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A Quartic Spline Based on a Variational Approach

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Abstract. The C^2 continuous cubic spline can be viewed as the solution of a variational problem. The spline derived in this paper is obtained by solving a slightly different variational problem that depends on the input data. The goal is to obtain a spline that may have high second derivatives at the interpolated points and low second derivatives between two consecutive interpolated points. The solution is a C^2 continuous quartic spline.

Key words: Approximation, calculus of variation, interpolation, spline.

1. Introduction

Commonly, the C^2 continuous cubic spline interpolating the univariate data in $\{(x_i, F_i)|i=0,\ldots,n\}$, where $x_{i+1}>x_i$, $i=0,\ldots,(n-1)$, is derived using calculus of variation. The objective is to minimize an energy function, which has a piecewise cubic spline as solution. When dealing with parametric curves, one must interpolate the ordered points in $\{(x_i, y_i, z_i)|i=0,\ldots,n\}$ considering an associated knot sequence $\{u_0<\cdots< u_n\}$. Often, the solution of the univariate case is directly applied to the three coordinate functions of a parametric spline curve.

In the univariate case, the functional

$$\int (f''(x))^2 dx \tag{1.1}$$

is minimized on $[x_0, x_n]$. In this paper, this functional is modified slightly, which leads to a C^2 continuous quartic spline. The modification of the functional (1.1) is motivated by the fact that the cubic spline tends to "overshoot" in regions where the given data changes rapidly. In the context of shape preservation, one wants to obtain a spline without (or at least very small) "overshoots". Thus, a different variational problem must be solved. One objective is to create a spline, which differs very little from the polygon obtained by connecting consecutive original data points. Intuitively, a spline that satisfies this criterion has high second derivatives at the knots x_i and low second derivatives between two knots x_i and x_{i+1} . Another objective is to construct a spline curve that has a second derivative that closely approximates a given function that may be dependent on the input data. It is shown in the following section how these objectives can be achieved by adding a single term to the functional (1.1).

It is not possible to list all references dealing with tension splines, monotone splines, or other shape preserving splines. The derivation of the C^2 continuous quartic uses a similar paradigm. Some of the related shape preserving curve and surface

modeling concepts are discussed in [1,5-14, 16]. General references covering additional material include [3,4,15].

2. The Modified Variational Approach

behavior of the second derivative of an interpolant to the given data. Therefore, the points, it is proposed to subtract a polynomial o(x) from f''(x) appearing in the functional (1.1). It is assumed that the polynomial $\omega(x)$ reflects the "desired" function w(x) must be computed from a preprocessing step (Section 4) that depends In order to incorporate the "shape" of the polygon implied by the original data on the input data,

The quartic spline is derived for the univariate case. The minimization problem to be solved considers the space $L^2[x_0,x_n]$ of functions $f''(x)-\omega(x)$ that are squareintegrable on the interval [xo, x,]. The modified functional is

$$(f''(x) - \omega(x))^2 dx$$
, (2.1)

where $\omega(x)$ is a polynomial. Several methods for defining the polynomial $\omega(x)$ (for each interval [x, x,+1]) are discussed in Section 4. This polynomial reflects the "desired" second derivative of a shape preserving interpolant. A necessary condition for minimizing the expression (2.1) is given by Euler's equation (see [2]):

$$\frac{\partial G}{\partial f} - \frac{d}{dx} \left(\frac{\partial G}{\partial f'} \right) + \frac{d^2}{dx^3} \left(\frac{\partial G}{\partial f''} \right) - \frac{d^3}{dx^3} \left(\frac{\partial G}{\partial f'''} \right) + \dots = 0,$$
 (2.2)

where, G = G(f, f', f',) is the integrand of the integral in (2.1). Substituting the integrand of (2.1) into (2.2) yields the differential equation to be solved. The integrand in (2.1) is

$$G(f, f', f'') = (f'')^2 - 2\omega f'' + \omega^2,$$
 (2.3)

and the differential equation (2.2) becomes

$$\frac{\partial G}{\partial f} - \frac{d}{dx} \left(\frac{\partial G}{\partial f} \right) + \frac{d^2}{dx^2} \left(\frac{\partial G}{\partial f^*} \right) = \frac{d^3}{dx^2} (2f'' - 2\omega) = 2(f''' - \omega'') = 0,$$
 (2.4)

which is equivalent to

$$f^{m}(x) = \omega^{n}(x).$$
 (2.5)

Equation (2.5) implies that the polynomial $\omega(x)$ must be at least of degree two for This is the lowest-degree polynomial that yields a spline different from the cubic spline. If a parametric spline curve $c(u) = \{(x(u), y(u), z(u)) \text{ is computed, the univari-}$ ate approach is applied to the three coordinate functions. Examples will be given for $\omega'(x)$ not to vanish. Therefore, a quadratic polynomial $\omega(x)$ is used in the following. both the non-parametric and the parametric case.

A Quartic Spline Based on a Variational Approach

3. Computing the Quartic Spline Segments

In this section, it is assumed that a Co piecewise quadratic polynomial, denoted by $\omega_i(x)$, $x \in [x_i, x_{i+1}]$, is given. Integrating Eq. (2.5) implies that each spline segment is a quartic polynomial, which is written as

$$f_i(x) = \sum_{j=0}^{4} c_{i,j}(x - x_i)^{j}, x \in [x_0, x_{i+1}], i = 0,...,(n-1),$$
 (3.1)

Each quartic spline segment is determined by continuity conditions and the quadratic functions

$$\omega_i(x) = \sum_{l=0}^{2} \hat{c}_{i,l}(x - x_i)^l, \quad x \in [x_i, x_{i+1}], \quad i = 0, ..., (n - 1).$$
 (3.2)

Differentiating the quadratic functions (3.2), one obtains $\omega_i^*(x) = 2\bar{c}_{i,2}$. Using Eq. (2.5) yields the coefficients for the quartic terms of each spline segment:

$$c_{i,4} = \frac{1}{12} \tilde{c}_{i,3}, i = 0,...,(n-1).$$
 (3.3)

and C^2 continuity conditions. The quadratic polynomials $\omega_i(x)$ are required to be C^0 Continuity conditions are imposed on the quartic spline segments; these are C', C', continuous at the interior knots, i.e., $\omega_{i-1}(x_i) = \omega_i(x_i)$, i = 1, ..., (n-1). The continuity conditions for the spline segments are stated next.

The interpolation conditions imply

$$f_i(x_i) = c_{i,o} = F_{js}$$
 $i = 0, ..., (n-1),$ (3.4)

the conditions for Co continuity are

$$f_i(x_{t+1}) = f_{i+1}(x_{i+1}), i = 0,...,(n-2),$$
 (3.5)

the conditions for C1 continuity are

$$f_i(x_{i+1}) = f_{i+1}(x_{i+1}), i = 0,...,(n-2),$$
 (3.6)

and, finally, the C2 conditions are

$$f_i^{\nu}(x_{i+1}) = f_{i+1}^{\nu}(x_{i+1}), i = 0,...,(n-2),$$
 (3.7)

Defining $h_i = (x_{i+1} - x_i)$, Eq. (3.7) can be written as

$$c_{i,3} = \frac{1}{3h_i}(c_{i+1,3} - c_{i,2} - 6c_{i,4}h_i^2), \quad i = 0,...,(n-1),$$
 (3.8)

The coefficients cit, are derived from (3.5) and (3.8) as

$$c_{i,1} = \frac{1}{h_i}(c_{i+1,0} - c_{i,0}) - \frac{h_i}{3}(2c_{i,2} + c_{i+1,2}) + h_i^3c_{i,4}, \quad i = 0,...,(n-1),$$
 (3.9)

A Quartic Spline Based on a Variational Approach

A linear system of (n-1) equations and (n+1) unknowns is obtained for the coefficients ci., using (3.6). This linear system is given by

$$h_{t-1}c_{t-1,3} + 2(h_{t-1} + h_t)c_{t,3} + h_tc_{t+1,3}$$

$$= 3\left(\frac{1}{h_{t-1}}c_{t-1,6} - \left(\frac{1}{h_{t-1}} + \frac{1}{h_t}\right)c_{t,0} + \frac{1}{h_t}c_{t+1,0} + h_{t-1}^2c_{t-1,4} + h_t^2c_{t,4}\right),$$
 $i = 1, ..., (n-1), (3.10)$

Assuming that values for co., and c., are known (using some end conditions for the spline), this linear system can be written in matrix form as

$$\frac{1}{h_0}c_{0,0} - \left(\frac{1}{h_0} + \frac{1}{h_1}\right)c_{1,0} + \frac{1}{h_1}c_{2,0} + h_0^2c_{0,4} + h_1^2c_{1,4} - h_0c_{0,2}$$

$$\frac{1}{h_1}c_{1,0} - \left(\frac{1}{h_1} + \frac{1}{h_2}\right)c_{2,0} + \frac{1}{h_2}c_{3,0} + h_2^2c_{1,4} + h_2^2c_{2,4}$$

$$\vdots$$

$$\vdots$$

$$\frac{1}{h_{n-2}}c_{n-2,0} - \left(\frac{1}{h_{n-2}} + \frac{1}{h_{n-2}}\right)c_{n-2,0} + \frac{1}{h_{n-2}}c_{n-1,0} + h_{n-2,1}^2c_{n-2,4} + h_{n-2,1}^2c_{n-2,4}$$

coefficients c_{0,2} and c_{e,2} can be derived from a local polynomial approximation of the given data at the ends. Obviously, the linear system of equations with its The two underlined terms in the first and last row of the right hand side of 3.11) indicate that the end conditions for the spline determine those values. The symmetric, tridiagonal, and diagonally dominant matrix can be solved in linear

 $f_{\kappa-1}(x_n)$, and $h_0 = h_{\kappa}$ hold. These periodicity constraints imply a linear system of equations with a cyclic matrix given by If periodic (cyclic) interpolation of the given data is desired, end conditions need not to be specified, since the equations $f_0(x_0) = f_{n-1}(x_n)$, $f_0(x_0) = f_{n-1}(x_n)$, $f_0'(x_0) = f_0(x_0)$

Solving the linear system provides the coefficients c_{1,2}. The coefficients c_{1,3} and c_{1,1} are then computed using (3.8) and (3.9).

4. Choosing the Quadratic Functions $\omega_i(x)$

These weight functions should have exactly one zero in the interior of [x, x,+1], if The quadratic functions $\omega_i(x)$ are defined for each interval $[x_i, x_{i+1}], i = 0, ..., (n-1)$, it is the desire to force the final interpolant to have second derivative extrema at the enots and small second derivatives between knots. In order to define the quadratic interpolating second derivative estimates at x_e . They are C^0 continuous at the knots. polynomials $\omega_l(x)$, it is necessary to derive estimates for the second derivatives at all enots. Several possibilities can be used to obtain these estimates.

In order to compute the quadratic weight function $\omega_i(x)$, a quadratic polynomial $\eta(x)$ is computed that interpolates the three data in

$$\{(x_{i-1}, F_{i-1}), (x_i, F_i), (x_{i+1}, F_{i+1})\}, i = 1, ..., (n-1),$$
 (4.1)

Alternatively, a quartic polynomial r₂(x) is computed that interpolates the five data in

$$\{(x_{i-2},F_{i-2}),(x_{i-1},F_{i-1}),(x_0,F_i),(x_{i+1},F_{i+1}),(x_{i+2},F_{i+2})\}, i=2,...,(n-2), (4.2)$$

By differentiating these local approximants at $x = x_i$ one obtains values $q_i^*(x_i)$ (or $r_i^*(x_i)$. These values are used as second derivative estimates and are set equal to $\omega_{i-1}(x_i) = \omega_i(x_i)$, leaving one degree of freedom for defining the quadratic weight function. Obviously, special cure is required at the ends. The values of $q_i^*(x)(r_i^*(x))$ and $q'_{n-1}(x)(r'_{n-2}(x))$ are used to obtain estimates at the ends. This, of course, is no problem in the periodic case, since the data are repeated cyclically. The use of quartic polynomials $\tau_i(x)$ for second derivative estimation can be usd to generate a curve scheme with quartic precision. One approach is to define A Quartic Spline Based on a Variational Approach

 $\frac{1}{2}(r_i(\frac{1}{2}(x_i+x_{i+1}))+r_{i+1}(\frac{1}{2}(x_i+x_{i+1}))), i=2,...,(n-3).$ Special care is required $\omega_i(x)$ as the quadratic that interpolates the three values $r_i'(x_i)$, $r_{i+1}'(x_{i+1})$, and for the end intervals when computing $\omega_0(x)$, $\omega_1(x)$, $\omega_{n-2}(x)$, and $\omega_{n-1}(x)$ (nonperiodic case). A simple solution is the requirement $\omega_0(x) = \omega_1(x) = r_2'(x)$ and $\omega_{s-2}(x) = \omega_{s-1}(x) = r_{s-2}'(x)$.

enough" in certain cases and might lead to unwanted oscillations in the final spline if the data varies rapidly. For more local results, quadratic polynomials should be Forcing quartic precision is effective if the data varies smoothly. Unfortunately, using quartic polynomials for second derivative estimation might not be "local used for the estimation.

nomials $\omega_i(x)$ can be defined by specifying one more value for each interval. To generate a spline curve with small second derivative between the interpolated points. Having computed second derivative estimates at all knots, the quadratic polythe weight function is computed using the following case distinctions:

- If the estimates at x_f and x_{f+1} are both zero set \(\omega_f(x) = 0\).
- . If the estimate at one knot is zero, and the estimate at the other knot is positive (negative) let $\omega_i(x)$ be the quadratic polynomial, which has a double zero at the knot where it must interpolate the zero estimate.
 - If the estimates at both knots are greater (smaller) than zero let \(\omega_i(x)\) be the
- If the estimate at one knot is negative, and the estimate at the other knot is positive quadratic polynomial that has a double zero in the open interval (x, x, +1) force $\omega_i(x)$ to have a zero at $(x_i + x_{i+1})/2$.

One can introduce real-valued parameters at to scale the second derivative estimates if $\alpha_i = 1, i = 0, \dots, n$, the "standard" quartic spline is obtained. Scaling the estimates of the second derivatives at the knots using increasing positive scaling factors a, This justifies the view of these scaling factors as tension parameters. They can be at each knot x_i . Obviously, if $x_i = 0, i = 0, \dots, n$, the common cubic spline is obtained. generally produces splines which approach the polygon implied by the original data. used as an interactive shaping tool for the quartic spline.

Unfortunately, increasing these scaling factors beyond a certain threshold can lead to splines with unwanted inflection points or even "loops". It is not clear at this point how these factors must be chosen in order to get the most pleasing spline with maximum shape preservation. Once determined, the functions $\omega_i(x)$ define the coefficients $c_{i,k}$ according to (3.3). Examples of possible quadratic polynomials $\omega_i(x)$ are shown in Fig. I.

In the parametric case, the method presented is applied to the three coordinate functions x(u), y(u), and z(u) of the parametric spline curve c(u). Three different sets of quadratic polynomials \alpha_i(u) are generated, one for each coordinate.

5. Conversion to Bernstein-Bézier Representation

The C2 continuous quartic spline has been derived in monomial form. The transformation of a single polynomial f(x) to its corresponding Bernstein-Bézier representation is given by

(4)/0

Figure 1. Possible quadratic polynomials as (x)

$$f_l(x) = \sum_{j=0}^{4} c_{i,j}(x - x_j)^j = \sum_{j=0}^{4} b_{i,j}B_j^{\dagger}(x), \quad l = 0, ..., (n-1).$$
 (5.1)

Here, x varies in $[x_0, x_{i+1}]$, $b_{i,j}$ are the Bézier ordinates for a single spline segment, and $B_j^*(x)$, $j=0,\ldots,4$, are the quartic Bernstein-Bézier polynomials defined as

$$B_j^4(x) = \frac{1}{h_i^4} \left(\frac{4}{j}\right) (x_{i+1} - x)^{4-j} (x - x_i)^{j}, \quad i = 0, ..., (n-1).$$
 (5.2)

In matrix notation, the conversion between monomial and Bernstein-Bezier representation is written as

$$\begin{pmatrix} c_{i,0} & -c_{i,1}x_{i} & +c_{i,2}x_{i}^{2} & -c_{i,2}x_{i}^{3} & +c_{i,4}x_{i}^{4} \\ 0 & c_{i,1} & -2c_{i,2}x_{i} & +3c_{i,3}x_{i}^{2} & -4c_{i,4}x_{i}^{3} \\ 0 & 0 & c_{i,2} & -3c_{i,3}x_{i} & +6c_{i,4}x_{i}^{2} \\ 0 & 0 & 0 & c_{i,3} & -4c_{i,4}x_{i} \\ 0 & 0 & 0 & c_{i,3} & -4c_{i,4}x_{i} \\ 0 & 0 & 0 & c_{i,4} \end{pmatrix} = \frac{1}{h_{i}^{4}}$$

$$\begin{pmatrix} x_{i+1}^4 & -4x_i^2x_{i+1}^2 & 6x_i^2x_{i+1}^2 & -4x_i^2x_{i+1} & x_i^4 \\ -4x_{i+1}^4 & 4(3x_ix_{i+1}^2+x_{i+1}^2) & -12(x_i^2x_{i+1}+x_ix_{i+1}^2) & 4(x_i^2+3x_i^2x_{i+1}) & -4x_i^2 \\ 6x_{i+1}^2 & -12(x_ix_{i+1}+x_{i+1}^2) & 6(x_i^2+4x_ix_{i+1}+x_{i+1}^2) & -12(x_i^2+x_ix_{i+1}) & 6x_i^2 \\ -4x_{i+1} & 4(x_i+3x_{i+1}) & -12(x_i+x_{i+1}) & 4(3x_i+x_{i+1}) & -4x_i \\ 1 & -4 & 6 & -4 & 1 \end{pmatrix}$$

(bLo bLI bL2 bL3 bLA)". (5.3)

The Bézier ordinates b_{1,3} can be computed directly from (5.3). Alternatively, it is possible to directly derive the quartic spline in Bernstein-Bezier representation.

6. Computing Biquartic Tensor Product Splines

In order to construct a tensor product surface method based on quartic splines, a set of cardinal basis functions is defined, where the quadratic weight functions depend on "cardinal data." More precisely, define the basis function $g_i(x)$ as the quartic spline interpolant that is zero at every knot except at x_i , where it is one. Thus, a C^2 continuous quartic spline can be written in cardinal form as

$$f(x) = \sum_{i=0}^{n} F_{i\beta_i}(x),$$
 (6.1)

where the functions $g_i(x)$, i=0,...,n, are C^2 continuous quartic cardinal splines satisfying $g_i(x_i)=\delta_{i,i}$ (Kronecker delta). This linear combination interpolates the data, but it can be different from the method described earlier, where the quadratic weight functions depended on the given data. Using the cardinal form (6.1), the weight functions depend on the data $(x_i, \delta_{i,k})$. Using the concept of cardinal spline bases, a C2 continuous biquartic tensor product spline is written as

$$f(x, y) = \sum_{j=0}^{n} \sum_{i=0}^{m} F_{i,j}q_i(x)h_j(y)$$
 (6.2)

interpolating the data in $\{(x_0, y_p F_{i,j})|x_{i+1} > x_0 y_{j+1} > y_p i = 0, ..., m, j = 0, ..., n\}$. Again, the basis functions $g_i(x)$ and $h_j(y)$ satisfy the conditions $g_i(x_k) = \delta_{i,k}$ and $h_j(y)$ satisfy the conditions $g_i(x_k) = \delta_{i,k}$ and $h_j(y) = \delta_{j,k}$. Both cardinal spline bases are computed using the univariate scheme.

In the parametric case, an interpolating parametric tensor product surface in three-dimensional space is written in cardinal form as

$$\mathbf{s}(u, v) = \sum_{j=0}^{n} \sum_{i=0}^{\infty} x_{i,j} g_{i}(u) h_{j}(v),$$
 (6.3)

where $x_{i,j} = (x_{i,p}, y_{i,p}, z_{i,p})$ is an interpolated point, and $g_i(u)$ and $h_i(v)$ are cardinal basis functions. Two increasing knot sequences are required in the parametric case, $\{u_0 < \cdots < u_m\}$ and $\{v_0 < \cdots < v_n\}$. A C^2 continuous quartic cardinal spline basis is shown in Fig. 2 using periodic end conditions, quadratic functions $\omega_i(x)$ for second derivative estimation, and tension parameters $\alpha_i = 1$.

7. Examples

The following examples demonstrate the new method for non-parametric and parametric cases. Figures 3 and 4 show C^2 continuous quartic splines/parametric spline curves obtained by increasing tension parameters α_i . The tension parameters used in Fig. 3 are 0 (= cubic spline, upper-left), 5 (upper-right), 10 (lower-left), and 15 (lower-right). For a particular spline/parametric spline curve, the tension parameters are the same at all knots. The second derivative estimates at the interior knots are based on local quadratic approximants q_i . In the non-periodic case, second derivative estimates at the end knots are zero, and natural end conditions are used



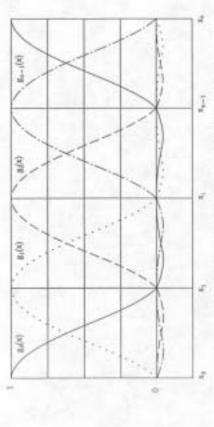


Figure 2. Cardinal spline basis functions using periodic and condition

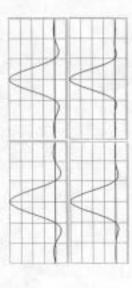


Figure 3. Quartic splines interpolating same data using increasing tension

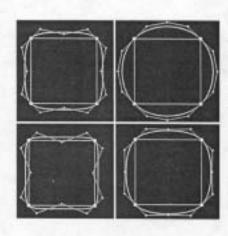


Figure 4. Quartic parametric spline curves interpoluting same data using increasing tension

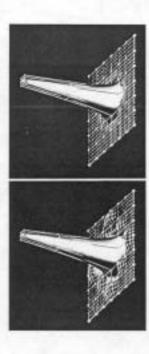


Figure 5. Product of two cubic and two quartic cardinal splines

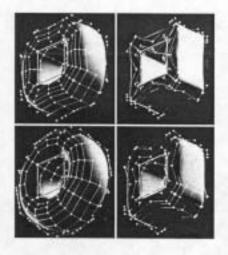


Figure 6. Modeling torus using increasing tension

for computing the quartic spline. Fig. 4 shows a periodic parametric quartic spline The tension parameters used in Fig. 4 are 0 (= cubic spline, upper-left), 2.2 (uppercurve and its Bezier control polygon; the parametrization is based on chord length. right), 4.4 (lower-left), and 6.6 (lower-right).

cardinal splines g₃(x) and h₃(y). The tension parameters applied in x- and y-direction The next three examples show biquartic splines/parametric spline surfaces. Figure 5 shows the piecewise bicubic function (left)/piecewise biquartic function (right) defined as the product $f(x, y) = 6g_3(x)h_3(y)$ of the two cubic (left)/two quartic (right) Figures 6 and 7 show the use of the method for interactively modeling parametric surfaces. The tension parameters used in Fig. 6 are 0 (= bicubic spline surface, upper-left), 6 (upper-right), 12 (lower-left), and 18 (lower-right). The tension parameters used in Fig. 7 are 0 (= bicubic spline surface, upper-left), 10 (upper-right), 15 are 12 in the biquartic case. The knots are $x_i = i$, i = 0, ..., 6, and $y_j = j = 0, ..., 6$. lower-left), and 20 (lower-right). All parametrizations are based on average chord

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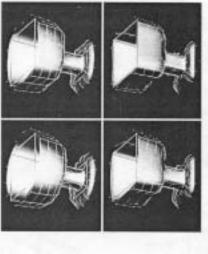


Figure 7. Modeling goblet using increasing tension

length, the same tension is applied in both parameter directions, and the associated Bezier control nets are shown.

8. Conclusions

This scaling parameter can be used to achieve interpolating curves of different shape with high second derivatives at the interpolated points. Since the quadratic poly-A C2 continuous quartic spline based on a minimization problem has been used as an interactive design tool by scaling second derivative estimates at the knots. nomials w, depend on the knots, it is investigated how the quartic spline reacts to introduced. The spline is an alternative to the cubic spline. The quartic spline can be changes in the parametrization.

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