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On the Elevated Temperature Thermal Stability of Nanoscale Mn-Ni-Si Precipitates Formed at Lower Temperature in Highly Irradiated Reactor Pressure Vessel Steels

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Atom probe tomography (APT) and scanning transmission electron microscopy (STEM) techniques were used to probe the long-time thermal stability of nm-scale Mn-Ni-Si precipitates (MNSPs) formed in intermediate and high Ni reactor pressure vessel steels under high fluence neutron irradiation at $\approx 320^\circ\text{C}$. Post irradiation annealing (PIA) at 425°C for up to 57 weeks was used to determine if the MNSPs are: (a) non-equilibrium solute clusters formed and sustained by radiation induced segregation (RIS); or, (b) equilibrium G or Γ_2 phases, that precipitate at accelerated rates due to radiation enhanced diffusion (RED). Note the latter is consistent with both thermodynamic models and x-ray diffraction (XRD) measurements. Both the experimental and an independently calibrated cluster dynamics (CD) model results show that the stability of the MNSPs is very sensitive to the alloy Ni and, to a lesser extent, Mn content. Thus, a small fraction of the largest MNSPs in the high Ni steel persist, and begin to coarsen at long times. These results suggest that the MNSPs remain a stable phase, even at 105°C higher than they formed at, thus are most certainly equilibrium phases at much lower service relevant temperatures of $\approx 290^\circ\text{C}$.

One potential barrier to extending nuclear light water reactor lifetimes to 80 years is embrittlement of their massive reactor pressure vessel (RPV)¹. Embrittlement is primarily due to the formation of nm-scale precipitates, which cause hardening and a corresponding increase in the ductile-to-brittle transition temperature^{2,3}. A major effect of irradiation is radiation enhanced solute diffusion (RED) associated with excess vacancy and self-interstitial concentrations. RED leads to hardening by Cu-rich precipitates (CRP) at low to intermediate neutron fluence (ϕt) in steels with more than ≈ 0.07 at.% Cu^{2,4}. Cu is highly insoluble at typical RPV service temperatures (T_i) of $\approx 290^\circ\text{C}$ and quickly precipitates as coherent bcc clusters that are also enriched in Mn, Ni and Si. Solute-defect cluster complexes, known as stable matrix features, which form in displacement cascades, also cause modest hardening, initially increasing roughly with the square root of ϕt in both low Cu and Cu bearing steels³. These features are thought to be precursors to formation of well-formed Mn-Ni-Si precipitates at higher ϕt , as discussed below.

A main challenge for RPV life extension is predicting embrittlement at low service-flux (ϕ) and high ϕt , where new embrittlement mechanisms may emerge. Notably, large mole fractions (f) of what have been shown

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Alloy	Cu	Ni	Mn	Mo	P	C	Si	Fe
LG	0.01	0.69	1.36	0.31	0.009	0.73	0.43	bal.
CM6	0.02	1.57	1.50	0.31	0.012	0.68	0.33	bal.

Table 1. Nominal steel compositions (at.%).

to be intermetallic Mn-Ni-Si precipitates (MNSPs), long ago predicted by Odette⁵, form at very high ϕt in high ϕ test reactor irradiations, both in low Cu and Cu-bearing steels⁶. They have also been observed in much lower ϕ test reactor and surveillance irradiations^{7–15}. However, MNSPs are not currently treated in US embrittlement models¹. Odette predicted that MNSPs are enhanced in low-alloy RPV steels by low ϕ and T_p , high Ni and even trace amounts of Cu^{16–18}. The concentration of dissolved Cu in RPV steels range from ≈ 0.01 to 0.3 wt.%. The corresponding concentration of Mn + Ni + Si is much larger, typically ranging from 2 to 4 wt.%. The latter solutes continue to slowly precipitate long after the matrix Cu is depleted. The MNSPs form as a separate appendage co-precipitate phase on the CRPs in Cu bearing steels, as is observed in thermal ageing studies⁹, low flux power reactor surveillance irradiations²⁰, and high flux test reactor irradiations⁶. As noted above, the cascade induced solute-defect cluster complexes, or stable matrix features, are thought to be precursor heterogeneous nucleation sites for MNSPs in low Cu steels, especially at medium Ni contents²¹. Although the existence of MNSPs is not in question, there are a number of unresolved issues regarding their detailed character and formation mechanisms.

Some have argued that MNSPs are not thermodynamic phases, but are rather non-equilibrium solute clusters primarily formed and sustained up to sizes of a few nm by radiation induced segregation (RIS) primarily at dislocation loops that form in displacement cascades^{22–25}. Specifically these models suggest either that Mn-Ni clusters are not thermally stable in Fe^{22,23}, or that they are only stable at combinations of very low temperatures and high solute concentrations, hence, require RIS to grow and persist^{24,25}. In contrast, equilibrium thermodynamic models predict that RED results in large MNSP mole fractions (f) at the low RPV operating temperatures of ≈ 300 °C²⁶. Notably, the predicted equilibrium precipitate f and compositions are in agreement with atom probe tomography (APT) data from steels irradiated to very high fluence⁶. In addition, recent X-ray diffraction and scattering experiments²⁷ have Γ_2 or G-phase intermetallic crystal structures, consistent with CALPHAD based thermodynamic predictions²¹.

Post irradiation annealing (PIA) can provide significant additional insight into the nature of the MNSPs. For example, clusters that form through a RIS mechanism should not be stable during PIA, even at $T_i \approx 290$ °C. However, very slow thermal diffusion kinetics precludes conducting meaningful experiments at such low annealing temperatures (T_a). While diffusion rates increase with higher T_a , the equilibrium MNSP phase fractions are also reduced. Thus, dissolution of what are argued to be RIS formed Mn-Ni-(Si) clusters following short term anneals at T_a from 450–500 °C^{10,28}, or in low solute content model alloys at $T_a = 400$ °C¹⁴, does not prove that they are thermodynamically unstable at much lower service $T_i \approx 290$ °C. Further, due to their small radii (r) of ≈ 0.50 –2.5 nm, even if MNSPs are bulk equilibrium phases, they will dissolve at a higher T_a , due to the Gibbs-Thomson effect, if they are below the critical radius in a post-annealing, solute-depleted matrix. The effect of precipitate size is discussed further in Section 4. Note this approach can also be used to estimate the phase boundary at elevated temperature.

Because of the slow diffusion rates below ≈ 450 °C, very long time (t_a) PIA is required to distinguish kinetic from thermodynamic effects, and to explore MNSP phase boundaries for comparison to thermodynamic models, it is absolutely critical to compare the PIA data to predictions of models that properly account for both thermodynamics and dissolution mechanisms and kinetics. Achieving these fundamental objectives also supports refining the predictive Mn-Ni-Si precipitation²¹ and PIA models, including for application to guiding embrittlement predictions and annealing remediation treatments.

Materials and Methods

The compositions of the two essentially Cu-free split-melt bainitic RPV steels studied here, designated LG and CM6, are shown in Table 1. The split-melt alloy microstructures and properties are fully representative of actual in-service RPV steels. The two steels have similar compositions, with the exception of Ni, that nominally ranges from ≈ 0.69 at.% (LG, medium) to ≈ 1.57 at.% (CM6, high). These alloys (among many others) were irradiated in the Advanced Test Reactor (ATR) to a very high fluence, $\phi t \approx 1.1 \pm 0.2 \times 10^{21}$ n/cm² at a high $\phi \approx 2.3 \pm 0.4 \times 10^{14}$ n/cm²-s ($E > 1$ MeV) at $\approx 320 \pm 15$ °C²⁹. This ϕt is ≈ 11 times higher than that expected for RPVs at extended life, while the corresponding ϕ is ≈ 4600 times higher than typical RPV $\phi \approx 5 \times 10^{10}$ n/cm²-s. It is well established that higher ϕ delays precipitation to higher ϕt , with a ϕ -adjusted effective fluence (ϕt_e) roughly scaling as $\phi t_e \approx \phi t (\phi_r / \phi)^p$, where ϕ_r is a specified reference flux and p ranges from ≈ 0.15 to 0.25^{2,5,16,30,31}. Thus the effective ATR ϕt_e is estimated to be only ≈ 2 – 4×10^{20} , which is 2 to 4 times the maximum $\phi t_e \approx 1 \times 10^{20}$ that an RPV would be expected to experience at an 80 year extended life.

Note, the exact relationship between the effective fluence of the ATR irradiation condition and that experienced under extended life is not critical to the main purpose of this experiment, which was to generate significant quantities of MNSPs that could be readily characterized and modeled under long-time, high-temperature PIA. Atom probe tomography (APT) studies show that in the as-irradiated (AI) condition the alloys are nearly fully decomposed, at an approximately saturated MNSP f^6 . The two steels were annealed in vacuum for times of 1, 7, 17, 29 and 57 weeks. The MNSPs were characterized by APT up to 29 weeks, and by Scanning Transmission Electron Microscopy (STEM)-Energy Dispersive X-ray Spectroscopy (EDS) at 57 weeks. The annealing times were selected to ensure that any changes, or lack thereof, in the MNSPs would not be limited by slow solute thermal diffusion

kinetics. Due to the very limited amount of irradiated material, the PIA was performed on 1.5 mm punched discs, precluding a sequence of standard microhardness measurements.

Atom probe tomography. Atom probe tomography (APT) was used to measure the MNSP composition, size distribution and average radius ($\langle r \rangle$), number density (N) and mole fraction (f) in the AI condition and following each anneal for all times but the longest annealing time of 57 weeks. The APT was carried out at the Center for Advanced Energy Studies (CAES) located in Idaho Falls, ID, with support from the Idaho National Laboratory managed Nuclear Science User Facilities. APT tips were fabricated using a FEI Quanta 3D FEG Focused Ion Beam, using 5 kV and 2 kV cleanup steps to reduce Ga damage. The tips were examined in a CAMECA LEAP 4000X HR in voltage mode, at a 20% pulse fraction and 50 K. Note one tip of the high Ni steel (CM6), annealed for 29 weeks, was run in laser mode with a pulse energy of 75 pJ, a repetition rate of 250 kHz and a temperature of 40 K, in anticipation that only a very low number density of MNSPs would remain in this condition, so a larger sample volume was required to increase the probability of observing them. However, an MNSP with similar size and composition was also seen in a shorter voltage mode run as well. A full description of the APT analysis procedures can be found in⁶.

APT reconstructions and analysis were performed using the CAMECA Integrated Visualization and Analysis Software (IVAS). The clusters were defined using the cluster analysis tool in the IVAS software with order = 5, $d_{max} = 0.6$ nm, $N_{min} = 20$ –30 and envelope = erosion = 0.6 nm. A constant d_{max} was used for all conditions. Decreases in d_{max} in a given tip results in a lower measured f and $\langle r \rangle$. Thus, measuring changes in f and $\langle r \rangle$ using a different d_{max} for each annealing interval could introduce artificial biases. The main consequence of choosing a d_{max} that is too large is that random solute density variations in the matrix might be misidentified as clusters. Note in the AI condition, the solutes are highly depleted from the matrix; hence, the probability of identifying random fluctuations as clusters is negligible. However, significant precipitate dissolution occurs after long-term annealing at 425 °C, resulting in a much higher matrix solute contents. In these cases, all measured precipitates had $N \gg N_{min}$, so no random solute density fluctuations were incorrectly identified as precipitates. The MNSP f was defined as the number of solute atoms in the clusters divided by the total number of atoms in the analyzed volume. The precipitate mole fraction varies slightly from volume fraction if the atomic densities of the precipitate and matrix phases differ. Thus, all model data shown for comparisons is also mole fraction. For further information regarding this difference see the Supplemental Information.

The low evaporation field of the precipitates changes the local magnification factor resulting in a focusing of matrix atoms into the precipitate region on the detector and is signaled by higher than physical atom densities in the reconstructed dataset^{32–37}. These artifacts can result in distortions of the composition, shape, and size of precipitates, and most specifically their apparent Fe content, some or all of which actually comes from the adjoining matrix thus contributing to the higher than physical atom density in the precipitate region. Using the number of solute atoms to define the cluster size minimizes these field evaporation distortions. The number of solute atoms associated with each precipitate, corrected for efficiency, was determined and multiplied by the atomic volume of Fe. The precipitate r was then defined as the radius of a sphere encompassing the total solute volume. While these precipitates are thought to be intermetallic phases, differences in their corresponding average atomic volume versus Fe results in variations in r of less than 2%. The MNSP number density (N) was calculated by dividing the number of clusters in the dataset by the total volume in the analyzed tip. Precipitates on the edge of the tip are not included in the determining the size distributions, or average $\langle r \rangle$, but are counted as one half in the estimating N . The associated error f , N and $\langle r \rangle$ estimates are based on the tip-to-tip variations observed here for conditions with multiple tips, or in the one case with a single tip, the average of the others. The standard IVAS reconstructions, as usual, suggested that there is a significant amount of Fe in all of the MNSPs. While, as noted above, Fe is thought to be an APT artifact, the nominal value is provided for those that wish to interpret the data differently.

Energy dispersive X-ray spectroscopy. At longer annealing times, a significant reduction in the precipitate number density was observed. While APT has very high spatial resolution and measures the detailed chemical nature of the precipitates, it has a very small sampling volume, making it difficult to characterize them when they are present at a very low number density ($\ll 10^{22} \text{ m}^{-3}$). Thus, at the longest annealing time (57 weeks), Energy Dispersive X-ray Spectroscopy (EDS) was performed using an FEI TALOS F200X S/TEM in the Low Activation Materials Development and Analysis Laboratory at Oak Ridge National Laboratory. EDS mapping was performed using a probe size of ~1 nm and current of 1.0 nA, respectively. Analysis of the data was performed using the Bruker-Esprit software. While the TALOS provided high-resolution chemical maps, it was not fully calibrated for quantitative chemical analysis. Thus to complement these high resolution maps, additional EDS scans were performed on the FEI Titan 300 kV FEG S/TEM at UCSB. A line scan with 4 nm spacing between points was taken across three grains, one with a high density of very large precipitates and two with a few sparse precipitates present, to measure the local solute contents.

Thermodynamic and cluster dynamics modeling. A cluster dynamics (CD) model, using CALPHAD thermodynamics, thermal diffusion coefficients from literature and fitted precipitate interface energies, was used to guide the experimental design and to help analyze the annealing results [21]. The model predictions of the equilibrium f have been reported previously and qualitatively favorably compare to the high ϕt ATR data⁶. The corresponding CALPHAD predicted equilibrium f for the two low Cu steels as a function of T_a are shown in Fig. 1 for the nominal alloy compositions²⁶. Again, the data from all models presented here gives precipitate mole fraction for comparison with APT data. CALPHAD predicts that only the Γ_2 phase ($\text{Mn}(\text{Ni}, \text{Si})_2$) is stable in the high Ni (CM6) steel, with composition about 33% Mn–52% Ni–15% Si, exists up to 500 °C, while the G phase ($\text{Mn}_6\text{Ni}_6\text{Si}_7$) persists only up to ≈ 390 °C in the medium Ni (LG) steel²⁶. Note that this bulk phase CALPHAD thermodynamic calculation leading to Fig. 1 does not include effects of the interface energies of the small

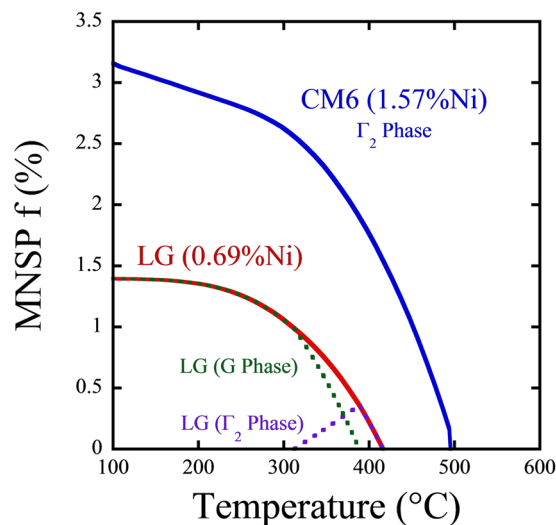


Figure 1. CALPHAD predictions of Mn-Ni-Si precipitate f as a function of annealing temperature for two Cu-free steels with varying Ni content.

precipitates, although they are included in the CD model discussed below. Again a recent XRD study for the as-irradiated condition found G phase precipitates in the medium Ni steel, while the high Ni steel contains the Γ_2 phase, both as predicted by CALPHAD at 320 °C²⁷.

Figure 1 shows that CALPHAD predicts that the MNSPs in the medium Ni steel (LG) should completely dissolve above ≈ 415 °C, while the Γ_2 phase in high Ni steel (CM6) is predicted to fully dissolve at ≈ 500 °C. Because lower T_a results in slower solute diffusion, the isothermal annealing was carried out at an intermediate temperature of 425 °C, with the intention of testing the thermodynamic model predicting full dissolution in LG (medium Ni) and that some MNSPs would remain in CM6 (high Ni). The complete MNSP dissolution of the phase in the medium Ni steel also acts as a kinetic marker to help estimate the effective diffusion distances at various annealing times that are pertinent to both alloys.

CD modeling was also carried out to help interpret the very complex MNSP dissolution and coarsening processes. Briefly, CD models the evolution of the MNSPs in discrete $n - 1$, n and $n + 1$ cluster sizes, where n is the number of atoms. The n ranges from 2 to n_{\max} in a coupled set of $n_{\max} - 1$ ordinary differential equations, which incorporate n -dependent effective solute impingement and emission transition rate coefficients. In this case the solutes are treated as stoichiometric molecules of the pertinent phase. The CD method applied to modeling G and Γ_2 phase precipitation under irradiation is described elsewhere²¹. The CD model for annealing used here assumes thermal-diffusion controlled kinetics, and requires only 4 key experimental input parameters: (a) the effective thermal solute diffusion coefficient (D), derived from the literature; (b) the solute equilibrium solubility (X_e), determined by the free energy difference between the dissolved and precipitated solute states (that is the equilibrium phase diagram), evaluated from the Thermo-Calc³⁸ TCAL2 database³⁹; (c) the MNSP-Fe interface energy (γ), which differ slightly for the G and Γ_2 phases; and (d) the as-irradiated MNSP size distribution, taken directly from the APT measurements. The γ were derived independently as fit parameters in the CD precipitation model, and were not adjusted in this PIA study²¹. Thus, the PIA CD model has no independently adjusted fit parameters.

Results and Discussion

STEM Observations. The APT data on the 29 weeks annealed high Ni alloy showed a very large reduction in the number densities (N) of the MNSPs, with few, if any, precipitates in a given tip. The tips without MNSPs coincided with lower local Ni and Mn contents. Hence, we first focus on the STEM-EDS characterization of the 57 weeks PIA condition, in order to significantly increase the sampling volume relative to the APT observations. This directly confronts the question of the thermodynamic stability of the MNSPs, given a sufficient alloy Ni and Mn content. The STEM-EDS observations generally show regions with no precipitates and other regions with coarsened precipitates still remaining. A typical region with Mn-Ni-Si precipitates, with $\langle r \rangle \approx 2.7$ nm versus ≈ 1.53 nm in the AI condition, is shown in 2a–e. The main conclusion of the STEM-EDS study is that sufficiently coarsened MNSP are stable at near nominal amounts of Ni and Mn, even at a very long t_a that is ≈ 8 times that required for full dissolution of the MNSPs in the medium Ni alloy.

Figure 2d is a dark field (DF) STEM image showing a number of dislocation lines. Figure 2e is the same DF image overlaid with a partially transparent image of the Ni EDS signal, clearly showing a strong association between the dislocations and the remaining precipitates. This association is not unexpected, since the energy of Mn-Ni solute clusters are lower on dislocations than in the matrix^{24,40} and, as a corollary, dislocations are attracted to MNSPs.

Figure 2f–j shows one grain that contained very large Mn-Ni enriched features, on the order of 20–30 nm long. These large precipitates were not significantly enriched in Si, except for one even larger MNSP on a grain boundary. The Mn-Ni enriched features are much larger than any previously reported precipitates in a neutron irradiated RPV steel. It is likely that they are a MnNi B₂ phase⁴¹. Note, such large features have also been

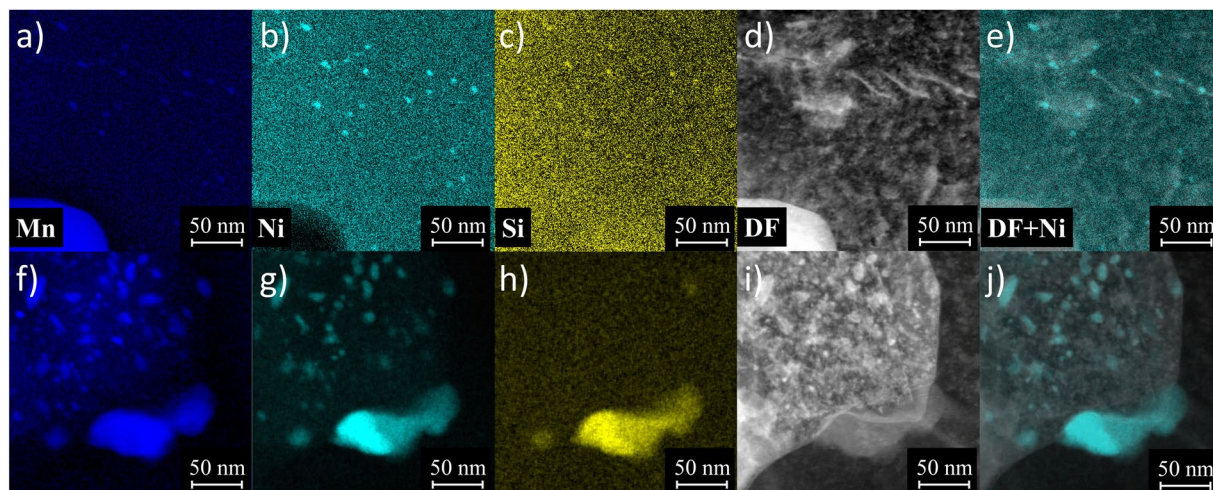


Figure 2. EDS maps showing Mn-Ni-Si precipitates remaining in the high Ni steel after annealing for 57 weeks at 425 °C from: (a–e) a region with relatively small precipitates, many of which are located on dislocations and (f–j) a region with very large Mn-Ni precipitates.

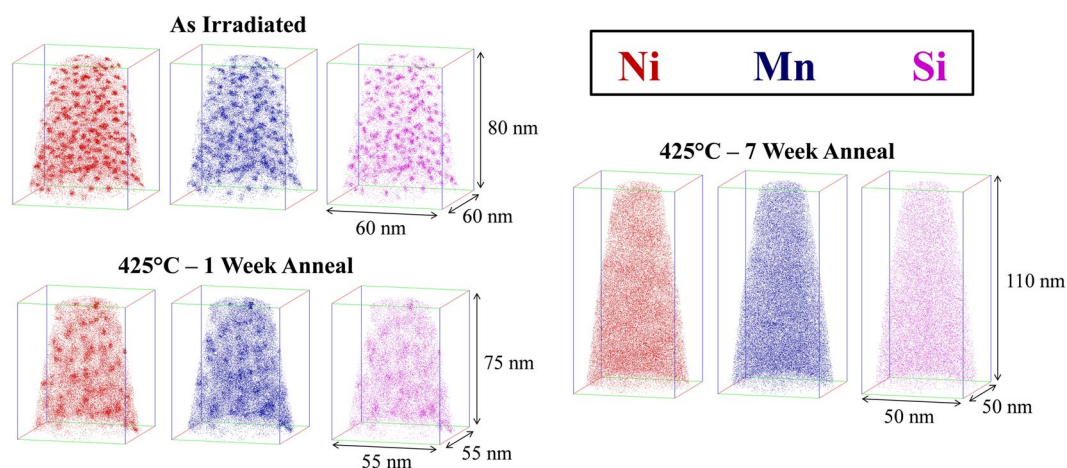


Figure 3. Atom maps for the Cu-free, medium Ni steel (LG) in the (a) AI condition, (b) 425 °C - 1 week annealed condition, and (c) 425 °C annealed - 7 weeks condition.

reported following proton irradiation⁴². A FEI Titan STEM EDS line scan was performed to determine the local solute composition of the grain with large precipitates, as well as the two nearby grains which had only a few, sparsely-spaced MNSPs. This scan showed the local composition of the grain with large features was ≈ 3.36 at.% Ni, 1.23 at.% Mn and 0.34 at.% Si, while both neighboring grains had compositions of ≈ 1.66 –1.70 at.% Ni, 0.60–0.72 at.% Mn and 0.36–0.48 at.% Si. The composition of the very high Ni grain is consistent with the formation of the MnNi B_2 phase with lower Si⁴¹. Additional details regarding the line scan can be found in the Supplemental Information.

The most important result from the STEM-EDS study is that, given sufficient Ni, sufficiently large MNSPs are thermodynamically a stable equilibrium phases at 425 °C, which is 105 °C higher than T_i , and 135 °C higher than for normal RPV service conditions. Figure 2 shows that the MNSPs are much more stable, and unambiguously thermodynamic equilibrium phases, at these lower T_i .

APT results. Atom maps from the medium Ni steel (LG) for the AI and 425 °C PIA conditions are shown in Fig. 3. The MNSPs are very clearly dissolving following the one-week anneal; and the Mn and Si appear to have diffused further than the Ni, hence are the most dilute. The solutes in the medium Ni steel are nearly entirely dissolved after the 7 weeks anneal, as predicted by the thermodynamic model (see Fig. 1), with only weak indications of residual solute clustering. The solutes are expected to be fully dissolved in the medium Ni steel after the 29 weeks anneal, since they have presumably diffused approximately twice as far compared to the 7 weeks condition⁴³.

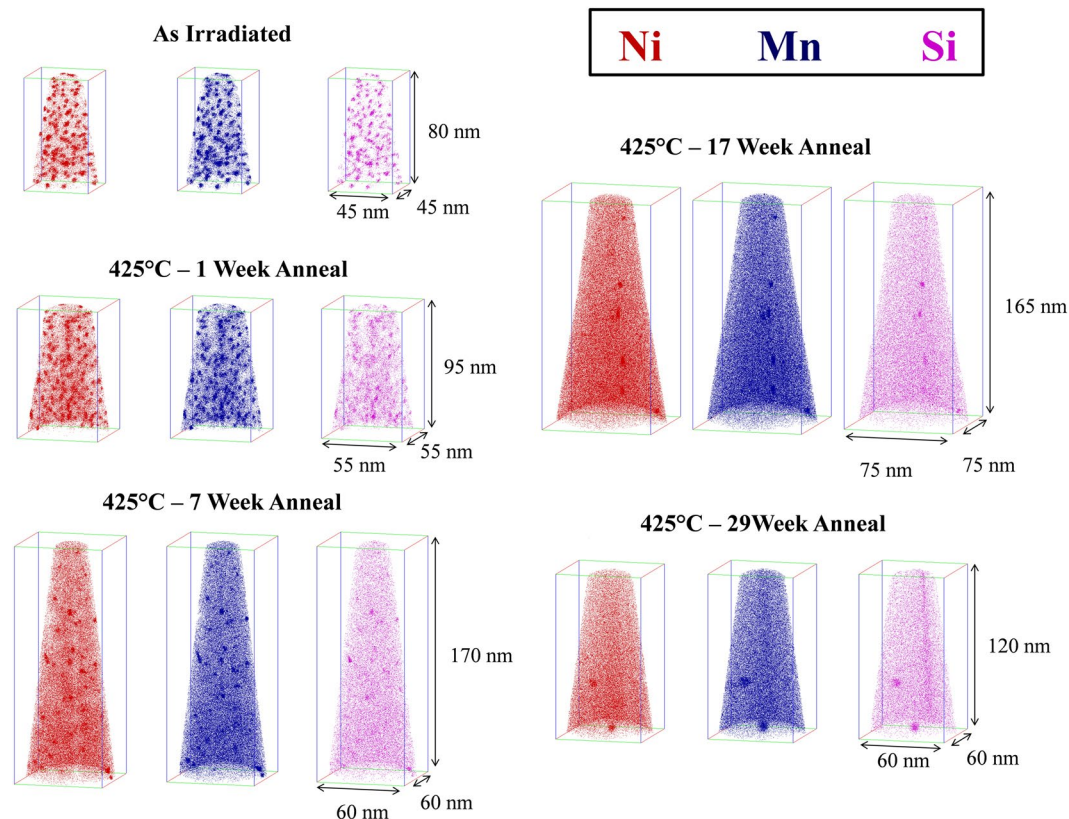


Figure 4. Atom maps for the low Cu, high Ni steel (CM6) in the AI condition (top left) and 425 °C annealed conditions at times of: 1 week (mid left), 7 weeks (bottom left), 17 weeks (top right) and 29 weeks (bottom right).

t_a	Average t_a , $\langle d \rangle$, N and f^a			Average Precipitate Composition (at.%)						Precipitate Fe	Relative Composition	
	$\langle r \rangle$	N	f	Cu	Ni	Mn	Si	Mo	C	P	Fe ^b	Mn/Ni/Si
0	1.50 ± 0.11	19.50 ± 1.47	2.82 ± 0.14	0.0	52.1	35.2	11.7	0.5	0.5	0.0	58.9	0.35/0.53/0.12
1	1.41 ± 0.19	11.80 ± 2.72	1.43 ± 0.53	0.3	53.0	35.4	10.0	0.8	0.3	0.3	62.1	0.36/0.54/0.10
7	1.63 ± 0.42	2.19 ± 0.70	0.38 ± 0.07	0.0	52.8	38.0	7.8	0.9	0.2	0.2	57.6	0.38/0.54/0.08
17	2.13 ± 0.22	0.30 ± 0.08	0.10 ± 0.02	0.0	52.6	37.6	7.0	1.6	0.9	0.2	55.8	0.39/0.54/0.07
29	2.78 ± 0.13	0.14 ± 0.07	0.11 ± 0.02	0.0	35.8	35.5	14.3	8.7	5.1	0.6	37.5	0.41/0.42/0.17

Table 2. Precipitate summary for the high Ni steel (CM6) from the AI and 425 °C annealed conditions. ^aUnits: t_a (wks), $\langle d \rangle$ (nm), N (10^{23} m^{-3}), f (%). ^bThe nominal IVAS Fe found in all the MNSPs, that is thought to largely be an artifact.

Atom maps in Fig. 4 for the high 1.6 at.% Ni steel (CM6) show that the MNSPs are much more stable, with well-defined precipitates still remaining after PIA for 29 weeks. The corresponding APT $\langle r \rangle$, N and f data are summarized in Table 2 and Fig. 5. Note that Table 2 gives the average values and uncertainty estimates for a given condition, while Fig. 5 shows a data point for each measured APT tip, demonstrating that N and f vary significantly from region to region. As will be discussed below, this variability is dictated by the local bulk composition of an individual APT tip. The solid lines in Fig. 5 are the CD model predictions for the nominal composition. Both N and f decrease rapidly with the increasing t_a . There is a corresponding small dip in $\langle r \rangle$, followed by a slight increase up to 7 weeks, which is primarily due to the dissolution of the smallest MNSPs, rather than significant coarsening of the larger ones. However, it is notable that between 7 and 29 weeks $\langle r \rangle$ closely tracks the kinetics predicted by the CD model. The initial decrease in the MNSP N is also in agreement with model, but the APT data fall below the CD predictions between 17 and 29 weeks, although the rate of decrease in N and f slow, as is expected, under mixed dissolution and coarsening kinetics. Clearly, the nominal CD model over predicts N and f at long times. However, this is not surprising given the approximate parameterization of the CD model and the complexity of the interacting and competing processes mediating precipitate annealing, as discussed below. Note, the continuing decrease in N during PIA would make MNSPs very unlikely to be found in APT studies at 57 weeks, while they are clearly present in the STEM-EDS observations. Figure 6 shows the high sensitivity of

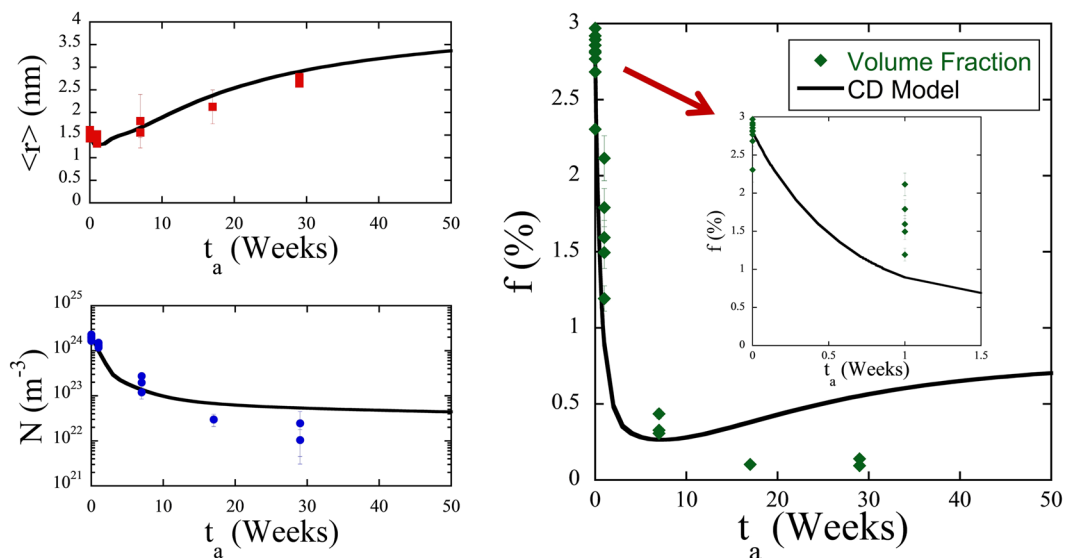


Figure 5. APT measured precipitate $\langle r \rangle$ (nm), N (m^{-3}) and f (%) after annealing (points) and CD predictions (lines) for the high Ni steel (CM6) at $T_a = 425^\circ C$. Note that the plot of f vs t_a includes a blowup of the shorter annealing times to more clearly see these values. CD simulation conditions are described in the text.

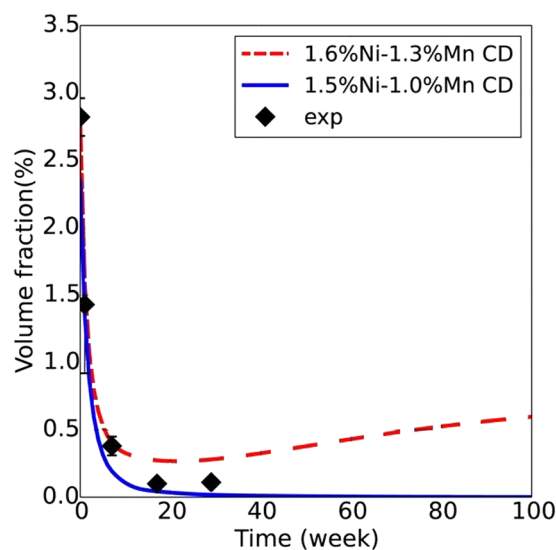


Figure 6. f as a function of annealing time at $T_a = 425^\circ C$ for two CD models with 0.34 at.% Si and either 1.6 at.% Ni and 1.3 at.% Mn or 1.5 at.% Ni and 1.0 at.% Mn.

the model to modest reductions in alloy Ni and Mn contents, of ≈ 6 and 23%, respectively, that lead to complete MNSP dissolution, again consistent with the STEM-EDS observations of lower solute regions.

The APT observations of MNSP response to PIA at temperatures much higher than they were formed at shows 3 stages: a) initial rapid dissolution of small precipitates between 0 and 7 weeks; b) mixed dissolution and coarsening between 7 and 17 weeks; and, c) coarsening between 17 and 29 weeks at a near minimum f . The kinetic order of coarsening beyond 7 weeks, as reflected in the time exponent, is illustrated in Fig. 7, showing plots of $\langle r(t_a) \rangle^3 - \langle r(7) \rangle^3$ and $1/N(t_a) - 1/N(7)$, which are both approximately linear in t_a , for classical diffusion controlled coarsening, often called Ostwald Ripening⁴⁴. Notably, the order of coarsening kinetics is insensitive to the various CD model parameters as a combination of interface energy, solubility and diffusion coefficients, which strongly influence the absolute predictions of $\langle r \rangle$, N and f . As discussed further below, the annealing processes in this case are more complex than those that are treated in simple coarsening models. However, the approximately linear t_a -dependence of $\langle r(t_a) \rangle^3$ and $1/N(t_a)$ kinetics is powerful evidence that coarsening is occurring during the high temperature PIA at longer t_a . The $\langle r \rangle$ at 17 weeks is a little lower than the mean fit line, likely due to the transition from dissolution to coarsening dominated kinetics; while $1/N(t_a)$ is almost perfectly linear. In both cases the linear kinetics are within the estimated scatter in the data.

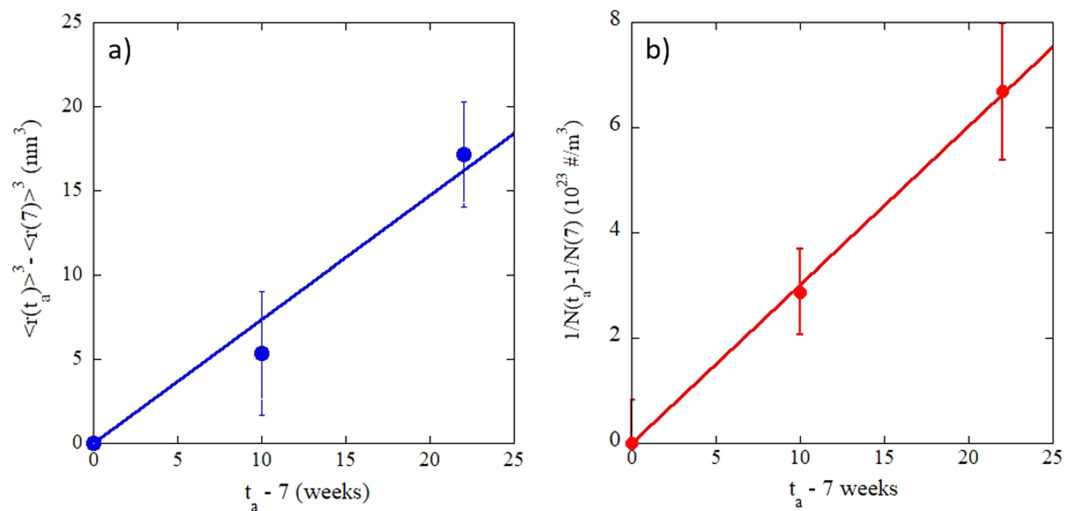


Figure 7. Plots showing MNSP coarsening kinetics that are consistent with a diffusion controlled mechanism for: (a) of $\langle r(t_a) \rangle^3 - \langle r(7) \rangle^3$; and, (b) $1/N(t_a) - 1/N(7)$.

t_a	Average Matrix Composition (at.%)					
	Ni	Mn	Si	Mo	C	P
0	0.17	0.32	0.04	0.25	0.16	0.00
1	0.62	0.62	0.18	0.22	0.12	0.00
7	1.43	1.24	0.34	0.25	0.06	0.01
17	1.60	1.08	0.37	0.22	0.08	0.01
29	1.66	1.34	0.38	0.25	0.16	0.00

Table 3. Amount of Mn, Ni and Si in the matrix for the high Ni steel (CM6) from the AI and 425 °C annealed conditions.

t_a (week)	Mn/Ni/Si	Closest Phase Mn/Ni/Si
0	0.35/0.53/0.12	Γ_2 : \approx 34/47-52/14-20 XRD
1	0.36/0.54/0.10	Γ_2 to B_2 : \approx 41-47/50/3-9
7	0.38/0.54/0.08	Γ_2 to B_2 : \approx 41-47/50/3-9
17	0.39/0.54/0.07	Γ_2 to B_2 : \approx 41-47/50/3-9
29	0.41/0.42/0.17	Γ_2 to T_7 : \approx 50/33/17

Table 4. Relative amount of Mn, Ni and Si in the precipitates and compared with known Mn-Ni-Si phases. Note phase name: $\Gamma_2 = T_6$ and $G = T_3$.

The average precipitate compositions as a function of t_a are also shown in Table 2. While Fe is an APT artifact, the nominal IVAS value is included in the table for those that wish to interpret the data differently. Table 3 summarizes the corresponding matrix compositions, which return to near nominal bulk values, reflecting the small residual f of the MNSPs. Table 4 shows the relative precipitate Mn, Ni and Si compositions compared to the closest known Mn-Ni-Si intermetallic phases. The Γ_2 phase (33%Mn-52%Ni-15%Si) is closest to the composition in the AI condition, but the MNSPs contain less Si for t_a up to 17 weeks, perhaps indicating initial evolution towards the cubic B_2 phase. The return to higher Si, at 29 weeks, may signal a partial transition to the lower Ni T_7 phase. Note these phase associations are speculative, since the extent of their composition fields are not known. For example, it is well established that Si and Mn are relatively interchangeable on their sub lattice in response to changes in the alloy bulk compositions^{45,46}. Indeed, while TEM showed extra diffraction spots due to the presence of the precipitates, it was not possible to index them to specific phases, due to their still very small sizes and possible association with dislocations.

It has been previously shown that tip-to-tip variability even in the same steel can be exploited to characterize the effects composition variations on precipitation^{6,21}. The local composition also has a strong effect on the precipitate stability during PIA. For example, while MNSPs were still found in all the high Ni steel (CM6) tips in the AI, 1 week and 7 weeks t_a conditions, they were only found in tips containing more measured \approx 1.5% Ni and 1.3% Mn bulk solutes (close to the nominal alloy composition) for longer t_a . Due to the strong and very systematic effect of Ni and Mn, only tips that contained close to nominal alloy composition were included in plots of $\langle r \rangle$, f

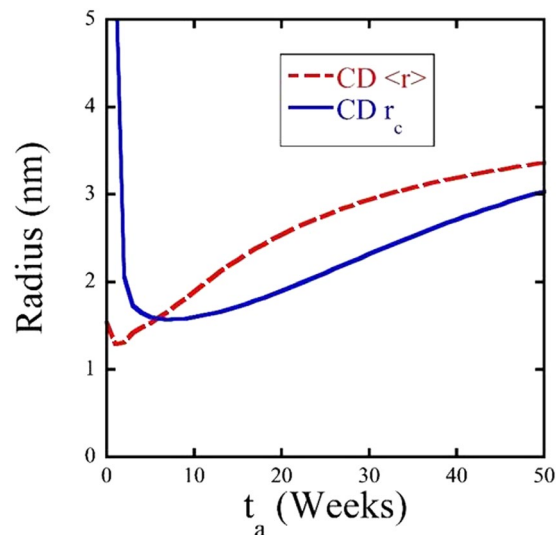


Figure 8. Cluster dynamics average precipitate radius ($\langle r \rangle$) and calculated critical radius (r_c) as a function of annealing time. Simulation conditions are the same as in Fig. 5.

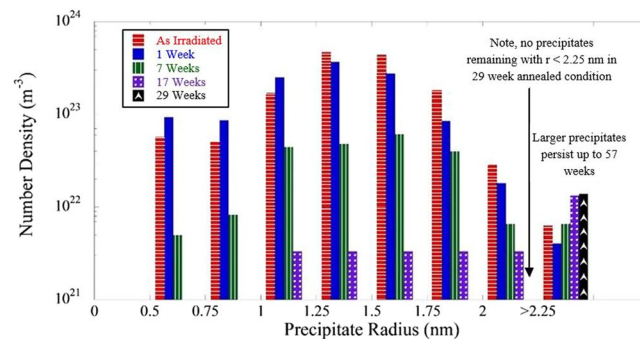


Figure 9. Size distribution of precipitates in the high Ni steel (CM6) for the AI and annealed conditions. Note that no precipitates with $r < 1$ nm were observed after 17 weeks of annealing and no precipitates with $r < 2.25$ nm were observed after 29 weeks of annealing.

and N . The full data for all runs taken is provided in the Supplemental Material (Tables S1 and S2) to more clearly demonstrate the tip-to-tip bulk composition variability and the corresponding impact on precipitate stability. It was also observed that small amounts of Mo and C at a ratio ≈ 1.25 (MoC to Mo₂C), are co-segregated to the MNSPs following the 29 weeks anneal. Note, other studies have shown these elements are depleted in the MNSPs in the AI condition at lower temperature⁸. Finally, we again note that the TEM-EDS results are qualitatively consistent with the 29 weeks APT data.

Cluster dynamics modeling. Figure 8 illustrates the complex physics of precipitate annealing at T_a much higher than in their nearly fully decomposed formation condition at lower temperatures in terms of the CD model predictions of critical radius (r_c) versus t_a compared to $\langle r \rangle$. The critical radius is $r_c = 2\gamma/\Delta G_v$, where γ is the MNSP interface energy and ΔG_v is the volumetric dissolved minus precipitate free energy difference for the matrix composition at t_a . Figure 6 shows that the $\langle r \rangle$ is initially far below r_c at 425 °C in the solute depleted matrix. However, the rapid re-solution of the Mn, Ni and Si, results in a corresponding rapid decrease in r_c with increasing t_a , while $\langle r \rangle$ increases following an initial dip. In this case the CD model predicts that the $\langle r \rangle$ and r_c curves cross at ≈ 5 weeks. At this point f begins to increase, initially by growth and subsequently by coarsening with decreasing N . The CD model predicts that the cross over occurs at $\langle r \rangle = r_c \approx 1.5$ nm. In other cases the intersection could be delayed in t_a and at a larger $\langle r \rangle = r_c$, while in other cases there would be no intersection at all, leading to full dissolution. This delicate interaction between $\langle r \rangle$ and r_c leads to the high sensitivity of $f(t_a)$ shown in Fig. 7. Thus it is useful to try to estimate actual r_c .

The histogram plot Fig. 9 shows that the APT N continuously decreases with t_a at all MNSP sizes except for $r > 2.25$ nm. Note, these N and corresponding f are highly uncertain at the long annealing times, since at most, only a few precipitates are observed in a given APT tip. While precise precipitate size distributions cannot be established, the APT results show that the largest MNSP survive and persist and slightly increase in numbers at longer t_a . Notably, no clusters with $r < 2.25$ nm were found in the 29 weeks condition. The largest MNSP in the AI condition was $r = 2.3$ nm, while the 3 precipitates found after the 29 weeks PIA all had $r > 2.6$ nm. The largest

MNSP in the AI condition had ≈ 4500 solute atoms, the 3 clusters found after the 29 weeks PIA contained 6500, 7200 and 8100 solute atoms, respectively. Thus the MNSP with $r > 2.25$ nm are not only stable, but appear to be growing, supporting the hypothesis that they are equilibrium phases. This interpretation of the APT results is consistent and supported by the EDS observations described previously, which showed a much larger number of coarsened MNSPs persist after annealing for 57 weeks in areas with sufficient Ni and Mn. Based on these results it appears that as parameterized the CD model $r_c \approx 1.5$ nm at the intersection with $\langle r \rangle$ underestimates the actual r_c which is closer to 2.3 nm. These results along with those in Fig. 8, suggest that at 425 °C the solvus boundary is larger than, for example, 1.5 at.% Ni and 1.0 at.% Mn and lower than 1.6 at.% Ni and 1.3 at.% Mn, since these compositions bracket the complete dissolution and overestimation of f , respectively.

The full dissolution in the medium Ni steel (LG) at 7 weeks demonstrates that 57 weeks t_a is far more than that needed to dissolve the MNSPs in the high Ni steel (CM6) if they are non-equilibrium solute clusters. The combination of APT results and CD model suggests that the significant reduction in the precipitate N is consistent with the nano-scale size of the MNSPs, which are predominantly below r_c at 425 °C in the initially solute depleted AI matrix. As the small MNSPs dissolve, the corresponding increase in the matrix solute concentration is sufficient to stabilize only the larger precipitates. The fact that MNSPs with $r > 2.3$ nm are stable in a matrix that is only slightly solute depleted ($\approx -0.11\%$) compared to the total solutes available in the AI condition, suggests that they are not induced by radiation, consistent with thermodynamic predictions, especially for much lower temperatures (see below). Thus, the overall CD predictions are qualitatively consistent with the observations, supporting the thermodynamic basis for the model and the interpretation of the PIA data. However, the CD model over predicts the number of stable precipitates that remain based on an independent (not fitted) γ_1 and ΔG_v , that underpredict r_c at 425 °C. Note, the PIA data could be used to fine-tune both precipitation and annealing models. However, such fitting is beyond the scope of this paper.

Finally, it is very important to return to the key question: *are the MNSPs stable, thermodynamic phases at a typical RPV service irradiation temperatures that are much lower than 425 °C?* This is clearly the case, since the CALPHAD ΔG_v is ≈ 4 times larger at 290 °C. Thus the corresponding r_c would be 0.54 nm, consistent, with the lower end of the observed MNSP size distribution in the AI condition.

Conclusions

PIA was used to investigate the character of MNSPs in neutron irradiated RPV steels. Annealing at 425 °C for long times, resulted in complete precipitate dissolution in a medium Ni (0.69%) steel after only 7 weeks, *consistent with thermodynamic predictions*. In contrast, some MNSPs still remained at the longest annealing time of 57 weeks in the high Ni (1.6%) steel, again qualitatively consistent with the CD model predictions. APT showed that the local regions with the highest precipitate stability contained at least 1.6 at.% Ni and 1.4 at.% Mn, although even in these regions a significant reduction in N and f were observed. However, the MNSP N with $r > 2.25$ nm coarsened slightly, while all the smaller precipitates dissolved at long t_a . This suggests that the critical radius r_c at 425 °C at the higher Ni and Mn contents is ≈ 2.3 nm. The number of Mn-Ni-Si atoms in the MNSPs found at 29 weeks averaged almost 50% higher than the largest cluster found in the AI condition, again indicating modest coarsening. Notably, the order of the t_a dependence of the increase in $\langle r \rangle$ and decrease in N is also consistent with classical diffusion controlled coarsening. Finally, TEM-EDS even more clearly showed stable precipitates in grains with sufficient Ni and Mn, even after annealing at 425 °C for 57 weeks, again strongly supporting the conclusion that MNSPs are a thermodynamically stable phase.

The $\langle r \rangle$, N and f predicted by unfitted CD model is only qualitatively consistent with the experimental APT trends. While the model accurately predicts the increases in $\langle r \rangle$, it overestimates the corresponding N and f . However, the model clearly reveals the basic PIA mechanism mediating the reduction in N and f is the large critical radius, r_c , at 425 °C in the initially AI solute depleted matrix. The precipitates smaller than r_c dissolve and re-enrich the matrix. Hence, $\langle r \rangle$ increases with t_a while r_c decreases and after they intersect some of the remaining larger precipitates subsequently continue grow and coarsen even at the higher temperature of 425 °C. The CD model over predictions of f can be traced to its independent parameterization that predicts an r_c that is smaller than that observed.

The key issue that is being addressed in this work is the thermodynamic stability of the MNSPs at much lower irradiation temperatures. Since ΔG_v is of order 4 times larger, and r_c is 4 times smaller, at 290 °C compared to 425 °C, there can be no question that MNSPs a stable thermodynamics phase at such service relevant temperatures. Notably, these conclusions are consistent with both CALPHAD thermodynamic predictions and XRD measurements^{21,27}.

Finally, we note that these results do not mean that solute (Mn-Ni-Si) segregation, including that driven by RIS, does not play a role in MNSP evolution at lower temperatures. Indeed they clearly do especially in the nucleation stage where these solutes segregate to small dislocation loops created in displacement cascades. Depending on the alloy composition, even if bulk MNSP phases (G and Γ_2) are thermodynamically stable, slow homogeneous nucleation rates may greatly limit precipitation. There are many APT observations of heterogeneous nucleation on loops, line dislocations and grain boundaries, especially at lower alloy solute contents and or higher irradiation temperatures. Indeed, RIS is the likely cause of solute cluster formation, widely identified as a generic G-phase, in highly sub saturated alloys^{6,40,47-49}.

Data Availability

The datasets generated during and/or analyzed during the current study are not publicly available due to proprietary reasons but are available from the corresponding author on reasonable request. The full data for all CM6 runs analyzed during this study is provided in the supplemental material.

References

1. Odette, G. R. & Nanstad, R. K. Predictive reactor pressure vessel steel irradiation embrittlement models: Issues and opportunities. *JOM* **61**, 17–23 (2009).
2. Eason, E. D., Odette, G. R., Nanstad, R. K. & Yamamoto, T. *A physically based correlation of irradiation-induced transition temperature shifts for RPV steels*. (Oak Ridge National Lab, 2007).
3. Eason, E. D., Odette, G. R., Nanstad, R. K. & Yamamoto, T. A physically-based correlation of irradiation-induced transition temperature shifts for RPV steels. *J. Nucl. Mater.* **433**, 240–254 (2013).
4. Odette, G. R. On the dominant mechanism of irradiation embrittlement of reactor pressure vessel steels. *Scr. Metall.* **17**, 1183–1188 (1983).
5. Odette, G. R. Radiation induced microstructural evolution in reactor pressure vessel steels. In *Materials Research Society Symposium - Proceedings* **373**, 137–148 (Materials Research Society, 1995).
6. Wells, P. B. *et al.* Evolution of manganese–nickel–silicon-dominated phases in highly irradiated reactor pressure vessel steels. *Acta Mater.* **80**, 205–219 (2014).
7. Miller, M. K., Sokolov, M. A., Nanstad, R. K. & Russell, K. F. APT characterization of high nickel RPV steels. *J. Nucl. Mater.* **351**, 187–196 (2006).
8. Miller, M. K. & Russell, K. F. Embrittlement of RPV steels: An atom probe tomography perspective. *J. Nucl. Mater.* **371**, 145–160 (2007).
9. Edmondson, P. D., Miller, M. K., Powers, K. A. & Nanstad, R. K. Atom probe tomography characterization of neutron irradiated surveillance samples from the R. E. Ginna reactor pressure vessel. *J. Nucl. Mater.* **470**, 147–154 (2016).
10. Styman, P. D. *et al.* Post-irradiation annealing of Ni–Mn–Si-enriched clusters in a neutron-irradiated RPV steel weld using Atom Probe Tomography. *J. Nucl. Mater.* **459**, 127–134 (2015).
11. Pareige, P., Van Duysen, J. C. & Auger, P. An APFIM study of the microstructure of a ferrite alloy after high fluence neutron irradiation. *Appl. Surf. Sci.* **67**, 342–347 (1993).
12. Wagner, A., Ulbricht, A., Bergner, F. & Altstadt, E. Influence of the copper impurity level on the irradiation response of reactor pressure vessel steels investigated by SANS. *Nucl. Instruments Methods Phys. Res. B* **280**, 98–102 (2012).
13. Takeuchi, T. *et al.* Effects of chemical composition and dose on microstructure evolution and hardening of neutron-irradiated reactor pressure vessel steels. *J. Nucl. Mater.* **402**, 93–101 (2010).
14. Meslin, E., Radiguet, B., Pareige, P., Toffolon, C. & Barbu, A. Irradiation-Induced Solute Clustering in a Low Nickel FeMnNi Ferritic Alloy. *Exp. Mech.* **51**, 1453–1458 (2011).
15. Meslin, E., Radiguet, B. & Loyer-Prost, M. Radiation-induced precipitation in a ferritic model alloy: An experimental and theoretical study. *Acta Mater.* **61**, 6246–6254 (2013).
16. Odette, G. R. & Lucas, G. E. Recent progress in understanding reactor pressure vessel steel embrittlement. *Radiat. Eff. Defects Solids* **144**, 189–231 (1998).
17. Liu, C. L., Odette, G. R., Wirth, B. D. & Lucas, G. E. A lattice Monte Carlo simulation of nanophase compositions and structures in irradiated pressure vessel Fe–Cu–Ni–Mn–Si steels. *Mater. Sci. Eng. A* **238**, 202–209 (1997).
18. Odette, G. R., Liu, C. L. & Wirth, B. D. On the Composition and Structure of Nanoprecipitates in Irradiated Pressure Vessel Steels. *Mater. Res. Soc. Symp. Proc.* **439**, 457–469 (1997).
19. Styman, P. D., Hyde, J. M. & Wilford, K. Morley, a. & Smith, G. D. W. Precipitation in long term thermally aged high copper, high nickel model RPV steel welds. *Prog. Nucl. Energy* **57**, 86–92 (2012).
20. Miller, M. K., Powers, K. A., Nanstad, R. K. & Efsing, P. Atom probe tomography characterizations of high nickel, low copper surveillance RPV welds irradiated to high fluences. *J. Nucl. Mater.* **437**, 107–115 (2013).
21. Ke, H. *et al.* Thermodynamic and kinetic modeling of Mn–Ni–Si precipitates in low-Cu reactor pressure vessel steels. *Acta Mater.* **138**, 10–26 (2017).
22. Ngayam-Happy, R., Becquart, C. S., Domain, C. & Malerba, L. Formation and evolution of MnNi clusters in neutron irradiated dilute Fe alloys modelled by a first principle-based AKMC method. *J. Nucl. Mater.* **426**, 198–207 (2012).
23. Ngayam-Happy, R., Becquart, C. S. & Domain, C. First principle-based AKMC modelling of the formation and medium-term evolution of point defect and solute-rich clusters in a neutron irradiated complex Fe–CuMnNiSiP alloy representative of reactor pressure vessel steels. *J. Nucl. Mater.* **440**, 143–152 (2013).
24. Bonny, G. *et al.* On the thermal stability of late blooming phases in reactor pressure vessel steels: An atomistic study. *J. Nucl. Mater.* **442**, 282–291 (2013).
25. Bonny, G., Terentyev, D., Zhurkin, E. E. & Malerba, L. Monte Carlo study of decorated dislocation loops in FeNiMnCu model alloys. *J. Nucl. Mater.* **452**, 486–492 (2014).
26. Xiong, W. *et al.* Thermodynamic models of low temperature Mn–Ni–Si precipitation in reactor pressure vessel steels. *Mater. Res. Soc. Commun.* **4**, 101–105 (2014).
27. Sprouster, D. J. *et al.* Structural characterization of nanoscale intermetallic precipitates in highly neutron irradiated reactor pressure vessel steels. *Scr. Mater.* **113**, 18–22 (2016).
28. Miller, M. K. *et al.* Evolution of the nanostructure of VVER-1000 RPV materials under neutron irradiation and post irradiation annealing. *J. Nucl. Mater.* **385**, 615–622 (2009).
29. Nielsen, J. W. *As-Run Physics Analysis for the UCSB-1 Experiment in the Advanced Test Reactor* (2015).
30. Odette, G. R. & Wirth, B. D. A computational microscopy study of nanostructural evolution in irradiated pressure vessel steels. *J. Nucl. Mater.* **251**, 157–171 (1997).
31. Odette, G. R., Yamamoto, T. & Klingensmith, D. On the effect of dose rate on irradiation hardening of RPV steels. *Philos. Mag.* **85**, 779–797 (2005).
32. Marquis, E. A. & Hyde, J. M. Applications of atom-probe tomography to the characterisation of solute behaviours. *Mater. Sci. Eng. R Reports* **69**, 37–62 (2010).
33. Larson, D. J., Gault, B., Geiser, B. P., De Geuser, F. & Vurpillot, F. Atom probe tomography spatial reconstruction: Status and directions. *Curr. Opin. Solid State Mater. Sci.* **17**, 236–247 (2013).
34. Miller, M. K. & Hetherington, M. G. Local magnification effects in the atom probe. *Surf. Sci.* **246**, 442–449 (1991).
35. Oberdorfer, C. & Schmitz, G. On the Field Evaporation Behavior of Dielectric Materials in Three-Dimensional Atom Probe: A Numeric Simulation. *Microsc. Microanal.* **17**, 15–25 (2010).
36. Beinke, D., Oberdorfer, C. & Schmitz, G. Towards an accurate volume reconstruction in atom probe tomography. *Ultramicroscopy* **165**, 34–41 (2016).
37. Cunningham, N. J. Study of the Structure, Composition, and Stability of Y-Ti-O nm-Scale Features. (University of California, Santa Barbara, 2012).
38. Andersson, J. O., Helander, T., Höglund, L., Shi, P. & Sundman, B. THERMO-CALC & DICTRA, Computational Tools For. *Materials Science*. **26**, 273–312 (2002).
39. Thermo-Calc Software TCAL2/Aluminum database version 2.
40. Ke, J. H., Ke, H., Odette, G. R. & Morgan, D. Cluster dynamics modeling of Mn–Ni–Si precipitates in ferritic-martensitic steel under irradiation. *J. Nucl. Mater.* **498**, 83–88 (2018).
41. Wen, Y. R. *et al.* Microstructure characterization of Cu-rich nanoprecipitates in a Fe – 2. 5. *Acta Mater.* **61**, 2133–2147 (2013).

42. Was, G. S., Hash, M. & Robert Odette, G. Hardening and microstructure evolution in proton-irradiated model and commercial pressure-vessel steels. *Phi* **85**, 703–722 (2005).
43. Hirano, K., Cohen, M. & Averbach, B. L. Diffusion of nickel into iron. *Acta Metall.* **9**, 440–445 (1961).
44. Ardell, A. J. On the coarsening of grain boundary precipitates. *Acta Metall.* **20**, 601–609 (1972).
45. Shu, S., Wells, P. B., Almirall, N., Odette, G. R. & Morgan, D. D. Acta Materialia Thermodynamics and kinetics of core-shell versus appendage co-precipitation morphologies: An example in the Fe-Cu-Mn-Ni-Si system. *Acta Mater.* **157**, 298–306 (2018).
46. Almirall, N. *et al.* Precipitation and Hardening in Irradiated Low Alloy Steels with a Wide Range of Ni and Mn Compositions. *Acta Mater.* Manuscript (2018).
47. Sun, W. W., Marceau, R. K. W., Styles, M. J., Barbier, D. & Hutchinson, C. R. G phase precipitation and strengthening in ultra-high strength ferritic steels: Towards lean 'maraging' metallurgy. *Acta Mater.* **130**, 28–46 (2017).
48. Chen, W. Y. *et al.* *In situ* TEM study of G-phase precipitates under heavy ion irradiation in CF8 cast austenitic stainless steel. *J. Nucl. Mater.* **464**, 185–192 (2015).
49. Matsukawa, Y. *et al.* The two-step nucleation of G-phase in ferrite. *Acta Mater.* **116**, 104–113 (2016).

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Author Contributions

P.W. originally drafted the main manuscript text, designed and carried out the annealing experiment, ran atom probe tomography (APT) tips and prepared figures 1–6, 8, 9. N.A. rewrote and revised the main manuscript, assisted the long term anneals, prepared figures 7 and contributed to the sample fabrication and APT data collection and analysis. G.R.O. was involved in and guided all aspects of the experimental and modeling from the inception, made major contributions to the analysis of the data and revisions of the manuscript. H.K. and D.M. carried out the thermodynamic and cluster dynamics modeling presented in this paper and figures 1, 5, 6, 8. P.E. assisted characterization by Scanning Transmission Electron Microscopy (STEM)-Energy Dispersive X-ray Spectroscopy (EDS). T.Y. carried out the irradiations editing the final manuscript. All authors reviewed the manuscript.

Additional Information

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