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## **Tuning Nanofillers in In-situ Prepared Polyimide Nanocomposites for High-Temperature Capacitive Energy Storage**

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**Abstract:** Modern electronics and electrical systems demand efficient operation of dielectric polymer-based capacitors at high electric fields and elevated temperatures. Here, we report the polyimide dielectric composites prepared from in-situ polymerization in the presence of inorganic nanofillers. The systematic manipulation of the dielectric constant and bandgap of the inorganic fillers, including Al<sub>2</sub>O<sub>3</sub>, HfO<sub>2</sub>, TiO<sub>2</sub> and boron nitride nanosheets, reveals the dominant role of the bandgap of the fillers in determining and improving the high-temperature capacitive performance of the polymer composites, which is very different from the design principle of the dielectric polymer composites operating at ambient temperature. The Al<sub>2</sub>O<sub>3</sub> and HfO<sub>2</sub> based polyimide composites with concomitantly large bandgap and moderate dielectric constants exhibit substantially improvement in the breakdown strength, discharged energy density and charge-discharge efficiency when compared to the state-of-the-art dielectric polymers. The work provides a design paradigm for high-performance dielectric polymer nanocomposites for electrical energy storage at elevated temperatures.

Dielectric capacitors possess the highest power density among the energy storage devices and are one of the major enabling technologies for advanced electronics and electrical power systems.<sup>[1–3]</sup> In particular, capacitors with high operating temperatures are of critical importance for next-generation automotive and aerospace power systems. In electric vehicles, power inverters convert direct current from batteries to alternating current at the frequency required to control the electric motor. Because of close proximity to the engine and the ever-increasing demand for power capability, it requires that capacitors, the essential element of power inverters, operate at a temperature of 140 °C or above.<sup>[4,5]</sup> While dielectric ceramics are traditional materials for high-temperature capacitors,<sup>[6]</sup> they are severely limited by scalability, weight, fracture toughness and breakdown strength in comparison to their polymer counterparts.<sup>[7–17]</sup> Biaxially oriented polypropylene film (BOPP), the state-of-the-art commercially available polymer dielectric, however, shows largely degraded high-field dielectric properties when operating at temperatures above 100 °C.<sup>[18]</sup>

To address these imperative needs, a variety of well-established engineering polymers, including polycarbonate (PC), polyimide (PI), polyetherimides (PEI) and poly(ether ether ketone) (PEEK), have been exploited as high-temperature dielectric materials.<sup>[19–25]</sup> As these aromatic polymers have high glass transition temperatures ( $T_g$ ) and excellent thermal stability, it is anticipated that the engineering polymers would retain electromechanical properties and thus dielectric stability at high temperatures. However, when subjected to high applied fields, the engineering polymers exhibit limited working temperatures that are much lower than their  $T_g$ s.<sup>[19,20]</sup> More recently, inorganic fillers represented by boron nitride nanosheets (BNNSs) have been incorporated into crosslinked divinyltetramethyldisiloxane-bis(benzocyclobutene) (*c*-BCB) to yield the dielectric polymer composites capable of operating efficiently at high temperatures, e.g. 150 °C.<sup>[26–29]</sup> Herein, we describe the high-temperature dielectric properties and capacitive performance of the PI-based polymer nanocomposites prepared via in-situ polycondensation. Compared with *c*-BCB, PI possesses the inherent advantages including much better processability, considerably lower

cost, and greater mechanical strength and flexibility, which potentially offers a scalable route toward robust high-temperature dielectric materials.<sup>[30,31]</sup> The investigation of the polymer composites containing the inorganic nanofillers with systematically varied dielectric constants ( $K$ ) and bandgap ( $\Delta E$ ), including aluminium oxide ( $\text{Al}_2\text{O}_3$ ) with a  $K$  of 9.5 and a  $\Delta E$  of 8.6 eV, hafnium dioxide ( $\text{HfO}_2$ ) with a  $K$  of 25 and a  $\Delta E$  of 5.8 eV, titanium dioxide ( $\text{TiO}_2$ ) with a  $K$  of 110 and a  $\Delta E$  of 3.5 eV, and BNNS with a  $K$  of 4 and a  $\Delta E$  of 5.97 eV,<sup>[26,32–34]</sup> would provide experimental guidelines for the design of high-performance high-temperature dielectric polymer composites.

As shown in Figure 1, pyromellitic dianhydride (PMDA), and 4, 4'-diaminodiphenyl ether (4, 4'-ODA) were condensed in the presence of inorganic nanofillers including  $\text{Al}_2\text{O}_3$ ,  $\text{HfO}_2$ ,  $\text{TiO}_2$  and BNNS. The in-situ synthesis of the PI composites starts from the mixture of ODA and the nanofiller suspension toward the preparation of the precursor of PI - poly(amic acid) (PAA), which has been found to be effective in disrupting nanofillers agglomeration and thus yield the composites with uniform filler dispersion and excellent dielectric properties.<sup>[35]</sup> The formation of PAA and subsequent thermal imidization were monitored by using attenuated total reflectance-Fourier transform infrared (ATR-FTIR) spectroscopy (Figure S1 Supporting Information). The absence of 3252 and 1624  $\text{cm}^{-1}$  absorption bands arising from N-H and C=O stretching of PAA, respectively, and the appearance of new peaks at 1775  $\text{cm}^{-1}$  (C=O asymmetric stretching), 1720  $\text{cm}^{-1}$  (C=O symmetric stretching), 1366  $\text{cm}^{-1}$  (C-N stretching) and 723  $\text{cm}^{-1}$  (C=O bending) indicate the successful conversion of PAA to PI upon thermal curing. The presence of the nanofillers in the in-situ prepared nanocomposites has been manifested by the FTIR spectra (Figure S1 Supporting Information) and cross-sectional scanning electron microscopic (SEM) images (Figure S2 Supporting Information). Homogeneous dispersion of the nanofillers in the PI matrix prepared by the in-situ polycondensation is evidenced in SEM. For the purpose of comparison, the dielectric properties and capacitive performance of pristine PI films were evaluated along with the PI nanocomposites.

As summarized in Figure 2A, the  $K$  of the nanocomposites is enhanced upon the incorporation of the nanofillers, *e.g.*, from 3.33 for PI to 3.46 of PI-BNNS, 3.58 of PI-Al<sub>2</sub>O<sub>3</sub>, 3.76 of PI-HfO<sub>2</sub> and 4.02 of PI-TiO<sub>2</sub> with 5 vol% filler content measured at 25 °C and 1 kHz, and increases gradually with the filler content. The increasing  $K$  is attributable to higher  $K$  values of the fillers relative to that of PI matrix. As expected, TiO<sub>2</sub> with the highest  $K$  among the nanofillers investigated herein gives rise to the largest  $K$  of the nanocomposites, whereas the PI-BNNS composites possess the lowest  $K$  owing to the smallest  $K$  of BNNS. It is found that the experimental  $K$  values of the PI-Al<sub>2</sub>O<sub>3</sub>, PI-HfO<sub>2</sub> and PI-TiO<sub>2</sub> composites agree well with the effective  $K$  calculated by using the Lichtenecker model (Eq. 1)<sup>[36]</sup> which is a widely used empirical model to determine the  $K$  of dielectric composites where the spherical particles were randomly dispersed in the matrix. The fitting results for the PI-Al<sub>2</sub>O<sub>3</sub>, PI-HfO<sub>2</sub> and PI-TiO<sub>2</sub> composites by using other theoretical models are shown in Figure S3 Supporting Information.<sup>[37]</sup> For PI-BNNS, the experimental  $K$  was fitted well by using the Polder-Van Santen (PVS) formalism (Eq. 2)<sup>[38]</sup>

$$\varepsilon_{\text{eff}} = e^{f_a \ln \varepsilon_a + (1-f_a) \ln \varepsilon_b} \quad (\text{Eq. 1})$$

$$\varepsilon_{\text{eff}} = \varepsilon_b + \frac{f_a (\varepsilon_a - \varepsilon_b)}{3} \sum_{j=x,y,z} \frac{\varepsilon_{\text{eff}}}{\varepsilon_{\text{eff}} + N_j (\varepsilon_a - \varepsilon_{\text{eff}})} \quad (\text{Eq. 2})$$

where  $\varepsilon_{\text{eff}}$ ,  $\varepsilon_b$  and  $\varepsilon_a$  are the  $K$  of the composite, matrix and nanofiller, respectively,  $f_a$  is the volume fraction of the nanofiller and  $N_j$  represents the depolarization factors (Eq. S1 Supporting Information). All the PI-based composites exhibit low dielectric loss (<0.5%) as shown in Figure 2A. In addition, dielectric spectroscopy reveals that  $K$  and dielectric loss of the PI composites are considerably stable with respect to temperature ranging from 25 to 200 °C and frequency ranging from 100 Hz to 1 MHz, which retain the unique features of PI matrix (Figures S4 and S5 Supporting Information).

The breakdown strength ( $E_b$ ) of the polymer nanocomposites at 150 °C is analyzed with a two-parameter Weibull statistic distribution function described as:

$$P(E) = 1 - \exp(-(E/E_b)^\beta) \quad (\text{Eq. 3})$$

where  $P(E)$  is the cumulative probability of electric failure,  $E$  is the measured breakdown field, Weibull breakdown strength  $E_b$  represents the field strength at the cumulative failure probability of 63.2%,  $\beta$  is the shape parameter evaluating the scatter of the breakdown data. At least 15 measurements were made for each Weibull fitting. Notably, as summarized in Figure 2B and Figure S7 Supporting Information, the  $E_b$  of the PI nanocomposites increases from 314 MV m<sup>-1</sup> of PI with the incorporation of the nanofillers and is maximized to 340 MV m<sup>-1</sup> at 1 vol% TiO<sub>2</sub>, 397 MV m<sup>-1</sup> at 5 vol% HfO<sub>2</sub>, 422 MV m<sup>-1</sup> at 7 vol% Al<sub>2</sub>O<sub>3</sub>, and 418 MV m<sup>-1</sup> at 5 vol% BNNS. This is in sharp contrast to the typical dielectric polymer composites with high- $K$  inclusions whose  $E_b$  is always largely reduced when compared to that of pristine polymers.<sup>[8,39,40]</sup> It is found that the systematic enhancement in the  $E_b$  of the PI nanocomposites coincides with the increasing trend of  $\Delta E$  of the nanofillers as summarized in Figure S8 Supporting Information. Al<sub>2</sub>O<sub>3</sub> has the largest  $\Delta E$  among the fillers and results in the highest  $E_b$  of the composites, while TiO<sub>2</sub> with the lowest  $\Delta E$  leads to the smallest improvement in  $E_b$  of the resulting composites. Apparently, the nanofillers with higher  $\Delta E$  are more efficient in acting as barriers against charge injection from electrodes and the growth of electrical trees in dielectrics at elevated temperatures. In addition, compared to Al<sub>2</sub>O<sub>3</sub> and BNNS, TiO<sub>2</sub> has the largest contrast in  $K$  with PI matrix, which may create more significant distortion of local fields and thus yield a reduced  $E_b$  in the composites at high filler contents.<sup>[8,41]</sup> Different from the PI composites with BNNS, Al<sub>2</sub>O<sub>3</sub> and HfO<sub>2</sub> fillers, the  $E_b$  of the PI-TiO<sub>2</sub> composites decrease rapidly with increasing filler concentration. The initial increase in the  $E_b$  of the PI-TiO<sub>2</sub> composites could be attributed to the contribution of the interfaces between the nanoparticles and the polymer, which serves as effective electron scatters and trapping centers to impede charge conduction in the composites.<sup>[16,17]</sup> As shown in Figures S6 and S7, further increase of the filler concentration results in decreased  $E_b$ ,<sup>[42,43]</sup> which matches the change of the electrical conductivity of the composites as discussed below.

Representative electric displacement-electric field ( $D$ - $E$ ) loops of the PI-nanocomposites measured at 150 °C and 200 MV m<sup>-1</sup>, which is the working condition of the power inverters in electric vehicles,<sup>[44]</sup> are displayed in Figure S12 Supporting Information, in which the integral of the area bounded by the upper line and the y-axis represents the dischargeable energy density ( $U_e$ ) and the area enclosed by the upper and bottom lines stands for energy loss ( $U_l$ ). The nanocomposites with high- $K$  nanofillers display correspondingly large values of  $D$ , *i.e.* the largest  $D$  of 0.0080 - 0.0084 C m<sup>-2</sup> found in the PI-HfO<sub>2</sub> and PI-TiO<sub>2</sub> composites. On the other hand, it is seen that the PI-BNNS, PI-Al<sub>2</sub>O<sub>3</sub> and PI-HfO<sub>2</sub> composites with large  $\Delta E$  fillers present the lowest  $U_l$ , and consequently, the highest charge-discharge efficiency ( $\eta = U_e/(U_e + U_l)$ ), *i.e.* 93.3% - 95.8%, which is much greater than neat PI, *i.e.* 79.7%. Figure 2C summarizes the  $U_e$  and  $\eta$  of the composites with the optimized filler content measured at 150 °C and under their respective  $E_b$ . Clearly, the PI-composites significantly outperform PI matrix in both  $U_e$  and  $\eta$ . For instance, at an applied field of 250 MV m<sup>-1</sup>, PI exhibits the maximum  $U_e$  of 0.82 J cm<sup>-3</sup> and a  $\eta$  of 55.7%, whereas the respective  $U_e$  and  $\eta$  are 1.12 J cm<sup>-3</sup> and 93.7% for PI-Al<sub>2</sub>O<sub>3</sub>, 1.21 J cm<sup>-3</sup> and 91.0% for PI-HfO<sub>2</sub>, 1.08 J cm<sup>-3</sup> and 91.8% for PI-BNNS, and 1.11 J cm<sup>-3</sup> and 81.8% for PI-TiO<sub>2</sub>. As compared in Figure 2D, the capacitive performance of the PI-composites under different applied fields critically depends on the  $K$  and  $\Delta E$  of the fillers. Although TiO<sub>2</sub> has the highest  $K$  of 110 and the largest  $D$  (e.g. 0.0084 C m<sup>-2</sup> @ 200 MV m<sup>-1</sup>) among the fillers, it fails to yield a superior  $U_e$  at high applied fields (*i.e.* >50 MV m<sup>-1</sup>). Its lowest  $\Delta E$  of 3.5 eV gives the largest  $U_l$  that can overshadow any other advantages gained from high  $K$ . At an applied field of 200 MV m<sup>-1</sup>, HfO<sub>2</sub>, which has a relatively high  $K$  of 25 and a moderately large  $\Delta E$  of 5.8 eV, gives rise to the PI composite with the highest  $U_e$ . On the other hand, the PI-BNNS composite has the lowest  $U_e$  as a direct consequence of its smallest  $K$  of 4 of BNNS. At high applied fields, it is found that  $\Delta E$  of the fillers vitally determines the capacitive performance of the composites. Al<sub>2</sub>O<sub>3</sub>, which has the largest  $\Delta E$  of 8.6 eV and a reasonably large  $K$  of 9.5, yields the best composite operating at 350 MV m<sup>-1</sup> and 150 °C. The  $U_e$  of the PI-Al<sub>2</sub>O<sub>3</sub> and PI-HfO<sub>2</sub>

composites surpasses that of *c*-BCB/BNNSs and rival the newly developed high-temperature dielectric polymer nanocomposites.<sup>[26,33]</sup> Moreover, compared to the BNNS-filled polymer composites, the PI-Al<sub>2</sub>O<sub>3</sub> and PI-HfO<sub>2</sub> composites have much improved scalability as Al<sub>2</sub>O<sub>3</sub> and HfO<sub>2</sub> nanofillers either are commercially available or can be prepared readily in large scales. On the contrary, BNNSs are typically prepared via solution exfoliation under sonication, which is a low-yield (<10%) and time-consuming (~48 hrs) process.<sup>[45]</sup> Comparatively, BOPP operating at 70 °C and 200 MV m<sup>-1</sup> has a  $U_e$  of 0.4 J cm<sup>-3</sup> and a  $\eta$  of 96%.<sup>[28]</sup> These results indicate that, by substitute BOPP with the PI-Al<sub>2</sub>O<sub>3</sub> and PI-HfO<sub>2</sub> nanocomposites in the power inverters, the secondary cooling system in electric vehicles could be eliminated to improve volume and fuel efficiency and enhance reliability and performance of power systems. In addition, improved  $U_e$  enables the reduction in weight and size of electrical energy storage and power conditioning systems. Currently, capacitors represent up to 23% of the inverter weight and up to 35-40% of the inverter volume. It is estimated that a 100% increase in  $U_e$  corresponds to more than 17% reduction in the inverter size.<sup>[46]</sup> To evaluate the stability of the PI composites, charge-discharge cycling has been conducted at 150 °C under an applied field of 200 MV m<sup>-1</sup>. Remarkably, as shown in Figure S16 Supporting Information, no sign of degradation in the discharged energy density and the charge-discharge efficiency has been detected in the PI composites over 25,000 cycles. SEM shown in Figure S17 Supporting Information confirms the structure durability of the composites after cycling.

It is recognized that electrical conduction is the major loss mechanism of dielectrics at high electric fields.<sup>[18,33,47]</sup> Indeed, as shown in Figure 3A, the conduction loss of PI and the PI composites increase exponentially with the applied electric fields, which accounts for the deteriorating  $U_e$  and  $\eta$  observed at high fields. It is clearly evident from Figure 3B and Figure S18 Supporting Information that significant reductions in the electrical conductivity have been achieved upon the introduction of the nanofillers in PI matrix, which is particularly prominent at high temperatures. At 25 °C, the volume conductivity of neat PI measured at 100 MV m<sup>-1</sup> is reduced by 33.4%, 47.0%, 53.2% and 72.6% with the incorporation of TiO<sub>2</sub>, HfO<sub>2</sub>, BNNS, and Al<sub>2</sub>O<sub>3</sub>,



respectively. While at 150 °C, the corresponding decreases in the conductivity are much more pronounced, *i.e.* 41.1%, 83.2%, 89.9% and 93.9%, respectively. It is noteworthy that the magnitude of reduction follows the trend of increasing  $\Delta E$  of the fillers from TiO<sub>2</sub>, HfO<sub>2</sub>, BNNS to Al<sub>2</sub>O<sub>3</sub>. Consequently, at high fields, the Al<sub>2</sub>O<sub>3</sub> composite presents the lowest loss and the best  $\eta$ , while the TiO<sub>2</sub> composite has the highest loss and the lowest  $\eta$  as shown in Fig. 2D. In addition, the exponential increase of current density ( $J$ ) over the electric field is shown in Figure 3C, in which  $J$  is given as:<sup>[48]</sup>

$$J = 2nedv * \exp[(-U / K_b T)] * \sinh(deE / 2K_b T) \quad (\text{Eq. 4})$$

where  $U$  is the activation energy,  $d$  is the hopping distance, and  $v$  is the attempt-to-escape frequency,  $n$  is the carrier density,  $K_b$  is the Boltzmann constant,  $T$  is the temperature and  $e$  represents the electric charge. Eq. 4 can be simplified as follows:

$$J = J_0 * \sinh(\alpha * E) \quad (\text{Eq. 5})$$

where  $J_0$  and  $\alpha$  are two lumped parameters. The fitting of the experimental  $J$  data of the PI nanocomposites to Eq.5 suggests that hopping conduction is dominant in the nanocomposites at high electric fields. The hopping distance  $d$  can be calculated from the slopes of the fitting curves. For PI, the  $d$  is about 1.83 nm at 150 °C, which is decreased to 1.69, 1.41, 1.38 and 1.25 nm of the PI-TiO<sub>2</sub>, PI-HfO<sub>2</sub>, PI-BNNS and PI-Al<sub>2</sub>O<sub>3</sub> nanocomposites, respectively. The decrease in the  $d$  denotes the increase in the trap depth, which is naturally responsible for the reduced conduction current and lowered dielectric loss.<sup>[33]</sup> Accordingly, the shortest  $d$  of the PI-Al<sub>2</sub>O<sub>3</sub> composites correlates well with the lowest high-field conductivity and the smallest  $U_l$ . Note that the decrease in the  $d$  of the PI nanocomposites also follows the increasing trend of  $\Delta E$  of the nanofillers, which is consistent with the  $E_b$  results (Figure S7 Supporting Information).

To better understand the dependence of leakage current density on the  $\Delta E$  of the fillers, we simulated the current density distribution as a function of the filler content and applied field at 150 °C according to the hopping conduction model. As shown in Figure 4, in concert with the

experimental results, the simulations indicate that the PI nanocomposites consisting of Al<sub>2</sub>O<sub>3</sub> and HfO<sub>2</sub> filler with larger  $\Delta E$  exhibit much lower leakage current than the PI-TiO<sub>2</sub> composite. The volume resistivity of the PI nanocomposites versus the volume fractions of nanofillers at 200 MV m<sup>-1</sup> has been summarized in Figure S20, S21 and S22 Supporting Information. The volume resistivity of the composites increases with the filler content and then decreases at a certain filler content, which is consistent with the trend of  $E_b$  results. High concentrations of the fillers are prone to structure defects and filler agglomeration and have better connectivity, thus leading to increased leakage current and the corresponding reduction in volume resistivity and breakdown strength.<sup>[49]</sup> In addition, the thermally stimulated depolarization current (TSDC) measurements have been conducted to assess the charge trapping characteristics of the materials. As can be seen in Figure 3D, the peak located at a low temperature region stems from dipole polarization, while the high temperature peak is associated with the space charge polarization by trapping of charge carriers in deeper traps.<sup>[50]</sup> The much increased intensity of the peaks in the PI composites relative to those of PI implies that more charges are trapped upon the incorporation of nanofillers. Moreover, the shift of the high temperature peak toward high temperatures (e.g., >200 °C) from PI to the PI nanocomposites is indicative of the formation of deeper traps in the composites.<sup>[51]</sup> These results offer direct insights in the origins of the suppressed conduction loss and improved  $\eta$  observed in the PI nanocomposites.

In summary, we have prepared a series of the PI-based polymer nanocomposites containing the inorganic nanofillers with systematically varied  $K$  and  $\Delta E$ . Different from the typical dielectric composites whose  $E_b$  is reduced with the incorporation of high- $K$  inclusions, the PI-composites exhibit much improved  $E_b$  in comparison to pristine PI. In contrast to the dielectric composites designed for operating at weak fields and room temperature, in which  $K$  of the fillers plays a crucial role in determining the dielectric performance, it is conclusively demonstrated that  $\Delta E$  of the fillers dominates the high-temperature capacitive performance of the polymer composites at high fields.

The addition of the inorganic fillers with large  $\Delta E$  significantly reduces conduction current, which yields the dielectric composites with high  $U_e$  and great  $\eta$  at high fields and elevated temperatures. The synergistic combination of a large  $\Delta E$  and a moderate  $K$  in  $\text{Al}_2\text{O}_3$  and  $\text{HfO}_2$  gives rise to the corresponding composites with superior capacitive performance than the state-of-the-art dielectric polymers and *c*-BCB/BNNS composite at elevated temperatures. Furthermore, the PI- $\text{Al}_2\text{O}_3$  and PI- $\text{HfO}_2$  composites have greater scalability when compared to the current high-temperature dielectric polymer composites which are mostly based on *c*-BCB matrix. This work reveals the pronounced impact of inorganic nanofillers on high-temperature capacitive performance of the polymer composites and sheds light on the rational design of scalable dielectric polymer composites for applications in electric energy storage under extreme environments.

### Supporting Information

Supporting Information is available from the Wiley Online Library or from the author.

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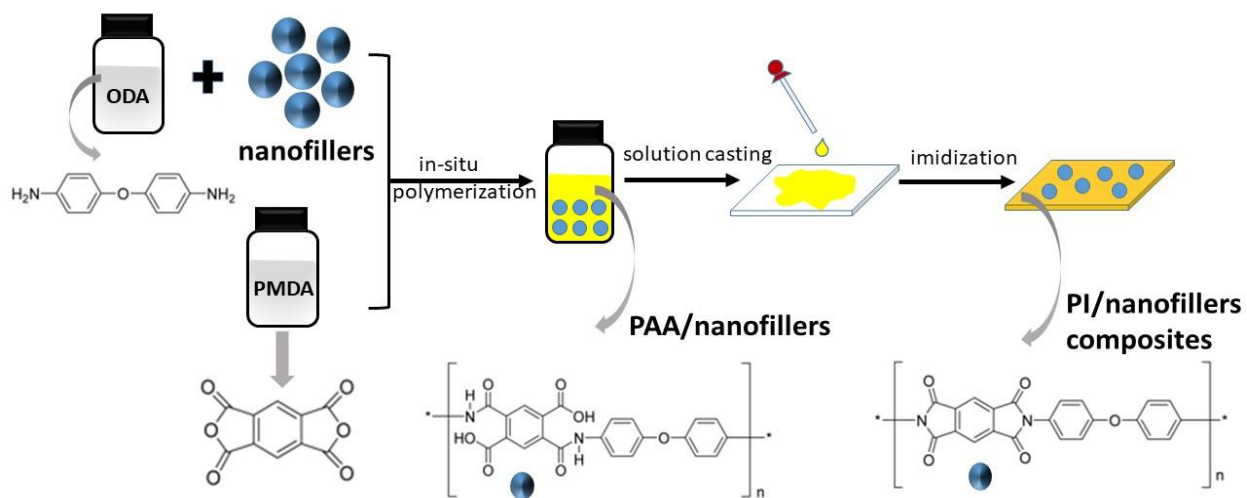
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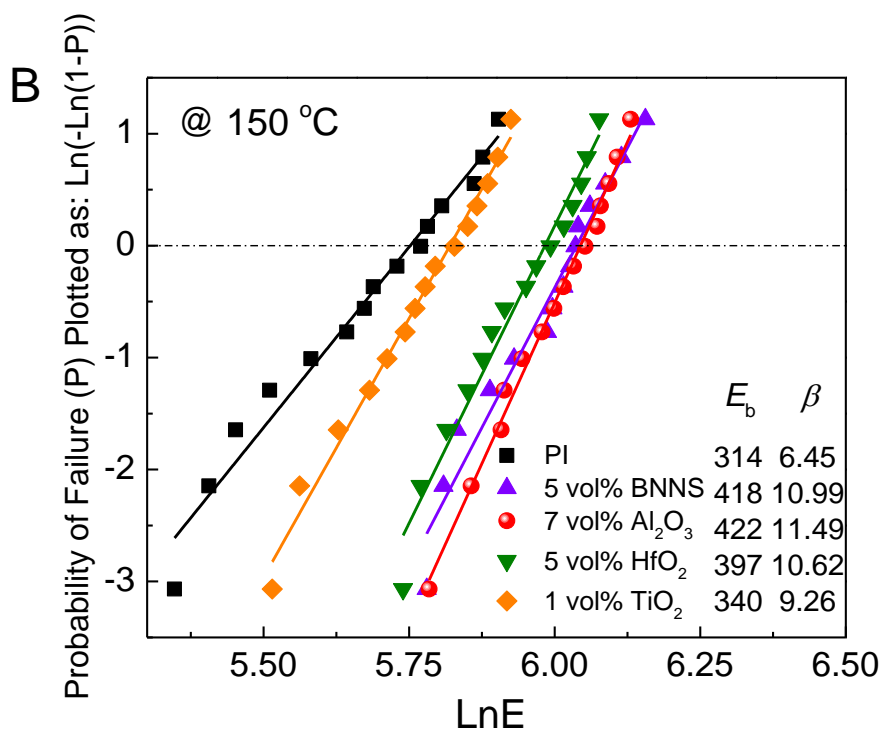
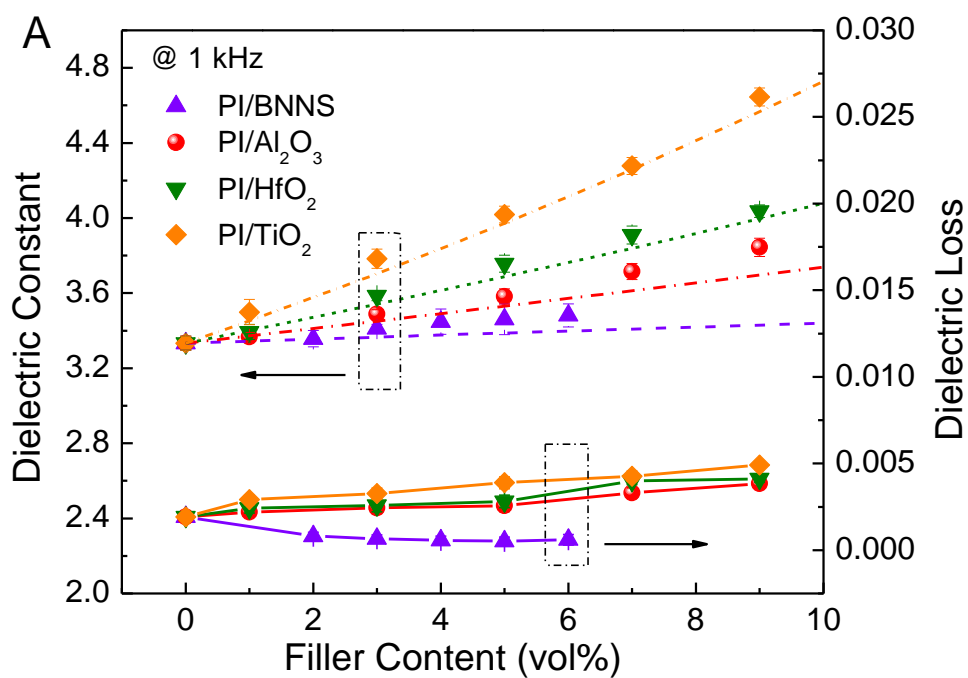
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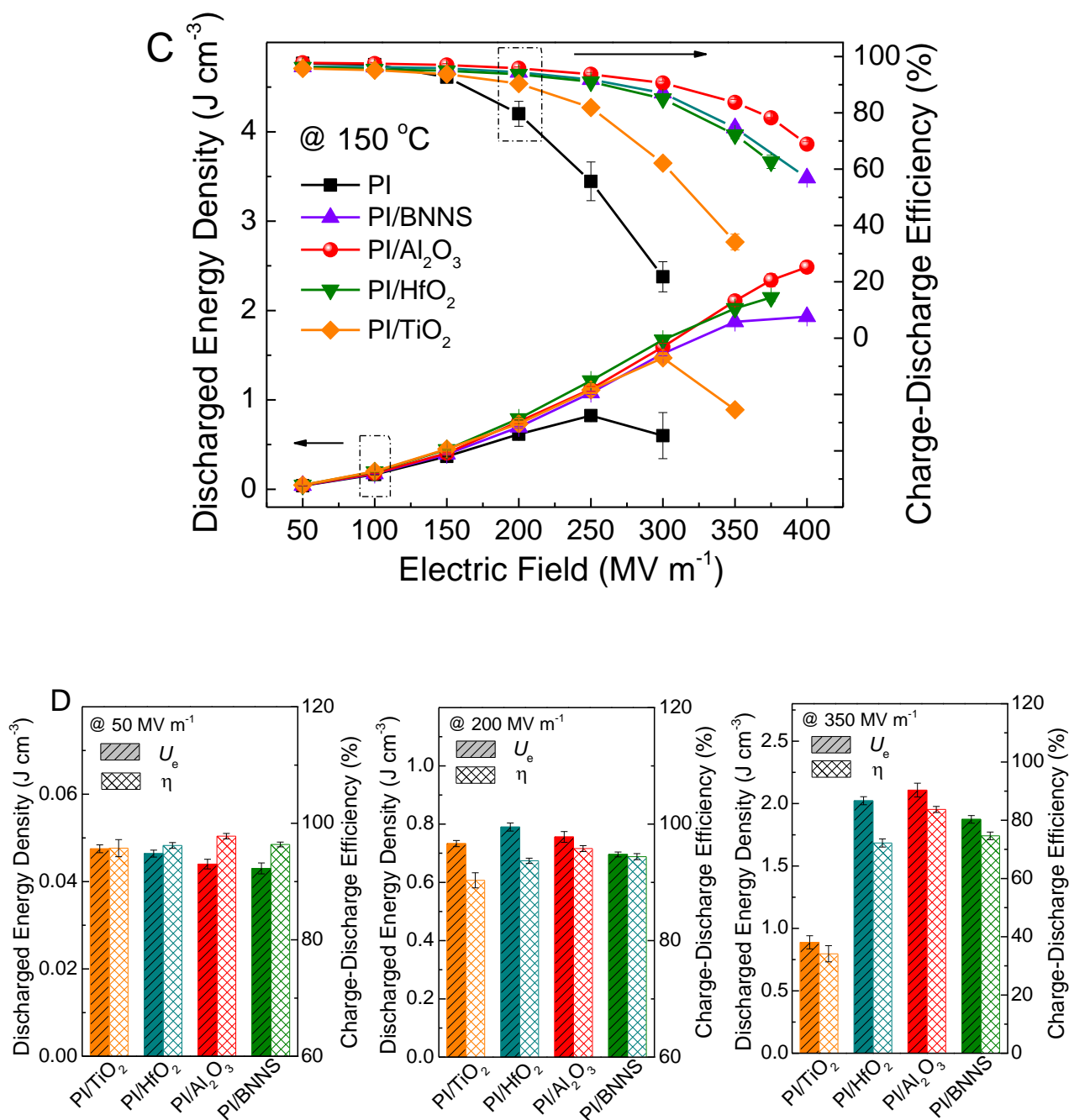
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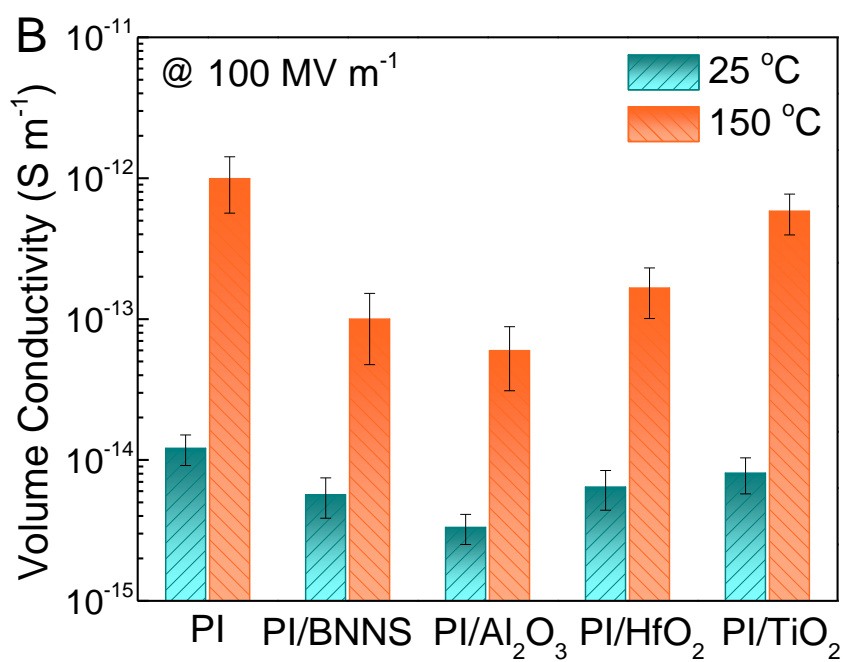
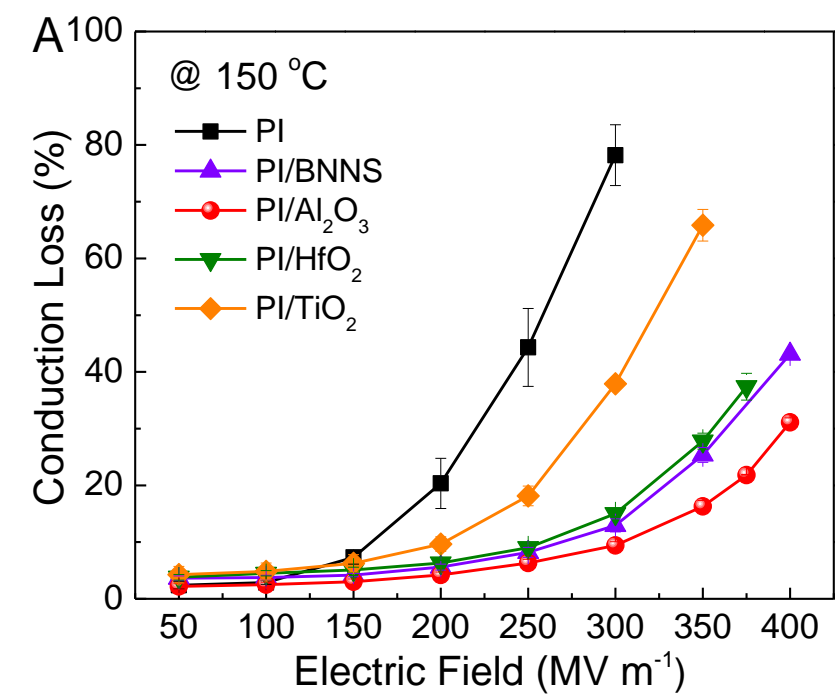
**Figure 1.** Schematic of the in-situ preparation of the PI-based polymer nanocomposites.

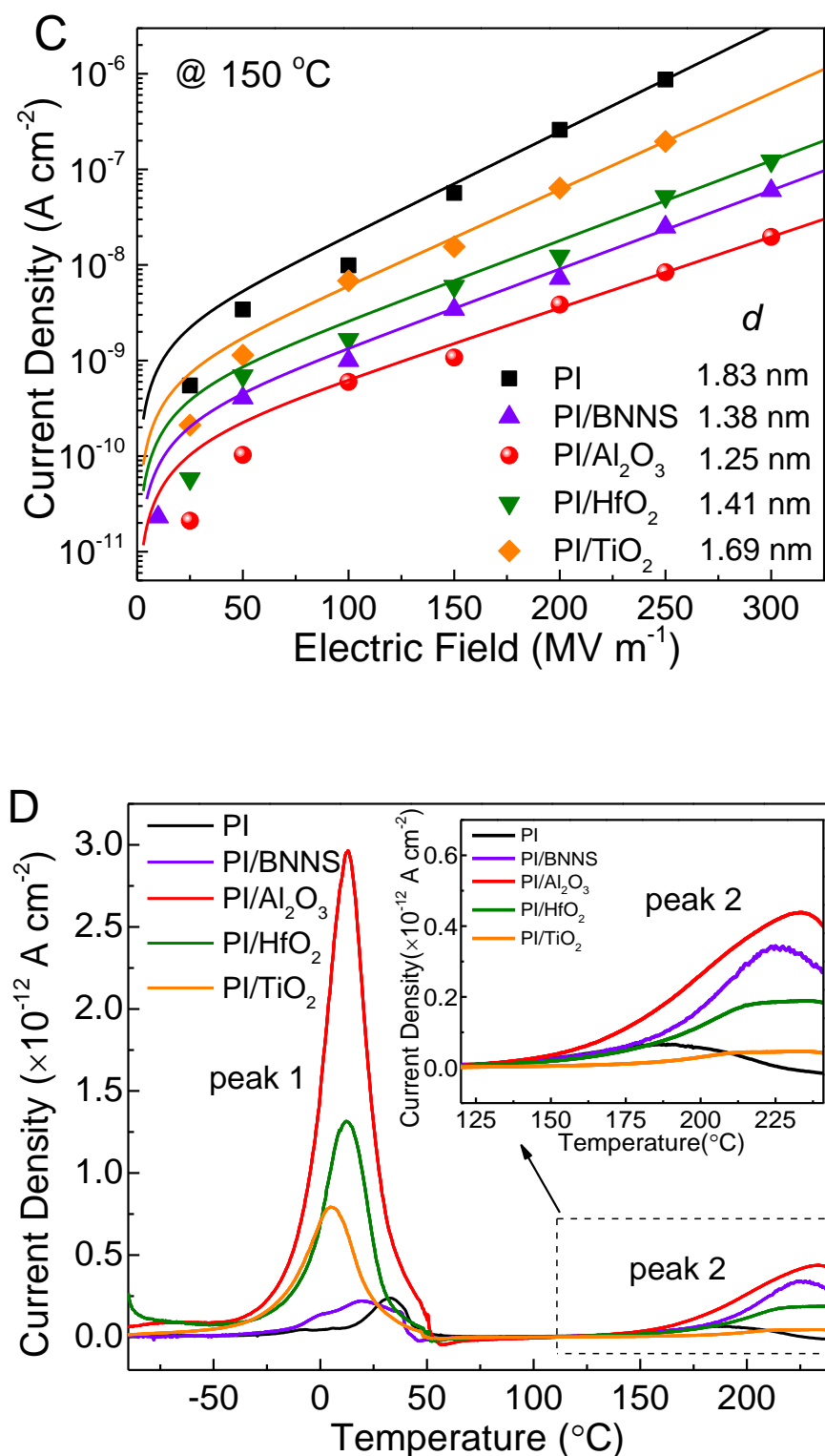




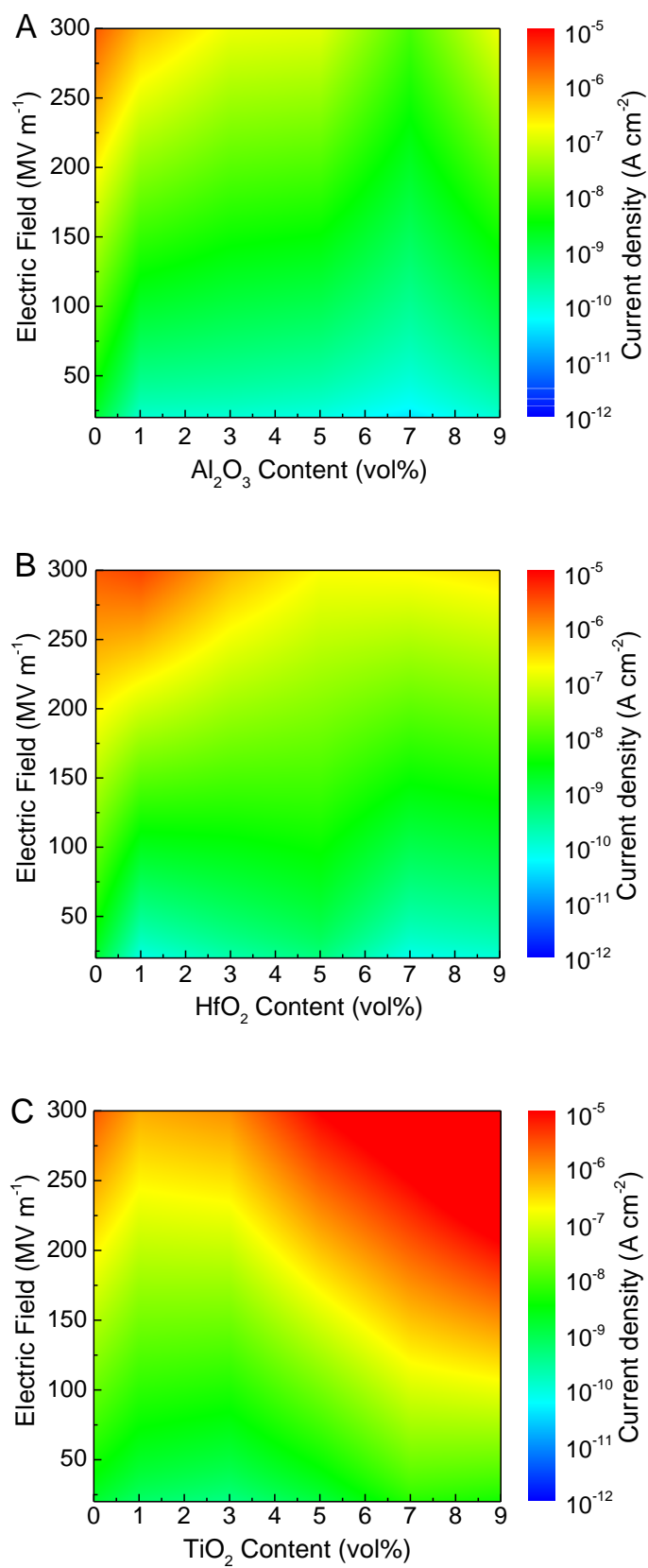


**Figure 2.** A) Dielectric constant and loss of the PI nanocomposites as a function of filler content at 25 °C and 1 kHz. The dash lines represent the calculated effective dielectric constant. B) Weibull breakdown strength of PI and the PI nanocomposites with the optimized filler contents measured at 150 °C. C) Discharged energy density and charge-discharge efficiency of PI and the PI nanocomposites with 5 vol% BNNS, 7 vol%  $\text{Al}_2\text{O}_3$ , 5 vol%  $\text{HfO}_2$  and 1 vol%  $\text{TiO}_2$  at 150 °C. D) Comparison of the discharged energy density and charge-discharge efficiency of the PI nanocomposites at 150 °C under different electric fields.





**Figure 3.** A) Conduction loss of PI and the PI nanocomposites with 5 vol% BNNS, 7 vol%  $\text{Al}_2\text{O}_3$ , 5 vol%  $\text{HfO}_2$  and 1 vol%  $\text{TiO}_2$  at 150 °C as a function of the applied field at 150 °C. B) Volume conductivity under  $100 \text{ MV m}^{-1}$  of PI and the PI nanocomposites at 25 °C and 150 °C. C) Current density of PI and the PI nanocomposites as a function of electric field at 150 °C. Solid curves represent the curve fits of Eq. 5. D) Thermally stimulated depolarization current (TSDC) spectra of PI and the PI nanocomposites.



**Figure 4.** Simulated current density distribution as a function of **A)** Al<sub>2</sub>O<sub>3</sub>, **B)** HfO<sub>2</sub> and **C)** TiO<sub>2</sub> filler content and the applied electric field at 150 °C.