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In-Use Passenger Vessel Emission Rates of Black Carbon and Nitrogen Oxides

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Peer reviewed

1	In-Use Passenger Vessel Emission Rates of Black Carbon and Nitrogen Oxides
2	
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11	
12	Abstract
13	This study quantified emission factors of black carbon (BC) and nitrogen oxides (NO <sub>x</sub> ) from 21
14	engines on in-use excursion vessels and ferries operating in California's San Francisco Bay,
15	including EPA uncertified and Tier 1-4 engines and across engine operating modes. On average,
16	$\sim$ 60 fuel-based emission factors per engine were measured using a novel combination of exhaust
17	plume capture combined with GPS location and speed data that can be more readily deployed
18	than common portable emissions measurement systems. BC and $NO_x$ emission factors (g kg <sup>-1</sup> )
19	were lowest and least variable during fast cruising and highest during maneuvering and docked
20	operation. Selective catalytic reduction (SCR) reduced NO <sub>x</sub> emissions by $\sim$ 80% when functional.
21	However, elevated NO <sub>x</sub> emissions that exceeded corresponding exhaust standards were

- 22 measured on most Tier 3 and Tier 4 engines sampled, which can be attributed to inactive SCR
- 23 during frequent low engine load operation. In contrast, BC emissions exceeded the PM emission

24	standard for only one engine, and SCR systems employed as a NO <sub>x</sub> reduction technology also
25	reduced emitted BC. Using these measured emission factors to compare commuting options, we
26	show that the CO <sub>2</sub> -equivalent emissions per passenger-kilometer are comparable when
27	commuting by car and ferry, but BC and NO <sub>x</sub> emissions can be several to more than ten times
28	larger when commuting by ferry.
29	
30	Keywords
31	selective catalytic reduction, pollutant emission inventory, carbon footprint, diesel exhaust, air
32	pollution, commercial harbor craft, transportation
33	
34	Synopsis
35	This study uses a novel approach to quantify pollutant emission rates from in-use passenger
36	vessels and the effectiveness of selective catalytic reduction of nitrogen oxides to support
37	emission inventory development and inform air pollution policy decision-making.
38	
39	Graphic for Table of Contents (TOC)/Abstract Art



### 42 Introduction

Diesel engines are an important source of air pollutants that degrade air quality and contribute to climate change, including nitrogen oxides (NO<sub>x</sub>), particulate matter (PM), and black carbon (BC), a major component of diesel PM.<sup>1–3</sup> While most diesel fuel is consumed by on-road vehicles, stricter regulations and broader use of emission control technologies by the onroad fleet mean that off-road engines increasingly contribute a larger portion of remaining emissions.<sup>4–10</sup>

49 Marine vessels are an off-road source that cause an estimated 60,000 cardiopulmonary and lung cancer deaths each year globally.<sup>11,12</sup> Commercial harbor craft (CHC), including ferries 50 51 and excursion vessels, are a subset of marine vessels that operate particularly close to shore and 52 nearby communities, unlike other categories of ocean-going vessels. Recognizing these impacts, 53 California has accelerated the adoption of higher tier marine engines that meet more stringent PM and NO<sub>x</sub> emission standards set by the U.S. Environmental Protection Agency (EPA).<sup>13,14</sup> 54 55 Since 2009, all newly purchased vessels must meet the standards for Tier 2 or better engines, and 56 select in-use vessel categories operating in Regulated California Waters must meet Tier 2 or Tier 3 engine standards by the end of 2022 via engine replacement or certification. 57

As efforts to control CHC emissions continue, it is noteworthy that pollutant emissions rates from in-use CHC have not been well characterized and only a few studies have related emissions to engine operating conditions.<sup>15–22</sup> Additionally, as Tier 4 engines are originally equipped and other engines can be retrofitted with selective catalytic reduction (SCR) to reduce NO<sub>x</sub> emissions, it is critical to verify the effectiveness of SCR on in-use vessels. Emission inventories used for air pollution hazard assessments currently rely heavily on outdated datasets and older, controlled engine certification tests.<sup>23</sup> These inventories need be updated with newly

measured emission factors that include in-use engine and emission control system operation and
 performance.

67 This study measured BC and  $NO_x$  emission rates from excursion vessels and ferries 68 operating in California's San Francisco (SF) Bay. Engines on the vessels met a range of emission 69 standards (EPA uncertified and Tier 1-4) and included Tier 3 engines retrofitted with SCR, as 70 described in Table S1 of the Supporting Information (SI). For simplification, we refer to EPA 71 uncertified engines as Tier 0. While the sampled fleet was based in the SF Bay, these vessels 72 comply with national engine emission standards. Therefore, the results of this study are 73 informative of what can be expected as CHC fleets outside of California modernize. The scope 74 of this study was made possible through a novel application of an exhaust plume capture method 75 that had previously been extensively applied to measure pollutant emission rates from on-road heavy-duty diesel trucks.<sup>5,6,24</sup> Owing to the low cost, size, and power consumption of modern 76 77 sensors and the noninvasive approach of exhaust plume capture, the method is more readily 78 deployable than a traditional portable emission measurements system (PEMS) and enables 79 access to a greater number of engines. More than 1400 short-duration exhaust samples were 80 captured on-board in-use vessels to characterize the influence of operating mode on emission 81 rates and effectiveness of SCR systems. On three vessels, engine data was provided by either the 82 manufacturer or another research team that concurrently deployed PEMS. This data provided 83 fuel consumption rates that informed the weighting of the snapshot emission factors measured in 84 the present study across engine operating modes for each sampled engine. These in-use, 85 operating-mode-weighted emission rates are also compared to EPA emission standards and used 86 to compare the carbon and air pollution footprints associated with commuter travel by ferry and 87 passenger vehicle.

## 89 Materials and Methods

90	Concentrations of carbon dioxide (CO <sub>2</sub> ), BC, and NO <sub>x</sub> were measured in the diluted
91	exhaust from the main engines of ferries and excursion vessels. In total, 25 tests were conducted
92	on 21 engines on 14 vessels, as summarized in Table S2. Emissions from one engine were
93	measured while testing two different fuel types, and three engines were measured under two
94	emission control modes (enabled or disabled SCR) for a total of 25 engine tests.
95	During all tests, an Aerosol Black Carbon Detector (ABCD) <sup>25</sup> and SBA-5 (PP Systems)
96	were used to measure BC and CO <sub>2</sub> , respectively. Both analyzers are relatively low cost, report
97	concentrations at a frequency of 1 Hz, and are small and battery powered. These features made
98	them convenient to carry aboard and use in this application, especially when compared to a
99	traditional PEMS method that is more invasive and, therefore, more difficult to deploy on a large
100	number of vessels. A NO <sub>x</sub> analyzer meeting those requirements does not currently exist.
101	Therefore, NO <sub>x</sub> was measured on a subset of the vessels where plug-in power was available,
102	using a research-grade EcoPhysics CLD64. For this subset of 10 tests, research-grade CO <sub>2</sub> (LI-
103	7000, LI-COR) and BC (Aethalometer AE33, Magee Scientific) analyzers were used in addition
104	to the corresponding lower cost analyzers. Analyzer specifications are provided in Table S3.
105	Prior to sampling onboard, CO <sub>2</sub> and NO <sub>x</sub> analyzers were calibrated with certified zero
106	and span concentration gases, and the zero-response of BC analyzers was verified by sampling
107	with a particle filter on their inlets. Post sampling, concentration data was corrected for sampling
108	artifacts and instrumental errors, as described in the SI.
109	During sampling, a pole was used to extend gas and particle sample lines into the engine
110	exhaust for approximately 5–10 seconds per minute throughout the course of each ferry and

excursion vessel trip, as shown in Figure S1. When not extended into the exhaust plume, the sample lines were oriented so that clean ambient air was sampled. This plume capture method generates peaks in the concentration time series related to the pollutants emitted and fuel burned by the engine.

115 Pollutant concentration peaks that correspond to each short-duration plume sample were 116 integrated to calculate fuel-based BC and NO<sub>x</sub> emission factors using a carbon balance method 117 (Equation 1). The emission factor for pollutant P ( $EF_P$ ) has units of g of pollutant emitted per kg 118 of fuel burned and is calculated over the time interval  $t_1 \le t \le t_2$ , which corresponds to the onset 119 and end of the rise above baseline concentration of each pollutant. The numerator and 120 denominator represent the baseline-subtracted peak areas for pollutant P and CO<sub>2</sub>, respectively. 121 This ratio compares the relative abundances of pollutant P and CO<sub>2</sub> in the sampled exhaust plume when [P] and [CO<sub>2</sub>] have mass concentration units (e.g.,  $\mu g m^{-3}$ ). The factor of 44/12 122 converts CO<sub>2</sub> to carbon mass, the weight fraction of carbon in diesel fuel ( $w_c = 0.87$ ) converts 123 that ratio to a per mass of fuel burned basis, and the factor of  $10^3$  converts units from g to kg of 124 125 fuel. This method assumes that all fuel carbon is oxidized to CO<sub>2</sub> during combustion, such that 126 carbon monoxide and volatile organic compounds are comparatively negligible in the total carbon balance.<sup>24,26</sup> 127

128 
$$EF_P\left[g \ kg^{-1}\right] = \frac{\int_{t_1}^{t_2} ([P]_t - [P]_{t_1})}{\int_{t_1}^{t_2} ([co_2]_t - [co_2]_{t_1})} \cdot \frac{44}{12} \cdot w_c \cdot 10^3 \tag{1}$$

The vessels in this study fell within two main types of travel routes, short-haul and longhaul (noted in Table S2). Excursion vessels tended to operate at slower speeds as they traveled short-haul routes in a loop between tourist attractions (e.g., SF to the Golden Gate Bridge and Alcatraz Island). Commuter ferries included shorter routes between Oakland and SF and longer routes between SF and Vallejo, with some vessels specifically noted as high-speed ferries.

134 Pollutant emission factors were averaged within four different engine operating modes: docked, 135 maneuvering, slow cruising, and fast cruising. When docked, engines were either idling or 136 pushing the vessel against the dock to allow passengers to board and disembark. Maneuvering 137 operation occurred when the vessel was entering or exiting the harbor or moving around tourist 138 attractions. These activities were recorded in an experimental log during each trip. Cruising 139 encompasses all other times when the vessel was moving at a steady speed between destinations; 140 slow cruising occurred while traveling along corridors, in harbors, or between tourist 141 destinations, and fast cruising occurred on long stretches between destination points. The 142 distinction between slow and fast cruising for all vessels was based on field notes and vessel speed, with slow cruising defined as 12.4-31.0 km h<sup>-1</sup> and fast cruising as >31.0 km h<sup>-1</sup> (see 143 144 Figure 1 and SI for additional details). Vessel speeds were measured at 0.2 Hz using a GPS 145 logger (GlobalSat DG-500).



Figure 1. (a) Map of San Francisco Bay overlaid with points depicting locations of on-board
exhaust plume measurement locations and (b) distribution of vessel speeds during all exhaust
plume measurements (n = 1438) categorized by engine operating mode (docked, maneuvering, or
cruising). Cutoffs for slow and fast cruising are shown as the solid and dashed lines, respectively.

152 Using Equation 2, individual emission factors characterized by operating mode were 153 averaged and then weighted based on the amount of fuel consumed in each mode over the course 154 of a trip to compute a single mode-weighted pollutant emission factor (EF<sub>wtd</sub>) for each vessel. 155 Fuel consumption rates for each operating mode were assumed based on engine data 156 concurrently collected by other teams from three representative vessels: (i) a short-haul (SH), 157 Tier 2 excursion vessel; (ii) a long-haul (LH), Tier 3 commuter ferry; and (iii) a long-haul, high-158 speed (LH/HS), Tier 4 commuter ferry. See Table S4 in the SI for additional details and data 159 sources. The engine data showed that most of the fuel is consumed in the cruising mode, so those 160 mode-average emission factors were weighted more heavily. For short-haul excursion tours and 161 ferry commutes, slow and fast cruising (SC + FC) together accounted for 90% of fuel 162 consumption during a trip and all other modes (docked and maneuvering, D + M) combined were 163 weighted by 10%. Long-haul ferry commutes follow a different fuel consumption pattern that is 164 dominated by fast cruise operation under high engine loads (Table S4), so slow cruise emission 165 factors were combined with those measured during docked and maneuvering operation for these 166 vessels. Fast cruising (FC) values were weighted by 90% for the long-haul ferries and by 96% 167 for designated high-speed, long-haul ferries, while docked, maneuvering, and slow cruising 168 modes (D + M + SC) were together weighted by the remaining 10% and 4%, respectively.

169 
$$EF_{wtd} = \begin{cases} 0.90(\overline{EF}_{SC + FC}) + 0.10(\overline{EF}_{D + M}), SH \\ 0.90(\overline{EF}_{FC}) + 0.10(\overline{EF}_{D + M + SC}), LH \\ 0.96(\overline{EF}_{FC}) + 0.04(\overline{EF}_{D + M + SC}), LH/HS \end{cases}$$
(2)

170	Another objective of this study was to evaluate the performance of SCR systems that
171	have been installed as retrofits on Tier 3 engines or as original equipment on Tier 4 engines. In
172	this study, the SCR system on a subset of Tier 3 engines was manually disabled such that the
173	impact of SCR operation on NOx and BC emission factors could be directly evaluated (Table
174	S2). The other engines equipped with SCR systems were sampled under their normal operation,
175	without any intervention. None of the vessels in this study were equipped with diesel particle
176	filters.

### 178 **Results and Discussion**

179 Between January and November 2019, 1438 BC and 589 NO<sub>x</sub> emission factors were 180 measured during the 25 tests of 21 engines on 14 vessels in the SF Bay. Approximately 65% of 181 these plume capture events were during slow and fast cruising, 25% during maneuvering, and 182 10% while docked. Details of this sampling, including route type, engine tier, fuel type, SCR 183 activity, orientation of engine exhaust, and auxiliary engine operation, are specified in Table S2. 184 The present study focuses on emissions differences due to engine tier, operation mode, and SCR 185 activity, as urea dosing depends on engine operation. For the results below, engine tests are 186 categorized as Inactive when there is evidence that urea was not dosing for a majority of the 187 vessel trip or when SCR systems were manually disabled. All other SCR engine tests are noted 188 as Active. Other factors such as fuel type showed comparatively minimal impact on the emission 189 trends. Emission factors reported below are average values  $\pm$  95% confidence intervals, unless 190 otherwise noted.

191

192 In-Use Emissions Trends

193 Mode-weighted and mode-specific average BC and NO<sub>x</sub> emission factors measured on 194 vessels with Tier 0-4 engines are shown in Figure 2 and reported in Tables S5 and S6. Across 195 the mode-weighted averages determined for each of the 25 engine tests in the present study, the mean BC emission factor for the sampled vessel fleet is  $0.34 \pm 0.03$  g kg<sup>-1</sup>. This result is similar 196 197 to average BC emission factors reported for passenger vessel fleets measured in Texas (0.36 g kg<sup>-1</sup>) and California (0.30 g kg<sup>-1</sup>) in 2006 and 2010, repsectively.<sup>15,18</sup> BC emission factors were 198 199 highest during maneuvering  $(0.44 \pm 0.31 \text{ g kg}^{-1})$  and lowest during fast cruising  $(0.27 \pm 0.02 \text{ g})$ 200 kg<sup>-1</sup>). Docked and maneuvering BC emissions were more variable than during cruising. It is 201 important to note that much of the docked mode variability is driven by a single test with only 202 two plume capture events (engine test 9, equal to  $1.09 \pm 9.63$  g kg<sup>-1</sup>). 203 NO<sub>x</sub> emissions were measured on a subset of engines (tests 7, 17–25): Tier 2 without 204 SCR, Tier 3 with retrofit SCR, and Tier 4 that were originally equipped with SCR. The average 205 NO<sub>x</sub> emission factor of this subset—not including the Tier 0 and non-SCR Tier 3 engines sampled in this study—was  $24.1 \pm 1.4$  g kg<sup>-1</sup>. Average NO<sub>x</sub> emission rates were highest when 206 docked (59.9  $\pm$  8.4 g kg<sup>-1</sup>) and lowest and least variable during fast cruising (19.2  $\pm$  1.2 g kg<sup>-1</sup>), 207 208 as shown in Figure 2b. Further, NO<sub>x</sub> emission factors during slow and fast cruising were lower 209 than when docked and maneuvering. As discussed in further detail below, this difference is most 210 likely attributable to SCR operation, as it is expected that engine exhaust temperatures exceed 211 the minimum requirement for SCR system urea dosing with the high engine load and power conditions typical of cruising operation.<sup>27</sup> 212 213



Figure 2. Distributions of average mode-weighted and mode-specific (a) BC and (b) NO<sub>x</sub> emission factors from the sampled engine tests. Mean values are shown as a closed circle and the number of engine test averages included in each distribution is listed. PCTL refers to percentile.

210

219 Average BC and NO<sub>x</sub> emission factors by engine tier are shown in Figure 3 and reported 220 in Tables S5 and S6. The trend in BC emission rates followed the increasingly more stringent 221 exhaust standards set by the EPA for each engine tier, which were highest for Tier 0 engines 222 (engine tests 1-2) and progressively lower for each subsequent tier (Table S1, Figure 3a). On 223 average, Tier 4 engines (engine tests 24-25) emitted 92% less BC per kg of fuel than Tier 0 224 engines. BC emission factors from SCR-equipped Tier 3 engines were 29% lower when the SCR 225 system was active (engine test 23) rather than inactive (engine tests 17–22). Relative to Tier 3 226 engines without SCR (engine tests 14–15), BC emissions from those with SCR retrofits were

31% lower with inactive SCR and 51% lower with active SCR. Thus, presence of SCR appears
to offer a co-benefit of reducing BC emissions in addition to the primary intention of reducing
NO<sub>x</sub> emissions.

230 Unlike the BC trend, NO<sub>x</sub> emission factors did not decrease with engine tier and 231 increasingly stringent EPA emission standards (Figure 3b). Rather, the main feature that stands 232 out is the marked reduction in NO<sub>x</sub> emissions with active SCR. This effect is most pronounced 233 for the active SCR system on the Tier 3 engine, which reduced NO<sub>x</sub> emissions by 83% compared 234 to Tier 3 engines with inactive SCR; this is similar to the 95% reduction seen on an SCRretrofitted Tier 2 tugboat previously studied.<sup>20</sup> SCR systems on the Tier 4 engines were much 235 236 less effective, reducing NO<sub>x</sub> emissions by only 52% relative to the inactive SCR on Tier 3 237 engines. Though these differences in SCR performance warrants further study, they may be 238 related to engine tuning. Similar to how heavy-duty diesel truck engines with diesel particle 239 filters and SCR are tuned, Tier 4 engines with original SCR systems may be tuned for higher engine-out NO<sub>x</sub> and lower engine-out PM compared to Tier 3 engines.<sup>6</sup> In use, however, SCR is 240 241 less effective under low engine load conditions like docked or maneuvering modes, when engine 242 exhaust temperatures likely fall below the minimum temperature required for urea injection (Figure S4).<sup>21</sup> 243

244



Figure 3. Average (a) BC and (b) NO<sub>x</sub> emission factors for each sampled engine tier. The
number (n) of engine tests included each average is noted. The error bars represent the 95%
confidence intervals about the mean value.

250

### 251 SCR Effectiveness

The NO<sub>x</sub> reduction performance of Tier 3 engines retrofitted with SCR was explicitly evaluated using two different approaches. First, emissions were measured during a vessel trip when the SCR system was manually disabled and then again with the same SCR system enabled, while all other factors like route and operating modes remained the same. Second, SCR data was provided by the vessel operator and used to evaluate SCR operation relative to measured NO<sub>x</sub>
emission factors.

258 Figure 4 shows the NO<sub>x</sub> emission factor distributions for two engine tests during the 259 docked, maneuvering, and cruising (combined slow and fast) operating modes with the SCR 260 system enabled (engine test 23) and intentionally disabled (engine test 22). On average, tailpipe 261 exhaust NO<sub>x</sub> emission factors were  $\sim$ 70% lower in the docked and maneuvering modes and 262 ~90% lower while cruising when the SCR system was enabled. However, the SCR performance 263 was not uniformly effective throughout the docked and maneuvering modes, as indicated by the 264 skewed emission factor distribution: mean values were much greater than median values, and 265 90<sup>th</sup> percentile NO<sub>x</sub> emission rates were comparable to those measured when SCR was 266 intentionally disabled. Periods of elevated NO<sub>x</sub> emissions that caused this skewness likely 267 occurred during intermittent high engine load operation to push the vessel steady against the 268 dock, leading to high engine-out NO<sub>x</sub> that was not scrubbed in the SCR because engine exhaust 269 temperatures fell below the temperature required for urea injection.



Figure 4. Distributions of operating-mode-specific tailpipe exhaust NO<sub>x</sub> emission factors
measured on a ferry with a Tier 3 engine, where the retrofit SCR system was enabled (left panel,
engine test 23) and intentionally disabled (right panel, engine test 22). The number of emission
factors included is noted above each distribution. The cruising distribution includes both slow
and fast cruising emission factors.

277

278 Figure 5 shows the SCR data from engine test 17 and the corresponding NO<sub>x</sub> emission 279 factors. As shown in Figure 5a, urea injection was intermittent for a majority of this route, but there were no reported SCR system errors. NO<sub>x</sub> emission rates decreased to <10 g kg<sup>-1</sup> following 280 urea injection and increased to  $\sim 40-70$  g kg<sup>-1</sup> minutes after urea injection stopped. As further 281 282 illustrated in the map of this vessel's roundtrip route between Oakland and SF (Figure 5b), the 283 lowest NO<sub>x</sub> emission factors were measured when the ferry was cruising at high speeds across 284 the SF Bay, while elevated NO<sub>x</sub> emissions occurred when the ferry was docked, maneuvering, 285 and slow cruising between docks in the Oakland Inner Harbor. An analogous pattern in NOx emissions was observed for the newest ferry measured in this study that featured a Tier 4 engine 286 287 originally equipped with an SCR system (Figure S5). Though data on the urea injection rate was 288 not available for this ferry, the operator confirmed that there were no SCR system errors. It 289 stands to reason that the elevated  $NO_x$  emissions occurred when the system stopped injecting

urea into the catalyst because exhaust temperatures dipped below the minimum threshold during
docked, maneuvering, and slow cruise operation, as was previously described from
measurements on-board a New York-based ferry equipped with SCR.<sup>21</sup> These results highlight
the importance of engine operation and vessel route on SCR effectiveness for NO<sub>x</sub> reduction.



Figure 5. (a) Time series of simultaneously measured urea injection rate (black line) and tailpipe exhaust NO<sub>x</sub> emission factors (circles) measured on a ferry with a Tier 3 engine with enabled SCR system (engine test 17). NO<sub>x</sub> emission factors are reported on the secondary vertical axis and are also indicated by the color scale. Vertical lines and labels indicate the ferry's progress over the roundtrip between SF and Oakland. (b) Corresponding map of measured NO<sub>x</sub> emission factors, which were greater during docked, maneuvering, and slow cruise operation compared to the fast cruising in the middle of the SF Bay. Docks are labeled and shown as black squares.

### 303 Comparison to EPA Emission Standards

304 The emission factors measured in this study are compared to EPA exhaust emission 305 standards, which all engines are required to meet during laboratory certification testing. For this 306 comparison, measured operating-mode-weighted average BC and NO<sub>x</sub> emission factors for each 307 engine test were converted from fuel- to power-based units using typical values for brake 308 specific fuel consumption (BSFC), as described in the SI and reported in Table S7. Figure 6 309 shows the ratios of these converted average BC and NO<sub>x</sub> emission factors and the corresponding 310 EPA PM and  $NO_x$  emission standards. It should be noted that BC is a major but not sole 311 component of diesel PM, such that real-world PM emission rates may be larger than the reported 312 BC emission rates. 313 In this study, measured BC emission rates were less than the corresponding PM emission 314 standards by 10-70% for all but one engine (Figure 6a). The in-use NO<sub>x</sub> emission rates exceeded 315 corresponding exhaust standards for most Tier 3 engines sampled, and Tier 4 engines were ~1.9 316 times the emission standard (Figure 6b). Note that the SCR system was intentionally disabled 317 during engine tests 18 and 20–22, however, these engines are held to a Tier 3 standard that is 318 independent of SCR retrofit. Though the in-use measurements presented here did not follow 319 procedures to verify compliance with EPA standards, this work highlights that these standards 320 should not be the default assumption in emission inventories.



Figure 6. Ratios of mode-weighted average (a) BC and (b) NO<sub>x</sub> emission factors measured for each engine test and their corresponding EPA PM and NO<sub>x</sub> emission standards, respectively. The error bars represent uncertainty in actual BSFC due to engine operation variability, showing the range of ratios if the minimum and maximum values from Table S4 were used instead of the average. Tier 0 engines are not EPA certified, so the emission factors for engine tests 1–2 are not compared to a PM emission standard.

### 330 Commuter Emissions Footprint

331 To put these results into meaningful context, we consider the pollution and carbon 332 footprints of commuting by ferry versus passenger vehicle. As an example, we compare the NO<sub>x</sub>, 333 BC, and CO<sub>2</sub>-equivalent (CO<sub>2</sub>-eq) emissions from modern light-duty, gasoline-fueled vehicles 334 and diesel-fueled ferries with engines ranging Tier 0-4, including Tier 3 engines with inactive 335 and active SCR retrofits. The following inputs and assumptions are used in this analysis. 336 BC and NO<sub>x</sub> emission rates for commuting by passenger car were assumed to be 0.02 g BC kg<sup>-1</sup> and 2.29 g NO<sub>x</sub> kg<sup>-1</sup>, based on light-duty vehicle fleet average values measured in the SF 337 Bay Area.<sup>26</sup> BC and NO<sub>x</sub> emission rates for each ferry engine type are reported in Tables S5 and 338 339 S6, and emissions from both main engines on the ferries are assumed equal and summed. Ferry 340 and light-duty car occupancies are assumed to be 200 and 1.18 passengers, respectively. The 341 former represents 50% capacity for the observed ferries and the latter is the national average

occupancy for a work commute.<sup>28</sup> The ferry fuel economy (0.2 km L<sup>-1</sup>) was derived from engine 342 data collected from the two long-haul ferries, as described above and detailed in Table S4. The 343 2020 national average fuel economy for passenger vehicles, 10.6 km L<sup>-1</sup>, was used.<sup>29</sup> Conversion 344 345 of BC and NO<sub>x</sub> to  $CO_2$ -equivalents ( $CO_2$ -eq) is based on 20-year global warming potential (GWP) values of 3200 and -2.4, respectively.<sup>30,31</sup> Results for GWP values on a 100-year time 346 347 horizon are reported in the SI. 348 Following these assumptions, emission rates of NO<sub>x</sub>, BC, and CO<sub>2</sub>-eq on a per passenger-349 km basis were calculated for each commute option, as summarized in Table S8 and shown in 350 Figure 7 as emission ratios for each ferry engine type relative to light-duty vehicles. Across all 351 engine tiers, ferries emit 1.6–9.4 and 2.0–27.1 times more NO<sub>x</sub> and BC per passenger-km, 352 respectively, than light-duty vehicles. Conversely, the net CO<sub>2</sub>-eq (20-year) emissions per 353 passenger-km is 1.0–1.3 times higher for the typical passenger vehicle than ferries. For both the

354 passenger vehicle and ferries, the carbon footprint of each commute mode is overwhelmingly

dominated by CO<sub>2</sub> emissions. The data reported in this study can be adapted to consider other

356 scenarios, for example, with different route distances or vehicle and ferry occupancy.



357

Figure 7. Ratio of ferry to light-duty vehicle  $NO_x$ , BC, and  $CO_2$ -eq (20-year GWP) emissions per passenger-km. Here, ratios greater than 1 indicate that commuting by ferry results in more pollution or carbon emissions than a commute by passenger car, and vice versa for ratios less than 1. A very small, negative contribution of  $NO_x$  emissions is not included in the reported  $CO_2$ eq emissions value for Tier 0 and 3 vessels, as there were no on-board  $NO_x$  measurements for these engines.

365

366 As shown in this study, BC emission rates—a proxy for toxic, carcinogenic diesel PM— 367 from ferries are lowest for Tier 4 engines. Thus, the disparity in BC emissions will decrease 368 overtime as ferry fleets modernize. However, these results also indicate that NO<sub>x</sub> emissions 369 reductions from SCR systems may not be fully achieved due to frequent operation at low engine 370 loads. This finding warrants further study to understand if it is generally true of a larger number 371 of vessels. The results of the commuter analysis highlight the dependence on ridership levels: 372 increasing ferry occupancy will help reduce the per-passenger air pollution and carbon footprints 373 in comparison to light-duty vehicles. Whereas this analysis is illustrative, a health impacts 374 assessment would further consider the proximity of emissions to population centers, as it is vital 375 to consider where the pollution is occurring with respect to where people reside and breathe.

377	Supporting Information		
378	Detailed description of materials and methods, BC and NO <sub>x</sub> emission rates categorized by engin		
379	tier an	d engine test, and supporting figures and tables (Figures S1–S5 and Tables S1–S8)	
380			
381	Ackn	owledgements & Dedication	
382	This p	aper is dedicated to our colleague and friend, Professor George Ban-Weiss, who left us too	
383	soon.		
384			
385	The p	roject was supported by the California Air Resource Board (CARB) under contract number	
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