

Lawrence Berkeley National Laboratory

Recent Work

Title

STRUCTURES OF BICYCLO(2.2.1) SYSTEMS III. 2-EXO-HYDROXY-7-METHYLBICYCLO(2.2.1)HEPTANE-7-SYN-CARBOXYLIC ACID.

Permalink

<https://escholarship.org/uc/item/63c5c13d>

Author

Chapuis, Gervais

Publication Date

1976-08-01

STRUCTURES OF BICYCLO(2.2.1) SYSTEMS III.
2-EXO-HYDROXY-7-METHYLBICYCLO(2.2.1)HEPTANE-7-SYN-CARBOXYLIC ACID

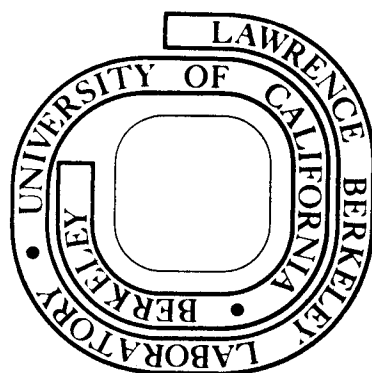
Gervais Chapuis, Allan Zalkin and David H. Templeton

August 1976

Prepared for the U.S. Energy Research and
Development Administration under Contract W-7405-ENG-48

For Reference

Not to be taken from this room



LBL-5450
c. 1

DISCLAIMER

This document was prepared as an account of work sponsored by the United States Government. While this document is believed to contain correct information, neither the United States Government nor any agency thereof, nor the Regents of the University of California, nor any of their employees, makes any warranty, express or implied, or assumes any legal responsibility for the accuracy, completeness, or usefulness of any information, apparatus, product, or process disclosed, or represents that its use would not infringe privately owned rights. Reference herein to any specific commercial product, process, or service by its trade name, trademark, manufacturer, or otherwise, does not necessarily constitute or imply its endorsement, recommendation, or favoring by the United States Government or any agency thereof, or the Regents of the University of California. The views and opinions of authors expressed herein do not necessarily state or reflect those of the United States Government or any agency thereof or the Regents of the University of California.

Structures of Bicyclo[2.2.1] Systems III.

2-exo-hydroxy-7-methylbicyclo[2.2.1]heptane-7-syn-carboxylic acid*

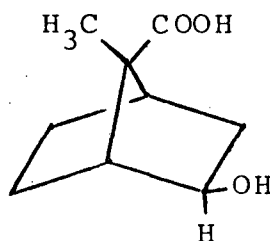
BY GERVAIS CHAPUIS, ALLAN ZALKIN AND DAVID H. TEMPLETON

*Materials and Molecular Research Division
Lawrence Berkeley Laboratory, University of California
Berkeley, California 94720 U.S.A.*

Abstract. $C_9H_{14}O_3$, monoclinic, $P2_1/c$, $a = 11.58(2)$, $b = 6.874(10)$,
 $c = 12.02(2)$ Å, $\beta = 115.21(5)^\circ$, $Z = 4$, $D_x = 1.306(7)$, $D_m = 1.32(1)$ g cm⁻³,
at 22°C. For 798 reflections with $I > \sigma$, $R = 0.056$ and $R_w = 0.032$.
The norbornane skeleton shows no distortion by the substituent groups,
and the O(hydroxyl)-C(carboxyl) distance 2.87 Å is less crowded than in
a related 2,6-hydroxyacid which lactonizes more rapidly.

* Work done in part with support from the U.S. Energy Research and Development Administration.

Introduction. This compound was studied as part of a program to establish the dimensions and their variation for a variety of substituted norbornane molecules (Chapuis, Zalkin & Templeton, 1973 and 197x). There has been contradiction in the literature concerning the identity of this isomer, and our work directly confirms its assignment by Moriarty & Adams (1973) to the structure:



This hydroxyacid was prepared from the lactone which melts at 125-126° (Storm & Koshland, 1972b) and was crystallized from ethyl acetate by Hackney (1975). Photographic and diffractometer x-ray experiments were made with a crystal 0.16 x 0.14 x 0.03 mm in size. Absent reflections $h0\ell$, $\ell \neq 2n$ and $0k0$, $k \neq 2n$ indicate space group $P2_1/c$. Setting angles of 12 reflections within the range $23^\circ < 2\theta < 28^\circ$ were used for least-squares adjustment of the cell dimensions (λ 0.70926 Å for $\text{MoK}\alpha_1$). Intensities were measured by θ - 2θ scan technique for 2293 reflections with $2\theta < 45^\circ$ in the half-sphere with k non-negative. Averaging of equivalent pairs yielded 1146 independent reflections; for 798 of them, $I > \sigma$. With $\mu(\text{Mo}) = 1.0 \text{ cm}^{-1}$ an absorption correction was deemed unnecessary. An empirical extinction correction added 13% to the structure factor of the strongest reflection. The structure was solved by the MULTAN program (Germain, Main & Woolfson, 1971). Hydrogen atoms were found in difference maps or by calculation from coordinates of carbon atoms. Atomic form factors, the method of

weighting, and definitions of R and R_w were the same as described before (Chapuis, et al., 197x) except that $w = 0$ if $I < \sigma$. In the last cycle, no parameter shifted more than 0.15σ . The final R was 0.056 for 798 reflections and 0.096 including reflections of zero weight; R_w was 0.032. Final parameters, distances, and angles are listed in Tables 1 - 4.*

Discussion. Figure 1 shows the molecular shape and numbering scheme. The range of C-C bond lengths from 1.51 to 1.56 suggests that the standard deviations are somewhat underestimated by the least-squares method, but otherwise these distances are unremarkable. The bond angles conform closely to the symmetry of unsubstituted norbornane, and they give little indication that the framework has been distorted by the substituent groups. This result is in contrast to the substantial distortion observed in the salt of a 2,6-hydroxyacid (Chapuis, et al., 197x). We note that the distance between O(3) and C(9) is 2.866(8) Å, only modestly greater than the 2.783(3) Å observed for the 2,6-hydroxyacid. Estimates from Dreiding models (Storm & Koshland, 1972a; Moriarty & Adams, 1973) correspond to about 2.9 and 2.2 Å, respectively, for these two distances; these values also indicate that there is considerable strain in the latter compound. The 2,6-compound undergoes acid-catalyzed lactonization with a rate about 7×10^4 times greater than the 2,7-compound (Hackney, 1975). For reference in

* A list of structure factors has been deposited with the British Library Lending Division as Supplementary Publication No.

discussions of these rates, we report also the angles

$C(2) - O(3) - C(9) = 78.7(2)^\circ$ and $C(7) - C(9) - O(3) = 82.0(2)^\circ$.

Each molecule is attached to three others by a total of four hydrogen bonds (Fig. 2), forming sheets parallel to (100). Each hydroxyl group forms a hydrogen bond to O(1) of one neighboring molecule while it accepts a hydrogen bond from O(2) of another neighbor.

We thank Dr. D.D. Hackney and Professor D.E. Koshland for providing the crystals. G. Chapuis acknowledges the Swiss National Funds for financial support.

References

Chapuis, G., Zalkin, A. & Templeton, D.H. (1973).

Acta Cryst. B 29, 2642-2644.

Chapuis, G., Zalkin, A. & Templeton, D.H. (197x).

Submitted to Acta Crystallographica.

Germain, G., Main, P. & Woolfson, M.M. (1971).

Acta Cryst. A 27, 368-376.

Hackney, D.D. (1975). Models for Chymotrypsin and the Interaction of Lysozyme with Urea. Thesis, University of California, Berkeley.

Moriarty, R.M. & Adams, T. (1973). J. Amer. Chem. Soc. 95, 4070-4071.

Storm, D.R. & Koshland, D.E. (1972a). J. Amer. Chem. Soc. 94, 5805-5814.

Storm, D.R. & Koshland, D.E. (1972b). J. Amer. Chem. Soc. 94, 5815-5825.

Table 1. Parameters for heavy atoms^a

	x	y	z	B ₁₁	B ₂₂	B ₃₃	B ₁₂	B ₁₃	B ₂₃
C(1)	.2123(3)	.1437(6)	.5756(3)	2.1(2)	3.1(2)	1.6(1)	- .1(2)	.7(1)	- .2(2)
C(2)	.1376(3)	.2964(6)	.4823(3)	2.8(2)	2.3(2)	2.8(2)	- .1(2)	1.1(2)	- .3(2)
C(3)	.2113(4)	.3148(7)	.4011(4)	3.7(2)	3.4(3)	3.0(2)	- .6(2)	1.7(2)	.5(2)
C(4)	.3218(3)	.1704(5)	.4621(3)	2.4(2)	3.8(2)	2.1(2)	- .1(2)	1.1(1)	- .6(2)
C(5)	.4152(4)	.2563(8)	.5847(4)	3.3(2)	4.1(3)	3.3(2)	- .8(2)	1.4(2)	- .8(2)
C(6)	.3374(4)	.2426(8)	.6633(4)	3.4(2)	4.0(3)	2.7(2)	- .2(2)	.9(2)	- .6(2)
C(7)	.2582(3)	.0056(5)	.5018(3)	1.9(2)	3.1(2)	1.7(1)	.1(1)	.5(1)	.2(2)
C(8)	.3480(5)	-.1569(7)	.5779(5)	2.9(2)	3.9(3)	3.7(2)	.9(2)	.8(2)	.5(2)
C(9)	.1522(3)	-.1019(6)	.3985(3)	2.5(2)	2.9(2)	2.2(2)	.5(2)	1.0(1)	.2(2)
O(1)	.0737(2)	-.2023(4)	.4135(2)	3.3(1)	3.8(1)	3.4(1)	-1.1(1)	1.8(1)	- .3(1)
O(2)	.1595(3)	-.0897(4)	.2917(2)	3.5(1)	5.4(2)	2.5(1)	-1.6(1)	1.5(1)	-1.1(1)
O(3)	.0087(2)	.2341(4)	.4050(2)	2.5(1)	4.3(2)	2.8(1)	.7(1)	1.0(1)	1.2(1)

^a The form of the temperature factor is $\exp [-0.25(h^2 a^{*2} B_{11} + 2hka^* b^* B_{12} + \dots)]$.

0 0 0 0 4 6 0 3 4 0 0

Table 2. Parameters for hydrogen atoms^a

	x	y	z	B
H(1)	.156(3)	.082(4)	.615(3)	1.7(8)
H(2)	.131(3)	.441(5)	.521(3)	2.6(8)
H(3)	.144(3)	.275(5)	.303(3)	2.5(7)
H(4)	.246(3)	.455(6)	.400(3)	2.6(9)
H(5)	.365(3)	.121(4)	.405(2)	1.4(7)
H(6)	.500(3)	.168(5)	.626(3)	3.3(9)
H(7)	.438(4)	.407(7)	.577(4)	5.4(12)
H(8)	.391(3)	.152(5)	.739(3)	2.4(9)
H(9)	.321(3)	.384(6)	.688(3)	4.0(10)
H(10)	.293(4)	-.261(7)	.611(4)	6.2(12)
H(11)	.389(4)	-.236(6)	.525(3)	5.2(11)
H(12)	.428(4)	-.102(6)	.647(3)	4.0(10)
H(13)	.083(5)	-.169(8)	.228(5)	9.9(18)
H(14)	-.038(5)	.217(8)	.459(4)	9.2(17)

^a The form of the temperature factor is $\exp(-B\lambda^{-2}\sin^2\theta)$.

Table 3. Bond distances (Å)

C(1)-C(2)	1.511(6)	C(1)-H(1)	1.04(3)
C(1)-C(6)	1.540(6)	C(2)-H(2)	1.11(3)
C(1)-C(7)	1.540(6)	C(3)-H(3)	1.13(3)
C(2)-C(3)	1.552(6)	C(3)-H(4)	1.05(4)
C(3)-C(4)	1.537(6)	C(4)-H(5)	1.06(3)
C(4)-C(5)	1.527(6)	C(5)-H(6)	1.08(3)
C(4)-C(7)	1.534(6)	C(5)-H(7)	1.08(4)
C(5)-C(6)	1.561(7)	C(6)-H(8)	1.06(3)
C(7)-C(8)	1.536(6)	C(6)-H(9)	1.06(4)
C(7)-C(9)	1.515(6)	C(8)-H(10)	1.14(5)
C(2)-O(3)	1.447(5)	C(8)-H(11)	1.09(4)
C(9)-O(1)	1.215(5)	C(8)-H(12)	1.02(4)
C(9)-O(2)	1.323(5)	O(2)-H(13)	1.04(5)
O(1)...O(3)	2.737(6)	O(3)-H(14)	1.01(5)
O(2)...O(3)	2.633(6)		

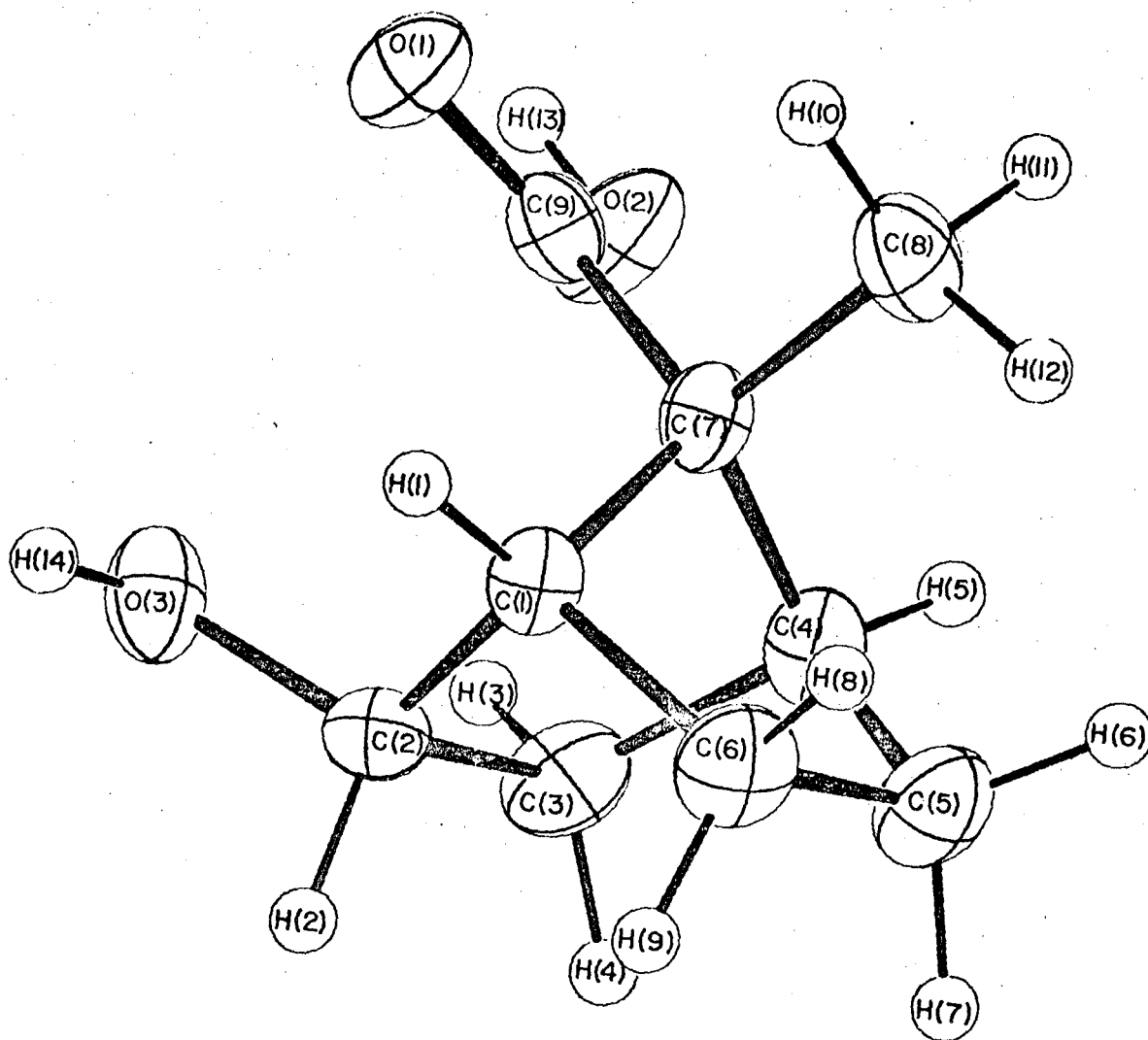
Table 4. Bond angles (deg)

C(2)-C(1)-C(6)	106.0(4)
C(2)-C(1)-C(7)	103.2(3)
C(6)-C(1)-C(7)	102.2(3)
C(1)-C(2)-C(3)	103.3(3)
C(1)-C(2)-O(3)	112.3(3)
C(3)-C(2)-O(3)	108.3(3)
C(2)-C(3)-C(4)	102.5(3)
C(3)-C(4)-C(5)	108.3(4)
C(3)-C(4)-C(7)	102.2(3)
C(5)-C(4)-C(7)	102.8(3)
C(4)-C(5)-C(6)	102.0(3)
C(1)-C(6)-C(5)	103.3(3)
C(1)-C(7)-C(4)	93.1(3)
C(1)-C(7)-C(8)	114.6(3)
C(1)-C(7)-C(9)	114.5(3)
C(4)-C(7)-C(8)	115.4(3)
C(4)-C(7)-C(9)	115.7(3)
C(8)-C(7)-C(9)	103.9(4)
C(7)-C(9)-O(1)	123.4(3)
C(7)-C(9)-O(2)	113.6(3)
O(1)-C(9)-O(2)	122.8(3)
C(9)-O(2)-H(13)	107(2)
C(2)-O(3)-H(14)	108(3)
O(1)...O(3)-H(14)	11(3)
O(3)...O(2)-H(13)	13(3)

Figure Captions

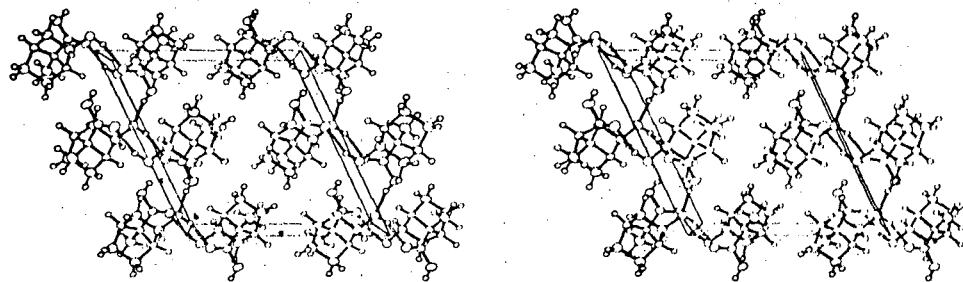
Fig 1. Perspective view of a molecule with 50% probability thermal ellipsoids, drawn with Johnson's ORTEP. Size of hydrogen atoms is arbitrary.

Fig 2. Stereoscopic view of the crystal structure along the b axis, showing hydrogen bonds between molecules.



XBL 741-239

Fig. 1



XBL 741-241

Fig. 2

OBSERVED STRUCTURE FACTORS, STANDARD DEVIATIONS, AND DIFFERENCES (X10.0) FOR THE NORBORNANE DERIVATIVE [C9 H14 O3]. F(0,0,0) = 7363

FOB AND FCA ARE THE OBSERVED AND CALCULATED STRUCTURE FACTORS.
 SG = ESTIMATED STANDARD DEVIATION OF FOB. DEL = /FOB/ - /FCA/.
 * INDICATES ZERO WEIGHTED DATA.

K	FOB	SG	DEL	K	FOB	SG	DEL	K	FOB	SG	DEL	K	FOB	SG	DEL	K	FOB	SG	DEL
	H,L=	0,	0	1	248	7	-6	2	212	22	19	7	7	81	-3*	2	186	10	1
21	940	20	18	2	250	9	-3	3	231	17	1		H,L=	1,	0	3	79	94	5*
4	154	11	-15	3	409	6	-12	4	148	36	-8	0	989	12	-14	4	68	93	-25*
6	74	98	71*	4	59	89	13*	5	67	92	-10*	11	1010	12	-17	5	891	106	-35*
	H,L=	0,	1	5	88	37	22	6	67	84	49*	2	277	21	-22	6	46	73	17*
11	352	14	15		H,L=	0,	8		H,L=	1,	-6	3	609	13	-9		H,L=	1,	7
2	780	11	-36	0	177	15	28	0	670	13	5	4	95	19	8	1	127	21	23
3	462	8	1	1	201	15	3	1	56	21	41	5	70	29	52	2	94	27	-8
4	53	65	9*	2	231	20	3	2	262	6	-2	6	92	23	5	3	64	77	36*
5	48	58	13*	3	260	13	20	3	69	82	4*	7	128	29	16	4	54	56	50*
6	50	53	30*	4	148	35	5	4	129	44	28		H,L=	1,	1	5	0	90	-14*
7	155	22	3	5	92100		13*	5	89	95	-2*	1	331	8	-11		H,L=	1,	8
	H,L=	0,	2		H,L=	0,	9	6	51117		-30*	2	187	21	-2	0	75	43	-11
01	980	21	45	1	203	21	2		H,L=	1,	-5	3	137	16	27	1	50	68	18*
1	288	17	-21	2	264	9	-5	1	116	43	-11	4	150	25	-2	2	136	12	1
2	674	11	-15	3	178	10	-7	2	246	16	11	5	200	20	-11	3	148	29	-10
3	293	12	-10	4	80	95	54*	3	207	24	7	6	138	46	-13	4	28	57	5*
4	228	10	-7		H,L=	0,	10	4	35	86	11*	7	138	27	18	5	107	79	14
5	55	35	-51*	0	526	14	-9	5	202	19	-18		H,L=	1,	2		H,L=	1,	9
6	239	12	-3	1	243	26	-4	6	80	49	57	0	382	11	-16	1	118	25	22
7	173	17	-1	2	87102		72*		H,L=	1,	-4	1	299	19	-20	2	366	10	10
	H,L=	0,	3	3	181	14	12	0	225	20	10	2	246	15	31	3	150	25	-12
1	68112		20*		H,L=	0,	11	1	56	86	1*	3	865	10	6	4	79	46	28
2	102	42	-40	1	116129		-2*	2	501	8	-2	4	58	59	-5*		H,L=	1,	10
3	242	8	3	2	130	48	41	3	82	44	31	5	323	14	5	0	598	8	-7
4	179	22	20		H,L=	1,	-12	4	225	15	5	6	0	96	-11*	1	96	41	14
5	140	31	-2	0	227	16	13	5	121	32	0	7	131	60	-10	2	228	21	-23
6	0	63	-26*	1	173	22	19	6	0	63	-32*		H,L=	1,	3	3	131	33	22
7	188	22	-1		H,L=	1,	-11	7	73	86	38*	1	658	10	-1		H,L=	1,	11
	H,L=	0,	4	1	92	22	-20		H,L=	1,	-3	2	851	9	10	1	136	47	-23
0	676	9	5	2	168	17	6	1	83	98	-9*	3	328	13	-20		H,L=	2,	-12
1	554	8	10	3	82103		72*	2	138	39	-1	4	142	23	-17	0	186	17	31
2	797	15	21		H,L=	1,	-10	3	86	28	23	5	15	80	-22*	1	30	91	9*
3	89	72	27	0	0	64	-15*	4	378	10	-13	6	77	91	4*	2	103	37	31
4	67	76	54*	1	91114		-4*	5	41	85	11*	7	85	53	60		H,L=	2,	-11
5	58	67	43*	2	53	69	30*	6	90	59	-9		H,L=	1,	4	1	116	73	-24
6	138	30	-25	3	122	20	29	7	138	22	17	0	135	19	5	2	15	78	6*
	H,L=	0,	5	4	68	82	-14*		H,L=	1,	-2	1	71	17	4	3	224	10	2
1	47	48	8*		H,L=	1,	-9	0	0124		-0*	2	158	16	10		H,L=	2,	-10
2	0	70	-46*	1	127	17	25	1	858	10	-21	3	131	15	7	0	106	68	25
3	513	13	-5	2	73	78	-21*	2	575	9	-12	4	193	12	6	1	62	91	-22*
4	52	62	10*	3	114	25	35	3	425	5	-1	5	280	17	19	2	446	7	5
5	56	74	30*	4	93	60	40	4	285	11	-2	6	41	82	22*	3	124	76	-39
6	53109		30*	5	31	81	-33*	5	228	11	-0		H,L=	1,	5	4	110	37	-30
	H,L=	0,	6		H,L=	1,	-8	6	70	72	52*	1	103	15	14		H,L=	2,	-9
0	847	14	-2	0	254	10	-15	7	29	77	25*	2	315	7	3	1	126	32	9
1	35	48	3*	1	49	67	11*		H,L=	1,	-1	3	279	15	-6	2	412	13	-3
2	554	7	7	2	15	82	12*	1	178	30	-29	4	318	14	-9	3	463	9	0
3	151	21	-3	3	200	18	-6	21	077	12	-8	5	152	35	-14	4	102	30	98
4	197	15	14	4	11	95	-61*	3	157	17	17	6	132	14	6	5	165	27	26
5	91	75	11	5	0	74	-29*	4	93	20	-23		H,L=	1,	6		H,L=	2,	-8
6	0	65	-37*		H,L=	1,	-7	5	151	39	-9	0	185	10	-7	0	518	8	-2
	H,L=	0,	7	1	277	6	-2	6	75	89	-36*	1	302	14	-10	1	132	11	-5

STRUCTURE FACTORS CONTINUED FOR
THE NORBORNANE DERIVATIVE [C9 H14 O3].

K	FOB	SG	DEL	K	FOB	SG	DEL	K	FOB	SG	DEL	K	FOB	SG	DEL	K	FOB	SG	DEL
2	159	46	8	5	242	18	-7	5	130	33	-4	1	524	6	3	1	401	13	11
3	214	11	-2	6	186	21	3	H,L=	2,	7	2	247	6	-4	21296	15	18		
4	319	18	-15	7	137	28	-3	1	115	20	-3	3	219	16	16	3	599	8	0
5	76	39	-39*	H,L=	2,	0	2	154	55	-10	4	180	21	26	4	197	7	4	
H,L=	2,	-7	0	978	10	-25	3	0	67	-17*	5	241	9	-4	5	452	9	-16	
1	175	19	-1	1	761	9	-3	4	27	74	-28*	6	80	96	51*	6	84	95	58*
2	92	22	-1	2	659	9	-6	5	171	12	-10	H,L=	3,	-5	7	66	48	-19	
3	402	7	-9	3	97	14	4	H,L=	2,	8	1	228	6	-9	H,L=	3,	2		
4	242	7	11	4	357	15	-4	0	372	8	-6	2	524	8	-2	0	467	6	-1
5	121	42	13	5	204	25	-17	1	155	23	-24	3	139	28	-5	1	722	10	5
6	79	94	64*	6	245	21	16	2	96	23	1	4	286	9	20	2	50	85	-1*
H,L=	2,	-6	7	149	31	-20	3	102	45	79	5	56	69	35*	3	346	5	3	
0	523	7	1	H,L=	2,	1	4	58	80	-1*	6	109	41	59	4	112	57	-29	
1	179	11	-0	1	58	91	27*	H,L=	2,	9	H,L=	3,	-4	5	163	17	-31		
2	140	10	11	2	818	11	-5	1	195	15	-8	0	478	10	-11	6	52	86	9*
3	33	77	-6*	3	347	11	4	2	31	57	-3*	11110	14	-13	H,L=	3,	3		
4	467	10	-14	4	154	20	-14	3	67	75	-3*	2	487	8	4	1	673	13	16
5	133	37	9	5	49	67	38*	H,L=	2,	10	3	264	20	-8	2	638	9	1	
6	128	23	-14	6	133	61	-31	0	103	53	-15	4	213	9	-7	3	456	8	-8
H,L=	2,	-5	7	253	24	17	1	63	75	-4*	5	161	15	3	4	441	11	9	
1	391	8	3	H,L=	2,	2	2	92109	1*	6	52	73	-13*	5	101	17	18		
2	253	10	-3	01414	16	13	H,L=	3,-12	7	87104	83*	6	85	86	24*				
3	106	33	30	1	339	15	-9	0	126	26	3	H,L=	3,	-3	H,L=	3,	4		
4	92	26	15	21017	12	10	1	63	69	37*	1	185	22	-20	0	136	10	7	
5	201	32	-22	3	69	82	-5*	2	0107	-24*	2	546	6	-16	1	299	9	-6	
6	74	46	5	4	188	11	-1	H,L=	3,-11	3	225	7	6	2	200	19	-3		
H,L=	2,	-4	5	68	91	-21*	1	54	76	44*	4	275	13	4	3	219	11	-0	
0	698	9	-8	6	376	11	10	2	98	20	-18	5	200	21	7	4	261	11	-19
1	45	72	3*	7	103103	-54*	3	70	83	1*	6	62	73	-15*	5	60	74	-14*	
2	421	7	-2	H,L=	2,	3	H,L=	3,-10	7	0	61	-11*	6	122	51	-14			
3	300	8	6	1	410	7	19	0	244	21	4	H,L=	3,	-2	H,L=	3,	5		
4	445	9	7	2	111	22	19	1	113	26	27	0	361	14	-20	1	6	49	-23*
5	161	23	-17	3	80	41	42	2	0	89	-35*	1	531	15	-14	2	149	25	-15
6	63118	3*	4	218	17	27	3	58	78	51*	2	111	47	0	3	0	68	-6*	
7	183	14	34	5	207	10	14	4	87104	23*	3	328	9	6	4	73	88	-1*	
H,L=	2,	-3	6	45	58	-13*	H,L=	3,-9	4	39	57	25*	5	50	82	40*			
1	210	32	-29	H,L=	2,	4	1	89	94	58*	5	94	53	42	H,L=	3,	6		
2	260	13	-26	0	341	8	7	2	180	14	8	6	75	34	63	0	67	53	21
3	0	50	-0*	1	488	7	3	3	262	8	-6	7	118	27	-19	1	139	22	0
4	149	19	-16	2	259	10	4	4	174	53	4	H,L=	3,-1	2	175	11	4		
5	171	35	-48	3	266	25	-16	5	258	23	6	1	90102	-7*	3	85	45	-5	
6	125	22	23	4	133	23	3	H,L=	3,-8	2	338	7	5	4	83	33	16		
7	63	73	-4*	5	127	45	13	0	77	79	48*	3	287	14	-12	5	119	33	51
H,L=	2,	-2	6	40	78	34*	1	345	17	8	4	219	15	-5	H,L=	3,	7		
02567	26	170	H,L=	2,	5	2	160	14	-12	5	353	11	-2	1	74	51	16		
1	472	13	-19	1	249	16	-11	3	0	72	-24*	6	120	24	20	2	185	21	11
2	354	11	-11	2	175	12	-4	4	130	21	-2	7	53	63	34*	3	213	23	36
3	285	5	5	3	95	25	-25	5	235	16	-7	H,L=	3,	0	4	19105	5*		
4	52	62	2*	4	72	54	1	H,L=	3,-7	0	69137	-19*	H,L=	3,	8				
5	102	25	-25	5	309	14	8	1	410	9	-1	1	476	9	-7	0	159	13	25
6	111	32	13	6	0	61	-33*	2	113	17	11	2	811	11	-5	1	376	13	16
7	168	33	18	H,L=	2,	6	3	218	12	2	3	242	10	-1	2	101	55	4	
H,L=	2,	-1	0	286	8	-2	4	124	47	-38	4	458	7	9	3	0	81	-18*	
11127	11	-15	1	149	19	12	5	76	25	47	5	207	25	2	4	0	61	-18*	
2	172	35	-25	2	268	11	16	6	0	66	-2*	6	84	96	12*	H,L=	3,	9	
3	107	12	3	3	160	9	13	H,L=	3,-6	7	143	28	26	1	205	17	33		
4	265	6	-1	4	353	15	-11	0	90	91	-30*	H,L=	3,	1	2	141	39	-17	

STRUCTURE FACTORS CONTINUED FOR
THE NORBORNANE DERIVATIVE [C9 H14 O3].

K	FOB	SG	DEL	K	FOB	SG	DEL	K	FOB	SG	DEL	K	FOB	SG	DEL	K	FOB	SG	DEL							
3	166	57	21	4	90	48	3	H,L=	4,	4		3	128	62	-4	1	0	52	-29*							
	H,L=	3,	10	5	83	29	6	0	490	12	-6	4	120	62	12	2	200	7	-3							
0	188	29	-17	6	106	65	16	1	241	7	-10	5	0	71	-69*	3	510	7	-3							
	H,L=	4,-	12	H,L=	4,	-3	2	24	58	10*	H,L=	5,	-7	4	12111	-37*	4	12111	-37*							
0	215	16	8	1	191	8	-3	3	186	22	-11	1	121	31	13	5	84100	63*	5	84100	63*					
1	149	20	-1	2	443	9	3	4	121	20	64	2	244	16	-6	6	122	31	29							
2	129	25	2	3	510	9	4	5	205	16	-19	3	51	75	-15*	H,L=	5,	1	1	295	9	-0				
	H,L=	4,-	11	4	118	32	21	6	91107	60*	4	145	43	35	5	144	33	-14	2	336	8	2				
1	148	20	-5	5	120	50	18	H,L=	4,	5	5	144	33	-14	6	117	18	-11	3	0	86	-4*				
2	111	16	-0	6	104	28	-3	1	218	33	-14	H,L=	5,	-6	4	99	29	-1	4	99	29	-1				
3	132	27	11	H,L=	4,	-2	2	276	23	-23	0	216	11	3	5	51	61	19*	5	51	61	19*				
	H,L=	4,-	10	0	225	14	4	3	196	24	54	1	967	10	4	6	148	70	19	H,L=	5,	2	6	148	70	19
0	254	16	19	1	56103	-40*	4	152	61	8	2	177	23	-25	0	38	72	7*	0	38	72	7*				
1	325	18	13	2	627	10	-0	H,L=	4,	6	3	122	17	7	4	92	93	27*	1	338	14	-8				
2	50	99	-58*	3	259	16	-2	0	51	70	30*	4	92	93	27*	5	82	90	33*	2	393	11	8			
3	458	8	-2	4	59	69	51*	1	590	9	-4	5	82	90	33*	6	82	47	48	3	179	18	-3			
4	198	39	-26	5	275	17	10	2	235	10	7	H,L=	5,	-5	4	234	10	3	4	234	10	3				
	H,L=	4,-	9	6	0	67	-39*	3	264	10	-1	1	110	19	23	5	82	89	-21*	5	82	89	-21*			
1	101	43	8	7	113	25	20	4	61103	-4*	2	41	74	17*	6	78	89	77*	H,L=	5,	3	6	78	89	77*	
2	179	12	-16	H,L=	4,	-1	5	34	88	-39*	3	103	27	22	1	0	66	-39*	1	0	66	-39*				
3	62	93	17*	1	113	55	-24	H,L=	4,	7	4	25	86	15*	2	59	63	51*	2	59	63	51*				
4	59	70	-26*	2	272	9	1	1	224	8	-6	5	38	75	14*	3	63	89	7*	3	63	89	7*			
5	256	28	-19	3	390	11	9	2	45	92	-21*	6	230	16	-21	4	62	94	-57*	4	62	94	-57*			
	H,L=	4,-	8	4	186	16	5	3	51	85	10*	H,L=	5,	-4	5	122	26	27	5	122	26	27				
0	212	11	-10	5	55	65	15*	4	39	99	-34*	0	720	8	7	0	269	7	1	0	269	7	1			
1	388	13	-8	6	64	82	-3*	H,L=	4,	8	1	225	13	6	1	152	20	-10	1	152	20	-10				
2	209	16	-10	7	77100	62*	0	122	24	12	2	110	27	-6	2	211	14	7	2	211	14	7				
3	105	75	14	H,L=	4,	0	1	257	15	2	3	67	79	1*	3	105	24	27	3	105	24	27				
4	395	16	1	0	563	7	-8	2	224	25	5	4	0	84	-7*	4	140	17	28	4	140	17	28			
5	178	19	2	1	437	6	-4	3	52	76	8*	5	172	14	-3	5	0	68	-3*	5	0	68	-3*			
	H,L=	4,-	7	2	233	15	24	H,L=	4,	9	6	48	60	-19*	H,L=	5,	5	H,L=	5,	5	H,L=	5,	5			
1	381	17	-6	3	392	5	1	1	76	41	23	H,L=	5,	-3	1	232	5	1	1	72	86	33*				
2	77	86	18*	4	264	17	9	H,L=	5,-	12	0	236	16	-2	2	235	17	7	2	90	32	-67				
3	33	82	-8*	5	132	14	20	0	236	16	-2	1	93120	-6*	3	129	15	18	3	125	42	9				
4	279	17	-9	6	129	25	-19	2	138	16	11	2	138	16	11	4	154	13	7	4	52	75	-8*			
5	184	13	-4	H,L=	4,	1	1	29	65	-4*	H,L=	5,-	11	5	100	23	16	5	61	73	-21*					
6	79	58	25	1	29	65	-4*	2	52	73	-1*	1	130	25	-30	6	228	9	6	H,L=	5,	6	H,L=	5,	6	
	H,L=	4,-	6	2	52	73	-1*	3	0	75	-14*	2	102121	27*	H,L=	5,	-2	0	89100	3*	0	583	8	-11		
0	107	41	-10	3	0	75	-14*	4	30	54	-4*	3	70	48	6	0	89100	3*	1	108	23	43				
1	445	13	-5	4	30	54	-4*	5	405	12	-5	H,L=	5,-	10	1	206	10	-6	1	108	23	43				
2	626	9	9	5	405	12	-5	6	81	44	60	0	615	8	2	2	261	12	7	2	223	13	-8			
3	16	91	-9*	6	81	44	60	H,L=	4,	2	1	138	30	-2	3	414	8	-0	3	36	66	28*				
4	97	37	26	H,L=	4,	2	0	615	8	2	2	326	7	-6	4	186	15	11	4	75	88	0*				
5	37110	-12*	0	305	16	-2	1	949	10	7	3	195	19	4	5	153	20	28	H,L=	5,	7	H,L=	5,	7		
6	23	59	-2*	1	949	10	7	2	98	19	12	4	77	92	28*	6	179	15	27	1	73	79	21*			
	H,L=	4,-	5	2	98	19	12	3	248	8	-0	H,L=	5,	-9	1	299	8	9	2	0	69	-74*				
1	218	10	-4	3	248	8	-0	4	178	11	-25	2	233	8	-10	3	70	83	64*	3	70	83	64*			
2	268	7	3	4	178	11	-25	5	307	10	4	1	84	99	1*	2	67	72	6*	H,L=	5,	8	H,L=	5,	8	
3	250	17	14	5	307	10	4	6	60	44	17	4	105118	2*	3	133	12	6	0	76	64	17				
4	58	68	-38*	6	60	44	17	H,L=	4,	3	5	94	51	-15	4	75	77	14*	1	56	78	-3*				
5	0	70	-33*	H,L=	4,	3	1	618	8	-1	H,L=	5,	-8	5	354	9	-9	2	93	73	14					
6	9	111	4*	1	618	8	-1	2	154	22	-1	0	133	25	35	6	80	82	50*	H,L=	6,-	12	H,L=	6,-	12	
	H,L=	4,-	4	2	154	22	-1	3	257	14	4	1	342	10	10	H,L=	5,	0	0	275	48	-25				
1	440	8	3	3	257	14	4	4	122	14	-5	2	284	8	-1	0	430	14	16	1	169	22	20			
2	939	10	9	4	122	14	-5	5	248	19	19	0	133	25	35	1	342	10	10	1	169	22	20			
3	324	7	-4	5	248	19	19	6	81	96	67*	2	284	8	-1	0	430	14	16	1	169	22	20			

STRUCTURE FACTORS CONTINUED FOR
THE NORBORNANE DERIVATIVE (C9 H14 O3).

K	FOB	SG	DEL	K	FOB	SG	DEL	K	FOB	SG	DEL	K	FOB	SG	DEL	K	FOB	SG	DEL
2	61	75	28*	4	372	14	8	H,L=	6,	6		2	103	31	-31	4	108	29	19
	H,L=	6,	-11	5	66	93	-10*	0	183	19	-7	3	79	47	57		H,L=	7,	5
1	84	89	-16*	6	127	22	-41	1	160	27	-46	4	101	42	-10	1	123	40	12
2	97	115	-25*		H,L=	6,	-2	2	130	27	3	5	84	99	22*	2	50	90	42*
3	35	78	-14*	0	210	21	-5	3	58	73	38*	6	167	12	12	3	62	74	51*
	H,L=	6,	-10	1	302	6	2		H,L=	6,	7		H,L=	7,	-3		H,L=	7,	6
0	66	27	18	2	106	11	16	1	132	18	2	1	161	31	8	0	226	8	17
1	81	27	53	3	437	6	-5	2	101	16	72	2	416	7	-9	1	67	44	30
2	69	82	67*	4	312	16	-6		H,L=	7,	-12	3	156	26	6	2	22	63	18*
3	35	58	2*	5	55	70	7*	0	271	22	-1	4	245	13	-1		H,L=	8,	-12
4	73	86	-35*	6	53	64	-2*	1	89	22	77	5	70	98	58*	0	111	51	6
	H,L=	6,	-9		H,L=	6,	-1	2	98	49	47	6	66	89	-40*	1	155	61	-7
1	93	30	-2	1	308	7	-1		H,L=	7,	-11		H,L=	7,	-2		H,L=	8,	-11
2	73	74	15*	2	41	48	-10*	1	123	28	-6	0	200	20	3	1	69	51	25
3	74	96	-3*	3	355	8	-10	2	212	14	-31	1	277	11	-3	2	83	40	48
4	210	9	8	4	158	13	10	3	134	32	-23	2	89	50	-11	3	74	88	40*
5	203	10	24	5	194	12	1		H,L=	7,	-10	3	256	15	-4		H,L=	8,	-10
	H,L=	6,	-8	6	110	15	84	0	100	42	14	4	292	24	10	0	230	23	13
0	43	69	25*		H,L=	6,	0	1	223	9	-8	5	79	93	65*	1	141	22	4
1	323	7	4	0	599	7	6	2	41	97	20*	6	72	76	28*	2	31	56	18*
2	435	13	-3	1	117	26	24	3	124	19	16		H,L=	7,	-1	3	216	39	4
3	450	14	-9	2	255	9	14	4	99	22	-11	1	180	14	2		H,L=	8,	-9
4	149	17	28	3	129	16	16		H,L=	7,	-9	2	32	54	31*	1	358	8	-10
5	150	18	14	4	222	16	-20	1	244	12	10	3	291	9	-17	2	260	17	-13
	H,L=	6,	-7	5	33	59	28*	2	187	29	-24	4	344	21	1	3	196	21	-8
1	436	12	-3	6	106	35	-12	3	0	66	-16*	5	108	28	74	4	0	60	-50*
2	12	53	-15*		H,L=	6,	1	4	234	39	-2	6	150	20	18		H,L=	8,	-8
3	68	83	31*	1	110	36	6		H,L=	7,	-8		H,L=	7,	0	0	423	8	18
4	17	63	14*	2	131	19	2	0	426	11	-6	0	124	15	0	1	233	20	-10
5	0	78	-4*	3	122	19	-23	1	90	44	2	1	72	74	-18*	2	207	30	-17
	H,L=	6,	-6	4	286	14	-5	2	145	41	9	2	139	12	-1	3	146	32	-5
0	487	6	2	5	98	50	-10	3	185	16	-8	3	205	14	-16	4	202	10	13
1	319	12	16	6	138	40	30	4	9	90	-9*	4	185	39	1		H,L=	8,	-7
2	626	8	6		H,L=	6,	2	5	48	63	38*	5	71	84	68*	1	247	10	-1
3	54	60	13*	0	259	8	2		H,L=	7,	-7		H,L=	7,	1	2	78	41	-1
4	104	29	-15	1	461	11	10	1	0	52	-26*	1	88	20	-6	3	89	98	-33*
5	57	70	1*	2	277	6	8	2	72	26	50	2	0	68	-51*	4	367	8	-3
6	42	73	35*	3	397	16	14	3	70	42	64	3	228	27	9	5	99	25	6
	H,L=	6,	-5	4	32	70	29*	4	282	19	7	4	82	96	-9*		H,L=	8,	-6
1	43	49	41*	5	47	63	15*	5	36	60	26*	5	192	27	21	0	34	58	18*
2	320	12	2		H,L=	6,	3		H,L=	7,	-6		H,L=	7,	2	1	218	23	8
3	218	46	22	1	349	12	-5	0	79	33	28	0	114	60	16	2	0	87	-14*
4	341	8	7	2	204	29	-19	1	150	17	33	1	74	88	9*	3	320	10	-12
5	109	16	-18	3	127	22	45	2	35	64	-1*	2	70	83	-15*	4	89	97	-7*
6	180	17	6	4	45	63	-61*	3	66	49	17	3	316	16	1	5	162	17	-3
	H,L=	6,	-4	5	0	61	-10*	4	109	76	2	4	130	22	-15		H,L=	8,	-5
0	43	62	-8*		H,L=	6,	4	5	73	87	3*	5	142	59	29	1	0	64	-33*
1	611	8	4	0	168	12	-6		H,L=	7,	-5		H,L=	7,	3	2	181	14	-6
2	121	17	-12	1	773	13	5	1	30	50	-29*	1	129	24	12	3	199	20	-10
3	192	8	4	2	79	84	-3*	2	54	64	41*	2	0	68	-13*	4	204	24	5
4	260	11	-12	3	249	12	-3	3	113	23	6	3	150	27	3	5	119	17	-3
5	70	43	-13	4	0	75	-47*	4	79	65	-20	4	18	60	-70*		H,L=	8,	-4
6	84	104	12*		H,L=	6,	5	5	105	36	31		H,L=	7,	4	0	386	31	3
	H,L=	6,	-3	1	141	36	-33	6	34	68	-14*	0	266	13	1	1	249	14	-1
1	150	19	0	2	59	70	-6*		H,L=	7,	-4	1	57	74	-44*	2	86	103	21*
2	366	6	8	3	85	102	83*	0	156	16	-25	2	148	13	5	3	115	44	5
3	357	7	4	4	91	109	85*	1	82	22	11	3	0	58	-41*	4	290	10	-7

STRUCTURE FACTORS CONTINUED FOR
THE NORBORNANE DERIVATIVE [C9 H14 O3].

K	FOB	SG	DEL	K	FOB	SG	DEL	K	FOB	SG	DEL	K	FOB	SG	DEL	K	FOB	SG	DEL								
5	69	42	37	2	35	67	-43*	2	319	21	-13	1	96	86	22					H,L=	11,	-2					
	H,L=	8,	-3	3	0	61	-41*	3	194	20	2	2	98117	20*		0	76	81	11*								
1	51	67	-27*		H,L=	9,	-9	4	37	59	-29*	3	225	11	-12	1	192	30	-0								
2	141	11	-4	1	105	30	-23		H,L=	9,	1	4	64	77	64*	2	246	35	11								
3	403	9	-18	2	54	65	30*	1	53	57	42*		H,L=	10,	-2	3	109	32	30								
4	13	79	-19*	3	67	80	29*	2	267	9	0	0	158	11	-1		H,L=	11,	-1								
5	59	73	40*	4	130	39	-11	3	79	98	-9*	1	321	8	-2	1	151	39	8								
	H,L=	8,	-2		H,L=	9,	-8	4	28	80	25*	2	167	17	19	2	185	15	-0								
0	109	21	-20	0	35	89	30*		H,L=	9,	2	3	140	18	35		H,L=	11,	0								
1	530	9	-7	1	213	8	9	0	217	9	1	4	58	88	28*	0	123	93	10								
2	0	54	-35*	2	73	44	21	1	230	21	38		H,L=	10,	-1	1	224	15	12								
3	261	18	2	3	79101	8*		2	0109	-57*		1	67	31	-2		H,L=	12,	-8								
4	296	11	18	4	65107	56*		3	91	27	55	2	158	18	-4	0	74	75	40*								
5	209	25	-17		H,L=	9,	-7		H,L=	9,	3	3	78	85	-54*	1	88104	20*									
	H,L=	8,	-1	1	98	23	-19	1	62	80	29*		H,L=	10,	0		H,L=	12,	-7								
1	199	21	-11	2	80	48	13	2	94	82	26	0	156	14	-4	1	13	82	9*								
2	78	43	18	3	116	21	-9		H,L=	9,	4	1	450	17	-8		H,L=	12,	-6								
3	348	9	-3	4	69	82	-7*	0	93	24	-22	2	181	14	-15	0	110	28	40								
4	134	33	8		H,L=	9,	-6	1	113	30	15	3	133	15	-14	1	46	78	-14*								
5	0	62	-20*	0	122	26	-13		H,L=	10,	-11		H,L=	10,	1	2	116	68	19								
	H,L=	8,	0	1	149	26	-5	1	96	29	-11	1	193	15	-0		H,L=	12,	-5								
0	46	66	18*	2	54	64	23*		H,L=	10,	-10	2	58	69	16*	1	113	48	-8								
1	36	56	-21*	3	157	26	14	0	351	15	-5		H,L=	10,	2	2	63	91	-0*								
2	146	18	5	4	0	78	-39*	1	207	18	15	0	141	18	33		H,L=	12,	-4								
3	311	11	-1		H,L=	9,	-5	2	30	72	-9*	1	51	93	-19*	0	51	62	9*								
4	170	56	9	1	63	99	14*		H,L=	10,	-9		H,L=	11,	-10	1	64	76	3*								
5	114	29	21	2	48	72	39*	1	322	17	2	0	111	19	-5		H,L=	12,	-3								
	H,L=	8,	1	3	161	16	-1	2	0	58	-2*	1	12	87	-46*	1	114	62	28								
1	238	7	10	4	107	19	8	3	132	33	4		H,L=	11,	-9												
2	204	20	16	5	105	91	-11		H,L=	10,	-8	1	91109	24*													
3	115	14	1		H,L=	9,	-4	0	302	18	-7	2	64	77	28*												
4	70	83	48*	0	181	19	-10	1	214	17	-10		H,L=	11,	-8												
	H,L=	8,	2	1	336	7	2	2	0	88	-11*	0	112	28	10												
0	290	11	-23	2	107107	-27*		3	82	69	5	1	254	27	-14												
1	118	26	17	3	186	23	-19		H,L=	10,	-7	2	72	85	45*												
2	112	15	8	4	194	22	26	1	86	42	53		H,L=	11,	-7												
3	66	32	-10	5	0	73	-2*	2	165	34	22	1	35	91	30*												
4	39	87	14*		H,L=	9,	-3	3	26	84	10*	2	296	37	-35												
	H,L=	8,	3	1	132	32	12	4	66	85	30*	3	108115	-1*													
1	127	28	1	2	21	87	-34*		H,L=	10,	-6		H,L=	11,	-6												
2	96	34	62	3	170	18	3	0	296	15	3	0	104	33	1												
3	68	90	50*	4	112	84	18	1	325	16	5	1	475	12	-13												
	H,L=	8,	4	5	62	74	18*	2	226	30	-3	2	117	49	23												
0	0	58	-41*		H,L=	9,	-2	3	119	28	-33	3	101	31	16												
1	35	58	-35*	0	134	20	4	4	246	19	-3		H,L=	11,	-5												
2	125	26	14	1	270	11	-10		H,L=	10,	-5	1	85	31	-23												
3	151	36	48	2	79	94	-30*	1	0	87	-29*	2	85100	-6*													
	H,L=	8,	5	3	0	62	-32*	2	87	94	27*	3	36	68	15*												
1	31	72	-51*	4	152	40	2	3	217	9	3		H,L=	11,	-4												
	H,L=	9,	-12		H,L=	9,	-1	4	36	61	-36*	0	53	63	8*												
0	61	73	-11*	1	89	36	-16		H,L=	10,	-4	1	99	30	1												
	H,L=	9,	-11	2	53	72	52*	3	250	12	0	2	37	73	-51*												
1	115	42	18	3	151	22	-20	1	218	15	24	3	49	67	19*												
2	178	25	-6	4	66	84	4*	2	95	30	39		H,L=	11,	-3												
	H,L=	9,	-10		H,L=	9,	0	3	89105	16*		1	99	46	6												
0	207	20	15	0	175	21	-10	4	139	43	-13	2	30	96	-8*												
1	152	24	37	1	59	64	32*		H,L=	10,	-3	3	48	70	-5*												

This report was done with support from the United States Energy Research and Development Administration. Any conclusions or opinions expressed in this report represent solely those of the author(s) and not necessarily those of The Regents of the University of California, the Lawrence Berkeley Laboratory or the United States Energy Research and Development Administration.

TECHNICAL INFORMATION DIVISION
LAWRENCE BERKELEY LABORATORY
UNIVERSITY OF CALIFORNIA
BERKELEY, CALIFORNIA 94720