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#### AN ELECTROMAGNETIC (EM-60) SURVEY IN THE PANTHER CANYON AREA GRASS VALLEY, NEVADA

M. Wilt, N. Goldstein, M. Stark, and R. Haught

### Abstract

Eight frequency domain electromagnetic soundings were measured over the Panther Canyon thermal anomaly in Grass Valley, Nevada. The data were collected with Lawrence Berkeley Laboratory's large moment-horizontal loop system (EM-60). At the transmitter site located near the center of the thermal anomaly, square wave currents of up to 70 A were impressed into a fourturn 50 m radius coil at frequencies from 0.033 to 500 Hz. At the eight receiver sites, 0.5 to 1.5 km from the loop, magnetic fields were detected with a three-component SQUID magnetometer and vertical and radial magnetic field spectra were calculated. Data were interpreted with a computer program which fit filled spectra and associated ellipse polarization data to onedimensional resistivity models and results were compared to interpretations from earlier dipole-dipole resistivity measurements. Comparison of these interpretations indicates fairly close agreement between the two, with both models clearly indicating the presence and dimensions of the conductivity anomaly associated with the thermal zone. Although the dc data was better able to resolve the high resistivity bedrock, the EM-data were able to resolve all major features without distortion at shorter transmitter receiver separations and in about one-third of the field time.

#### Introduction

As part of the Department of Energy, Division of Geothermal Energy's (DOE/DGE) Industry-Coupled Program to stimulate geothermal resource development, Lawrence Berkeley Laboratory has conducted a series of electromagnetic (EM-60) sounding surveys over several promising geothermal sites in Nevada.

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This report describes the results of a controlled-source EM survey in the Panther Canyon region of Grass Valley, Nevada (Figure 1). The soundings were performed with the EM-60 horizontal loop, frequency-domain electromagnetic system (Morrison et al., 1978). We performed eight frequency domain electromagnetic soundings within a 12 km<sup>2</sup> region surrounding a single four-turn, 50-m-radius horizontal loop. For each sounding, a layered model interpretation was made, and the layered interpretations were combined into resistivity



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Figure 1. Survey location map of Panther Canyon area, Grass Valley, Nevada.

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sections. These interpretations are compared to other geophysical data for confirmation and as a way of evaluating the EM method.

#### Geology

Grass Valley is an elongate northerly-trending Basin and Range valley located in north-central Nevada. The region is characterized by higher-thannormal heat flow (Sass et al., 1971), active hot springs (Olmsted et al., 1975) and recent faulting (Noble, 1975; Majer, 1978). Grass Valley has been an area of active geothermal exploration for about the past eight years, but to date no major discovery has been made.

Surface geologic studies consisting of regional photogeology (Noble, 1975) and detailed field mapping (Olmsted et al., 1975; Silberling, 1975; Noble, 1975; and Nichols, 1972) were done partly in conjunction with geothermal studies (Beyer et al., 1976). A bedrock geologic map of the Leach Hot Springs quadrangle is given in Figure 2. This map is a composite from the sources cited and includes the area of the present survey.

The Panther Canyon area is located in the southwestern portion of Grass Valley near the intersection of the Tobin and Sonoma Ranges. Exposed rocks in these ranges consist mainly of the Paleozoic Havallah sequence of cherts, argillites and sandstones. Also present in the mountains are Tertiary Kiapoto formation rhyolite and trachitic tuffs and Triassic cherts, dolomites, and conglomerates of the Panther Canyon Formation. Figures 3 and 4 are idealized geologic cross sections along the orthogonal EM-60 survey lines. These composite profiles correspond to the lines shown in Figure 1.

#### Geophysics

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Reconnaissance and detailed geophysical investigations have been performed throughout Grass Valley and several detailed studies were done in the Panther Canyon area. Work has included dipole-dipole resistivity and telluric profiles (Beyer, 1977), magnetotelluric soundings (Morrison et al., 1979), passive seismics (Majer, 1978), gravity (Goldstein and Paulsson, 1978) and heat flow (Sass et al., 1977). Composite profiles and syntheses of these and other data are given in Beyer (1977) and Morrison et al. (1978).

Geothermal interest in the Panther Canyon area was heightened after several shallow boreholes indicated anomalously high heat flow values of 7 heat flow units (HFU), about three times the regional average. Subsequent telluric and



Figure 2. Bedrock geologic map of the Leach Hot Springs Quadrangle, Grass Valley Nevada (after Sass et al., 1977).

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Figure 4. Idealized geologic cross section for survey line T-T' (after Sass et al., XBL 763-622 A 1977). Markings (Q3) denote heat flow boreholes.

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resistivity studies over the heat flow anomaly revealed a low resistivity zone, thus suggesting the presence of geothermal waters at depth.

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## Field Survey and the device that the shafe be appreciated to exercise out

The EM-60 field survey in Panther Canyon consisted of eight soundings arranged in two orthogonal profiles about a central four-turn, 50-radius horizontal loop. Transmitter-receiver separations varied from 400 m to 1.6 km, and data at each site were recorded over at least two frequency decades within the frequency band 0.033-500 Hz Since the depth of penetration for EM induction sounding is proportional to both the transmitter-receiver separation and the period of the transmitted wave, it was desirable to occupy receiven sites at different separations with respect to one loop. This permitted a more complete resistivity depth section and a better knowledge of surface inhomogeneities. At Panther Canyon four of the soundings were placed about 500 m from the loop source for shallow information, and four other sites were occupied at about 1.5 km for better resolution of deeper horizons. A crew of four completed the entire survey in six field days, including laying out and retrieving the transmitter coil and one day of system testing and debugging. The maximum production rate achieved was three soundings in a 12 hr work day. Recording times varied from about four hr per station at the more distant sites to one at the closer stations. Radial and vertical magnetic fields were measured at each station by means of a three-component SQUID magnetometer (Appendix A). The survey was performed under ideal weather conditions, and there was good vehicular access to stations.

#### Results and the second s

Data for the eight EM-60 soundings are given in Appendix B. Each sounding is presented in terms of normalized amplitudes and phases of the observed magnetic fields, as well as the polarization ellipse parameters of the fields: namely, ellipticity and tilt angle. The observed fields are normalized by the free-space primary field so that the secondary fields, due to the presence of the earth can be better visualized. The phases are given with respect to the phase of the current impressed into the loop. The ellipticity parameter is the ratio of the minor to major axis of the polarization ellipse traced out by the observed field; the sign of the

ellipticity refers to the direction in which the ellipse is traced, a negative sign denotes anticlockwise rotation. The tilt angle parameter refers to the inclination from the vertical of the polarization ellipse. The polarization ellipse parameters are calculated from relative phases between the observed fields, and thus these measurements may be made without an absolute phase reference to the loop current.

Data listed in Appendix B indicate that accurate amplitude-phase data were obtained at Panther Canyon up to about 100 Hz, whereas good polarization ellipse data could sometimes be obtained to 500 Hz. The declining strength of the primary and secondary fields with frequency and the increasing noise in the reference wire cause amplitude-phase data to be particularly noisy above 100 Hz. Because polarization ellipse data can be taken without a reference wire, this information is often more reliable at the higher frequencies. The errors shown in Appendix B refer to one standard deviation of the observed data. These are accurate representations of the true error if the sources of noise are random. Unfortunately, most noise sources observed are not random, especially above 30 Hz, so the noise estimate given in Appendix B is probably somewhat low at higher frequencies where nonrandom noise sources are greatest.

#### Data Interpretation

All EM soundings were interpreted individually using a layered-earth least-squares inversion program (Inman, 1975). The program finds a layered model whose EM response fits the weighted observed data. It also estimates parameter resolution and data point-parameter sensitivity. Layered model fits, model parameters, and estimated resolutions of the parameters are given in Appendix C. As it is difficult to estimate the true errors, and because, for some soundings, a one-dimensional model may not be appropriate, the errors for parameters resolution in Appendix C may be somewhat low.

Points with high errors and points that do not fall on a layered model curve were deleted from the inversions. Such data often were vertical magnetic field components because the vertical component is sensitive to, and will be distorted by, lateral inhomogeneities (Ward, 1976; Wilt et al., 1979).

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### Discussion

Figures 5 and 6 are resistivity cross sections along orthogonal lines over the Panther Canyon thermal anomaly. Each figure gives a comparison between dipole-dipole resistivity and EM-60 Electromagnetic interpretations. The resistivity data and the 2-D interpretation are from Beyer (1977). An example of observed dipole-dipole data, the two-dimensional and the fit of calculated-to-observed data, is given in Figure 7. The EM-60 cross sections are made from one dimensional interpretations given in Appendix C.

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Along the north-south line (Figure 5), the EM and dipole-dipole interpretations are remarkably similar. Both cross sections indicate resistive surface material overlying an irregular southward-dipping conductive body. Depth to resistive basement (which may be the Havallah formation) is shown to vary between 250 and 800 m below the surface. The depth to, and lateral extent of, the conductive body, which may be associated with the thermal anomaly, is well resolved by both methods. The two profiles disagree somewhat on the depth to resistive basement beneath the conductor. Because the EM method is less sensitive to resistive formations, and because the transmitter-receiver separations were more than five times greater with the dipole-dipole data, the conventional resistivity section is probably more accurate in determining this parameter.

Figure 6 shows results for an east-west line over the central portion of the thermal anomaly. For this cross section, the EM and dc resistivity interpretations disagree somewhat. Both cross sections indicate the presence of an irregularly shaped conductive body near the central portion of the thermal anomaly. The EM data place the thickest portion slightly west of the thermal maximum, whereas the dc data place it directly beneath the maximum. The dc resistivity data indicate that basement dips steeply westward from 250 to about 800 m adjacent to the edge of the Tobin Range; the EM induction data show a similar behavior, but with fewer points and larger uncertainty.

Although the interpreted sections in both cases are similar, the EM results show a smoother variation, a consequence of one-dimensional interpretation. However, there are other differences between the EM and dc resistivity surveys that are not apparent in the data and interpretations. The dipole-dipole sections required a crew of four working for about 20 field days; whereas the same size crew collected the EM data in six field days.







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Figure 6. Resistivity cross section over line H-H' in Panther Canyon: (a) two-dimensional dipole-dipole resistivity model; (b) profile of one-dimensional EM-60 electromagnetic soundings; (c) comparison of parts (a) and (b).



Figure 7. Dipole-dipole apparent resistivity pseudosection for 1 km dipoles along line H-H': field data, model generated data,

and two-dimensional model.

The dc resistivity data cover an area about 50% larger, but far more labor was required to achieve coverage comparable to that of the EM survey. Interpretation of dipole-dipole data is presently better able to handle complex geology, and the data is better able to resolve resistive bedrock. However, deep EM interpretations required much shorter transmitter-receiver separations, thus reducing the effects of lateral inhomogeneities on interpretations. The two cross sections suggest that, even in regions of two, and three-dimensional geology, EM data will adequately resolve major features without severe distortion.

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#### References

- Beyer, J. H., Dey, A., Liaw, A., Majer, E., McEvilly, T. V., Morrison, H. F., and Wollenberg, H. A., 1976. Preliminary Open File Report. Geological and geophysical studies in Grass Valley, Nevada. Lawrence Berkeley Laboratory, LBL-5262.
- Beyer, J. H., 1977. Telluric and d.c. resistivity techniques applied to the geophysical investigation of basin and range geothermal systems, Part III: The analysis of data from Grass Valley, Nevada. Lawrence Berkeley Laboratory, LBL-6325, March 3, 115 p.
- Goldstein, N. E., and Paulsson, B., 1977. Interpretation of gravity surveys in Grass and Buena Vista Valleys, Nevada. Lawrence Berkeley Laboratory, LBL-7013.
- Inman, J. R., 1975. Resistivity inversion with Ridge regression. Geophysics, 40, pp. 798-817.
- Majer, E., 1978. Seismological investigations in geothermal areas. Ph. D. dissertation, Department of Geology and Geophysics, University of California Berkeley, LBL-7054.
- Morrison, H. F., Goldstein, N. E. Hoversten, N., Opplinger, G., and Riveros,
   C., 1978. Description, field test and data analysis of controlled-source
   EM system EM-60, Lawrence Berkeley Laboratory, LBL-7088.

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Nichols, K. M., 1972. Triassic depositional history of China Mountain and vicinity, north-central Nevada. Ph. D. dissertation, Stanford University.

- Noble, D. C., 1975. Geologic history and geothermal potential of the Leach Hot Springs area, Pershing County, Nevada. Preliminary report to Lawrence Berkeley Laboratory.
- Olmsted, F. H., Glancy, P. A., Harrill, J. R., Rush, F. E., Van Denburgh, A. S., 1975. Preliminary hydrologic appraisal of selected hydrothermal
- systems in northern and central Nevada. USGS Open File Report 75-56. Sass, J. H., Siagos, J. P. Wollenberg, H. A., Munroe, R. J., DiSomma, D., and Lachenbruch, A. H., 1977. Application of heat flow techniques to geothermal energy exploration. Leach Hot Springs, Grass Valley, Nevada. Lawrence Berkeley Laboratory, LBL-6809, USGS Open File Report (in preparation).
- Sass, J. H., Lachenbruch, A. H., Munroe, R. G., Greene, G. W., and Moses, T. H., Jr., 1971. Heat flow in the western United States. J. Geophys. Res. 76, 6376.
- Silberling, N. J., 1975. Age relationships of the Golconda thrust fault, Sonoma Range, north-central Nevada. Geol. Soc. America, Special Paper 163.
- Ward, S. H., 1967. Mining geophysics, vol. 2, Society of Exploration Geophysicists, Tulsa, Oklahoma,
- Wilt, M., Goldstein, N. E., Hoversten, M. and Morrison, H. F., 1979. Controlled-source EM experiment at Mt. Hood, Oregon, Lawrence Berkeley Laboratory, LBL-9399.

#### APPENDIX A

#### EM-60 Electromagnetic System

In 1976 the Lawrence Berkeley Laboratory (LBL), in conjunction with the University of California at Berkeley, made preliminary measurements with a prototype large-moment, horizontal-loop electromagnetic prospecting system (Jain, 1978) in a geothermal area in Nevada. Encouraging results from this work led to the development of the EM-60 horizontal-loop system (Morrison et al., 1978) which has now been operated for more than 500 hr at various geothermal sites in Nevada and Oregon.

The EM method may be a significant improvement over existing techniques, i.e., dc resistivity and magnetotellurics in geothermal exploration, for three reasons:

1. The maximum depth of exploration with EM is approximately equal to the distance between the transmitter and receiver; this compares to almost five times the source receiver separation for dc resistivity.

2. The EM method is faster and less expensive than the dc resistivity or Magnetotelluric method (MT).

3. Distant lateral inhomogeneities, which often affect MT data, have relatively minor significance for EM because the strength of the fields strongly decreases with increasing distance from the transmitter.

#### System Description

The system, as shown schematically in Figure A-1 consists of two sections:

(a) a transmitter section consisting of the power source, control electronics, timing, and a transistorized switch capable of handling large current: and
(b) a receiver section consisting of magnetic, or a combination of magnetic and electric, field detectors, signal conditioning amplifiers. and antialias filters, and a multichannel programmable receiver (spectrum analyzer).

#### Transmitter System

The EM-60 transmitter is powered by a Hercules gasoline engine linked to an aircraft 60-kW 400-Hz, 3¢ alternator. These two components are mounted in the bed of a one-ton, four-wheel-drive truck. The output is full-wave rectified and capable of providing  $\pm 150$  V at up to 400 A to the horizontal



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coil. The square wave current pulses are created by means of a transistorized switch, which consists of two parallel arrays of from 6 to 60 transistors in interchangeable modules within the "crate" (the lower outward pivoting box in Figure A-2). The upper unit contains array-driving electronics and timing circuitry. The transmitter is operated by one man who controls the frequency of the primary magnetic field over the range of  $10^{-3}$  to  $10^{3}$  Hz by means of switches on a remote control box which contains a crystal-controlled oscillator and dividers (Morrison et al., 1978).

The dipole moment, which is a measure of the strength of the signal, is determined by the resistance and inductance of the loop. At frequencies below 50 Hz, inductive reactance is negligible and the dipole moment is governed by the load resistance. Four turns of No. 6 wire in a square or circular loop, 50 m in radius, will yield a dipole moment of about  $3 \times 10^6$  mks. This provides adequate signal for soundings where transmitter-receiver separations are less than about 5 km, which corresponds to a maximum depth of exploration of about 5 km. At frequencies above about 100 Hz, the inductance causes the moment to decrease and the current waveform to become quasisinusoidal. High frequency information is thus more difficult to obtain at large transmitter-receiver separations.

### Receiver Section

The fields are detected at a point up to 5 km distant from the transmitter by means of a three-component SQUID magnetometer oriented to measure the vertical, radial, and tangential components with respect to the loop. Signals are amplified, antialias filtered, and inputted to a six-channel, programmable, multifrequency phase-sensitive receiver (Figure 1). Through the receiver key-pad, the operator sets parameters controlling signal processing: (a) fundamental period of the waveform to be processed; (b) maximum number of harmonics to be analyzed, up to 15; (c) number of cycles in increments of  $2^{N}$ , to be stacked prior to Fourier decomposition; and (d) number of input channels of data to be processed. Signal processing results in a raw amplitude estimate for each component and a phase estimate relative to the phase of the current in the loop. Phase referencing is maintained with a hard-wire link between a shunt on the loop and the receiver. This reference voltage is applied directly to channel 1 of the receiver for phase comparison.



Figure A-2. The EM-60 transmitter in field operation.

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Raw amplitude estimates must be later corrected for dipole moment and distance between loop and magnetometer.

In practice, the hard-wire link was found to be a source of noise, particularly above 50 Hz. This has required the elimination of the absolute phase reference at high frequencies in favor of relative phase measurements between vertical and radial components. With relative phase measurements, interpretation is based on the ellipticity and tilt angle of the magnetic field rather than the amplitude-phase of the vertical and radial fields. At low frequencies ( $\leq 0.1$  Hz), natural geomagnetic signal amplitude increases roughly as 1/f while the signal sought decreases as 1/f. The net result is an effective signal-to-noise ratio that decreases as  $1/f^2$ , making noise cancellation imperative for recovery of low frequency information. To cancel geomagnetic noise, a reference magnetometer is placed far enough from the transmitter loop (10-12 km) so that the observed fields will consist only of the geomagnetic fluctuations. Once installed, the reference magnetometer can often remain fixed over the course of a survey. The remote signals are transmitted to the mobile receiver station from the transmitter via FM radio telemetry. Before the loop is energized, the remote signals are inverted, adjusted in amplitude, and then added to the base station geomagnetic signal to produce essentially a null signal. A good example of this simple noise cancellation scheme is shown in Figure A-3. The resulting signal-to-noise improvement of roughly 20 dB has allowed us to obtain reliable data to 0.05 Hz, a gain of three or four important data points on the sounding curve. These points are invaluable for resolving deeper horizons.

#### Data Interpretation

Basic data interpretation is accomplished by direct inversion of observed data to fit one-dimensional models. The program used fits amplitude-phase and/or ellipse polarization parameters jointly or separately, to fit arbitrarily layered models. This program allows the use of ellipse polarization parameters to separately fit high frequency points, where absolute phase data is much noisier, while simultaneously using absolute phase data at the lower frequencies, where the phase reference may allow for better parameter resolution. Two-dimensional modeling, although possible, is currently cumbersome and prohibitively expensive (Lee, 1979).



Figure A-3. Example of data improvement using the telluric noise cancellation scheme. (a) Natural geomagnetic signal and initial cancelling at the receiver site with transmitter off; (b) same system, but with transmitter on.

Samples of EM-60 amplitude-phase spectra soundings are given in Figures A-4 and A-5; the error bars signify one standard deviation. The fit to a three-layer model is fairly good, but data were interpreted only to 50 Hz, because high noise due to the use of the reference wire prohibited obtaining higher frequency amplitude-phase data. Ellipticity data, however, could be intepreted to 500 Hz.

### References

Jain, B., 1978. A low frequency electromagnetic prospecting system, Ph. D. dissertation, Department of Engineering Geosciences, University of California. Berkeley, Lawrence Berkeley Laboratory, LBL-7042.
Morrison, H. F., Goldstein, N. E., Hoversten, N., Oppliger, G., and Riveros, C., 1978. Description, field test and data analysis of a controlled-source EM system EM-60. Lawrence Berkeley Laboratory, LBL-7088.
Lee, K. H., 1978. Electromagnetic scattering by a two-dimensional inhomogeneity due to an oscillating magnetic dipole. Ph. D. dissertation, Department of Engineering Geosciences, University of California, Berkeley. Lawrence Berkeley Laboratory, LBL-8275.

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Figure A-4. Normalized magnetic field amplitude spectra normal and radial fields sounding T-T' Km 4 Panther Canyon.

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sounding T-T' Km 4 Panther Canyon.

## APPENDIX B

Observed data and estimated error for Panther Canyon prospect at Grass Valley, Nevada. Listed errors are one standard-deviation from the mean.

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tilt angle vs frequency

seperation=562 meters station: t-t .5km north loop radius=50 meters number of turns=4 hr mag const=7.936 hz mag const=7.092 hr phase 255.000 249.300 241.750 235.250 230.500 205.500 frequency hr amp amp err 0.001 phase err 0.009 0.590 0.250 0.250 1.000 0.106 0.292 3.000 0.001 0.446 0.571 0.794 5.000 0.002 0.002 7.000 10.000 0.002 0.500 1.237 30.000 0.001 0.500 198.500 0.500 50.000 1.409 0.003 175.500 109.090 0.855 0.001 0.508 164.500 0.500 150.000 8.649 0.001 hz phase 172.500 phase err hz amp amp err frequency 0.004 0.500 1.000 1.027 0.999 0.002 178.750 3.000 179.700 0.993 0.003 0.100 5.000 0.001 180.750 9.250 1.000 7.000 178.250 0.001 0.250 10.000 1.144 1.295 38.090 0.006 171.500 0.500 154.500 129.250 115.500 9.500 50.000 1.220 0.003 0.250 100.000 0.489 0.001 0.500 150.000 0.257 0.001 frequency tilt angle tilt err 89.217 0.060 ellipticity ellip err 1.000 -0.103 0.001 3.000 -0.274 0.002 84.038 0.203 76.091 0.001 0.270 8.236 7.000 -0.409 0.003 67.747 -0.443 10.000 0.003 60.673 0.049 46.598 30.000 0.000 0.183 39.310 24.774 50.000 0.000 0.020 100.000 -0.349 0.002 0.053 -0.278 150.000 0.001 15.814 0.059 -0.299 0.001 200.000 18.153 0.077



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XBL 806-9808



station: t-t .5km north separation=562 meters

XBL 806-9809

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XBL 806-9810



XBL 806-9807

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station: t-t .	5km south	seperation	=451 meters	
number of turn	s=4 loop	radius=50	meters	
hr mag const=7	.936 hz ma	ig const=7.1	892	
frequency	hr amp	amp err	hr phase	phase err
1.000	0.107	0.000	257.533	0.089
3.000	0.306	0.000	250.840	0.062
5.000	0.476	0.003	241.683	0.041
7.000	0.602	0.001	234.360	0.090
10.000	0.847	0.005	228.603	0.009
30.000	0.998	0.009	202.253	0.095
50.000	0.720	0.023	208.460	0.670
100.000	0.611	0.001	185.235	0.179
200.000	0.380	0.003	165.722	0.455
frequency 1.000 3.000 5.000 7.000 10.000 30.000 50.000 100.000 200.000	hz amp 1.014 1.003 1.009 1.002 1.125 1.326 0.662 0.358 0.258	CMp err 0.005 0.005 0.001 0.005 0.007 0.012 0.021 0.000 0.000 0.002	hz phase 171.163 177.817 179.360 180.973 180.320 180.806 168.437 143.378 125.720	phase err 0.027 0.009 0.021 0.027 0.610 0.682 0.156 0.461
frequency	211 ipticity	ellip err	tilt ang	le tilt er
1.000	-0.105	0.000	89.613	0.009
3.000	-0.289	0.001	84.441	0.040
5.000	-0.395	0.002	75.293	0.112
7.000	-0.415	0.000	65.885	0.132
10.000	-0.423	0.000	56.672	0.129
30.000	-0.181	0.000	53.617	0.044
50.000	-0.362	0.000	41.821	0.002
100.000	-0.321	0.000	26.516	0.031
200.000	-0.315	0.000	27.723	0.967
500.000	-0.231	0.000	19.822	0.057



Hr and Hz amplitude Hr=x Hz=o

station: t-t .5km south separation=451 meters

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XBL 806-9820



Hr and Hz phase Altrax Hz=0.

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XBL 806-9819





station: t-t .5km south separation=451 meters

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XBL 806-9822

지하는 것은 관람이다.



XBL 806-9821

nur hr	iber of tu nag const	-1.5km south rns=4 loop =7.936 hz m	seperation radius=50 n ig const=7.(	n=1951 Mete Neters 192	rs
	requency 0.033 0.100 0.500 0.500 0.500 1.000 3.000 5.000 7.000 10.000 30.000 50.000	hr amp 0.033 0.040 0.107 0.178 0.177 0.238 0.335 0.797 0.983 1.015 1.097 0.795 0.695	amp err 0.017 0.004 0.005 0.008 0.005 0.005 0.001 0.002 0.004 0.004 0.001 0.003 0.003 0.007	hr phase 210.667 274.467 264.433 261.300 257.400 257.400 250.575 219.470 196.633 181.133 167.856 135.219 110.279	phase err 31.756 13.593 0.296 0.907 0.550 0.306 0.229 0.058 0.120 0.441 0.034 0.291 0.649
	requency 0.033 0.100 0.300 0.500 0.500 0.700 1.000 3.000 7.000 10.000 30.000 50.000	hz amp 0.886 0.997 0.998 0.992 0.980 1.017 1.032 1.101 1.015 0.870 0.768 0.344 0.239	amp err 0.013 0.019 0.022 0.016 0.019 0.011 0.001 0.001 0.003 0.000 0.001 0.001 0.000 0.001 0.000 0.000 0.004	hz phase 133.333 180.133 179.000 180.267 181.400 179.367 176.775 160.670 143.167 129.667 117.467 94.367 64.833	phase err 55.360 0.882 0.577 0.819 0.400 1.567 0.025 0.025 0.000 0.176 0.120 0.033 0.176 0.353
	requency 0.033 0.109 0.300 0.500 0.500 1.000 3.000 5.000 10.000 10.000 10.000 10.000 10.000 10.000	ellipticity -0.020 -0.038 -0.107 -0.177 -0.177 -0.228 -0.309 -0.513 -0.503 -0.473 -0.428 -0.254 -0.231 -0.254	ellip err 0.005 0.004 0.002 0.003 0.006 0.008 0.008 0.008 0.003 0.004 0.001 0.002 0.002 0.002	tilt ang 88.741 90.176 89.506 88.348 87.979 87.095 84.272 61.202 46.518 37.989 30.135 19.437 14.342 5.368	le tilt err 1.440 0.454 0.041 0.299 0.112 0.255 0.096 0.276 0.291 0.016 0.097 0.233 0.340





计分子状态

XBL 806-9816



station: t-t 1.5km south separation=1451 meters

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XBL 806-9815



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XBL 806-9818

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XBL 806-9817

station: h-h 1 number of turn hr mag const#7	.5km east s=4 100p .936 hz m	seperation radius=50 r 1g const=7.6	*1438 meter: leters 192	<b>B</b>
frequency 0.100 0.380 0.500 0.700 1.000 3.000 7.000 10.000 30.000 50.000 100.000	hr amp 0.062 0.105 0.164 0.244 0.320 0.837 1.115 1.200 1.438 1.011 0.895 0.469	amp err 0.000 0.001 0.001 0.001 0.003 0.014 0.002 0.003 0.006 0.003 0.006 0.003	hr phase 265.829 274.526 258.282 259.145 254.206 224.968 205.785 191.233 177.359 137.969 133.213 109.635	phase err 0.650 0.574 0.546 0.458 0.506 0.491 0.507 0.154 0.490 0.495 0.249 0.019
frequency 0.100 0.300 0.500 0.700 1.000 3.000 5.000 10.000 30.000 50.000 100.000	hz amp 1.065 1.007 1.006 0.988 1.012 1.007 0.996 0.939 0.939 0.937 0.332 0.229 0.078	GNP err 0.000 0.003 0.000 0.000 0.003 0.003 0.003 0.001 0.001 0.001 0.002 0.002 0.002 0.005	hz phase 175.617 177.261 177.530 175.937 174.787 161.310 150.947 130.158 128.965 93.881 67.869 38.202	phase err 0.250 0.001 0.099 0.498 0.499 0.008 0.034 0.688 0.524 0.226 0.548 0.548 0.691
frequency 0.108 0.309 0.509 0.709 1.009 3.000 5.000 7.000 10.009 50.009 50.009 100.800	11 ipticity -0.058 -0.104 -0.161 -0.245 -0.309 -0.598 -0.513 -0.556 -0.396 -0.216 -0.230 -0.158	ellip err 0.000 0.000 0.001 0.000 0.000 0.005 0.005 0.002 0.002 0.002 0.002 0.002 0.002 0.002 0.002 0.003	tilt angl 98.012 98.766 88.461 88.220 86.329 56.334 39.417 31.440 28.191 13.945 6.429 3.127	tilt eri 0.023 0.059 0.070 0.259 0.001 0.161 0.552 0.298 0.308 0.195 0.095 0.299



station: h-h 1.5km east separation=1438 meters

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XBL 806-9797 \*



Phase

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degrees

Hz=o Hr and Hz phase Hr=x

XBL 806-9796



ellipticity vs frequency

station: h-h 1.5km east separation=1438 meters

XBL 806-9795



XBL 806-9798

number of turns=4 loop radius=50 meters hr mag const=7.936 hz mag const=7.092 hr phase phase err frequency hr amp amp err 0.000 0.119 0.085 1.000 278.825 0.200 0.315 253,970 3.000 0.000 5.000 0.001 241.600 0.000 0.467 7.000 0.002 233.500 0.000 0.580 0.779 0.003 10.000 227.440 0.103 1.100 201.140 30.000 0.038 0.024 50.000 1.246 0.009 194.550 0.250 195.600 0.200 50.000 1.062 0.010 0.238 100.000 0.692 0.007 177.700 150.000 0.669 0.032 160.800 0.850 frequency hz phase 181.263 hz amp amp err phase err 1.000 0.001 0.152 1.046 3.000 0.002 182.670 1.115 0.058 179.600 5.000 1.170 0.004 0.000 177.225 177.500 161.213 7.000 1.187 0.004 0.243 10.000 1.407 0.210 0.005 1.222 0.043 30.000 0.091 50.000 1.182 0.008 154.550 0.250 159.480 144.725 50.000 0.973 0.010 0.185 100.000 0.508 0.005 0.243 0.469 150.000 0.023 127.650 0.858 tilt angle 🕾 frequency ellipticity ellip err tilt err 0.000 1.000 0.026 -0.113 90.872 84.432 3.000 0.073 -0.265 0.000 5.000 77.979 0.042 -0.339 0.001 7.000 -0.374 0.001 72.242 0.111 0.001 18.000 -0.368 67.098 0.046 -0.361 48.917 38.000 0.001 0.026 -0.363 50.000 0.000 43.028 0.030 41.930 34.734 50.000 0.001 0.009 108.000 -0.280 0.000 0.012 159.000 -8.277 33.288 34.788 0.002 0.088 209.000 -0.269 0.007 0.082

station: h-h .5km east separation=646 meters









Hr and Hz phase Hr=x Hz=o

station: h-h .5km east separation=646 meters

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XBL 806-9792



XBL 806-9793



ellipticity vs frequency

XBL 806-9794

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station: h-h.3k humber of turns hr mag const=7.	(m west se ==4 loop 936 hz ma	peration=34 radius=50 r g_const=7.0	neters Neters 192	•
frequency 0.100 0.300 0.500 0.700 1.000 3.000 5.000 10.000 30.000 50.000 100.000	hr amp 0.019 0.035 0.055 0.075 0.108 0.300 0.457 0.580 0.793 1.124 1.060 0.624	amp err 0.002 0.001 0.000 0.000 0.000 0.000 0.001 0.001 0.005 0.010 0.019 0.007	hr phase 218.800 241.000 248.750 252.133 254.763 247.870 239.600 232.833 226.667 200.200 193.467 174.020	phase err 3.512 1.080 0.479 0.333 0.137 0.100 0.000 0.333 0.333 0.000 0.333 0.058
frequency 0.100 0.300 0.500 0.700 1.000 3.000 5.000 7.000 10.000 30.000 50.000	hz amp 0.948 0.781 0.562 0.359 1.070 0.976 0.998 1.003 1.224 1.334 1.407	amp err 0.002 0.005 0.003 0.003 0.002 0.000 0.001 0.002 0.009 0.009 0.018	hz phase 174.800 164.750 156.750 155.800 174.873 178.770 178.600 179.167 176.000 166.200 148.800	phase err 0.008 0.759 0.259 0.008 0.077 0.080 0.080 0.080 0.080 0.080 0.080 0.080 0.080 0.080 0.080 0.080 0.080 0.080
frequency 0.100 0.300 0.500 0.700 1.090 3.090 5.090 10.000 30.000 50.000 100.000 200.000 500.000	1) ipticity -0.013 -0.044 -0.098 -0.209 -0.283 -0.378 -0.407 -0.413 -0.300 -0.389 -0.361 -0.302 -0.196	ellip err 0.001 0.002 0.001 0.000 0.000 0.000 0.003 0.003 0.003 0.000 0.003 0.000 0.002 0.001	tilt ang 89.186 99.200 91.389 88.974 83.194 75.345 67.095 62.610 50.879 55.989 28.090 18.636 12.700	tilt en 0.126 0.045 0.058 0.066 0.009 0.028 0.028 0.037 0.088 0.072 0.111 0.171 0.087 0.086 0.086 0.086



XBL 806-9800



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XBL 806-9799



station: h-h.5km west separation=548 meters

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XBL 806-9801

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frequency

station: h-h.5km west separation=548 meters

XBL 806-9802

frequency 0.100 0.300 0.500 0.700 1.000 3.000 7.000 10.000 30.000 50.000 150.000 frequency 0.100 0.300 0.500 0.700 1.000 3.000 5.000 7.000	hr amp 0.042 0.147 0.215	amp err 0.001 0.002	hr phase 1	ohase err
frequency 0.100 0.300 0.500 0.700 1.000 3.000 5.000 7.000	0.323 0.412 0.984 1.254 1.323 1.641 1.087 0.770 0.495	0.001 0.001 0.002 0.002 0.001 0.001 0.011 0.003 0.001 0.002	261.033 256.408 256.737 251.091 221.706 201.067 185.772 172.332 171.135 134.891 168.818	0.229 0.332 0.075 0.482 0.506 0.493 0.502 0.500 0.496 0.524 0.524 0.499 0.507
10.000 30.000 50.000 150.000	hz anp 1.000 1.108 1.096 1.101 1.099 1.115 1.025 0.882 0.720 0.274 0.160 0.073	amp err 0.005 0.004 0.001 0.002 0.002 0.001 0.002 0.001 0.001 0.015 0.000 0.002	hz phase 1 179.093 177.790 176.924 175.140 173.806 157.279 138.933 124.475 112.044 119.246 75.483 92.000	bhase err 0.002 0.503 0.501 0.502 0.003 0.505 0.497 0.499 0.522 0.117 0.513 0.297
frequency 0.100 0.300 0.500 1.000 3.000 5.000 10.000 30.000 50.000 150.000 200.000	ellipticity -0.042 -0.132 -0.192 -0.290 -0.362 -0.619 -0.578 -0.510 -0.361 -0.194 -0.177 -0.144 -0.140	ellip err 0.001 0.001 0.001 0.001 0.002 0.000 0.000 0.000 0.000 0.000 0.000 0.003 0.003 0.008	tilt angle 89.980 89.089 87.876 87.317 84.576 53.051 33.250 24.537 14.159 9.206 6.220 1.977 -0.457	tilt err 0.010 0.033 0.095 0.014 0.193 0.191 0.055 0.011 0.078 0.417 0.006 0.079 0.154

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station: h-h 1.5 km west separation=1562 meters



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XBL 806-9803

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XBL 806-9806

 $(\gamma_{i},\gamma_{i}) \in \{1,2\}$ 



station: h-h 1.5 km west separation=1562 meters

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XBL 806-9805

## APPENDIX C

One dimensional interpretation EM sounding data.



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PANTHER CANYON T-T 1.5KM NORTH

CALCU	JLATED DATA	MEASURED	DATA	LAYER	RESISTIVIT	Y(OHM-M)	THICKNESS	(M)	
HR	······································	HRR	х	1	4.90±	.00	233.0	±	١.
HZ	<u> </u>	HZ	*	2	150.00±	17.11	.1000E+1	1±	0.

DATA VARIENCE ESTIMATE 260.2

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XBL 803-8997

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## COMPARSION OF CALCULATED AND MEASURED DATA

PANTHER CANYON T-T I.5KM NORTH

CALCULATED DATA	8. 19 19 19 19 19 19 19 19 19 19 19 19 19 19 19 19 19 19 19 19 19 19 19 19 19 19 19 19 19 19 19 19 19 19 19 19 19 19.	MEASURED DATA	LAYER RESISTIVITY(OHM-M)	THICKNESS(M)
HR	<u></u>	HRX	1 4.90± .00	233.0 ± 1,
нг — —	—	HZ *	2 150.00: 17.11	.1000E+11+ 0.

DATA VARIENCE ESTIMATE 260.2 

XBL 803-8983



COMPARSION OF CALCULATED AND MEASURED DATA

PANTHER CANYON T-T 1.5KM NORTH

CALCULATED DATA	MEASURED DATA		LAYER	RESISTIVITY (OHM-N	D THICKNESS(M)
ELLIPTICITY	ELLIPTICITY	x	1	4.90= .00	233.0 <b>*</b> *
			2	150.00± 17.11	.1000E+11± 0.

DATA VARIENCE ESTIMATE 260.2

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XBL 804-9016


DATA VARIENCE ESTIMATE 260.2

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XBL 804-9015



PANTHER CANYON T-T Ø.5KM NORTH

CALCULATED DATA MEASURED DATA LAYER RESISTIVITY(OHM-M) THICKNESS(M) HR HR х 1 6.3ر . 2. .00 90.00 2 2.20: .06 200.0 16. ÷ 3 150.00: 611.83 .1000E+11: 0. DATA VARIENCE ESTIMATE 303.4 

XBL 803-8977



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COMPARSION OF CALCULATED AND MEASURED DATA

DATA VARIENCE ESTIMATE 303.4

·注意:4. 《金子》:《中国中华》(4. 1998)

XBL 803-8970

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PANTHER CANYON T-T Ø.5KM NORTH

CALCULATED D	ATA	MEASURED DATA		LAYER	RESISTIVITY	(OHM-M)	THICKNESS	×. MD
ELLIPTICITY		ELLIPTICITY	х	1	6.30±	.00	90.00	* · 2.
				2	2.20±	.06	200.0	± 16.
DATA VARIENCE	ESTIMATE 303.4			3	150.00± 6	11.83	.1000E+11	* Ø.

XBL 803-8976

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CALCULATED DATA	MEASURED DATA LAYER RE	SISTIVITY(OHM-M)	THICKNESS(N)
TILT ANGLE	TILT ANGLE X	6.30: .00	90.00 = 2.
	2	2.20* .06	200.0 + 16.
	3	150.00+ 611.83	.1000E+11: 0.

DATA VARIENCE ESTIMATE 303.4

XBL 804-9012





PANTHER CANYON T-T 0.5KM SOUTH

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CALCULATED DATA	MEASURED	DATA	LAYER	RESISTIVITY	(OHM-M)	THICKNESS (M)
HR	HR	x	1	6.30±	.00	90.00 ± 1.
			2	2.20±	.03	.1000E+11: 0.
		÷		1		- sin sastri.
DATA VARIENCE ESTIMATE 381.7	1			a ha sata y		a and the second second second second second second second second second second second second second second se

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PANTHER CANYON T-T 0.5KM SOUTH

CALCULATED DATA	MEASURED DATA LAYER RE	SISTIVITY(OHM-M)	THICKNESS(M)
HR	HR X	6.30: .00	90.00 + 1.
the constant of the relation	1719 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	2.20: .03	.1000E+11+ 0.
	2월 - 11일 - 11일 - 11일 (Y)라이트 (Y)라이트 (Y)라이트 (Y)라이트 (Y)라이트 (Y)라이트 (Y)라이트 (Y)라이트 (Y)라이트 (Y)라이트 (Y)라이트 (Y)라이트 (Y)라이트 (Y)라이트 (Y)라이트 (Y)라이트 (Y)라이트 (Y)라이트 (Y)라이트 (Y)라이트 (Y)라이트 (Y)라이트 (Y)라이트 (Y)라이트 (Y)라이트 (Y)라이트 (Y)라이트 (Y)라이트 (Y)라이트 (Y)라이트 (Y)라이트 (Y)라이트 (Y)라이트 (Y)라이트 (Y)라이트 (Y)라이트 (Y)라이트 (Y)라이트 (Y)라이트 (Y)라이트 (Y)라이트 (Y)라이트 (Y)라이트 (Y)라이트 (Y)라이트 (Y)라이트 (Y)라이트 (Y)라이트 (Y)라이트 (Y)라이트 (Y)라이트 (Y)라이트 (Y)라이트 (Y)라이트 (Y)라이트 (Y)라이트 (Y)라이트 (Y)라이트 (Y)라이트 (Y)라이트 (Y)라이트 (Y)라이트 (Y)라이트 (Y)라이트 (Y)라이트 (Y)라이트 (Y)라이트 (Y)라이트 (Y)라이트 (Y)라이트 (Y)라이트 (Y)라이트 (Y)라이트 (Y)라이트 (Y)라이트 (Y)라이트 (Y)라이트 (Y)라이트 (Y)라이트 (Y)라이트 (Y)라이트 (Y)라이트 (Y)라이트 (Y)라이트 (Y)라이트 (Y)라이트 (Y)라이트 (Y)라이트 (Y)라이트 (Y)라이트 (Y)라이트 (Y)라이트 (Y)라이트 (Y)라이트 (Y)라이트 (Y)라이트 (Y)라이트 (Y)라이트 (Y)라이트 (Y)라이트 (Y)라이트 (Y)라이트 (Y)라이트 (Y)라이트 (Y)라이트 (Y)라이트 (Y)라이트 (Y)라이트 (Y)라이트 (Y)라이트 (Y)라이트 (Y) (Y) (Y) (Y) (Y) (Y) (Y) (Y) (Y) (Y)		Section (Marchaele

DATA VARIENCE ESTIMATE 381.7

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XBL 803-8988



ELLIPTICITY ELLIPTICITY X ł 6.30\* .00 90.00 1. 2 2.20: .03 .1000E+11+ 0.

DATA VARIENCE ESTIMATE 381.7

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XBL 803-8986



CALCULATED DATA	MEASURED DATA	LAYER	RESISTIVITY(OHM-M)	THICKNESS(M)	
TILT ANGLE	TILT ANGLE	X I	6.30* .00	90.00 +	1
		•	2 20 · 02	1000E.11.	-

XBL 803-8985

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DATA VARIENCE ESTIMATE 153.8

XBL 804-9008



PANTHER CANYON T-T I.5KM SOUTH

CALCULATED DATA	MEASURED DATA	LAYER	RESISTIVITY(OHM-M) THICKNESS(M)	
HR	HR X	1	8.10± .00 340.0 ±	16.
нг — — —	HZ *	2	3.90* .38 280.0 *	47.
		3	150.00± 173.45 .1000E+11±	Ø.
DATA VARIENCE ESTIMATE 153.8				

XBL 804-9013



XBL 804-9005



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CALCULATED DATA	MEASURED DATA	LAYER	RESISTIVITY(OHM-M)	THICKNESS(N)	
TILT ANGLE	TILT ANGLE	<b>X</b> 1	8.10: .00	340.0 + 16.	
		2	3.90± .38	280.0 + 47.	
		3	150.00: 173.45	.1000E+11+ 0.	
DATA VARIENCE ESTIMATE	53.8				

XBL 803-8971

81



PANTHER CANYON H-H 1.5KM EAST

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CALCULATED DATA	MEASU	RED DATA	LAYER	RESISTIVI	Y(OHM-M)	THICKNESS(M)	
HR ~	HIR	x	1	9.00±	.00	200.0 ±	15.
			2	2.7ر	.57	125.0 •	34.
			3	150.00±	102.33	.1000E+11±	0.
DATA VARIENCE ESTIMATE 126.2							

### XBL 805-9744

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DATA VARIENCE ESTIMATE 126.2 940 J34 - 1- E

e server al algerada

XBL 805-9746

.1000E+11: 0.

\* 34.

125.0

.57

150.00± 102.33



CALCULATED DATA	MEASURED DATA		LAYER	RESISTIVI	(M-MHO)Y1	THICKNESS(M)	
TILT ANGLE	TILT ANGLE	x	1	9.00:	.00	200.0 +	15.
an an an an an an an an an an an an an a			2	2.7ر	.57	125.0 ±	34.
- -			3	150.00+	102.33	.1000E+11±	0.
DATA VARIENCE ESTIMATE	126.2						

XBL 805-9748

COMPARSION OF CALCULATED AND MEASURED DATA



		stal <u>Tit</u>		· · · · · · · · · · · · · · · · · · ·	14
ELLIPTICITY	ELLIPTICITY	K I	9.00* .00	200.0 ± 15.	
		2	2.70± .57	125.0 . 34.	
(a) A set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the set of the se	1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1	3	150.00± 102.33	.1000E+11: 0.	
DATA VARIENCE ESTIMATE	26.2			slad, Highlight and the Attraction	

11.1

XBL 805-9747



DATA VARIENCE ESTIMATE 90.07

XBL 806-9848

COMPARSION OF CALCULATED AND MEASURED DATA

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CALCULATED DATA	MEASUR	ED DATA	LAYER RE	SISTIVITY(O	M-M)	THICKNESS	(M)	4 J.
HR	- HR	x	1	15.00+	.00	120.0	<b>±</b> <sup>±</sup>	2.
LI7	- HZ	*	2	2.80±	.08	200.0	*	20.
			3	10.00± 1	.85	.1000E+1	1±	0.
DATA VARIENCE ESTIMA	TE 90.07						1.51	

물건 아파 물질 것 같

XBL 806-9847

COMPARSION OF CALCULATED AND MEASURED DATA

20.00				
0.00				
0.00		10.00	100.00	

.2

з

2.80±

10.00±

.08

1.85

200.0

.1000E+11:

COMPARSION OF CALCULATED AND MEASURED DATA

DATA VARIENCE ESTIMATE 90.07

XBL 805-9741

0.

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100.00

80.00

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PANTHER CANYON H-H 0.5KM EAST

15-00± .00 120-0 ± 2
2.80* .08 200.0 * 20.
10.00± 1.85 .1000E+11± 0

XBL 805-9740



DATA VARIENCE ESTIMATE 504.5

XBL 803-8979



COMPARSION OF CALCULATED AND MEASURED DATA

<sup>11</sup> A. M. M. M. M. Martin and M. M. Martin, Phys. Rev. Lett. 19, 121 (1996).



PANTHER CANYON H-H 0.5KM WEST

 CALCULATED DATA
 MEASURED DATA
 LAYER
 RESISTIVITY(0HM-M)
 THICKNESS(N)

 HR
 HR
 1
 10.00±
 .60
 50.00
 ±
 1.

 12
 3.20±
 .63
 .1000E+11±
 0.

DATA VARIENCE ESTIMATE 504.5

XBL 803-8965



PANTHER CANYON H-H 0.5KM WEST

CALCULATED DATA	MEASURED DATA		LAYER	RESISTIVITY	OHM-M)	THICKNESS	( <b>M</b> )	
ELLIPTICITY	ELLIPTICITY	x	1	10.00±	.00	50.00	*	۱.
			2	3.20+	.03	.1000E+11	<b>!</b> *	0.
				1				

DATA VARIENCE ESTIMATE 504.5

XBL 804-9018

1.1.1.1.



PANTHER CANYON H-H 0.5KM WEST

.00 50.00 + 1. S. Bar 2 3.20: .03 .1000E+11: 0.

DATA VARIENCE ESTIMATE 504.5

5. S. . . .

1998年1月2日日日

XBL 803-8982

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DATA VARIENCE ESTIMATE \$2.50

XBL 803-8999



PANTHER CANYON H-H 1.5KM WEST

 CALCULATED DATA
 MEASURED DATA
 LAYER
 RESISTIVITY(OHM-M)
 THICKNESS(N)

 HR
 1
 8.00±
 00
 700.0
 ±
 42.

 2
 25.00±
 6.31
 .1000E+11±
 0.

DATA VARIENCE ESTIMATE 82.50

2003-542-19 12<del>5</del>2

XBL 804-9002



XBL 803-8995

DATA VARIENCE ESTIMATE 82.50



CALCULATED DATA	MEASURED DATA	LAYER	RESISTIVITY(OHM-M)	THICKNESS(N)	
TILT ANGLE	TILT ANGLE X	1	8.00: .00	700.0 + 42.	
		2	25.00: 6.31	.1000E+11= 0.	

DATA VARIENCE ESTIMATE 82.50

XBL 803-8996