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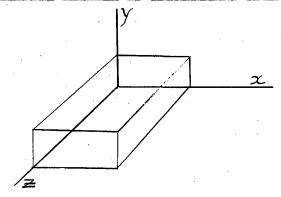
UNIVERSITY OF CALIFORNIA Radiation Laboratory Berkeley, California

ELECTRICAL ENGINEERING REVIEW COURSE

Lecture XVI July 21, 1952

E. Martinelli (Notes by: R. Byrns, R. Burleigh)

Maxwell's Equations Applied to Rectangular Tube



Consider a sinuscidal wave transmitted in +Z direction and having only a y component E = jEy. This is known as the transverse electric mode. We look for a mode in which:

$$E = Ey(x_1y)e^{j(wt - kz)}$$

$$\nabla^2 \vec{E} - \frac{1}{c^2} \vec{A} + \vec{B} = 0$$

The symbol —>may be removed as this is essentially a scaler equation, then:

$$\nabla^2 \mathbf{E} - \frac{1}{\mathbf{c}^2} \frac{\partial^2 \mathbf{E}}{\partial \mathbf{t}^2} = 0$$

substituting:

$$\frac{\partial^2 \mathbf{E}}{\partial \mathbf{x}^2} + \frac{\partial^2 \mathbf{E}}{\partial \mathbf{y}^2} + \frac{\partial^2 \mathbf{E}}{\partial \mathbf{z}^2} - \frac{1}{\mathbf{c}^2} \frac{\partial^2 \mathbf{E}}{\partial \mathbf{t}^2} = 0$$

or:

$$\frac{\partial^2 E_y}{\partial x^2} + \frac{\partial^2 E_y}{\partial y^2} - K^2 E_y + \frac{W^2}{C^2} E_y = 0$$

Then:

$$\frac{\int_{-\infty}^{2} E_{y}}{\partial x^{2}} + \frac{\int_{-\infty}^{2} E_{y}}{\partial y^{2}} - (K^{2} - \frac{W^{2}}{c^{2}})E_{y} = 0$$

(This is the differential equation of a wave in a rectangular tube.)

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Solving the above equation:

let Ey = X(x) Y(y)
X''Y + Y''X =
$$(K^2 - \frac{w^2}{c^2})XY = 0$$

 $\frac{X''}{X} = -\frac{Y''}{Y} + K^2 = \frac{w^2}{c^2} = -\frac{\lambda^2}{2}$
X = A sin $\lambda x + B \cos \lambda x$
Y = C sin By + D cos By
B = $\sqrt{-\lambda^2 - K^2 + \frac{w^2}{2}}$

(K is an arbitrary propagation constant)

Putting in boundary condition:

where

Then, as we have only a y component:

$$\frac{\partial Ey}{\partial y} = 0$$
, $Ey = f(x)$

since there is only
$$E_v$$
, $\beta = 0$

$$\beta = \sqrt{-\lambda^2 - \kappa^2 + \frac{w^2}{c^2}} = 0$$

then:

$$-\left(\frac{n}{a}\right)^{2} - K^{2} + \left(\frac{2\Pi}{\lambda}\right)^{2} = 0$$

$$K = \frac{2\Pi}{\lambda y}$$

$$\lambda y = \frac{\lambda}{1 - \left(\frac{n\lambda}{2a}\right)^{2}}$$

Therefore, it may be seen that a number of wavelengths maybe propagated down the guide, i.e., for n = 1, 2, etc. (n represents type of mode.)

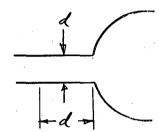
For cut-off:

$$\frac{n}{2a} = 1$$

$$K^2 = (\frac{211}{2})^2 - (\frac{n}{2})^2$$

$$K^2 = (\frac{n}{211})^2 = 1 - (\frac{n}{2a})^2$$

Wave is attenuated if wave length is greater than cut-off (if λ is too large). This is utilized in attenuators:



In one diameter the field will be attenuated by e (where length of pipe managed diameter.)

For cut-off:
$$\lambda = \frac{2a}{n}$$

Therefore, lowest frequency that can be propagated:

$$\lambda = 2a$$

Magnetic Field

Knowing the electric field we can apply Maxwell's Equations and investigate the magnetic field.

curl
$$\vec{E} = -\frac{1}{c} \frac{d\vec{B}}{dt}$$

 $\vec{E} = j\vec{E}_y e^{j(wt - kz)}$
 $\vec{B} = \vec{B}_{x,y} e^{j(wt - kz)}$

Take the curl of the vector with only one component and get two terms.

$$\operatorname{curl} \stackrel{>}{E} = \stackrel{\wedge}{\mathbf{i}} - \frac{\operatorname{dE}_{\mathbf{y}}}{\operatorname{dz}} + \stackrel{\wedge}{\mathbf{k}} \frac{\operatorname{dE}_{\mathbf{y}}}{\operatorname{dx}} \left(\operatorname{E}_{\mathbf{y}} = \operatorname{E}_{\max} \operatorname{Sin} \frac{\mathcal{T}_{\mathbf{x}}}{\operatorname{a}} \right)$$

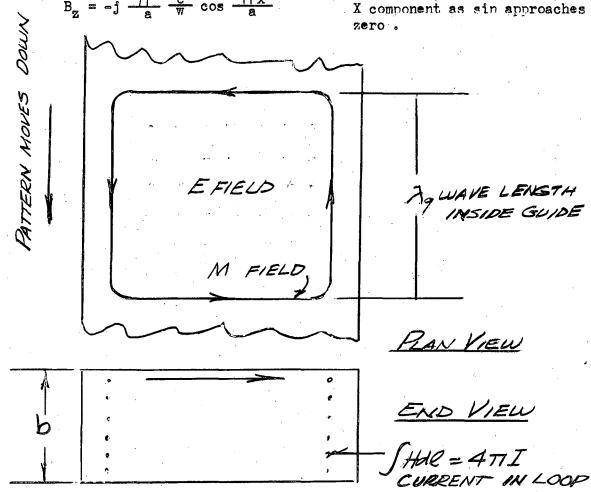
$$= \stackrel{\wedge}{\mathbf{i}} \left(\operatorname{jkE}_{\max} \operatorname{sin} \frac{\mathcal{T}_{\mathbf{x}}}{\operatorname{a}} \right) + \stackrel{\wedge}{\mathbf{k}} \frac{\mathcal{T}}{\operatorname{a}} \operatorname{E}_{\max} \operatorname{cos} \frac{\mathcal{T}_{\mathbf{x}}}{\operatorname{a}} \right)$$

$$= -\operatorname{j} \frac{\operatorname{w}}{\operatorname{c}} \operatorname{B}_{\mathbf{x}} - \operatorname{j} \frac{\operatorname{w}}{\operatorname{c}} \operatorname{B}_{\mathbf{z}} \left(\operatorname{Only two components, z and x, of magnetic field} \right).$$

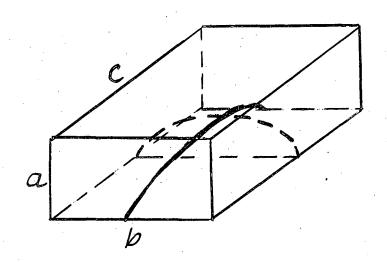
Solving: $B_{x} = \frac{kc}{w} E_{max} \sin \frac{\pi x}{a}$

 $B_z = -j \frac{C}{a} \frac{c}{w} \cos \frac{Tx}{a}$

At X = 0, only z component. is present, at middle only



 $I = \frac{10bc}{4aw}$ E_{max} gives current flowing in sides of guide.



Make
$$C = \frac{\lambda g}{2}$$
 to get 0 at both ends

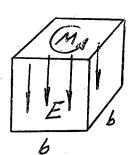
Solve for C:

$$2C = \frac{1 - \left(\frac{\lambda}{2b}\right)^2}$$

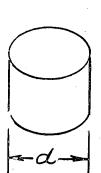
$$\lambda = c \frac{1}{\sqrt{1 + \frac{c^2}{b^2}}}$$

We thus can get an infinite number of cavities of many shapes all resonant at the same frequency.

b (similar to Linac, Bldg. 10)



In the square resonator, the resonant frequency is lowered slightly by the corner effect.



The round cavity, similar to square, frequency is given by:

$$\mathcal{A} = \frac{d}{1.31}$$