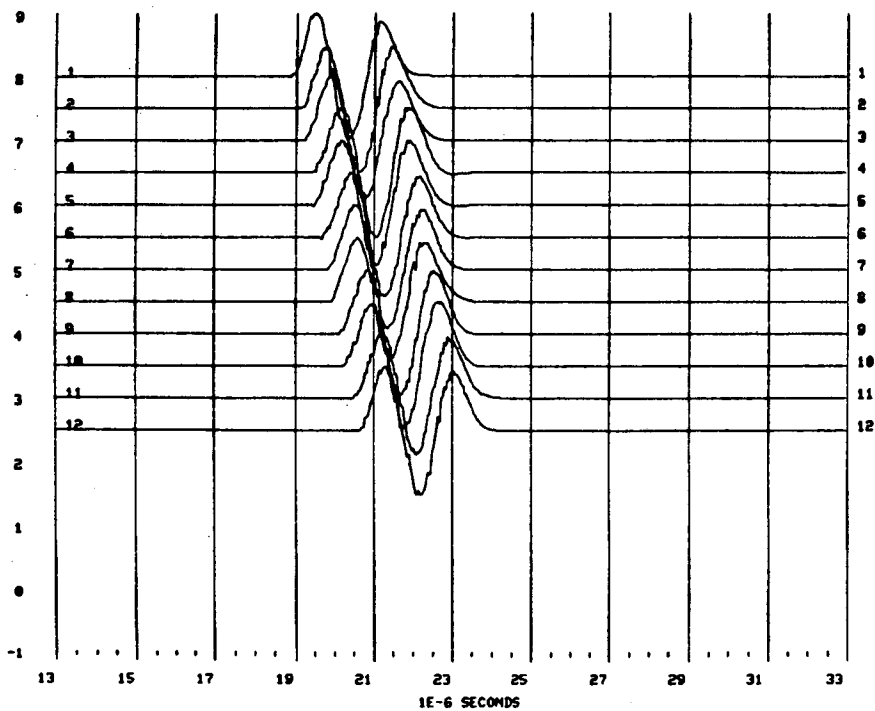


Fig. E:8.3 Truncated P waves for 12 saturation conditions under a) 5 MPa, b) 10 MPa, c) 20 MPa, d) 30 MPa uniaxial stress.

STRIPA 82, SAT -> DRY, 20 MPa U. STRESS, TRUNC. P-WAVES WITH 4E-6 SEC, 821026



STRIPA 82, SAT -> DRY, 30 MPa U. STRESS, TRUNC. P-WAVES WITH 4E-6 SEC WIND. 821026



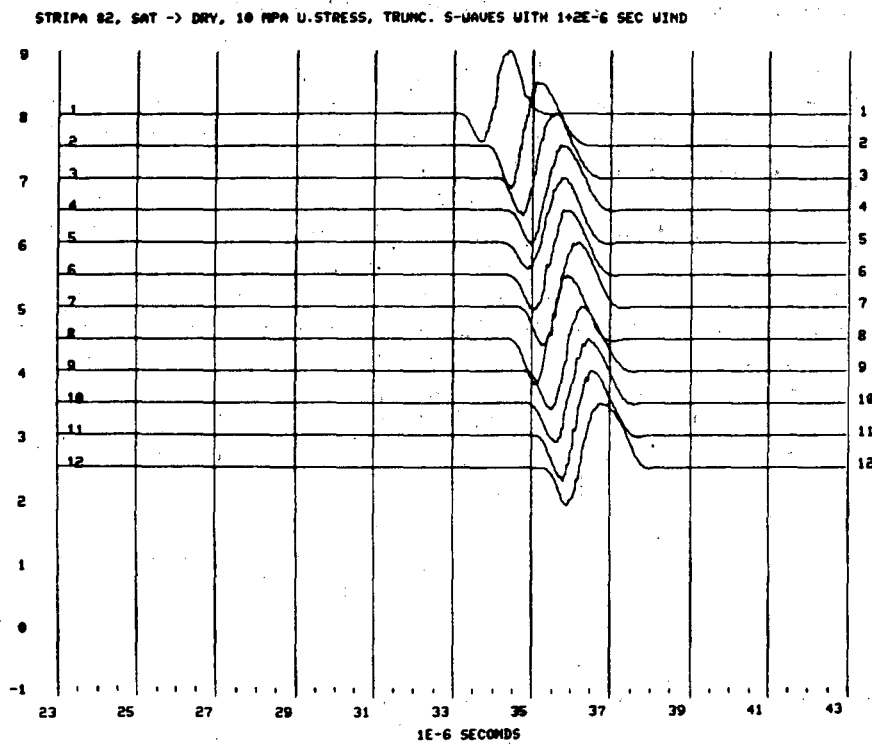
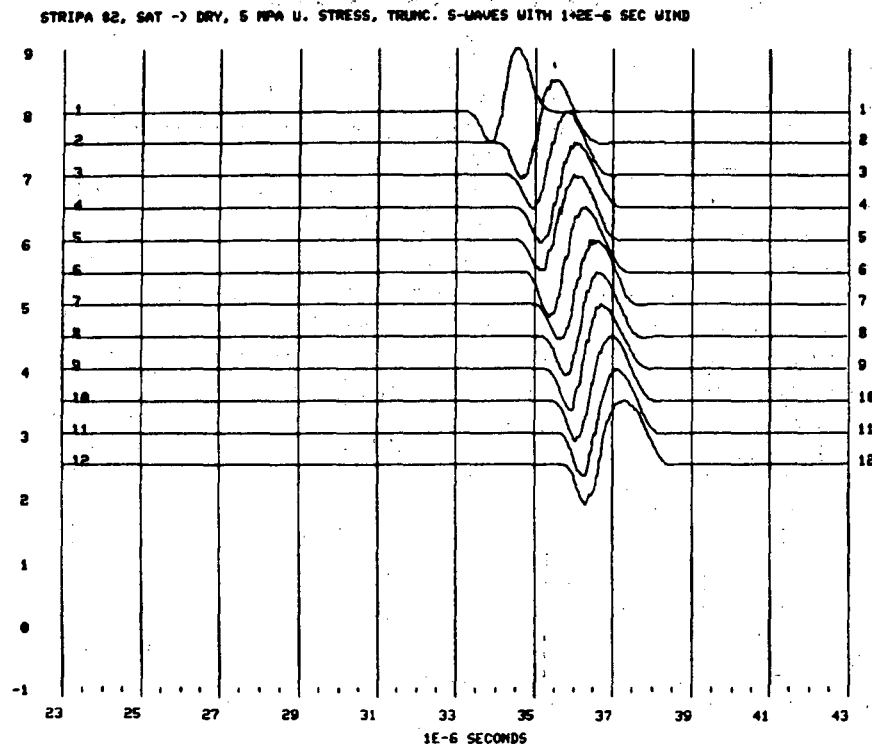
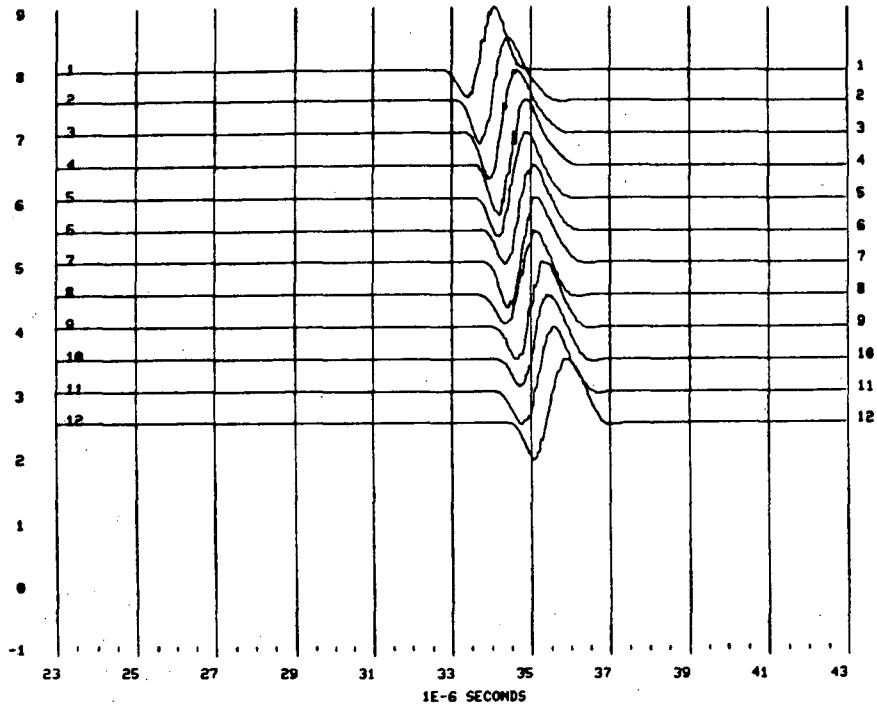
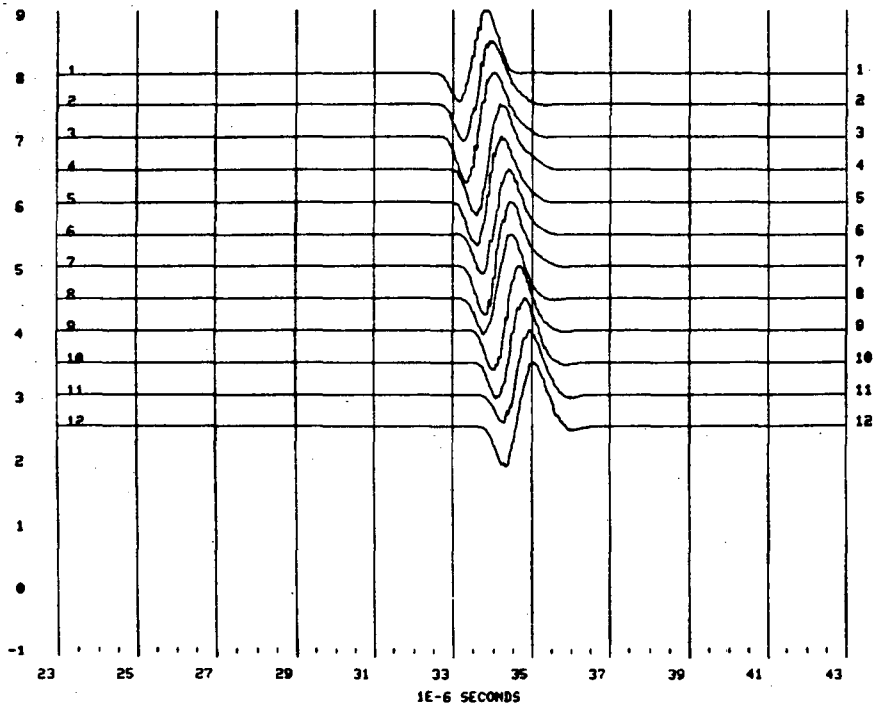


Fig. E:8.4 Truncated S waves for 12 saturation conditions under a) 5 MPa, b) 10 MPa, c) 20 MPa, d) 30 MPa uniaxial stress.

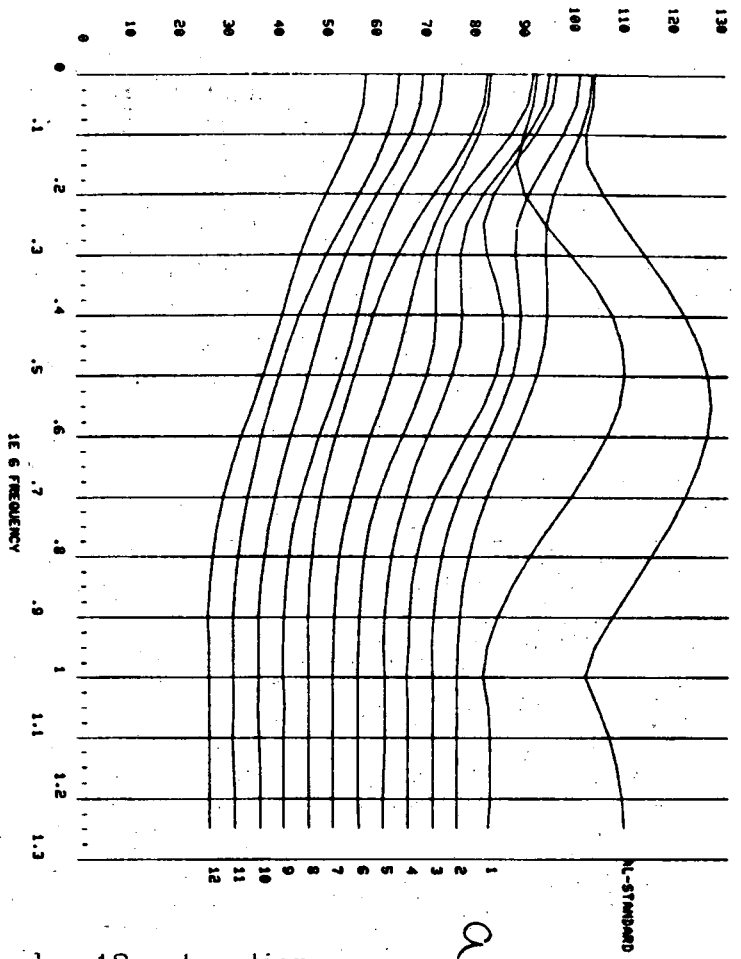
STRIPA 82, SAT -> DRY, 20 NPA U. STRESS, TRUNC. S-WAVES WITH 1+2E-6 SEC WIND



STRIPA 82, SAT -> DRY, 30 NPA U. STRESS, TRUNC. S-WAVES WITH 1+2E-6 SEC WIND.

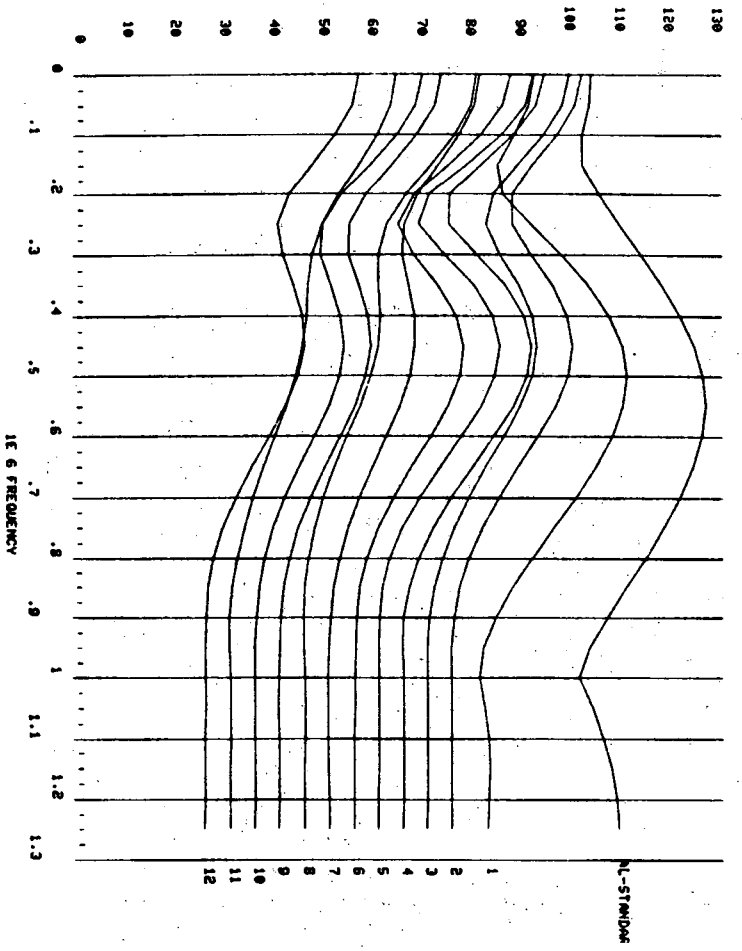


SPECIMEN : STRIPA 82, E24, RT-99 CONDITION : SAT -> DRV WINDOW : 4E-6 SEC  
 SMOOTH : 0 FILE : STRIP10  
 DATE : 27 OCTOBER, 1982  
 P-WAVES



a

SPECIMEN : STRIPA 82, E24, RT-99 CONDITION : SAT -> DRV WINDOW : 4E-6 SEC  
 SMOOTH : 0 FILE : STRIP10  
 DATE : 27 OCTOBER, 1982  
 P-WAVES

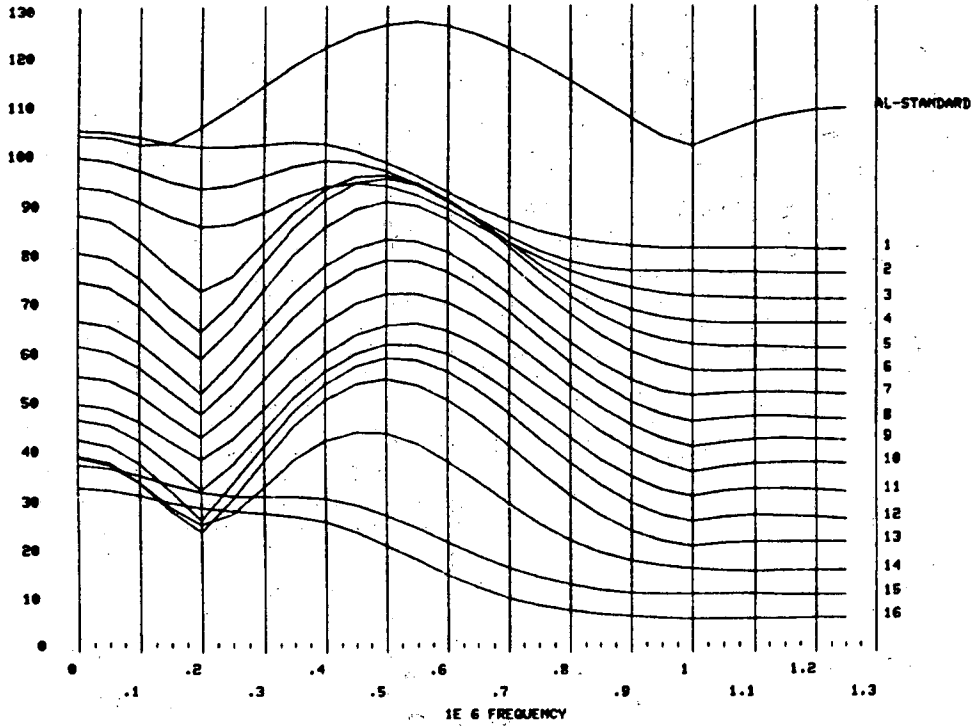


b

Fig. E:8.5 Fourier amplitude spectra for P waves under 12 saturation conditions under a) 5 MPa, b) 10 MPa, c) 20 MPa, d) 30 MPa uniaxial stress.

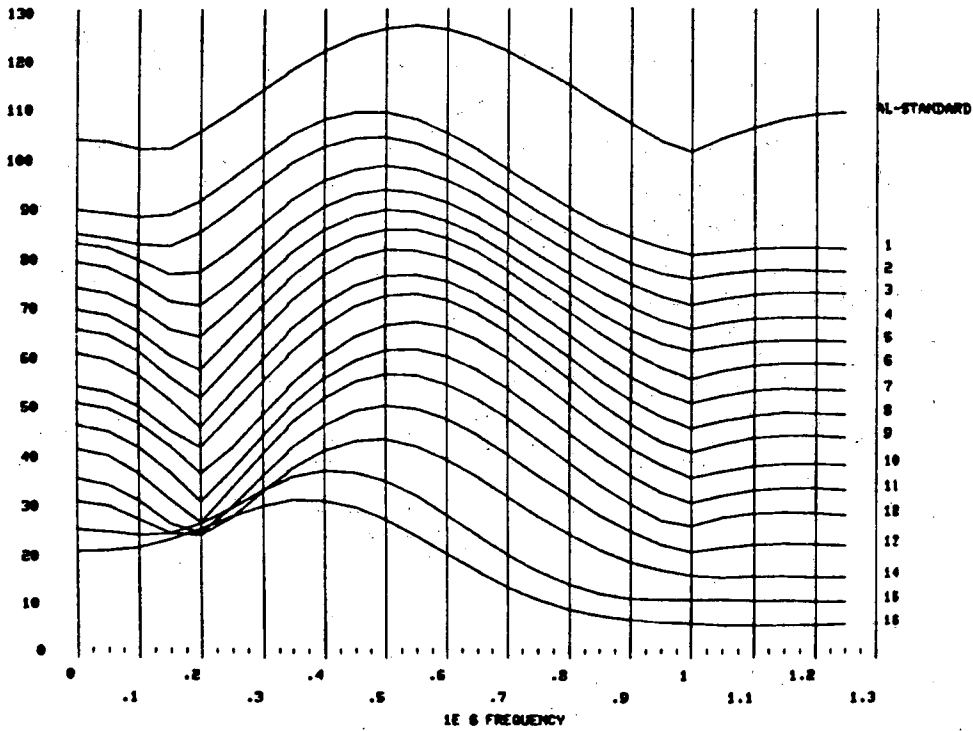
SPECIMEN : STRIPA 82, P-WAVES, WIND: 4E-6 SEC    CONDITION : DRY    WINDOW : 4E-6  
SMOOTH : 0    FILE : STRPA2  
P-WAVES    DATE : 7 SEPTEMBER, 1982

C



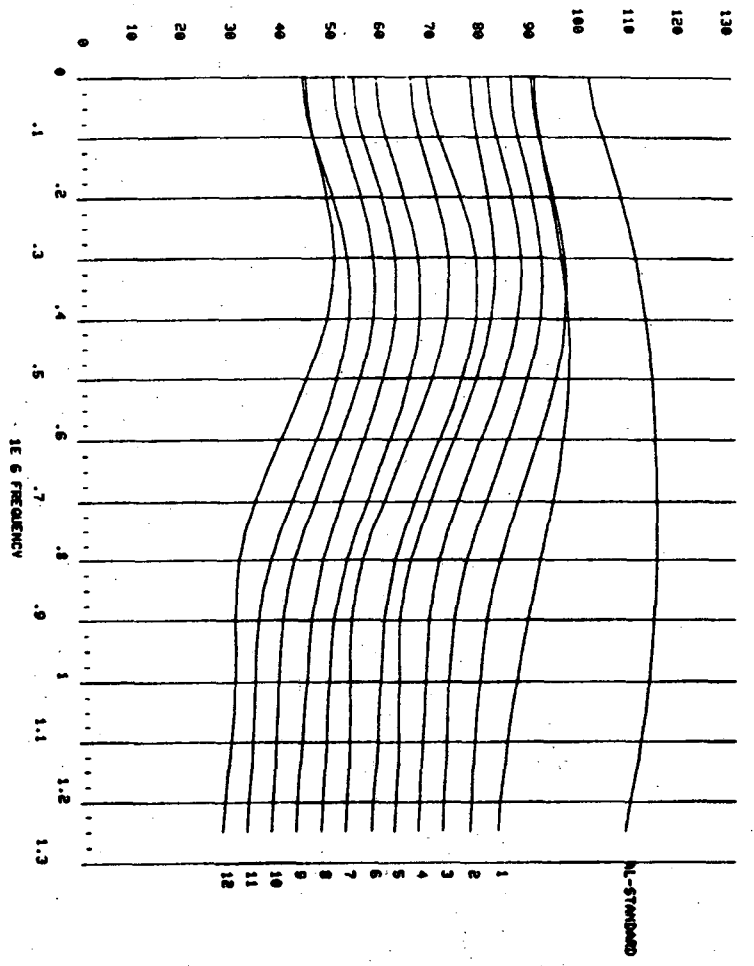
SPECIMEN : STRIPA 82    CONDITION : SATURATED    WINDOW : 4E-6 SEC  
SMOOTH : 0    FILE : STRPA2  
P-WAVES    DATE : 31 AUGUST, 1982

D





SPECIMEN : STRIPA 82, M7-M9 CONDITION : SAT -> DRV WINDOW : 1+2E-6 SEC  
 SMOOTH : 0 FILE : 575518 DATE : 27 OCTOBER, 1982  
 S-WAVES



SPECIMEN : STRIPA 82, E24, M7-M9 CONDITION : SAT -> DRV WINDOW : 1+2E-6 SEC  
 SMOOTH : 0 FILE : 575518 DATE : 27 OCTOBER, 1982  
 S-WAVES

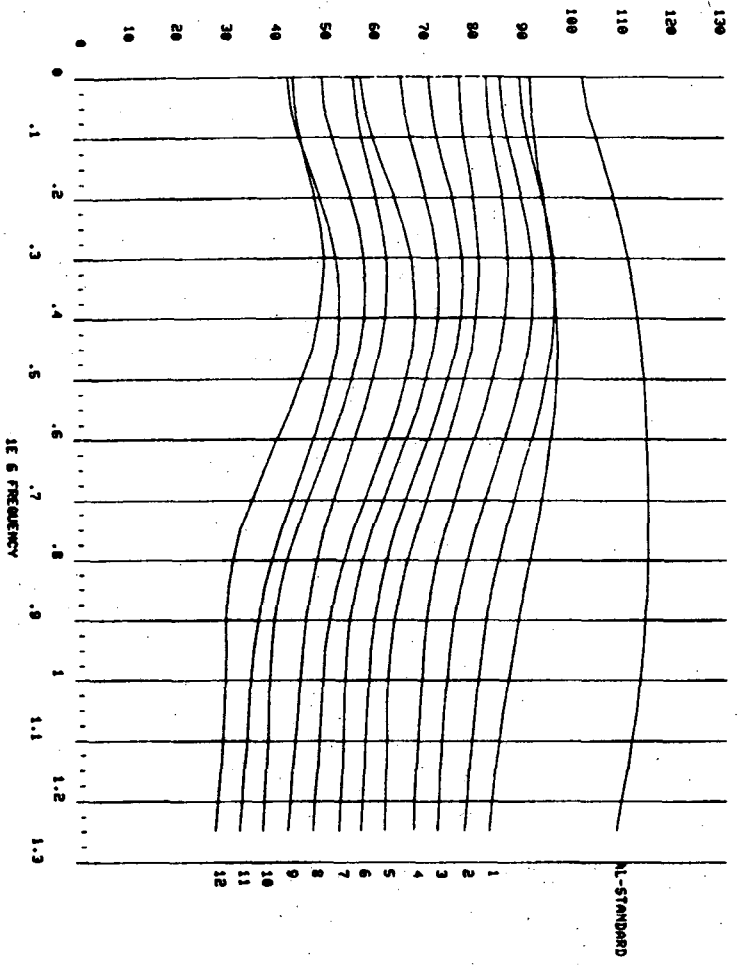
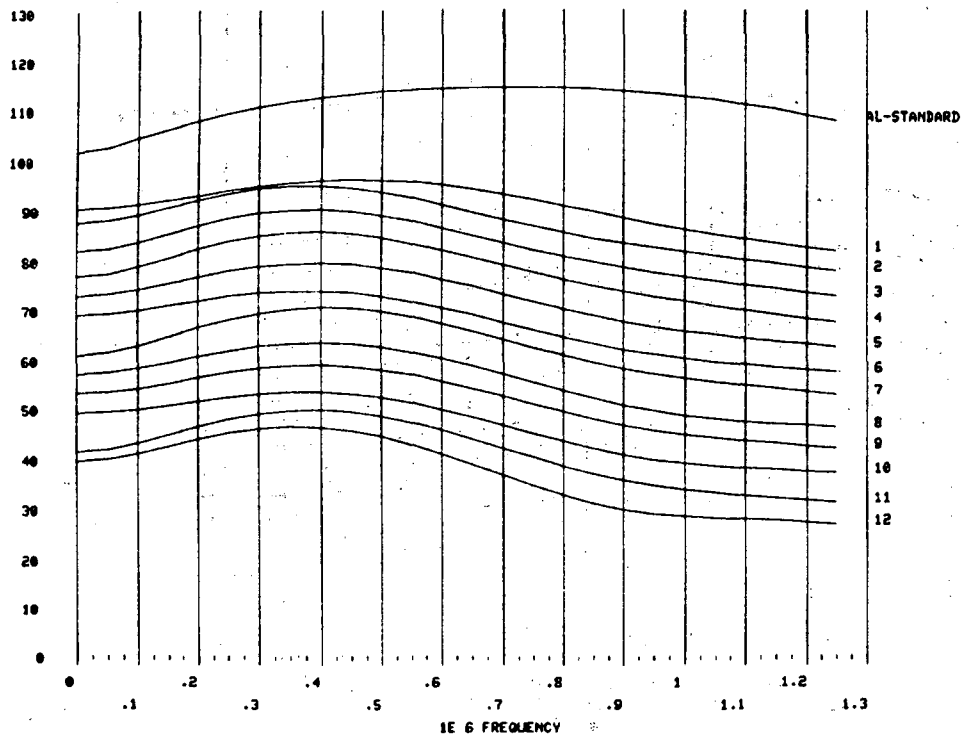


Fig. E:8.6 Fouries amplitude spectra for S waves under 12 saturation conditions under a) 5 MPa, b) 10 MPa, c) 20 MPa, d) 20 MPa (unaxis)

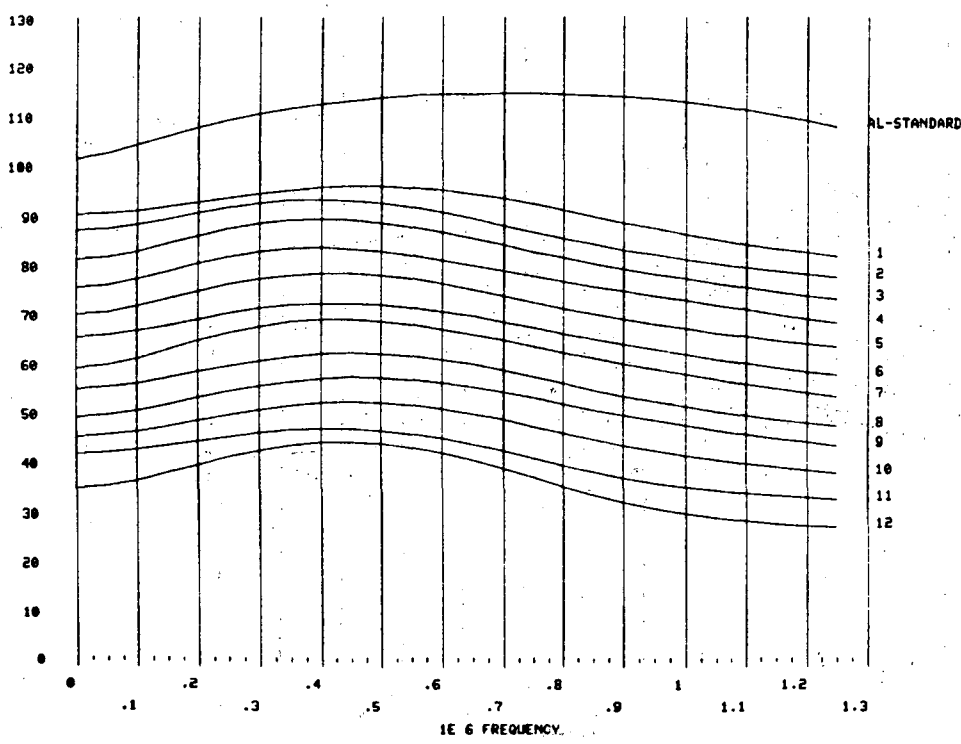
SPECIMEN : STRIPA 82, E24, M7-M9 CONDITION : SAT -> DRY WINDOW : 1+2E-6 SEC  
 SMOOTH : 0 FILE : ST5A29  
 S-WAVES DATE : 27 OCTOBER, 1982

C



SPECIMEN : STRIPA 82, M7-M9, E24 CONDITION : SAT -> DRY WINDOW : 1+2E-6 SEC  
 SMOOTH : 0 FILE : ST5A30  
 S-WAVES DATE : 27 OCTOBER, 1982

D

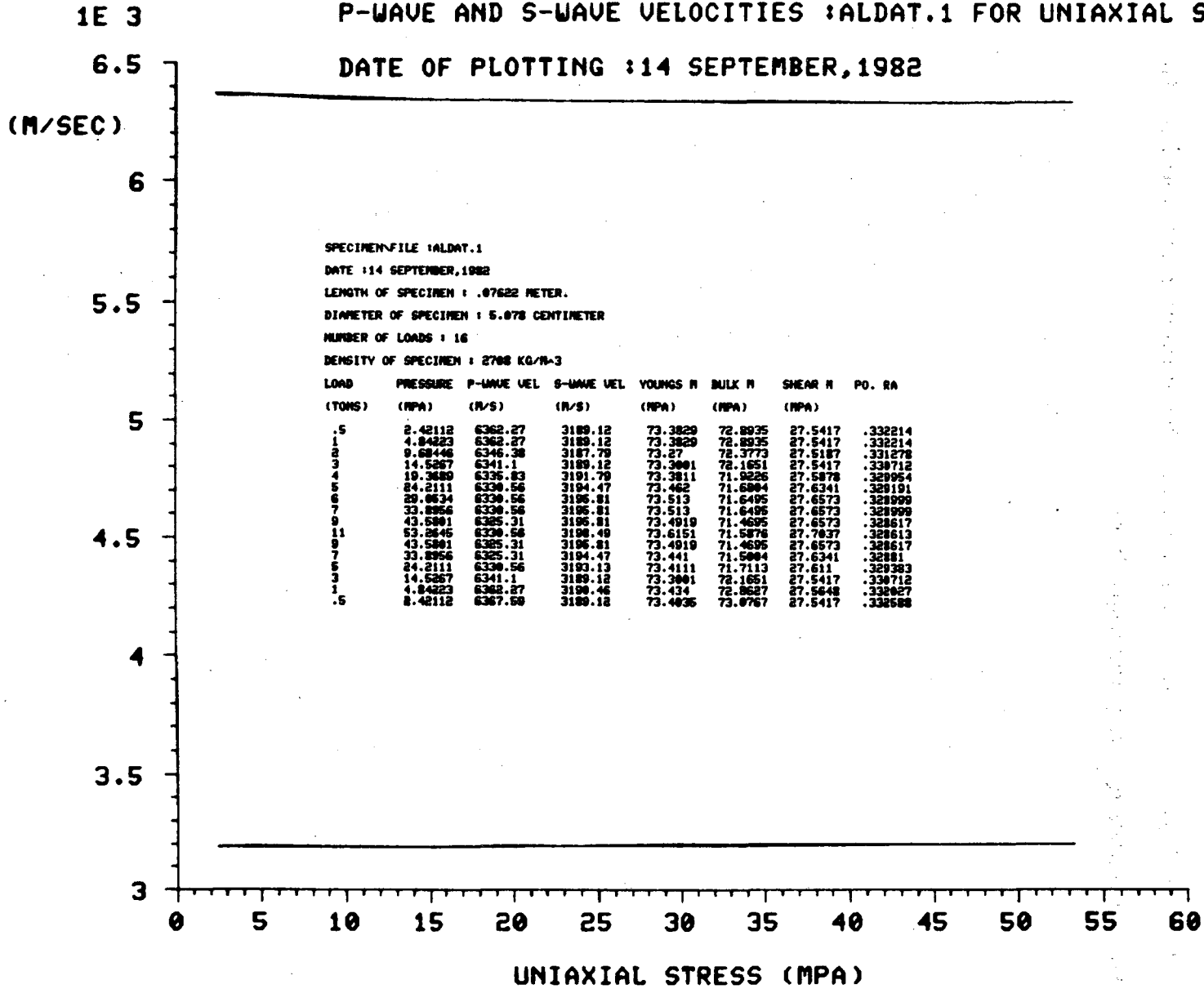


## Appendix E:9 - Test of the influence of the press.

In this appendix the response of testing a specimen with-out microfractures is obtained by subjecting the aluminum standard for the same test cycle as a granite specimen.

P-WAVE AND S-WAVE VELOCITIES :ALDAT.1 FOR UNIAXIAL STRESS

DATE OF PLOTTING :14 SEPTEMBER,1982



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TECHNICAL INFORMATION DEPARTMENT  
LAWRENCE BERKELEY LABORATORY  
UNIVERSITY OF CALIFORNIA  
BERKELEY, CALIFORNIA 94720