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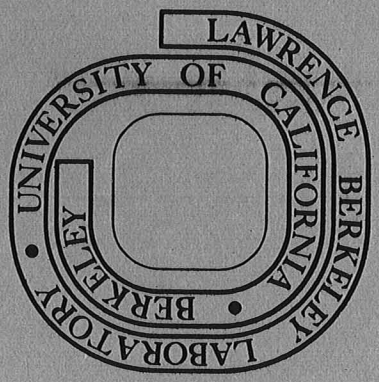

SYNTHESIS AND CRYSTAL STRUCTURE OF A NEODYMIUM ISOPROPOXIDE CHLORIDE, $Nd_6[OCH(CH_3)_2]_{17}Cl$[1]

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ABSTRACT

Neodymium (III) chloride reacts with sodium isopropoxide in isopropyl alcohol to produce a complex which has been characterized by an x-ray crystal structure determination to be hexa-isopropoxy-nona(μ_2-isopropoxy)-di-(μ_3-isopropoxy)-(μ_6-chloro-hexa-neodymium), $Nd_6[OCH(CH_3)_2]_{17}Cl$. The pale blue crystals are monoclinic, space group $P2_1/n$ with cell dimensions $\underline{a}$ = 24.52(2) Å, $\underline{b}$ = 22.60(2) Å, $\underline{c}$ = 14.22(1) Å, and β = 101.05(5)°; for four molecules in the unit cell the calculated density is 1.636 gm/cc. The structure was refined by full-matrix least-squares to a conventional R factor of 0.076 for 2327 data with $I > 2\sigma$. The six neodymium atoms form a trigonal prism centered about the chloride atom. Six isopropoxide groups are terminal, nine are edge bridging, and two are bridging a trigonal face of the prism yielding six two-coordinate, nine three-coordinate, and two four-coordinate oxygen atoms, respectively.

The average Nd-Cl distance is 3.05(1) Å. The average Nd-O distances for oxygen atoms which are bonded to one, two, and three Nd atoms are 2.05(2) Å, 2.36(4) Å, and 2.45(5) Å, respectively.

INTRODUCTION

Neodymium tri-isopropoxide, prepared from neodymium trichloride and sodium isopropoxide in refluxing isopropyl alcohol, is said to be monomeric in benzene solution (ebullioscopically) as is the praseodymium analogue.[2,3] In contrast, gadolinium and erbium isopropoxides are tetrameric in benzene.[4] The samarium[5] and ytterbium[6] compounds are also known though their solution molecular weights have not been reported. Mass spectrometric examination of $M(O\text{-}i\text{-}Pr)_3$ [M - Nd, Er, Tb, and Lu], prepared from the metal and alcohol, show tetrameric ions in gas phase.[7]

It has been said that preparation of isopropoxides of the lanthanide elements from sodium isopropoxide and metal chloride results in materials that are contaminated by chloride though nothing was known about their consitution.[7,8] We have carried out a single crystal x-ray analysis of the chloride-containing material and have shown it to be $Nd_6(O\text{-}i\text{-}Pr)_{17}Cl$.

EXPERIMENTAL

Microanalysis was by Analytical Laboratories, University of California, Berkeley. Isopropyl alcohol was dried by refluxing over and distilling from magnesium isopropoxide. Neodymium trichloride was dried by refluxing with thionyl chloride. The magnetic susceptibility was measured with a PAR model 155 vibrating sample magnetometer and

was calibrated with $HgCo(CNS)_4$.[9] Temperature was measured with a calibrated GaAs diode.

Heptadecaisopropoxychlorohexaneodymium (III). Sodium isopropoxide was prepared from sodium (1.3 g-atom, 0.055 mole), isopropyl alcohol (20 ml), and benzene (40 ml); it was then added to a gently refluxing solution of neodymium trichloride (4.6 g, 0.018 mole) in isopropyl alcohol (40 ml). The suspension was refluxed for 12 h then centrifuged. The light blue mother liquor was filtered and the residue was washed with benzene (2 x 25 ml). The combined extracts were evaporated to dryness in vacuum. The blue solid was crystallized from toluene (-15°) as light blue needles. Yield was 6.2 g. The compound did not melt nor decompose when heated in a sealed capillary to 300°. Anal. Calcd for $C_{51}H_{119}ClNd_6O_{17}$; C, 32.2; H, 6.25; Cl, 1.86. Found: C, 31.8; H, 6.04; Cl, 1.80.

X-Ray Diffraction. The pale blue crystals were transferred to quartz capillaries inside of an argon filled dry box and sealed with vacuum grease. The capillaries were fire-sealed immediately upon removal from the box. Weissenberg photography showed the material to be monoclinic, and rough cell dimensions were obtained. A crystal was mounted on a Picker FACS-I automated diffractometer equipped with a graphite monochromator and molybdenum tube. The cell dimensions were obtained by a least-squares procedure from the angular settings of 12 manually centered reflections for which

the 2θ values were between 29° and 32°. The space group and cell dimensions are given in Table I with some other details of the experiment. Omega scans of several low angle reflections showed widths at half-peak height of about 0.25°. Using the θ-2θ scan technique, a total of 10397 scans, including standards, were measured and later averaged to give a set of 4920 unique data of which 2137 had $F^2 > 2\sigma$. Three standard reflections were measured after each 200th scan to monitor for crystal decay, instrumental stability and crystal alignment. A decay of about 15% was observed in the intensities of all three standard reflections, and the data were adjusted accordingly.

No absorption correction was made because the crystal faces were too indistinct to measure. Azimuthal scans of a few reflections indicated variations in intensities of about 10% from the average. The data were processed, averaged, and given estimated standard deviations using formulas presented in the Supplementary Material. The factor $p = 0.06$ was used in the calculation of $\sigma(F^2)$.

The full-matrix least squares program used minimizes the function $\Sigma w(\Delta F)^2/\Sigma wF_o^2$. Scattering factors for Nd were taken from Cromer and Waber,[10] and those for Cl, C and O from Doyle and Turner;[11] dispersion corrections used were from Cromer and Liberman.[12]

Structure Determination. The positions of the six Nd atoms, at the corners of a regular trigonal prism, were deduced from a three-dimensional Patterson function calculation. A least-squares refine-

ment of the Nd atoms followed by a difference-Fourier calculation revealed the positions of 18 additional atoms which were presumed to be oxygen atoms. One of these atoms occupied the center of the trigonal prism and was equidistant from all six Nd atoms. Refinement of the 6 Nd atoms and the 18 oxygen atoms yielded a negative temperature parameter for the atom at the prism center. When this atom was assumed to be a chlorine atom, derived from the $NdCl_3$ in the synthesis, further refinement resulted in comparable thermal parameters for all the atoms. The presence of chlorine was confirmed by a chemical test using silver nitrate and by the analysis reported above. Least-squares calculations and difference-Fourier maps were used to determine the locations of the 51 carbon atoms. The carbon atoms were not well resolved, due to the paucity of high angle data; and although most of the carbon atoms refined to reasonable positions, some did not. To handle this poor resolution problem, restraints were imposed on the interatomic distances as suggested by Waser.[13] In this method, interatomic distances between selected atoms are introduced into the least-squares calculations and treated as observations; estimated standard deviations of these distances are also introduced and used to calculate the weights. Except that the derivatives are calculated by a special patch and these "observations" are not included in the R values reported here, these terms are included in the least-squares calculation in the same manner as observed structure factors. This procedure allows the structure to adjust to the electron density with a flexibility governed by

the weighting. The isopropoxide carbon atoms were restrained by the following distances; O-C (nearest neighbor) to 1.44 ± 0.06 Å, O-C (2nd neighbor) to 2.42 ± 0.1 Å, C-C (nearest neighbor) to 1.52 ± 0.03 Å and C-C (2nd neighbor) to 2.48 ± 0.1 Å. These distances impose tetrahedral bond angles on this isopropoxide group, but permit rotation about the O-C bond. To promote faster convergence of the structure, the isotropic thermal parameters of the two terminal carbon atoms from each isopropoxide group were constrained to a single value. No extinction was indicated, and no correction for it was made. Because of some large weighted residuals at low angles, all 87 data for $\sin\theta/\lambda < .127$ were zero weighted.

The final structure with R indices as given in Table I and parameters as shown in Table II is partially shown in Fig. 1. In the last cycle the largest shift of a parameter was 0.19 σ. The largest peak in the final difference Fourier was 1.5 e/Å^3. Hydrogen atoms were not observed and not included in the calculations. A list of distances is given in Table III, with atoms numbered as in Fig. 1.

DISCUSSION

The neodymium atoms are at the corners of a very nearly regular trigonal prism in which the triangular edges average 3.808 ± .006 Å and the axial edges average 4.230 ± .010 Å. All of the angles in the triangular faces are within 0.1° of 60°. Because of a slight

twist of the triangular faces with respect to each other about the prism axis, the angles are about one degree from 90° for the three quadrilateral faces. The cause of this minor distortion is unknown; perhaps it is a result of some steric effects of the isopropoxide ligands. The chloride ion is equidistant from the six Nd atoms at a distance of 3.05 ± .01 Å, and is perhaps the stabilizing factor for this remarkable cluster of atoms.

There are three types of oxygen-Nd bonds. Each Nd atom is bonded singly to an isopropoxide ligand with an average Nd-O distance of 2.05 ± .02 Å. A bridging isopropoxide ligand bonds 2 Nd atoms at each edge of the prism to give eighteen Nd-O bond lengths that average 2.36 ± 0.04 Å. The isopropoxide ligands which are centered on the triangular faces bond to three Nd atoms with an average bond length of 2.45 ± .05 Å.

The molecular packing resembles the hexagonal closest packing of spheres. The globular complexes with centers near y = 1/4 form a layer in which each cluster has six neighbors, and a similar layer occurs at y = 3/4. The stacking of these layers is according to the ABAB sequence of hexagonal closest packing. This description is imperfect because the molecules are not spherical, and Cl-Cl distances for the twelve nearest neighbors range from 12.94 to 16.34 Å.

The magnetic susceptibility of the complex followed the Curie-Weiss equation $\chi = \frac{C_M}{T + \Theta}$ in the temperature range 7.5° - 100° K. The magnetic moment, μ_{eff}, was 3.22 B.M. per neodymium atom with Θ = -2.8° K and C_M = 1.293.

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Supplementary Material Available: A list of selected angles, data processing formulas and listing of observed structure factors (32 pages). Ordering information is given in any current masthead page.

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Table I. Summary of Crystal Data and Intensity Collection

Compound	$Nd_6[OCH(CH_3)_2]_{17}Cl$
Formula Weight	1905.4
a (Å)	24.52(2)
b (Å)	22.60(2)
c (Å)	14.22(1)
β (deg)	101.05(5)
V	7736 $Å^3$
Z	4
Density (calc, gm/cm^3)	1.636
Space Group [a]	$P2_1/n$ (alternate setting of $P2_1/a$)
Crystal Shape and Size (mm)	Roundish fragment; .25 x .15 x .20
Temperature (deg C)	21
Radiation	MoKα(λ = 0.70926 and 0.71354 Å), monochromated from (002) face of mosaic graphite
μ (cm^{-1})	40.5
Data Collection Method	θ-2θ scan (1°/min along 2θ)
Scan Range (deg. 2θ)	0.9° below $K\alpha_1$ to 0.9° above $K\alpha_2$
Background Counts	8 sec. Background offset from scan limits by 0.12° 2θ
Two-theta limits (deg)	3.5 - 40
Final No. of Variables	314
Unique Data Used $F_o^2 > 2\sigma$; .127 < 2θ < .482	2327

Table I. Continued

No. Distance Restraints	102
R_w [b]	0.074
R [c] (2327 data used in R_w)	0.076
R (all 4920 data)	0.239
Goodness of Fit	1.36

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[a] The general positions are $\pm(x,y,z;\ 1/2 + x,\ 1/2 - y,\ 1/2 + z)$.

[b] $R_w = [\Sigma w(|F_o|-|F_c|)^2/\Sigma w|F_o|^2]^{1/2}$.

[c] $R = \Sigma||F_o|-|F_c||/\Sigma|F_o|$.

Table II. Parameters for $Nd_6(OCH(CH_3)_2]_{17}Cl$

ATOM	x	y	z	B
Nd(1)	.3206(1)	.1954(2)	.2153(2)	*
Nd(2)	.4709(1)	.1944(1)	.3476(2)	
Nd(3)	.3963(1)	.3410(1)	.2799(2)	
Nd(4)	.2624(1)	.2044(1)	.4756(2)	
Nd(5)	.4121(1)	.1893(1)	.6084(2)	
Nd(6)	.3487(1)	.3422(2)	.5512(2)	
O(1)	.286(1)	.164(2)	.083(2)	7.4(9)
O(2)	.540(2)	.159(2)	.303(3)	10.0(11)
O(3)	.415(1)	.405(2)	.189(3)	7.8(9)
O(4)	.190(1)	.176(2)	.518(2)	7.7(9)
O(5)	.443(2)	.146(2)	.732(3)	10.2(11)
O(6)	.338(1)	.405(2)	.649(3)	8.9(10)
O(7)	.394(1)	.130(2)	.282(2)	6.0(8)
O(8)	.479(1)	.301(1)	.360(2)	6.3(8)
O(9)	.311(1)	.300(1)	.201(2)	6.5(8)
O(10)	.334(1)	.136(2)	.542(2)	7.2(10)
O(11)	.430(1)	.292(1)	.619(2)	6.2(8)
O(12)	.258(1)	.305(1)	.474(2)	5.2(7)
O(13)	.253(1)	.180(1)	.311(2)	5.7(7)
O(14)	.476(1)	.166(1)	.508(2)	4.7(7)
O(15)	.371(2)	.387(1)	.415(3)	6.4(7)
O(16)	.410(1)	.247(1)	.212(2)	4.3(7)
O(17)	.327(1)	.246(1)	.611(2)	6.0(8)

Table II. Continued

Cl	.3681(5)	.2449(4)	.4132(9)	4.0(2)
C(1)	.270(3)	.122(3)	.006(5)	17.2(32)
C(2)	.305(4)	.088(4)	-.049(6)	17.3(21)
C(3)	.216(3)	.148(4)	-.047(6)	17.3
C(4)	.586(3)	.124(3)	.281(6)	14.9(26)
C(5)	.576(4)	.127(5)	.172(6)	21.4(27)
C(6)	.642(3)	.145(5)	.328(7)	21.4
C(7)	.431(5)	.443(4)	.116(7)	22.0(43)
C(8)	.472(6)	.488(6)	.16(1)	31.6(51)
C(9)	.377(6)	.468(7)	.06(1)	31.6
C(10)	.143(3)	.144(4)	.544(7)	18.6(34)
C(11)	.092(4)	.166(6)	.476(8)	23.0(29)
C(12)	.142(5)	.169(6)	.645(7)	23.0
C(13)	.459(3)	.129(4)	.831(4)	19.1(36)
C(14)	.441(3)	.066(3)	.843(6)	14.7(18)
C(15)	.519(3)	.141(4)	.872(5)	14.7
C(16)	.339(5)	.440(4)	.735(6)	22.4(42)
C(17)	.379(5)	.490(5)	.73(1)	26.7(39)
C(18)	.282(5)	.460(6)	.74(1)	26.7
C(19)	.397(3)	.067(2)	.288(4)	10.4(19)
C(20)	.339(3)	.039(3)	.256(5)	11.7(14)
C(21)	.435(2)	.042(3)	.227(5)	11.7
C(22)	.522(3)	.343(3)	.403(5)	12.6(23)
C(23)	.563(4)	.302(4)	.467(7)	19.7(25)

Table II. Continued

C(24)	.551(4)	.365(4)	.326(7)	19.7
C(25)	.260(3)	.333(3)	.164(5)	13.4(24)
C(26)	.265(5)	.399(4)	.163(8)	22.0(31)
C(27)	.231(5)	.302(5)	.074(7)	22.0
C(28)	.319(3)	.074(2)	.534(5)	12.3(22)
C(29)	.376(3)	.043(4)	.560(7)	18.0(22)
C(30)	.297(4)	.062(4)	.626(6)	18.0
C(31)	.481(2)	.320(3)	.663(5)	14.3(25)
C(32)	.484(4)	.385(4)	.638(7)	18.0(23)
C(33)	.501(4)	.302(4)	.764(6)	18.0
C(34)	.217(2)	.342(3)	.420(4)	11.7(22)
C(35)	.170(3)	.305(3)	.361(5)	13.4(17)
C(36)	.196(3)	.386(3)	.484(5)	13.4
C(37)	.207(3)	.148(3)	.252(6)	20.5(39)
C(38)	.198(3)	.094(3)	.305(6)	14.4(18)
C(39)	.164(3)	.193(3)	.212(5)	14.4
C(40)	.519(3)	.129(3)	.565(6)	20.1(38)
C(41)	.568(3)	.166(4)	.612(6)	17.3(22)
C(42)	.531(4)	.076(4)	.507(7)	17.3
C(43)	.370(3)	.450(2)	.404(6)	12.8(20)
C(44)	.421(3)	.483(3)	.448(6)	14.2(17)
C(45)	.315(3)	.477(3)	.410(6)	14.2
C(46)	.436(3)	.238(3)	.126(4)	12.9(23)
C(47)	.424(4)	.172(3)	.106(6)	17.7(22)

Table II. Continued

C(48)	.394(4)	.262(4)	.040(5)	17.7
C(49)	.309(3)	.246(4)	.702(4)	18.7(34)
C(50)	.254(3)	.278(3)	.696(5)	12.8(15)
C(51)	.349(3)	.275(3)	.782(5)	12.8

*ATOM	B_{11}[a]	B_{22}	B_{33}	B_{12}	B_{13}	B_{23}
Nd(1)	4.8(2)	8.4(2)	4.1(2)	-1.3(2)	.4(1)	-.5(2)
Nd(2)	4.2(2)	6.9(2)	5.3(2)	.5(1)	1.3(1)	-.1(2)
Nd(3)	6.2(2)	6.0(2)	5.3(2)	-.5(1)	1.6(1)	.8(1)
Nd(4)	4.1(2)	7.2(2)	5.3(2)	-.8(1)	1.4(1)	.6(1)
Nd(5)	5.1(2)	7.1(2)	4.2(2)	.7(2)	.2(1)	.5(1)
Nd(6)	5.7(2)	6.2(2)	5.5(2)	.3(1)	1.7(1)	-1.0(1)

[a]The form of the anisotropic temperature factor is

$$\exp[-0.25(h^2a^{*2}B_{11} + 2hka^*b^*B_{12} + \ldots)].$$

Table III. Interatomic Distances (Å) [a]

Cl	-Nd(1)	3.05(2)		-Nd(4)	2.27(3)
	-Nd(2)	3.07(2)	O(13)	-Nd(1)	2.36(3)
	-Nd(3)	3.05(2)		-Nd(4)	2.37(3)
	-Nd(4)	3.04(2)	O(14)	-Nd(2)	2.34(3)
	-Nd(5)	3.05(2)		-Nd(5)	2.38(3)
	-Nd(6)	3.05(2)	O(15)	-Nd(3)	2.36(4)
O(1)	-Nd(1)	2.03(4)		-Nd(6)	2.34(4)
O(2)	-Nd(2)	2.07(4)	O(16)	-Nd(1)	2.49(3)
O(3)	-Nd(3)	2.04(4)		-Nd(2)	2.51(3)
O(4)	-Nd(4)	2.07(4)		-Nd(3)	2.38(3)
O(5)	-Nd(5)	2.02(4)	O(17)	-Nd(4)	2.44(3)
O(6)	-Nd(6)	2.05(4)		-Nd(5)	2.44(3)
O(7)	-Nd(1)	2.38(4)		-Nd(6)	2.43(3)
	-Nd(2)	2.42(4)	Nd(1)	-Nd(2)	3.81(1)
O(8)	-Nd(2)	2.43(4)		-Nd(3)	3.80(1)
	-Nd(3)	2.31(4)	Nd(2)	-Nd(3)	3.82(1)
O(9)	-Nd(3)	2.38(3)	Nd(4)	-Nd(5)	3.81(1)
	-Nd(1)	2.37(4)		-Nd(6)	3.80(1)
O(10)	-Nd(4)	2.39(4)	Nd(5)	-Nd(6)	3.81(1)
	-Nd(5)	2.30(4)	Nd(1)	-Nd(4)	4.22(1)
O(11)	-Nd(5)	2.36(4)	Nd(2)	-Nd(5)	4.23(1)
	-Nd(6)	2.33(3)	Nd(3)	-Nd(6)	4.24(1)
O(12)	-Nd(6)	2.43(3)			

[a] O-C and C-C distances were restrained in the least-squares refinements and average to the values reported in the text.

FIGURE CAPTION

Fig. 1. ORTEP drawing of the Nd, Cl and O framework in $Nd_6[OCH(CH_3)_2]_{17}Cl$.

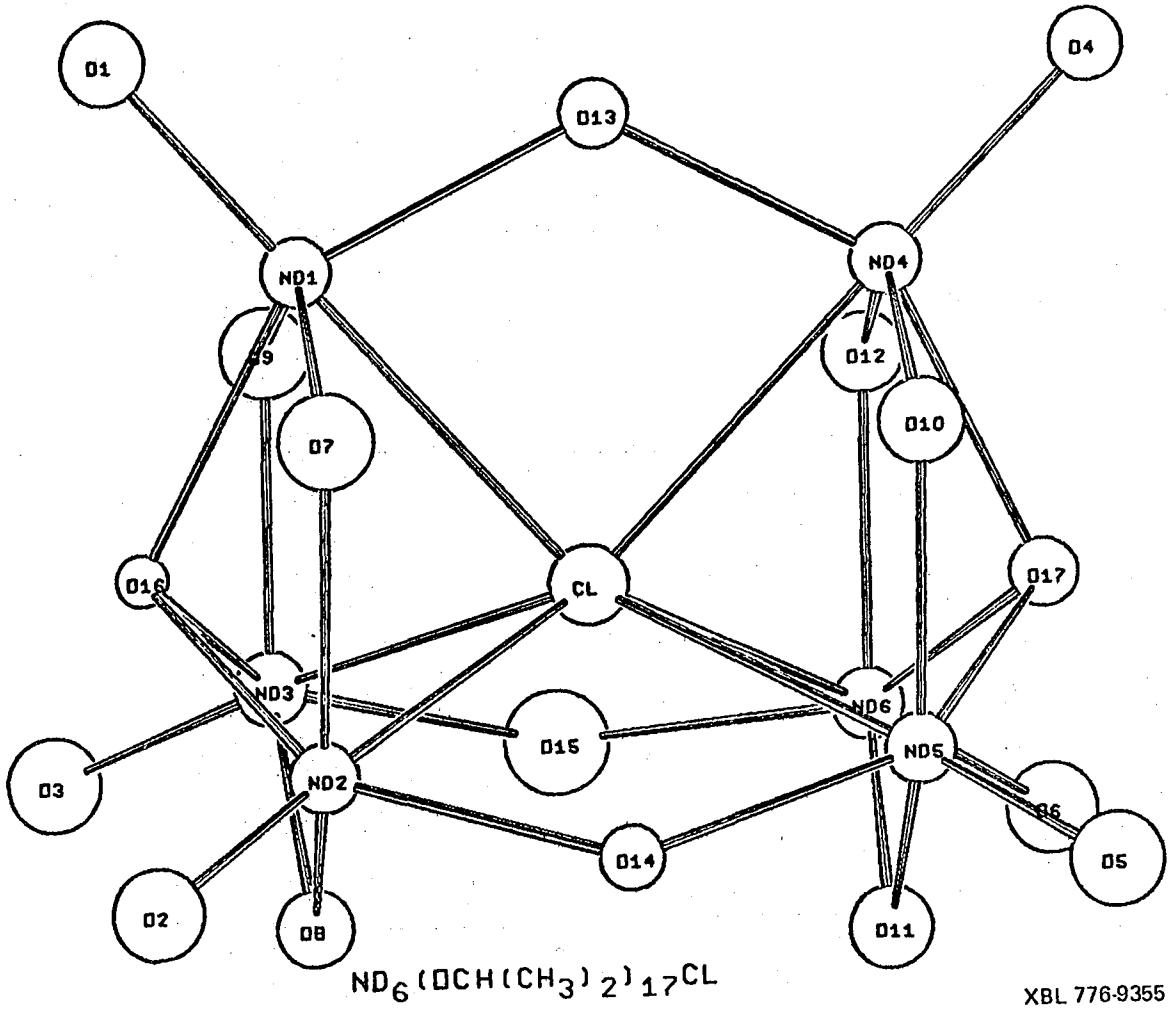
O1
O13
O4
ND1
ND4
O9
O12
O7
O10
O16
CL
O17
ND3
ND6
O15
ND5
O3
ND2
O6
O14
O5
O2
O8
O11
ND6(OCH(CH3)2)17CL
XBL 776-9355

Fig. 1

Table IV. Selected Angles (deg.)

Nd(2)-Nd(1)-Nd(3)	60.2(1)	Nd(1)-Cl -Nd(4)	88(1)
Nd(1)-Nd(2)-Nd(3)	59.9(1)	Nd(2)-Cl -Nd(5)	87(1)
Nd(1)-Nd(3)-Nd(2)	59.9(1)	Nd(3)-Cl -Nd(6)	88(1)
Nd(5)-Nd(4)-Nd(6)	60.1(1)	Nd(1)-Cl -Nd(5)	134(1)
Nd(4)-Nd(5)-Nd(6)	59.9(1)	Nd(2)-Cl -Nd(6)	135(1)
Nd(4)-Nd(6)-Nd(5)	60.0(1)	Nd(3)-Cl -Nd(4)	135(1)
Nd(2)-Nd(1)-Nd(4)	91.4(1)	Nd(1)-Cl -Nd(6)	141(1)
Nd(3)-Nd(1)-Nd(4)	88.8(1)	Nd(2)-Cl -Nd(4)	141(1)
Nd(3)-Nd(2)-Nd(5)	91.0(1)	Nd(3)-Cl -Nd(5)	141(1)
Nd(1)-Nd(2)-Nd(5)	88.5(1)	O(1) -Nd(1)-Cl	178(1)
N(1) -Nd(3)-Nd(6)	91.1(1)	O(2) -Nd(2)-Cl	179(1)
Nd(2)-Nd(3)-Nd(6)	88.8(1)	O(3) -Nd(3)-Cl	179(1)
Nd(5)-Nd(4)-Nd(1)	88.6(1)	O(4) -Nd(4)-Cl	180(1)
Nd(6)-Nd(4)-Nd(1)	91.4(1)	O(5) -Nd(5)-Cl	175(1)
Nd(6)-Nd(5)-Nd(2)	89.0(1)	O(6) -Nd(6)-Cl	177(1)
Nd(4)-Nd(5)-Nd(2)	91.2(1)	Nd(1)-O(7) -Nd(2)	105(2)
Nd(4)-Nd(6)-Nd(3)	88.4(1)	Nd(2)-O(8) -Nd(3)	107(2)
Nd(5)-Nd(6)-Nd(3)	90.9(1)	Nd(3)-O(9) -Nd(1)	106(2)
Nd(1)-Cl -Nd(2)	76.9(3)	Nd(4)-O(10)-Nd(5)	109(2)
Nd(1)-Cl -Nd(3)	77.2(3)	Nd(5)-O(11)-Nd(6)	109(2)
Nd(2)-Cl -Nd(3)	77.2(3)	Nd(6)-O(12)-Nd(4)	108(2)
Nd(4)-Cl -Nd(5)	77.4(3)	Nd(1)-O(13)-Nd(4)	126(2)
Nd(4)-Cl -Nd(6)	77.4(3)	Nd(2)-O(14)-Nd(5)	127(2)
Nd(5)-Cl -Nd(6)	77.4(3)	Nd(3)-O(15)-Nd(6)	128(2)

Table IV. Continued

Nd(1)-O(16)-Nd(2)	99(1)	O(5) -Nd(5)-O(14)	103(2)
Nd(2)-O(16)-Nd(3)	103(1)	O(5) -Nd(5)-O(17)	115(2)
Nd(3)-O(16)-Nd(1)	103(1)	O(6) -Nd(6)-O(11)	106(2)
Nd(4)-O(17)-Nd(5)	103(1)	O(6) -Nd(6)-O(12)	109(2)
Nd(5)-O(17)-Nd(6)	103(1)	O(6) -Nd(6)-O(15)	110(2)
Nd(6)-O(17)-Nd(4)	103(1)	O(6) -Nd(6)-O(17)	109(2)
O(1) -Nd(1)-O(7)	107(2)	Cl -Nd(1)-O(7)	74(1)
O(1) -Nd(1)-O(9)	105(2)	Cl -Nd(1)-O(9)	74(1)
O(1) -Nd(1)-O(13)	106(2)	Cl -Nd(1)-O(13)	73(1)
O(1) -Nd(1)-O(16)	111(2)	Cl -Nd(1)-O(16)	70(1)
O(2) -Nd(2)-O(7)	106(2)	Cl -Nd(2)-O(7)	74(1)
O(2) -Nd(2)-O(8)	110(2)	Cl -Nd(2)-O(8)	71(1)
O(2) -Nd(2)-O(14)	107(2)	Cl -Nd(2)-O(14)	73(1)
O(2) -Nd(2)-O(16)	110(2)	Cl -Nd(2)-O(16)	70(1)
O(3) -Nd(3)-O(8)	107(2)	Cl -Nd(3)-O(8)	73(1)
O(3) -Nd(3)-O(9)	106(2)	Cl -Nd(3)-O(9)	74(1)
O(3) -Nd(3)-O(15)	109(2)	Cl -Nd(3)-O(15)	71(1)
O(3) -Nd(3)-O(16)	108(2)	Cl -Nd(3)-O(16)	72(1)
O(4) -Nd(4)-O(10)	107(2)	Cl -Nd(4)-O(10)	73(1)
O(4) -Nd(4)-O(12)	106(2)	Cl -Nd(4)-O(12)	75(1)
O(4) -Nd(4)-O(13)	107(2)	Cl -Nd(4)-O(13)	73(1)
O(4) -Nd(4)-O(17)	111(2)	Cl -Nd(4)-O(17)	69(1)
O(5) -Nd(5)-O(10)	105(2)	Cl -Nd(5)-O(10)	74(1)
O(5) -Nd(5)-O(11)	112(2)	Cl -Nd(5)-O(11)	72(1)

Table IV. Continued

Cl	-Nd(5)-O(14)	73(1)	O(11)-Nd(5)-O(14)		97(1)
Cl	-Nd(5)-O(17)	69(1)	O(10)-Nd(5)-O(17)		69(1)
Cl	-Nd(6)-O(11)	72(1)	O(11)-Nd(5)-O(17)		68(1)
Cl	-Nd(6)-O(12)	73(1)	O(11)-Nd(6)-O(15)		104(1)
Cl	-Nd(6)-O(15)	72(1)	O(12)-Nd(6)-O(15)		97(1)
Cl	-Nd(6)-O(17)	69(1)	O(11)-Nd(6)-O(17)		69(1)
O(7)	-Nd(1)-O(13)	104(1)	O(12)-Nd(6)-O(17)		67(1)
O(9)	-Nd(1)-O(13)	97(1)	O(13)-Nd(1)-O(16)		143(1)
O(7)	-Nd(1)-O(16)	72(1)	O(14)-Nd(2)-O(16)		142(1)
O(9)	-Nd(1)-O(16)	67(1)	O(15)-Nd(3)-O(16)		143(1)
O(7)	-Nd(2)-O(14)	96(1)	O(13)-Nd(4)-O(17)		142(1)
O(8)	-Nd(2)-O(14)	102(1)	O(14)-Nd(5)-O(17)		142(1)
O(7)	-Nd(2)-O(16)	71(1)	O(15)-Nd(6)-O(17)		141(1)
O(8)	-Nd(2)-O(16)	67(1)	O(7)	-Nd(1)-O(9)	135(1)
O(8)	-Nd(3)-O(15)	97(1)	O(7)	-Nd(2)-O(8)	132(1)
O(9)	-Nd(3)-O(15)	102(1)	O(8)	-Nd(3)-O(9)	134(1)
O(8)	-Nd(3)-O(16)	71(1)	O(10)-Nd(4)-O(12)		132(1)
O(9)	-Nd(3)-O(16)	69(1)	O(10)-Nd(5)-O(11)		132(1)
O(10)	-Nd(4)-O(13)	99(1)	O(11)-Nd(6)-O(12)		131(1)
O(12)	-Nd(4)-O(13)	103(1)	Nd(1)-O(1)	-C(1)	159(4)
O(10)	-Nd(4)-O(17)	67(2)	Nd(2)-O(2)	-C(4)	169(4)
O(12)	-Nd(4)-O(17)	69(1)	Nd(3)-O(3)	-C(7)	171(5)
O(10)	-Nd(5)-O(14)	103(1)	Nd(4)-O(4)	-C(10)	169(4)

Table IV. Continued

Nd(5)-O(5) -C(13)	164(5)	Nd(4)-O(17)-C(49)	116(3)
Nd(6)-O(6) -C(16)	165(5)	Nd(5)-O(17)-C(49)	115(3)
Nd(1)-O(7) -C(19)	132(3)	Nd(6)-O(17)-C(49)	116(4)
Nd(2)-O(7) -C(19)	123(3)		
Nd(2)-O(8) -C(22)	136(3)		
Nd(3)-O(8) -C(22)	117(3)		
Nd(3)-O(9) -C(25)	125(4)		
Nd(1)-O(9) -C(25)	128(4)		
Nd(4)-O(10)-C(28)	116(3)		
Nd(5)-O(10)-C(28)	136(3)		
Nd(5)-O(11)-C(31)	126(4)		
Nd(6)-O(11)-C(31)	125(4)		
Nd(6)-O(12)-C(34)	122(3)		
Nd(4)-O(12)-C(34)	129(3)		
Nd(1)-O(13)-C(37)	107(4)		
Nd(4)-O(13)-C(37)	126(4)		
Nd(2)-O(14)-C(40)	127(4)		
Nd(5)-O(14)-C(40)	106(4)		
Nd(3)-O(15)-C(43)	111(4)		
Nd(6)-O(15)-C(43)	121(4)		
Nd(1)-O(16)-C(46)	118(3)		
Nd(2)-O(16)-C(46)	106(3)		
Nd(3)-O(16)-C(46)	124(3)		

DATA PROCESSING FORMULAE

$$I = C - (t_c/2t_b)(B_1+B_2)$$

$$\sigma(B) = \text{Max}[(t_c/2t_b)(B_1+B_2)^{\frac{1}{2}}, (t_c/2t_b)|B_1-B_2|]$$

$$\sigma(I) = [C + \sigma^2(B)]^{\frac{1}{2}}$$

$$F^2 = (D \cdot A/Lp)I$$

$$\sigma(F^2) = (D \cdot A/Lp)\sigma(I)$$

$$F_a^2 = \Sigma F^2/n$$

$$\sigma(F_a^2) = [\Sigma\sigma^2(F^2)/n]^{\frac{1}{2}}$$ When $S(F_a^2) > 4\sigma(F_a^2)$, $\sigma(F_a^2)$ is replaced by $S(F_a^2)$.

$$S(F_a^2) = [\Sigma|F^2-F_a^2|^2/n(n-1)]^{\frac{1}{2}}$$

$$\sigma(F_o^2) = [\sigma^2(F_a^2) + (pF_a^2)^2 + q^2]^{\frac{1}{2}}$$

$$F_o = (F_a^2)^{\frac{1}{2}}$$

$$\sigma(F) = F_o - [F_a^2 - \sigma(F_o^2)]^{\frac{1}{2}} \text{ when } \sigma(F_o^2) \leq F_a^2 \text{ or } [\sigma(F_a^2)]^{\frac{1}{2}} \text{ when } \sigma(F_a^2) > F_a^2$$

$$Lp = [\cos^2 2\theta_m + \cos^2 2\theta]/[\sin 2\theta\ (1 + \cos^2 2\theta_m)]$$

$$wtg = 1/\sigma^2(F)$$

C = counts recorded during a scan

I = individual raw intensity, background removed.

t_c = scan count time

t_b = background count time

B_1 = individual background count

$\sigma(B)$ = estimated standard deviation of the total background count

F = structure factor

D = decay correction; an empirically applied correction obtained from the fluctuations of the standard reflections.

A = absorption correction

Lp = Lorentz and polarization corrections

θ_m = monochromater angle

θ = crystal diffraction angle

S = scatter

a = average

q = additional uncertainty that affects the weak intensities

p = estimate of non-statistical errors

wtg = weighting factors in least squares

OBSERVED STRUCTURE FACTORS, STANDARD DEVIATIONS, AND DIFFERENCES (ALL X 1.0)
ND6(OCH(CH3)2)17CL. F(0,0,0) = 3265

FOB AND FCA ARE THE OBSERVED AND CALCULATED STRUCTURE FACTORS.
SG = ESTIMATED STANDARD DEVIATION OF FOB. DEL = /FOB/ - /FCA/.
* INDICATES ZERO WEIGHTED DATA.

H	FOB	SG	DEL	H	FOB	SG	DEL	H	FOB	SG	DEL	H	FOB	SG	DEL	H	FOB	SG	DEL
K,L=	0,	0		16	53	20	11*	-17	90	13	6	1	62	12	18	-8	193	9	-1
4	157	0	-19*	18	111	12	-0	-15	355	11	17	3	132	10	-5	-6	208	8	-7
6	89	0	7*	20	50	70	13*	-13	86	18	1	5	42	24	29*	-4	87	12	29
8	33	51	-2*	22	0	48	-19*	-11	309	10	16	7	64	14	-8	-2	93	22	5
10	29	37	-3*	K,L=	0,	3	-9	49	13	-1	9	55	44	19*	0	62	25	11*	
12	290	9	7	-21	84	16	1	-7	373	12	-7	11	65	28	0*	2	0	43	-4*
14	294	9	5	-19	24	46	2*	-5	63	8	3	13	165	9	-1	4	98	30	-8*
16	174	8	0	-17	320	11	-5	-3	120	7	3	15	74	81	-8*	6	85	15	-10
18	170	8	14	-15	36	40	11*	-1	27	43	15*	17	0	47	-2*	8	46	74	22*
20	0	79	-31*	-13	0	33	-4*	1	264	8	-2	K,L=	0,	8	10	43	69	33*	
22	0	65	-36*	-11	26	30	-4*	3	262	8	-11	-20	216	25	4	12	128	11	15
K,L=	0,	1	-9	251	9	6	5	71	8	-13	-18	135	17	7	K,L=	0,	11		
-21	0	49	-28*	-7	36	53	-22*	7	334	10	-6	-16	51	29	7*	-17	63	24	10*
-19	61	21	-11*	-5	606	19	7	9	402	13	-15	-14	88	13	17	-15	0	49	-35*
-17	100	10	-4	-3	607	0	-66*	11	188	11	-3	-12	107	10	13	-13	11	60	8*
-15	400	13	-9	-1	456	0	-92*	13	62	16	-3	-10	46	27	-26*	-11	58	68	17*
-13	502	16	11	1	106	0	-6*	15	75	15	19	-8	23	58	19*	-9	68	18	44
-11	97	9	-12	3	28	69	-5*	17	0	83	-37*	-6	214	7	2	-7	108	25	-0
-9	77	17	-1	5	135	12	4	19	44	47	6*	-4	55	18	-49*	-5	20	45	-5*
-7	154	18	-29	7	42	20	28*	K,L=	0,	6	-2	147	6	12	-3	127	12	-20	
-5	12	0	-9*	9	456	14	2	-22	0	48	-9*	0	57	17	31*	-1	14	45	-40*
-3	48	0	-21*	11	129	11	-17	-20	77	79	-14*	2	64	11	4	1	141	10	-15
1	127	0	-97*	13	396	13	-19	-18	56	26	-9*	4	81	44	0*	3	128	10	1
3	123	0	-2*	15	67	15	-14	-16	109	10	-5	6	452	15	14	5	83	20	-4
5	104	0	10*	17	114	11	20	-14	26	41	0*	8	36	47	20*	7	23	81	14*
7	70	32	-11*	19	70	74	-9*	-12	35	41	-29*	10	102	11	-14	9	71	18	26
9	43	13	-9*	21	84	49	2*	-10	75	8	-2	12	57	23	31*	K,L=	0,	12	
11	454	14	32	K,L=	0,	4	-8	443	14	-1	14	104	28	-21	-14	71	20	50	
13	16	36	-7*	-22	0	49	-3*	-6	123	6	9	16	8	74	-1*	-12	254	10	-7
15	28	39	-6*	-20	14	74	8*	-4	761	23	7	K,L=	0,	9	-10	61	30	26*	
17	93	11	5	-18	399	14	1	-2	36	37	30*	-19	0	66	-28*	-8	76	32	-19*
19	178	9	29	-16	44	61	10*	0	18	45	-28*	-17	55	76	30*	-6	53	71	46*
21	108	36	2*	-14	325	11	31	2	54	19	-6*	-15	39	47	28*	-4	93	35	-3*
K,L=	0,	2	-12	61	10	10	4	112	9	-21	-13	103	24	6	-2	45	69	26*	
-22	17	63	-14*	-10	116	8	-7	6	135	7	-7	-11	100	11	-1	0	149	20	11
-20	40	47	-8*	-8	43	15	42*	8	470	15	-4	-9	377	12	-12	2	108	17	-1
-18	37	43	26*	-6	166	9	-15	10	186	8	-1	-7	240	15	-2	4	211	13	-15
-16	76	13	-4	-4	309	11	9	12	0	46	-31*	-5	66	13	-9	6	0	50	-13*
-14	173	7	0	-2	685	21	-7	14	155	12	-1	-3	0	39	-11*	K,L=	0,	13	
-12	144	6	0	0	159	21	2	16	0	78	-38*	-1	0	46	-19*	-11	156	11	40
-10	91	14	-9	2	310	11	19	18	38	68	24*	1	35	42	-3*	-9	185	15	6
-8	395	13	-21	4	215	7	-9	K,L=	0,	7	3	117	9	-19	-7	0	49	-9*	
-6	134	16	65	6	169	6	-2	-21	141	18	13	5	469	15	5	-5	23	51	-0*
-4	323	0	-48*	8	133	7	-6	-19	257	14	8	7	77	59	-30*	-3	0	48	-16*
-2	640	0	-18*	10	63	11	11	-17	103	13	6	9	66	28	-11*	-1	39	42	31*
0	89	0	-32*	12	86	10	-22	-15	87	12	-12	11	57	76	-0*	1	46	63	23*
2	0	0	-18*	14	0	41	-4*	-13	131	11	6	13	0	67	-16*	3	134	16	-2
4	58	0	15*	16	204	9	-0	-11	37	27	28*	K,L=	0,	10	K,L=	1,	0		
6	101	21	12	18	93	41	20*	-9	178	7	3	-18	0	49	-6*	21	143	0	71*
8	108	7	-1	20	99	14	-10	-7	268	9	-3	-16	0	60	-4*	3	171	0	-29*
10	784	24	39	K,L=	0,	5	-5	736	23	-4	-14	42	78	18*	4	0	0	-34*	
12	69	18	43	-21	33	72	32*	-3	73	8	-9	-12	49	32	23*	5	136	0	-27*
14	320	11	10	-19	155	13	1	-1	99	10	3	-10	326	16	-8	6	129	0	62*

STRUCTURE FACTORS CONTINUED FOR
ND6(OCH(CH3)2)17CL.

H	FOB	SG	DEL	H	FOB	SG	DEL	H	FOB	SG	DEL	H	FOB	SG	DEL	H	FOB	SG	DEL
7	175	12	-24	19	174	13	-6	-16	48	51	-16*	-4	558	17	28	9	336	11	-18
8	0	56	-20*	20	0	132	-27*	-15	233	8	6	-3	29	81	6*	10	40	55	3*
9	24	46	-21*	21	0	53	-32*	-14	12	49	-8*	-2	352	14	-19	11	184	7	11
10	68	15	16	22	66	19	29	-13	33	34	10*	-1	33	79	-8*	12	49	31	6*
11	0	50	-31*	K,L=	1,	2	-12	22	33	0*	0	176	18	8	13	0	42	-14*	
12	147	6	3	-22	117	12	-20	-11	81	9	16	1	135	21	12	14	0	43	-11*
13	0	288	-37*	-21	0	51	-40*	-10	162	6	11	2	302	11	-10	15	63	23	6*
14	370	12	8	-20	0	46	-5*	-9	81	14	-15	3	3	50	-5*	16	0	48	-11*
15	0	92	-62*	-19	67	17	63	-8	63	16	19	4	121	7	-5	17	113	39	17*
16	96	10	-8	-18	33	47	-14*	-7	39	50	-34*	5	265	9	24	18	0	100	-8*
17	0	50	-28*	-17	33	42	4*	-6	0	68	-29*	6	69	10	-14	19	40	47	23*
18	34	45	-11*	-16	64	15	12	-5	386	14	12	7	18	30	-7*	K,L=	1,	6	
19	102	41	-12*	-15	0	70	-22*	-4	54	0	33*	8	127	6	-3	-22	45	48	27*
20	163	16	-9	-14	281	9	-4	-3	667	0	-62*	9	74	8	-8	-21	0	76	-14*
21	0	109	-11*	-13	0	90	-37*	-2	50	0	13*	10	0	34	-8*	-20	109	27	3
22	0	48	-36*	-12	151	6	7	-1	488	0	-85*	11	21	35	7*	-19	0	48	-57*
K,L=	1,	1	-11	0	60	-7*	0	11	0	6*	12	19	38	-1*	-18	0	47	-37*	
-22	0	67	-7*	-10	268	10	3	1	73	0	-3*	13	0	40	-2*	-17	0	50	-3*
-21	51	75	48*	-9	405	13	8	2	44	0	33*	14	28	44	-15*	-16	39	43	-7*
-20	62	24	14*	-8	250	9	-12	3	45	64	-21*	15	0	57	-37*	-15	21	43	-27*
-19	28	45	16*	-7	14	69	12*	4	0	67	-28*	16	0	99	-22*	-14	101	10	1
-18	19	44	18*	-6	112	27	-24	5	54	44	-11*	17	0	66	-106*	-13	76	11	-1
-17	37	48	-13*	-5	218	0	101*	6	37	51	28*	18	93	116	-8*	-12	85	20	3
-16	0	55	-1*	-4	414	0	-27*	7	55	24	-3*	19	0	94	-23*	-11	182	7	11
-15	283	9	-16	-3	0	0	-4*	8	0	31	-32*	20	69	20	25	-10	105	7	9
-14	0	64	-64*	-2	310	0	-42*	9	105	6	-8	K,L=	1,	5	-9	92	12	6	
-13	428	13	-21	-1	20	0	-7*	10	0	299	-65*	-22	0	48	-13*	-8	69	12	2
-12	0	237	-17*	0	136	0	-11*	11	608	19	11	-21	27	70	-7*	-7	40	15	39*
-11	167	9	-7	1	13	0	3*	12	0	435	-72*	-20	82	27	57*	-6	823	25	-34
-10	33	74	-36*	2	0	0	-13*	13	0	44	-69*	-19	60	23	28*	-5	28	31	23*
-9	107	221	-90*	3	59	0	-13*	14	43	34	-28*	-18	0	89	-16*	-4	45	12	23
-8	247	20	-13	4	246	0	-2*	15	0	44	-4*	-17	300	16	7	-3	35	45	-1*
-7	115	160	-11*	5	84	41	-22*	16	0	102	-67*	-16	0	56	-42*	-2	252	8	2
-6	65	0	4*	6	14	91	1*	17	0	92	-96*	-15	22	43	-16*	-1	88	7	2
-5	26	0	25*	7	162	202	-47*	18	22	78	-72*	-14	64	14	-13	0	25	38	7*
-4	72	0	4*	8	273	64	-37	19	0	105	-18*	-13	25	41	-0*	1	14	32	-10*
-3	153	0	-15*	9	0	227	-21*	20	0	76	-32*	-12	194	7	6	2	194	7	11
-2	0	0	-21*	10	55	12	-18	21	0	48	-24*	-11	99	7	-2	3	46	13	-9
-1	190	0	-64*	11	0	422	-56*	K,L=	1,	4	-10	137	6	-8	4	56	12	2	
1	926	0	25*	12	691	21	48	-22	47	49	-2*	-9	47	12	1	5	13	37	-16*
2	121	0	-16*	13	0	316	-10*	-21	0	85	-42*	-8	81	10	6	6	297	9	17
3	12	0	-32*	14	0	40	-11*	-20	71	52	-24*	-7	6	32	-13*	7	107	11	-7
4	280	0	-19*	15	20	41	-46*	-19	30	47	-5*	-6	12	29	-24*	8	251	10	-8
5	25	0	-62*	16	0	47	-57*	-18	72	24	18*	-5	395	12	7	9	0	42	-20*
6	227	9	-6	17	37	43	15*	-17	0	78	-59*	-4	20	31	14*	10	264	10	-1
7	67	68	-53*	18	0	54	-10*	-16	501	16	9	-3	0	44	-45*	11	35	41	22*
8	193	7	-12	19	0	47	-14*	-15	0	107	-25*	-2	0	54	-19*	12	18	43	-35*
9	383	13	30	20	56	69	-28*	-14	0	41	-47*	-1	25	51	1*	13	49	72	35*
10	0	63	-40*	21	0	90	-3*	-13	27	37	-2*	0	26	40	-5*	14	67	20	19*
11	67	8	17	22	0	47	-16*	-12	149	7	25	1	116	9	-18	15	81	18	-11
12	50	13	-2	K,L=	1,	3	-11	92	10	-17	2	46	12	-30	16	30	98	-20*	
13	71	14	-10	-22	0	51	-68*	-10	0	39	-1*	3	388	12	18	17	50	35	36*
14	48	59	-35*	-21	0	66	-60*	-9	48	12	13	4	240	8	3	18	50	35	6*
15	28	51	-13*	-20	47	44	25*	-8	46	15	35*	5	40	17	-21*	K,L=	1,	7	
16	0	42	-0*	-19	94	22	-11	-7	36	23	14*	6	42	34	-13*	-22	75	60	54*
17	78	49	-14*	-18	11	46	8*	-6	31	51	-30*	7	418	13	8	-21	162	32	-8
18	0	91	-79*	-17	28	69	10*	-5	0	65	-3*	8	0	42	-38*	-20	31	65	-1*

STRUCTURE FACTORS CONTINUED FOR
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H	FOB	SG	DEL	H	FOB	SG	DEL	H	FOB	SG	DEL	H	FOB	SG	DEL	H	FOB	SG	DEL
-19	173	27	2	-2	49	20	8*-18		0	48	-15*	8	0	48	-8*	13	127	15	-26
-18	0	79	-36*	-1	227	8	4 -17		42	56	37*	9	43	62	-20*	14	199	12	-14
-17	79	15	8	0	236	8	-5 -16		0	86	-16*	10	0	53	-13*	15	41	64	-26*
-16	32	45	-11*	1	90	8	3 -15		0	64	-14*	K,L=	1,	12		16	66	15	-11
-15	64	18	-12	2	54	16	-2*-14		20	65	18*-15		52	41	-7*	17	52	77	-49*
-14	46	28	43*	3	96	9	-15 -13		69	17	54 -14		72	76	-11*	18	129	10	-4
-13	107	19	7	4	402	14	28 -12		81	15	24 -13		0	51	-16*	19	44	47	27*
-12	22	49	3*	5	36	46	4*-11		15	45	1*-12		53	42	-1*	20	51	36	-4*
-11	0	42	-6*	6	63	48	29*-10		100	25	-3 -11		0	53	-17*	21	127	44	-30*
-10	22	40	-13*	7	15	43	-4* -9		0	78	-21*-10		223	15	-0	22	0	126	-41*
-9	74	9	0	8	203	8	-0 -8		363	12	-24 -9		32	52	23*	K,L=	2,	1	
-8	10	48	-3*	9	26	53	16* -7		49	30	42* -8		0	55	-6*-22		0	50	-21*
-7	547	17	-16	10	0	44	-5* -6		83	30	-14* -7		71	33	58*-21		0	50	-8*
-6	32	57	31*	11	58	33	50* -5		20	43	9* -6		50	52	19*-20		58	24	55*
-5	195	7	4	12	104	18	-27 -4		64	70	-4* -5		48	71	37*-19		92	13	10
-4	53	15	13	13	0	89	-26* -3		139	9	-0 -4		71	76	62*-18		122	10	3
-3	236	8	-20	14	37	84	-13* -2		122	9	7 -3		0	66	-27*-17		0	43	-29*
-2	73	11	-4	15	0	58	-16* -1		44	34	24* -2		18	74	-39*-16		24	71	-43*
-1	20	34	16*	16	59	22	55* 0		0	52	-9* -1		66	76	39*-15		251	9	-16
0	183	7	-10	K,L=	1,	9	1		62	23	0* 0		39	60	10*-14		86	176	-37*
1	199	7	3 -20		0	60	-6* 2		0	44	-18* 1		52	85	39*-13		310	10	5
2	112	6	1 -19		72	22	8* 3		0	59	-1* 2		254	14	3 -12		54	102	-51*
3	35	22	1*-18		29	96	2* 4		48	54	-22* 3		46	76	11*-11		13	62	-8*
4	50	13	-3 -17		11	81	-24* 5		52	26	21* 4		91	16	-6 -10		273	9	-3
5	116	8	-11 -16		45	94	13* 6		130	10	-19 5		55	20	39* -9		167	6	-1
6	60	11	1 -15		92	27	-22 7		22	67	9* 6		0	50	-59* -8		91	14	-29
7	59	14	13 -14		132	12	0 8		33	69	8* 7		25	49	-10* -7		89	31	-32*
8	18	48	-4*-13		0	46	-18* 9		0	80	-60*	K,L=	1,	13	-6		172	12	-10
9	83	13	0 -12		66	17	43 10		107	13	-20 -11		244	20	-2 -5		65	0	59*
10	0	42	-4*-11		132	9	-15 11		32	50	-2*-10		48	53	42* -4		0	0	-17*
11	27	43	-33*-10		42	53	18* 12		21	58	-6* -9		79	19	29 -3		12	0	-3*
12	13	58	-9* -9		240	10	6	K,L=	1,	11	-8		0	51	-39* -2		0	0	-3*
13	179	9	8 -8		0	72	-12*-17		41	63	-27* -7		28	49	24* -1		497	0	-42*
14	96	23	-4 -7		247	14	-5 -16		64	23	12* -6		50	51	6* 0		28	0	-31*
15	104	36	-19* -6		0	53	-5*-15		0	49	-24* -5		39	42	30* 1		35	0	-33*
16	29	50	1* -5		60	21	-9*-14		50	66	15* -4		25	43	-21* 2		248	0	-31*
17	60	23	13* -4		0	52	-7*-13		32	83	-23* -3		28	49	-1* 3		152	0	43*
K,L=	1,	8	-3		44	21	41*-12		60	81	50* -2		41	42	28* 4		291	0	-97*
-21	0	79	-7*	-2	30	38	-11*-11		26	66	21* -1		0	53	-8* 5		15	0	-5*
-20	92	34	3*	-1	34	38	-2*-10		0	56	-0* 0		0	42	-22* 6		588	18	15
-19	56	80	31*	0	0	47	-5* -9		78	16	-17 1		89	25	-4 7		225	13	35
-18	161	25	7	1	0	42	-22* -8		0	79	-5* 2		0	51	-36* 8		269	9	-13
-17	86	21	10	2	0	42	-43* -7		49	33	20* 3		0	82	-33* 9		0	52	-18*
-16	2	47	-27*	3	221	8	-9 -6		48	49	22*	K,L=	2,	0	10		132	8	-10
-15	49	32	41*	4	52	25	13* -5		79	15	8	0	113	7	0 -39*	11	292	9	24
-14	189	9	-9	5	153	10	0 -4		124	14	5 1		86	0	-25* 12		28	35	-53*
-13	141	9	-0	6	0	68	-16* -3		65	26	-25* 2		60	0	-40* 13		0	38	-8*
-12	77	13	14	7	289	10	-13 -2		61	22	7* 3		168	0	-24* 14		61	11	6
-11	0	40	-4*	8	0	65	-2* -1		0	46	-37* 4		144	0	36* 15		0	40	-29*
-10	32	40	-39*	9	52	27	3* 0		82	22	4 5		296	0	-64* 16		0	42	-11*
-9	26	38	23*	10	60	33	1* 1		79	15	20 6		79	31	-5* 17		39	44	-19*
-8	0	36	-5*	11	14	71	-17* 2		34	57	4* 7		177	13	-18 18		0	75	-27*
-7	0	35	-2*	12	0	60	-32* 3		154	9	-10 8		42	65	-21* 19		125	14	-3
-6	100	7	-15	13	9	47	-32* 4		69	18	65 9		105	11	-2 20		0	105	-159*
-5	35	44	28*	14	0	64	-34* 5		48	64	-6* 10		19	32	-22* 21		0	131	-89*
-4	122	7	12	K,L=	1,	10	6		21	92	11* 11		24	30	-8* 22		0	74	-42*
-3	47	16	-5*-19		0	50	-21* 7		27	60	2* 12		203	9	5	K,L=	2,	2	

STRUCTURE FACTORS CONTINUED FOR
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H	FOB	SG	DEL	H	FOB	SG	DEL	H	FOB	SG	DEL	H	FOB	SG	DEL	H	FOB	SG	DEL
-22	0	52	-23*	-11	0	31	-11*	1	13	55	-16*	14	43	44	-7*	-14	123	9	19
-21	55	34	4*	-10	85	21	-12	2	262	10	-12	15	0	46	-44*	-13	89	12	2
-20	0	54	-43*	-9	275	10	1	3	695	25	90	16	26	47	-8*	-12	0	40	-23*
-19	0	55	-15*	-8	331	11	13	4	251	8	-22	17	0	76	-20*	-11	23	47	8*
-18	0	44	-8*	-7	46	47	-16*	5	44	19	15*	18	51	70	14*	-10	115	12	-3
-17	0	43	-15*	-6	0	63	-26*	6	60	9	14	19	60	31	36*	-9	65	10	15
-16	29	41	-3*	-5	333	14	3	7	200	7	8	K,L=	2,	6	-8	20	33	-18*	
-15	39	42	35*	-4	64	39	17*	8	103	8	-3	-22	0	50	-1*	-7	159	9	5
-14	106	8	-9	-3	521	0	-33*	9	35	18	33*	-21	56	30	13*	-6	84	10	-4
-13	35	76	-28*	-2	59	0	14*	10	20	42	19*	-20	39	54	-26*	-5	404	13	-8
-12	533	30	-17*	-1	346	0	-36*	11	86	8	-4	-19	45	48	31*	-4	49	13	13
-11	401	14	45	0	216	0	93*	12	54	62	-25*	-18	84	14	49	-3	31	32	10*
-10	91	157	-43*	1	85	0	37*	13	0	40	-3*	-17	61	20	-5*	-2	223	8	-18
-9	36	120	18*	2	46	52	37*	14	0	114	-7*	-16	73	15	12	-1	249	8	27
-8	343	14	-39	3	78	40	-7*	15	0	159	-130*	-15	65	22	17*	0	251	8	-11
-7	691	21	84	4	205	11	41	16	124	21	-57	-14	0	41	-13*	1	37	37	15*
-6	166	18	-9	5	45	46	-2*	17	32	111	-81*	-13	187	8	-16	2	251	9	-7
-5	59	0	53*	6	31	39	-2*	18	0	84	-42*	-12	149	8	4	3	60	10	18
-4	143	0	-36*	7	26	40	-4*	19	99	18	-15	-11	194	8	9	4	88	8	1
-3	11	0	-20*	8	30	83	-17*	20	61	81	-8*	-10	71	9	3	5	14	43	11*
-2	338	0	0*	9	294	11	14	K,L=	2,	5	-9	208	7	-0	6	52	15	-10	
-1	0	0	-23*	10	99	66	-41*	-22	0	62	-23*	-8	196	7	-9	7	0	43	-39*
0	0	0	-3*	11	57	57	-22*	-21	22	76	21*	-7	29	38	21*	8	106	9	-7
1	88	0	10*	12	0	94	-44*	-20	7	66	-35*	-6	75	7	-1	9	0	41	-29*
2	10	0	-5*	13	249	10	8	-19	71	25	5*	-5	78	7	-16	10	0	62	-5*
3	97	0	-1*	14	0	114	-7*	-18	71	22	25*	-4	451	20	31	11	76	15	-2
4	55	36	-6*	15	0	100	-23*	-17	78	15	3	-3	55	14	-17	12	148	33	2
5	460	15	18	16	133	18	-51	-16	0	44	-10*	-2	0	31	-16*	13	137	10	6
6	285	10	15	17	90	15	-29	-15	196	8	11	-1	84	7	-8	14	49	73	-6*
7	124	10	-15	18	108	26	-12	-14	164	8	-6	0	0	44	-27*	15	77	99	-7*
8	35	39	-10*	19	23	92	-18*	-13	38	46	-37*	1	0	30	-32*	16	86	32	-26*
9	161	21	-22	20	67	72	-15*	-12	341	11	-1	2	0	37	-8*	17	0	48	-8*
10	536	16	25	21	0	65	-47*	-11	321	10	28	3	33	22	-16*	K,L=	2,	8	
11	50	100	-66*	K,L=	2,	4	-10	279	10	-14	4	90	11	-10	-21	28	51	-5*	
12	60	41	29*	-22	43	82	1*	-9	33	38	25*	5	3	41	-21*	-20	133	27	-6
13	58	21	-26*	-21	56	72	-27*	-8	111	11	7	6	85	9	5	-19	48	78	37*
14	154	10	7	-20	29	48	27*	-7	294	9	14	7	27	35	17*	-18	86	45	15*
15	0	52	-47*	-19	0	54	-28*	-6	14	39	0*	8	304	10	-4	-17	0	49	-11*
16	0	42	-14*	-18	244	9	3	-5	51	10	-4	9	139	15	-14	-16	72	19	-4
17	0	46	-70*	-17	0	46	-13*	-4	19	38	-5*	10	108	9	-13	-15	255	9	-1
18	42	46	-5*	-16	66	24	38*	-3	25	52	16*	11	16	53	-25*	-14	99	12	-1
19	33	48	17*	-15	92	17	-2	-2	20	41	4*	12	39	66	0*	-13	0	55	-18*
20	20	76	-16*	-14	180	9	14	-1	13	50	8*	13	185	16	8	-12	113	17	0
21	0	67	-5*	-13	152	8	17	0	43	49	-15*	14	129	15	4	-11	106	9	-1
22	0	48	-16*	-12	50	13	17	1	257	8	-10	15	0	89	-22*	-10	30	45	-14*
K,L=	2,	3	-11	125	6	-17	2	431	13	12	16	0	50	-6*	-9	0	45	-8*	
-22	102	15	-17	-10	86	10	-7	3	252	8	-7	17	67	87	-11*	-8	36	47	27*
-21	63	29	-43*	-9	86	6	-7	4	115	8	-11	18	0	47	-8*	-7	21	35	14*
-20	78	16	-2	-8	39	31	38*	5	30	38	-2*	K,L=	2,	7	-6	117	8	13	
-19	0	61	-5*	-7	40	25	16*	6	122	6	15	-22	36	72	15*	-5	0	36	-6*
-18	0	85	-61*	-6	24	52	-16*	7	207	7	-7	-21	93	51	32*	-4	0	51	-9*
-17	216	9	-9	-5	0	63	-10*	8	80	10	-7	-20	65	67	-4*	-3	225	8	12
-16	63	66	4*	-4	165	16	7	9	250	8	2	-19	171	19	3	-2	188	7	15
-15	0	44	-26*	-3	0	74	-16*	10	10	38	-13*	-18	45	48	14*	-1	170	7	-3
-14	54	16	-12*	-2	430	15	-6	11	124	8	4	-17	14	47	-42*	0	51	47	-7*
-13	0	35	-2*	-1	96	34	14*	12	0	48	-38*	-16	46	49	8*	1	369	12	9
-12	94	7	4	0	0	71	-12*	13	0	48	-13*	-15	95	12	-5	2	27	41	-14*

STRUCTURE FACTORS CONTINUED FOR
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H	FOB	SG	DEL	H	FOB	SG	DEL	H	FOB	SG	DEL	H	FOB	SG	DEL	H	FOB	SG	DEL
3	43	25	0*	-12	0	50	-6*	-13	16	51	-3*	21	0	115	-10*	-14	60	14	-13
4	44	60	-17*	-11	0	48	-0*	-12	160	13	-7	22	0	75	-13*	-13	13	34	-19*
6	291	10	8	-10	183	9	-9	-11	26	66	18*	K,L=	3,	1	-12	52	24	14*	
7	0	43	-30*	-9	26	45	-16*	-10	71	20	50	-22	0	69	-22*	-11	3	71	0*
8	23	43	22*	-8	118	10	-4	-9	0	78	-9*	-21	0	109	-31*	-10	283	14	8
9	67	16	24	-7	0	47	-11*	-8	8	65	-41*	-20	104	21	-12	-9	824	26	30
10	0	45	-63*	-6	85	13	2	-7	0	98	-27*	-19	44	47	-5*	-8	294	9	-21
11	25	45	7*	-5	166	12	-5	-6	49	64	44*	-18	0	45	-7*	-7	0	45	-30*
12	47	56	20*	-4	98	11	21	-5	34	68	19*	-17	0	43	-31*	-6	157	17	-10
13	0	69	-16*	-3	91	17	50	-4	82	37	1*	-16	0	42	-7*	-5	84	32	3*
14	85	88	-14*	-2	101	11	-14	-3	91	58	5*	-15	0	50	-37*	-4	53	0	37*
15	41	49	-0*	-1	211	12	12	-2	27	89	5*	-14	150	9	3	-3	35	0	3*
16	0	47	-14*	0	75	21	18	-1	56	79	13*	-13	147	13	-17	-2	75	0	5*
K,L=	2,	9	1	60	38	46*	0	86	35	9*	-12	32	41	4*	-1	0	0	-56*	
-20	0	57	-10*	2	0	44	-1*	1	62	73	21*	-11	30	30	26*	0	0	0	-2*
-19	53	30	40*	3	30	44	-28*	2	88	24	12	-10	81	21	-30	1	31	0	30*
-18	22	62	6*	4	58	23	-20*	3	14	71	1*	-9	172	12	-33	2	51	0	46*
-17	0	86	-1*	5	22	66	-6*	4	113	17	-19	-8	494	17	25	3	346	0	51*
-16	170	12	15	6	66	19	8	5	48	50	35*	-7	186	10	6	4	274	12	2
-15	22	58	6*	7	36	64	32*	6	28	50	23*	-6	3	66	-22*	5	293	11	-19
-14	81	22	10	8	45	72	42*	7	51	53	22*	-5	61	0	40*	6	0	51	-50*
-13	123	24	-9	9	10	69	-22*	K,L=	2,	13	-4	6	0	-43*	7	401	14	-4	
-12	170	9	-8	10	0	58	-18*	-11	112	13	34	-3	36	0	-8*	8	36	45	27*
-11	58	30	27*	11	155	10	4	-10	8	52	-6*	-2	0	0	-11*	9	36	15	14*
-10	0	43	-15*	12	88	27	-19*	-9	123	18	16	-1	39	0	-48*	10	18	34	8*
-9	247	10	13	K,L=	2,	11	-8	0	51	-47*	0	108	0	-1*	11	20	35	10*	
-8	62	73	24*	-17	0	51	-39*	-7	71	20	61	1	184	0	3*	12	198	7	10
-7	124	18	-27	-16	118	12	7	-6	114	14	3	2	135	0	-11*	13	68	13	-36
-6	24	48	11*	-15	55	29	8*	-5	49	24	4*	3	25	0	-47*	14	0	44	-47*
-5	0	55	-22*	-14	63	49	9*	-4	49	51	1*	4	432	0	-89*	15	86	11	-12
-4	23	45	-10*	-13	70	81	62*	-3	50	22	42*	5	644	23	68	16	78	36	10*
-3	53	43	43*	-12	49	71	42*	-2	10	42	-32*	6	584	18	-20	17	40	45	10*
-2	0	39	-18*	-11	47	64	16*	-1	0	51	-2*	7	28	60	-26*	18	0	46	-10*
-1	25	39	-11*	-10	22	76	15*	0	23	51	-22*	8	359	14	-15	19	51	78	26*
0	92	22	6	-9	41	46	28*	1	43	32	29*	9	35	42	-2*	20	0	82	-32*
1	65	14	31	-8	49	50	45*	2	0	49	-31*	10	33	16	-6*	21	0	58	-8*
2	0	41	-21*	-7	67	23	8*	K,L=	3,	0	11	47	19	-9*	22	35	46	34*	
3	70	15	-10	-6	81	15	-4	1	195	0	-18*	12	87	14	6	K,L=	3,	3	
4	40	45	10*	-5	0	46	-27*	2	105	0	-16*	13	0	34	-1*	-22	117	35	-28*
5	305	10	3	-4	102	12	9	3	179	0	-51*	14	114	8	-5	-21	0	97	-10*
6	84	15	-6	-3	168	11	-8	4	22	0	-11*	15	0	40	-18*	-20	24	48	-36*
7	44	47	-3*	-2	248	11	7	5	235	0	-39*	16	41	42	31*	-19	0	46	-10*
8	62	71	11*	-1	52	50	-13*	6	253	12	28	17	48	95	-14*	-18	0	53	-30*
9	36	46	20*	0	64	71	-5*	7	327	11	-12	18	203	12	2	-17	28	43	22*
10	74	16	27	1	84	31	8*	8	0	43	-13*	19	90	15	-4	-16	139	8	4
11	41	53	16*	2	54	57	33*	9	49	25	10*	20	0	101	-33*	-15	70	72	-21*
12	105	31	10*	3	93	40	12*	10	76	14	24	21	41	49	-3*	-14	69	18	9
13	29	55	22*	4	0	47	-33*	11	62	8	1	22	89	55	8*	-13	0	34	-6*
14	0	49	-39*	5	31	69	-7*	12	64	10	-4	K,L=	3,	2	-12	13	33	-25*	
K,L=	2,	10	6	78	39	55*	13	37	25	4*	-22	0	64	-86*	-11	72	17	-13	
-19	0	49	-7*	7	0	54	-2*	14	93	9	-17	-21	43	60	-43*	-10	413	13	38
-18	0	49	-20*	8	26	48	12*	15	158	8	-3	-20	69	18	66	-9	126	9	13
-17	0	71	-25*	9	0	49	-32*	16	13	41	-12*	-19	43	45	39*	-8	92	10	19
-16	0	97	-2*	10	77	24	5*	17	0	57	-38*	-18	69	16	9	-7	204	8	-23
-15	22	86	9*	K,L=	2,	12	18	102	62	-7*	-17	103	10	18	-6	131	16	33	
-14	72	48	32*	-15	54	39	-5*	19	264	12	-9	-16	49	22	27*	-5	23	69	-17*
-13	31	53	-23*	-14	0	58	-18*	20	102	73	-27*	-15	44	24	-20*	-4	35	79	5*

STRUCTURE FACTORS CONTINUED FOR
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H	FOB	SG	DEL	H	FOB	SG	DEL	H	FOB	SG	DEL	H	FOB	SG	DEL	H	FOB	SG	DEL
-3	290	12	4	9	92	7	-5	-21	0	49	-26*	-6	52	12	-1	11	43	45	26*
-2	167	0	63*	10	57	10	31	-20	18	71	-28*	-5	38	20	10*	12	55	28	-4*
-1	73	0	-7*	11	0	38	-26*	-19	104	12	-6	-4	52	12	21	13	71	50	-15*
0	58	0	54*	12	0	38	-21*	-18	0	54	-24*	-3	81	7	25	14	0	79	-38*
1	155	16	-7	13	0	46	-2*	-17	42	45	40*	-2	195	7	-5	15	35	48	0*
2	451	15	22	14	0	82	-48*	-16	37	45	2*	-1	40	49	-10*	K,L=		3,	9
3	150	16	-26	15	100	15	-2	-15	51	65	-5*	0	398	13	-16	-20	0	49	-7*
4	38	47	5*	16	0	103	-14*	-14	45	27	11*	1	250	15	7	-19	0	48	-17*
5	15	41	-15*	17	212	9	-11	-13	119	8	-5	2	266	9	3	-18	49	73	4*
6	36	42	7*	18	25	111	-49*	-12	78	23	-0	3	20	33	-5*	-17	0	69	-1*
7	0	49	-11*	19	83	59	25*	-11	405	13	11	4	119	6	-3	-16	84	92	15*
8	63	8	-4	20	0	48	-7*	-10	265	9	22	5	69	10	17	-15	123	17	-8
9	52	10	0	K,L=		3,	5	-9	146	8	-2	6	92	9	-9	-14	271	17	-8
10	116	8	-10	-22	30	48	19*	-8	54	11	7	7	22	39	18*	-13	70	19	-5
11	205	8	-5	-21	35	69	9*	-7	56	10	15	8	59	16	-2	-12	89	13	43
12	177	12	-9	-20	39	76	-6*	-6	231	10	-14	9	0	41	-20*	-11	27	45	8*
13	0	68	-35*	-19	33	67	10*	-5	97	6	-8	10	0	42	-7*	-10	0	43	-10*
14	82	14	-17	-18	62	31	47*	-4	29	30	15*	11	0	64	-26*	-9	64	31	18*
15	69	85	-32*	-17	85	16	5	-3	0	37	-8*	12	61	21	8*	-8	59	17	28
16	143	9	-13	-16	60	20	-3*	-2	15	36	4*	13	135	13	-2	-7	45	29	-8*
17	0	61	-11*	-15	0	42	-14*	-1	136	6	-1	14	228	16	-20	-6	0	53	-4*
18	161	9	-8	-14	161	8	-4	0	0	33	-2*	15	61	89	-20*	-5	27	47	2*
19	0	97	-29*	-13	144	7	4	1	25	30	-24*	16	0	68	-57*	-4	0	39	-3*
20	0	64	-61*	-12	371	12	5	2	66	8	8	17	0	48	-3*	-3	29	48	-1*
21	0	67	-10*	-11	57	13	3	3	147	8	18	K,L=		3,	8	-2	33	39	-11*
K,L=		3,	4	-10	361	12	-8	4	52	13	7	-21	29	77	25*	-1	55	17	-0*
-22	22	50	3*	-9	185	7	5	5	31	43	9*	-20	0	81	-6*	0	0	59	-25*
-21	57	88	-28*	-8	133	6	11	6	64	10	3	-19	56	57	-2*	1	0	42	-33*
-20	0	64	-45*	-7	10	31	-8*	7	266	9	4	-18	35	91	-4*	2	30	42	-21*
-19	50	50	-2*	-6	23	41	-11*	8	94	9	-8	-17	154	13	13	3	53	21	6*
-18	94	13	43	-5	190	7	1	9	61	14	22	-16	54	69	16*	4	78	15	-21
-17	154	9	-7	-4	35	40	24*	10	8	40	-8*	-15	0	49	-32*	5	43	44	9*
-16	163	10	-7	-3	22	36	16*	11	35	46	-6*	-14	188	12	5	6	51	81	-37*
-15	21	52	-4*	-2	15	41	2*	12	70	16	13	-13	340	12	19	7	114	10	25
-14	10	39	-21*	-1	40	16	-8*	13	25	57	-13*	-12	117	18	6	8	22	46	-3*
-13	75	15	-10	0	161	6	-0	14	93	72	4*	-11	0	68	-0*	9	39	61	15*
-12	117	7	2	1	96	12	-13	15	194	19	-10	-10	0	40	-6*	10	124	14	6
-11	252	9	-4	2	145	7	-8	16	0	94	-41*	-9	0	39	-0*	11	74	19	-3
-10	0	34	-29*	3	356	11	15	17	59	76	33*	-8	29	37	3*	12	18	53	-51*
-9	39	21	-15*	4	616	19	37	18	0	48	-3*	-7	0	37	-10*	13	26	49	21*
-8	98	8	14	5	137	8	-9	K,L=		3,	7	-6	20	35	-7*	14	58	27	-10*
-7	29	40	24*	6	107	7	-6	-22	48	55	7*	-5	43	17	35*	K,L=		3,	10
-6	31	51	-1*	7	137	7	10	-21	67	72	12*	-4	0	35	-3*	-18	27	53	21*
-5	18	42	1*	8	129	6	3	-20	114	26	19	-3	93	9	2	-17	0	48	-24*
-4	179	12	21	9	130	7	-16	-19	49	76	5*	-2	97	8	1	-16	44	54	34*
-3	0	66	-11*	10	54	19	-37*	-18	77	17	11	-1	450	20	9	-15	57	89	21*
-2	74	35	-20*	11	0	40	-16*	-17	9	47	5*	0	281	10	7	-14	36	62	28*
-1	0	64	-28*	12	45	60	-12*	-16	75	16	-30	1	198	7	-3	-13	19	47	-6*
0	171	11	12	13	7	42	-23*	-15	58	22	-2*	2	32	36	28*	-12	0	47	-35*
1	640	32	70	14	31	44	-1*	-14	40	43	28*	3	169	8	-19	-11	0	52	-14*
2	248	8	-9	15	0	50	-1*	-13	55	59	-2*	4	93	17	3	-10	54	33	47*
3	37	44	-27*	16	73	78	32*	-12	0	41	-13*	5	88	13	-3	-9	57	26	9*
4	218	7	-13	17	55	62	7*	-11	52	17	25*	6	0	45	-10*	-8	99	21	2
5	546	20	24	18	0	58	-24*	-10	19	35	-29*	7	30	43	1*	-7	0	53	-22*
6	70	11	16	19	31	51	14*	-9	20	33	14*	8	55	21	15*	-6	52	24	39*
7	27	29	-4*	K,L=		3,	6	-8	16	33	0*	9	0	44	-3*	-5	43	44	2*
8	38	20	17*	-22	0	79	-27*	-7	97	7	-15	10	16	44	11*	-4	153	18	-4

STRUCTURE FACTORS CONTINUED FOR
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H	FOB	SG	DEL	H	FOB	SG	DEL	H	FOB	SG	DEL	H	FOB	SG	DEL	H	FOB	SG	DEL
-3	324	11	14	-2	72	81	6*-13		28	39	-33*	-2	128	0	3*	9	12	41	-8*
-2	112	11	-8	-1	68	85	7*-12		91	7	0	-1	53	0	-14*	10	159	6	-7
-1	50	25	15*	0	0	69	-2*-11		112	10	-9	0	59	0	42*	11	0	36	-27*
0	55	42	14*	1	32	73	22*-10		392	12	18	1	42	0	38*	12	162	8	-0
1	127	9	-2	2	74	26	-3* -9		229	8	21	2	83	0	41*	13	0	50	-50*
2	0	48	-20*	3	116	12	9 -8		54	20	-3*	3	147	18	-3	14	0	42	-10*
3	0	54	-6*	4	59	18	17* -7		51	39	-10*	4	70	34	-18*	15	0	75	-61*
4	13	45	-22*	5	0	43	-21* -6		185	13	15	5	600	25	26	16	170	9	-13
5	110	15	10	6	74	22	38* -5		102	28	39	6	359	12	19	17	64	36	-38*
6	58	23	1*	K,L=		3,	13 -4		73	0	29*	7	144	9	-19	18	145	24	-10
7	7	69	-17*-10		45	59	43* -3		64	0	3*	8	38	17	19*	19	0110		-18*
8	32	62	4* -9		32	70	30* -2		32	0	-27*	9	26	31	-32*	20	60	23	-1*
9	46	64	-77* -8		91	16	15 -1		89	0	-2*	10	13	49	0*	21	0	59	-2*
10	53	60	-54* -7		0	52	-44* 0		127	0	-47*	11	217	7	-12	K,L=		4,	4
11	108	13	18 -6		99	15	10 1		25	0	-44*	12	46	16	-27*-23		75	80	-9*
12	54	38	42* -5		37	47	31* 2		53	0	-35*	13	18	38	-15*-22		0	52	-78*
K,L=		3,	11 -4		71	24	-22* 3		78	0	60*	14	120	8	-5 -21		42	51	-35*
-17	69	24	-8* -3		21	46	13* 4		457	20	-56	15	0	41	-27*-20		0	60	-24*
-16	124	20	18 -2		44	49	22* 5		5	63	-48*	16	0	44	-9*-19		72	24	2*
-15	0	50	-2* -1		0	48	-2* 6		557	24	0	17	29	45	-23*-18		29	47	-17*
-14	112	13	39 0		43	52	1* 7		436	14	35	18	68	18	30 -17		77	15	23
-13	0	98	-20* 1		55	19	19* 8		222	9	-27	19	68	80	17*-16		0	48	-25*
-12	0	59	-5* 2		90	11	6 9		0	45	-12*	20	0	85	-22*-15		127	16	-3
-11	61	68	57* K,L=			4,	0 10		80	6	10	21	0	64	-2*-14		82	10	13
-10	58	59	56* 0		291	0	5* 11		56	9	4	K,L=		4,	3 -13		158	7	1
-9	71	17	42 1		301	0	-22* 12		18	35	16*-23		0	86	-1*-12		48	21	36*
-8	45	46	30* 2		51	0	-49* 13		27	39	5*-22		153	52	-16*-11		187	7	1
-7	0	57	-15* 3		45	0	6* 14		48	50	-10*-21		0121		-98*-10		68	13	17
-6	43	47	-17* 4		178	0	3* 15		0	40	-22*-20		106	15	22 -9		74	6	-4
-5	118	11	5 5		369	12	-8 16		25	51	9*-19		9	50	-39* -8		28	33	12*
-4	271	10	-6 6		25	65	-27* 17		18	44	12*-18		82	14	-17 -7		26	51	18*
-3	106	12	27 7		144	11	-12 18		62	34	48*-17		16	46	-26* -6		120	8	-3
-2	126	10	10 8		28	43	-0* 19		41	62	-31*-16		114	18	-2 -5		31	34	20*
-1	122	10	16 9		21	34	7* 20		212	31	-14 -15		0	40	-13* -4		32	42	-21*
0	134	15	-20 10		30	35	-10* 21		0136		-39*-14		57	14	5 -3		22	59	-42*
1	0	56	-4* 11		21	44	17* 22		0	47	-26*-13		14	33	9* -2		125	17	-14
2	55	26	11* 12		16	33	-6* K,L=			4,	2 -12		108	6	13 -1		0	50	-4*
3	45	55	18* 13		268	9	1 -22		0	86	-5*-11		26	35	-15* 0		132	10	18
4	52	54	35* 14		0	36	-33*-21		94	26	0 -10		118	7	2 1		62	24	-17*
5	39	52	29* 15		45	26	15*-20		37	47	35* -9		256	9	21 2		321	10	6
6	0	77	-16* 16		129	9	10 -19		40	46	20* -8		469	15	20 3		813	38	25
7	29	54	15* 17		136	9	18 -18		0	54	-26* -7		240	8	-16 4		229	8	-11
8	0	55	-21* 18		62	29	-6*-17		11	43	2* -6		0	51	-17* 5		38	39	17*
9	0	49	-23* 19		76	24	63*-16		56	20	-32* -5		226	12	9 6		62	8	-6
K,L=		3,	12 20		38	73	-50*-15		0	40	-15* -4		89	31	39* 7		182	6	5
-14	0	61	-8* 21		175	38	-22 -14		47	30	-8* -3		81	37	16* 8		25	35	-8*
-13	0	66	-17* 22		0128		-37*-13		85	8	2 -2		21	78	4* 9		28	33	27*
-12	42	49	11* K,L=			4,	1 -12		74	18	-30 -1		237	13	-4 10		28	35	-25*
-11	0	65	-57*-22		0	70	-11*-11		461	14	54 0		90	45	-2* 11		112	8	21
-10	92	15	18 -21		45	53	13*-10		191	7	8 1		199	13	2 12		42	26	-9*
-9	31	53	29*-20		0	83	-8* -9		65	16	19 2		66	27	1* 13		34	41	29*
-8	0	76	-5*-19		75	18	-23 -8		251	9	-6 3		98	14	-10 14		0	53	-34*
-7	25	71	6*-18		125	14	-8 -7		740	24	53 4		167	9	16 15		165	10	-11
-6	0	85	-2*-17		125	9	-1 -6		320	10	12 5		58	15	-13 16		16	62	-47*
-5	32	78	-6*-16		91	11	-3 -5		0	68	-6* 6		20	40	-9* 17		185	25	15
-4	0	72	-3*-15		48	22	18* -4		113	21	7 7		0	34	-6* 18		0100		-10*
-3	74	85	3*-14		268	9	14 -3		52	0	34* 8		20	29	6* 19		116	24	11

STRUCTURE FACTORS CONTINUED FOR
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H	FOB	SG	DEL	H	FOB	SG	DEL	H	FOB	SG	DEL	H	FOB	SG	DEL	H	FOB	SG	DEL
20	0	80	-7*	-10	48	15	17*	6	75	11	2	-13	128	17	-11	10	54	34	4*
K,L=	4,	5		-9	200	7	-11	7	28	40	17*	-12	191	9	12	11	175	10	-9
-22	0	49	-16*	-8	182	6	7	8	122	9	-13	-11	99	18	-6	12	32	52	-25*
-21	0	77	-13*	-7	53	11	-25	9	50	22	36*	-10	0	44	-24*	K,L=	4,	11	
-20	0	96	-25*	-6	0	36	-12*	10	0	43	-1*	-9	59	21	19*	-16	159	10	14
-19	43	48	-18*	-5	171	6	-22	11	61	68	-17*	-8	132	10	6	-15	0	53	-43*
-18	32	56	15*	-4	27	39	-31*	12	198	9	-10	-7	48	32	3*	-14	43	48	-2*
-17	56	22	17*	-3	28	30	19*	13	0	49	-36*	-6	62	14	48	-13	36	74	18*
-16	65	17	-2	-2	0	39	-14*	14	83	67	24*	-5	103	9	-0	-12	23	65	19*
-15	75	13	17	-1	96	6	-5	15	30	88	-43*	-4	81	11	22	-11	0	70	-22*
-14	133	8	-2	0	58	12	16	16	110	34	-35*	-3	71	13	-9	-10	15	50	9*
-13	0	66	-45*	1	31	41	-1*	17	44	48	30*	-2	0	39	-26*	-9	16	46	10*
-12	424	13	-14	2	0	31	-5*	K,L=	4,	8		-1	0	40	-14*	-8	0	66	-17*
-11	279	9	17	3	62	15	23	-21	66	41	18*	0	94	15	1	-7	3	47	-26*
-10	337	11	2	4	91	9	-15	-20	0	68	-15*	1	88	15	-1	-6	82	19	-5
-9	37	41	-10*	5	33	33	28*	-19	25	80	-22*	2	38	56	28*	-5	50	31	42*
-8	114	7	8	6	62	15	-6	-18	0	79	-22*	3	0	57	-15*	-4	108	24	-8
-7	6	29	1*	7	45	16	34*	-17	58	76	56*	4	124	10	-9	-3	161	10	4
-6	43	15	-13*	8	74	23	22*	-16	108	34	8*	5	20	44	9*	-2	294	11	-3
-5	33	43	13*	9	245	9	6	-15	305	12	-7	6	164	8	21	-1	68	20	-3
-4	63	13	3	10	0	42	-11*	-14	104	20	-17	7	63	25	-1*	0	43	58	-14*
-3	34	44	26*	11	66	16	19	-13	50	32	10*	8	48	33	48*	1	0	51	-58*
-2	25	44	-1*	12	145	17	-5	-12	109	26	21	9	76	85	-8*	2	66	20	36*
-1	21	39	-3*	13	228	9	3	-11	115	14	-5	10	47	67	-9*	3	42	60	24*
0	73	13	-7	14	49	54	-12*	-10	73	25	10*	11	0	53	-28*	4	43	67	18*
1	276	9	-2	15	74	44	61*	-9	0	43	-4*	12	71	33	-35*	5	61	47	4*
2	623	28	31	16	80	90	31*	-8	0	49	-16*	13	59	26	26*	6	65	21	56*
3	154	8	9	17	54	29	-22*	-7	48	19	-3*	14	67	20	28*	7	39	51	14*
4	129	7	-13	18	0	47	-8*	-6	0	36	-2*	K,L=	4,	10	8	0	58	-19*	
5	172	6	11	K,L=	4,	7	-5	8	42	-14*	-18	63	29	41*	9	11	48	7*	
6	170	6	15	-21	55	56	-8*	-4	46	18	7*	-17	0	49	-35*	K,L=	4,	12	
7	28	34	-13*	-20	109	28	31	-3	198	7	13	-16	0	73	-1*	-14	51	37	41*
8	98	7	1	-19	0	53	-1*	-2	120	9	6	-15	0	98	-9*	-13	0	49	-12*
9	79	8	9	-18	89	14	9	-1	195	7	-3	-14	57	75	-8*	-12	5	55	-8*
10	114	8	-4	-17	49	35	17*	0	76	14	-7	-13	41	82	-27*	-11	73	19	29
11	69	13	10	-16	66	18	45	1	385	17	-6	-12	44	47	8*	-10	35	65	31*
12	58	17	13*	-15	100	12	35	2	162	7	3	-11	43	50	20*	-9	0	50	-29*
13	76	13	1	-14	192	8	11	3	48	21	9*	-10	56	25	4*	-8	0	65	-24*
14	54	23	20*	-13	40	78	-1*	4	3	45	-12*	-9	141	9	13	-7	0	82	-19*
15	64	20	46*	-12	0	41	-2*	5	58	17	23	-8	32	45	4*	-6	0	85	-7*
16	50	68	-2*	-11	0	40	-19*	6	22	47	-2*	-7	47	32	28*	-5	50	73	18*
17	0	87	-11*	-10	97	9	-2	7	90	11	12	-6	119	10	1	-4	47	86	6*
18	12	47	-38*	-9	105	7	3	8	31	46	-2*	-5	165	8	-3	-3	100	49	-18*
19	33	47	26*	-8	11	42	-1*	9	30	44	-4*	-4	54	78	-30*	-2	55	83	36*
K,L=	4,	6		-7	22	36	19*	10	56	22	12*	-3	59	21	17*	-1	60	69	19*
-22	28	49	17*	-6	217	8	-8	11	71	17	18	-2	124	10	-15	0	0	77	-37*
-21	42	50	-18*	-5	107	12	25	12	0	67	-9*	-1	243	9	6	1	75	21	-9
-20	27	91	15*	-4	13	34	-3*	13	27	76	-1*	0	72	24	19*	2	0	48	-1*
-19	0	69	-19*	-3	74	8	5	14	24	74	-12*	1	42	48	30*	3	47	56	32*
-18	56	25	45*	-2	252	8	-10	15	0	55	-75*	2	28	45	6*	4	62	23	8*
-17	66	18	34	-1	292	10	17	K,L=	4,	9		3	59	22	-30*	5	42	43	-7*
-16	0	45	-1*	0	345	11	-2	-19	19	52	9*	4	30	46	7*	6	54	32	39*
-15	53	21	34*	1	36	28	25*	-18	0	69	-8*	5	41	46	5*	K,L=	4,	13	
-14	0	43	-22*	2	270	9	-6	-17	0	83	-39*	6	45	58	35*	-10	0	70	-59*
-13	202	12	-3	3	64	10	-6	-16	177	30	17	7	26	73	-15*	-9	0	51	-19*
-12	193	12	1	4	64	10	12	-15	61	69	13*	8	0	78	-28*	-8	87	27	50*
-11	179	7	-10	5	18	34	-6*	-14	121	25	17	9	22	50	-35*	-7	41	51	12*

STRUCTURE FACTORS CONTINUED FOR
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H	FOB	SG	DEL	H	FOB	SG	DEL	H	FOB	SG	DEL	H	FOB	SG	DEL	H	FOB	SG	DEL
-6	116	14	-13	3	112	24	-15	13	178	9	-5	-21	0	135	-63*	-8	65	9	8
-5	59	29	2*	4	344	12	-5	14	36	44	-14*	-20	130	12	-3	-7	32	40	-27*
-4	53	30	1*	5	213	10	36	15	60	21	40*	-19	0	48	-18*	-6	54	10	-10
-3	41	47	38*	6	487	21	-3	16	104	15	-12	-18	62	29	18*	-5	13	30	-20*
-2	23	45	-15*	7	0	51	-11*	17	54	24	41*	-17	215	9	-3	-4	70	15	23
-1	0	41	-5*	8	95	13	-19	18	16	53	8*	-16	140	10	-13	-3	14	40	-24*
0	33	45	-17*	9	144	6	-6	19	0	80	-1*	-15	89	33	16*	-2	10	35	-20*
1	16	46	10*	10	27	31	-25*	20	40	78	23*	-14	26	39	20*	-1	161	8	7
K,L=		5,	0	11	0	35	-11*	21	46	46	12*	-13	83	10	-1	0	171	7	1
1	210	0	-33*	12	19	35	16*	K,L=		5,	3	-12	47	16	-18*	1	0	43	-20*
2	86	0	-23*	13	77	11	5	-23	0	54	-32*	-11	212	7	-6	2	123	10	-25
3	68	0	41*	14	48	51	-15*	-22	81	33	-24*	-10	56	12	30	3	207	7	6
4	45	74	-19*	15	26	40	16*	-21	45	77	-6*	-9	41	20	-29*	4	498	20	22
5	139	14	-11	16	25	42	19*	-20	60	23	4*	-8	144	6	-7	5	121	9	4
6	191	9	17	17	29	64	15*	-19	66	19	3	-7	49	27	29*	6	21	32	-15*
7	151	9	-10	18	196	9	-3	-18	73	23	-3*	-6	88	11	-10	7	179	8	-4
8	18	48	1*	19	12	65	-8*	-17	41	55	4*	-5	40	40	12*	8	263	9	25
9	0	34	-1*	20	0	62	-6*	-16	128	9	-6	-4	214	8	-4	9	130	9	4
10	40	20	30*	21	0	48	-27*	-15	40	47	10*	-3	226	7	16	10	83	30	28*
11	33	36	-2*	22	55	43	-0*	-14	69	12	22	-2	145	6	-9	11	184	9	3
12	51	17	-17*	K,L=		5,	2	-13	0	47	-25*	-1	35	40	-3*	12	0	47	-2*
13	25	34	-5*	-23	109	33	-2*	-12	37	25	24*	0	380	16	-20	13	65	17	-15
14	155	13	6	-22	0	54	-11*	-11	65	19	-8*	1	461	25	-7	14	0	54	-15*
15	216	9	-3	-21	50	51	-43*	-10	299	10	26	2	134	8	-2	15	52	57	15*
16	0	45	-37*	-20	44	47	31*	-9	147	10	8	3	33	48	25*	16	82	50	8*
17	0	47	-5*	-19	41	60	31*	-8	90	15	9	4	208	7	5	17	0	70	-31*
18	115	11	-18	-18	66	22	-13*	-7	326	11	1	5	366	17	13	18	0	48	-34*
19	216	9	-21	-17	57	20	5*	-6	105	10	-0	6	89	8	-3	19	0	48	-12*
20	0	110	-33*	-16	88	12	-13	-5	377	19	-9	7	22	32	7*	K,L=		5,	6
21	34	72	5*	-15	66	15	-2	-4	35	45	15*	8	25	31	-24*	-22	65	25	-6*
22	0	48	-47*	-14	169	7	-8	-3	324	11	-4	9	25	33	15*	-21	0	51	-20*
K,L=		5,	1	-13	92	7	9	-2	526	25	43	10	25	46	-28*	-20	0	72	-23*
-22	48	45	25*	-12	121	6	-13	-1	329	12	-4	11	62	13	26	-19	81	19	-22
-21	0	92	-55*	-11	43	17	-14*	0	16	62	-26*	12	50	20	45*	-18	34	48	12*
-20	59	70	-16*	-10	164	11	3	1	222	10	-0	13	0	41	-15*	-17	0	48	-11*
-19	82	23	-15	-9	699	21	32	2	324	19	41	14	0	50	-15*	-16	31	57	10*
-18	0	46	-6*	-8	264	8	3	3	117	10	-20	15	111	12	-3	-15	29	44	-2*
-17	93	13	-15	-7	30	35	13*	4	0	36	-26*	16	0	53	-40*	-14	53	23	-10*
-16	113	10	4	-6	123	10	-14	5	41	41	10*	17	173	23	-8	-13	13	49	-26*
-15	233	9	9	-5	86	25	16	6	39	46	-29*	18	0	95	-15*	-12	37	55	7*
-14	99	11	-0	-4	293	12	31	7	59	14	5	19	59	90	-5*	-11	302	10	13
-13	174	8	-3	-3	0	77	-40*	8	34	21	-12*	20	0	47	-16*	-10	179	7	-5
-12	88	8	-14	-2	125	14	12	9	0	33	-23*	K,L=		5,	5	-9	79	11	-6
-11	122	6	-7	-1	139	15	-17	10	210	8	-4	-22	0	50	-5*	-8	3	34	-28*
-10	32	42	20*	0	48	64	1*	11	120	7	10	-21	0	77	-39*	-7	191	7	-11
-9	95	13	18	1	26	65	-5*	12	205	8	4	-20	0	60	-8*	-6	355	17	17
-8	418	13	10	2	65	69	3*	13	88	24	-9	-19	41	90	40*	-5	203	8	-16
-7	88	7	0	3	275	12	20	14	0	42	-6*	-18	61	24	-30*	-4	40	43	2*
-6	37	52	25*	4	20	56	10*	15	86	40	-15*	-17	84	15	-19	-3	55	19	-0*
-5	67	73	-10*	5	313	10	-17	16	153	9	-11	-16	54	23	18*	-2	199	16	15
-4	48	76	24*	6	0	54	-29*	17	48	63	-1*	-15	45	48	38*	-1	80	10	-14
-3	297	12	19	7	183	7	-3	18	94	51	2*	-14	74	14	-10	0	7	33	1*
-2	98	0	-2*	8	180	7	-9	19	0	63	-23*	-13	129	9	-13	1	33	34	13*
-1	29	0	-8*	9	88	6	-9	20	0	52	-30*	-12	239	8	-0	2	36	36	18*
0	336	0	-6*	10	23	40	-12*	21	0	50	-30*	-11	8	43	-20*	3	144	6	2
1	170	0	-39*	11	185	9	-27	K,L=		5,	4	-10	325	16	4	4	47	18	-6*
2	124	0	-20*	12	206	8	-3	-22	0	73	-12*	-9	178	6	7	5	17	32	6*

STRUCTURE FACTORS CONTINUED FOR
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H	FOB	SG	DEL	H	FOB	SG	DEL	H	FOB	SG	DEL	H	FOB	SG	DEL	H	FOB	SG	DEL
6	201	7	12	-16	75	86	19*	5	51	62	-14*	0	82	49	0*	15	64	19	59*
7	275	9	-2	-15	95	17	27	6	182	15	-9	1	94	18	29	16	182	9	1
8	86	11	-13	-14	74	18	0	7	110	11	-6	2	32	47	27*	17	49	29	18*
9	48	50	45*	-13	269	10	-7	8	70	60	18*	3	107	12	3	18	0	48	-25*
10	230	9	7	-12	107	11	-17	9	41	58	-36*	4	69	35	2*	19	90	31	35*
11	23	66	9*	-11	0	59	-14*	10	55	63	-10*	5	71	21	23*	20	0	62	-41*
12	0	45	-27*	-10	76	12	24	11	102	13	29	6	0	50	-11*	21	96	57	5*
13	23	51	18*	-9	61	15	36	12	25	58	-41*	7	54	28	-1*	22	21	71	11*
14	74	18	-22	-8	34	43	9*	13	0	49	-26*	8	31	48	-0*	K,L=		6,	1
15	154	15	-1	-7	37	38	19*	K,L=		5,	10	9	0	50	-39*	-22	0	49	-38*
16	0	75	-20*	-6	0	38	-7*	-18	0	47	-2*	K,L=		5,	12	-21	35	48	-6*
17	0	54	-2*	-5	59	15	-22	-17	0	49	-40*	-13	52	35	37*	-20	44	85	15*
18	20	61	-18*	-4	0	35	-14*	-16	0	50	-10*	-12	71	20	67	-19	0	48	-57*
K,L=		5,	7	-3	34	36	0*	-15	30	68	8*	-11	82	18	-19	-18	56	59	34*
-21	67	78	-5*	-2	74	12	13	-14	12	84	3*	-10	39	58	-31*	-17	161	9	-16
-20	150	11	-6	-1	320	10	-2	-13	17	71	-1*	-9	30	59	-1*	-16	14	72	-37*
-19	70	24	-19*	0	105	32	0*	-12	100	18	-6	-8	0	58	-11*	-15	220	10	-5
-18	35	62	-2*	1	170	15	-8	-11	52	29	7*	-7	0	83	-7*	-14	362	12	17
-17	87	22	19	2	17	40	-15*	-10	97	12	15	-6	57	72	41*	-13	286	12	14
-16	28	47	-54*	3	0	53	-44*	-9	83	15	1	-5	51	80	13*	-12	0	51	-44*
-15	40	50	-15*	4	151	17	-7	-8	146	9	-19	-4	33	84	23*	-11	94	7	-23
-14	38	49	32*	5	129	19	-1	-7	129	10	-4	-3	38	83	-21*	-10	238	8	28
-13	0	47	-3*	6	0	65	-51*	-6	47	48	-14*	-2	17	77	-27*	-9	37	26	2*
-12	42	34	-6*	7	76	14	16	-5	50	65	21*	-1	31	79	-12*	-8	0	44	-15*
-11	0	50	-7*	8	119	9	11	-4	138	9	-11	0	52	76	17*	-7	61	13	-5
-10	0	39	-29*	9	0	45	-26*	-3	227	9	-5	1	50	54	15*	-6	131	11	-16
-9	24	36	16*	10	57	21	49*	-2	66	18	-6	2	99	18	-5	-5	104	13	33
-8	152	8	3	11	0	50	-6*	-1	0	44	-16*	3	159	15	-2	-4	16	57	-42*
-7	261	21	12	12	61	61	29*	0	61	34	3*	4	47	40	18*	-3	52	69	1*
-6	121	7	-14	13	98	53	-8*	1	64	18	-4	5	55	20	53*	-2	220	15	8
-5	100	7	8	14	3	48	-6*	2	0	45	-16*	K,L=		5,	13	-1	442	14	22
-4	135	8	6	15	0	70	-23*	3	0	46	-2*	-9	45	61	4*	0	281	14	-20
-3	217	19	19	K,L=		5,	9	4	12	47	0*	-8	0	51	-30*	1	113	23	20
-2	133	7	10	-19	42	48	10*	5	134	11	2	-7	50	51	4*	2	193	14	-7
-1	73	9	-11	-18	27	47	17*	6	37	57	18*	-6	56	74	-7*	3	55	61	-15*
0	335	11	-7	-17	0	70	-18*	7	63	90	43*	-5	0	43	-8*	4	198	9	-5
1	119	7	6	-16	34	103	-34*	8	66	95	15*	-4	41	46	-22*	5	82	14	-12
2	177	7	4	-15	99	39	25*	9	73	20	-16	-3	0	42	-21*	6	167	8	-9
3	0	34	-5*	-14	198	11	-12	10	0	66	-19*	-2	0	42	-7*	7	11	36	-27*
4	22	34	-18*	-13	95	26	1	11	119	12	13	-1	36	41	28*	8	91	6	8
5	0	38	-27*	-12	38	62	4*	K,L=		5,	11	0	49	56	14*	9	35	15	22*
6	34	39	-3*	-11	131	13	5	-16	93	15	19	K,L=		6,	0	10	74	8	-15
7	50	20	10*	-10	95	16	-8	-15	37	49	14*	0	747	23	-19	11	127	6	6
8	27	42	-18*	-9	152	14	13	-14	0	48	-45*	1	458	15	17	12	83	8	-9
9	28	44	-26*	-8	53	58	11*	-13	0	73	-6*	2	46	66	-42*	13	35	39	6*
10	0	76	-12*	-7	158	11	9	-12	0	67	-17*	3	86	34	-31*	14	26	40	20*
11	0	45	-31*	-6	46	64	-7*	-11	41	81	38*	4	115	18	23	15	33	41	29*
12	46	53	10*	-5	110	10	-5	-10	0	65	-11*	5	138	10	9	16	53	25	43*
13	0	50	-62*	-4	42	52	40*	-9	60	73	18*	6	22	39	6*	17	53	31	-5*
14	223	11	-19	-3	79	14	-8	-8	12	49	-49*	7	28	40	12*	18	43	74	40*
15	25101		20*	-2	0	55	-16*	-7	0	70	-2*	8	36	43	-3*	19	0	51	-29*
16	0	66	-15*	-1	47	22	27*	-6	8	47	-22*	9	78	6	15	20	146	29	-17
K,L=		5,	8	0	60	28	12*	-5	68	35	-9*	10	0	33	-24*	21	0	78	-20*
-20	30	72	-32*	1	48	50	26*	-4	211	9	-7	11	9	32	-12*	K,L=		6,	2
-19	55	73	1*	2	36	47	32*	-3	0	64	-23*	12	98	12	-17	-22	0	52	-18*
-18	36	77	-35*	3	105	18	3	-2	55	28	-19*	13	262	9	8	-21	77	29	-8*
-17	32	81	-10*	4	111	10	16	-1	98	15	3	14	123	9	-1	-20	25	60	-26*

STRUCTURE FACTORS CONTINUED FOR
ND6(OCH(CH3)2)17CL.

H	FOB	SG	DEL	H	FOB	SG	DEL	H	FOB	SG	DEL	H	FOB	SG	DEL	H	FOB	SG	DEL
-19	30	54	24*	-7	246	8	-3	6	62	8	-9	-21	0	52	-66*	-4	167	7	9
-18	33	46	3*	-6	0	49	-28*	7	68	8	9	-20	64	49	-19*	-3	113	7	-3
-17	10	44	1*	-5	392	24	-28	8	43	22	4*	-19	0	51	-8*	-2	88	12	7
-16	126	13	-5	-4	434	13	21	9	0	39	-1*	-18	66	22	9*	-1	54	16	-20*
-15	105	10	0	-3	436	14	-24	10	67	22	18*	-17	48	50	28*	0	167	8	5
-14	160	8	-7	-2	0	55	-17*	11	95	14	21	-16	41	47	37*	1	0	35	-18*
-13	43	19	26*	-1	404	13	-16	12	41	34	28*	-15	30	49	-8*	2	10	38	-38*
-12	177	7	-1	0	256	9	6	13	0	57	-15*	-14	20	42	9*	3	58	13	-1
-11	69	16	-11	1	88	15	-31	14	0	44	-41*	-13	58	27	-16*	4	21	38	-14*
-10	92	9	0	2	37	32	32*	15	120	10	7	-12	0	41	-19*	5	0	40	-28*
-9	118	7	11	3	51	55	-1*	16	99	13	-6	-11	42	27	-17*	6	3	49	3*
-8	23	41	14*	4	7	36	-16*	17	138	11	-2	-10	32	37	-27*	7	50	54	-16*
-7	300	10	25	5	83	7	6	18	69	89	47*	-9	16	37	-5*	8	96	11	0
-6	183	7	11	6	45	11	-2	19	0	59	-10*	-8	291	9	-5	9	0	64	-11*
-5	17	40	4*	7	0	38	-9*	K,L=	6,	5	-7	158	9	-9	10	0	44	-7*	
-4	116	14	11	8	48	11	-13	-22	58	60	51*	-6	41	41	28*	11	0	46	-44*
-3	354	13	22	9	135	7	7	-21	47	48	35*	-5	283	9	-2	12	105	12	-24
-2	252	13	13	10	135	8	-6	-20	0	95	-2*	-4	376	26	27	13	0	79	-64*
-1	44	72	2*	11	29	47	-52*	-19	102	82	13*	-3	126	6	-5	14	55	78	53*
0	0	73	-44*	12	255	10	5	-18	39	48	-12*	-2	41	16	-6*	15	0	82	-9*
1	47	62	11*	13	159	9	-12	-17	50	35	49*	-1	37	19	-17*	16	70	41	-4*
2	33	55	-5*	14	0	44	-20*	-16	167	9	5	0	80	11	8	K,L=	6,	8	
3	27	44	-10*	15	18	45	-59*	-15	130	10	-3	1	32	26	30*	-20	89	92	-23*
4	24	39	-2*	16	50	30	-21*	-14	40	41	-5*	2	34	24	13*	-19	137	20	5
5	252	8	6	17	0	48	-24*	-13	0	40	-8*	3	14	35	-24*	-18	35	51	-22*
6	41	20	-9*	18	110	35	6*	-12	245	9	1	4	69	8	5	-17	52	39	29*
7	132	6	-19	19	0	73	-34*	-11	19	36	-4*	5	20	34	14*	-16	57	74	18*
8	11	36	2*	20	0	55	-22*	-10	165	6	2	6	136	7	-4	-15	141	14	-10
9	161	6	-6	K,L=	6,	4	-9	81	7	-8	7	70	29	-4*	-14	84	14	40	
10	207	8	-10	-22	68	20	34*	-8	35	24	33*	8	336	11	12	-13	58	23	16*
11	248	8	-23	-21	0	73	-6*	-7	151	7	1	9	284	10	1	-12	0	45	-11*
12	0	37	-43*	-20	0	110	-29*	-6	105	7	-5	10	74	32	-7*	-11	52	22	26*
13	147	8	0	-19	80	90	-22*	-5	0	34	-6*	11	0	56	-4*	-10	130	17	9
14	192	10	3	-18	214	9	-5	-4	15	32	-9*	12	129	18	-18	-9	0	42	-15*
15	16	48	12*	-17	144	10	-2	-3	47	20	8*	13	117	11	8	-8	0	52	-43*
16	0	44	-11*	-16	0	54	-8*	-2	29	33	-48*	14	39	93	9*	-7	52	18	9*
17	32	46	15*	-15	144	18	4	-1	18	42	-8*	15	14	59	-23*	-6	0	46	-23*
18	41	63	-19*	-14	152	8	1	0	50	14	-21	16	32	82	-10*	-5	27	39	-17*
19	49	105	-16*	-13	0	39	-23*	1	115	9	20	17	34	49	30*	-4	0	39	-9*
20	0	82	-2*	-12	0	35	-14*	2	350	17	27	K,L=	6,	7	-3	45	20	32*	
21	0	54	-4*	-11	146	7	-3	3	20	31	0*	-21	112	28	-5	-2	75	11	-5
K,L=	6,	3	-10	97	9	-3	4	44	28	28*	-20	0	81	-46*	-1	104	9	-2	
-22	141	22	9	-9	10	32	-3*	5	135	7	0	-19	129	13	1	0	42	48	33*
-21	0	51	-16*	-8	53	16	15*	6	78	9	5	-18	133	28	-3	1	150	8	-4
-20	54	74	36*	-7	23	30	20*	7	192	9	-3	-17	94	13	16	2	53	21	-20*
-19	59	24	-7*	-6	241	8	9	8	0	49	-8*	-16	32	49	10*	3	0	63	-1*
-18	127	10	12	-5	163	7	-7	9	279	10	-3	-15	45	48	28*	4	44	59	14*
-17	101	12	-8	-4	196	7	-3	10	206	8	4	-14	128	9	-9	5	168	8	1
-16	133	9	5	-3	105	11	-15	11	141	8	5	-13	63	32	39*	6	190	8	-4
-15	21	46	11*	-2	418	18	-27	12	38	42	36*	-12	29	47	19*	7	86	14	-31
-14	38	39	23*	-1	232	8	4	13	53	27	-32*	-11	39	40	22*	8	40	45	-2*
-13	16	37	-11*	0	129	8	13	14	13	45	1*	-10	21	39	17*	9	32	45	-3*
-12	48	19	-4*	1	32	47	4*	15	70	21	6*	-9	97	9	8	10	89	24	5
-11	52	13	21	2	157	7	3	16	18	69	-18*	-8	31	41	9*	11	73	32	32*
-10	66	9	14	3	365	21	23	17	31	59	7*	-7	107	8	12	12	66	76	54*
-9	108	6	-0	4	51	11	-7	18	40	91	2*	-6	329	11	-9	13	0	72	-33*
-8	250	8	11	5	24	30	-12*	K,L=	6,	6	-5	346	25	25	14	0	62	-28*	

STRUCTURE FACTORS CONTINUED FOR
ND6(OCH(CH3)2)17CL.

H	FOB	SG	DEL	H	FOB	SG	DEL	H	FOB	SG	DEL	H	FOB	SG	DEL	H	FOB	SG	DEL
15	33	61	-32*	4	0	67	-19*	-5	48	40	41*	7	22	33	2*	19	28	64	-6*
K,L=	6,	9		5	0	48	-31*	-4	41	51	15*	8	109	6	-2	20	0	48	-34*
-19	6	59	-15*	6	55	82	22*	-3	67	14	64	9	34	18	22*	21	44	47	0*
-18	0	70	-10*	7	70	111	5*	-2	31	42	26*	10	118	6	-17	K,L=	7,	3	
-17	0	73	-23*	8	54	84	53*	-1	66	15	45	11	0	34	-2*	-22	45	65	35*
-16	43	77	8*	9	70	73	24*	K,L=	7,	0		12	82	8	2	-21	45	50	-11*
-15	42	75	24*	10	0	54	-27*	1	336	12	10	13	41	44	13*	-20	0	79	-16*
-14	75	24	0*	11	102	14	0	2	437	14	41	14	0	54	-7*	-19	88	66	21*
-13	0	80	-36*	K,L=	6,	11		3	261	10	2	15	0	42	-9*	-18	87	25	-16
-12	55	61	11*	-15	41	59	30*	4	79	11	-14	16	46	28	29*	-17	41	45	25*
-11	142	9	9	-14	9	46	4*	5	0	47	-3*	17	45	45	5*	-16	83	27	-3*
-10	36	46	-9*	-13	45	65	25*	6	149	9	19	18	97	26	-1	-15	102	11	5
-9	212	13	5	-12	0	65	-25*	7	29	32	17*	19	94	46	-8*	-14	0	41	-2*
-8	236	9	3	-11	0	49	-17*	8	5	33	-11*	20	0	103	-40*	-13	40	27	7*
-7	146	9	1	-10	0	77	-23*	9	59	16	-7	21	0	49	-31*	-12	48	15	15*
-6	0	43	-5*	-9	30	87	14*	10	22	39	20*	K,L=	7,	2	-11	6	35	-20*	
-5	145	9	1	-8	61	50	15*	11	35	41	19*	-22	117	14	16	-10	69	9	-8
-4	46	26	12*	-7	71	35	3*	12	123	12	-11	-21	20	54	-39*	-9	28	33	11*
-3	105	9	-9	-6	0	64	-16*	13	62	14	24	-20	41	75	27*	-8	0	32	-35*
-2	39	59	24*	-5	0	49	-25*	14	253	9	24	-19	0	60	-9*	-7	96	9	12
-1	48	24	14*	-4	47	64	-8*	15	203	12	10	-18	0	47	-39*	-6	82	10	-12
0	83	19	13	-3	31	53	20*	16	0	58	-50*	-17	66	17	55	-5	349	11	-7
1	0	43	-25*	-2	159	15	5	17	0	64	-10*	-16	102	11	17	-4	80	15	-9
2	63	18	47	-1	53	27	22*	18	3	54	-24*	-15	47	56	16*	-3	479	20	-16
3	34	44	10*	0	37	57	21*	19	90	26	3	-14	213	8	1	-2	563	22	-44
4	203	9	4	1	105	34	8*	20	71	73	-5*	-13	252	9	10	-1	321	10	-13
5	205	9	10	2	139	12	27	21	54	56	-16*	-12	107	10	-2	0	86	9	6
6	135	15	1	3	85	20	2	K,L=	7,	1	-11	79	8	-14	1	119	8	12	
7	90	14	1	4	0	46	-0*	-22	0	68	-4*	-10	105	6	-0	2	23	40	19*
8	91	14	4	5	101	10	-0	-21	60	24	28*	-9	101	6	19	3	40	24	37*
9	69	38	-15*	6	0	51	-22*	-20	35	71	23*	-8	67	8	2	4	34	25	20*
10	0	50	-42*	7	70	18	24	-19	57	28	9*	-7	0	35	-10*	5	0	43	-37*
11	43	48	-3*	8	49	35	42*	-18	16	46	-9*	-6	72	7	0	6	54	9	-2
12	0	63	-30*	K,L=	6,	12	-17	81	14	-10	-5	228	9	0	7	27	31	-5*	
13	27	48	17*	-13	82	18	7	-16	197	14	10	-4	246	8	-10	8	25	31	15*
K,L=	6,	10	-12	91	38	-21*	-15	247	9	3	-3	0	43	-68*	9	0	45	-28*	
-17	50	33	11*	-11	75	30	4*	-14	0	44	-2*	-2	119	39	-81*	10	241	8	-1
-16	17	51	7*	-10	0	50	-20*	-13	286	10	-15	-1	53	53	28*	11	261	10	14
-15	0	81	-0*	-9	60	27	16*	-12	233	9	11	0	70	26	-5*	12	167	8	11
-14	85	26	41*	-8	0	85	-47*	-11	64	12	-5	1	49	23	19*	13	73	15	4
-13	0	94	-27*	-7	0	83	-6*	-10	68	9	-6	2	11	47	-0*	14	71	14	11
-12	27	62	-18*	-6	0	70	-3*	-9	104	6	-5	3	25	36	-7*	15	41	45	-1*
-11	44	76	-11*	-5	0	77	-21*	-8	181	6	1	4	298	10	9	16	70	22	-17*
-10	178	9	-8	-4	9	57	-15*	-7	110	8	-2	5	111	11	-8	17	58	78	12*
-9	210	11	-1	-3	59	82	-13*	-6	2	41	-28*	6	24	29	-3*	18	35	97	8*
-8	96	13	-11	-2	0	74	-5*	-5	72	18	-13	7	38	31	-7*	19	51	65	5*
-7	0	50	-44*	-1	0	49	-11*	-4	72	35	-10*	8	51	10	2	20	0	48	-21*
-6	153	9	-15	0	73	78	-14*	-3	152	10	-4	9	101	7	-20	K,L=	7,	4	
-5	38	44	20*	1	121	15	8	-2	41	56	-20*	10	0	50	-2*	-22	32	71	5*
-4	0	45	-25*	2	82	20	22	-1	0	60	-82*	11	290	9	5	-21	23	49	5*
-3	47	30	31*	3	69	23	18*	0	418	14	12	12	297	13	26	-20	75	66	-4*
-2	78	14	21	4	136	11	-19	1	354	11	15	13	182	9	2	-19	62	79	-10*
-1	84	13	-12	5	36	50	-44*	2	284	10	-12	14	0	60	-29*	-18	0	62	-2*
0	66	28	37*	K,L=	6,	13	3	82	22	3	15	34	43	-12*	-17	181	9	-16	
1	0	45	-4*	-8	56	33	41*	4	0	32	-28*	16	0	57	-35*	-16	253	12	-4
2	0	46	-37*	-7	47	61	22*	5	387	17	0	17	49	32	47*	-15	165	11	-6
3	81	22	37	-6	19	52	-36*	6	156	6	-2	18	58	23	41*	-14	28	41	20*

STRUCTURE FACTORS CONTINUED FOR
ND6(OCH(CH3)2)17CL.

H	FOB	SG	DEL	H	FOB	SG	DEL	H	FOB	SG	DEL	H	FOB	SG	DEL	H	FOB	SG	DEL
-13	29	39	-14*	2	12	33	-5*	K,L=	7,	7		-1	69	15	8	-9	89	22	-5
-12	93	13	-0	3	127	6	6	-20	166	11	13	0	186	9	-4	-8	239	9	-1
-11	56	12	-7	4	53	19	21*	-19	106	15	-19	1	104	12	26	-7	191	10	-6
-10	0	34	-15*	5	21	35	4*	-18	0	53	-12*	2	40	58	18*	-6	62	21	16*
-9	29	41	25*	6	115	10	-5	-17	84	21	-2	3	143	8	9	-5	40	51	24*
-8	122	6	-14	7	251	10	-14	-16	23	53	21*	4	169	11	2	-4	51	25	35*
-7	43	12	18	8	346	11	21	-15	42	51	30*	5	107	11	-12	-3	49	27	4*
-6	128	8	-1	9	214	8	5	-14	0	45	-8*	6	0	46	-24*	-2	0	46	-22*
-5	96	15	19	10	0	49	-9*	-13	0	43	-23*	7	147	14	9	-1	24	44	15*
-4	391	12	10	11	153	8	-4	-12	8	43	-23*	8	114	14	4	0	46	55	34*
-3	428	20	-0	12	58	62	10*	-11	66	15	14	9	33	46	4*	1	75	16	29
-2	210	10	1	13	31	50	-12*	-10	0	40	-13*	10	52	38	44*	2	39	46	35*
-1	7	34	-17*	14	0	45	-12*	-9	17	39	14*	11	61	64	25*	3	43	51	38*
0	243	10	18	15	78	17	50	-8	154	9	-5	12	11	69	-55*	4	43	47	39*
1	23	33	20*	16	71	40	4*	-7	284	10	-17	13	0	72	-70*	5	95	39	6*
2	95	6	-11	17	34	59	-44*	-6	137	8	-7	14	0	48	-16*	6	83	75	31*
3	42	12	-5*	18	0	59	-33*	-5	117	10	12	K,L=	7,	9	7	0	89	-31*	
4	69	12	-9	K,L=	7,	6	-4	252	9	1	-18	79	17	3	8	0	89	-17*	
5	33	21	-2*	-21	0	69	-8*	-3	96	9	-11	-17	0	67	-2*	9	64	46	37*
6	31	35	18*	-20	86	17	8	-2	63	17	11	-16	33	59	5*	10	108	12	11
7	16	42	-8*	-19	26	81	-42*	-1	33	38	9*	-15	89	101	24*	K,L=	7,	11	
8	54	14	-6	-18	80	18	18	0	47	19	17*	-14	0	48	-39*	-15	8	63	-27*
9	101	8	-3	-17	30	47	28*	1	143	6	10	-13	43	58	27*	-14	0	48	-13*
10	19	39	17*	-16	5	46	-19*	2	25	44	16*	-12	0	47	-16*	-13	0	48	-3*
11	48	22	17*	-15	75	15	-18	3	23	54	9*	-11	113	11	16	-12	40	48	7*
12	51	20	35*	-14	0	43	-33*	4	100	13	9	-10	179	9	-4	-11	0	82	-8*
13	53	20	23*	-13	70	14	8	5	27	40	14*	-9	182	9	9	-10	0	90	-24*
14	89	15	9	-12	60	17	1	6	0	52	-38*	-8	56	47	25*	-9	67	88	6*
15	31	70	-29*	-11	63	15	-0	7	0	43	-57*	-7	212	11	1	-8	96	49	0*
16	44	48	33*	-10	74	11	12	8	24	43	8*	-6	118	12	17	-7	33	95	31*
17	17	68	-33*	-9	49	15	16*	9	97	11	-0	-5	96	10	6	-6	15	47	7*
18	103	34	-15*	-8	37	28	24*	10	41	48	-15*	-4	0	42	-1*	-5	47	77	7*
19	0	52	-38*	-7	317	10	5	11	84	13	31	-3	49	49	-22*	-4	73	39	32*
K,L=	7,	5	-6	474	15	-6	12	40	73	38*	-2	28	41	22*	-3	55	64	-2*	
-21	0	49	-5*	-5	293	19	-3	13	0	68	-58*	-1	101	10	5	-2	25	69	17*
-20	0	77	-18*	-4	59	18	8*	14	88	32	-27*	0	46	52	10*	-1	55	67	35*
-19	0	93	-1*	-3	118	6	-11	15	85	37	21*	1	37	43	-0*	0	25	93	-18*
-18	129	14	7	-2	154	6	2	16	34	48	-17*	2	0	62	-41*	1	93	28	28*
-17	146	26	6	-1	22	33	14*	K,L=	7,	8		3	131	9	11	2	73	32	27*
-16	130	10	4	0	47	18	45*	-19	50	51	18*	4	57	61	3*	3	121	10	-2
-15	33	44	12*	1	15	38	-25*	-18	77	54	-12*	5	68	26	6*	4	105	28	9
-14	31	43	-16*	2	51	13	13	-17	89	41	-5*	6	214	10	9	5	59	64	-5*
-13	41	51	-20*	3	68	9	-12	-16	0	70	-6*	7	163	16	-4	6	32	47	26*
-12	0	40	-21*	4	8	40	-3*	-15	89	24	22	8	88	74	25*	7	46	49	-9*
-11	75	11	2	5	62	13	-13	-14	108	11	25	9	26	57	-28*	8	47	51	19*
-10	61	16	-17	6	258	10	13	-13	53	61	-26*	10	66	36	54*	K,L=	7,	12	
-9	97	7	4	7	219	8	8	-12	49	29	20*	11	34	48	15*	-12	48	52	33*
-8	83	15	4	8	197	10	2	-11	0	43	-7*	12	0	60	-36*	-11	125	12	16
-7	40	41	-12*	9	73	17	14	-10	62	40	-0*	K,L=	7,	10	-10	108	15	-1	
-6	124	6	-6	10	228	10	-10	-9	101	12	-3	-17	55	29	14*	-9	71	21	26
-5	122	6	-6	11	98	34	-1*	-8	72	38	18*	-16	53	30	40*	-8	0	50	-12*
-4	6	32	-58*	12	35	45	4*	-7	0	41	-4*	-15	54	28	39*	-7	70	71	70*
-3	31	31	-15*	13	62	20	24*	-6	0	54	-1*	-14	19	47	10*	-6	19	80	-2*
-2	26	32	-12*	14	18	75	13*	-5	91	10	-20	-13	29	88	28*	-5	0	52	-6*
-1	80	8	5	15	0	87	-25*	-4	0	40	-45*	-12	67	88	-2*	-4	39	59	22*
0	30	32	24*	16	0	58	-26*	-3	49	51	1*	-11	107	12	26	-3	0	73	-12*
1	70	6	-2	17	0	48	-29*	-2	55	43	27*	-10	113	39	27*	-2	50	65	23*

STRUCTURE FACTORS CONTINUED FOR
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H	FOB	SG	DEL	H	FOB	SG	DEL	H	FOB	SG	DEL	H	FOB	SG	DEL	H	FOB	SG	DEL
-1	21	58	20*	6	117	6	-0	19	24	48	-20*	-9	19	34	-4*	6	225	8	3
0	51	53	8*	7	428	18	18	20	37	51	16*	-8	0	33	-7*	7	186	8	0
1	78	19	3	8	46	13	-15*	K,L=	8,		3	-7	35	22	8*	8	46	28	-24*
2	155	9	-5	9	19	34	18*-21		97	15	-11	-6	140	6	-14	9	203	8	7
3	147	19	-3	10	165	7	-4 -20		0	56	-23*	-5	174	6	7	10	170	8	2
4	58	59	-4*	11	67	15	2 -19		44	84	25*	-4	198	8	1	11	98	22	19
K,L=		8,	0	12	115	8	-4 -18		74	18	-5	-3	98	9	-10	12	61	18	44
0	633	19	47	13	69	12	40 -17		172	10	17	-2	348	11	4	13	38	45	29*
1	352	12	25	14	0	41	-27*-16		81	14	-12	-1	312	13	6	14	52	27	16*
2	5	40	-14*	15	0	62	-40*-15		43	52	22*	0	14	34	-28*	15	59	69	5*
3	87	13	6	16	56	26	42*-14		0	41	-23*	1	17	36	-11*	16	25	75	18*
4	192	7	2	17	75	19	7 -13		0	39	-13*	2	207	14	-5	17	0	58	-28*
5	64	9	-4	18	38	46	38*-12		140	9	-1	3	49	18	-9*	18	62	21	56*
6	67	7	10	19	89	88	-17*-11		0	40	-13*	4	252	8	-9	K,L=		8,	6
7	97	6	0	20	0	50	-40*-10		25	34	12*	5	71	18	-31 -21		35	68	-13*
8	94	6	14	21	0	50	-61* -9		188	7	12	6	52	17	-4*-20		75	32	-15*
9	93	6	-11	K,L=		8,	2	-8	45	15	-6*	7	239	8	3 -19		0	51	-13*
10	21	46	-2*-21		0	50	-33* -7		39	39	5*	8	43	18	3*-18		86	73	8*
11	40	18	19*-20		59	27	-13* -6		70	14	-14	9	35	38	20*-17		52	37	5*
12	168	11	9 -19		0	77	-9* -5		216	21	10	10	0	40	-14*-16		48	34	31*
13	133	8	6 -18		15	53	14* -4		426	13	-5	11	46	25	19*-15		56	24	-2*
14	180	8	-6 -17		0	45	-13* -3		382	22	-40	12	0	57	-26*-14		38	53	13*
15	0	64	-1*-16		50	51	-12* -2		19	44	16*	13	53	33	27*-13		0	53	-40*
16	80	42	-6*-15		144	19	17 -1		301	11	-17	14	15	56	7*-12		202	10	-11
17	43	45	0*-14		91	11	-1 0		177	7	0	15	0	70	-17*-11		34	52	-18*
18	108	11	6 -13		19	41	-3* 1		19	41	7*	16	205	15	-11 -10		75	21	-15
19	0	93	-56*-12		61	12	9 2		9	33	-15*	17	39	97	-12* -9		150	7	8
20	46	60	-18*-11		280	9	3 3		19	29	-19*	18	0	51	-4* -8		124	7	-9
21	26	57	-4*-10		157	8	-12 4		53	10	11	19	47	72	-26* -7		141	9	-15
K,L=		8,	1	-9	65	13	-16 5		40	18	16*	K,L=		8,	5	-6	40	29	10*
-21	0	49	-2*	-8	311	19	2	6	32	32	1*-21		0	57	-12*	-5	260	9	-1
-20	72	19	32	-7	97	8	-11	7	0	32	-24*-20		0	72	-7*	-4	268	10	2
-19	0	91	-32*	-6	87	6	-6	8	29	33	-3*-19		0	71	-25*	-3	176	7	6
-18	0	46	-40*	-5	36	15	-4*	9	173	7	-10 -18		64	99	16*	-2	13	36	-29*
-17	78	14	20	-4	114	7	-4	10	71	17	-7 -17		78	32	47*	-1	36	39	13*
-16	0	54	-16*	-3	274	9	-3	11	53	19	15*-16		151	12	-7	0	68	11	-10
-15	236	14	-7	-2	158	10	-22	12	180	12	17 -15		43	46	-11*	1	39	39	17*
-14	255	9	-3	-1	26	39	0*	13	109	10	7 -14		173	9	1	2	0	35	-8*
-13	220	15	9	0	46	25	-9*	14	58	19	20*-13		51	24	20*	3	0	34	-9*
-12	102	8	-16	1	138	7	6	15	46	36	24*-12		0	46	-6*	4	31	35	12*
-11	44	29	21*	2	138	8	6	16	0	48	-29*-11		365	12	15	5	31	39	19*
-10	71	11	-2	3	63	8	-20	17	170	17	-10 -10		34	48	-23*	6	133	8	8
-9	215	8	7	4	53	9	-2	18	33	87	13* -9		57	14	20	7	103	10	-10
-8	34	39	30*	5	20	33	-16*	19	45	55	27* -8		151	7	2	8	284	12	-3
-7	142	6	-5	6	412	16	7	K,L=	8,		4	-7	84	9	19	9	190	16	-5
-6	49	17	34*	7	72	8	-14 -21		53	31	22*	-6	164	6	9	10	80	15	-17
-5	37	27	33*	8	18	33	-50*-20		32	70	23*	-5	49	13	45	11	19	45	1*
-4	34	41	-0*	9	263	9	2 -19		89	108	12*	-4	46	17	17*	12	59	21	54*
-3	37	39	1*	10	249	9	16 -18		169	21	-5	-3	29	36	-4*	13	0	46	-14*
-2	151	9	-10	11	220	9	5 -17		136	10	-10	-2	127	6	12	14	105	23	3
-1	334	11	-10	12	27	46	15*-16		78	15	34	-1	23	32	14*	15	54	67	-3*
0	206	10	-22	13	133	14	11 -15		85	13	-1	0	30	34	19*	16	0	49	-21*
1	26	44	-0*	14	69	15	10 -14		68	24	3*	1	180	7	-0	17	71	18	16
2	242	9	-22	15	28	51	8*-13		117	15	16	2	57	10	12	K,L=		8,	7
3	256	8	10	16	24	56	13*-12		0	40	-3*	3	179	7	10 -20		50	87	37*
4	128	5	-6	17	22	68	-26*-11		26	36	-10*	4	129	6	2 -19		164	17	4
5	32	21	-16*	18	40	58	33*-10		171	7	2	5	37	52	-26*-18		127	18	8

STRUCTURE FACTORS CONTINUED FOR
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H	FOB	SG	DEL	H	FOB	SG	DEL	H	FOB	SG	DEL	H	FOB	SG	DEL	H	FOB	SG	DEL
-17	0	79	-46*	4	29	55	22*	-3	0	48	-1*	4	44	12	-24	17	61	21	5*
-16	56	26	5*	5	199	9	-3	-2	84	13	6	5	55	11	3	18	60	26	38*
-15	0	55	-27*	6	164	9	4	-1	45	45	-11*	6	364	17	13	19	111	13	-10
-14	0	45	-32*	7	106	11	9	0	0	57	-17*	7	82	9	-10	20	0	50	-43*
-13	0	45	-1*	8	65	22	54*	1	0	47	-17*	8	40	17	12*	K,L=		9,	2
-12	49	24	34*	9	66	69	14*	2	19	46	1*	9	47	13	-18	-21	21	73	13*
-11	47	26	10*	10	0	65	-23*	3	78	15	56	10	31	33	29*	-20	43	48	36*
-10	0	44	-11*	11	0	54	-1*	4	79	36	25*	11	50	21	25*	-19	7	88	-22*
-9	48	30	43*	12	0	65	-27*	5	55	72	30*	12	121	9	-2	-18	0	49	-21*
-8	0	40	-5*	13	42	58	20*	6	81	84	54*	13	29	41	-10*	-17	25	45	22*
-7	72	20	-14	14	68	27	9*	7	0	64	-43*	14	168	8	-5	-16	30	44	25*
-6	218	10	-11	K,L=		8,	9	8	39	47	-3*	15	75	14	2	-15	0	43	-6*
-5	247	9	-22	-18	55	30	30*	9	0	48	-1*	16	38	45	-5*	-14	117	12	4
-4	189	8	-7	-17	48	61	13*	10	0	51	-26*	17	0	46	-14*	-13	202	8	11
-3	44	19	8*	-16	99	19	21	K,L=		8,	11	18	104	12	-4	-12	43	25	29*
-2	66	21	-9*	-15	36	52	-14*	-14	0	50	-23*	19	0	54	-31*	-11	70	20	-1
-1	311	21	31	-14	0	51	-14*	-13	0	49	-9*	20	145	20	6	-10	266	10	-16
0	4	48	-24*	-13	121	28	2	-12	25	55	-12*	21	53	63	-3*	-9	213	7	-6
1	36	45	20*	-12	70	18	13	-11	0	62	-5*	K,L=		9,	1	-8	352	19	-14
2	156	11	2	-11	30	47	-21*	-10	0	79	-13*	-21	0	56	-8*	-7	0	46	-29*
3	40	56	-27*	-10	31	48	-29*	-9	0	88	-14*	-20	72	19	34	-6	201	18	17
4	56	43	-28*	-9	186	9	-17	-8	0	93	-44*	-19	74	55	17*	-5	243	8	-4
5	0	59	-19*	-8	194	9	-10	-7	74	87	48*	-18	47	37	39*	-4	98	8	-11
6	78	13	26	-7	132	10	3	-6	101	86	13*	-17	6	46	-10*	-3	0192		-41*
7	90	16	-11	-6	0	44	-18*	-5	50	73	-2*	-16	80	37	-3*	-2	99	18	-32
8	22	55	-6*	-5	82	23	-2	-4	36	67	34*	-15	81	29	-10*	-1	8	32	2*
9	46	35	5*	-4	68	15	52	-3	167	15	0	-14	37	55	-1*	0	30	38	-7*
10	0	49	-3*	-3	7	43	-52*	-2	40	66	28*	-13	234	9	8	1	65	12	-6
11	60	60	31*	-2	0	42	-9*	-1	45	67	6*	-12	172	9	13	2	42	12	-5
12	10	48	-4*	-1	43	41	-14*	0	89	34	10*	-11	33	46	-17*	3	121	5	-4
13	67	39	-43*	0	85	18	50	1	65	42	17*	-10	110	7	1	4	404	20	26
14	0	67	-45*	1	89	13	32	2	114	20	-12	-9	186	8	6	5	49	24	-7*
15	79	50	-9*	2	52	26	21*	3	96	14	15	-8	44	14	12*	6	56	12	-35
K,L=		8,	8	3	36	51	33*	4	52	26	31*	-7	188	7	-10	7	165	8	2
-19	131	34	-3	4	153	9	7	5	51	23	-10*	-6	27	35	0*	8	168	6	13
-18	20	52	-9*	5	233	12	22	6	7	48	-21*	-5	0	39	-2*	9	28	36	-17*
-17	0	60	-31*	6	101	27	21	7	4	48	-34*	-4	83	10	-4	10	66	17	12
-16	67	69	-1*	7	35	64	0*	K,L=		8,	12	-3	16	49	-24*	11	191	13	11
-15	33	50	-3*	8	82	87	-1*	-11	51	75	-8*	-2	0	71	-25*	12	192	8	16
-14	83	16	-2	9	0	74	-14*	-10	55	56	33*	-1	0	62	-65*	13	78	21	-0
-13	0	74	-12*	10	0	67	-11*	-9	49	51	16*	0	116	10	-8	14	0	43	-16*
-12	86	14	7	11	32	70	21*	-8	0	50	-25*	1	104	11	9	15	27	45	0*
-11	46	34	-27*	12	51	36	14*	-7	0	49	-3*	2	245	9	-0	16	96	16	3
-10	67	25	-8*	K,L=		8,	10	-6	16	67	14*	3	0	31	-20*	17	0	60	-11*
-9	37	42	30*	-16	0	51	-15*	-5	0	46	-5*	4	143	8	2	18	41	60	25*
-8	57	25	2*	-15	56	59	54*	-4	70	51	-12*	5	701	31	2	19	31	49	0*
-7	0	41	-35*	-14	0	53	-32*	-3	28	67	18*	6	107	6	5	20	0	53	-19*
-6	28	46	1*	-13	16	96	15*	-2	44	59	30*	7	40	28	1*	K,L=		9,	3
-5	49	21	2*	-12	10	98	-2*	-1	20	68	-28*	8	238	8	-0	-21	37	54	23*
-4	9	40	-25*	-11	68	105	13*	0	64	39	12*	9	120	6	4	-20	0	57	-18*
-3	85	11	-12	-10	135	25	-18	1	82	13	5	10	133	7	-8	-19	0	68	-3*
-2	222	8	-20	-9	175	15	12	2	61	39	-17*	11	30	38	8*	-18	48	76	1*
-1	54	39	38*	-8	85	16	-3	3	78	15	27	12	63	15	2	-17	28	46	9*
0	101	15	7	-7	32	55	10*	K,L=		9,	0	13	0	42	-42*	-16	32	46	15*
1	107	12	23	-6	66	40	-11*	1	39	69	-47*	14	0	42	-15*	-15	102	10	9
2	138	9	22	-5	80	27	-10*	2	87	14	1	15	31	43	6*	-14	25	42	9*
3	0	44	-13*	-4	67	22	0*	3	211	8	-0	16	20	45	-0*	-13	0	40	-19*

STRUCTURE FACTORS CONTINUED FOR
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H	FOB	SG	DEL	H	FOB	SG	DEL	H	FOB	SG	DEL	H	FOB	SG	DEL	H	FOB	SG	DEL
-12	23	40	-14*	3	27	57	-13*	-20	90	16	0	0	138	28	-2	-10	84	37	-23*
-11	76	14	7	4	328	17	-19	-19	0	50	-19*	1	388	13	24	-9	108	12	2
-10	179	7	-11	5	232	8	23	-18	84	16	23	2	61	23	-5*	-8	0	60	-8*
-9	165	7	-6	6	91	12	6	-17	88	16	75	3	20	42	19*	-7	134	10	-0
-8	22	34	15*	7	0	40	-49*	-16	39	48	28*	4	111	11	-19	-6	0	45	-62*
-7	243	15	-17	8	33	38	15*	-15	106	11	19	5	40	43	-17*	-5	0	44	-11*
-6	107	6	11	9	110	9	3	-14	119	14	15	6	73	18	-10	-4	0	45	-5*
-5	93	8	5	10	60	26	13*	-13	89	13	-6	7	48	30	1*	-3	25	42	14*
-4	77	88	-28*	11	27	42	10*	-12	111	11	0	8	39	46	30*	-2	0	46	-7*
-3	317	32	-41	12	65	15	57	-11	91	12	11	9	84	14	2	-1	87	12	-18
-2	269	9	-10	13	0	44	-20*	-10	274	9	-6	10	65	67	12*	0	0	82	-13*
-1	156	6	4	14	97	12	-18	-9	31	44	16*	11	62	78	33*	1	19	46	-41*
0	81	10	8	15	0	83	-16*	-8	0	39	-10*	12	35	48	29*	2	13	46	-11*
1	55	11	-5	16	50	65	10*	-7	188	10	-2	13	140	21	-17	3	52	30	-16*
2	52	17	-4*	17	90	25	40	-6	232	8	-28	14	32	49	14*	4	45	72	34*
3	149	11	-7	18	149	22	-16	-5	142	9	-18	15	92	15	5	5	50	52	23*
4	27	31	9*	K,L=	9,	5	-4	25	43	4*	K,L=	9,	8	6	90	70	6*		
5	25	32	9*	-21	28	59	-27*	-3	4	39	-21*	-18	83	20	35	7	107	42	5*
6	94	7	6	-20	41	48	35*	-2	113	9	14	-17	140	18	13	8	71	91	29*
7	50	13	18	-19	34	85	30*	-1	51	13	12	-16	69	77	-4*	9	46	65	31*
8	63	10	-3	-18	58	108	-6*	0	24	42	0*	-15	93	94	54*	10	0	48	-22*
9	0	38	-19*	-17	57	70	-12*	1	25	35	-24*	-14	190	9	-6	11	100	22	-22
10	110	11	4	-16	115	11	11	2	42	20	38*	-13	64	22	1*	K,L=	9,	10	
11	232	9	16	-15	75	15	46	3	46	33	37*	-12	78	16	-2	-15	0	67	-19*
12	61	18	-6*	-14	70	17	-7	4	0	39	-12*	-11	0	45	-33*	-14	0	57	-25*
13	35	43	14*	-13	262	10	1	5	71	12	5	-10	0	45	-37*	-13	0	80	-5*
14	0	54	-29*	-12	164	10	3	6	136	9	-0	-9	105	10	1	-12	0	89	-30*
15	199	9	10	-11	44	57	3*	7	10	44	-22*	-8	24	44	-34*	-11	0	80	-20*
16	0	50	-2*	-10	120	26	7	8	177	10	-4	-7	44	51	24*	-10	69	104	34*
17	61	64	52*	-9	298	10	7	9	0	59	-31*	-6	0	49	-19*	-9	0	91	-45*
18	88	27	6*	-8	105	15	12	10	87	12	12	-5	67	15	3	-8	143	10	-1
19	78	87	-25*	-7	40	19	30*	11	86	13	23	-4	43	49	-7*	-7	133	10	11
K,L=	9,	4	-6	128	6	1	12	48	34	-8*	-3	91	29	-7*	-6	17	46	16*	
-21	35	53	34*	-5	72	9	-6	13	69	32	46*	-2	82	13	-21	-5	0	46	-21*
-20	0	49	-52*	-4	42	16	32*	14	83	27	-33*	-1	99	10	4	-4	119	21	-12
-19	0	88	-28*	-3	31	33	12*	15	23	59	-33*	0	385	13	17	-3	84	14	18
-18	55	69	3*	-2	21	32	-6*	16	0	71	-54*	1	37	45	37*	-2	90	41	-11*
-17	82	16	3	-1	39	18	31*	K,L=	9,	7	2	53	25	-2*	-1	54	34	19*	
-16	159	9	-14	0	117	7	7	-19	87	28	13*	3	161	12	-1	0	68	31	30*
-15	120	10	-12	1	130	6	4	-18	0	52	-40*	4	65	18	15	1	95	14	-6
-14	0	51	-35*	2	64	11	3	-17	0	51	-51*	5	65	18	20	2	40	46	28*
-13	45	27	31*	3	375	20	-6	-16	0	80	-40*	6	41	46	20*	3	62	68	60*
-12	191	8	-20	4	168	7	2	-15	48	59	1*	7	103	11	17	4	29	78	6*
-11	57	66	8*	5	77	20	-0	-14	55	24	42*	8	48	48	32*	5	0	70	-10*
-10	35	55	16*	6	148	7	5	-13	27	45	2*	9	0	79	-4*	6	17	56	-42*
-9	56	20	-7*	7	120	8	17	-12	39	46	32*	10	0	67	-8*	7	0	47	-31*
-8	12	34	9*	8	176	8	11	-11	46	50	-30*	11	40	68	16*	8	0	58	-26*
-7	86	8	-6	9	165	8	7	-10	29	41	24*	12	0	48	-38*	9	25	49	12*
-6	21	35	-35*	10	0	62	-6*	-9	0	42	-17*	13	0	49	-7*	K,L=	9,	11	
-5	70	15	3	11	0	48	-9*	-8	62	15	22	K,L=	9,	9	-13	0	68	-1*	
-4	232	8	-3	12	0	44	-21*	-7	156	9	3	-17	33	57	10*	-12	0	51	-38*
-3	271	9	8	13	63	19	45*	-6	27	41	-28*	-16	0	86	-2*	-11	0	51	-6*
-2	105	7	10	14	63	20	37*	-5	47	24	6*	-15	174	27	2	-10	14	68	4*
-1	32	34	-8*	15	13	81	8*	-4	110	12	-11	-14	91	16	29	-9	0	56	-36*
0	111	7	-11	16	20	49	-4*	-3	104	9	10	-13	58	74	-25*	-8	81	10	-47*
1	200	10	19	17	71	19	-8	-2	142	13	8	-12	54	38	9*	-7	0	106	-1*
2	336	18	-13	K,L=	9,	6	-1	37	59	-21*	-11	54	63	54*	-6	0	83	-7*	

STRUCTURE FACTORS CONTINUED FOR
ND6(OCH(CH3)2)17CL.

H	FOB	SG	DEL	H	FOB	SG	DEL	H	FOB	SG	DEL	H	FOB	SG	DEL	H	FOB	SG	DEL
-5	145	17	-3	-10	114	7	6	4	78	27	-33*	-20	0	58	-15*	-3	62	13	6
-4	98	26	25	-9	272	9	-8	5	137	8	2	-19	39	56	39*	-2	67	11	-13
-3	105	18	5	-8	36	39	15*	6	508	23	-9	-18	0	99	-58*	-1	16	50	-1*
-2	62	41	8*	-7	145	6	-2	7	27	44	-3*	-17	58	61	44*	0	22	38	11*
-1	116	29	-13	-6	142	6	-4	8	46	16	-15*	-16	50	36	-19*	1	319	11	11
0	92	23	6	-5	37	15	32*	9	173	7	-3	-15	38	46	19*	2	156	8	-3
1	4	73	-23*	-4	49	15	21*	10	110	23	-15	-14	90	12	40	3	193	10	-15
2	28	58	-29*	-3	27	32	-1*	11	46	54	28*	-13	100	10	21	4	95	13	-9
3	76	15	11	-2	0	39	-1*	12	87	18	20	-12	0	43	-19*	5	162	8	-1
4	42	57	-12*	-1	120	6	-11	13	0	43	-16*	-11	57	18	14*	6	80	12	3
5	60	30	23*	0	26	31	-25*	14	68	17	-12	-10	160	17	-1	7	105	10	9
6	0	48	-12*	1	20	33	-24*	15	0	46	-13*	-9	60	22	24*	8	42	42	-2*
K,L=	9,	12		2	55	12	-16	16	0	48	-2*	-8	6	35	-24*	9	51	23	15*
-9	76	20	43	3	396	13	6	17	0	88	-23*	-7	29	35	-13*	10	49	26	33*
-8	0	56	-3*	4	224	9	-23	18	62	23	17*	-6	30	34	11*	11	0	57	-6*
-7	29	49	29*	5	0	39	-5*	19	0	49	-0*	-5	91	7	17	12	36	52	24*
-6	0	52	-14*	6	205	10	-5	K,L=	10,	3	-4	81	9	-7	13	64	35	-1*	
-5	0	68	-19*	7	573	23	5	-20	16	57	10*	-3	0	33	-2*	14	23	70	19*
-4	34	57	18*	8	75	9	-15	-19	11	65	-25*	-2	85	16	-22	15	0	80	-23*
-3	38	67	28*	9	0	42	-2*	-18	0	77	-23*	-1	112	6	21	16	0	63	-23*
-2	49	75	-40*	10	115	8	-3	-17	101	49	-14*	0	128	8	7	17	30	49	18*
-1	38	55	35*	11	0	54	-4*	-16	53	31	33*	1	76	17	4	K,L=	10,	6	
0	55	66	31*	12	46	25	9*	-15	0	44	-11*	2	455	24	-5	-19	0	50	-15*
1	55	45	-4*	13	0	45	-2*	-14	24	43	-19*	3	228	8	15	-18	71	20	18
K,L=	10,	0	14	33	42	31*	-13	9	41	-18*	4	328	11	-20	-17	0	74	-33*	
0	165	7	2	15	28	45	-27*	-12	85	11	5	5	45	18	-35*	-16	0	76	-12*
1	19	56	10*	16	0	46	-43*	-11	61	39	14*	6	94	8	-0	-15	40	47	-2*
2	27	29	-30*	17	0	68	-36*	-10	0	39	-7*	7	165	7	0	-14	0	65	-48*
3	38	14	8*	18	63	53	55*	-9	281	10	-13	8	33	40	6*	-13	58	62	-20*
4	377	12	-2	19	108	16	-12	-8	73	11	2	9	0	41	-15*	-12	289	10	-8
5	72	10	-13	20	0	61	-56*	-7	228	8	-4	10	0	42	-22*	-11	72	16	25
6	58	11	-11	K,L=	10,	2	-6	95	7	3	11	24	42	20*	-10	76	14	8	
7	91	7	-2	-21	52	38	23*	-5	16	39	2*	12	51	25	9*	-9	86	12	-7
8	98	9	-2	-20	65	23	5*	-4	56	17	-12*	13	50	28	4*	-8	85	10	7
9	65	15	-21	-19	0	62	-7*	-3	110	124	-68*	14	78	17	36	-7	0	39	-37*
10	20	34	14*	-18	50	58	25*	-2	23	43	-11*	15	68	22	34*	-6	0	47	-37*
11	70	12	24	-17	23	56	10*	-1	56	10	-9	16	198	18	-15	-5	0	48	-13*
12	124	8	9	-16	0	45	-12*	0	44	23	7*	17	0	85	-34*	-4	62	13	-12
13	76	13	39	-15	4	44	2*	1	153	7	-2	18	0	58	-22*	-3	51	19	3*
14	151	11	2	-14	17	43	13*	2	42	17	11*	K,L=	10,	5	-2	0	71	-4*	
15	0	64	-22*	-13	28	46	5*	3	144	6	-7	-20	41	60	23*	-1	29	64	21*
16	48	31	10*	-12	0	65	-28*	4	71	8	1	-19	0	70	-43*	0	192	10	5
17	26	57	-7*	-11	211	8	-6	5	30	33	16*	-18	0	73	-10*	1	34	40	27*
18	92	61	-22*	-10	231	8	-24	6	0	34	-13*	-17	0	103	-49*	2	18	40	5*
19	0	54	-2*	-9	23	38	-18*	7	24	39	-4*	-16	38	47	-3*	3	0	40	-16*
20	130	12	7	-8	362	13	-20	8	42	48	1*	-15	54	27	25*	4	45	26	-4*
K,L=	10,	1	-7	155	8	-6	9	99	12	1	-14	113	13	-16	5	55	28	6*	
-20	0	49	-21*	-6	261	8	-1	10	45	26	12*	-13	73	16	24	6	66	15	7
-19	40	83	-45*	-5	83	7	2	11	63	16	41	-12	91	13	-10	7	64	21	30*
-18	0	50	-5*	-4	44	12	-10	12	40	43	23*	-11	464	15	11	8	132	11	-1
-17	83	14	2	-3	122	6	-0	13	0	44	-13*	-10	65	87	-24*	9	0	45	-23*
-16	0	46	-15*	-2	68	24	-12*	14	58	80	30*	-9	0	41	-26*	10	72	17	-6
-15	146	9	-3	-1	28	23	4*	15	0	49	-43*	-8	112	8	-19	11	50	31	17*
-14	0	45	-12*	0	0	32	-8*	16	69	49	27*	-7	22	40	-13*	12	131	13	-7
-13	99	11	13	1	72	6	8	17	217	16	-11	-6	60	14	15	13	34	50	-3*
-12	109	9	8	2	80	7	17	18	0	77	-34*	-5	19	36	-9*	14	79	33	-30*
-11	48	20	5*	3	126	9	-11	K,L=	10,	4	-4	26	36	2*	15	49	49	22*	

STRUCTURE FACTORS CONTINUED FOR
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H	FOB	SG	DEL	H	FOB	SG	DEL	H	FOB	SG	DEL	H	FOB	SG	DEL	H	FOB	SG	DEL
K,L= 10, 7				3	13	49	-3*	3	48	61	-4*	-18	28	53	13*	-2	41	18	21*
-19	81	29	-30*	4	0	45	-27*	4	40	84	-14*	-17	20	58	-8*	-1	19	31	-1*
-18	21	64	-5*	5	44	46	-26*	5	0	63	-1*	-16	113	11	-4	0	58	11	-1
-17	19	62	11*	6	69	18	12	6	37	50	28*	-15	39	46	13*	1	27	31	-27*
-16	0	88	-46*	7	54	65	42*	7	0	48	-3*	-14	49	68	30*	2	15	32	-23*
-15	80	24	24*	8	0	65	-29*	8	54	30	-1*	-13	114	10	11	3	104	8	2
-14	43	47	19*	9	39	64	35*	K,L= 10, 11				-12	56	19	6*	4	278	9	2
-13	0	60	-20*	10	21	63	-32*	-12	0	50	-39*	-11	65	33	7*	5	122	10	-2
-12	30	47	13*	11	28	48	-13*	-11	20	49	7*	-10	80	22	8	6	39	51	-27*
-11	0	51	-46*	12	44	53	19*	-10	0	49	-24*	-9	174	8	-5	7	126	7	-3
-10	36	43	22*	K,L= 10,		9		-9	0	70	-7*	-8	137	6	5	8	222	8	6
-9	67	16	-9	-16	98	27	12	-8	0	71	-2*	-7	188	7	7	9	70	13	-10
-8	25	44	-24*	-15	88	54	7*	-7	0	63	-15*	-6	0	35	-14*	10	0	40	-42*
-7	30	41	-4*	-14	0	92	-16*	-6	72	76	3*	-5	14	33	-21*	11	25	43	-34*
-6	0	41	-8*	-13	185	28	-5	-5	42	61	0*	-4	64	9	-3	12	36	43	-5*
-5	92	10	-15	-12	18	94	-17*	-4	45	71	35*	-3	51	16	-17*	13	52	26	-8*
-4	89	11	-1	-11	40	81	-4*	-3	242	17	3	-2	55	68	-32*	14	79	15	28
-3	19	41	-27*	-10	69	27	23*	-2	89	37	11*	-1	30	32	0*	15	51	32	9*
-2	47	36	1*	-9	109	11	6	-1	53	61	-18*	0	83	15	-29	16	138	23	-5
-1	409	13	-15	-8	0	46	-24*	0	46	55	-28*	1	31	34	21*	17	511	09	24*
0	97	17	2	-7	56	23	-5*	1	0	53	-2*	2	92	6	-3	18	55	66	48*
1	24	45	3*	-6	0	49	-29*	2	0	44	-40*	3	74	9	-32	19	0	63	-9*
2	123	17	-29	-5	0	45	-13*	3	63	22	15*	4	78	10	-12	K,L= 11,			3
3	152	12	4	-4	47	31	18*	4	51	29	42*	5	621	29	12	-20	0	51	-32*
4	74	14	4	-3	0	63	-20*	5	33	44	32*	6	145	18	-21	-19	34	49	-3*
5	0	44	-11*	-2	26	45	-8*	K,L= 10,		12		7	9	63	-33*	-18	0	50	-50*
6	27	45	-19*	-1	0	48	-46*	-7	0	51	-1*	8	160	7	3	-17	16	51	-16*
7	82	14	-15	0	0	56	-7*	-6	0	51	-0*	9	158	10	16	-16	47	63	12*
8	65	18	34	1	105	18	-2	-5	0	54	-1*	10	0	46	-13*	-15	0	46	-41*
9	45	59	-4*	2	53	72	4*	-4	77	22	-5	11	40	37	12*	-14	0	44	-2*
10	33	53	4*	3	53	28	51*	-3	0	63	-19*	12	0	42	-25*	-13	0	42	-6*
11	0	74	-68*	4	0	64	-6*	-2	0	66	-24*	13	56	21	-3*	-12	0	43	-15*
12	47	48	-10*	5	126	33	-9	-1	38	48	9*	14	0	45	-13*	-11	49	23	5*
13	84	17	-2	6	0	84	-6*	K,L= 11,		0		15	0	46	-30*	-10	67	29	-14*
14	0	51	-27*	7	56	69	26*	1	741	24	-54*	16	0	46	-15*	-9	152	9	-10
K,L= 10, 8				8	0	65	-14*	2	102	7	6	17	65	52	15*	-8	41	27	22*
-18	42	50	40*	9	92	29	-1*	3	31	33	22*	18	76	34	-4*	-7	253	10	-15
-17	0	70	-29*	10	0	61	-10*	4	21	32	11*	19	36	67	-39*	-6	104	7	-10
-16	117	40	-3*	K,L= 10,		10		5	0	42	-6*	K,L= 11,		2	-5	88	14	11	
-15	81	82	-27*	-15	50	44	33*	6	333	10	10	-20	0	49	-12*	-4	2020	5	-61*
-14	141	24	-12	-14	82	29	7*	7	38	22	-1*	-19	0	60	-39*	-3	116	7	-24
-13	38	48	17*	-13	0	59	-21*	8	15	37	8*	-18	48	82	1*	-2	167	6	-7
-12	112	14	1	-12	0	72	-29*	9	45	20	32*	-17	74	34	27*	-1	27	32	1*
-11	56	25	-14*	-11	40	80	27*	10	0	44	-26*	-16	9	55	-32*	0	63	12	-22
-10	26	49	14*	-10	74	86	19*	11	67	14	13	-15	47	31	47*	1	195	7	13
-9	36	44	23*	-9	0	95	-3*	12	57	25	11*	-14	39	44	-21*	2	26	35	16*
-8	40	46	-6*	-8	0	111	-40*	13	0	43	-9*	-13	42	42	20*	3	208	7	7
-7	0	43	-43*	-7	0	99	-22*	14	56	33	-2*	-12	36	41	15*	4	46	15	18*
-6	30	60	21*	-6	87	29	47*	15	62	39	-21*	-11	54	23	15*	5	39	20	-3*
-5	48	23	28*	-5	84	15	14	16	27	54	-12*	-10	250	13	13	6	62	11	-14
-4	62	16	20	-4	106	12	2	17	64	75	11*	-9	179	8	-10	7	81	22	5
-3	113	14	17	-3	59	23	52*	18	145	22	-8	-8	338	13	-25	8	69	12	-7
-2	235	9	-7	-2	137	12	-21	19	0	65	-56*	-7	33	37	-33*	9	0	40	-7*
-1	69	17	-18	-1	88	34	-9*	20	105	29	-6	-6	162	7	-8	10	79	14	10
0	126	18	7	0	36	88	-1*	K,L= 11,		1		-5	51	17	-3*	11	110	17	1
1	135	10	5	1	0	70	-16*	-20	0	50	-0*	-4	41	17	5*	12	0	45	-30*
2	237	10	23	2	0	79	-4*	-19	73	47	-14*	-3	0	64	-25*	13	81	14	7

STRUCTURE FACTORS CONTINUED FOR
ND6(OCH(CH3)2)17CL.

H	FOB	SG	DEL	H	FOB	SG	DEL	H	FOB	SG	DEL	H	FOB	SG	DEL	H	FOB	SG	DEL
14	52	58	-3*	-7	36	54	-14*	13	0	50	-25*	3	27	46	-22*	5	14	54	-33*
15	183	16	-24	-6	20	38	4*	14	119	22	-16	4	0	46	-6*	6	51	57	13*
16	38	66	-11*	-5	40	25	20*	15	47	64	-0*	5	61	21	11*	7	0	66	-21*
17	0	57	-18*	-4	21	43	1*	K,L= 11, 7				6	32	46	-5*	K,L= 11, 11			
18	65	27	7*	-3	30	37	14*	-18	0	77	-30*	7	39	52	-12*	-11	0	60	-1*
K,L= 11, 4				-2	0	35	-24*	-17	0	50	-8*	8	56	85	10*	-10	0	51	-16*
-20	123	12	13	-1	26	45	0*	-16	12	63	-6*	9	46	62	15*	-9	6	69	-27*
-19	73	20	3	0	66	21	-17*	-15	72	76	17*	10	28	48	20*	-8	59	46	38*
-18	66	73	-1*	1	75	12	-11	-14	40	46	40*	11	0	48	-10*	-7	0	66	-12*
-17	45	64	-17*	2	45	25	32*	-13	40	66	23*	12	0	49	-8*	-6	0	88	-18*
-16	74	31	-8*	3	312	11	-7	-12	32	49	7*	K,L= 11, 9				-5	141	22	6
-15	0	46	-4*	4	111	10	8	-11	56	24	-16*	-15	157	38	5	-4	80	31	-2*
-14	43	45	34*	5	98	10	-2	-10	0	57	-13*	-14	62	91	10*	-3	70	79	-6*
-13	46	48	36*	6	71	13	12	-9	0	43	-17*	-13	103	41	-12*	-2	28	63	-13*
-12	208	8	-5	7	44	45	15*	-8	84	12	-3	-12	0	72	-43*	-1	124	23	3
-11	80	14	18	8	118	14	10	-7	0	42	-19*	-11	43	83	1*	0	48	36	21*
-10	22	41	-3*	9	57	22	-24*	-6	0	43	-70*	-10	65	39	-0*	1	16	47	15*
-9	75	12	3	10	24	53	2*	-5	0	42	-5*	-9	18	66	-2*	2	34	41	14*
-8	9	54	-29*	11	81	15	-4	-4	94	10	17	-8	45	46	35*	3	0	50	-13*
-7	97	8	-19	12	85	28	21*	-3	127	10	-7	-7	70	18	39	K,L= 12, 0			
-6	29	48	-9*	13	57	66	3*	-2	70	15	-26	-6	73	16	25	0	39	41	35*
-5	0	60	-10*	14	0	78	-28*	-1	46	32	-32*	-5	39	48	2*	1	132	185	-86*
-4	98	7	-10	15	0	49	-16*	0	95	24	-3	-4	38	44	30*	2	44	19	-20*
-3	153	7	10	16	59	45	26*	1	331	13	12	-3	40	45	1*	3	142	9	-3
-2	45	17	-24*	K,L= 11, 6				2	69	31	27*	-2	47	31	8*	4	274	9	2
-1	122	7	-5	-19	47	49	21*	3	0	44	-8*	-1	71	17	2	5	12	46	-6*
0	253	8	11	-18	43	63	5*	4	50	26	-16*	0	0	57	-11*	6	45	51	2*
1	98	8	16	-17	10	56	-9*	5	0	44	-42*	1	38	71	-4*	7	27	35	-1*
2	276	10	-12	-16	0	63	-5*	6	74	15	15	2	37	51	19*	8	42	24	12*
3	33	43	32*	-15	45	76	17*	7	53	56	42*	3	56	24	52*	9	37	38	34*
4	274	9	-22	-14	82	15	2	8	40	47	23*	4	64	45	-1*	10	45	24	-1*
5	172	7	9	-13	9	74	-50*	9	45	56	-13*	5	33	58	31*	11	0	41	-11*
6	82	11	-3	-12	75	78	-18*	10	0	95	-11*	6	81	31	-9*	12	59	18	23*
7	0	42	-36*	-11	91	24	4	11	0	88	-12*	7	0	70	-27*	13	158	9	3
8	38	40	36*	-10	290	11	-5	12	0	50	-30*	8	0	49	-1*	14	0	47	-70*
9	45	47	34*	-9	55	23	-13*	13	105	23	-30	9	52	36	-7*	15	0	47	-47*
10	58	19	11*	-8	23	56	-20*	K,L= 11, 8				10	33	51	15*	16	72	27	-6*
11	54	37	50*	-7	44	45	-10*	-17	33	51	-10*	K,L= 11, 10				17	0	77	-36*
12	18	44	2*	-6	86	10	11	-16	47	58	-14*	-14	12	65	-10*	18	0	78	-49*
13	38	46	37*	-5	56	78	-25*	-15	0	76	-6*	-13	0	51	-19*	19	50	50	6*
14	74	30	-6*	-4	41	50	22*	-14	149	36	-30	-12	62	43	-5*	K,L= 12, 1			
15	63	81	-8*	-3	105	14	-10	-13	13	70	-71*	-11	84	41	4*	-19	67	41	6*
16	57	96	7*	-2	160	8	-6	-12	110	19	-6	-10	0	74	-11*	-18	79	37	6*
17	29	60	-50*	-1	0	49	-1*	-11	0	62	-51*	-9	56	93	30*	-17	79	44	-16*
K,L= 11, 5				0	42	79	27*	-10	0	46	-24*	-8	43	75	-5*	-16	29	47	10*
-19	48	55	47*	1	0	43	-22*	-9	23	45	5*	-7	59	78	15*	-15	22	55	-42*
-18	0	49	-37*	2	38	42	30*	-8	28	46	-14*	-6	48	79	42*	-14	235	9	-1
-17	0	72	-20*	3	45	27	44*	-7	11	44	-8*	-5	33	72	-8*	-13	0	45	-39*
-16	20	68	19*	4	0	42	-28*	-6	0	43	-7*	-4	157	13	-17	-12	39	43	20*
-15	0	60	-7*	5	42	39	40*	-5	70	16	60	-3	84	15	30	-11	79	11	26
-14	0	73	-18*	6	54	57	-1*	-4	0	43	-8*	-2	88	14	-12	-10	19	40	-8*
-13	246	12	4	7	149	9	3	-3	48	30	-26*	-1	63	22	31*	-9	181	10	9
-12	101	19	2	8	124	9	25	-2	71	82	-36*	0	39	62	-1*	-8	47	19	37*
-11	10	58	-13*	9	45	46	-5*	-1	110	11	5	1	44	67	-17*	-7	63	11	1
-10	129	9	-1	10	12	47	-16*	0	317	15	9	2	0	69	-4*	-6	95	8	-12
-9	273	9	-0	11	45	52	-5*	1	52	54	28*	3	8	64	-8*	-5	0	46	-7*
-8	45	30	24*	12	61	51	15*	2	0	69	-37*	4	0	42	-22*	-4	28	33	6*

STRUCTURE FACTORS CONTINUED FOR
ND6(OCH(CH3)2)17CL.

H	FOB	SG	DEL	H	FOB	SG	DEL	H	FOB	SG	DEL	H	FOB	SG	DEL	H	FOB	SG	DEL
-3	0	36	-10*	15	58	92	17*	-5	222	8	-17	15	0	69	-3*	4	0	44	-5*
-2	62	15	-51	16	0	68	-0*	-4	0	64	-20*	K,L=	12,	6		5	0	46	-19*
-1	20	49	19*	17	42	48	32*	-3	52	69	-35*	-18	17	50	3*	6	36	46	31*
0	59	131	-62*	18	28	48	-14*	-2	53	19	-15*	-17	0	49	-8*	7	0	47	-47*
1	56	12	7	K,L=	12,	3		-1	196	7	4	-16	62	80	52*	8	70	73	10*
2	129	6	-4	-19	79	18	24	0	0	43	-11*	-15	0	90	-2*	9	57	92	17*
3	209	7	7	-18	0	72	-29*	1	93	8	13	-14	0	74	-34*	10	31	80	-6*
4	144	16	-16	-17	43	64	-9*	2	279	9	-8	-13	0	68	-43*	11	0	54	-32*
5	34	63	-38*	-16	56	26	13*	3	130	12	18	-12	158	20	-10	12	53	69	-7*
6	103	10	-1	-15	0	46	-4*	4	184	11	1	-11	0	52	-6*	13	3	49	-25*
7	338	11	-4	-14	47	34	11*	5	42	30	16*	-10	39	45	33*	K,L=	12,	8	
8	30	47	-2*	-13	70	15	-2	6	28	61	12*	-9	0	44	-21*	-16	31	59	-42*
9	0	49	-20*	-12	42	38	32*	7	16	41	2*	-8	109	14	9	-15	13	82	-52*
10	0	41	-17*	-11	0	42	-1*	8	69	14	36	-7	164	8	-11	-14	106	42	7*
11	0	51	-13*	-10	0	41	-6*	9	19	44	4*	-6	41	42	3*	-13	0	66	-41*
12	21	66	-27*	-9	142	8	-8	10	70	17	26	-5	178	16	-21	-12	57	92	4*
13	0	54	-7*	-8	35	39	30*	11	0	47	-2*	-4	55	21	46*	-11	55	59	54*
14	39	45	13*	-7	173	8	-5	12	53	28	5*	-3	59	17	-14	-10	24	62	15*
15	15	47	-25*	-6	32	37	-30*	13	43	80	3*	-2	12	40	-28*	-9	54	55	31*
16	53	78	20*	-5	46	20	41*	14	28	80	-13*	-1	20	56	-15*	-8	43	45	17*
17	0	48	-12*	-4	368	12	22	15	33	63	-14*	0	136	14	2	-7	32	45	19*
18	0	49	-23*	-3	14	44	-49*	16	100	27	-13	1	0	51	-18*	-6	0	45	-5*
K,L=	12,	2	-2	0	133	-44*		K,L=	12,	5	2	26	42	16*	-5	0	45	-20*	
-19	28	49	7*	-1	48	29	2*	-19	20	51	-33*	3	0	43	-8*	-4	30	43	13*
-18	0	71	-8*	0	212	7	-0	-18	0	51	-67*	4	46	28	27*	-3	41	44	10*
-17	34	74	26*	1	127	6	-1	-17	0	64	-38*	5	82	20	-5	-2	79	21	-18
-16	0	68	-13*	2	0	35	-22*	-16	57	94	-24*	6	0	44	-9*	-1	88	13	6
-15	134	10	8	3	118	8	-10	-15	0	92	-4*	7	28	46	-19*	0	0	97	-72*
-14	18	49	9*	4	0	39	-0*	-14	35	50	21*	8	59	23	2*	1	81	26	13*
-13	0	55	-13*	5	0	42	-12*	-13	36	47	-19*	9	183	14	-11	2	141	10	12
-12	0	46	-10*	6	0	44	-11*	-12	74	38	-14*	10	53	58	1*	3	23	50	-28*
-11	0	41	-19*	7	0	39	-1*	-11	240	10	-11	11	55	76	-21*	4	25	47	24*
-10	98	21	-8	8	67	14	1	-10	51	35	22*	12	115	20	-5	5	86	44	-4*
-9	0	52	-7*	9	0	42	-17*	-9	46	30	-4*	13	0	49	-5*	6	75	18	54
-8	224	8	-1	10	80	14	-18	-8	31	55	-19*	14	41	51	-20*	7	0	60	-60*
-7	71	16	-9	11	17	45	-11*	-7	25	40	11*	K,L=	12,	7		8	55	29	26*
-6	196	7	-11	12	151	11	-9	-6	62	35	-0*	-17	22	49	13*	9	0	77	-63*
-5	93	7	-3	13	26	54	-29*	-5	0	39	-7*	-16	31	49	14*	10	88	17	12
-4	27	34	-16*	14	0	85	-10*	-4	64	13	28	-15	0	50	-48*	11	70	19	20
-3	120	9	-10	15	8	75	-54*	-3	75	11	-20	-14	24	75	-8*	K,L=	12,	9	
-2	10	33	-17*	16	12	69	6*	-2	0	46	-14*	-13	45	72	24*	-14	0	76	-22*
-1	0	86	-19*	17	134	11	-10	-1	41	24	5*	-12	58	21	41*	-13	109	22	-10
0	38	22	18*	K,L=	12,	4		0	71	18	29	-11	0	46	-33*	-12	0	51	-46*
1	75	7	13	-19	64	26	-5*	1	144	8	-4	-10	14	61	-33*	-11	66	74	-5*
2	39	18	-15*	-18	0	51	-2*	2	113	11	0	-9	83	14	-2	-10	64	25	52*
3	112	7	2	-17	102	37	-16*	3	114	19	6	-8	92	12	14	-9	41	52	1*
4	60	29	-20*	-16	38	64	10*	4	12	41	-15*	-7	45	37	28*	-8	173	18	14
5	120	14	-8	-15	117	22	21	5	50	24	9*	-6	187	8	-10	-7	0	48	-23*
6	309	10	6	-14	49	41	-4*	6	124	9	19	-5	0	57	-33*	-6	0	70	-37*
7	0	39	-16*	-13	0	45	-15*	7	38	43	10*	-4	0	43	-39*	-5	57	61	0*
8	0	46	-30*	-12	0	49	-3*	8	26	45	14*	-3	80	12	-6	-4	29	46	-25*
9	59	17	21	-11	42	50	-26*	9	0	91	-11*	-2	60	18	31*	-3	0	45	-52*
10	69	14	26	-10	108	9	4	10	182	9	2	-1	224	9	-13	-2	0	67	-34*
11	121	16	-21	-9	54	19	10*	11	28	74	2*	0	76	41	9*	-1	61	74	35*
12	48	61	-19*	-8	54	17	38*	12	56	73	41*	1	0	66	-4*	0	42	89	14*
13	146	9	-4	-7	0	39	-58*	13	71	83	1*	2	44	52	-16*	1	102	36	11*
14	115	16	-4	-6	34	42	-12*	14	37	64	-12*	3	61	20	-6*	2	26	62	-11*

STRUCTURE FACTORS CONTINUED FOR
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H	FOB	SG	DEL	H	FOB	SG	DEL	H	FOB	SG	DEL	H	FOB	SG	DEL	H	FOB	SG	DEL
3	31	61	16*	18	64	77	-12*	-1	154	7	14	-17	140	12	-2	4	0	44	-8*
4	116	23	-1	K,L=	13,		1	0	53	18	-10*	-16	59	29	24*	5	0	56	-42*
5	55	58	1*	-18	38	63	21*	1	21	36	20*	-15	85	105	-1*	6	47	30	27*
6	64	24	-1*	-17	53	94	42*	2	28	34	23*	-14	20	46	-21*	7	56	25	-22*
7	60	25	11*	-16	191	27	-11	3	45	50	-9*	-13	60	30	56*	8	268	14	9
8	102	20	-1	-15	69	74	47*	4	33	43	-6*	-12	91	12	1	9	53	66	14*
9	107	15	21	-14	41	48	29*	5	122	8	7	-11	52	59	3*	10	57	29	16*
K,L=	12,		10	-13	36	47	2*	6	0	55	-5*	-10	25	42	0*	11	45	83	-23*
-12	54	55	16*	-12	196	9	1	7	0	40	-29*	-9	72	14	10	12	73	89	-24*
-11	0	59	-28*	-11	66	23	23*	8	50	33	-25*	-8	24	48	-4*	13	0	69	-42*
-10	0	51	-17*	-10	0	41	-1*	9	97	22	-19	-7	77	16	8	14	0	48	-7*
-9	152	14	-5	-9	82	13	12	10	35	45	20*	-6	17	41	-35*	K,L=	13,		6
-8	0	71	-18*	-8	114	8	24	11	201	9	-7	-5	0	68	-45*	-17	0	50	-23*
-7	44	60	-18*	-7	48	21	-32*	12	38	47	25*	-4	73	20	-30	-16	5	49	-15*
-6	49	52	-4*	-6	5	46	-26*	13	126	24	4	-3	332	11	-16	-15	0	58	-20*
-5	28	57	2*	-5	28	37	-18*	14	0	81	-42*	-2	103	9	-0	-14	0	79	-12*
-4	53	77	-3*	-4	36	38	12*	15	79	67	7*	-1	71	13	-26	-13	61	79	57*
-3	33	57	25*	-3	82	8	-3	16	83	25	-11*	0	69	25	2*	-12	0	89	-32*
-2	111	23	5	-2	64	93	-34*	17	0	76	-17*	1	0	47	-37*	-11	0	67	-42*
-1	57	76	24*	-1	38	20	6*	K,L=	13,		3	2	23	41	-30*	-10	90	13	-18
0	2	56	-7*	0	178	31	-46	-18	111	12	19	3	0	41	-21*	-9	62	20	-16*
1	36	54	32*	1	29	38	25*	-17	31	62	11*	4	41	40	1*	-8	71	16	3
2	0	68	-1*	2	68	15	-10	-16	86	28	20*	5	0	41	-3*	-7	199	9	-0
3	22	60	-10*	3	104	7	-10	-15	48	60	27*	6	0	59	-7*	-6	50	28	29*
4	34	41	19*	4	46	17	22*	-14	59	21	42*	7	0	43	-2*	-5	169	13	-24
5	0	42	-17*	5	203	8	3	-13	43	54	26*	8	0	44	-19*	-4	0	69	-50*
6	0	49	-8*	6	131	9	5	-12	41	50	29*	9	71	17	-7	-3	124	20	-17
K,L=	12,		11	7	45	25	1*	-11	7	50	-49*	10	0	46	-4*	-2	95	17	-18
-9	19	51	18*	8	0	41	-11*	-10	0	44	-12*	11	47	62	26*	-1	15	60	-12*
-8	36	78	2*	9	0	61	-13*	-9	12	51	1*	12	27	83	26*	0	0	54	-4*
-7	32	51	20*	10	78	26	3*	-8	28	50	13*	13	0	73	-8*	1	0	43	-4*
-6	0	55	-5*	11	18	43	-4*	-7	46	53	-12*	14	0	48	-18*	2	23	43	-9*
-5	0	66	-2*	12	82	14	4	-6	204	8	6	15	78	18	7	3	0	44	-4*
-4	0	64	-3*	13	37	46	15*	-5	42	59	-24*	16	36	49	13*	4	0	44	-22*
-3	128	28	-5	14	0	94	-12*	-4	0	307	-16*	K,L=	13,		5	5	50	28	22*
-2	67	55	17*	15	0	78	-30*	-3	87	10	3	-18	108	20	17	6	68	18	24
-1	36	61	-16*	16	0	77	-11*	-2	451	14	11	-17	21	64	0*	7	210	9	8
0	48	24	27*	17	72	32	59*	-1	51	41	7*	-16	38	79	-37*	8	56	59	35*
1	0	43	-11*	18	65	81	-4*	0	0	76	-41*	-15	49	77	31*	9	43	69	-33*
K,L=	13,		0	K,L=	13,		2	1	122	8	-2	-14	35	77	1*	10	32	82	6*
1	188	190	-105*	-18	52	64	29*	2	67	16	-19	-13	46	72	5*	11	114	62	5*
2	93	8	4	-17	0	58	-56*	3	76	34	-11*	-12	36	45	14*	12	0	63	-3*
3	123	9	-23	-16	0	80	-14*	4	0	45	-25*	-11	0	68	-8*	13	34	56	-11*
4	20	37	-31*	-15	42	62	37*	5	51	18	37*	-10	80	16	-7	K,L=	13,		7
5	25	38	-21*	-14	62	22	-3*	6	0	43	-9*	-9	55	21	-13*	-16	56	62	33*
6	120	8	-6	-13	166	9	8	7	65	15	-8	-8	69	15	5	-15	61	23	49*
7	0	38	-3*	-12	59	20	-11*	8	72	14	16	-7	32	42	-18*	-14	0	50	-8*
8	0	39	-3*	-11	0	46	-2*	9	0	44	-33*	-6	65	40	6*	-13	23	82	22*
9	0	40	-5*	-10	63	16	23	10	157	9	3	-5	0	43	-10*	-12	32	78	14*
10	36	41	6*	-9	80	12	5	11	0	47	-25*	-4	0	41	-4*	-11	58	62	16*
11	67	16	-6	-8	107	11	-4	12	86	20	4	-3	0	42	-11*	-10	34	55	23*
12	71	19	49	-7	70	13	2	13	68	21	-3*	-2	0	40	-24*	-9	33	56	31*
13	0	46	-31*	-6	0	42	-9*	14	92	30	-1*	-1	65	14	-8	-8	152	9	3
14	0	48	-6*	-5	154	7	3	15	77	26	-31*	0	33	50	-4*	-7	0	46	-26*
15	157	30	-12	-4	10	68	4*	16	26	62	-34*	1	0	41	-19*	-6	106	12	-25
16	0	103	-38*	-3	0	186	-41*	K,L=	13,		4	2	0	51	-2*	-5	47	30	25*
17	50	43	-4*	-2	15	45	3*	-18	38	67	-3*	3	47	25	20*	-4	162	9	-20

STRUCTURE FACTORS CONTINUED FOR
ND6(OCH(CH3)2)17CL.

H	FOB	SG	DEL	H	FOB	SG	DEL	H	FOB	SG	DEL	H	FOB	SG	DEL	H	FOB	SG	DEL
-3	40	49	23*	0	61	64	33*	-9	0	55	-46*	11	158	10	-13	-3	49	27	-28*
-2	12	43	-11*	1	0	73	-1*	-8	54	18	47*	12	0	54	-26*	-2	38	42	-31*
-1	0	55	-56*	2	35	62	-4*	-7	46	53	-4*	13	154	34	6	-1	218	9	-13
0	58	39	35*	3	0	66	-19*	-6	23	51	19*	14	66	83	3*	0	126	11	14
1	80	15	-11	4	59	27	-12*	-5	83	12	30	15	0	73	-24*	1	51	21	20*
2	0	80	-12*	5	0	53	-8*	-4	16	38	15*	16	0	49	-9*	2	0	42	-19*
3	0	69	-20*	6	164	13	-8	-3	0	48	-27*	K,L=	14,	3		3	76	12	41
4	53	26	48*	7	14	50	12*	-2	104	16	-18	-18	70	23	12*	4	0	72	-30*
5	0	46	-16*	K,L=	13,	10		-1	38	31	-3*	-17	37	50	26*	5	0	64	-15*
6	55	63	37*	-11	114	29	-1	0	0	75	-155*	-16	66	32	-4*	6	114	20	13
7	0	89	-13*	-10	20	52	-2*	1	41	27	25*	-15	41	65	23*	7	109	11	-12
8	0	87	-13*	-9	94	17	27	2	177	11	-4	-14	61	86	42*	8	68	18	-1
9	43	63	4*	-8	0	53	-29*	3	27	39	-0*	-13	83	64	-10*	9	29	46	8*
10	47	76	15*	-7	163	33	7	4	54	19	33*	-12	81	14	27	10	51	61	39*
11	0	48	-41*	-6	31	51	-1*	5	0	46	-52*	-11	62	24	-5*	11	68	22	62*
12	48	68	19*	-5	31	43	-14*	6	12	51	-15*	-10	0	43	-3*	12	0	84	-14*
K,L=	13,	8		-4	48	59	-29*	7	35	41	13*	-9	66	15	23	13	0	74	-4*
-15	0	87	-18*	-3	32	59	25*	8	0	51	-1*	-8	0	42	-2*	14	0	53	-30*
-14	0	54	-52*	-2	0	49	-30*	9	35	43	-6*	-7	15	41	-17*	15	52	57	8*
-13	27	49	-9*	-1	30	44	17*	10	70	21	-19*	-6	0	72	-8*	K,L=	14,	5	
-12	53	85	-1*	0	0	46	-15*	11	74	16	15	-5	78	51	-27*	-17	23	67	10*
-11	0	93	-35*	1	0	41	-14*	12	58	23	-1*	-4	386	12	3	-16	89	35	-25*
-10	64	87	25*	2	0	56	-36*	13	56	39	44*	-3	51	22	14*	-15	25	70	-44*
-9	0	46	-57*	3	0	45	-21*	14	53	87	26*	-2	0	48	-25*	-14	57	79	12*
-8	0	62	-39*	4	14	50	9*	15	21	98	-1*	-1	57	24	18*	-13	25	53	-19*
-7	39	46	20*	K,L=	13,	11		16	0	48	-3*	0	230	9	0	-12	62	63	2*
-6	19	51	4*	-4	30	48	-13*	17	25	48	-14*	1	32	56	19*	-11	55	24	36*
-5	61	74	17*	-3	0	43	-13*	K,L=	14,	2		2	54	33	40*	-10	11	46	6*
-4	61	19	13*	K,L=	14,	0		-18	58	27	43*	3	44	26	20*	-9	47	32	-5*
-3	37	50	15*	0	41	48	10*	-17	56	72	53*	4	54	17	17*	-8	0	45	-25*
-2	0	56	-54*	1	144	57	-144*	-16	45	85	22*	5	0	41	-22*	-7	48	30	9*
-1	60	20	6*	2	48	20	-19*	-15	121	37	-3*	6	0	42	-20*	-6	81	13	-6
0	88	22	2	3	150	7	3	-14	54	66	12*	7	84	11	72	-5	0	43	-20*
1	60	22	32*	4	57	15	-13	-13	0	47	-7*	8	0	54	-30*	-4	47	25	9*
2	55	67	26*	5	41	44	37*	-12	100	12	16	9	0	46	-47*	-3	89	11	-12
3	59	65	8*	6	41	41	33*	-11	70	17	-9	10	74	20	-32	-2	54	31	2*
4	45	51	22*	7	0	40	-9*	-10	111	10	-6	11	28	48	19*	-1	0	42	-73*
5	75	26	-20*	8	43	28	3*	-9	0	46	-26*	12	166	31	1	0	28	52	21*
6	0	52	-11*	9	49	47	26*	-8	41	42	-5*	13	0	76	-37*	1	88	12	4
7	99	23	-24	10	71	36	18*	-7	37	41	26*	14	67	83	61*	2	91	11	22
8	52	32	12*	11	0	46	-15*	-6	0	40	-16*	15	0	76	-34*	3	45	34	28*
9	0	49	-34*	12	26	47	25*	-5	0	41	-54*	16	46	47	45*	4	60	26	46*
10	0	48	-6*	13	155	21	-10	-4	78	43	-12*	K,L=	14,	4		5	125	10	6
K,L=	13,	9		14	68	95	66*	-3	250	9	12	-17	135	27	2	6	151	18	-1
-13	78	33	20*	15	0	92	-30*	-2	44	23	-1*	-16	59	30	36*	7	0	48	-7*
-12	0	51	-16*	16	0	76	-33*	-1	0	39	-14*	-15	99	28	-2	8	0	72	-38*
-11	0	52	-2*	17	58	67	8*	0	0	48	-45*	-14	58	84	57*	9	0	62	-17*
-10	174	12	-3	K,L=	14,	1		1	27	38	9*	-13	23	56	16*	10	155	22	-27
-9	63	70	61*	-18	0	50	-50*	2	80	11	-3	-12	37	45	12*	11	0	53	-5*
-8	46	56	19*	-17	12	49	-20*	3	38	39	11*	-11	76	15	23	12	0	89	-23*
-7	0	78	-4*	-16	0	85	-5*	4	34	39	13*	-10	0	43	-23*	13	0	47	-15*
-6	116	22	-9	-15	24	91	5*	5	55	36	-9*	-9	0	48	-13*	K,L=	14,	6	
-5	33	45	20*	-14	252	18	-6	6	0	40	-12*	-8	17	52	0*	-16	65	23	35*
-4	0	74	-18*	-13	60	63	-2*	7	39	47	-3*	-7	32	42	13*	-15	10	75	-16*
-3	54	54	21*	-12	0	51	-31*	8	51	25	-45*	-6	14	68	9*	-14	0	49	-5*
-2	71	38	24*	-11	0	45	-8*	9	136	9	7	-5	180	8	-4	-13	0	91	-21*
-1	0	74	-13*	-10	58	19	17*	10	0	47	-25*	-4	0	42	-8*	-12	0	50	-27*

STRUCTURE FACTORS CONTINUED FOR
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H	FOB	SG	DEL	H	FOB	SG	DEL	H	FOB	SG	DEL	H	FOB	SG	DEL	H	FOB	SG	DEL
-11	38	45	34*	-9	0	80	-11*	7	0	42	-13*	-6	145	8	1	-16	6	51	3*
-10	9	65	-24*	-8	0	71	-18*	8	0	44	-4*	-5	138	8	-0	-15	105	13	22
-9	81	16	14	-7	0	58	-15*	9	0	45	-16*	-4	0	46	-54*	-14	11	50	-56*
-8	0	51	-14*	-6	49	70	46*	10	66	17	50	-3	0	46	-17*	-13	0	75	-10*
-7	142	10	-11	-5	0	66	-35*	11	0	46	-38*	-2	31	40	24*	-12	51	28	35*
-6	0	46	-24*	-4	0	65	-9*	12	67	19	10	-1	78	12	-15	-11	52	26	24*
-5	209	10	-16	-3	8	82	-17*	13	0	103	-20*	0	0	49	-10*	-10	53	37	31*
-4	19	44	2*	-2	59	63	-2*	14	0	70	-9*	1	20	41	-15*	-9	35	44	28*
-3	95	11	4	-1	42	71	-6*	15	120	21	-5	2	0	54	-16*	-8	40	43	36*
-2	28	50	-13*	0	0	77	-16*	16	0	77	-22*	3	0	50	-2*	-7	0	54	-24*
-1	56	18	32*	1	39	70	20*	K,L=	15,	1		4	97	26	-10	-6	0	44	-42*
0	39	54	-25*	2	76	38	53*	-17	0	83	-12*	5	72	14	9	-5	0	55	-31*
1	0	64	-16*	3	47	51	6*	-16	102	34	-11*	6	37	43	-5*	-4	0	59	-55*
2	0	62	-12*	4	40	53	-9*	-15	0	70	-6*	7	0	61	-1*	-3	237	12	-4
3	20	44	13*	5	127	9	-6	-14	0	89	-6*	8	58	22	11*	-2	77	14	-6
4	0	45	-37*	6	0	48	-19*	-13	44	96	38*	9	82	15	15	-1	25	58	11*
5	82	14	19	7	34	61	-36*	-12	154	15	-1	10	36	48	-34*	0	88	25	28
6	74	16	34	8	20	49	4*	-11	127	10	3	11	140	19	-17	1	43	43	41*
7	25	97	-33*	K,L=	14,	9	-10	47	58	24*	12	0	99	-24*	2	121	10	-8	
8	53	82	21*	-12	54	36	-2*	-9	0	45	-28*	13	101	90	13*	3	13	45	-6*
9	190	33	-12	-11	82	18	51	-8	44	35	-5*	14	0	73	-9*	4	155	16	-7
10	11	51	-20*	-10	39	52	20*	-7	64	16	6	15	0	56	-23*	5	40	45	7*
11	0	97	-45*	-9	57	36	21*	-6	49	22	47*	K,L=	15,	3	6	92	13	13	
12	40	56	12*	-8	193	13	-8	-5	0	41	-47*	-17	0	50	-3*	7	0	47	-19*
K,L=	14,	7		-7	64	45	26*	-4	34	40	1*	-16	49	49	-7*	8	0	57	-51*
-15	18	50	2*	-6	0	63	-27*	-3	58	57	-8*	-15	80	53	24*	9	63	21	-2*
-14	47	49	29*	-5	37	63	-2*	-2	47	23	10*	-14	0	62	-7*	10	23	85	-21*
-13	0	49	-5*	-4	13	62	-26*	-1	55	21	27*	-13	66	82	57*	11	42	85	12*
-12	0	72	-9*	-3	10	52	-19*	0	116	29	-44	-12	46	63	35*	12	0	84	-22*
-11	58	91	37*	-2	18	64	5*	1	24	54	-5*	-11	106	11	-1	13	0	47	-6*
-10	0	54	-24*	-1	35	61	28*	2	100	10	-9	-10	51	27	42*	14	0	57	-22*
-9	59	51	11*	0	0	71	-40*	3	56	17	0*	-9	88	13	-7	K,L=	15,	5	
-8	0	84	-55*	1	49	65	19*	4	0	58	-4*	-8	0	55	-16*	-16	70	22	3*
-7	43	84	24*	2	0	54	-7*	5	156	9	22	-7	101	10	-7	-15	0	51	-33*
-6	203	11	-7	3	77	13	33	6	70	15	-2	-6	82	28	2*	-14	0	56	-22*
-5	16	46	-18*	4	137	11	2	7	0	60	-49*	-5	0	71	-24*	-13	95	55	-21*
-4	87	14	-9	5	42	53	42*	8	42	64	0*	-4	0	49	-35*	-12	58	29	52*
-3	27	45	-39*	6	62	23	-10*	9	125	10	3	-3	46	62	9*	-11	0	47	-4*
-2	27	44	-21*	K,L=	14,	10	10	99	22	22	-2	300	11	-1	-10	37	46	3*	
-1	40	44	24*	-8	66	27	42*	11	11	46	2*	-1	64	16	-1	-9	83	19	3
0	97	21	54	-7	64	78	8*	12	73	17	11	0	0	59	-6*	-8	52	25	6*
1	23	58	2*	-6	0	50	-4*	13	37	101	28*	1	0	43	-22*	-7	0	45	-30*
2	0	46	-4*	-5	61	20	3*	14	0	75	-15*	2	0	42	-5*	-6	93	12	7
3	0	47	-32*	-4	40	45	5*	15	34	66	18*	3	12	43	-23*	-5	43	35	26*
4	67	18	41	-3	21	46	12*	16	24	73	24*	4	39	48	35*	-4	0	46	-9*
5	46	71	39*	-2	0	42	-21*	K,L=	15,	2		5	43	48	-2*	-3	37	42	35*
6	25	58	9*	-1	16	42	0*	-17	57	27	51*	6	11	44	-34*	-2	55	61	50*
7	0	81	-3*	0	43	48	13*	-16	0	51	-6*	7	76	15	6	-1	108	10	-0
8	61	81	2*	1	18	43	14*	-15	0	76	-10*	8	32	49	13*	0	0	53	-2*
9	56	31	38*	2	0	43	-25*	-14	56	102	-3*	9	0	47	-51*	1	92	24	2
10	0	48	-15*	K,L=	15,	0	-13	136	46	9*	10	119	35	2	2	10	45	6*	
K,L=	14,	8		1	81	92	-11	4*	-12	106	33	-13*	11	67	90	20*	3	153	9	-7
-14	0	52	-20*	2	0	44	-12*	-11	0	47	-17*	12	64	105	-21*	4	0	46	-14*
-13	22	59	-1*	3	117	9	10	-10	111	32	-4	13	25	78	-9*	5	45	46	36*
-12	55	46	15*	4	72	12	7	-9	36	45	-7*	14	58	23	26*	6	60	29	19*
-11	0	51	-52*	5	0	41	-4*	-8	121	17	-7	15	62	53	55*	7	116	20	18
-10	0	50	-16*	6	55	19	-2*	-7	0	65	-15*	K,L=	15,	4	8	168	26	-19	

STRUCTURE FACTORS CONTINUED FOR
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H	FOB	SG	DEL	H	FOB	SG	DEL	H	FOB	SG	DEL	H	FOB	SG	DEL	H	FOB	SG	DEL
9	49	77	39*	K,L=	15,	8	-14	89	82	-22*	10	43	87	33*	6	141	17	13	
10	0	92	-12*-12	0	58	-28*-13		58	61	14*	11	75	87	-8*	7	83	39	11*	
11	58	24	50*-11	54	32	52*-12		0102		-28*	12	0	76	-18*	8	47	76	-11*	
12	0	48	-37*-10	0	51	-51*-11		61	75	60*	13	23	64	0*	9	0	84	-4*	
K,L=	15,	6	-9	101	17	20	-10	37	52	24*	14	52	30	41*	10	0	85	-13*	
-15	0	52	-23*	-8	25	62	-11*	-9	145	9	0	K,L=	16,	3	11	0	47	-24*	
-14	54	37	-25*	-7	0	79	-12*	-8	66	17	56	-15	19	49	-6*	12	47	38	34*
-13	0	69	-13*	-6	11	60	-12*	-7	82	13	5	-14	0	54	-3*	K,L=	16,	5	
-12	33	73	23*	-5	45	78	4*	-6	45	48	26*-13		0	61	-64*-14		48	50	12*
-11	0	74	-37*	-4	27	78	-38*	-5	0	43	-47*-12		39	81	-1*-13		0	51	-28*
-10	0	88	-60*	-3	29	45	11*	-4	0	42	-17*-11		44	93	-25*-12		36	59	-22*
-9	57	71	42*	-2	50	63	44*	-3	0	42	-9*-10		0	74	-18*-11		157	35	2
-8	54	64	0*	-1	44	63	1*	-2	19	53	-8*	-9	104	12	-19	-10	80	19	53
-7	159	18	0	0	92	25	-8	-1	40	51	0*	-8	61	21	-13*	-9	0	54	-38*
-6	0	56	-6*	1	37	69	-2*	0	41	55	-26*	-7	35	50	-15*	-8	66	33	13*
-5	130	10	-10	2	75	14	-2	1	0	59	-13*	-6	0	72	-37*	-7	33	58	-4*
-4	62	20	16*	3	73	14	11	2	0	51	-32*	-5	86	13	-2	-6	39	66	-15*
-3	57	26	-10*	4	54	20	12*	3	133	9	2	-4	135	9	-8	-5	55	23	30*
-2	0	62	-25*	5	7	44	-62*	4	52	30	48*	-3	22	69	17*	-4	0	44	-15*
-1	0	49	-2*	6	7	58	-4*	5	0	74	-6*	-2	0	69	-1*	-3	59	36	11*
0	41	53	32*	7	98	28	14	6	34	48	-23*	-1	41	41	12*	-2	58	21	7*
1	0	47	-7*	K,L=	15,	9	7	209	9	5	0	0	77	-34*	-1	89	17	29	
2	0	46	-33*-10	123	31	-4	8	30	46	4*	1	96	11	18	0	50	55	30*	
3	49	31	28*	-9	19	86	9*	9	20	54	-28*	2	0	44	-0*	1	152	12	7
4	47	57	31*	-8	61	64	38*	10	83	14	23	3	68	18	1	2	76	35	15*
5	20	46	-1*	-7	56	33	54*	11	69	51	22*	4	0	50	-19*	3	76	59	2*
6	49	73	17*	-6	92	20	1	12	35	64	5*	5	68	17	33	4	0	48	-22*
7	108	24	-19	-5	0	51	-30*	13	25	80	8*	6	21	46	-4*	5	138	16	-7
8	38	77	9*	-4	0	43	-13*	14	0	48	-2*	7	41	46	31*	6	63	91	11*
9	38	73	7*	-3	39	41	35*	15	50	33	47*	8	73	16	67	7	56108		38*
10	0	71	-4*	-2	10	46	-16*	K,L=	16,	2	9	100	12	23	8	0	97	-16*	
11	68	23	7*	-1	22	63	1*-16		0	49	-29*	10	55	68	6*	9	49	69	30*
K,L=	15,	7	0	0	41	-24*-15		0	66	-37*	11	12	84	0*	10	22	48	-31*	
-14	0	57	-4*	1	34	56	5*-14		28	74	-4*	12	41	82	-11*	11	0	57	-5*
-13	71	20	50	2	44	48	27*-13		28	97	28*	13	0	47	-20*	K,L=	16,	6	
-12	0	60	-15*	3	37	50	10*-12		40	99	-39*	K,L=	16,	4	-14	0	51	-7*	
-11	0	74	-5*	4	60	26	21*-11		0	66	-33*-15		52	41	12*-13		66	23	33*
-10	36	55	24*	K,L=	16,	0	-10	174	9	-11	-14	28	58	-2*-12		110	14	-11	
-9	64	76	59*	0	34	49	-4*	-9	9	47	-15*-13		0	50	-2*-11		53	35	19*
-8	68108		-5*	1	80104		-32*	-8	154	23	-10	-12	51	40	20*-10		35	67	-3*
-7	44101		18*	2	45	29	-9*	-7	35	48	-24*-11		0	51	-31*	-9	0103		-13*
-6	88	36	-1*	3	0	42	-15*	-6	71	17	-12	-10	39	45	10*	-8	0	85	-26*
-5	51106		42*	4	95	20	29	-5	0	95	-26*	-9	49	29	27*	-7	0108		-28*
-4	110	17	-9	5	46	68	-2*	-4	84	33	19*	-8	23	45	-1*	-6	0	68	-8*
-3	90	13	7	6	9	52	4*	-3	127	8	6	-7	71	17	54	-5	101	37	11*
-2	13	45	0*	7	0	45	-1*	-2	0	42	-32*	-6	0	45	-24*	-4	51	52	37*
-1	25	52	9*	8	86	13	19	-1	0	41	-7*	-5	71	17	44	-3	6	57	-31*
0	0	82	-18*	9	35	45	5*	0	30	50	-3*	-4	13	44	-20*	-2	66	23	38*
1	126	23	34	10	68	17	33	1	17	42	-21*	-3	0	62	-25*	-1	61	70	39*
2	20	71	6*	11	60	26	51*	2	76	13	22	-2	0	60	-21*	0	68	29	57*
3	38	74	8*	12	56	74	46*	3	0	43	-27*	-1	101	11	7	1	82	26	82*
4	16	49	-17*	13	11	89	-62*	4	0	54	-1*	0	146	12	12	2	0	70	-16*
5	40	66	-5*	14	0	50	-40*	5	76	15	22	1	17	66	-19*	3	42	58	31*
6	21	58	14*	15	10	48	-4*	6	145	14	6	2	174	13	9	4	33	55	-1*
7	43	61	19*	K,L=	16,	1	7	54	26	-13*	3	91	15	19	5	65	73	61*	
8	0	93	-1*-16	21	70	-1*	8	93	13	-6	4	115	12	-7	6	0	55	-47*	
9	26	46	9*-15	0	62	-14*	9	65	67	-5*	5	57	63	31*	7	0	48	-25*	

STRUCTURE FACTORS CONTINUED FOR
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H	FOB	SG	DEL	H	FOB	SG	DEL	H	FOB	SG	DEL	H	FOB	SG	DEL	H	FOB	SG	DEL
8	0	60	-6*	5	91	16	11	2	0	54	-3*	2	149	25	2	K,L=	17,		7
9	71	21	-13*	6	120	10	8	3	0	45	-2*	3	31	48	25*	-10	75	19	42
10	24	47	21*	7	25	46	-10*	4	148	9	25	4	172	17	-2	-9	54	32	52*
K,L=	16,		7	8	0	59	-8*	5	40	46	9*	5	17	72	4*	-8	0	50	-39*
-12	0	50	-8*	9	30	66	21*	6	0	47	-37*	6	35	95	-21*	-7	0	51	-41*
-11	50	50	34*	10	22	79	9*	7	51	32	9*	7	0	83	-11*	-6	0	50	-2*
-10	41	50	-0*	11	24	94	3*	8	97	20	34	8	0	56	-26*	-5	0	42	-9*
-9	0	50	-12*	12	34	49	-19*	9	0	88	-35*	9	0	68	-5*	-4	0	56	-20*
-8	39	78	30*	13	0	99	-1*	10	60	88	-0*	10	61	38	20*	-3	70	20	-1
-7	0	92	-14*	14	0	49	-21*	11	35	74	27*	11	0	48	-15*	-2	40	42	35*
-6	68	83	-2*	K,L=	17,	1		12	49	36	-2*	K,L=	17,	5		-1	0	44	-4*
-5	0	74	-11*	-14	0	48	-12*	13	32	48	27*	-13	146	17	9	0	50	53	-9*
-4	46	78	-20*	-13	37	59	-2*	K,L=	17,	3		-12	0	52	-26*	1	130	16	-7
-3	0	67	-29*	-12	55	63	38*	-14	0	48	-4*	-11	23	51	11*	2	34	42	7*
-2	31	73	3*	-11	49	97	-34*	-13	41	48	37*	-10	48	51	24*	3	0	53	-29*
-1	134	14	-9	-10	0	80	-30*	-12	0	77	-12*	-9	75	79	-33*	4	0	54	-22*
0	31	60	-10*	-9	51	60	-5*	-11	57	70	-9*	-8	48	85	34*	5	38	41	-2*
1	0	44	-27*	-8	46	47	-10*	-10	29	94	11*	-7	0	80	-9*	6	0	50	-14*
2	39	42	32*	-7	87	14	3	-9	74	77	-25*	-6	46	70	4*	K,L=	17,		8
3	90	15	7	-6	48	78	27*	-8	43	67	32*	-5	40	47	25*	-7	40	49	36*
4	0	50	-21*	-5	0	46	-36*	-7	115	26	-10	-4	55	29	53*	-6	0	49	-5*
5	39	53	38*	-4	73	14	9	-6	74	31	-2*	-3	0	70	-13*	-5	37	41	33*
6	26	54	8*	-3	53	32	26*	-5	0	78	-14*	-2	0	60	-1*	-4	0	41	-26*
7	39	46	14*	-2	0	42	-29*	-4	0	45	-47*	-1	47	71	-13*	-3	59	22	28*
8	0	49	-31*	-1	0	43	-3*	-3	60	63	26*	0	55	95	40*	-2	24	62	8*
K,L=	16,		8	0	0	53	-1*	-2	52	61	25*	1	116	15	22	-1	72	27	7*
-10	0	61	-26*	1	0	43	-6*	-1	47	28	19*	2	7	98	-14*	0	139	16	3
-9	0	56	-1*	2	0	74	-38*	0	0	54	-38*	3	152	19	-12	1	62	40	12*
-8	17	50	9*	3	0	45	-20*	1	67	17	34	4	44	76	-15*	2	51	68	-8*
-7	12	49	-20*	4	117	10	13	2	109	11	10	5	0	70	-19*	K,L=	18,		0
-6	41	34	28*	5	229	9	15	3	61	28	1*	6	0	58	-33*	0	114	14	3
-5	21	59	-5*	6	88	14	7	4	47	38	39*	7	9	62	-31*	1	0	115	-60*
-4	0	69	-11*	7	0	49	-34*	5	38	46	-18*	8	0	48	-30*	2	0	92	-14*
-3	12	60	9*	8	53	28	46*	6	42	58	-0*	9	0	47	-25*	3	136	9	4
-2	99	18	-22	9	88	112	-4*	7	17	49	-4*	10	0	48	-22*	4	82	17	26
-1	62	42	42*	10	0	76	-14*	8	38	86	-1*	K,L=	17,	6		5	84	36	3*
0	37	44	-16*	11	37	77	30*	9	0	78	-34*	-12	17	52	-1*	6	0	74	-6*
1	40	43	8*	12	0	48	-5*	10	0	60	-20*	-11	35	69	-26*	7	74	93	58*
2	90	21	-2	13	22	53	16*	11	75	18	-7	-10	111	13	11	8	0	84	-37*
3	28	53	22*	14	0	49	-34*	12	24	52	-14*	-9	79	18	10	9	0	78	-22*
4	42	43	-15*	K,L=	17,	2		K,L=	17,	4		-8	0	61	-22*	10	0	79	-1*
5	84	12	15	-14	0	54	-16*	-14	44	55	-8*	-7	0	50	-22*	11	0	48	-9*
K,L=	16,		9	-13	0	65	-34*	-13	0	56	-42*	-6	23	70	-18*	12	0	48	-21*
-7	30	51	-3*	-12	59	50	-17*	-12	63	26	-5*	-5	25	72	10*	13	28	49	17*
-6	13	46	13*	-11	60	99	31*	-11	68	21	38*	-4	50	71	28*	K,L=	18,		1
-5	33	42	30*	-10	98	117	-18*	-10	0	69	-20*	-3	0	59	-43*	-13	0	51	-17*
-4	45	26	38*	-9	60	67	-13*	-9	0	92	-18*	-2	64	37	35*	-12	0	49	-20*
-3	46	25	43*	-8	151	10	-15	-8	34	56	30*	-1	21	58	-18*	-11	0	55	-3*
-2	0	47	-7*	-7	54	58	14*	-7	86	16	13	0	20	61	5*	-10	91	34	35*
-1	27	45	22*	-6	118	10	-11	-6	45	48	28*	1	55	39	51*	-9	78	84	-15*
0	35	43	-13*	-5	30	45	23*	-5	0	64	-16*	2	15	69	3*	-8	33	99	24*
1	0	45	-8*	-4	0	50	-6*	-4	57	20	42*	3	37	61	2*	-7	7	51	-58*
K,L=	17,	0	-3	0	58	-9*	-3	63	18	25	4	11	45	8*	-6	45	65	20*	
1	0	44	-29*	-2	0	51	-21*	-2	0	44	-17*	5	27	51	21*	-5	0	48	-6*
2	0	43	-18*	-1	0	44	-10*	-1	35	52	-26*	6	37	40	30*	-4	0	46	-30*
3	0	88	-26*	0	52	46	36*	0	49	57	-29*	7	33	47	22*	-3	30	67	24*
4	0	69	-32*	1	0	44	-34*	1	90	14	23	8	71	18	25	-2	57	22	1*

STRUCTURE FACTORS CONTINUED FOR
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H	FOB	SG	DEL	H	FOB	SG	DEL	H	FOB	SG	DEL	H	FOB	SG	DEL	H	FOB	SG	DEL
-1	0	53	-67*	3	63	34	-7*	-7	68	23	-8*	7	0	60	-0*	-3	66	20	-1*
0	0	94	-17*	4	37	66	5*	-6	0	44	-7*	8	0	54	-1*	-2	0	54	-40*
1	0	85	-10*	5	23	77	21*	-5	25	43	-24*	9	59	23	40*	-1	50	60	-26*
2	82	17	-9	6	0	78	-21*	-4	24	58	-7*	10	58	39	35*	0	20	69	-12*
3	68	19	3	7	0	81	-5*	-3	0	45	-29*	K,L=	19,	2		1	44	47	-13*
4	0	61	-24*	8	26	47	-9*	-2	43	50	41*	-11	29	49	-4*	2	47	70	-25*
5	0	56	-6*	9	0	49	-61*	-1	32	57	-27*	-10	29	71	-31*	3	17	63	9*
6	68	79	-15*	10	0	49	-23*	0	18	55	-14*	-9	0	70	-42*	4	78	18	5
7	139	34	-10	11	59	25	56*	1	0	60	-23*	-8	73	76	-13*	5	0	47	-15*
8	82	91	21*	K,L=	18,	4		2	50	51	24*	-7	0	52	-50*	6	14	40	14*
9	61	64	39*	-12	0	53	-12*	3	20	45	16*	-6	42	62	-9*	7	26	61	24*
10	0	78	-1*	-11	0	66	-26*	4	31	45	14*	-5	30	49	-7*	K,L=	19,	5	
11	25	47	8*	-10	67	22	18*	5	16	50	-30*	-4	38	42	-8*	-9	77	19	30
12	84	14	74	-9	26	60	19*	6	50	26	23*	-3	0	68	-19*	-8	49	52	-7*
K,L=	18,	2		-8	0	50	-29*	K,L=	18,	7		-2	63	34	29*	-7	0	50	-3*
-13	31	48	29*	-7	0	93	-21*	-7	0	51	-14*	-1	43	65	-6*	-6	0	42	-9*
-12	0	66	-19*	-6	44	72	35*	-6	67	14	17	0	48	55	34*	-5	0	41	-24*
-11	0	77	-14*	-5	83	35	5*	-5	0	43	-49*	1	0	56	-12*	-4	28	49	14*
-10	88	54	-22*	-4	55	28	15*	-4	27	54	17*	2	43	60	32*	-3	43	29	32*
-9	40	97	19*	-3	0	52	-20*	-3	50	23	44*	3	19	70	15*	-2	0	56	-6*
-8	102	102	-37*	-2	38	61	7*	-2	89	12	-3	4	65	69	10*	-1	0	51	-4*
-7	108	43	28*	-1	51	59	20*	-1	134	9	17	5	24	70	20*	0	0	59	-34*
-6	53	93	-9*	0	59	89	-5*	0	46	37	8*	6	29	59	28*	1	37	66	-15*
-5	53	27	-20*	1	57	67	-14*	1	22	48	-0*	7	0	80	-40*	2	44	56	25*
-4	35	44	25*	2	139	12	-0	2	34	43	22*	8	0	49	-4*	3	77	35	-4*
-3	0	45	-7*	3	55	91	-20*	3	60	28	9*	9	0	51	-75*	4	36	55	-10*
-2	35	44	12*	4	77	86	-11*	K,L=	19,	0		10	57	29	57*	5	33	42	20*
-1	0	44	-6*	5	0	84	-27*	1	131	13	4	K,L=	19,	3		K,L=	19,	6	
0	61	36	43*	6	52	61	-1*	2	84	23	1	-11	41	49	34*	-7	98	19	43
1	44	45	-6*	7	0	69	-13*	3	0	50	-72*	-10	47	59	45*	-6	85	23	5
2	61	20	44*	8	0	57	-6*	4	25	82	22*	-9	25	50	-28*	-5	62	19	5*
3	35	49	0*	9	0	47	-16*	5	69	38	-17*	-8	0	82	-1*	-4	0	49	-2*
4	42	58	40*	K,L=	18,	5		6	47	93	-6*	-7	46	75	-16*	-3	96	11	1
5	78	28	13*	-11	136	12	-3	7	0	67	-37*	-6	101	15	-11	-2	0	43	-19*
6	136	28	12	-10	23	61	-39*	8	0	71	-17*	-5	0	45	-20*	-1	51	23	-3*
7	69	104	-12*	-9	0	53	-20*	9	0	56	-6*	-4	0	44	-37*	0	63	18	45
8	0	104	-30*	-8	0	50	-21*	10	0	48	-9*	-3	55	25	-29*	1	0	45	-19*
9	11	75	-5*	-7	0	90	-3*	11	0	49	-39*	-2	87	39	-24*	2	56	24	45*
10	64	37	-5*	-6	8	66	5*	K,L=	19,	1		-1	30	56	-9*	3	38	42	20*
11	0	49	-22*	-5	47	68	33*	-11	0	49	-1*	0	0	58	-51*	K,L=	20,	0	
K,L=	18,	3		-4	26	41	5*	-10	0	52	-29*	1	23	74	-2*	0	143	14	-9
-13	0	64	-9*	-3	0	74	-4*	-9	38	48	-18*	2	91	30	-1*	1	79	32	-4*
-12	49	41	22*	-2	41	60	-2*	-8	0	66	-23*	3	34	57	5*	2	0	76	-15*
-11	0	69	-41*	-1	0	63	-27*	-7	38	71	-5*	4	42	61	24*	3	106	32	-11*
-10	25	50	6*	0	45	63	10*	-6	25	69	7*	5	0	60	-23*	4	35	68	30*
-9	51	101	-44*	1	95	36	-5*	-5	0	69	-17*	6	50	54	14*	5	38	54	-5*
-8	97	99	7*	2	0	90	-38*	-4	82	25	15*	7	0	52	-15*	6	14	59	6*
-7	26	77	-35*	3	35	69	-36*	-3	45	69	36*	8	69	20	11*	7	38	47	37*
-6	38	51	-17*	4	41	65	23*	-2	0	47	-62*	9	0	64	-7*	8	0	49	-19*
-5	7	45	-1*	5	36	67	-38*	-1	0	51	-10*	K,L=	19,	4		9	0	76	-16*
-4	93	30	19*	6	0	63	-36*	0	39	58	-38*	-10	0	50	-17*	K,L=	20,	1	
-3	74	16	17	7	0	62	-36*	1	57	32	-24*	-9	0	50	-22*	-9	0	69	-18*
-2	29	45	0*	8	60	31	56*	2	27	47	22*	-8	25	68	14*	-8	0	58	-3*
-1	51	55	10*	K,L=	18,	6		3	16	70	13*	-7	59	69	2*	-7	0	48	-31*
0	100	29	-9	-10	74	41	59*	4	115	33	2	-6	30	49	22*	-6	46	61	11*
1	39	51	-7*	-9	0	52	-50*	5	104	60	5*	-5	0	53	-9*	-5	39	61	27*
2	41	61	30*	-8	46	59	45*	6	62	78	11*	-4	0	70	-54*	-4	26	70	-1*

STRUCTURE FACTORS CONTINUED FOR
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H	FOB	SG	DEL	H	FOB	SG	DEL	H	FOB	SG	DEL	H	FOB	SG	DEL	H	FOB	SG	DEL
-3	0	62	-6*	3	29	40	16*												
-2	66	70	5*	4	0	41	-24*												
-1	76	13	-6	K,L= 20, 5															
0	44	60	1*	-5	27	43	23*												
1	0	55	-8*	-4	35	47	-3*												
2	84	19	-3	-3	35	41	18*												
3	0	73	-36*	-2	60	17	25												
4	36	72	30*	-1	44	46	36*												
5	0	56	-3*	0	0	51	-18*												
6	44	53	23*	1	38	41	9*												
7	43	47	34*	2	21	50	5*												
8	0	49	-29*	K,L= 21, 0															
K,L= 20, 2				1	59	70	-26*												
-9	0	65	-15*	2	70	26	-22*												
-8	0	50	-56*	3	0	66	-27*												
-7	0	50	-17*	4	55	24	34*												
-6	37	52	23*	5	0	41	-26*												
-5	27	48	-36*	6	28	48	21*												
-4	5	55	-37*	K,L= 21, 1															
-3	0	64	-35*	-6	0	41	-10*												
-2	37	52	-8*	-5	5	46	-2*												
-1	15	52	-5*	-4	44	28	8*												
0	27	61	26*	-3	0	50	-5*												
1	35	60	1*	-2	40	56	-7*												
2	20	59	-10*	-1	0	48	-14*												
3	0	75	-31*	0	49	57	1*												
4	0	49	-8*	1	81	21	-22												
5	21	55	-2*	2	23	48	18*												
6	28	53	-4*	3	0	48	-12*												
7	44	48	0*	4	0	58	-30*												
K,L= 20, 3				5	0	40	-14*												
-8	0	66	-29*	K,L= 21, 2															
-7	0	50	-32*	-5	44	46	38*												
-6	31	51	-15*	-4	46	39	2*												
-5	59	27	10*	-3	0	56	-10*												
-4	112	10	2	-2	0	42	-28*												
-3	41	46	-39*	-1	66	15	30												
-2	0	54	-31*	0	42	45	22*												
-1	26	45	-15*	1	2	53	-1*												
0	97	23	-0	2	0	41	-16*												
1	45	65	42*	3	49	23	44*												
2	0	69	-11*	4	30	40	13*												
3	30	59	-1*	K,L= 21, 3															
4	25	46	21*	-4	30	47	5*												
5	30	50	15*	-3	79	25	1*												
6	25	58	18*	-2	104	15	22												
K,L= 20, 4				-1	33	48	-26*												
-7	51	60	40*	0	0	67	-42*												
-6	0	42	-5*	1	0	42	-15*												
-5	70	33	-5*	2	39	43	19*												
-4	0	42	-29*																
-3	43	35	25*																
-2	65	32	7*																
-1	0	61	-42*																
0	0	43	-13*																
1	49	59	-3*																
2	67	33	20*																