

Lawrence Berkeley National Laboratory

Recent Work

Title

X-RAY DIFFRACTION REFINEMENT OF THE CALCIUM TUNGSTATE STRUCTURE

Permalink

<https://escholarship.org/uc/item/7mp8m04j>

Authors

Zalkin, A.

Templeton, D.H.

Publication Date

1963-07-01

University of California
Ernest O. Lawrence
Radiation Laboratory

**X-RAY DIFFRACTION REFINEMENT OF THE
CALCIUM TUNGSTATE STRUCTURE**

TWO-WEEK LOAN COPY

*This is a Library Circulating Copy
which may be borrowed for two weeks.
For a personal retention copy, call
Tech. Info. Division, Ext. 5545*

DISCLAIMER

This document was prepared as an account of work sponsored by the United States Government. While this document is believed to contain correct information, neither the United States Government nor any agency thereof, nor the Regents of the University of California, nor any of their employees, makes any warranty, express or implied, or assumes any legal responsibility for the accuracy, completeness, or usefulness of any information, apparatus, product, or process disclosed, or represents that its use would not infringe privately owned rights. Reference herein to any specific commercial product, process, or service by its trade name, trademark, manufacturer, or otherwise, does not necessarily constitute or imply its endorsement, recommendation, or favoring by the United States Government or any agency thereof, or the Regents of the University of California. The views and opinions of authors expressed herein do not necessarily state or reflect those of the United States Government or any agency thereof or the Regents of the University of California.

UNIVERSITY OF CALIFORNIA
Lawrence Radiation Laboratory
Berkeley, California
Contract No. W-7405-eng-48

X-RAY DIFFRACTION REFINEMENT OF THE CALCIUM
TUNGSTATE STRUCTURE

A. Zalkin and D. H. Templeton

July, 1963

X-ray Diffraction Refinement of the Calcium Tungstate Structure

Allan Zalkin and David H. Templeton

Lawrence Radiation Laboratory and Department of Chemistry,

University of California, Berkeley, California

The crystal structure of CaWO_4 (scheelite) has been refined with single-crystal x-ray diffraction data. For the tetragonal cell $a = 5.243 \pm 0.002$, $c = 11.376 \pm 0.003$ Å. Oxygen coordinates 0.1504, 0.0085, 0.2111 correspond to Ca—O distances 2.44 and 2.48 Å and W—O distances 1.78 Å.

INTRODUCTION

We became interested in the crystal structure of calcium tungstate (scheelite) because we wished to compare it with the closely-related structure of europium tungstate which we recently determined.¹ The scheelite structure was investigated by Sillén and Nylander² who reviewed earlier work and determined oxygen coordinates from considerations of shape and size. They confirmed this structure with a limited amount of x-ray data. We have refined this structure with more precise x-ray diffraction data to obtain oxygen coordinates which agree with those of Sillén and Nylander within the accuracy which they claimed. A recent study by neutron diffraction³ is in excellent agreement with our results for both coordinates and thermal parameters.

EXPERIMENTAL

We used a large triply-pulled single crystal of synthetic CaWO_4 which was grown by Dr. Kurt Nassau at the Bell Telephone Laboratory. A trapezoidal fragment was chipped from the large boule; it was roughly a parallelepiped of dimensions $0.015 \times 0.035 \times 0.11$ mm. It was mounted on a goniometer head with the long dimension (the $[110]$ direction) as the axis of rotation. Measurements were made with a General Electric XRD-5 goniostat, scintillation counter, and Mo x-ray tube ($\lambda = 0.70926 \text{ \AA}$ for $\text{K}\alpha_1$). Intensities were measured for 828 independent reflections permitted by the space group ($2\theta < 100^\circ$), 163 of which were recorded as zero. Each was counted for 20 sec. The most intense reflection, (112), was 1000 counts/sec. The smallest increment recorded by the scaler was 0.5 counts/sec. Background at the larger angles was 0.5 to 1.0 counts/sec.

We estimate the linear absorption coefficient as 405 cm^{-1} for MoK α radiation. Absorption corrections were calculated by a numerical integration for a rectangular prism which approximated the shape of the crystal. These factors ranged from 1.8 to 2.7 and were checked by the angular variation of intensities with ϕ for reflections with χ equal 90° . The intensities were corrected by an empirical function for the alpha-doublet separation, which was complete for the higher angles. A correction for extinction was made with an empirical factor $2500/(2500 - I)$, where I is the observed intensity in counts/sec. This correction had an insignificant effect on most of the intensities, but increased the strongest by a factor 1.7.

Atomic scattering factors for Ca^{+2} and neutral O and W were taken from International Tables,⁴ Table 3.3.1A. The values for O were increased slightly below $\sin\theta/\lambda = 0.2$ to approximate a charge state of $-\frac{1}{2}$. Values for the dispersion correction $\Delta f'$ were taken from Table 3.3.2C.⁴ The correction $\Delta f''$ was taken as 0.4 for Ca and 7.5 for W.

We minimized the function $\sum w(|F_o| - |F_c|)^2 / \sum w F_o^2$ with a least-squares program⁵ which we modified to include the effect of the imaginary dispersion correction in the calculation of $|F_c|$. Each reflection was given unit weight. Atoms were given anisotropic temperature factors of the form $\exp(-\beta_{11}h^2 - \beta_{22}k^2 - \beta_{33}l^2 - 2\beta_{12}hk - 2\beta_{13}hl - 2\beta_{23}kl)$, with suitable constraints for the Ca and W atoms. Refinement was continued until no parameter changed in the sixth decimal place. $R = \sum ||F_o| - |F_c|| / \sum |F_o|$ was reduced to 0.061. The final observed and calculated structure factors are listed in Table I.

RESULTS

The space group is $\underline{I}4_1/a$. For the body-centered cell we find, with the synthetic CaWO_4 :

$$\underline{a} = 5.243 \pm 0.002, \quad \underline{c} = 11.376 \pm 0.003 \text{ \AA}.$$

These values are in good agreement with those of Swanson et al.⁶ who report 5.242 and 11.372 from powder data. We compared powder photographs (CuK α radiation) of our synthetic CaWO₄ and of a sample of natural scheelite. No difference in cell dimensions could be detected, also in agreement with Swanson et al.⁶

There are two distinct ways in which the axial system may be oriented with respect to the structure; one is changed to the other by interchange of the a and b axes (and reversal of c if one wishes to preserve the handedness of the axes). The orientation of a particular specimen which corresponds to our oxygen coordinates may be determined by comparison of the intensities: (121) weaker than (211), (123) stronger than (213).. In our calculations the correct orientation was determined by trial and error.

The parameters and standard deviations determined by least squares are listed in Table II together with the neutron-diffraction results of Kay, Frazer and Almodovar.³ The coordinates agree more closely than the claimed accuracy, and the thermal parameters differ at most by little more than the sum of the two standard deviations. This concordance is gratifying evidence of the accuracy of both methods. These results are stated with the origin at the center of symmetry. If the origin is placed at a tungsten atom, our coordinates for oxygen can be chosen as 0.2415, 0.1504, 0.0861 to conform with the setting used by Sillén and Nylander.²

The structure is shown in Fig. 1. The interatomic distances less than 3.7 Å are listed in Table III. Calcium has 8 oxygen neighbors at an average distance of 2.46 Å. The WO₄ group is nearly regular tetrahedral with O—W—O angles 107.5° (4 times) and 113.4° (2 times). These distortions from a regular tetrahedron are not much outside our limits of error, but are confirmed very precisely by the neutron diffraction results. The

W—O bond distance 1.784 Å becomes 1.789 Å when corrected for thermal motion with the assumption that O rides on W. The fact that the tetrahedron is not regular is consistent with the much larger distortions observed in $\text{Eu}_2(\text{WO}_4)_3$ in which the environment is less symmetrical.¹ In the latter structure, the nearest-neighbor W—O distances average 1.74 and 1.78 Å for two kinds of W atoms.

We thank Prof. A. Pabst for giving us some crystals of scheelite and Dr. M. P. Klein for giving us the synthetic crystal.

References

- *Work done under the auspices of the U. S. Atomic Energy Commission.
- ¹D. H. Templeton and A. Zalkin, *Acta Cryst.* (in press)
- ²L. G. Sillén and A.-L. Nylander, *Arkiv Kemi Mineral. Geol.* 17A, No. 4 (1943).
- ³M. I. Kay, B. C. Frazer and I. Almodovar (private communication)
- ⁴International Tables for X-ray Crystallography (Kynoch Press, Birmingham, 1962) Vol. III, pp. 202-216.
- ⁵P. K. Gantzel, R. A. Sparks and K. N. Trueblood, private communication.
- ⁶H. E. Swanson, N. T. Gilfrich and M. I. Cook, *Natl. Bur. Standards U. S. Circ. No. 539*, 6, 23 (1956).

Table I. Observed structure factor magnitudes (FOB) and calculated structure factors (FCA).

(table to be reproduced photographically)

M ₀ K = 0.0 L FCB FCA 4 240-252 8 210 103 12 206-106 16 120 110 20 84-86 24 74 69	7 52 -51 9 65 60 11 52 50 13 42 -42 15 46 -43 17 32 32 19 33 26	M ₀ K = 0.8 L FCB FCA 0 126 121 2 0 -3 4 106-105 6 0 -0 8 94 95 10 0 2 12 91 -66 14 0 2 16 72 63	16 0 1 L FCB FCA 1 175-154 3 163-151 5 110 100 7 105 79 9 117 -99 11 95 -99 13 82 74 15 71 65 17 49 -88 19 46 -40 21 44 40 23 36 33	M ₀ K = 0.9 L FCB FCA 1 48 -49 3 46 -43 5 49 47 7 46 46 9 24 -37 11 26 -37 13 27 35 15 0 -2 17 215-210 19 10 9 21 149 143 23 0 7	M ₀ K = 0.10 L FCB FCA 0 71 -72 2 0 1 4 83 81 6 0 1 8 80 -72 10 0 -1	M ₀ K = 0.11 L FCB FCA 1 37 32 3 37 34 5 45 -35 7 49 49 9 31 50 11 37 -38 13 35 -35 15 42 -39 17 38 31 19 184-186 21 11 5 23 14 145 141	M ₀ K = 0.1 L FCB FCA 0 126 121 2 0 -3 4 106-105 6 0 -0 8 94 95 10 0 2 12 91 -66 14 0 2 16 72 63	M ₀ K = 0.2 L FCB FCA 0 215-240 2 31 -25 4 255 203 6 0 -2 8 215-210 10 10 9 12 149 143 14 0 7 16 135-126 18 0 1 20 85 86 22 0 -2 24 54 -55	M ₀ K = 0.3 L FCB FCA 1 112 104 3 106 82 5 135-117 7 121-108 9 83 74 11 78 69 13 68 -64 15 62 -54 17 62 55 19 43 46 21 30 -30 23 26 -26	M ₀ K = 0.4 L FCB FCA 0 204 209 2 34 -32 4 192-194 6 0 -3 8 175 171 10 16 16 12 137-138 14 0 14 16 102 103 18 0 3 20 77 -76 22 0 -5	M ₀ K = 0.5 L FCB FCA 1 96 -92 3 90 -84 5 82 81 7 77 77 9 74 -69 11 69 -65 13 61 57 15 45 46 17 40 -41 19 36 -37 21 38 31	M ₀ K = 0.6 L FCB FCA 0 157-157 2 21 -17 4 154 151 6 0 -2 8 137-133 10 0 11 12 114 108 14 15 10 16 84 -85 18 0 2 20 72 64	M ₀ K = 0.7 L FCB FCA 1 70 65 3 76 73 5 60 -56	M ₀ K = 1.5 L FCB FCA 2 182-193 4 0 -1 6 143 139 8 0 -1 10 149-148 12 0 0 14 117 110 16 0 1 18 71 -71 20 0 0	M ₀ K = 1.6 L FCB FCA 1 85 -82 3 69 67 5 74 72 7 73 -68 9 57 -57 11 59 59 13 57 52 15 36 -39 17 39 -38 19 33 34	M ₀ K = 1.7 L FCB FCA 2 129 127 4 0 4 6 132-130 8 0 4 10 101 99 12 0 1 14 85 -83 16 0 -2 18 74 69	M ₀ K = 1.8 L FCB FCA 1 54 50 3 64 -60 5 56 -53 7 49 49 9 31 50 11 37 -38 13 35 -35 15 42 -39 17 38 31 19 184-186 21 11 5 23 14 145 141	M ₀ K = 1.9 L FCB FCA 0 150-148 2 15 12 4 140 144 6 0 2 8 128-128 10 0 -7 12 109 103 14 0 -8 16 80 -82 18 0 -3 20 63 62	M ₀ K = 2.0 L FCB FCA 1 70 65 3 61 61 5 71 -68 7 67 -64 9 49 49 11 40 41 13 40 -38 15 39 -38 17 38 38	M ₀ K = 2.1 L FCB FCA 2 101 109 4 0 1 6 132-130 8 0 4 10 101 99 12 0 1 14 85 -83 16 0 -2 18 74 69	M ₀ K = 2.2 L FCB FCA 1 57 56 3 61 61 5 71 -68 7 67 -64 9 49 49 11 40 41 13 40 -38 15 39 -38 17 38 38	M ₀ K = 2.3 L FCB FCA 2 101 109 4 0 1 6 132-130 8 0 4 10 101 99 12 0 1 14 85 -83 16 0 -2 18 74 69	M ₀ K = 2.4 L FCB FCA 1 57 56 3 61 61 5 71 -68 7 67 -64 9 49 49 11 40 41 13 40 -38 15 39 -38 17 38 38	M ₀ K = 2.5 L FCB FCA 2 101 109 4 0 1 6 132-130 8 0 4 10 101 99 12 0 1 14 85 -83 16 0 -2 18 74 69	M ₀ K = 2.6 L FCB FCA 1 57 56 3 61 61 5 71 -68 7 67 -64 9 49 49 11 40 41 13 40 -38 15 39 -38 17 38 38	M ₀ K = 2.7 L FCB FCA 2 101 109 4 0 1 6 132-130 8 0 4 10 101 99 12 0 1 14 85 -83 16 0 -2 18 74 69	M ₀ K = 2.8 L FCB FCA 1 57 56 3 61 61 5 71 -68 7 67 -64 9 49 49 11 40 41 13 40 -38 15 39 -38 17 38 38	M ₀ K = 2.9 L FCB FCA 2 101 109 4 0 1 6 132-130 8 0 4 10 101 99 12 0 1 14 85 -83 16 0 -2 18 74 69	M ₀ K = 3.0 L FCB FCA 1 57 56 3 61 61 5 71 -68 7 67 -64 9 49 49 11 40 41 13 40 -38 15 39 -38 17 38 38	M ₀ K = 3.1 L FCB FCA 2 101 109 4 0 1 6 132-130 8 0 4 10 101 99 12 0 1 14 85 -83 16 0 -2 18 74 69	M ₀ K = 3.2 L FCB FCA 1 57 56 3 61 61 5 71 -68 7 67 -64 9 49 49 11 40 41 13 40 -38 15 39 -38 17 38 38	M ₀ K = 3.3 L FCB FCA 2 101 109 4 0 1 6 132-130 8 0 4 10 101 99 12 0 1 14 85 -83 16 0 -2 18 74 69	M ₀ K = 3.4 L FCB FCA 1 57 56 3 61 61 5 71 -68 7 67 -64 9 49 49 11 40 41 13 40 -38 15 39 -38 17 38 38	M ₀ K = 3.5 L FCB FCA 2 101 109 4 0 1 6 132-130 8 0 4 10 101 99 12 0 1 14 85 -83 16 0 -2 18 74 69	M ₀ K = 3.6 L FCB FCA 1 57 56 3 61 61 5 71 -68 7 67 -64 9 49 49 11 40 41 13 40 -38 15 39 -38 17 38 38	M ₀ K = 3.7 L FCB FCA 2 101 109 4 0 1 6 132-130 8 0 4 10 101 99 12 0 1 14 85 -83 16 0 -2 18 74 69	M ₀ K = 3.8 L FCB FCA 1 57 56 3 61 61 5 71 -68 7 67 -64 9 49 49 11 40 41 13 40 -38 15 39 -38 17 38 38	M ₀ K = 3.9 L FCB FCA 2 101 109 4 0 1 6 132-130 8 0 4 10 101 99 12 0 1 14 85 -83 16 0 -2 18 74 69	M ₀ K = 4.0 L FCB FCA 1 57 56 3 61 61 5 71 -68 7 67 -64 9 49 49 11 40 41 13 40 -38 15 39 -38 17 38 38	M ₀ K = 4.1 L FCB FCA 2 101 109 4 0 1 6 132-130 8 0 4 10 101 99 12 0 1 14 85 -83 16 0 -2 18 74 69	M ₀ K = 4.2 L FCB FCA 1 57 56 3 61 61 5 71 -68 7 67 -64 9 49 49 11 40 41 13 40 -38 15 39 -38 17 38 38	M ₀ K = 4.3 L FCB FCA 2 101 109 4 0 1 6 132-130 8 0 4 10 101 99 12 0 1 14 85 -83 16 0 -2 18 74 69	M ₀ K = 4.4 L FCB FCA 1 57 56 3 61 61 5 71 -68 7 67 -64 9 49 49 11 40 41 13 40 -38 15 39 -38 17 38 38	M ₀ K = 4.5 L FCB FCA 2 101 109 4 0 1 6 132-130 8 0 4 10 101 99 12 0 1 14 85 -83 16 0 -2 18 74 69	M ₀ K = 4.6 L FCB FCA 1 57 56 3 61 61 5 71 -68 7 67 -64 9 49 49 11 40 41 13 40 -38 15 39 -38 17 38 38	M ₀ K = 4.7 L FCB FCA 2 101 109 4 0 1 6 132-130 8 0 4 10 101 99 12 0 1 14 85 -83 16 0 -2 18 74 69	M ₀ K = 4.8 L FCB FCA 1 57 56 3 61 61 5 71 -68 7 67 -64 9 49 49 11 40 41 13 40 -38 15 39 -38 17 38 38	M ₀ K = 4.9 L FCB FCA 2 101 109 4 0 1 6 132-130 8 0 4 10 101 99 12 0 1 14 85 -83 16 0 -2 18 74 69	M ₀ K = 5.0 L FCB FCA 1 57 56 3 61 61 5 71 -68 7 67 -64 9 49 49 11 40 41 13 40 -38 15 39 -38 17 38 38	M ₀ K = 5.1 L FCB FCA 2 101 109 4 0 1 6 132-130 8 0 4 10 101 99 12 0 1 14 85 -83 16 0 -2 18 74 69	M ₀ K = 5.2 L FCB FCA 1 57 56 3 61 61 5 71 -68 7 67 -64 9 49 49 11 40 41 13 40 -38 15 39 -38 17 38 38	M ₀ K = 5.3 L FCB FCA 2 101 109 4 0 1 6 132-130 8 0 4 10 101 99 12 0 1 14 85 -83 16 0 -2 18 74 69	M ₀ K = 5.4 L FCB FCA 1 57 56 3 61 61 5 71 -68 7 67 -64 9 49 49 11 40 41 13 40 -38 15 39 -38 17 38 38	M ₀ K = 5.5 L FCB FCA 2 101 109 4 0 1 6 132-130 8 0 4 10 101 99 12 0 1 14 85 -83 16 0 -2 18 74 69	M ₀ K = 5.6 L FCB FCA 1 57 56 3 61 61 5 71 -68 7 67 -64 9 49 49 11 40 41 13 40 -38 15 39 -38 17 38 38	M ₀ K = 5.7 L FCB FCA 2 101 109 4 0 1 6 132-130 8 0 4 10 101 99 12 0 1 14 85 -83 16 0 -2 18 74 69	M ₀ K = 5.8 L FCB FCA 1 57 56 3 61 61 5 71 -68 7 67 -64 9 49 49 11 40 41 13 40 -38 15 39 -38 17 38 38	M ₀ K = 5.9 L FCB FCA 2 101 109 4 0 1 6 132-130 8 0 4 10 101 99 12 0 1 14 85 -83 16 0 -2 18 74 69	M ₀ K = 6.0 L FCB FCA 1 57 56 3 61 61 5 71 -68 7 67 -64 9 49 49 11 40 41 13 40 -38 15 39 -38 17 38 38	M ₀ K = 6.1 L FCB FCA 2 101 109 4 0 1 6 132-130 8 0 4 10 101 99 12 0 1 14 85 -83 16 0 -2 18 74 69	M ₀ K = 6.2 L FCB FCA 1 57 56 3 61 61 5 71 -68 7 67 -64 9 49 49 11 40 41 13 40 -38 15 39 -38 17 38 38	M ₀ K = 6.3 L FCB FCA 2 101 109 4 0 1 6 132-130 8 0 4 10 101 99 12 0 1 14 85 -83 16 0 -2 18 74 69	M ₀ K = 6.4 L FCB FCA 1 57 56 3 61 61 5 71 -68 7 67 -64 9 49 49 11 40 41 13 40 -38 15 39 -38 17 38 38	M ₀ K = 6.5 L FCB FCA 2 101 109 4 0 1 6 132-130 8 0 4 10 101 99 12 0 1 14 85 -83 16 0 -2 18 74 69	M ₀ K = 6.6 L FCB FCA 1 57 56 3 61 61 5 71 -68 7 67 -64 9 49 49 11 40 41 13 40 -38 15 39 -38 17 38 38	M ₀ K = 6.7 L FCB FCA 2 101 109 4 0 1 6 132-130 8 0 4 10 101 99 12 0 1 14 85 -83 16 0 -2 18 74 69	M ₀ K = 6.8 L FCB FCA 1 57 56 3 61 61 5 71 -68 7 67 -64 9 49 49 11 40 41 13 40 -38 15 39 -38 17 38 38	M ₀ K = 6.9 L FCB FCA 2 101 109 4 0 1 6 132-130 8 0 4 10 101 99 12 0 1 14 85 -83 16 0 -2 18 74 69	M ₀ K = 7.0 L FCB FCA 1 57 56 3 61 61 5 71 -68 7 67 -64 9 49 49 11 40 41 13 40 -38 15 39 -38 17 38 38	M ₀ K = 7.1 L FCB FCA 2 101 109 4 0 1 6 132-130 8 0 4 10 101 99 12 0 1 14 85 -83 16 0 -2 18 74 69	M ₀ K = 7.2 L FCB FCA 1 57 56 3 61 61 5 71 -68 7 67 -64 9 49 49 11 40 41 13 40 -38 15 39 -38 17 38 38	M ₀ K = 7.3 L FCB FCA 2 101 109 4 0 1 6 132-130 8 0 4 10 101 99 12 0 1 14 85 -83 16 0 -2 18 74 69	M ₀ K = 7.4 L FCB FCA 1 57 56 3 61 61 5 71 -68 7 67 -64 9 49 49 11 40 41 13 40 -38 15 39 -38 17 38 38	M ₀ K = 7.5 L FCB FCA 2 101 109 4 0 1 6 132-130 8 0 4 10 101 99 12 0 1 14 85 -83 16 0 -2 18 74 69	M ₀ K = 7.6 L FCB FCA 1 57 56 3 61 61 5 71 -68 7 67 -64 9 49 49 11 40 41 13 40 -38 15 39 -38 17 38 38	M ₀ K = 7.7 L FCB FCA 2 101 109 4 0 1 6 132-130 8 0 4 10 101 99 12 0 1 14 85 -83 16 0 -2 18 74 69	M ₀ K = 7.8 L FCB FCA 1 57 56 3 61 61 5 71 -68 7 67 -64 9 49 49 11 40 41 13 40 -38 15 39 -38 17 38 38	M ₀ K = 7.9 L FCB FCA 2 101 109 4 0 1 6 132-130 8 0 4 10 101 99 12 0 1 14 85 -83 16 0 -2 18 74 69	M ₀ K = 8.0 L FCB FCA 1 57 56 3 61 61 5 71 -68 7 67 -64 9 49 49 11 40 41 13 40 -38 15 39 -38 17 38 38	M ₀ K = 8.1 L FCB FCA 2 101 109 4 0 1 6 132-130 8 0 4 10 101 99 12 0 1 14 85 -83 16 0 -2 18 74 69	M ₀ K = 8.2 L FCB FCA 1 57 56 3 61 61 5 71 -68 7 67 -64 9 49 49 11 40 41 13 40 -38 15 39 -38 17 38 38	M ₀ K = 8.3 L FCB FCA 2 101 109 4 0 1 6 132-130 8 0 4 10 101 99 12 0 1 14 85 -83 16 0 -2 18 74 69	M ₀ K = 8.4 L FCB FCA 1 57 56 3 61 61 5 71 -68 7 67 -64 9 49 49 11 40 41 13 40 -38 15 39 -38 17 38 38	M ₀ K = 8.5 L FCB FCA 2 101 109 4 0 1 6 132-130 8 0 4 10 101 99 12 0 1 14 85 -83 16 0 -2 18 74 69	M ₀ K = 8.6 L FCB FCA 1 57 56 3 61 61 5 71 -68 7 67 -64 9 49 49 11 40 41 13 40 -38 15 39 -38 17 38 38	M ₀ K = 8.7 L FCB FCA 2 101 109 4 0 1 6 132-130 8 0 4 10 101 99 12 0 1 14 85 -83 16 0 -2 18 74 69	M ₀ K = 8.8 L FCB FCA 1 57 56 3 61 61 5 71 -68 7 67 -64 9 49 49 11 40 41 13 40 -38 15 39 -38 17 38 38	M ₀ K = 8.9 L FCB FCA 2 101 109 4 0 1 6 132-130 8 0 4 10 101 99 12 0 1 14 85 -83 16 0 -2 18 74 69	M ₀ K = 9.0 L FCB FCA 1 57 56 3 61 61 5 71 -68 7 67 -64 9 49 49 11 40 41 13 40 -38 15 39 -38 17 38 38
---	---	---	--	--	--	---	---	---	---	---	--	--	---	--	---	--	---	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--

Table II. Parameters and standard deviations from least squares.^a

Parameter	This work	Neutron diffraction ^b
Oxygen		
x	0.1504 ± 0.0013	0.1511 ± 0.0006
y	0.0085 ± 0.0014	0.0087 ± 0.0005
z	0.2111 ± 0.0006	0.2111 ± 0.0001
β_{11}	0.0100 ± 0.0016	0.0057 ± 0.0012
β_{22}	0.0115 ± 0.0016	0.0073 ± 0.0014
β_{33}	0.0016 ± 0.0003	0.0016 ± 0.0003
β_{12}	0.0016 ± 0.0013	0.0014 ± 0.0007
β_{13}	0.0004 ± 0.0006	0.0004 ± 0.0002
β_{23}	0.0008 ± 0.0006	0.0005 ± 0.0002
Calcium		
β_{11}	0.0071 ± 0.0004	0.0051 ± 0.0022
β_{33}	0.0011 ± 0.0001	0.0019 ± 0.0006
Tungsten		
β_{11}	0.0036 ± 0.0001	0.0038 ± 0.0022
β_{33}	0.00095 ± 0.00003	0.00038 ± 0.00053

^aOrigin at center of symmetry. Ca at $\pm(0, \frac{1}{4}, \frac{5}{8}) + \mathbb{I}$. W at $\pm(0, \frac{1}{4}, \frac{1}{8}) + \mathbb{I}$. O at $\pm(x, y, z; -x, \frac{1}{2} - y, z; \frac{3}{4} - y, \frac{1}{4} + x, \frac{1}{4} + z; \frac{1}{4} + y, \frac{1}{4} - x, \frac{1}{4} + z) + \mathbb{I}$. $\mathbb{I} = (0, 0, 0; \frac{1}{2}, \frac{1}{2}, \frac{1}{2})$.

^bRef. 3.

Table III. Interatomic distances in CaWO_4 .

Atom	Neighbors	Distance, ^a Å
Ca	4 O	2.44
	4 O	2.48
W	4 O ^b	1.78
	4 O	2.91
O	W	1.78
	W	2.91
	Ca	2.44
	Ca	2.48
	2 O ^b	2.88
	O ^b	2.98
	2 O	2.77
	O	2.88
	2 O	2.94
	O	3.04
O	3.14	

^aStandard deviations 0.01 Å for Ca—O and W—O distances and 0.02 Å for O—O distances.

^bNeighbor in same WO_4 group.

(figure caption)

Fig. 1. Crystal structure of CaWO_4 . The number on each atom is its y coordinate $\times 100$.

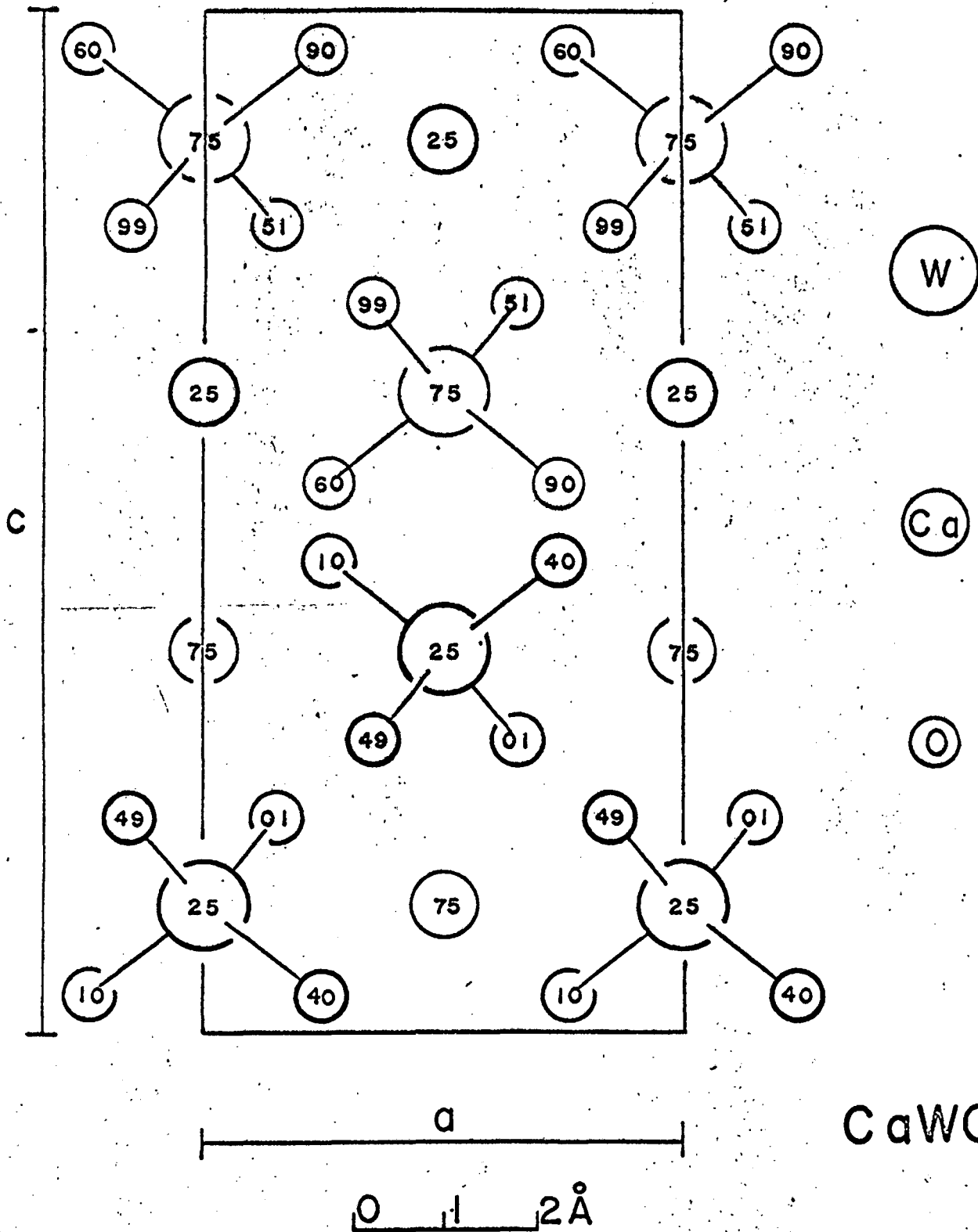


Fig. 1.

MUB-1562

This report was prepared as an account of Government sponsored work. Neither the United States, nor the Commission, nor any person acting on behalf of the Commission:

- A. Makes any warranty or representation, expressed or implied, with respect to the accuracy, completeness, or usefulness of the information contained in this report, or that the use of any information, apparatus, method, or process disclosed in this report may not infringe privately owned rights; or
- B. Assumes any liabilities with respect to the use of, or for damages resulting from the use of any information, apparatus, method, or process disclosed in this report.

As used in the above, "person acting on behalf of the Commission" includes any employee or contractor of the Commission, or employee of such contractor, to the extent that such employee or contractor of the Commission, or employee of such contractor prepares, disseminates, or provides access to, any information pursuant to his employment or contract with the Commission, or his employment with such contractor.

