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Three-Dimensional Steady State Flow of Fluids in Porous Solids

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Authors

Taylor, Robert

Doherty, William

Wilson, Edward

Publication Date

1969-07-01

THREE-DIMENSIONAL, STEADY STATE FLOW
OF FLUIDS IN POROUS SOLIDS

by

Robert L. Taylor

William P. Doherty

and

Edward L. Wilson

Berkeley, California

July 1969

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INTRODUCTION

The steady flow of water beneath the floor of a large barrage develops non-uniform pressures which cannot be accurately predicted by a two-dimensional analysis. In order to obtain predictive information for design the analysis must be completely three-dimensional and be able to include the various geologic factors encountered at most barrage sites. Some of these are stratification, lenses of highly pervious or impervious material, and material anisotropy.

In this report we present the necessary theory and discuss the development of a three-dimensional finite element computer program for the determination of fluid pressures and flows in a porous solid governed by a generalized Darcy law.

An elementary three-dimensional analysis is included to indicate the type of analytical capabilities possible with this computer program.

GENERAL THEORY

In this report the flow of liquids in a saturated porous solid is considered. The flows are specified by a generalized Darcy law expressed by [1]:

$$q_i = - K_{ij} (p,j - F_j) \quad i,j = 1, 2, 3 \quad (2.1)$$

where q_i is the flow rate in the i -direction; p is the liquid pressure; F_j is the body force component in the j -direction; and K_{ij} is a symmetric, second rank tensor [2], which describes the local permeability of the solid. In this section cartesian tensor notation is employed (e.g. see [3]). Accordingly, a comma followed by a subscript denotes partial differentiation with respect to the subscript and a repeated index implies summation over the range of the subscript.

The body forces are usually restricted to gravity effects such that

$$F_j = \rho g_j$$

and ρ is the fluid mass density, g_j the component of acceleration in the j -direction.

Every solid possesses three orthogonal directions for which the local permeability tensor assumes the form (2)

$$\tilde{K}_{ij}(y) = \begin{pmatrix} K_I & 0 & 0 \\ 0 & K_{II} & 0 \\ 0 & 0 & K_{III} \end{pmatrix} \quad (2.2)$$

The y -directions are called the principle material directions. The local values of the permeability tensor are obtained from the principle values by a coordinate transformation. For example, in two cartesian reference frames x_i and y_i , where x_i is a global reference frame and y_i is the principal material frame, we have

$$x_j = a_{jk} y_k \quad (2.3)$$

where a_{jk} is an orthonormal transformation matrix of the direction cosines. Then if $\tilde{q}_m(y)$ are the flow rates in the principal directions we have

$$q_i = a_{im} \tilde{q}_m \quad (2.4)$$

also

$$\frac{\partial p}{\partial y_k} = \frac{\partial p}{\partial x_j} \frac{\partial x_j}{\partial y_k} = a_{jk} \frac{\partial p}{\partial x_j} \quad (2.5)$$

and

$$\tilde{F}_k = (a_{kj})^{-1} F_j = a_{jk} F_j \quad (2.6)$$

finally we obtain from (2.1)

$$q_i = a_{im} \tilde{K}_{mk}(y) a_{jk} \left(\frac{\partial p}{\partial x_j} - F_j(x) \right) \quad (2.7)$$

and hence

$$K_{ij}(x) = a_{im} \tilde{K}_{mk} a_{jk} \quad (2.8)$$

defines the transformation equation from one reference frame to another.

The steady flow of fluids through the porous solid is defined by the solution to the continuity equation

$$(\rho q_i)_{,i} = 0 \quad (2.9)$$

along with suitable boundary conditions. Substitution of the constitutive equation (2.1) into (2.9) yields

$$-(K_{ij} \rho (p_{,j} - F_j))_{,i} = 0 \quad (2.10)$$

For an isotropic material the permeability tensor is independent of direction and may then be expressed in terms of a single parameter

$$K_{ij} = \delta_{ij} K \quad (2.11)$$

where

$$\delta_{ij} = \begin{cases} 1 & i = j \\ 0 & i \neq j \end{cases}$$

Hence, (2.10) reduces to

$$-(\rho K (p_{,i} - F_i))_{,i} = 0 \quad (2.12)$$

By expressing the pressure gradient and body force by a potential

$$\phi_{,i} = p_{,i} - F_i \quad (2.13)$$

and assuming a homogeneous material, (2.12) reduces to a Laplace equation

$$\phi_{,ii} = \nabla^2 \phi = 0 \quad (2.14)$$

Methods of potential theory may be used to solve some boundary value problems. However for arbitrary domains and/or non-homogeneous or stratified solids solutions become intractable. It is then desirable to consider numerical solutions.

In two-dimensional flows it has been traditional to obtain solutions to (2.14) by sketching flow nets [4] or by solving the finite difference model to (2.14). Finite element solutions have also been obtained and shown to be superior numerical solutions as compared to either of the other above cited methods [5,6]. A variational theorem whose Euler equation is (2.12) and whose natural and rigid boundary conditions coincide with the flow problem forms a solid basis for constructing a finite element model.

A VARIATIONAL THEOREM FOR FLUID FLOW IN POROUS SOLIDS

In this report the fluid pressure is chosen as the independent variable instead of the classical potential defined by (2.13). Fluid pressure along free boundaries can easily be computed or is zero. Along sealed boundaries the flow normal to the boundary is known to be zero (in some instances in finite element model refinements known boundary flow rates may be prescribed).

A variational theorem for fluid flow in porous solids governed by a Darcy law is given by

$$\begin{aligned}
 J(p) = & \frac{1}{2} \int_V \rho p_{,i} K_{ij} (p_{,j} - 2 F_j) dV \\
 & + \int_{S_q} \rho \bar{q}_i \eta_i p dS
 \end{aligned}
 \tag{3.1}$$

where in addition to previously defined quantities η_i are direction cosines of the outward normal to the boundary with the i -direction, \bar{q}_i are prescribed boundary flow rates (note $\bar{q}_i \eta_i = \bar{q}_n$) and S_q is that portion of the boundary on which flow rates are prescribed.

Proof of the variational theorem is obtained by setting

$$\delta J(p) = 0
 \tag{3.2}$$

Accordingly

$$\begin{aligned}
 \delta J(p) = & \int_V \rho \delta p_{,i} K_{ij} (p_{,j} - F_j) dV \\
 & + \int_{S_q} \rho \bar{q}_i \eta_i \delta p dS
 \end{aligned}
 \tag{3.3}$$

Use of the divergence theorem yields

$$\begin{aligned} \delta J(p) = & - \int_V \delta p \left(\rho K_{ij} (p_{,j} - F_j) \right)_{,i} dV \\ & + \int_{S_q} \delta p \rho \left(\bar{q}_i + K_{ij} (p_{,j} - F_j) \right) n_i dS \end{aligned} \quad (3.4)$$

The variational theorem is proved since the Euler equation is seen to coincide with (2.12) and the boundary conditions stipulate flows prescribed by (2.1) on S_q and pressures on the boundary conjugate to S_q . Consequently (3.1) is the equivalent variational formulation to the flow problem discussed in Section 2.

The construction of a finite element algorithm from (3.1) and the development of a three-dimensional finite element permeability matrix and flow vector are discussed in Appendix B. A users manual for the computer program (FLPM3D) is contained in Appendix A and a listing of the program appears in Appendix D. In order to illustrate the use of this program in connection with three-dimensional flow under barrages a sample problem is included in Appendix C.

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1. Scheidegger, A.E., The Physics of Flow Through Porous Media, The MacMillan Co., New York, 1960.
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3. Jeffreys, H.J., Cartesian Tensors, Cambridge University Press, 1931.
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APPENDIX A

USER MANUAL FOR COMPUTER PROGRAM FLPM3D

PROGRAM FOR THREE-DIMENSION FLOW OF INCOMPRESSIBLE FLUID
IN ORTHOTROPICALLY PERMEABLE POROUS MEDIA

IDENTIFICATION

FLPM3D - Programmed June 1969 in FORTRAN IV for the CDC 6400.

DESCRIPTION

A finite element procedure is used to solve a generalized Darcy's Law for flow of an incompressible fluid in a three dimensional domain. The approximate solution consists of:

- 1) Nodal point fluid pressures
- 2) Components of flow (velocity) at element centroids. (nodal point components are optional)

The forcing 'function' of the formulation consists of specified nodal point flows and boundary surface flows. The unknowns are nodal point pressures. The governing equations are termed 'media permeability equations.' The residual vector is evaluated from the solution and given with the output as a partial check on accuracy.

The core storage requirements of the program are separated into fixed and variable parts with the fixed portion consisting of instructions, non-subscripted variables and those arrays which are not dependent on the size of an individual problem. The variable portion is controlled by the array A which appears in the blank COMMON statement of the main program. The variable MTOT which also appears in the main program is assigned the value of the dimension of A. In the program listing of Appendix D, MTOT has been set to 12,000. This device serves the following purposes:

1) The capacity of the program is altered by repunching the following two statements of the main program

```
COMMON A (12000)
```

```
MTOT = 12000
```

2) When data input to blank COMMON has been processed and no longer needed it is overwritten to conserve storage.

3) Storage requirements are computed and assigned during execution. In this way only the amount of storage needed for the particular problem being analysed need be reserved. In addition to allowing greater flexibility to the size of problem which can be handled, considerable savings are encountered in the solution of linear equations. In addition, options are included in the program which require no storage if not used.

The complete set of equations is divided into blocks of equations. The number of equations in a block is optimized during execution and depends on the value of MTOT and on the particular problem (in particular on the half-bandwidth). Since temporary storage units are used in the solution of equations the number of time consuming READ, WRITE, BACKSPACE and REWIND statements is decreased when:

- a) Half-bandwidth is decreased
- b) MTOT is increased

The program consists of two equation solving subroutines called GAUSS1 and GAUSS2. GAUSS1 applies when the number of equations in a block is greater than or equal to the half-bandwidth. The program causes the following quantities to be printed:

- a) Total number of equations (equal to number of nodal points)
- b) Half-bandwidth MM

For a given element $ND = JMAX - JMIN + 1$

where

JMAX = numerically largest nodal point for that element

JMIN = numerically smallest nodal point for that element

The value of MM is the largest value that occurs when evaluated for all elements

- c) Number of equations per block
- d) Number of blocks
- e) The name of the subroutine used to solve equations

GAUSS1 is considerably more economical than GAUSS2. GAUSS2 allows the solution of very large systems. The equation solver that will be used for a given problem can be anticipated. (See SIZE LIMITATIONS, page A-15).

The region to be analysed is divided into elements with eight nodes. The most general admissible element has faces which are hyperbolic paraboloids, (figure 1). Let (X, Y, Z) be a right hand cartesian.

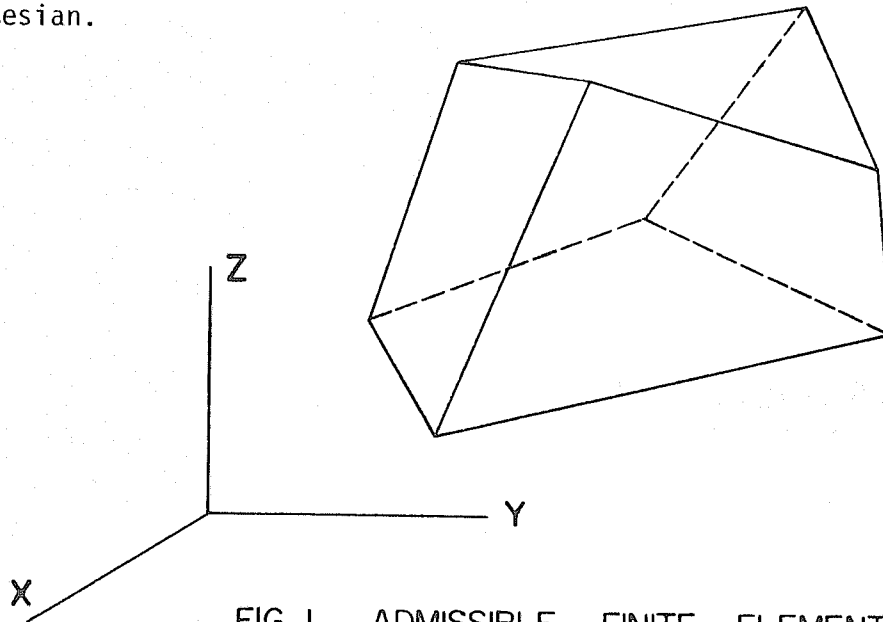


FIG. 1. ADMISSIBLE FINITE ELEMENTS

coordinate frame. The complete geometry of an element is specified by eight interpolation functions and the global coordinates of the nodes.

$$\text{i.e. } X = \sum h_i(r, s, t) X_i \quad i = 1 \dots 8$$

$$Y = \sum h_i(r, s, t) Y_i$$

$$Z = \sum h_i(r, s, t) Z_i$$

where

X, Y, Z are global coordinates of an arbitrary point in the element

X_i, Y_i, Z_i are global coordinates of the nodes

$h_i(r, s, t)$ are the same interpolation functions used in the derivation of the element permeability matrix (see Appendix B).

The interpolation functions map the finite element onto a cube with sides two units in length (figure 2). A scheme for ordering the nodal point numbers is required to match corresponding interpolation functions and global nodal coordinates.

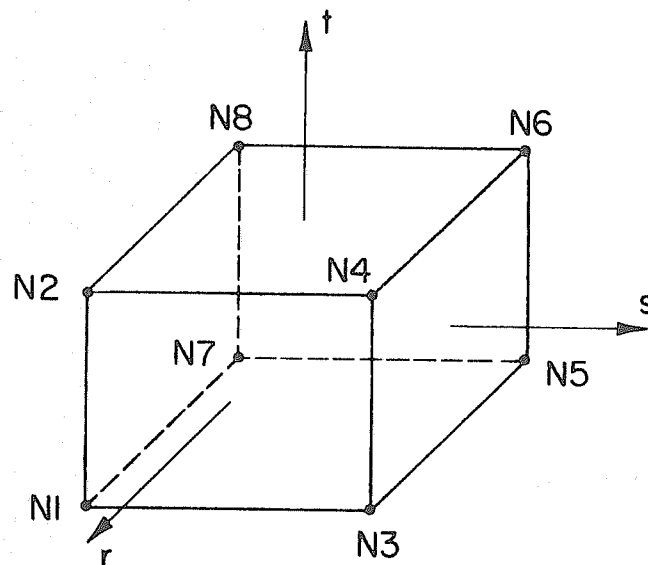


FIG. 2. MAPPED REGION

On the mapped region a right hand cartesian natural coordinate system (r, s, t) is selected arbitrarily. The equations of the six faces are $r = \pm 1, s = \pm 1, t = \pm 1$.

| <u>Face</u> | <u>Equation</u> |
|-------------|-----------------|
| 1 | $r = +1$ |
| 2 | $r = -1$ |
| 3 | $s = +1$ |
| 4 | $s = -1$ |
| 5 | $t = +1$ |
| 6 | $t = -1$ |

Once the orientation of the (r, s, t) system is selected the nodal point sequence $N1, N2---N8$ must be as shown in figure 2. The nodes are numbered in pairs from the $t = -1$ face to the $t = +1$ face progressing around the t axis by the right hand screw rule. The first pair of nodes is determined by the intersection of the $r = +1$ and $s = -1$ faces. To recapitulate: (1) The arbitrary element is mapped onto a cube; (2) Three faces of the cube are chosen arbitrarily to define the (r, s, t) coordinates; (3) Once the (r, s, t) system is chosen the face numbers 1 to 6 are defined as above and the eight nodal point numbers $N1, N2---N8$ have a natural ordering which must be as shown in figure 2.

INPUT

The following sequence of punched cards numerically defines the media to be analysed:

A) START CARD (72H)

The characters FLPM3D must be punched in columns 1 to 6 of the first card for each problem. (There is no limit to the number of different problems). The remainder of the Hollerith field may contain information to be printed as titles on the output. If an error in the input data is detected by the program the current problem is dropped and a search for the next FLPM3D card is initiated.

B) CONTROL CARDS (915/4F10.0)

First Card

Columns

- 1 - 5 NP - Number of nodal points
- 6 - 10 NE - Number of elements
- 11 - 15 NM - Number of different 'media' (maximum = 50)
- 16 - 20 NF - Number of distributed boundary flow cards
- 21 - 25 ND - Number of sets of reference direction numbers
- 26 - 30 NL - Number of loading cases (maximum = 3)
- 31 - 35 NV - Element velocity option
- 36 - 40 NB - Limit on allowable half-bandwidth
- 41 - 45 NS - Number of temporary element storage blocks

Second Card

Columns

- 1 - 10 AX - Global X component of gravitational acceleration
- 11 - 20 AY - Global Y component of gravitational acceleration
- 21 - 30 AZ - Global Z component of gravitational acceleration
- 31 - 40 UW - Unit weight of fluid in media

By a 'media' is meant a unique set of principal permeability components of the generalized permeability tensor. These components are defined by Darcy's Law

$$\{q\} = - [K] (\{grad\ p\} + \{F\})$$

where

$\{q\} \equiv$ fluid velocity vector

$\{grad\ p\} \equiv$ pressure gradient vector

$\{F\} \equiv$ body force vector per unit volume due to gravitational acceleration

$[K] \equiv$ components of permeability tensor

Since principal components are input, the components of $[K]$ must be transformed to components relative to the global basis. Direction numbers are input for this purpose (see section E).

If $NV = 0$, flows are derived from the pressure field at the centroid of each element and output. If $NV = 1$ the flows are also evaluated at element nodal points and averaged with adjacent elements. It is to be noted that for $NV = 1$ increased storage is required as well as a substantial increase in computation time.

ND is a safety device. If the upper limit on the half-bandwidth is exceeded by any element, execution of that problem is

terminated. Since the program contains an equation solver that will handle very large systems an error on an element card resulting in an erroneously high half-bandwidth could prove to be costly if this device is not used.

Since elements are very often similar, considerable savings can be realized by utilizing the same element permeability matrix for all of its similar elements. For this reason it is possible to specify up to three temporary storage regions in which common element properties are stored for reference by other elements (see (J)). It is to be noted that storage is reserved only for the number of blocks specified by NS.

C) LOADING CASES CONTROL CARD (215)

One card is required for each loading case.

Columns

1 - 5 NPL - Number of specified non-zero nodal flows for this loading case

6 - 10 NEL - Number of element faces with distributed normal flows for this loading case

D) PRINCIPAL PERMEABILITY COMPONENTS (I5,3F10.0)

One card is required for each unique set of components.

Columns

1 - 5 N - Identification

6 - 15 KI

16 - 25 KII

26 - 35 KIII

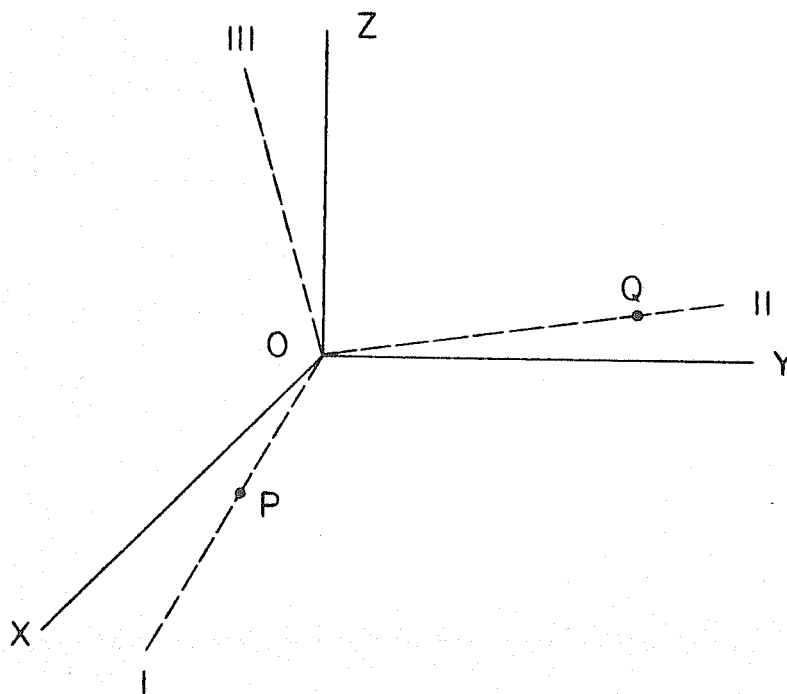
} Principal permeability components where
I, II, III are right hand cartesian axes.

E) DIRECTION NUMBERS (I5,6F10,0)

One card is required for each unique set. These numbers are used to compute basis transformations between global and principal permeability axes.

Columns

| | | | |
|---------|----|---|----------------------------------|
| 1 - 5 | N | - | Identification |
| 6 - 15 | P1 | } | Direction Numbers for I Axis |
| 16 - 25 | P2 | | |
| 26 - 35 | P3 | | |
| 36 - 45 | Q1 | } | Direction Numbers for II Axis |
| 46 - 55 | Q2 | | |
| 56 - 65 | Q3 | | |



Let P and Q be points on the I and II axes respectively. Let global coordinates of P be X(P), Y(P) and Z(P) with a similar notation for points O and Q. Then

$$P1 = X(P) - X(O)$$

$$P2 = Y(P) - Y(O)$$

$$P3 = Z(P) - Z(O)$$

$$Q1 = X(Q) - X(O)$$

$$Q2 = Y(Q) - Y(O)$$

$$Q3 = Z(Q) - Z(O)$$

Note that these numbers are not unique but serve to uniquely specify the I and II axes. The direction cosines for the III axes are obtained in the program by forming a vector (cross) product.

F) NODAL POINT CARDS (3I5,4F10.0,I5)

Columns

1 - 5 NI - Nodal point identification number
6 - 10 K - Nodal point data generation option
11 - 15 KD - Boundary condition code
16 - 25 X - Global X coordinate of NI
26 - 35 Y - Global Y coordinate of NI
36 - 45 Z - Global Z coordinate of NI
46 - 55 P - Value of pressure boundary condition if KD = 1,
otherwise blank
56 - 60 L - Boundary value generation parameter

The value of KD is:

0 if nodal flow is specified

1 if nodal pressure is specified

Pressure boundary conditions must be the same for each loading case.

If a series of nodal points occur on a straight line only the first and last nodal point of the series need be input if:

1) each nodal point in the series is obtained from the previous by adding a fixed constant. The data generation option K is the value of this constant.

2) If the value of L is

- a) 0 - KD is set to zero for each generated node
 - P is set to zero for each generated node if $KD = 1$ on input card
- b) 1 - KD is set equal to that of the first node in the series
 - P is set equal to that of first node in series for each generated node if $KD = 1$
- c) 2 - KD for each generated node is set equal to that of first node in series
 - P for each generated node is interpolated linearly between end nodes if $KD = 1$

Note that it is not necessary to input the nodal cards in numerical sequence (i.e. order of increasing nodal point numbers). Suppose nodal point data cards for nodes NI and NJ are input in succession. If the numerical quantity $NJ - NI$ is -

- a) positive: nodal point data will be generated for nodes $NI + K, NI + 2K, \dots, NJ - K$
- b) negative: no nodal point generation

This option is illustrated in the examples given with this report.

G) NON-ZERO NODAL FLOW BOUNDARY CONDITIONS (I5,F10.0)

One set of cards is required for each loading case. The number of cards must be equal to NPL in (C). If NPL is zero for a particular case no cards are input for that loading.

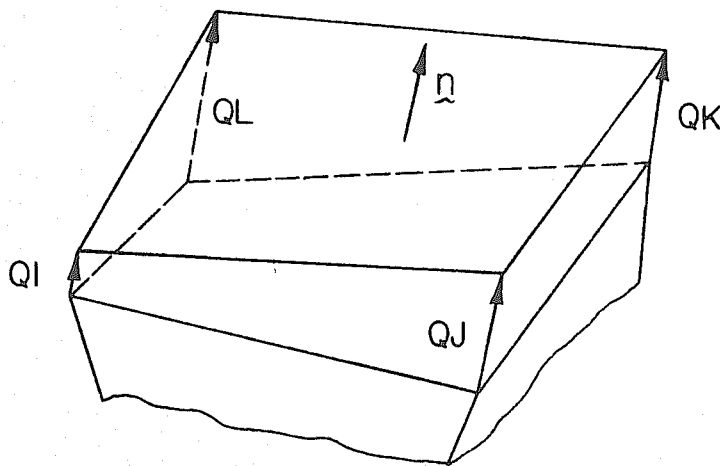
Columns

1 - 5 NI - Nodal point identification number

6 - 15 Q - Non-zero specified nodal flow (positive flow if fluid is added to node, otherwise negative)

H) SURFACE BOUNDARY FLOW TYPES (I5,4F10.0)

One card is required for each unique distribution of normal flow through an element surface.



DISTRIBUTED FLOW
NORMAL TO
ELEMENT SURFACE

Columns

1 - 5 N - Identification number

6 - 15 QI - Magnitude of outward normal flow at node NI

16 - 25 QJ - Magnitude of outward normal flow at node NJ

26 - 35 QK - Magnitude of outward normal flow at node NK

36 - 45 QL - Magnitude of outward normal flow at node NL

Note that nodes NI, NJ, NK, NI must be ordered by right hand screw rule about the outward normal. Specifying four magnitudes allows a bilinear variation in normal flow. Equivalent nodal flows are evaluated by the program using numerical integration. Specifying nodal flows rather than surface distributions is computationally more economical.

I) SURFACE FLOW LOADING CASES (4I5)

One card is required for each element face in each loading condition that has surface flow. The number of cards must agree with NEL given in (C).

Columns

- 1 - 5 L - Load case number (1, 2 or 3)
- 6 - 10 NE - Element identification number
- 11 - 15 NF - Face identification number (a number from 1 to 6 as described previously)
- 16 - 20 N - Identification number of loading type in (H) above

J) ELEMENT CARDS (18I4)

Columns

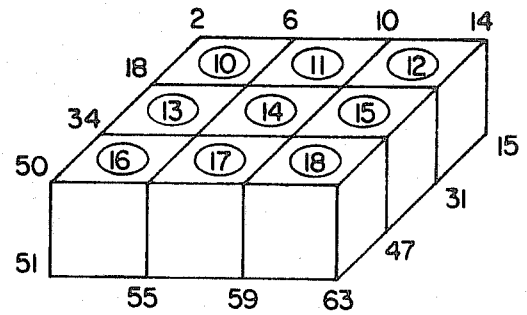
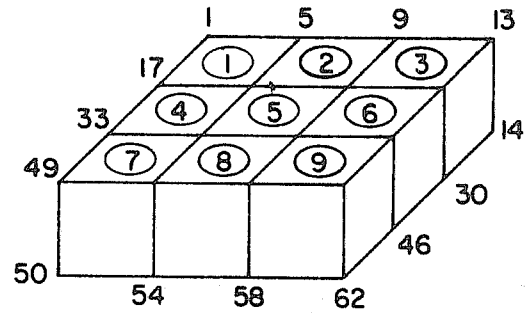
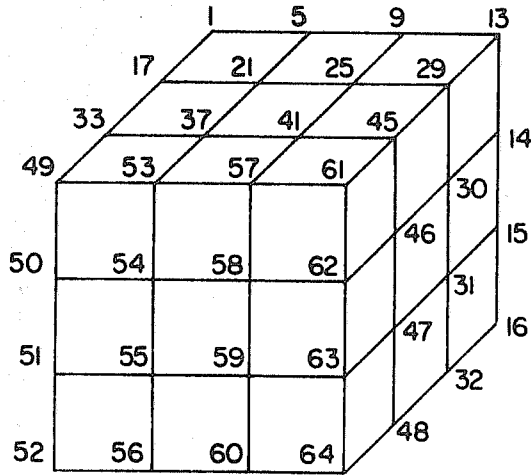
- 1 - 4 NE - Element identification number
 - 5 - 8 NI -
 - 9 - 12 N2 -
 - 13 - 16 N3 -
 - 17 - 20 N4 -
 - 21 - 24 N5 -
 - 25 - 28 N6 -
 - 29 - 32 N7 -
 - 33 - 36 N8 -
- } Element nodal point numbers in sequence discussed previously

| | |
|---------|---|
| 37 - 40 | M - Media identification number |
| 41 - 44 | ND - Identification number of applicable direction numbers. If left blank the principal axes of permeability are taken to be coincident with global X, Y, Z axes |
| 45 - 48 | GET - The element permeability matrix for this element will be obtained from storage block identified by the number GET |
| 49 - 52 | STORE - The computed permeability matrix for this element will be stored in storage block identified by the number STORE for reference by elements input later whose GET is equal to this STORE |
| 53 - 56 | I1 - Increment factor for 1 dimensional element generation |
| 57 - 60 | I2 - Increment factor for 2 dimensional element generation |
| 61 - 64 | I3 - Increment factor for 3 dimensional element |
| 65 - 68 | J1 - Number of elements in a row when I2 \neq 0 |
| 69 - 72 | J2 - Number of elements in a plane when I3 \neq 0 |

I1, I2, I3, J1 and J2 are used to generate rows, planes and three-dimensional arrays of similar elements. Two elements are similar if

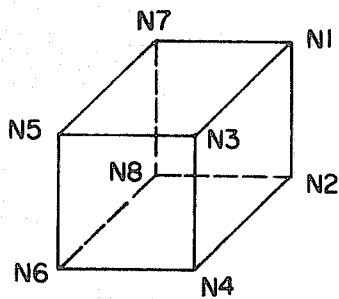
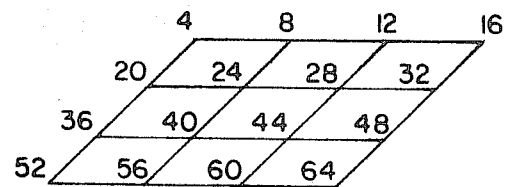
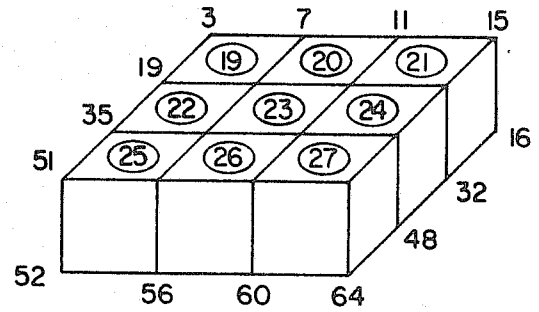
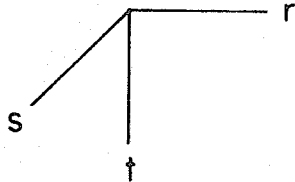
- 1) one element can be obtained from the other by translations (no rotations) along the global axes;
- 2) the nodal point sequence N1, N2.....N8 is preserved under the above translation;
- 3) the element numbers of the generated sequence form an arithmetic progression with an increment of unity;

FIG. 3 ELEMENT GENERATION



ELEMENTS ——— (E)
 NODES ——— N

r, s, t DIRECTIONS FOR ALL ELEMENTS



- 4) the media and direction number identifications as well as the value of GET for each generated element are identical. If both GET and STORE are specified on an element data card then the STORE applies to the input element while the GET applies to the generated elements.
- 5) the surface boundary flow loadings must be identical for similar elements.

When such a sequence occurs only the first element need by input. That element whose identification number is equal to the number of elements must always be input.

The use of I1, I2, I3, J1 and J2 is illustrated by the following example (figure 3).

| NE | N1 | N2 | N3 | N4 | N5 | N6 | N7 | N8 |
|----|----|----|----|----|----|----|----|----|
| 1 | 5 | 6 | 21 | 22 | 17 | 18 | 1 | 2 |
| 2 | 9 | 10 | 25 | 26 | 21 | 22 | 5 | 6 |
| 3 | 13 | 14 | 29 | 30 | 25 | 26 | 9 | 10 |
| 4 | 21 | 22 | 37 | 38 | 33 | 34 | 17 | 18 |

} I1 = 4
} I2 = 8

| | | | | | | | | |
|----|----|----|----|----|----|----|----|----|
| 9 | 45 | 46 | 61 | 62 | 57 | 58 | 41 | 42 |
| 10 | 6 | 7 | 22 | 23 | 18 | 19 | 2 | 3 |

} I3 = - 39

- a) Elements 1,2,3 form a row. The nodal point numbers of element 2 are obtained by adding 4 to each nodal point number of element 1. Element 3 is obtained similarly from element 2. Hence the value of I1 is 4. This applies to each set of 3 elements (1,2,3), (4,5,6).....(25,26,27).

- b) Element 4 in the second row is obtained from element 3 in the first row by an increment factor of 8. Similarly element 7 is obtained from element 6. Hence value of I2 is 8 and since there are 3 elements per row the value of J2 is 3. This applies to each of the sets (3,4), (6,7), (9,10),....(24,25)
- c) Element 10 in the second plane is obtained from element 9 in the first plane by an increment factor of -39. Element 19 is obtained similarly from element 18. Hence value of I3 is -39. Since there are 9 elements per plane the value of J3 is 9.

Consequently the 27 elements can be generated by inputting element 1 only (If element 27 is the last element in the media, it must also be input) as follows:

| NE | N1 | N2 | N3 | N4 | N5 | N6 | N7 | N8 | I1 | I2 | I3 | J2 | J3 |
|----|----|----|----|----|----|----|----|----|----|----|----|----|----|
|----|----|----|----|----|----|----|----|----|----|----|----|----|----|

| | | | | | | | | | | | | | |
|----|----|----|----|----|----|----|----|---|---|---|-----|---|---|
| 1 | 5 | 6 | 21 | 22 | 17 | 18 | 1 | 2 | 4 | 8 | -39 | 3 | 9 |
| 27 | 47 | 48 | 63 | 64 | 59 | 60 | 44 | | | | | | |

As an illustration of two-dimensional generation elements 11 through 18 can be generated from element 10 as follows:

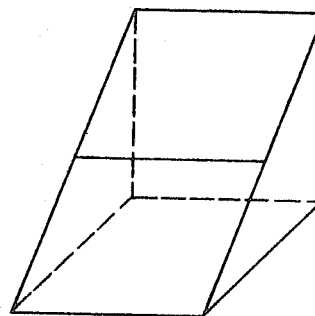
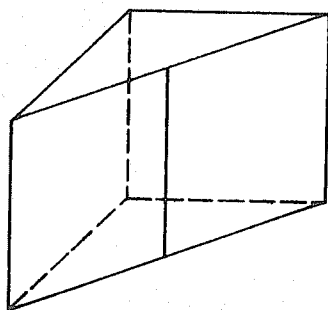
| NE | N1 | N2 | N3 | N4 | N5 | N6 | N7 | N8 | I1 | I2 | I3 | J2 | J3 |
|----|----|----|----|----|----|----|----|----|----|----|----|----|----|
| 10 | 6 | 7 | 22 | 23 | 18 | 19 | 2 | 3 | 4 | 8 | | 3 | |

As an illustration of one-dimensional generation elements 11 and 12 can be generated from element 10, elements 14 and 15 from 13, and elements 17 and 18 from 16 as follows:

| NE | N1 | N2 | N3 | N4 | N5 | N6 | N7 | N8 | I1 | I2 | I3 | J2 | J3 |
|----|----|----|----|----|----|----|----|----|----|----|----|----|----|
| 10 | 6 | 7 | 22 | 23 | 18 | 19 | 2 | 3 | 4 | | | | |
| 13 | 22 | 23 | 38 | 39 | 34 | 35 | 18 | 19 | 4 | | | | |
| 16 | 38 | 39 | 54 | 55 | 50 | 51 | 34 | 35 | 4 | | | | |

"WEDGE" ELEMENTS

These elements are admissible and are useful for approximating irregular boundaries and for mesh gradation. Note that whenever a mesh contains one or more of these elements the velocity option parameter (NV on CONTROL CARD) must be zero (0).



K) STOP card

Normal termination will result if the word STOP is punched in columns 1 to 4 on a separate card following the last problem data.

SIZE LIMITATIONS

$$(a) \quad NP*(5 + NL) + 6*ND + 4*NEL + 99*NS + 4*NF \leq MTOT$$

NP = Number of nodal points

NL = Number of load cases

ND = Number of sets of direction numbers

NS = Number of temporary element storage blocks

NEL = Total number of element faces with distributed normal surface flows for all loading cases

NF = Number of distributed boundary flow cards

(b) The number of rows of equations in a block is evaluated by the following logic using integer arithmetic.

NC = MM + NL

NC1 = NC + 1

NR2 = (MTOT - NL*NP)/NC1

NR = NR2/2

IF (NR2.GE.NP) NR = NP

IF (NR.LT.MM) GO TO 60

ITYPE = 1

GO TO 70

60 ITYPE = 2

70 NSET = (NP - 1)/NR + 1

where

MM = Half bandwidth

NR = Number of equations per block

NSET = Number of blocks

GAUSS1 will be called if ITYPE = 1

GAUSS2 will be called if ITYPE = 2

If ITYPE = 1 and NSET = 1 then $N4 = NR*NC1 + NL*NP$ Otherwise

$$N4 = NR*(2*NC + 1) + NL*NP$$

Three additional size limitations are

i) $N4 \leq MTOT$

ii) $NR*NC \geq NP$

iii) $NR \geq 2$

Actually ii) was imposed to allow for more efficient coding and hence does not result strictly from limitations on core storage.

The above four restrictions are checked by the program. Execution is terminated if any are violated.

CHANGING ALLOWABLE CAPACITY

Changing the overall capacity of the program has already been described. The only other limitation is on the number of different media (described as 50 herein). This limitation can be altered by changing the 50 in the following COMMON assignment in the 3 subroutines in which it occurs.

```
COMMON / MATARG /  
1 UWT,ACCG,E(50,3)
```

TEMPORARY STORAGE UNITS

Logical units are assigned for temporary storage in the main program by the statements

NTAPE1 = 1

NTAPE2 = 2

etc.

The number of temporary storage units required depends on the equation solver used and on the number of loading cases.

| Number of Loading Cases | Equation Solver | Storage Units |
|-------------------------|-----------------|--|
| 1 | GAUSS1 | NTAPE2, NTAPE3, NTAPE4 |
| | GAUSS2 | NTAPE2, NTAPE3, NTAPE4, NTAPE5 |
| 2 | GAUSS1 | NTAPE2, NTAPE3, NTAPE4, NTAPE5 |
| | GAUSS2 | NTAPE2, NTAPE3, NTAPE4, NTAPE5 |
| 3 | GAUSS1 | NTAPE2, NTAPE3, NTAPE4, NTAPE5, NTAPE6 |
| | GAUSS2 | NTAPE2, NTAPE3, NTAPE4, NTAPE5, NTAPE6 |

NTAPE1 is required for all cases. Note that logical units 5 and 6 are the printer READ and WRITE units.

SUBROUTINE CPTIME

This subroutine calls the library routine SECOND(T) which returns the elapsed central processor time in seconds from the beginning of the job. Subroutine CPTIME is called six times by subroutine FPCALL. The values returned by these calls are used to evaluate the time log printed with the output.

SUMMARY OF INPUT (FLPM3D)

| | | | | | | | | |
|--|----|----|----|----|----|----|----|----|
| | 10 | 20 | 30 | 40 | 50 | 60 | 70 | 80 |
|--|----|----|----|----|----|----|----|----|

A. START CARD (72H)

FLPM3D

B. CONTROL CARDS (9I5/4F10.0)

| | | | | | | | | |
|----|----|----|----|----|----|----|----|----|
| NP | NE | NM | NF | ND | NL | NV | NB | NS |
| AX | AY | AZ | UW | | | | | |

C. LOADING CASES CONTROL CARDS (2I5) - ONE CARD FOR EACH LOADING CASE

NPL NEL

D. PRINCIPAL PERMEABILITY COEFFICIENTS (I5, 3F10.0)

| | | | |
|---|----|-----|------|
| N | KI | KII | KIII |
|---|----|-----|------|

E. DIRECTION NUMBERS (I5, 6F10.0)

| | | | | | | |
|---|----|----|----|----|----|----|
| N | PI | P2 | P3 | Q1 | Q2 | Q3 |
|---|----|----|----|----|----|----|

F. NODAL POINT CARDS (3I5, 4F10.0, I5)

| | | | | | | | |
|----|---|----|---|---|---|---|---|
| NI | K | KD | X | Y | Z | P | L |
|----|---|----|---|---|---|---|---|

G. NON-ZERO NODAL FLOWS (I5, F10.0)

NI Q

H. SURFACE BOUNDARY FLOW TYPES (I5, 4F10.0)

| | | | | |
|---|----|----|----|----|
| N | QI | QJ | QK | QL |
|---|----|----|----|----|

I. SURFACE FLOW LOADING CASES (4I5)

| | | | |
|---|----|----|---|
| L | NE | NF | N |
|---|----|----|---|

J. ELEMENT CARDS (I8I4)

| | | | | | | | | | | | | | | | | | |
|----|----|----|----|----|----|----|----|----|---|----|-----|-------|----|----|----|----|----|
| NE | NI | N2 | N3 | N4 | N5 | N6 | N7 | N8 | M | ND | GET | STORE | I1 | I2 | I3 | J2 | J3 |
|----|----|----|----|----|----|----|----|----|---|----|-----|-------|----|----|----|----|----|

K. STOP CARD (4H) - FOLLOWS LAST PROBLEM DATA

STOP

APPENDIX B

DERIVATION OF FINITE ELEMENT PERMEABILITY
MATRIX AND FLOW VECTOR FOR
THREE-DIMENSIONAL FLOW IN POROUS MEDIA

The functional defining Darcy flow in a porous solid was given in Section 3 as:

$$J(p) = \frac{1}{2} \int_V \rho p_{,i} K_{ij} (p_{,j} - 2 F_j) dV + \int_{S_q} \rho \bar{q}_i n_i p dS \quad (B.1)$$

where:

- p is the fluid pressure
- K_{ij} is the local (engineering) permeability tensor
- F_j is a body force
- \bar{q}_i are prescribed boundary flows
- n_i are direction cosines of the outward normal to the boundary surfaces
- ρ is the mass density of the fluid
- V is the volume occupied by the solid
- S_q is that portion of the boundary surface for which flows are prescribed.

Application of the finite element method divides the volume into subregions (elements); the boundary surface is then defined by the surface of the elements.

$$V = \sum_{m=1}^M \Delta V_m$$

where M is the total number of elements

In using the finite element method to obtain approximate solutions from (B.1) we require p to be a continuous function and possess piecewise continuous first derivatives. In this report we take the three-dimensional

finite elements as shown in Fig. A.1. Each element is defined by 8 corner nodes and the interior region (global coordinates x, y, z) lies within

$$-1 \leq r \leq 1 \quad -1 \leq s \leq 1 \quad -1 \leq t \leq 1$$

where r, s, t are natural coordinates as shown in Fig. A.2. The mapping between the global and natural coordinates is given by (A.1) where

$$h_i(r, s, t) = (1 + r \cdot R_i) (1 + s \cdot S_i) (1 + t \cdot T_i) \quad (B.3)$$

where:

$$R_i = \langle 1, 1, 1, 1, -1, -1, -1, -1 \rangle$$

$$S_i = \langle -1, -1, 1, 1, 1, 1, -1, -1 \rangle$$

$$T_i = \langle -1, 1, -1, 1, -1, 1, -1, 1 \rangle$$

Since (A.1) produces a continuous mapping of the interior region of V , a continuous distribution of fluid pressure is also given by

$$p = \sum_{i=1}^8 h_i P_i \quad (B.4)$$

where P_i are the nodal values of the pressure.

The element permeability matrix and flow vector for each element are derived from

$$U_m(p) = \frac{1}{2} \int_{\Delta V_m} \rho \langle DP \rangle [D] \left(\{DP\} - 2 \{F\} \right) dV \quad (B.5)$$

where:

$$\langle DP \rangle = \left\langle \frac{\partial p}{\partial x}, \frac{\partial p}{\partial y}, \frac{\partial p}{\partial z} \right\rangle \quad \text{pressure gradients}$$

$$\{F\}^T = \langle F_x, F_y, F_z \rangle \quad \text{body forces}$$

$$[D] = \begin{bmatrix} K_{xx} & K_{xy} & K_{xz} \\ K_{xy} & K_{yy} & K_{yz} \\ K_{xz} & K_{yz} & K_{zz} \end{bmatrix} \quad \begin{array}{l} \text{local permeabilities} \\ \text{in global} \\ \text{coordinates} \end{array}$$

Using (B.4) the pressure gradient vector can be expressed in terms of the nodal pressures as

$$\{DP\} = [B] \{P\} \quad (B.6)$$

where

$$[B] = \begin{bmatrix} \frac{\partial h_1}{\partial x} & \frac{\partial h_2}{\partial x} & \cdot & \cdot & \cdot & \cdot & \cdot & \frac{\partial h_8}{\partial x} \\ \frac{\partial h_1}{\partial y} & \frac{\partial h_2}{\partial y} & \cdot & \cdot & \cdot & \cdot & \cdot & \frac{\partial h_8}{\partial y} \\ \frac{\partial h_1}{\partial z} & \frac{\partial h_2}{\partial z} & \cdot & \cdot & \cdot & \cdot & \cdot & \frac{\partial h_8}{\partial z} \end{bmatrix} \quad (B.7)$$

$$\{P\}^T = \langle P_1, P_2, \cdot, \cdot, \cdot, \cdot, \cdot, P_8 \rangle$$

Now

$$U_m(p) = \frac{1}{2} \langle P \rangle [QK] \{P\} - \langle P \rangle \{Q\} \quad (B.8)$$

where

$$[QK] = \int_{V_m} \rho [B]^T [D] [B] dV \quad (B.9)$$

and

$$\{Q\} = \int_{V_m} \rho [B]^T [D] \{F\} dV \quad (B.10)$$

The elements of [B] are obtained by use of the chain rule for differentiation.

Accordingly,

$$\begin{Bmatrix} \frac{\partial}{\partial r} \\ \frac{\partial}{\partial s} \\ \frac{\partial}{\partial t} \end{Bmatrix} = [J] \begin{Bmatrix} \frac{\partial}{\partial x} \\ \frac{\partial}{\partial y} \\ \frac{\partial}{\partial z} \end{Bmatrix} \quad (B.11)$$

where

$$[J] = \begin{bmatrix} \frac{\partial x}{\partial r} & \frac{\partial y}{\partial r} & \frac{\partial z}{\partial r} \\ \frac{\partial x}{\partial s} & \frac{\partial y}{\partial s} & \frac{\partial z}{\partial s} \\ \frac{\partial x}{\partial t} & \frac{\partial y}{\partial t} & \frac{\partial z}{\partial t} \end{bmatrix} = [H \ D] \begin{bmatrix} x_1 & y_1 & z_1 \\ x_2 & y_2 & z_2 \\ \cdot & \cdot & \cdot \\ \cdot & \cdot & \cdot \\ \cdot & \cdot & \cdot \\ x_8 & y_8 & z_8 \end{bmatrix} \quad (B.12)$$

and

$$[H \ D] = \begin{bmatrix} \frac{\partial h_1}{\partial r} & \frac{\partial h_2}{\partial r} & \cdot & \cdot & \cdot & \cdot & \cdot & \frac{\partial h_8}{\partial r} \\ \frac{\partial h_1}{\partial s} & \frac{\partial h_2}{\partial s} & \cdot & \cdot & \cdot & \cdot & \cdot & \frac{\partial h_8}{\partial s} \\ \frac{\partial h_1}{\partial t} & \frac{\partial h_2}{\partial t} & \cdot & \cdot & \cdot & \cdot & \cdot & \frac{\partial h_8}{\partial t} \end{bmatrix} \quad (B.13)$$

The pressure gradient vector may now be expressed as

$$\{DP\} = [J]^{-1} [HD] \{P\} = [B] \{P\} \quad (B.14)$$

The determinant of $[J]$ is the jacobian, XJAC, for each point (r,s,t) in the natural coordinate frame. By making a change in coordinates to the natural reference frame for (B.9) and (B.10) the integrals become

$$\int_{V_m} (\quad) dV = \int_{-1}^1 \int_{-1}^1 \int_{-1}^1 (\quad) XJAC dr ds dt \quad (B.15)$$

which can be accurately evaluated numerically using Gaussian formulae repeatedly in the three directions.

APPENDIX C

EXAMPLE PROBLEM

FLOW UNDER A BARRAGE
SUPPORTED ON VARIABLE MEDIA FOUNDATION

1.0 Problem Statement

A simplified problem of flow under a barrage supported on a two-media foundation and a finite element idealization is described in figures C-1 to C-5.

2.0 Graphical Results

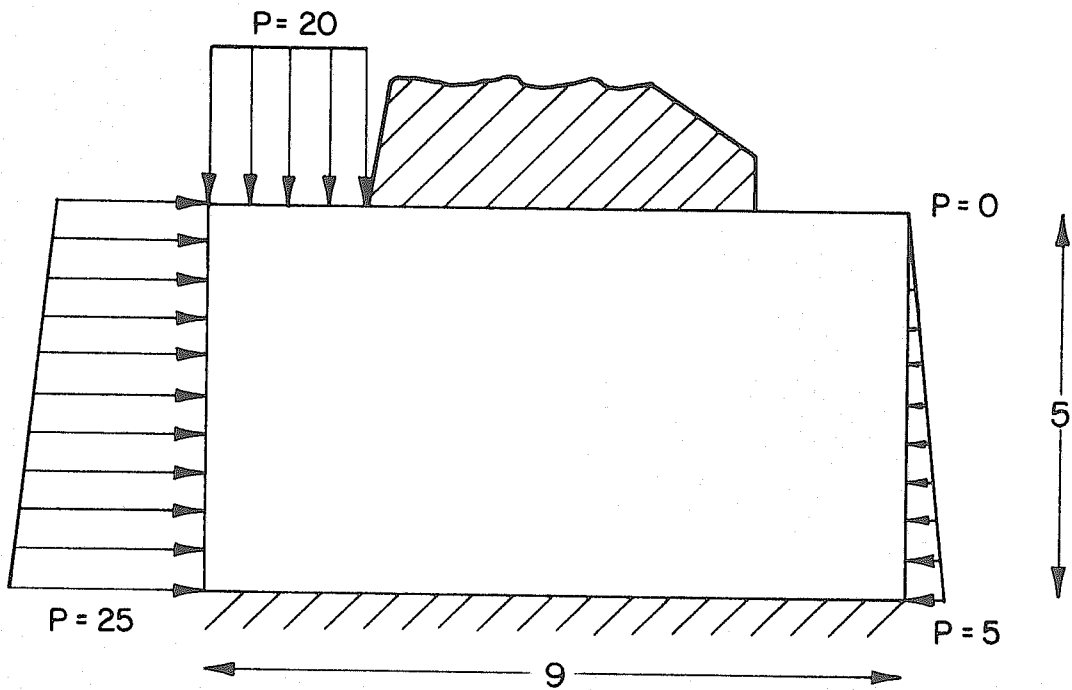
Pressure distributions along base of barrage obtained from computer program are plotted in figures C-6 and C-7.

3.0 Input Data

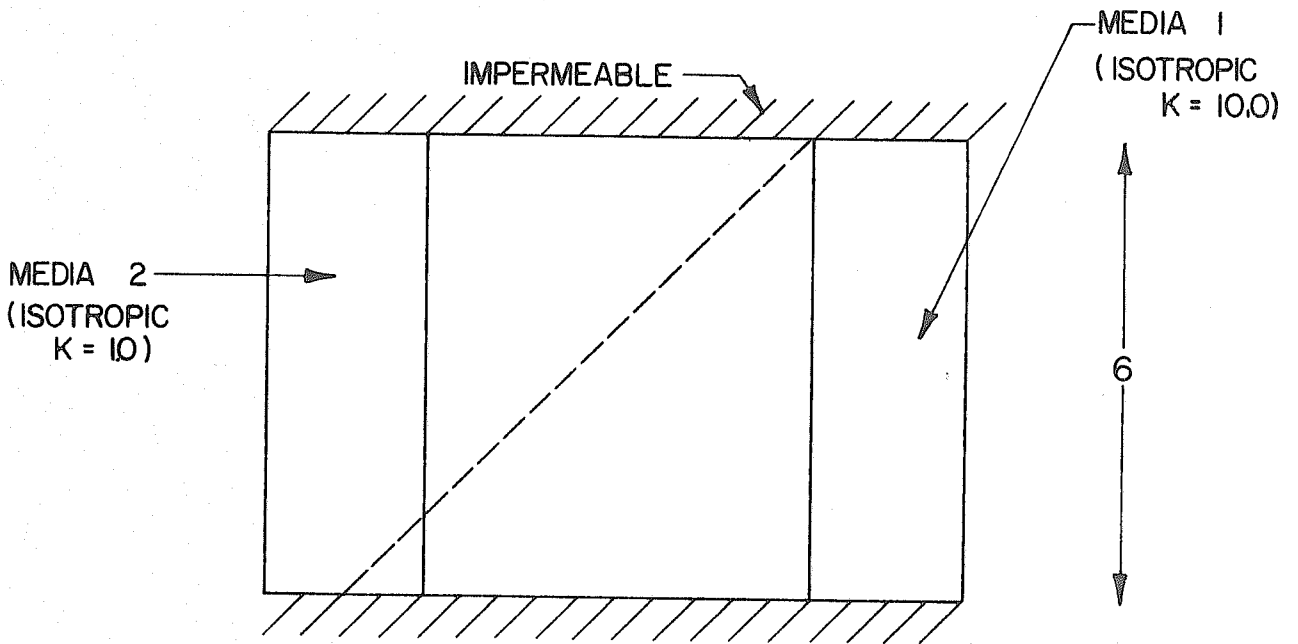
Pages C-8 to C-12 is a listing of data cards.

4.0 Computer Output

Computer output for the example problem begins on page C-13.



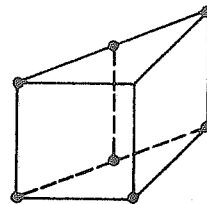
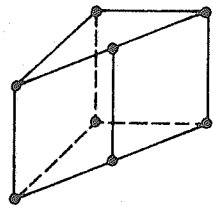
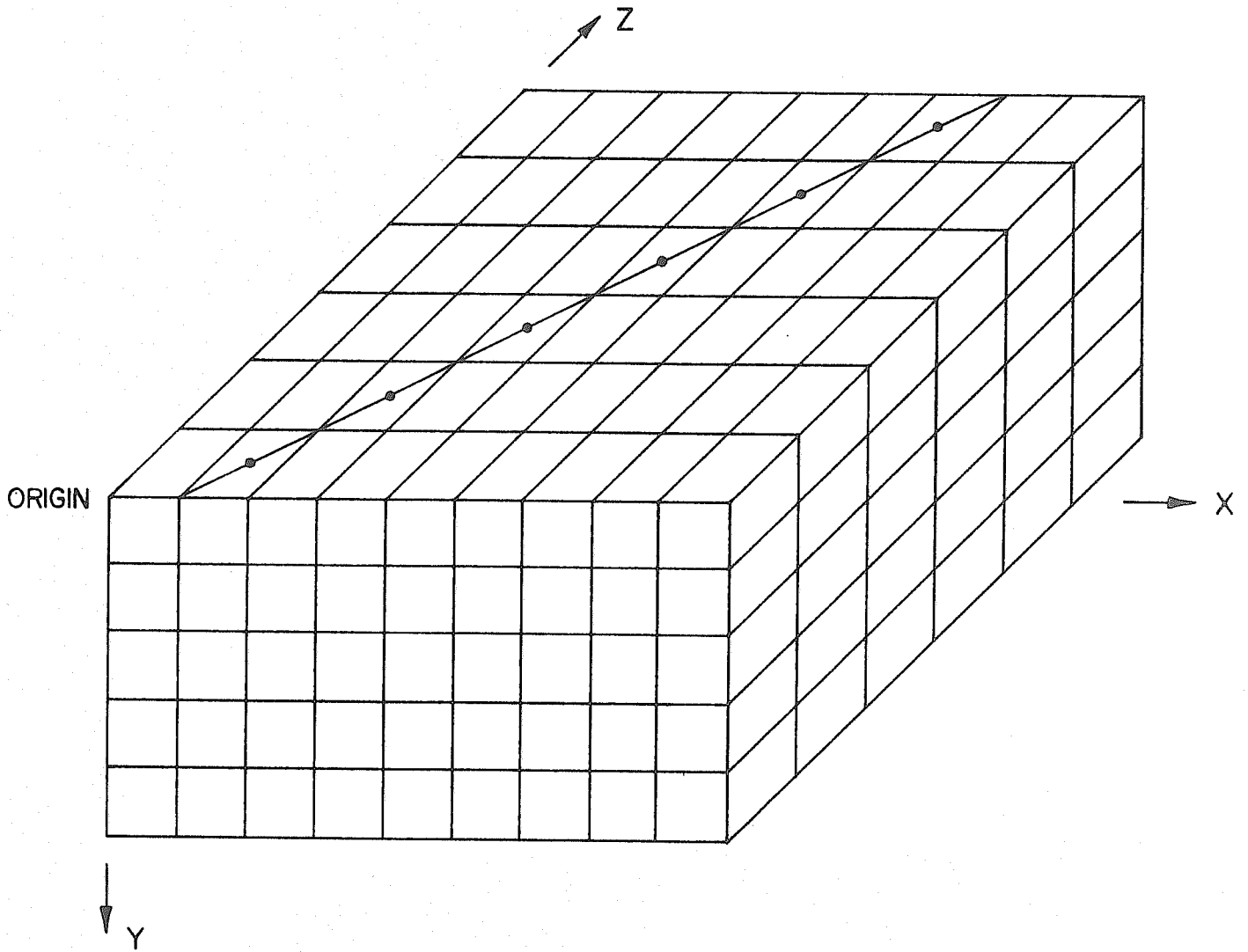
ELEVATION



PLAN

FLUID UNIT WEIGHT ————— 1.0
 GRAVITATIONAL ACCELERATION — 1.0

FIG. C-1 FLOW UNDER A TWO-MEDIA BARRAGE



"WEDGE"
ELEMENTS

FIG. C-2 FINITE ELEMENT IDEALIZATION

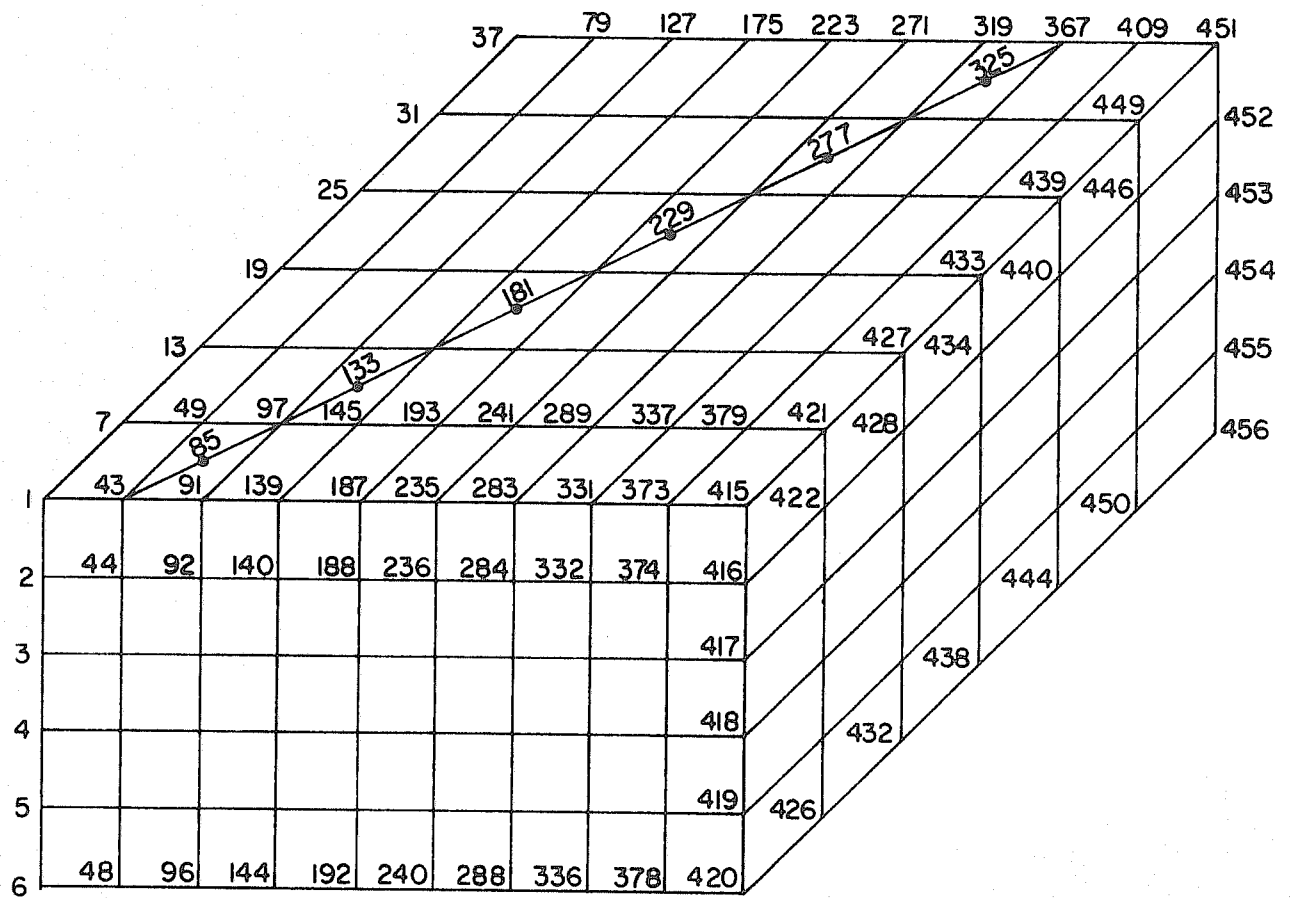


FIG. C-3 NODAL POINT IDENTIFICATION

$$K_I = K_{II} = K_{III} = 10.0$$

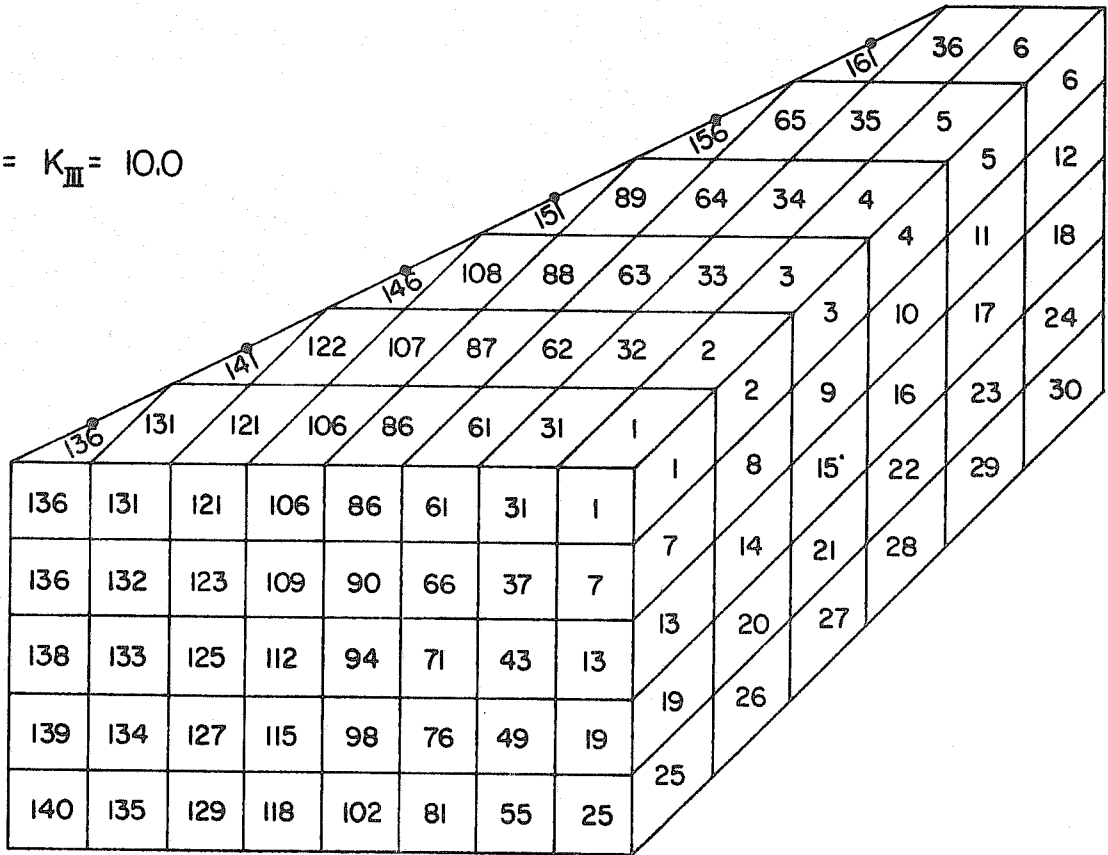


FIG. C-4 ELEMENT IDENTIFICATION - MEDIA I

$$K_I = K_{II} = K_{III} = 1.0$$

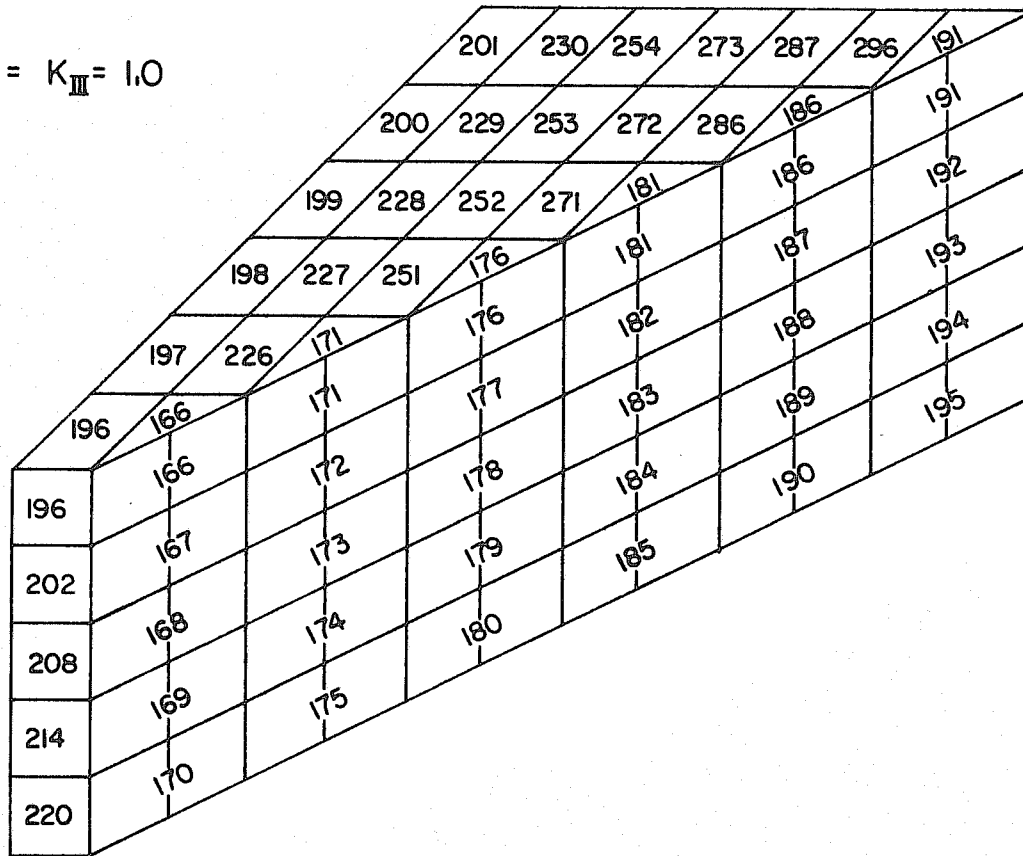


FIG. C-5 ELEMENT IDENTIFICATION — MEDIA 2

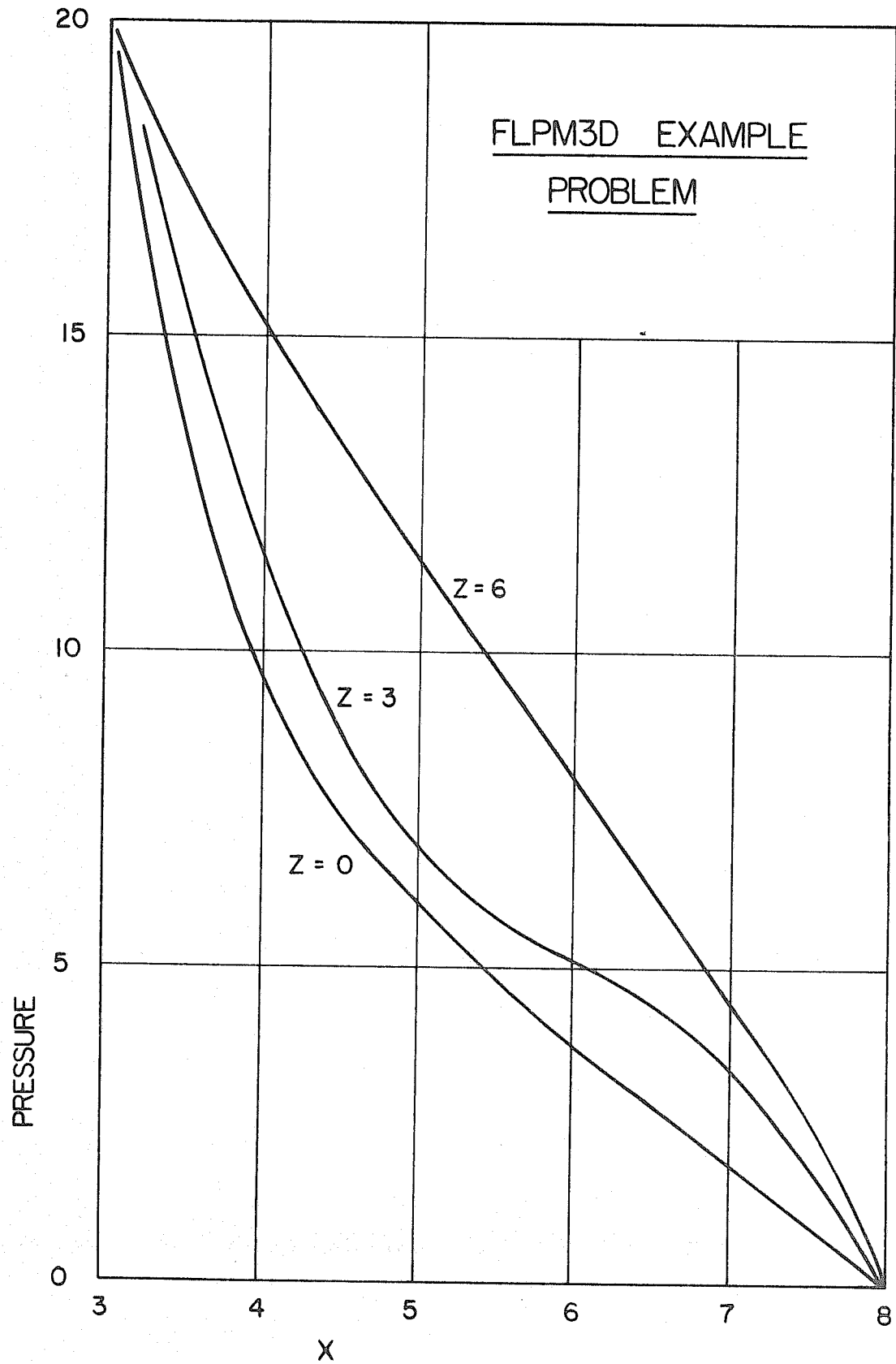


FIG. C-6 PRESSURE ON BASE OF BARRAGE

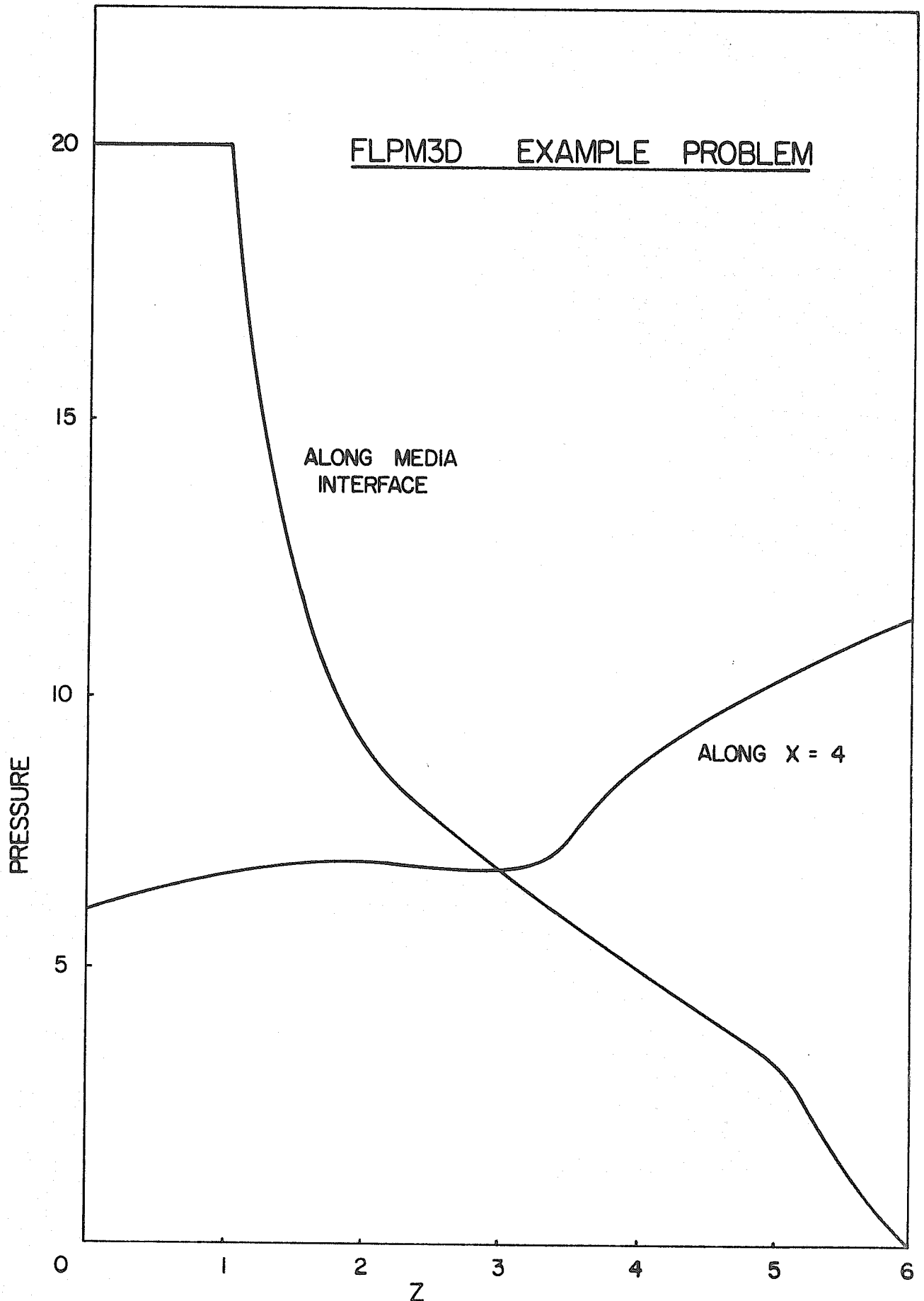


FIG. C-7 PRESSURE ON BASE OF BARRAGE

DATA CARDS PAGE 1
 FLP30 FLOW UNDER DAM SUPPORTED ON TWO MEDIA FOUNDATION

| CARD NO. | COLUMNS | 10 | 15 | 20 | 25 | 30 | 35 | 40 | 45 | 50 | 55 | 60 | 65 | 70 | 75 | 80 |
|----------|---------|-----|-----|-----|-----|-----|----|-----|-----|----|----|----|----|----|----|----|
| 1 | FLP30 | 0 | 0 | 0 | 0 | 1 | 0 | 70 | 1 | | | | | | | |
| 2 | 456 | 300 | 2 | 0 | 0 | 1 | 0 | 70 | | | | | | | | |
| 3 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | | | | | | | | |
| 4 | 0 | 0 | 10 | 10 | 10 | 10 | 10 | | | | | | | | | |
| 5 | 1 | 1 | 10 | 10 | 10 | 10 | 10 | | | | | | | | | |
| 6 | 2 | 1 | 1 | 1 | 1 | 1 | 1 | | | | | | | | | |
| 7 | 1 | 6 | 1 | 0 | 0 | 0 | 0 | | | | | | | | | |
| 8 | 37 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | | 20 | 1 | | | | |
| 9 | 2 | 6 | 1 | 0 | 0 | 0 | 1 | 0 | 0 | | 20 | 1 | | | | |
| 10 | 38 | 1 | 1 | 0 | 0 | 0 | 1 | 0 | 0 | | 21 | 1 | | | | |
| 11 | 3 | 6 | 1 | 0 | 0 | 0 | 2 | 0 | 0 | | 21 | 1 | | | | |
| 12 | 39 | 1 | 1 | 0 | 0 | 0 | 2 | 0 | 0 | | 22 | 1 | | | | |
| 13 | 4 | 6 | 1 | 0 | 0 | 0 | 3 | 0 | 0 | | 22 | 1 | | | | |
| 14 | 4 | 6 | 1 | 0 | 0 | 0 | 3 | 0 | 0 | | 23 | 1 | | | | |
| 15 | 5 | 6 | 1 | 0 | 0 | 0 | 4 | 0 | 0 | | 23 | 1 | | | | |
| 16 | 41 | 1 | 1 | 0 | 0 | 0 | 4 | 0 | 0 | | 24 | 1 | | | | |
| 17 | 6 | 6 | 1 | 0 | 0 | 0 | 5 | 0 | 0 | | 24 | 1 | | | | |
| 18 | 42 | 1 | 1 | 0 | 0 | 0 | 5 | 0 | 0 | | 25 | 1 | | | | |
| 19 | 43 | 6 | 1 | 0 | 0 | 0 | 5 | 0 | 0 | | 25 | 1 | | | | |
| 20 | 79 | 1 | 1 | 1 | 1 | 1 | 0 | 0 | 0 | | 20 | 1 | | | | |
| 21 | 44 | 6 | 1 | 1 | 1 | 1 | 0 | 0 | 0 | | 20 | 1 | | | | |
| 22 | 8 | 6 | 1 | 1 | 1 | 1 | 1 | 0 | 0 | | 20 | 1 | | | | |
| 23 | 45 | 6 | 1 | 1 | 1 | 1 | 2 | 0 | 0 | | 20 | 1 | | | | |
| 24 | 81 | 6 | 1 | 1 | 1 | 1 | 2 | 0 | 0 | | 20 | 1 | | | | |
| 25 | 46 | 6 | 1 | 1 | 1 | 1 | 3 | 0 | 0 | | 20 | 1 | | | | |
| 26 | 82 | 1 | 1 | 1 | 1 | 1 | 3 | 0 | 0 | | 20 | 1 | | | | |
| 27 | 47 | 6 | 1 | 1 | 1 | 1 | 4 | 0 | 0 | | 20 | 1 | | | | |
| 28 | 83 | 6 | 1 | 1 | 1 | 1 | 4 | 0 | 0 | | 20 | 1 | | | | |
| 29 | 48 | 6 | 1 | 1 | 1 | 1 | 5 | 0 | 0 | | 20 | 1 | | | | |
| 30 | 84 | 1 | 1 | 1 | 1 | 1 | 5 | 0 | 0 | | 20 | 1 | | | | |
| 31 | 85 | 1 | 1 | 1.5 | 1.5 | 1.5 | 0 | 0.5 | 0.5 | | 20 | 1 | | | | |
| 32 | 90 | 1 | 1.5 | 1.5 | 1.5 | 1.5 | 5 | 0.5 | 0.5 | | 20 | 1 | | | | |
| 33 | 91 | 6 | 1 | 2 | 2 | 2 | 0 | 0 | 0 | | 20 | 1 | | | | |
| 34 | 127 | 6 | 1 | 2 | 2 | 2 | 0 | 0 | 0 | | 20 | 1 | | | | |
| 35 | 92 | 6 | 6 | 2 | 2 | 2 | 1 | 0 | 0 | | 20 | 1 | | | | |

1 5 10 15 20 25 30 35 40 45 50 55 60 65 70 75 80
 COLUMNS

DATA CARDS PAGE 2
 FLOW UNDER DAM SUPPORTED ON TWO MEDIA FOUNDATION

| CARD NO. | COLUMNS | 1 | 5 | 10 | 15 | 20 | 25 | 30 | 35 | 40 | 45 | 50 | 55 | 60 | 65 | 70 | 75 | 80 |
|----------|---------|---|---|----|----|----|-----|----|----|----|-----|----|----|----|----|----|----|----|
| 36 | 128 | . | . | . | . | . | 2. | . | 1. | . | . | . | . | . | . | . | . | . |
| 37 | 93 | 6 | . | . | . | . | 2. | . | 2. | . | 6. | . | . | . | . | . | . | . |
| 38 | 129 | . | . | . | . | . | 2. | . | 2. | . | 6. | . | . | . | . | . | . | . |
| 39 | 94 | 6 | . | . | . | . | 2. | . | 3. | . | 6. | . | . | . | . | . | . | . |
| 40 | 130 | 6 | . | . | . | . | 2. | . | 3. | . | 6. | . | . | . | . | . | . | . |
| 41 | 95 | 6 | . | . | . | . | 2. | . | 4. | . | 6. | . | . | . | . | . | . | . |
| 42 | 131 | 6 | . | . | . | . | 2. | . | 4. | . | 6. | . | . | . | . | . | . | . |
| 43 | 96 | . | . | . | . | . | 2. | . | 5. | . | 6. | . | . | . | . | . | . | . |
| 44 | 132 | . | . | . | . | . | 2. | . | 5. | . | 6. | . | . | . | . | . | . | . |
| 45 | 133 | . | . | . | . | . | 2.5 | . | 5. | . | 6. | . | . | . | . | . | . | . |
| 46 | 138 | . | . | . | . | . | 2.5 | . | 5. | . | 1.5 | . | . | . | . | . | . | . |
| 47 | 139 | 6 | . | . | . | . | 3. | . | 5. | . | 1.5 | . | . | . | . | . | . | . |
| 48 | 175 | 6 | . | . | . | . | 3. | . | 5. | . | 6. | . | . | . | . | . | . | . |
| 49 | 14 | 6 | . | . | . | . | 3. | . | 5. | . | 6. | . | . | . | . | . | . | . |
| 50 | 176 | 6 | . | . | . | . | 3. | . | 1. | . | 6. | . | . | . | . | . | . | . |
| 51 | 141 | 6 | . | . | . | . | 3. | . | 1. | . | 6. | . | . | . | . | . | . | . |
| 52 | 177 | 6 | . | . | . | . | 3. | . | 2. | . | 6. | . | . | . | . | . | . | . |
| 53 | 142 | 6 | . | . | . | . | 3. | . | 2. | . | 6. | . | . | . | . | . | . | . |
| 54 | 178 | 6 | . | . | . | . | 3. | . | 3. | . | 6. | . | . | . | . | . | . | . |
| 55 | 143 | 6 | . | . | . | . | 3. | . | 3. | . | 6. | . | . | . | . | . | . | . |
| 56 | 179 | 6 | . | . | . | . | 3. | . | 4. | . | 6. | . | . | . | . | . | . | . |
| 57 | 144 | 6 | . | . | . | . | 3. | . | 4. | . | 6. | . | . | . | . | . | . | . |
| 58 | 180 | . | . | . | . | . | 3. | . | 5. | . | 6. | . | . | . | . | . | . | . |
| 59 | 181 | . | . | . | . | . | 3. | . | 5. | . | 6. | . | . | . | . | . | . | . |
| 60 | 186 | . | . | . | . | . | 3.5 | . | 5. | . | 2.5 | . | . | . | . | . | . | . |
| 61 | 187 | 6 | . | . | . | . | 3.5 | . | 5. | . | 2.5 | . | . | . | . | . | . | . |
| 62 | 223 | . | . | . | . | . | 4. | . | 5. | . | 6. | . | . | . | . | . | . | . |
| 63 | 188 | 6 | . | . | . | . | 4. | . | 5. | . | 6. | . | . | . | . | . | . | . |
| 64 | 224 | 6 | . | . | . | . | 4. | . | 1. | . | 6. | . | . | . | . | . | . | . |
| 65 | 189 | 6 | . | . | . | . | 4. | . | 1. | . | 6. | . | . | . | . | . | . | . |
| 66 | 225 | 6 | . | . | . | . | 4. | . | 2. | . | 6. | . | . | . | . | . | . | . |
| 67 | 190 | 6 | . | . | . | . | 4. | . | 2. | . | 6. | . | . | . | . | . | . | . |
| 68 | 226 | . | . | . | . | . | 4. | . | 3. | . | 6. | . | . | . | . | . | . | . |
| 69 | 191 | 6 | . | . | . | . | 4. | . | 3. | . | 6. | . | . | . | . | . | . | . |
| 70 | 227 | 6 | . | . | . | . | 4. | . | 4. | . | 6. | . | . | . | . | . | . | . |

DATA CARDS PAGE 3
 FLPM30 FLOW UNDER DAM SUPPORTED ON TWO MEDIA FOUNDATION

| CARD NO. | 1 | 5 | 10 | 15 | 20 | 25 | 30 | 35 | 40 | 45 | 50 | 55 | 60 | 65 | 70 | 75 | 80 |
|----------|-----|---|----|----|----|----|----|----|----|-----|----|----|----|----|----|----|----|
| 71 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 72 | 192 | 6 | | | 4 | | | 5 | | | | | | | | | |
| 73 | 228 | | | | 4 | | | 5 | | 6 | | | | | | | |
| 74 | 229 | | | | 4 | | | 0 | | 3.5 | | | | | | | |
| 75 | 234 | | | | 4 | | | 0 | | 3.5 | | | | | | | |
| 76 | 235 | | 6 | | | 5 | | 0 | | 0 | | | | | | | |
| 77 | 271 | | 6 | | | 5 | | 0 | | 6 | | | | | | | |
| 78 | 236 | | 6 | | | 5 | | 1 | | 0 | | | | | | | |
| 79 | 272 | | 6 | | | 5 | | 1 | | 6 | | | | | | | |
| 80 | 237 | | 6 | | | 5 | | 2 | | 0 | | | | | | | |
| 81 | 273 | | 6 | | | 5 | | 2 | | 0 | | | | | | | |
| 82 | 238 | | 6 | | | 5 | | 3 | | 0 | | | | | | | |
| 83 | 274 | | 6 | | | 5 | | 3 | | 0 | | | | | | | |
| 84 | 239 | | 6 | | | 5 | | 4 | | 0 | | | | | | | |
| 85 | 275 | | 6 | | | 5 | | 4 | | 6 | | | | | | | |
| 86 | 240 | | 6 | | | 5 | | 5 | | 0 | | | | | | | |
| 87 | 276 | | 6 | | | 5 | | 5 | | 6 | | | | | | | |
| 88 | 277 | | 6 | | | 5 | | 0 | | 6 | | | | | | | |
| 89 | 282 | | 6 | | | 5 | | 5 | | 4.5 | | | | | | | |
| 90 | 283 | | 6 | | | 6 | | 0 | | 4.5 | | | | | | | |
| 91 | 319 | | 6 | | | 6 | | 0 | | 0 | | | | | | | |
| 92 | 284 | | 6 | | | 6 | | 1 | | 0 | | | | | | | |
| 93 | 320 | | 6 | | | 6 | | 1 | | 0 | | | | | | | |
| 94 | 285 | | 6 | | | 6 | | 2 | | 0 | | | | | | | |
| 95 | 321 | | 6 | | | 6 | | 2 | | 0 | | | | | | | |
| 96 | 286 | | 6 | | | 6 | | 3 | | 0 | | | | | | | |
| 97 | 322 | | 6 | | | 6 | | 3 | | 6 | | | | | | | |
| 98 | 287 | | 6 | | | 6 | | 4 | | 0 | | | | | | | |
| 99 | 323 | | 6 | | | 6 | | 4 | | 0 | | | | | | | |
| 100 | 288 | | 6 | | | 6 | | 5 | | 0 | | | | | | | |
| 101 | 324 | | 6 | | | 6 | | 5 | | 0 | | | | | | | |
| 102 | 325 | | 6 | | | 6 | | 0 | | 6.5 | | | | | | | |
| 103 | 330 | | 6 | | | 6 | | 5 | | 5.5 | | | | | | | |
| 104 | 331 | | 6 | 1 | | 7 | | 0 | | 0 | | 0 | 1 | | | | |
| 105 | 367 | | 6 | 1 | | 7 | | 0 | | 6 | | 0 | | | | | |
| 105 | 332 | | 6 | | | 7 | | 1 | | 0 | | | | | | | |

! C10 !

COLUMNS

DATA CARDS PAGE 4
 FLP130 FLOW UNDER DAM SUPPORTED ON TWO MEDIA FOUNDATION

| CARD NO. | COLUMNS | 1 | 5 | 10 | 15 | 20 | 25 | 30 | 35 | 40 | 45 | 50 | 55 | 60 | 65 | 70 | 75 | 80 |
|----------|---------|-----|-----|-----|-----|-----|-----|-----|----|----|----|----|----|----|-----|-----|----|----|
| 106 | 368 | . | . | . | . | . | . | . | . | . | . | . | . | . | . | . | . | . |
| 107 | 333 | 6 | . | . | 7. | . | . | . | 1. | . | 6. | . | . | . | . | . | . | . |
| 108 | 369 | 6 | . | . | 7. | . | . | . | 2. | . | 6. | . | . | . | . | . | . | . |
| 109 | 334 | 6 | . | . | 7. | . | . | . | 2. | . | 6. | . | . | . | . | . | . | . |
| 110 | 370 | 6 | . | . | 7. | . | . | . | 3. | . | 6. | . | . | . | . | . | . | . |
| 111 | 335 | 6 | . | . | 7. | . | . | . | 3. | . | 6. | . | . | . | . | . | . | . |
| 112 | 371 | 6 | . | . | 7. | . | . | . | 4. | . | 6. | . | . | . | . | . | . | . |
| 113 | 336 | 6 | . | . | 7. | . | . | . | 4. | . | 6. | . | . | . | . | . | . | . |
| 114 | 372 | 6 | . | . | 7. | . | . | . | 5. | . | 6. | . | . | . | . | . | . | . |
| 115 | 373 | 6 | 1 | . | 7. | . | . | . | 5. | . | 6. | . | . | . | . | . | . | . |
| 116 | 409 | 6 | 1 | . | 8. | . | . | . | 0. | . | 6. | . | . | . | . | . | . | . |
| 117 | 374 | 6 | . | . | 8. | . | . | . | 0. | . | 6. | . | . | . | . | . | . | . |
| 118 | 410 | 6 | . | . | 8. | . | . | . | 0. | . | 6. | . | . | . | . | . | . | . |
| 119 | 375 | 6 | . | . | 8. | . | . | . | 1. | . | 6. | . | . | . | . | . | . | . |
| 120 | 411 | 6 | . | . | 8. | . | . | . | 1. | . | 6. | . | . | . | . | . | . | . |
| 121 | 376 | 6 | . | . | 8. | . | . | . | 2. | . | 6. | . | . | . | . | . | . | . |
| 122 | 412 | 6 | . | . | 8. | . | . | . | 2. | . | 6. | . | . | . | . | . | . | . |
| 123 | 377 | 6 | . | . | 8. | . | . | . | 3. | . | 6. | . | . | . | . | . | . | . |
| 124 | 413 | 6 | . | . | 8. | . | . | . | 3. | . | 6. | . | . | . | . | . | . | . |
| 125 | 378 | 6 | . | . | 8. | . | . | . | 4. | . | 6. | . | . | . | . | . | . | . |
| 126 | 414 | 6 | . | . | 8. | . | . | . | 4. | . | 6. | . | . | . | . | . | . | . |
| 127 | 415 | 6 | . | . | 8. | . | . | . | 5. | . | 6. | . | . | . | . | . | . | . |
| 128 | 451 | 6 | 1 | . | 9. | . | . | . | 0. | . | 6. | . | . | . | . | . | . | . |
| 129 | 416 | 6 | 1 | . | 9. | . | . | . | 0. | . | 6. | . | . | . | . | . | . | . |
| 130 | 452 | 6 | 1 | . | 9. | . | . | . | 1. | . | 6. | . | . | . | . | . | . | . |
| 131 | 417 | 6 | 1 | . | 9. | . | . | . | 1. | . | 6. | . | . | . | . | . | . | . |
| 132 | 453 | 6 | 1 | . | 9. | . | . | . | 2. | . | 6. | . | . | . | . | . | . | . |
| 133 | 418 | 6 | 1 | . | 9. | . | . | . | 2. | . | 6. | . | . | . | . | . | . | . |
| 134 | 454 | 6 | 1 | . | 9. | . | . | . | 3. | . | 6. | . | . | . | . | . | . | . |
| 135 | 419 | 6 | 1 | . | 9. | . | . | . | 3. | . | 6. | . | . | . | . | . | . | . |
| 136 | 455 | 6 | 1 | . | 9. | . | . | . | 4. | . | 6. | . | . | . | . | . | . | . |
| 137 | 420 | 6 | 1 | . | 9. | . | . | . | 4. | . | 6. | . | . | . | . | . | . | . |
| 138 | 456 | 6 | 1 | . | 9. | . | . | . | 5. | . | 6. | . | . | . | . | . | . | . |
| 139 | 416 | 415 | 422 | 421 | 380 | 379 | 374 | 373 | 5. | 1 | 6. | 1 | 1 | 6 | -29 | -76 | 6 | 30 |
| 140 | 332 | 331 | 338 | 337 | 290 | 289 | 284 | 283 | 5. | 1 | 6. | 1 | 1 | 6 | -23 | 5 | 70 | 80 |
| 141 | 5 | 10 | 15 | 20 | 25 | 30 | 35 | 40 | 45 | 50 | 55 | 60 | 65 | 70 | 75 | 80 | | |

DATA CARDS PAGE 5
 FLPM30 FLOW UNDER DAM SUPPORTED ON TWO MEDIA FOUNDATION

| CARD NO. | 1 | 5 | 10 | 15 | 20 | 25 | 30 | 35 | 40 | 45 | 50 | 55 | 60 | 65 | 70 | 75 | 80 |
|----------|-----|-----|-----|-----|-----|-----|-----|-----|-----|----|----|----|-----|----|----|----|----|
| 141 | 86 | 284 | 283 | 290 | 289 | 242 | 241 | 236 | 235 | . | . | . | . | . | . | . | . |
| 142 | 126 | 236 | 235 | 242 | 241 | 194 | 193 | 188 | 187 | . | . | 6 | -17 | . | . | . | . |
| 143 | 121 | 188 | 187 | 194 | 193 | 146 | 145 | 140 | 139 | . | . | 6 | -11 | . | 4 | . | . |
| 144 | 131 | 140 | 139 | 146 | 145 | 98 | 97 | 92 | 91 | . | . | 6 | -5 | . | 3 | . | . |
| 145 | 136 | 92 | 91 | 98 | 97 | 86 | 85 | 44 | 43 | . | . | . | . | . | 2 | . | . |
| 146 | 141 | 146 | 145 | 152 | 151 | 134 | 133 | 98 | 97 | . | . | . | . | . | . | . | . |
| 147 | 146 | 200 | 199 | 206 | 205 | 182 | 181 | 152 | 151 | . | . | . | . | . | . | . | . |
| 148 | 151 | 254 | 253 | 260 | 259 | 230 | 229 | 206 | 205 | . | . | . | . | . | . | . | . |
| 149 | 156 | 308 | 307 | 314 | 313 | 278 | 277 | 260 | 259 | . | . | . | . | . | . | . | . |
| 150 | 161 | 362 | 361 | 368 | 367 | 326 | 325 | 314 | 313 | . | . | . | . | . | . | . | . |
| 151 | 166 | 86 | 85 | 98 | 97 | 50 | 49 | 44 | 43 | . | . | . | . | . | . | . | . |
| 152 | 171 | 134 | 133 | 152 | 151 | 104 | 103 | 98 | 97 | . | . | . | . | . | . | . | . |
| 153 | 176 | 182 | 181 | 206 | 205 | 158 | 157 | 152 | 151 | . | . | . | . | . | . | . | . |
| 154 | 181 | 230 | 229 | 260 | 259 | 212 | 211 | 206 | 205 | . | . | . | . | . | . | . | . |
| 155 | 186 | 278 | 277 | 314 | 313 | 266 | 265 | 260 | 259 | . | . | . | . | . | . | . | . |
| 156 | 191 | 326 | 325 | 368 | 367 | 320 | 319 | 314 | 313 | . | . | . | . | . | . | . | . |
| 157 | 196 | 44 | 43 | 50 | 49 | 8 | 7 | 2 | 1 | . | . | 6 | -29 | . | 6 | . | . |
| 158 | 226 | 98 | 97 | 104 | 103 | 56 | 55 | 50 | 49 | . | . | 6 | -23 | . | 5 | . | . |
| 159 | 251 | 152 | 151 | 158 | 157 | 110 | 109 | 104 | 103 | . | . | 6 | -17 | . | 4 | . | . |
| 160 | 271 | 206 | 205 | 212 | 211 | 164 | 163 | 158 | 157 | . | . | 6 | -11 | . | 3 | . | . |
| 161 | 286 | 260 | 259 | 266 | 265 | 218 | 217 | 212 | 211 | . | . | 6 | -5 | . | 2 | . | . |
| 162 | 296 | 314 | 313 | 320 | 319 | 272 | 271 | 266 | 265 | . | . | . | . | . | . | . | . |
| 163 | 300 | 318 | 317 | 324 | 323 | 276 | 275 | 270 | 269 | . | . | . | . | . | . | . | . |

F1 PM3D FLOW UNDER DAM SUPPORTED ON TWO MEDIA FOUNDATION

| | |
|--|---------|
| NUMBER OF NODAL POINTS | 456 |
| NUMBER OF ELEMENTS | 300 |
| NUMBER OF MATERIALS | 2 |
| NUMBER OF SURFACE FLOW TYPES | 0 |
| NUMBER OF SETS OF DIRECTION RATIOS | 0 |
| NUMBER OF LOADING CASES | 1 |
| ELEMENT VELOCITY OPTION | 0 |
| LIMIT ON ALLOWABLE HALF BAND WIDTH | 70 |
| NUMBER OF ELEMENT STORAGE BLOCKS | 1 |
| CONSTANT ACCELERATION IN X DIRECTION | 0. |
| CONSTANT ACCELERATION IN Y DIRECTION | 0. |
| CONSTANT ACCELERATION IN Z DIRECTION | 1.00000 |
| ACCELERATION DUE TO GRAVITY | 1.00000 |
| UNIT WEIGHT OF FLUID | 1.00000 |
| | |
| LOAD CASE | 1 |
| NUMBER OF NODES WITH PRESCRIBED FLOW | 0 |
| NUMBER OF ELEMENT FACES WITH PRESCRIBED SURFACE FLOWS | 0 |

| MATERIAL TYPE | PRINCIPAL PERMEABILITIES | | |
|------------------|--------------------------|------------|------------|
| | I | II | III |
| 1 | .10000E+02 | .10000E+02 | .10000E+02 |
| 2 | .10000E+01 | .10000E+01 | .10000E+01 |

FI PM3D FLOW UNDER DAM SUPPORTED ON TWO MEDIA FOUNDATION

| NODE | GLOBAL COORDINATES | | | PRESCRIBED |
|------|--------------------|---------|---------|------------|
| | X | Y | Z | PRESSURES |
| 1 | 0. | 0. | 0. | 20.00000 |
| 2 | 0. | 1.00000 | 0. | 21.00000 |
| 3 | 0. | 2.00000 | 0. | 22.00000 |
| 4 | 0. | 3.00000 | 0. | 23.00000 |
| 5 | 0. | 4.00000 | 0. | 24.00000 |
| 6 | 0. | 5.00000 | 0. | 25.00000 |
| 7 | 0. | 0. | 1.00000 | 20.00000 |
| 8 | 0. | 1.00000 | 1.00000 | 21.00000 |
| 9 | 0. | 2.00000 | 1.00000 | 22.00000 |
| 10 | 0. | 3.00000 | 1.00000 | 23.00000 |
| 11 | 0. | 4.00000 | 1.00000 | 24.00000 |
| 12 | 0. | 5.00000 | 1.00000 | 25.00000 |
| 13 | 0. | 0. | 2.00000 | 20.00000 |
| 14 | 0. | 1.00000 | 2.00000 | 21.00000 |
| 15 | 0. | 2.00000 | 2.00000 | 22.00000 |
| 16 | 0. | 3.00000 | 2.00000 | 23.00000 |
| 17 | 0. | 4.00000 | 2.00000 | 24.00000 |
| 18 | 0. | 5.00000 | 2.00000 | 25.00000 |
| 19 | 0. | 0. | 3.00000 | 20.00000 |
| 20 | 0. | 1.00000 | 3.00000 | 21.00000 |
| 21 | 0. | 2.00000 | 3.00000 | 22.00000 |
| 22 | 0. | 3.00000 | 3.00000 | 23.00000 |
| 23 | 0. | 4.00000 | 3.00000 | 24.00000 |
| 24 | 0. | 5.00000 | 3.00000 | 25.00000 |
| 25 | 0. | 0. | 4.00000 | 20.00000 |
| 26 | 0. | 1.00000 | 4.00000 | 21.00000 |
| 27 | 0. | 2.00000 | 4.00000 | 22.00000 |
| 28 | 0. | 3.00000 | 4.00000 | 23.00000 |
| 29 | 0. | 4.00000 | 4.00000 | 24.00000 |
| 30 | 0. | 5.00000 | 4.00000 | 25.00000 |
| 31 | 0. | 0. | 5.00000 | 20.00000 |
| 32 | 0. | 1.00000 | 5.00000 | 21.00000 |
| 33 | 0. | 2.00000 | 5.00000 | 22.00000 |
| 34 | 0. | 3.00000 | 5.00000 | 23.00000 |
| 35 | 0. | 4.00000 | 5.00000 | 24.00000 |
| 36 | 0. | 5.00000 | 5.00000 | 25.00000 |
| 37 | 0. | 0. | 6.00000 | 20.00000 |
| 38 | 0. | 1.00000 | 6.00000 | 21.00000 |
| 39 | 0. | 2.00000 | 6.00000 | 22.00000 |
| 40 | 0. | 3.00000 | 6.00000 | 23.00000 |

FI PM3D FLOW UNDER DAM SUPPORTED ON TWO MEDIA FOUNDATION

| NO-E | GLOBAL COORDINATES | | | PRESCRIBED PRESSURES |
|------|--------------------|----------|----------|----------------------|
| | X | Y | Z | |
| 41 | 0. | 4.000000 | 6.000000 | 24.00000 |
| 42 | 0. | 5.000000 | 6.000000 | 25.00000 |
| 43 | 1.000000 | 0. | 0. | 20.00000 |
| 44 | 1.000000 | 1.000000 | 0. | |
| 45 | 1.000000 | 2.000000 | 0. | |
| 46 | 1.000000 | 3.000000 | 0. | |
| 47 | 1.000000 | 4.000000 | 0. | |
| 48 | 1.000000 | 5.000000 | 0. | |
| 49 | 1.000000 | 0. | 1.000000 | 20.00000 |
| 50 | 1.000000 | 1.000000 | 1.000000 | |
| 51 | 1.000000 | 2.000000 | 1.000000 | |
| 52 | 1.000000 | 3.000000 | 1.000000 | |
| 53 | 1.000000 | 4.000000 | 1.000000 | |
| 54 | 1.000000 | 5.000000 | 1.000000 | |
| 55 | 1.000000 | 0. | 2.000000 | 20.00000 |
| 56 | 1.000000 | 1.000000 | 2.000000 | |
| 57 | 1.000000 | 2.000000 | 2.000000 | |
| 58 | 1.000000 | 3.000000 | 2.000000 | |
| 59 | 1.000000 | 4.000000 | 2.000000 | |
| 60 | 1.000000 | 5.000000 | 2.000000 | |
| 61 | 1.000000 | 0. | 3.000000 | 20.00000 |
| 62 | 1.000000 | 1.000000 | 3.000000 | |
| 63 | 1.000000 | 2.000000 | 3.000000 | |
| 64 | 1.000000 | 3.000000 | 3.000000 | |
| 65 | 1.000000 | 4.000000 | 3.000000 | |
| 66 | 1.000000 | 5.000000 | 3.000000 | |
| 67 | 1.000000 | 0. | 4.000000 | 20.00000 |
| 68 | 1.000000 | 1.000000 | 4.000000 | |
| 69 | 1.000000 | 2.000000 | 4.000000 | |
| 70 | 1.000000 | 3.000000 | 4.000000 | |
| 71 | 1.000000 | 4.000000 | 4.000000 | |
| 72 | 1.000000 | 5.000000 | 4.000000 | |
| 73 | 1.000000 | 0. | 5.000000 | 20.00000 |
| 74 | 1.000000 | 1.000000 | 5.000000 | |
| 75 | 1.000000 | 2.000000 | 5.000000 | |
| 76 | 1.000000 | 3.000000 | 5.000000 | |
| 77 | 1.000000 | 4.000000 | 5.000000 | |
| 78 | 1.000000 | 5.000000 | 5.000000 | |
| 79 | 1.000000 | 0. | 6.000000 | 20.00000 |
| 80 | 1.000000 | 1.000000 | 6.000000 | |

FIPM3D FLOW UNDER DAM SUPPORTED ON TWO MEDIA FOUNDATION

| NODE | GLOBAL COORDINATES | | | PRESCRIBED PRESSURES |
|------|--------------------|---------|---------|----------------------|
| | X | Y | Z | |
| 81 | 1.00000 | 2.00000 | 6.00000 | |
| 82 | 1.00000 | 3.00000 | 6.00000 | |
| 83 | 1.00000 | 4.00000 | 6.00000 | |
| 84 | 1.00000 | 5.00000 | 6.00000 | |
| 85 | 1.50000 | 0. | .50000 | 20.00000 |
| 86 | 1.50000 | 1.00000 | .50000 | |
| 87 | 1.50000 | 2.00000 | .50000 | |
| 88 | 1.50000 | 3.00000 | .50000 | |
| 89 | 1.50000 | 4.00000 | .50000 | |
| 90 | 1.50000 | 5.00000 | .50000 | |
| 91 | 2.00000 | 0. | 0. | 20.00000 |
| 92 | 2.00000 | 1.00000 | 0. | |
| 93 | 2.00000 | 2.00000 | 0. | |
| 94 | 2.00000 | 3.00000 | 0. | |
| 95 | 2.00000 | 4.00000 | 0. | |
| 96 | 2.00000 | 5.00000 | 0. | |
| 97 | 2.00000 | 0. | 1.00000 | 20.00000 |
| 98 | 2.00000 | 1.00000 | 1.00000 | |
| 99 | 2.00000 | 2.00000 | 1.00000 | |
| 100 | 2.00000 | 3.00000 | 1.00000 | |
| 101 | 2.00000 | 4.00000 | 1.00000 | |
| 102 | 2.00000 | 5.00000 | 1.00000 | |
| 103 | 2.00000 | 0. | 2.00000 | 20.00000 |
| 104 | 2.00000 | 1.00000 | 2.00000 | |
| 105 | 2.00000 | 2.00000 | 2.00000 | |
| 106 | 2.00000 | 3.00000 | 2.00000 | |
| 107 | 2.00000 | 4.00000 | 2.00000 | |
| 108 | 2.00000 | 5.00000 | 2.00000 | |
| 109 | 2.00000 | 0. | 3.00000 | 20.00000 |
| 110 | 2.00000 | 1.00000 | 3.00000 | |
| 111 | 2.00000 | 2.00000 | 3.00000 | |
| 112 | 2.00000 | 3.00000 | 3.00000 | |
| 113 | 2.00000 | 4.00000 | 3.00000 | |
| 114 | 2.00000 | 5.00000 | 3.00000 | |
| 115 | 2.00000 | 0. | 4.00000 | 20.00000 |
| 116 | 2.00000 | 1.00000 | 4.00000 | |
| 117 | 2.00000 | 2.00000 | 4.00000 | |
| 118 | 2.00000 | 3.00000 | 4.00000 | |
| 119 | 2.00000 | 4.00000 | 4.00000 | |
| 120 | 2.00000 | 5.00000 | 4.00000 | |

FI PM30 FLOW UNDER DAM SUPPORTED ON TWO MEDIA FOUNDATION

| NO. E | GLOBAL COORDINATES | | | PRESCRIBED PRESSURES |
|-------|--------------------|----------|----------|----------------------|
| | X | Y | Z | |
| 121 | 2.000000 | 0. | 5.000000 | 20.00000 |
| 122 | 2.000000 | 1.000000 | 5.000000 | |
| 123 | 2.000000 | 2.000000 | 5.000000 | 20.00000 |
| 124 | 2.000000 | 3.000000 | 5.000000 | |
| 125 | 2.000000 | 4.000000 | 5.000000 | |
| 126 | 2.000000 | 5.000000 | 5.000000 | |
| 127 | 2.000000 | 0. | 6.000000 | |
| 128 | 2.000000 | 1.000000 | 6.000000 | |
| 129 | 2.000000 | 2.000000 | 6.000000 | |
| 130 | 2.000000 | 3.000000 | 6.000000 | |
| 131 | 2.000000 | 4.000000 | 6.000000 | |
| 132 | 2.000000 | 5.000000 | 6.000000 | |
| 133 | 2.500000 | 0. | 1.500000 | 20.00000 |
| 134 | 2.500000 | 1.000000 | 1.500000 | |
| 135 | 2.500000 | 2.000000 | 1.500000 | |
| 136 | 2.500000 | 3.000000 | 1.500000 | |
| 137 | 2.500000 | 4.000000 | 1.500000 | |
| 138 | 2.500000 | 5.000000 | 1.500000 | |
| 139 | 3.000000 | 0. | 0. | |
| 140 | 3.000000 | 1.000000 | 0. | |
| 141 | 3.000000 | 2.000000 | 0. | |
| 142 | 3.000000 | 3.000000 | 0. | |
| 143 | 3.000000 | 4.000000 | 0. | |
| 144 | 3.000000 | 5.000000 | 0. | |
| 145 | 3.000000 | 0. | 1.000000 | 20.00000 |
| 146 | 3.000000 | 1.000000 | 1.000000 | |
| 147 | 3.000000 | 2.000000 | 1.000000 | |
| 148 | 3.000000 | 3.000000 | 1.000000 | |
| 149 | 3.000000 | 4.000000 | 1.000000 | |
| 150 | 3.000000 | 5.000000 | 1.000000 | |
| 151 | 3.000000 | 0. | 2.000000 | |
| 152 | 3.000000 | 1.000000 | 2.000000 | |
| 153 | 3.000000 | 2.000000 | 2.000000 | |
| 154 | 3.000000 | 3.000000 | 2.000000 | |
| 155 | 3.000000 | 4.000000 | 2.000000 | |
| 156 | 3.000000 | 5.000000 | 2.000000 | |
| 157 | 3.000000 | 0. | 3.000000 | 20.00000 |
| 158 | 3.000000 | 1.000000 | 3.000000 | |
| 159 | 3.000000 | 2.000000 | 3.000000 | |
| 160 | 3.000000 | 3.000000 | 3.000000 | |

FIPM3D FLOW UNDER DAM SUPPORTED ON TWO MEDIA FOUNDATION

| NODE | GLOBAL COORDINATES | | | PRESCRIBED PRESSURES |
|------|--------------------|----------|----------|----------------------|
| | X | Y | Z | |
| 161 | 3.000000 | 4.000000 | 3.000000 | |
| 162 | 3.000000 | 5.000000 | 3.000000 | |
| 163 | 3.000000 | 0. | 4.000000 | |
| 164 | 3.000000 | 1.000000 | 4.000000 | |
| 165 | 3.000000 | 2.000000 | 4.000000 | |
| 166 | 3.000000 | 3.000000 | 4.000000 | |
| 167 | 3.000000 | 4.000000 | 4.000000 | |
| 168 | 3.000000 | 5.000000 | 4.000000 | |
| 169 | 3.000000 | 0. | 5.000000 | |
| 170 | 3.000000 | 1.000000 | 5.000000 | |
| 171 | 3.000000 | 2.000000 | 5.000000 | |
| 172 | 3.000000 | 3.000000 | 5.000000 | |
| 173 | 3.000000 | 4.000000 | 5.000000 | |
| 174 | 3.000000 | 5.000000 | 5.000000 | |
| 175 | 3.000000 | 0. | 6.000000 | |
| 176 | 3.000000 | 1.000000 | 6.000000 | |
| 177 | 3.000000 | 2.000000 | 6.000000 | |
| 178 | 3.000000 | 3.000000 | 6.000000 | |
| 179 | 3.000000 | 4.000000 | 6.000000 | |
| 180 | 3.000000 | 5.000000 | 6.000000 | |
| 181 | 3.500000 | 0. | 2.500000 | |
| 182 | 3.500000 | 1.000000 | 2.500000 | |
| 183 | 3.500000 | 2.000000 | 2.500000 | |
| 184 | 3.500000 | 3.000000 | 2.500000 | |
| 185 | 3.500000 | 4.000000 | 2.500000 | |
| 186 | 3.500000 | 5.000000 | 2.500000 | |
| 187 | 4.000000 | 0. | 0. | |
| 188 | 4.000000 | 1.000000 | 0. | |
| 189 | 4.000000 | 2.000000 | 0. | |
| 190 | 4.000000 | 3.000000 | 0. | |
| 191 | 4.000000 | 4.000000 | 0. | |
| 192 | 4.000000 | 5.000000 | 0. | |
| 193 | 4.000000 | 0. | 1.000000 | |
| 194 | 4.000000 | 1.000000 | 1.000000 | |
| 195 | 4.000000 | 2.000000 | 1.000000 | |
| 196 | 4.000000 | 3.000000 | 1.000000 | |
| 197 | 4.000000 | 4.000000 | 1.000000 | |
| 198 | 4.000000 | 5.000000 | 1.000000 | |
| 199 | 4.000000 | 0. | 2.000000 | |
| 200 | 4.000000 | 1.000000 | 2.000000 | |

FI PM3D FLOW UNDER DAM SUPPORTED ON TWO MEDIA FOUNDATION

| NO. E | GLOBAL COORDINATES | | | PRESCRIBED PRESSURES |
|-------|--------------------|----------|----------|----------------------|
| | X | Y | Z | |
| 201 | 4.000000 | 2.000000 | 2.000000 | |
| 202 | 4.000000 | 3.000000 | 2.000000 | |
| 203 | 4.000000 | 4.000000 | 2.000000 | |
| 204 | 4.000000 | 5.000000 | 2.000000 | |
| 205 | 4.000000 | 0. | 3.000000 | |
| 206 | 4.000000 | 1.000000 | 3.000000 | |
| 207 | 4.000000 | 2.000000 | 3.000000 | |
| 208 | 4.000000 | 3.000000 | 3.000000 | |
| 209 | 4.000000 | 4.000000 | 3.000000 | |
| 210 | 4.000000 | 5.000000 | 3.000000 | |
| 211 | 4.000000 | 0. | 4.000000 | |
| 212 | 4.000000 | 1.000000 | 4.000000 | |
| 213 | 4.000000 | 2.000000 | 4.000000 | |
| 214 | 4.000000 | 3.000000 | 4.000000 | |
| 215 | 4.000000 | 4.000000 | 4.000000 | |
| 216 | 4.000000 | 5.000000 | 4.000000 | |
| 217 | 4.000000 | 0. | 5.000000 | |
| 218 | 4.000000 | 1.000000 | 5.000000 | |
| 219 | 4.000000 | 2.000000 | 5.000000 | |
| 220 | 4.000000 | 3.000000 | 5.000000 | |
| 221 | 4.000000 | 4.000000 | 5.000000 | |
| 222 | 4.000000 | 5.000000 | 5.000000 | |
| 223 | 4.000000 | 0. | 6.000000 | |
| 224 | 4.000000 | 1.000000 | 6.000000 | |
| 225 | 4.000000 | 2.000000 | 6.000000 | |
| 226 | 4.000000 | 3.000000 | 6.000000 | |
| 227 | 4.000000 | 4.000000 | 6.000000 | |
| 228 | 4.000000 | 5.000000 | 6.000000 | |
| 229 | 4.500000 | 0. | 3.500000 | |
| 230 | 4.500000 | 1.000000 | 3.500000 | |
| 231 | 4.500000 | 2.000000 | 3.500000 | |
| 232 | 4.500000 | 3.000000 | 3.500000 | |
| 233 | 4.500000 | 4.000000 | 3.500000 | |
| 234 | 4.500000 | 5.000000 | 3.500000 | |
| 235 | 5.000000 | 0. | 0. | |
| 236 | 5.000000 | 1.000000 | 0. | |
| 237 | 5.000000 | 2.000000 | 0. | |
| 238 | 5.000000 | 3.000000 | 0. | |
| 239 | 5.000000 | 4.000000 | 0. | |
| 240 | 5.000000 | 5.000000 | 0. | |

FI PM3D FLOW UNDER DAM SUPPORTED ON TWO MEDIA FOUNDATION

| Node | GLOBAL COORDINATES | | | PRESCRIBED PRESSURES |
|------|--------------------|----------|----------|----------------------|
| | X | Y | Z | |
| 241 | 5.000000 | 0. | 1.000000 | |
| 242 | 5.000000 | 1.000000 | 1.000000 | |
| 243 | 5.000000 | 2.000000 | 1.000000 | |
| 244 | 5.000000 | 3.000000 | 1.000000 | |
| 245 | 5.000000 | 4.000000 | 1.000000 | |
| 246 | 5.000000 | 5.000000 | 1.000000 | |
| 247 | 5.000000 | 0. | 2.000000 | |
| 248 | 5.000000 | 1.000000 | 2.000000 | |
| 249 | 5.000000 | 2.000000 | 2.000000 | |
| 250 | 5.000000 | 3.000000 | 2.000000 | |
| 251 | 5.000000 | 4.000000 | 2.000000 | |
| 252 | 5.000000 | 5.000000 | 2.000000 | |
| 253 | 5.000000 | 0. | 3.000000 | |
| 254 | 5.000000 | 1.000000 | 3.000000 | |
| 255 | 5.000000 | 2.000000 | 3.000000 | |
| 256 | 5.000000 | 3.000000 | 3.000000 | |
| 257 | 5.000000 | 4.000000 | 3.000000 | |
| 258 | 5.000000 | 5.000000 | 3.000000 | |
| 259 | 5.000000 | 0. | 4.000000 | |
| 260 | 5.000000 | 1.000000 | 4.000000 | |
| 261 | 5.000000 | 2.000000 | 4.000000 | |
| 262 | 5.000000 | 3.000000 | 4.000000 | |
| 263 | 5.000000 | 4.000000 | 4.000000 | |
| 264 | 5.000000 | 5.000000 | 4.000000 | |
| 265 | 5.000000 | 0. | 5.000000 | |
| 266 | 5.000000 | 1.000000 | 5.000000 | |
| 267 | 5.000000 | 2.000000 | 5.000000 | |
| 268 | 5.000000 | 3.000000 | 5.000000 | |
| 269 | 5.000000 | 4.000000 | 5.000000 | |
| 270 | 5.000000 | 5.000000 | 5.000000 | |
| 271 | 5.000000 | 0. | 6.000000 | |
| 272 | 5.000000 | 1.000000 | 6.000000 | |
| 273 | 5.000000 | 2.000000 | 6.000000 | |
| 274 | 5.000000 | 3.000000 | 6.000000 | |
| 275 | 5.000000 | 4.000000 | 6.000000 | |
| 276 | 5.000000 | 5.000000 | 6.000000 | |
| 277 | 5.500000 | 0. | 4.500000 | |
| 278 | 5.500000 | 1.000000 | 4.500000 | |
| 279 | 5.500000 | 2.000000 | 4.500000 | |
| 280 | 5.500000 | 3.000000 | 4.500000 | |

FI PM3D FLOW UNDER DAM SUPPORTED ON TWO MEDIA FOUNDATION

| NO. E | GLOBAL COORDINATES | | | PRESCRIBED PRESSURES |
|-------|--------------------|----------|----------|----------------------|
| | X | Y | Z | |
| 281 | 5.500000 | 4.000000 | 4.500000 | |
| 282 | 5.500000 | 5.000000 | 4.500000 | |
| 283 | 6.000000 | 0. | 0. | |
| 284 | 6.000000 | 1.000000 | 0. | |
| 285 | 6.000000 | 2.000000 | 0. | |
| 286 | 6.000000 | 3.000000 | 0. | |
| 287 | 6.000000 | 4.000000 | 0. | |
| 288 | 6.000000 | 5.000000 | 0. | |
| 289 | 6.000000 | 0. | 1.000000 | |
| 290 | 6.000000 | 1.000000 | 1.000000 | |
| 291 | 6.000000 | 2.000000 | 1.000000 | |
| 292 | 6.000000 | 3.000000 | 1.000000 | |
| 293 | 6.000000 | 4.000000 | 1.000000 | |
| 294 | 6.000000 | 5.000000 | 1.000000 | |
| 295 | 6.000000 | 0. | 2.000000 | |
| 296 | 6.000000 | 1.000000 | 2.000000 | |
| 297 | 6.000000 | 2.000000 | 2.000000 | |
| 298 | 6.000000 | 3.000000 | 2.000000 | |
| 299 | 6.000000 | 4.000000 | 2.000000 | |
| 300 | 6.000000 | 5.000000 | 2.000000 | |
| 301 | 6.000000 | 0. | 3.000000 | |
| 302 | 6.000000 | 1.000000 | 3.000000 | |
| 303 | 6.000000 | 2.000000 | 3.000000 | |
| 304 | 6.000000 | 3.000000 | 3.000000 | |
| 305 | 6.000000 | 4.000000 | 3.000000 | |
| 306 | 6.000000 | 5.000000 | 3.000000 | |
| 307 | 6.000000 | 0. | 4.000000 | |
| 308 | 6.000000 | 1.000000 | 4.000000 | |
| 309 | 6.000000 | 2.000000 | 4.000000 | |
| 310 | 6.000000 | 3.000000 | 4.000000 | |
| 311 | 6.000000 | 4.000000 | 4.000000 | |
| 312 | 6.000000 | 5.000000 | 4.000000 | |
| 313 | 6.000000 | 0. | 5.000000 | |
| 314 | 6.000000 | 1.000000 | 5.000000 | |
| 315 | 6.000000 | 2.000000 | 5.000000 | |
| 316 | 6.000000 | 3.000000 | 5.000000 | |
| 317 | 6.000000 | 4.000000 | 5.000000 | |
| 318 | 6.000000 | 5.000000 | 5.000000 | |
| 319 | 6.000000 | 0. | 6.000000 | |
| 320 | 6.000000 | 1.000000 | 6.000000 | |

FIPM3D FLOW UNDER DAM SUPPORTED ON TWO MEDIA FOUNDATION

| NODE | GLOBAL COORDINATES | | | PRESCRIBED PRESSURES |
|------|--------------------|----------|----------|----------------------|
| | X | Y | Z | |
| 321 | 6.000000 | 2.000000 | 6.000000 | |
| 322 | 6.000000 | 3.000000 | 6.000000 | |
| 323 | 6.000000 | 4.000000 | 6.000000 | |
| 324 | 6.000000 | 5.000000 | 6.000000 | |
| 325 | 6.500000 | 0. | 5.500000 | |
| 326 | 6.500000 | 1.000000 | 5.500000 | |
| 327 | 6.500000 | 2.000000 | 5.500000 | |
| 328 | 6.500000 | 3.000000 | 5.500000 | |
| 329 | 6.500000 | 4.000000 | 5.500000 | |
| 330 | 6.500000 | 5.000000 | 5.500000 | |
| 331 | 7.000000 | 0. | 0. | 0. |
| 332 | 7.000000 | 1.000000 | 0. | |
| 333 | 7.000000 | 2.000000 | 0. | |
| 334 | 7.000000 | 3.000000 | 0. | |
| 335 | 7.000000 | 4.000000 | 0. | |
| 336 | 7.000000 | 5.000000 | 0. | |
| 337 | 7.000000 | 0. | 1.000000 | 0. |
| 338 | 7.000000 | 1.000000 | 1.000000 | |
| 339 | 7.000000 | 2.000000 | 1.000000 | |
| 340 | 7.000000 | 3.000000 | 1.000000 | |
| 341 | 7.000000 | 4.000000 | 1.000000 | |
| 342 | 7.000000 | 5.000000 | 1.000000 | |
| 343 | 7.000000 | 0. | 2.000000 | 0. |
| 344 | 7.000000 | 1.000000 | 2.000000 | |
| 345 | 7.000000 | 2.000000 | 2.000000 | |
| 346 | 7.000000 | 3.000000 | 2.000000 | |
| 347 | 7.000000 | 4.000000 | 2.000000 | |
| 348 | 7.000000 | 5.000000 | 2.000000 | |
| 349 | 7.000000 | 0. | 3.000000 | 0. |
| 350 | 7.000000 | 1.000000 | 3.000000 | |
| 351 | 7.000000 | 2.000000 | 3.000000 | |
| 352 | 7.000000 | 3.000000 | 3.000000 | |
| 353 | 7.000000 | 4.000000 | 3.000000 | |
| 354 | 7.000000 | 5.000000 | 3.000000 | |
| 355 | 7.000000 | 0. | 4.000000 | 0. |
| 356 | 7.000000 | 1.000000 | 4.000000 | |
| 357 | 7.000000 | 2.000000 | 4.000000 | |
| 358 | 7.000000 | 3.000000 | 4.000000 | |
| 359 | 7.000000 | 4.000000 | 4.000000 | |
| 360 | 7.000000 | 5.000000 | 4.000000 | |

FIPM3D FLOW UNDER DAM SUPPORTED ON TWO MEDIA FOUNDATION

| NO. E | GLOBAL COORDINATES | | | PRESCRIBED PRESSURES |
|-------|--------------------|----------|----------|----------------------|
| | X | Y | Z | |
| 361 | 7.000000 | 0. | 5.000000 | 0. |
| 362 | 7.000000 | 1.000000 | 5.000000 | |
| 363 | 7.000000 | 2.000000 | 5.000000 | |
| 364 | 7.000000 | 3.000000 | 5.000000 | |
| 365 | 7.000000 | 4.000000 | 5.000000 | |
| 366 | 7.000000 | 5.000000 | 5.000000 | |
| 367 | 7.000000 | 0. | 6.000000 | 0. |
| 368 | 7.000000 | 1.000000 | 6.000000 | |
| 369 | 7.000000 | 2.000000 | 6.000000 | |
| 370 | 7.000000 | 3.000000 | 6.000000 | |
| 371 | 7.000000 | 4.000000 | 6.000000 | |
| 372 | 7.000000 | 5.000000 | 6.000000 | |
| 373 | 8.000000 | 0. | 0. | 0. |
| 374 | 8.000000 | 1.000000 | 0. | |
| 375 | 8.000000 | 2.000000 | 0. | |
| 376 | 8.000000 | 3.000000 | 0. | |
| 377 | 8.000000 | 4.000000 | 0. | |
| 378 | 8.000000 | 5.000000 | 0. | |
| 379 | 8.000000 | 0. | 1.000000 | 0. |
| 380 | 8.000000 | 1.000000 | 1.000000 | |
| 381 | 8.000000 | 2.000000 | 1.000000 | |
| 382 | 8.000000 | 3.000000 | 1.000000 | |
| 383 | 8.000000 | 4.000000 | 1.000000 | |
| 384 | 8.000000 | 5.000000 | 1.000000 | |
| 385 | 8.000000 | 0. | 2.000000 | 0. |
| 386 | 8.000000 | 1.000000 | 2.000000 | |
| 387 | 8.000000 | 2.000000 | 2.000000 | |
| 388 | 8.000000 | 3.000000 | 2.000000 | |
| 389 | 8.000000 | 4.000000 | 2.000000 | |
| 390 | 8.000000 | 5.000000 | 2.000000 | |
| 391 | 8.000000 | 0. | 3.000000 | 0. |
| 392 | 8.000000 | 1.000000 | 3.000000 | |
| 393 | 8.000000 | 2.000000 | 3.000000 | |
| 394 | 8.000000 | 3.000000 | 3.000000 | |
| 395 | 8.000000 | 4.000000 | 3.000000 | |
| 396 | 8.000000 | 5.000000 | 3.000000 | |
| 397 | 8.000000 | 0. | 4.000000 | 0. |
| 398 | 8.000000 | 1.000000 | 4.000000 | |
| 399 | 8.000000 | 2.000000 | 4.000000 | |
| 400 | 8.000000 | 3.000000 | 4.000000 | |

FI PM3D FLOW UNDER DAM SUPPORTED ON TWO MEDIA FOUNDATION

| Node | GLOBAL COORDINATES | | | PRESCRIBED PRESSURES |
|------|--------------------|----------|----------|----------------------|
| | X | Y | Z | |
| 401 | 8.000000 | 4.000000 | 4.000000 | |
| 402 | 8.000000 | 5.000000 | 4.000000 | |
| 403 | 8.000000 | 0. | 5.000000 | 0. |
| 404 | 8.000000 | 1.000000 | 5.000000 | |
| 405 | 8.000000 | 2.000000 | 5.000000 | |
| 406 | 8.000000 | 3.000000 | 5.000000 | |
| 407 | 8.000000 | 4.000000 | 5.000000 | |
| 408 | 8.000000 | 5.000000 | 5.000000 | |
| 409 | 8.000000 | 0. | 6.000000 | 0. |
| 410 | 8.000000 | 1.000000 | 6.000000 | |
| 411 | 8.000000 | 2.000000 | 6.000000 | |
| 412 | 8.000000 | 3.000000 | 6.000000 | |
| 413 | 8.000000 | 4.000000 | 6.000000 | |
| 414 | 8.000000 | 5.000000 | 6.000000 | |
| 415 | 9.000000 | 0. | 0. | 0. |
| 416 | 9.000000 | 1.000000 | 0. | 1.000000 |
| 417 | 9.000000 | 2.000000 | 0. | 2.000000 |
| 418 | 9.000000 | 3.000000 | 0. | 3.000000 |
| 419 | 9.000000 | 4.000000 | 0. | 4.000000 |
| 420 | 9.000000 | 5.000000 | 0. | 5.000000 |
| 421 | 9.000000 | 0. | 1.000000 | 0. |
| 422 | 9.000000 | 1.000000 | 1.000000 | 1.000000 |
| 423 | 9.000000 | 2.000000 | 1.000000 | 2.000000 |
| 424 | 9.000000 | 3.000000 | 1.000000 | 3.000000 |
| 425 | 9.000000 | 4.000000 | 1.000000 | 4.000000 |
| 426 | 9.000000 | 5.000000 | 1.000000 | 5.000000 |
| 427 | 9.000000 | 0. | 2.000000 | 0. |
| 428 | 9.000000 | 1.000000 | 2.000000 | 1.000000 |
| 429 | 9.000000 | 2.000000 | 2.000000 | 2.000000 |
| 430 | 9.000000 | 3.000000 | 2.000000 | 3.000000 |
| 431 | 9.000000 | 4.000000 | 2.000000 | 4.000000 |
| 432 | 9.000000 | 5.000000 | 2.000000 | 5.000000 |
| 433 | 9.000000 | 0. | 3.000000 | 0. |
| 434 | 9.000000 | 1.000000 | 3.000000 | 1.000000 |
| 435 | 9.000000 | 2.000000 | 3.000000 | 2.000000 |
| 436 | 9.000000 | 3.000000 | 3.000000 | 3.000000 |
| 437 | 9.000000 | 4.000000 | 3.000000 | 4.000000 |
| 438 | 9.000000 | 5.000000 | 3.000000 | 5.000000 |
| 439 | 9.000000 | 0. | 4.000000 | 0. |
| 440 | 9.000000 | 1.000000 | 4.000000 | 1.000000 |

FI PM3D FLOW UNDER DAM SUPPORTED ON TWO MEDIA FOUNDATION

| NO. E | GLOBAL COORDINATES | | | PRESCRIBED PRESSURES |
|-------|--------------------|---------|---------|----------------------|
| | X | Y | Z | |
| 441 | 9.00000 | 2.00000 | 4.00000 | 2.00000 |
| 442 | 9.00000 | 3.00000 | 4.00000 | 3.00000 |
| 443 | 9.00000 | 4.00000 | 4.00000 | 4.00000 |
| 444 | 9.00000 | 5.00000 | 4.00000 | 5.00000 |
| 445 | 9.00000 | 0. | 5.00000 | 0. |
| 446 | 9.00000 | 1.00000 | 5.00000 | 1.00000 |
| 447 | 9.00000 | 2.00000 | 5.00000 | 2.00000 |
| 448 | 9.00000 | 3.00000 | 5.00000 | 3.00000 |
| 449 | 9.00000 | 4.00000 | 5.00000 | 4.00000 |
| 450 | 9.00000 | 5.00000 | 5.00000 | 5.00000 |
| 451 | 9.00000 | 0. | 6.00000 | 0. |
| 452 | 9.00000 | 1.00000 | 6.00000 | 1.00000 |
| 453 | 9.00000 | 2.00000 | 6.00000 | 2.00000 |
| 454 | 9.00000 | 3.00000 | 6.00000 | 3.00000 |
| 455 | 9.00000 | 4.00000 | 6.00000 | 4.00000 |
| 456 | 9.00000 | 5.00000 | 6.00000 | 5.00000 |

F1PM3D FLOW UNDER DAM SUPPORTED ON TWO MEDIA FOUNDATION

| ELEMENT | N1 | N2 | N3 | N4 | N5 | N6 | N7 | NR | MATERIAL | VOLUME | STORE IN BLOCK | OBTAIN FROM BLOCK |
|---------|-----|-----|-----|-----|-----|-----|-----|-----|----------|-----------|-------------------|----------------------|
| 1 | 416 | 415 | 422 | 421 | 380 | 379 | 374 | 373 | I | 10000E+01 | I | O |
| 2 | 422 | 421 | 428 | 427 | 386 | 385 | 380 | 379 | I | 10000E+01 | O | I |
| 3 | 428 | 427 | 434 | 433 | 392 | 391 | 386 | 385 | I | 10000E+01 | O | I |
| 4 | 434 | 433 | 440 | 439 | 398 | 397 | 392 | 391 | I | 10000E+01 | O | I |
| 5 | 440 | 439 | 446 | 445 | 404 | 403 | 398 | 397 | I | 10000E+01 | O | I |
| 6 | 446 | 445 | 452 | 451 | 410 | 409 | 404 | 403 | I | 10000E+01 | O | I |
| 7 | 417 | 416 | 423 | 422 | 381 | 380 | 375 | 374 | I | 10000E+01 | O | I |
| 8 | 423 | 422 | 429 | 428 | 387 | 386 | 381 | 380 | I | 10000E+01 | O | I |
| 9 | 429 | 428 | 435 | 434 | 393 | 392 | 387 | 386 | I | 10000E+01 | O | I |
| 10 | 435 | 434 | 441 | 440 | 399 | 398 | 393 | 392 | I | 10000E+01 | O | I |
| 11 | 441 | 440 | 447 | 446 | 405 | 404 | 399 | 399 | I | 10000E+01 | O | I |
| 12 | 447 | 446 | 453 | 452 | 411 | 410 | 405 | 404 | I | 10000E+01 | O | I |
| 13 | 418 | 417 | 424 | 423 | 382 | 381 | 376 | 375 | I | 10000E+01 | O | I |
| 14 | 424 | 423 | 430 | 429 | 388 | 387 | 382 | 381 | I | 10000E+01 | O | I |
| 15 | 430 | 429 | 436 | 435 | 394 | 393 | 388 | 387 | I | 10000E+01 | O | I |
| 16 | 436 | 435 | 442 | 441 | 400 | 399 | 394 | 393 | I | 10000E+01 | O | I |
| 17 | 442 | 441 | 448 | 447 | 406 | 405 | 400 | 399 | I | 10000E+01 | O | I |
| 18 | 448 | 447 | 454 | 453 | 412 | 411 | 406 | 405 | I | 10000E+01 | O | I |
| 19 | 419 | 418 | 425 | 424 | 383 | 382 | 377 | 376 | I | 10000E+01 | O | I |
| 20 | 425 | 424 | 431 | 430 | 389 | 388 | 383 | 382 | I | 10000E+01 | O | I |
| 21 | 431 | 430 | 437 | 436 | 395 | 394 | 389 | 388 | I | 10000E+01 | O | I |
| 22 | 437 | 436 | 443 | 442 | 401 | 400 | 395 | 394 | I | 10000E+01 | O | I |
| 23 | 443 | 442 | 449 | 448 | 407 | 406 | 401 | 400 | I | 10000E+01 | O | I |
| 24 | 449 | 448 | 455 | 454 | 413 | 412 | 407 | 406 | I | 10000E+01 | O | I |
| 25 | 420 | 419 | 426 | 425 | 384 | 383 | 378 | 377 | I | 10000E+01 | O | I |
| 26 | 426 | 425 | 432 | 431 | 390 | 389 | 384 | 383 | I | 10000E+01 | O | I |
| 27 | 432 | 431 | 438 | 437 | 396 | 395 | 390 | 389 | I | 10000E+01 | O | I |
| 28 | 438 | 437 | 444 | 443 | 402 | 401 | 396 | 395 | I | 10000E+01 | O | I |
| 29 | 444 | 443 | 450 | 449 | 408 | 407 | 402 | 401 | I | 10000E+01 | O | I |
| 30 | 450 | 449 | 456 | 455 | 414 | 413 | 408 | 407 | I | 10000E+01 | O | I |
| 31 | 374 | 373 | 380 | 379 | 338 | 337 | 332 | 331 | I | 10000E+01 | O | I |
| 32 | 380 | 379 | 386 | 385 | 344 | 343 | 338 | 337 | I | 10000E+01 | O | I |
| 33 | 386 | 385 | 392 | 391 | 350 | 349 | 344 | 343 | I | 10000E+01 | O | I |
| 34 | 392 | 391 | 398 | 397 | 356 | 355 | 350 | 349 | I | 10000E+01 | O | I |
| 35 | 398 | 397 | 404 | 403 | 362 | 361 | 356 | 355 | I | 10000E+01 | O | I |
| 36 | 404 | 403 | 410 | 409 | 368 | 367 | 362 | 361 | I | 10000E+01 | O | I |
| 37 | 375 | 374 | 381 | 380 | 339 | 338 | 333 | 332 | I | 10000E+01 | O | I |
| 38 | 381 | 380 | 387 | 386 | 345 | 344 | 339 | 338 | I | 10000E+01 | O | I |
| 39 | 387 | 386 | 393 | 392 | 351 | 350 | 345 | 344 | I | 10000E+01 | O | I |
| 40 | 393 | 392 | 399 | 398 | 357 | 356 | 351 | 350 | I | 10000E+01 | O | I |

FIPM3D FLOW UNDER DAM SUPPORTED ON TWO MEDIA FOUNDATION

| ELEMENT | N1 | N2 | N3 | N4 | N5 | N6 | N7 | NA | MATERIAL | VOLUME | STORE IN BLOCK | OBTAIN FROM BLOCK |
|---------|-----|-----|-----|-----|-----|-----|-----|-----|----------|------------|----------------|-------------------|
| 41 | 399 | 398 | 405 | 404 | 363 | 362 | 357 | 354 | I | 100000E+01 | 0 | I |
| 42 | 405 | 404 | 411 | 410 | 369 | 368 | 363 | 362 | I | 100000E+01 | 0 | I |
| 43 | 376 | 375 | 382 | 381 | 340 | 339 | 334 | 333 | I | 100000E+01 | 0 | I |
| 44 | 382 | 381 | 388 | 387 | 346 | 345 | 340 | 339 | I | 100000E+01 | 0 | I |
| 45 | 388 | 387 | 394 | 393 | 352 | 351 | 346 | 345 | I | 100000E+01 | 0 | I |
| 46 | 394 | 393 | 400 | 399 | 358 | 357 | 352 | 351 | I | 100000E+01 | 0 | I |
| 47 | 400 | 399 | 406 | 405 | 364 | 363 | 358 | 357 | I | 100000E+01 | 0 | I |
| 48 | 406 | 405 | 412 | 411 | 370 | 369 | 364 | 363 | I | 100000E+01 | 0 | I |
| 49 | 377 | 376 | 383 | 382 | 341 | 340 | 335 | 334 | I | 100000E+01 | 0 | I |
| 50 | 383 | 382 | 389 | 388 | 347 | 346 | 341 | 340 | I | 100000E+01 | 0 | I |
| 51 | 389 | 388 | 395 | 394 | 353 | 352 | 347 | 346 | I | 100000E+01 | 0 | I |
| 52 | 395 | 394 | 401 | 400 | 359 | 358 | 353 | 352 | I | 100000E+01 | 0 | I |
| 53 | 401 | 400 | 407 | 406 | 365 | 364 | 359 | 358 | I | 100000E+01 | 0 | I |
| 54 | 407 | 406 | 413 | 412 | 371 | 370 | 365 | 364 | I | 100000E+01 | 0 | I |
| 55 | 378 | 377 | 384 | 383 | 342 | 341 | 336 | 335 | I | 100000E+01 | 0 | I |
| 56 | 384 | 383 | 390 | 389 | 348 | 347 | 342 | 341 | I | 100000E+01 | 0 | I |
| 57 | 390 | 389 | 396 | 395 | 354 | 353 | 348 | 347 | I | 100000E+01 | 0 | I |
| 58 | 396 | 395 | 402 | 401 | 360 | 359 | 354 | 353 | I | 100000E+01 | 0 | I |
| 59 | 402 | 401 | 408 | 407 | 366 | 365 | 360 | 359 | I | 100000E+01 | 0 | I |
| 60 | 408 | 407 | 414 | 413 | 372 | 371 | 366 | 365 | I | 100000E+01 | 0 | I |
| 61 | 332 | 331 | 338 | 337 | 290 | 289 | 284 | 283 | I | 100000E+01 | 0 | I |
| 62 | 338 | 337 | 344 | 343 | 296 | 295 | 290 | 289 | I | 100000E+01 | 0 | I |
| 63 | 344 | 343 | 350 | 349 | 302 | 301 | 296 | 295 | I | 100000E+01 | 0 | I |
| 64 | 350 | 349 | 356 | 355 | 308 | 307 | 302 | 301 | I | 100000E+01 | 0 | I |
| 65 | 356 | 355 | 362 | 361 | 314 | 313 | 308 | 307 | I | 100000E+01 | 0 | I |
| 66 | 333 | 332 | 339 | 338 | 291 | 290 | 285 | 284 | I | 100000E+01 | 0 | I |
| 67 | 339 | 338 | 345 | 344 | 297 | 296 | 291 | 290 | I | 100000E+01 | 0 | I |
| 68 | 345 | 344 | 351 | 350 | 303 | 302 | 297 | 296 | I | 100000E+01 | 0 | I |
| 69 | 351 | 350 | 357 | 356 | 309 | 308 | 303 | 302 | I | 100000E+01 | 0 | I |
| 70 | 357 | 356 | 363 | 362 | 315 | 314 | 309 | 308 | I | 100000E+01 | 0 | I |
| 71 | 334 | 333 | 340 | 339 | 292 | 291 | 286 | 285 | I | 100000E+01 | 0 | I |
| 72 | 340 | 339 | 346 | 345 | 298 | 297 | 292 | 291 | I | 100000E+01 | 0 | I |
| 73 | 346 | 345 | 352 | 351 | 304 | 303 | 298 | 297 | I | 100000E+01 | 0 | I |
| 74 | 352 | 351 | 358 | 357 | 310 | 309 | 304 | 303 | I | 100000E+01 | 0 | I |
| 75 | 358 | 357 | 364 | 363 | 316 | 315 | 310 | 309 | I | 100000E+01 | 0 | I |
| 76 | 335 | 334 | 341 | 340 | 293 | 292 | 287 | 286 | I | 100000E+01 | 0 | I |
| 77 | 341 | 340 | 347 | 346 | 299 | 298 | 293 | 292 | I | 100000E+01 | 0 | I |
| 78 | 347 | 346 | 353 | 352 | 305 | 304 | 299 | 298 | I | 100000E+01 | 0 | I |
| 79 | 353 | 352 | 359 | 358 | 311 | 310 | 305 | 304 | I | 100000E+01 | 0 | I |
| 80 | 359 | 358 | 365 | 364 | 317 | 316 | 311 | 310 | I | 100000E+01 | 0 | I |

FIPM3D FLOW UNDER DAM SUPPORTED ON TWO MEDIA FOUNDATION

| ELEMENT | N1 | N2 | N3 | N4 | N5 | N6 | N7 | N8 | MATERIAL | VOLUME | STORE IN BLOCK | OBTAIN FROM BLOCK |
|---------|-----|-----|-----|-----|-----|-----|-----|-----|----------|------------|----------------|-------------------|
| 81 | 336 | 335 | 342 | 341 | 294 | 293 | 288 | 287 | I | 100000E+01 | 0 | I |
| 82 | 342 | 341 | 348 | 347 | 300 | 299 | 294 | 293 | I | 100000E+01 | 0 | I |
| 83 | 348 | 347 | 354 | 353 | 306 | 305 | 300 | 299 | I | 100000E+01 | 0 | I |
| 84 | 354 | 353 | 360 | 359 | 312 | 311 | 306 | 305 | I | 100000E+01 | 0 | I |
| 85 | 360 | 359 | 366 | 365 | 318 | 317 | 312 | 311 | I | 100000E+01 | 0 | I |
| 86 | 284 | 283 | 290 | 289 | 242 | 241 | 236 | 235 | I | 100000E+01 | 0 | I |
| 87 | 290 | 289 | 296 | 295 | 248 | 247 | 242 | 241 | I | 100000E+01 | 0 | I |
| 88 | 296 | 295 | 302 | 301 | 254 | 253 | 248 | 247 | I | 100000E+01 | 0 | I |
| 89 | 302 | 301 | 308 | 307 | 260 | 259 | 254 | 253 | I | 100000E+01 | 0 | I |
| 90 | 285 | 284 | 291 | 290 | 243 | 242 | 237 | 236 | I | 100000E+01 | 0 | I |
| 91 | 291 | 290 | 297 | 296 | 249 | 248 | 243 | 242 | I | 100000E+01 | 0 | I |
| 92 | 297 | 296 | 303 | 302 | 255 | 254 | 249 | 248 | I | 100000E+01 | 0 | I |
| 93 | 303 | 302 | 309 | 308 | 261 | 260 | 255 | 254 | I | 100000E+01 | 0 | I |
| 94 | 286 | 285 | 292 | 291 | 244 | 243 | 238 | 237 | I | 100000E+01 | 0 | I |
| 95 | 292 | 291 | 298 | 297 | 250 | 249 | 244 | 243 | I | 100000E+01 | 0 | I |
| 96 | 298 | 297 | 304 | 303 | 256 | 255 | 250 | 249 | I | 100000E+01 | 0 | I |
| 97 | 304 | 303 | 310 | 309 | 262 | 261 | 256 | 255 | I | 100000E+01 | 0 | I |
| 98 | 287 | 286 | 293 | 292 | 245 | 244 | 239 | 238 | I | 100000E+01 | 0 | I |
| 99 | 293 | 292 | 299 | 298 | 251 | 250 | 245 | 244 | I | 100000E+01 | 0 | I |
| 100 | 299 | 298 | 305 | 304 | 257 | 256 | 251 | 250 | I | 100000E+01 | 0 | I |
| 101 | 305 | 304 | 311 | 310 | 263 | 262 | 257 | 256 | I | 100000E+01 | 0 | I |
| 102 | 288 | 287 | 294 | 293 | 246 | 245 | 240 | 239 | I | 100000E+01 | 0 | I |
| 103 | 294 | 293 | 300 | 299 | 252 | 251 | 246 | 245 | I | 100000E+01 | 0 | I |
| 104 | 290 | 289 | 296 | 295 | 258 | 257 | 252 | 251 | I | 100000E+01 | 0 | I |
| 105 | 306 | 305 | 312 | 311 | 264 | 263 | 258 | 257 | I | 100000E+01 | 0 | I |
| 106 | 306 | 305 | 312 | 311 | 194 | 193 | 188 | 187 | I | 100000E+01 | 0 | I |
| 107 | 236 | 235 | 242 | 241 | 200 | 199 | 194 | 193 | I | 100000E+01 | 0 | I |
| 108 | 242 | 241 | 248 | 247 | 206 | 205 | 200 | 199 | I | 100000E+01 | 0 | I |
| 109 | 248 | 247 | 254 | 253 | 212 | 211 | 206 | 205 | I | 100000E+01 | 0 | I |
| 110 | 237 | 236 | 243 | 242 | 218 | 217 | 212 | 211 | I | 100000E+01 | 0 | I |
| 111 | 243 | 242 | 249 | 248 | 224 | 223 | 218 | 217 | I | 100000E+01 | 0 | I |
| 112 | 249 | 248 | 255 | 254 | 230 | 229 | 224 | 223 | I | 100000E+01 | 0 | I |
| 113 | 238 | 237 | 244 | 243 | 236 | 235 | 230 | 229 | I | 100000E+01 | 0 | I |
| 114 | 244 | 243 | 250 | 249 | 242 | 241 | 236 | 235 | I | 100000E+01 | 0 | I |
| 115 | 239 | 238 | 245 | 244 | 248 | 247 | 242 | 241 | I | 100000E+01 | 0 | I |
| 116 | 245 | 244 | 251 | 250 | 254 | 253 | 248 | 247 | I | 100000E+01 | 0 | I |
| 117 | 251 | 250 | 257 | 256 | 260 | 259 | 254 | 253 | I | 100000E+01 | 0 | I |
| 118 | 246 | 245 | 252 | 251 | 266 | 265 | 260 | 259 | I | 100000E+01 | 0 | I |
| 119 | 246 | 245 | 252 | 251 | 266 | 265 | 260 | 259 | I | 100000E+01 | 0 | I |
| 120 | 252 | 251 | 258 | 257 | 270 | 269 | 264 | 263 | I | 100000E+01 | 0 | I |

FIPM30 FLOW UNDER DAM SUPPORTED ON TWO MEDIA FOUNDATION

| ELEMENT | N1 | N2 | N3 | N4 | N5 | N6 | N7 | NR | MATERIAL | VOLUME | STORE IN ALOCK | OBTAIN FROM ALOCK |
|---------|-----|-----|-----|-----|-----|-----|-----|-----|----------|------------|-------------------|----------------------|
| 121 | 188 | 187 | 194 | 193 | 194 | 145 | 140 | 139 | I | 100000E+00 | 0 | I |
| 122 | 194 | 188 | 195 | 194 | 147 | 151 | 146 | 145 | I | 100000E+00 | 0 | I |
| 123 | 189 | 189 | 201 | 194 | 153 | 146 | 141 | 140 | I | 100000E+00 | 0 | I |
| 124 | 195 | 189 | 196 | 195 | 148 | 152 | 147 | 140 | I | 100000E+00 | 0 | I |
| 125 | 190 | 195 | 202 | 195 | 154 | 153 | 142 | 141 | I | 100000E+00 | 0 | I |
| 126 | 196 | 190 | 197 | 196 | 149 | 148 | 148 | 147 | I | 100000E+00 | 0 | I |
| 127 | 191 | 196 | 203 | 196 | 155 | 148 | 143 | 142 | I | 100000E+00 | 0 | I |
| 128 | 197 | 191 | 198 | 197 | 149 | 154 | 149 | 143 | I | 100000E+00 | 0 | I |
| 129 | 192 | 197 | 204 | 197 | 150 | 149 | 144 | 143 | I | 100000E+00 | 0 | I |
| 130 | 198 | 197 | 204 | 203 | 156 | 155 | 150 | 149 | I | 100000E+00 | 0 | I |
| 131 | 140 | 139 | 146 | 145 | 98 | 97 | 92 | 149 | I | 100000E+00 | 0 | I |
| 132 | 141 | 140 | 147 | 146 | 99 | 98 | 93 | 92 | I | 100000E+00 | 0 | I |
| 133 | 142 | 142 | 148 | 147 | 100 | 99 | 94 | 93 | I | 100000E+00 | 0 | I |
| 134 | 143 | 143 | 149 | 148 | 101 | 100 | 95 | 94 | I | 100000E+00 | 0 | I |
| 135 | 144 | 143 | 150 | 149 | 102 | 101 | 96 | 95 | I | 100000E+00 | 0 | I |
| 136 | 92 | 91 | 98 | 97 | 86 | 85 | 44 | 43 | I | 500000E+00 | I | O |
| 137 | 93 | 92 | 99 | 98 | 87 | 86 | 45 | 44 | I | 500000E+00 | 0 | I |
| 138 | 94 | 93 | 100 | 99 | 88 | 87 | 46 | 45 | I | 500000E+00 | 0 | I |
| 139 | 95 | 94 | 101 | 100 | 89 | 88 | 47 | 46 | I | 500000E+00 | 0 | I |
| 140 | 96 | 95 | 102 | 101 | 90 | 89 | 48 | 47 | I | 500000E+00 | 0 | I |
| 141 | 146 | 145 | 152 | 151 | 134 | 133 | 99 | 97 | I | 500000E+00 | 0 | I |
| 142 | 147 | 146 | 153 | 152 | 135 | 134 | 100 | 98 | I | 500000E+00 | 0 | I |
| 143 | 148 | 147 | 154 | 153 | 136 | 135 | 101 | 99 | I | 500000E+00 | 0 | I |
| 144 | 149 | 148 | 155 | 154 | 137 | 136 | 102 | 100 | I | 500000E+00 | 0 | I |
| 145 | 150 | 149 | 156 | 155 | 138 | 137 | 102 | 101 | I | 500000E+00 | 0 | I |
| 146 | 200 | 199 | 206 | 205 | 181 | 180 | 152 | 151 | I | 500000E+00 | 0 | I |
| 147 | 201 | 200 | 207 | 206 | 182 | 181 | 153 | 152 | I | 500000E+00 | 0 | I |
| 148 | 202 | 201 | 208 | 207 | 183 | 182 | 154 | 153 | I | 500000E+00 | 0 | I |
| 149 | 203 | 202 | 209 | 208 | 184 | 183 | 155 | 154 | I | 500000E+00 | 0 | I |
| 150 | 204 | 203 | 210 | 209 | 185 | 184 | 156 | 155 | I | 500000E+00 | 0 | I |
| 151 | 254 | 253 | 261 | 259 | 186 | 185 | 206 | 205 | I | 500000E+00 | 0 | I |
| 152 | 255 | 254 | 262 | 261 | 230 | 229 | 207 | 206 | I | 500000E+00 | 0 | I |
| 153 | 256 | 255 | 263 | 262 | 231 | 230 | 208 | 207 | I | 500000E+00 | 0 | I |
| 154 | 257 | 256 | 264 | 263 | 232 | 231 | 209 | 208 | I | 500000E+00 | 0 | I |
| 155 | 258 | 257 | 264 | 263 | 233 | 232 | 210 | 209 | I | 500000E+00 | 0 | I |
| 156 | 308 | 307 | 314 | 313 | 278 | 277 | 260 | 259 | I | 500000E+00 | 0 | I |
| 157 | 309 | 308 | 315 | 314 | 279 | 278 | 261 | 260 | I | 500000E+00 | 0 | I |
| 158 | 310 | 309 | 316 | 315 | 280 | 279 | 262 | 261 | I | 500000E+00 | 0 | I |
| 159 | 311 | 310 | 317 | 316 | 281 | 280 | 263 | 262 | I | 500000E+00 | 0 | I |
| 160 | 312 | 311 | 318 | 317 | 282 | 281 | 264 | 263 | I | 500000E+00 | 0 | I |

FI PM3D FLOW UNDER DAM SUPPORTED ON TWO MEDIA FOUNDATION

| ELEMENT | N1 | N2 | N3 | N4 | N5 | N6 | N7 | NR | MATERIAL | VOLUME | STORE IN ALOCK | OBTAIN FROM ALOCK |
|---------|-----|-----|-----|-----|-----|-----|-----|-----|----------|------------|----------------|-------------------|
| 161 | 362 | 361 | 368 | 367 | 326 | 325 | 314 | 313 | I | .50000E+00 | 0 | I |
| 162 | 363 | 362 | 369 | 368 | 327 | 326 | 315 | 314 | I | .50000E+00 | 0 | I |
| 163 | 364 | 363 | 370 | 369 | 328 | 327 | 316 | 315 | I | .50000E+00 | 0 | I |
| 164 | 365 | 364 | 371 | 370 | 329 | 328 | 317 | 316 | I | .50000E+00 | 0 | I |
| 165 | 366 | 365 | 372 | 371 | 330 | 329 | 318 | 317 | I | .50000E+00 | 0 | I |
| 166 | 86 | 85 | 98 | 97 | 50 | 49 | 44 | 43 | I | .50000E+00 | 0 | I |
| 167 | 87 | 86 | 99 | 98 | 51 | 50 | 45 | 44 | I | .50000E+00 | 0 | I |
| 168 | 88 | 87 | 100 | 99 | 52 | 51 | 46 | 45 | I | .50000E+00 | 0 | I |
| 169 | 89 | 88 | 101 | 100 | 53 | 52 | 47 | 46 | I | .50000E+00 | 0 | I |
| 170 | 90 | 89 | 102 | 101 | 54 | 53 | 48 | 47 | I | .50000E+00 | 0 | I |
| 171 | 134 | 133 | 152 | 151 | 104 | 103 | 98 | 97 | I | .50000E+00 | 0 | I |
| 172 | 135 | 134 | 153 | 152 | 105 | 104 | 99 | 98 | I | .50000E+00 | 0 | I |
| 173 | 136 | 135 | 154 | 153 | 106 | 105 | 100 | 99 | I | .50000E+00 | 0 | I |
| 174 | 137 | 136 | 155 | 154 | 107 | 106 | 101 | 100 | I | .50000E+00 | 0 | I |
| 175 | 138 | 137 | 156 | 155 | 108 | 107 | 102 | 101 | I | .50000E+00 | 0 | I |
| 176 | 182 | 181 | 206 | 205 | 158 | 157 | 152 | 151 | I | .50000E+00 | 0 | I |
| 177 | 183 | 182 | 207 | 206 | 159 | 158 | 153 | 152 | I | .50000E+00 | 0 | I |
| 178 | 184 | 183 | 208 | 207 | 160 | 159 | 154 | 153 | I | .50000E+00 | 0 | I |
| 179 | 185 | 184 | 209 | 208 | 161 | 160 | 155 | 154 | I | .50000E+00 | 0 | I |
| 180 | 186 | 185 | 210 | 209 | 162 | 161 | 156 | 155 | I | .50000E+00 | 0 | I |
| 181 | 230 | 229 | 260 | 259 | 212 | 211 | 206 | 205 | I | .50000E+00 | 0 | I |
| 182 | 231 | 230 | 261 | 260 | 213 | 212 | 207 | 206 | I | .50000E+00 | 0 | I |
| 183 | 232 | 231 | 262 | 261 | 214 | 213 | 208 | 207 | I | .50000E+00 | 0 | I |
| 184 | 233 | 232 | 263 | 262 | 215 | 214 | 209 | 208 | I | .50000E+00 | 0 | I |
| 185 | 234 | 233 | 264 | 263 | 216 | 215 | 210 | 209 | I | .50000E+00 | 0 | I |
| 186 | 278 | 277 | 314 | 313 | 266 | 265 | 260 | 259 | I | .50000E+00 | 0 | I |
| 187 | 279 | 278 | 315 | 314 | 267 | 266 | 261 | 260 | I | .50000E+00 | 0 | I |
| 188 | 280 | 279 | 316 | 315 | 268 | 267 | 262 | 261 | I | .50000E+00 | 0 | I |
| 189 | 281 | 280 | 317 | 316 | 269 | 268 | 263 | 262 | I | .50000E+00 | 0 | I |
| 190 | 282 | 281 | 318 | 317 | 270 | 269 | 264 | 263 | I | .50000E+00 | 0 | I |
| 191 | 326 | 325 | 368 | 367 | 319 | 318 | 314 | 313 | I | .50000E+00 | 0 | I |
| 192 | 327 | 326 | 369 | 368 | 320 | 319 | 315 | 314 | I | .50000E+00 | 0 | I |
| 193 | 328 | 327 | 370 | 369 | 321 | 320 | 316 | 315 | I | .50000E+00 | 0 | I |
| 194 | 329 | 328 | 371 | 370 | 322 | 321 | 317 | 316 | I | .50000E+00 | 0 | I |
| 195 | 330 | 329 | 372 | 371 | 323 | 322 | 318 | 317 | I | .50000E+00 | 0 | I |
| 196 | 44 | 43 | 50 | 49 | 324 | 323 | 318 | 317 | I | .50000E+00 | 0 | I |
| 197 | 50 | 49 | 56 | 55 | 8 | 7 | 2 | 1 | I | .50000E+00 | 0 | I |
| 198 | 56 | 55 | 62 | 61 | 13 | 12 | 8 | 7 | I | .50000E+00 | 0 | I |
| 199 | 62 | 61 | 68 | 67 | 19 | 18 | 14 | 13 | I | .50000E+00 | 0 | I |
| 200 | 68 | 67 | 74 | 73 | 25 | 24 | 20 | 19 | I | .50000E+00 | 0 | I |

FIPM3D FLOW UNDER DAM SUPPORTED ON TWO MEDIA FOUNDATION

| ELEMENT | N1 | N2 | N3 | N4 | N5 | N6 | N7 | NR | MATERIAL | VOLUME | STORE IN ALOCK | OBTAIN FROM ALOCK |
|---------|-----|-----|-----|-----|----|----|----|----|----------|--------|----------------|-------------------|
| 201 | 74 | 73 | 80 | 79 | 38 | 37 | 32 | 31 | 2 | 100000 | 0 | 1 |
| 202 | 45 | 44 | 51 | 50 | 15 | 14 | 15 | 13 | 2 | 100000 | 0 | 1 |
| 203 | 51 | 50 | 57 | 56 | 21 | 20 | 21 | 19 | 2 | 100000 | 0 | 1 |
| 204 | 57 | 56 | 63 | 62 | 27 | 26 | 27 | 25 | 2 | 100000 | 0 | 1 |
| 205 | 63 | 62 | 69 | 68 | 33 | 32 | 33 | 31 | 2 | 100000 | 0 | 1 |
| 206 | 69 | 68 | 75 | 74 | 39 | 38 | 39 | 37 | 2 | 100000 | 0 | 1 |
| 207 | 75 | 74 | 81 | 80 | 45 | 44 | 45 | 43 | 2 | 100000 | 0 | 1 |
| 208 | 46 | 45 | 52 | 51 | 10 | 9 | 10 | 8 | 2 | 100000 | 0 | 1 |
| 209 | 52 | 51 | 58 | 57 | 16 | 15 | 16 | 14 | 2 | 100000 | 0 | 1 |
| 210 | 58 | 57 | 64 | 63 | 22 | 21 | 22 | 20 | 2 | 100000 | 0 | 1 |
| 211 | 64 | 63 | 70 | 69 | 28 | 27 | 28 | 26 | 2 | 100000 | 0 | 1 |
| 212 | 70 | 69 | 76 | 75 | 34 | 33 | 34 | 32 | 2 | 100000 | 0 | 1 |
| 213 | 76 | 75 | 82 | 81 | 40 | 39 | 40 | 38 | 2 | 100000 | 0 | 1 |
| 214 | 47 | 46 | 53 | 52 | 11 | 10 | 11 | 9 | 2 | 100000 | 0 | 1 |
| 215 | 53 | 52 | 59 | 58 | 17 | 16 | 17 | 15 | 2 | 100000 | 0 | 1 |
| 216 | 59 | 58 | 65 | 64 | 23 | 22 | 23 | 21 | 2 | 100000 | 0 | 1 |
| 217 | 65 | 64 | 71 | 70 | 29 | 28 | 29 | 27 | 2 | 100000 | 0 | 1 |
| 218 | 71 | 70 | 77 | 76 | 35 | 34 | 35 | 33 | 2 | 100000 | 0 | 1 |
| 219 | 77 | 76 | 83 | 82 | 41 | 40 | 41 | 39 | 2 | 100000 | 0 | 1 |
| 220 | 48 | 47 | 54 | 53 | 12 | 11 | 12 | 10 | 2 | 100000 | 0 | 1 |
| 221 | 54 | 53 | 60 | 59 | 18 | 17 | 18 | 16 | 2 | 100000 | 0 | 1 |
| 222 | 60 | 59 | 66 | 65 | 24 | 23 | 24 | 22 | 2 | 100000 | 0 | 1 |
| 223 | 66 | 65 | 72 | 71 | 30 | 29 | 30 | 28 | 2 | 100000 | 0 | 1 |
| 224 | 72 | 71 | 78 | 77 | 36 | 35 | 36 | 34 | 2 | 100000 | 0 | 1 |
| 225 | 78 | 77 | 84 | 83 | 42 | 41 | 42 | 40 | 2 | 100000 | 0 | 1 |
| 226 | 98 | 97 | 104 | 103 | 56 | 55 | 56 | 54 | 2 | 100000 | 0 | 1 |
| 227 | 104 | 103 | 110 | 109 | 62 | 61 | 62 | 60 | 2 | 100000 | 0 | 1 |
| 228 | 110 | 109 | 116 | 115 | 68 | 67 | 68 | 66 | 2 | 100000 | 0 | 1 |
| 229 | 116 | 115 | 122 | 121 | 74 | 73 | 74 | 72 | 2 | 100000 | 0 | 1 |
| 230 | 122 | 121 | 128 | 127 | 80 | 79 | 80 | 78 | 2 | 100000 | 0 | 1 |
| 231 | 99 | 98 | 105 | 104 | 57 | 56 | 57 | 55 | 2 | 100000 | 0 | 1 |
| 232 | 105 | 104 | 111 | 110 | 63 | 62 | 63 | 61 | 2 | 100000 | 0 | 1 |
| 233 | 111 | 110 | 117 | 116 | 69 | 68 | 69 | 67 | 2 | 100000 | 0 | 1 |
| 234 | 117 | 116 | 123 | 122 | 75 | 74 | 75 | 73 | 2 | 100000 | 0 | 1 |
| 235 | 123 | 122 | 129 | 128 | 81 | 80 | 81 | 79 | 2 | 100000 | 0 | 1 |
| 236 | 100 | 99 | 106 | 105 | 58 | 57 | 58 | 56 | 2 | 100000 | 0 | 1 |
| 237 | 106 | 105 | 112 | 111 | 64 | 63 | 64 | 62 | 2 | 100000 | 0 | 1 |
| 238 | 112 | 111 | 118 | 117 | 70 | 69 | 70 | 68 | 2 | 100000 | 0 | 1 |
| 239 | 118 | 117 | 124 | 123 | 76 | 75 | 76 | 74 | 2 | 100000 | 0 | 1 |
| 240 | 124 | 123 | 130 | 129 | 82 | 81 | 82 | 80 | 2 | 100000 | 0 | 1 |

FIPM3D FLOW UNDER DAM SUPPORTED ON TWO MEDIA FOUNDATION

| ELEMENT | N1 | N2 | N3 | N4 | N5 | N6 | N7 | NA | MATERIAL | VOLUME | STORE IN BLOCK | OBTAIN FROM BLOCK |
|---------|-----|-----|-----|-----|-----|-----|-----|-----|----------|-----------|----------------|-------------------|
| 241 | 101 | 100 | 107 | 106 | 59 | 58 | 53 | 52 | 2 | 10000E+01 | 0 | 1 |
| 242 | 107 | 106 | 113 | 112 | 65 | 64 | 59 | 58 | 2 | 10000E+01 | 0 | 1 |
| 243 | 119 | 118 | 119 | 118 | 71 | 70 | 65 | 64 | 2 | 10000E+01 | 0 | 1 |
| 244 | 125 | 124 | 125 | 124 | 77 | 76 | 71 | 70 | 2 | 10000E+01 | 0 | 1 |
| 245 | 102 | 101 | 131 | 130 | 83 | 82 | 77 | 76 | 2 | 10000E+01 | 0 | 1 |
| 246 | 108 | 107 | 108 | 107 | 60 | 59 | 54 | 53 | 2 | 10000E+01 | 0 | 1 |
| 247 | 114 | 113 | 114 | 113 | 66 | 65 | 60 | 59 | 2 | 10000E+01 | 0 | 1 |
| 248 | 126 | 125 | 126 | 125 | 72 | 71 | 66 | 65 | 2 | 10000E+01 | 0 | 1 |
| 249 | 152 | 151 | 132 | 131 | 78 | 77 | 72 | 71 | 2 | 10000E+01 | 0 | 1 |
| 250 | 158 | 157 | 158 | 157 | 84 | 83 | 78 | 77 | 2 | 10000E+01 | 0 | 1 |
| 251 | 164 | 163 | 164 | 163 | 110 | 109 | 104 | 103 | 2 | 10000E+01 | 0 | 1 |
| 252 | 170 | 169 | 170 | 169 | 116 | 115 | 110 | 109 | 2 | 10000E+01 | 0 | 1 |
| 253 | 153 | 152 | 176 | 175 | 122 | 121 | 122 | 121 | 2 | 10000E+01 | 0 | 1 |
| 254 | 159 | 158 | 159 | 158 | 117 | 116 | 111 | 110 | 2 | 10000E+01 | 0 | 1 |
| 255 | 165 | 164 | 171 | 170 | 123 | 122 | 117 | 116 | 2 | 10000E+01 | 0 | 1 |
| 256 | 171 | 170 | 177 | 176 | 129 | 128 | 123 | 122 | 2 | 10000E+01 | 0 | 1 |
| 257 | 154 | 153 | 166 | 165 | 112 | 111 | 106 | 105 | 2 | 10000E+01 | 0 | 1 |
| 258 | 160 | 159 | 166 | 165 | 118 | 117 | 112 | 111 | 2 | 10000E+01 | 0 | 1 |
| 259 | 166 | 165 | 172 | 171 | 124 | 123 | 118 | 117 | 2 | 10000E+01 | 0 | 1 |
| 260 | 172 | 171 | 178 | 177 | 130 | 129 | 124 | 123 | 2 | 10000E+01 | 0 | 1 |
| 261 | 155 | 154 | 161 | 160 | 113 | 112 | 107 | 106 | 2 | 10000E+01 | 0 | 1 |
| 262 | 161 | 160 | 167 | 166 | 119 | 118 | 113 | 112 | 2 | 10000E+01 | 0 | 1 |
| 263 | 167 | 166 | 173 | 172 | 125 | 124 | 119 | 118 | 2 | 10000E+01 | 0 | 1 |
| 264 | 173 | 172 | 179 | 178 | 131 | 130 | 125 | 124 | 2 | 10000E+01 | 0 | 1 |
| 265 | 156 | 155 | 162 | 161 | 114 | 113 | 108 | 107 | 2 | 10000E+01 | 0 | 1 |
| 266 | 162 | 161 | 168 | 167 | 120 | 119 | 114 | 113 | 2 | 10000E+01 | 0 | 1 |
| 267 | 168 | 167 | 174 | 173 | 126 | 125 | 120 | 119 | 2 | 10000E+01 | 0 | 1 |
| 268 | 174 | 173 | 180 | 179 | 132 | 131 | 126 | 125 | 2 | 10000E+01 | 0 | 1 |
| 269 | 206 | 205 | 212 | 211 | 164 | 163 | 158 | 157 | 2 | 10000E+01 | 0 | 1 |
| 270 | 212 | 211 | 218 | 217 | 170 | 169 | 164 | 163 | 2 | 10000E+01 | 0 | 1 |
| 271 | 218 | 217 | 224 | 223 | 176 | 175 | 170 | 169 | 2 | 10000E+01 | 0 | 1 |
| 272 | 207 | 206 | 213 | 212 | 165 | 164 | 159 | 158 | 2 | 10000E+01 | 0 | 1 |
| 273 | 213 | 212 | 219 | 218 | 171 | 170 | 165 | 164 | 2 | 10000E+01 | 0 | 1 |
| 274 | 219 | 218 | 225 | 224 | 177 | 176 | 171 | 170 | 2 | 10000E+01 | 0 | 1 |
| 275 | 208 | 207 | 214 | 213 | 166 | 165 | 160 | 159 | 2 | 10000E+01 | 0 | 1 |
| 276 | 214 | 213 | 220 | 219 | 172 | 171 | 166 | 165 | 2 | 10000E+01 | 0 | 1 |
| 277 | 220 | 219 | 226 | 225 | 178 | 177 | 172 | 171 | 2 | 10000E+01 | 0 | 1 |
| 278 | 209 | 208 | 215 | 214 | 167 | 166 | 161 | 160 | 2 | 10000E+01 | 0 | 1 |
| 279 | | | | | | | | | | | | |
| 280 | | | | | | | | | | | | |

FIPM30 FLOW UNDER DAM SUPPORTED ON TWO MEDIA FOUNDATION

| ELEMENT | N1 | N2 | N3 | N4 | N5 | N6 | N7 | NA | MATERIAL | VOLUME | STORE IN BLOCK | OBTAIN FROM BLOCK |
|---------------|-----|-----|------------|-----|-----|-----|-----|-----|----------|------------|-------------------|----------------------|
| 281 | 215 | 214 | 221 | 220 | 173 | 172 | 167 | 166 | 2 | .10000E+01 | 0 | 1 |
| 282 | 221 | 220 | 227 | 226 | 179 | 178 | 173 | 172 | 2 | .10000E+01 | 0 | 1 |
| 283 | 210 | 209 | 216 | 215 | 168 | 167 | 162 | 161 | 2 | .10000E+01 | 0 | 1 |
| 284 | 216 | 215 | 222 | 221 | 174 | 173 | 168 | 167 | 2 | .10000E+01 | 0 | 1 |
| 285 | 222 | 221 | 228 | 227 | 180 | 179 | 174 | 173 | 2 | .10000E+01 | 0 | 1 |
| 286 | 260 | 259 | 266 | 265 | 218 | 217 | 212 | 211 | 2 | .10000E+01 | 0 | 1 |
| 287 | 266 | 265 | 272 | 271 | 224 | 223 | 218 | 217 | 2 | .10000E+01 | 0 | 1 |
| 288 | 261 | 260 | 267 | 266 | 219 | 218 | 213 | 212 | 2 | .10000E+01 | 0 | 1 |
| 289 | 267 | 266 | 273 | 272 | 225 | 224 | 219 | 218 | 2 | .10000E+01 | 0 | 1 |
| 290 | 262 | 261 | 268 | 267 | 220 | 219 | 214 | 213 | 2 | .10000E+01 | 0 | 1 |
| 291 | 268 | 267 | 274 | 273 | 226 | 225 | 220 | 219 | 2 | .10000E+01 | 0 | 1 |
| 292 | 263 | 262 | 269 | 268 | 221 | 220 | 215 | 214 | 2 | .10000E+01 | 0 | 1 |
| 293 | 269 | 268 | 275 | 274 | 227 | 226 | 221 | 220 | 2 | .10000E+01 | 0 | 1 |
| 294 | 264 | 263 | 270 | 269 | 222 | 221 | 216 | 215 | 2 | .10000E+01 | 0 | 1 |
| 295 | 27 | 269 | 276 | 275 | 228 | 227 | 222 | 221 | 2 | .10000E+01 | 0 | 1 |
| 296 | 314 | 313 | 320 | 319 | 272 | 271 | 266 | 265 | 2 | .10000E+01 | 0 | 1 |
| 297 | 315 | 314 | 321 | 320 | 273 | 272 | 267 | 266 | 2 | .10000E+01 | 0 | 1 |
| 298 | 316 | 315 | 322 | 321 | 274 | 273 | 268 | 267 | 2 | .10000E+01 | 0 | 1 |
| 299 | 317 | 316 | 323 | 322 | 275 | 274 | 269 | 268 | 2 | .10000E+01 | 0 | 1 |
| 300 | 318 | 317 | 324 | 323 | 276 | 275 | 270 | 269 | 2 | .10000E+01 | 0 | 1 |
| TOTAL VOLUME= | | | .27000E+03 | | | | | | | | | |

FI PM3D FLOW UNDER DAM SUPPORTED ON TWO MEDIA FOUNDATION
 LOAD CASE 1

| NODE | PRESSURE |
|------|------------|
| 1 | .20000E+02 |
| 2 | .21000E+02 |
| 3 | .22000E+02 |
| 4 | .23000E+02 |
| 5 | .24000E+02 |
| 6 | .25000E+02 |
| 7 | .20000E+02 |
| 8 | .21000E+02 |
| 9 | .22000E+02 |
| 10 | .23000E+02 |
| 11 | .24000E+02 |
| 12 | .25000E+02 |
| 13 | .20000E+02 |
| 14 | .21000E+02 |
| 15 | .22000E+02 |
| 16 | .23000E+02 |
| 17 | .24000E+02 |
| 18 | .25000E+02 |
| 19 | .20000E+02 |
| 20 | .21000E+02 |
| 21 | .22000E+02 |
| 22 | .23000E+02 |
| 23 | .24000E+02 |
| 24 | .25000E+02 |
| 25 | .20000E+02 |
| 26 | .21000E+02 |
| 27 | .22000E+02 |
| 28 | .23000E+02 |
| 29 | .24000E+02 |
| 30 | .25000E+02 |
| 31 | .20000E+02 |
| 32 | .21000E+02 |
| 33 | .22000E+02 |
| 34 | .23000E+02 |
| 35 | .24000E+02 |
| 36 | .25000E+02 |
| 37 | .20000E+02 |
| 38 | .21000E+02 |
| 39 | .22000E+02 |
| 40 | .23000E+02 |
| 41 | .24000E+02 |
| 42 | .25000E+02 |
| 43 | .20000E+02 |
| 44 | .14672E+02 |
| 45 | .11462E+02 |
| 46 | .10408E+02 |
| 47 | .10044E+02 |
| 48 | .99560E+01 |
| 49 | .20000E+02 |
| 50 | .17230E+02 |

FI PM3D FLOW UNDER DAM SUPPORTED ON TWO MEDIA FOUNDATION
 LOAD CASE 1

| NODE | PRESSURE |
|------|------------|
| 51 | .15675E+02 |
| 52 | .15323E+02 |
| 53 | .15423E+02 |
| 54 | .15481E+02 |
| 55 | .20000E+02 |
| 56 | .18284E+02 |
| 57 | .17384E+02 |
| 58 | .17377E+02 |
| 59 | .17649E+02 |
| 60 | .17766E+02 |
| 61 | .20000E+02 |
| 62 | .18858E+02 |
| 63 | .18355E+02 |
| 64 | .18533E+02 |
| 65 | .18903E+02 |
| 66 | .19049E+02 |
| 67 | .20000E+02 |
| 68 | .19253E+02 |
| 69 | .19009E+02 |
| 70 | .19303E+02 |
| 71 | .19726E+02 |
| 72 | .19889E+02 |
| 73 | .20000E+02 |
| 74 | .19596E+02 |
| 75 | .19574E+02 |
| 76 | .19934E+02 |
| 77 | .20386E+02 |
| 78 | .20557E+02 |
| 79 | .20000E+02 |
| 80 | .20382E+02 |
| 81 | .20404E+02 |
| 82 | .20791E+02 |
| 83 | .21252E+02 |
| 84 | .21426E+02 |
| 85 | .20000E+02 |
| 86 | .13386E+02 |
| 87 | .10597E+02 |
| 88 | .95690E+01 |
| 89 | .91475E+01 |
| 90 | .90445E+01 |
| 91 | .20000E+02 |
| 92 | .11935E+02 |
| 93 | .94384E+01 |
| 94 | .83193E+01 |
| 95 | .78645E+01 |
| 96 | .77425E+01 |
| 97 | .20000E+02 |
| 98 | .12005E+02 |
| 99 | .99945E+01 |
| 100 | .89630E+01 |

FI PM3D FLOW UNDER DAM SUPPORTED ON TWO MEDIA FOUNDATION
 LOAD CASE 1

| NODE | PRESSURE |
|------|------------|
| 101 | .85432E+01 |
| 102 | .84276E+01 |
| 103 | .20000E+02 |
| 104 | .14113E+02 |
| 105 | .12756E+02 |
| 106 | .12232E+02 |
| 107 | .12077E+02 |
| 108 | .12055E+02 |
| 109 | .20000E+02 |
| 110 | .15488E+02 |
| 111 | .14519E+02 |
| 112 | .14239E+02 |
| 113 | .14228E+02 |
| 114 | .14252E+02 |
| 115 | .20000E+02 |
| 116 | .16449E+02 |
| 117 | .15763E+02 |
| 118 | .15634E+02 |
| 119 | .15701E+02 |
| 120 | .15751E+02 |
| 121 | .20000E+02 |
| 122 | .17219E+02 |
| 123 | .16777E+02 |
| 124 | .16741E+02 |
| 125 | .16850E+02 |
| 126 | .16912E+02 |
| 127 | .20000E+02 |
| 128 | .18141E+02 |
| 129 | .17749E+02 |
| 130 | .17751E+02 |
| 131 | .17873E+02 |
| 132 | .17939E+02 |
| 133 | .12597E+02 |
| 134 | .10609E+02 |
| 135 | .90308E+01 |
| 136 | .83582E+01 |
| 137 | .80271E+01 |
| 138 | .79415E+01 |
| 139 | .95113E+01 |
| 140 | .90663E+01 |
| 141 | .74434E+01 |
| 142 | .66622E+01 |
| 143 | .62983E+01 |
| 144 | .61952E+01 |
| 145 | .98909E+01 |
| 146 | .95128E+01 |
| 147 | .81095E+01 |
| 148 | .74333E+01 |
| 149 | .71104E+01 |
| 150 | .70194E+01 |

FI PM3D FLOW UNDER DAM SUPPORTED ON TWO MEDIA FOUNDATION

LOAD CASE 1

| NODE | PRESSURE |
|------|------------|
| 151 | .91308E+01 |
| 152 | .89689E+01 |
| 153 | .82632E+01 |
| 154 | .78017E+01 |
| 155 | .75858E+01 |
| 156 | .75232E+01 |
| 157 | .11529E+02 |
| 158 | .11338E+02 |
| 159 | .10541E+02 |
| 160 | .10279E+02 |
| 161 | .10194E+02 |
| 162 | .10179E+02 |
| 163 | .12996E+02 |
| 164 | .12844E+02 |
| 165 | .12250E+02 |
| 166 | .12081E+02 |
| 167 | .12067E+02 |
| 168 | .12076E+02 |
| 169 | .14107E+02 |
| 170 | .14012E+02 |
| 171 | .13567E+02 |
| 172 | .13470E+02 |
| 173 | .13490E+02 |
| 174 | .13512E+02 |
| 175 | .15171E+02 |
| 176 | .15019E+02 |
| 177 | .14657E+02 |
| 178 | .14582E+02 |
| 179 | .14615E+02 |
| 180 | .14640E+02 |
| 181 | .78494E+01 |
| 182 | .77455E+01 |
| 183 | .74647E+01 |
| 184 | .72589E+01 |
| 185 | .71691E+01 |
| 186 | .71453E+01 |
| 187 | .60473E+01 |
| 188 | .58507E+01 |
| 189 | .54865E+01 |
| 190 | .51274E+01 |
| 191 | .49504E+01 |
| 192 | .48984E+01 |
| 193 | .67198E+01 |
| 194 | .65546E+01 |
| 195 | .62546E+01 |
| 196 | .59489E+01 |
| 197 | .57994E+01 |
| 198 | .57555E+01 |
| 199 | .69138E+01 |
| 200 | .68179E+01 |

FI PM3D FLOW UNDER DAM SUPPORTED ON TWO MEDIA FOUNDATION

LOAD CASE 1

| NODE | PRESSURE |
|------|------------|
| 201 | .66294E+01 |
| 202 | .64643E+01 |
| 203 | .63863E+01 |
| 204 | .63658E+01 |
| 205 | .67675E+01 |
| 206 | .67560E+01 |
| 207 | .67577E+01 |
| 208 | .67662E+01 |
| 209 | .67907E+01 |
| 210 | .68024E+01 |
| 211 | .88000E+01 |
| 212 | .87724E+01 |
| 213 | .87685E+01 |
| 214 | .87936E+01 |
| 215 | .88590E+01 |
| 216 | .88877E+01 |
| 217 | .10287E+02 |
| 218 | .10269E+02 |
| 219 | .10290E+02 |
| 220 | .10345E+02 |
| 221 | .10429E+02 |
| 222 | .10465E+02 |
| 223 | .11424E+02 |
| 224 | .11425E+02 |
| 225 | .11452E+02 |
| 226 | .11521E+02 |
| 227 | .11610E+02 |
| 228 | .11648E+02 |
| 229 | .58890E+01 |
| 230 | .59643E+01 |
| 231 | .61380E+01 |
| 232 | .63310E+01 |
| 233 | .64657E+01 |
| 234 | .65131E+01 |
| 235 | .37294E+01 |
| 236 | .37398E+01 |
| 237 | .37627E+01 |
| 238 | .37887E+01 |
| 239 | .38038E+01 |
| 240 | .38113E+01 |
| 241 | .45148E+01 |
| 242 | .45444E+01 |
| 243 | .45857E+01 |
| 244 | .46394E+01 |
| 245 | .46716E+01 |
| 246 | .46848E+01 |
| 247 | .49319E+01 |
| 248 | .49863E+01 |
| 249 | .50972E+01 |
| 250 | .52214E+01 |

FIPM30 FLOW UNDER DAM SUPPORTED ON TWO MEDIA FOUNDATION

LOAD CASE 1

| NODE | PRESSURE |
|------|------------|
| 251 | .53017E+01 |
| 252 | .53308E+01 |
| 253 | .50943E+01 |
| 254 | .51894E+01 |
| 255 | .53956E+01 |
| 256 | .56217E+01 |
| 257 | .57712E+01 |
| 258 | .58234E+01 |
| 259 | .50678E+01 |
| 260 | .52281E+01 |
| 261 | .55603E+01 |
| 262 | .59268E+01 |
| 263 | .61610E+01 |
| 264 | .62415E+01 |
| 265 | .67273E+01 |
| 266 | .68894E+01 |
| 267 | .72222E+01 |
| 268 | .75758E+01 |
| 269 | .78069E+01 |
| 270 | .78881E+01 |
| 271 | .79686E+01 |
| 272 | .80950E+01 |
| 273 | .84315E+01 |
| 274 | .87802E+01 |
| 275 | .90109E+01 |
| 276 | .90917E+01 |
| 277 | .41792E+01 |
| 278 | .44188E+01 |
| 279 | .50767E+01 |
| 280 | .56150E+01 |
| 281 | .59427E+01 |
| 282 | .60553E+01 |
| 283 | .18809E+01 |
| 284 | .20646E+01 |
| 285 | .24521E+01 |
| 286 | .27536E+01 |
| 287 | .29465E+01 |
| 288 | .30132E+01 |
| 289 | .27172E+01 |
| 290 | .28399E+01 |
| 291 | .32891E+01 |
| 292 | .36079E+01 |
| 293 | .38126E+01 |
| 294 | .38831E+01 |
| 295 | .31288E+01 |
| 296 | .32910E+01 |
| 297 | .38295E+01 |
| 298 | .42036E+01 |
| 299 | .44402E+01 |
| 300 | .45215E+01 |

FIPM3D FLOW UNDER DAM SUPPORTED ON TWO MEDIA FOUNDATION
 LOAD CASE 1

| NODE | PRESSURE |
|------|------------|
| 201 | .33356E+01 |
| 202 | .35338E+01 |
| 203 | .41688E+01 |
| 204 | .46206E+01 |
| 205 | .49064E+01 |
| 206 | .50040E+01 |
| 207 | .34012E+01 |
| 208 | .36566E+01 |
| 209 | .44126E+01 |
| 210 | .49697E+01 |
| 211 | .53162E+01 |
| 212 | .54338E+01 |
| 213 | .33572E+01 |
| 214 | .36129E+01 |
| 215 | .46428E+01 |
| 216 | .53247E+01 |
| 217 | .57417E+01 |
| 218 | .58825E+01 |
| 219 | .44771E+01 |
| 220 | .50189E+01 |
| 221 | .59281E+01 |
| 222 | .65910E+01 |
| 223 | .69927E+01 |
| 224 | .71301E+01 |
| 225 | .15262E+01 |
| 226 | .31408E+01 |
| 227 | .44157E+01 |
| 228 | .52024E+01 |
| 229 | .57006E+01 |
| 230 | .58710E+01 |
| 231 | . |
| 232 | .88879E+00 |
| 233 | .15877E+01 |
| 234 | .21364E+01 |
| 235 | .25041E+01 |
| 236 | .26388E+01 |
| 237 | . |
| 238 | .16794E+01 |
| 239 | .23931E+01 |
| 240 | .29639E+01 |
| 241 | .33393E+01 |
| 242 | .34766E+01 |
| 243 | . |
| 244 | .20407E+01 |
| 245 | .28855E+01 |
| 246 | .35013E+01 |
| 247 | .38995E+01 |
| 248 | .40439E+01 |
| 249 | . |
| 250 | .22369E+01 |

PIPM3D FLOW UNDER DAM SUPPORTED ON TWO MEDIA FOUNDATION

LOAD CASE 1

| NODE | PRESSURE |
|------|------------|
| 251 | .31790E+01 |
| 252 | .38587E+01 |
| 253 | .42907E+01 |
| 254 | .44459E+01 |
| 255 | . |
| 256 | .23669E+01 |
| 257 | .34111E+01 |
| 258 | .41669E+01 |
| 259 | .46407E+01 |
| 260 | .48090E+01 |
| 261 | . |
| 262 | .25467E+01 |
| 263 | .37384E+01 |
| 264 | .45768E+01 |
| 265 | .50923E+01 |
| 266 | .52749E+01 |
| 267 | . |
| 268 | .29415E+01 |
| 269 | .42983E+01 |
| 270 | .51934E+01 |
| 271 | .57468E+01 |
| 272 | .59434E+01 |
| 273 | . |
| 274 | .33503E+00 |
| 275 | .12627E+01 |
| 276 | .20413E+01 |
| 277 | .26774E+01 |
| 278 | .29009E+01 |
| 279 | . |
| 280 | .10711E+01 |
| 281 | .20104E+01 |
| 282 | .28033E+01 |
| 283 | .34437E+01 |
| 284 | .36685E+01 |
| 285 | . |
| 286 | .12553E+01 |
| 287 | .23161E+01 |
| 288 | .31354E+01 |
| 289 | .37884E+01 |
| 290 | .40169E+01 |
| 291 | . |
| 292 | .13553E+01 |
| 293 | .24871E+01 |
| 294 | .33450E+01 |
| 295 | .40161E+01 |
| 296 | .42502E+01 |
| 297 | . |
| 298 | .14385E+01 |
| 299 | .26339E+01 |
| 400 | .35336E+01 |

FI PM3D FLOW UNDER DAM SUPPORTED ON TWO MEDIA FOUNDATION
 LOAD CASE 1

| NODE | PRESSURE |
|------|------------|
| 401 | .42258E+01 |
| 402 | .44665E+01 |
| 403 | 0. |
| 404 | .15706E+01 |
| 405 | .28747E+01 |
| 406 | .38102E+01 |
| 407 | .45229E+01 |
| 408 | .47699E+01 |
| 409 | 0. |
| 410 | .23050E+01 |
| 411 | .35936E+01 |
| 412 | .45515E+01 |
| 413 | .52708E+01 |
| 414 | .55200E+01 |
| 415 | 0. |
| 416 | .10000E+01 |
| 417 | .20000E+01 |
| 418 | .30000E+01 |
| 419 | .40000E+01 |
| 420 | .50000E+01 |
| 421 | 0. |
| 422 | .10000E+01 |
| 423 | .20000E+01 |
| 424 | .30000E+01 |
| 425 | .40000E+01 |
| 426 | .50000E+01 |
| 427 | 0. |
| 428 | .10000E+01 |
| 429 | .20000E+01 |
| 430 | .30000E+01 |
| 431 | .40000E+01 |
| 432 | .50000E+01 |
| 433 | 0. |
| 434 | .10000E+01 |
| 435 | .20000E+01 |
| 436 | .30000E+01 |
| 437 | .40000E+01 |
| 438 | .50000E+01 |
| 439 | 0. |
| 440 | .10000E+01 |
| 441 | .20000E+01 |
| 442 | .30000E+01 |
| 443 | .40000E+01 |
| 444 | .50000E+01 |
| 445 | 0. |
| 446 | .10000E+01 |
| 447 | .20000E+01 |
| 448 | .30000E+01 |
| 449 | .40000E+01 |
| 450 | .50000E+01 |

FIPM3D FLOW UNDER DAM SUPPORTED ON TWO MEDIA FOUNDATION

LOAD CASE 1

| NODE | PRESSURE |
|------|------------|
| 451 | 0. |
| 452 | .10000E+01 |
| 453 | .20000E+01 |
| 454 | .30000E+01 |
| 455 | .40000E+01 |
| 456 | .50000E+01 |

FIPM3D FLOW UNDER DAM SUPPORTED ON TWO MEDIA FOUNDATION
 LOAD CASE 1

| ELEMENT | X | Y | Z | X | Y | Z | X | Y | Z | VFLOCITIES |
|---------|---------|--------|---------|------------|-------------|-----------|------------|-------------|-----------|------------|
| 1 | 8.50000 | .50000 | .50000 | .14846E+01 | .8154E+01 | .8154E+01 | .14846E+01 | .8154E+01 | .8154E+01 | .81598E+01 |
| 2 | 8.50000 | .50000 | 1.50000 | .81617E+00 | .10816E+02 | 1.50000 | .81617E+00 | .10816E+02 | 1.50000 | .95395E+01 |
| 3 | 8.50000 | .50000 | 2.50000 | .15266E+02 | .11527E+02 | 2.50000 | .15266E+02 | .11527E+02 | 2.50000 | .97501E+01 |
| 4 | 8.50000 | .50000 | 3.50000 | .19844E+01 | .11984E+02 | 3.50000 | .19844E+01 | .11984E+02 | 3.50000 | .97921E+01 |
| 5 | 8.50000 | .50000 | 4.50000 | .25225E+01 | .12522E+02 | 4.50000 | .25225E+01 | .12522E+02 | 4.50000 | .96697E+01 |
| 6 | 8.50000 | .50000 | 5.50000 | .46889E+01 | .14689E+02 | 5.50000 | .46889E+01 | .14689E+02 | 5.50000 | .81640E+01 |
| 7 | 8.50000 | .50000 | 1.50000 | .33017E+01 | .96675E+01 | 1.50000 | .33017E+01 | .96675E+01 | 1.50000 | .62905E+01 |
| 8 | 8.50000 | .50000 | 2.50000 | .16327E+01 | .10000E+02 | 2.50000 | .16327E+01 | .10000E+02 | 2.50000 | .87752E+01 |
| 9 | 8.50000 | .50000 | 3.50000 | .35346E+01 | .10481E+02 | 3.50000 | .35346E+01 | .10481E+02 | 3.50000 | .93228E+01 |
| 10 | 8.50000 | .50000 | 4.50000 | .47867E+01 | .10818E+02 | 4.50000 | .47867E+01 | .10818E+02 | 4.50000 | .94251E+01 |
| 11 | 8.50000 | .50000 | 5.50000 | .62941E+01 | .11249E+02 | 5.50000 | .62941E+01 | .11249E+02 | 5.50000 | .90676E+01 |
| 12 | 8.50000 | .50000 | 1.50000 | .10860E+02 | .11482E+02 | 1.50000 | .10860E+02 | .11482E+02 | 1.50000 | .63669E+01 |
| 13 | 8.50000 | .50000 | 2.50000 | .47056E+01 | .92285E+01 | 2.50000 | .47056E+01 | .92285E+01 | 2.50000 | .62256E+01 |
| 14 | 8.50000 | .50000 | 3.50000 | .66323E+00 | .90330E+01 | 3.50000 | .66323E+00 | .90330E+01 | 3.50000 | .84056E+01 |
| 15 | 8.50000 | .50000 | 4.50000 | .32090E+01 | .91930E+01 | 4.50000 | .32090E+01 | .91930E+01 | 4.50000 | .90486E+01 |
| 16 | 8.50000 | .50000 | 5.50000 | .49990E+01 | .93944E+01 | 5.50000 | .49990E+01 | .93944E+01 | 5.50000 | .91614E+01 |
| 17 | 8.50000 | .50000 | 1.50000 | .71312E+01 | .95881E+01 | 1.50000 | .71312E+01 | .95881E+01 | 1.50000 | .87064E+01 |
| 18 | 8.50000 | .50000 | 2.50000 | .12075E+02 | .97337E+01 | 2.50000 | .12075E+02 | .97337E+01 | 2.50000 | .63496E+01 |
| 19 | 8.50000 | .50000 | 3.50000 | .75859E+01 | .91911E+01 | 3.50000 | .75859E+01 | .91911E+01 | 3.50000 | .61791E+01 |
| 20 | 8.50000 | .50000 | 4.50000 | .20730E+01 | .92335E+01 | 4.50000 | .20730E+01 | .92335E+01 | 4.50000 | .83080E+01 |
| 21 | 8.50000 | .50000 | 5.50000 | .71237E+00 | .93103E+01 | 5.50000 | .71237E+00 | .93103E+01 | 5.50000 | .89067E+01 |
| 22 | 8.50000 | .50000 | 1.50000 | .28014E+01 | .94080E+01 | 1.50000 | .28014E+01 | .94080E+01 | 1.50000 | .90043E+01 |
| 23 | 8.50000 | .50000 | 2.50000 | .52315E+01 | .95121E+01 | 2.50000 | .52315E+01 | .95121E+01 | 2.50000 | .85656E+01 |
| 24 | 8.50000 | .50000 | 3.50000 | .10389E+02 | .95800E+01 | 3.50000 | .10389E+02 | .95800E+01 | 3.50000 | .62770E+01 |
| 25 | 8.50000 | .50000 | 4.50000 | .13274E+02 | .961210E+01 | 4.50000 | .13274E+02 | .961210E+01 | 4.50000 | .61652E+01 |
| 26 | 8.50000 | .50000 | 5.50000 | .77061E+01 | .961334E+01 | 5.50000 | .77061E+01 | .961334E+01 | 5.50000 | .82671E+01 |
| 27 | 8.50000 | .50000 | 1.50000 | .48208E+01 | .961565E+01 | 1.50000 | .48208E+01 | .961565E+01 | 1.50000 | .84477E+01 |
| 28 | 8.50000 | .50000 | 2.50000 | .26037E+01 | .961869E+01 | 2.50000 | .26037E+01 | .961869E+01 | 2.50000 | .89352E+01 |
| 29 | 8.50000 | .50000 | 3.50000 | .37433E+01 | .96190E+01 | 3.50000 | .37433E+01 | .96190E+01 | 3.50000 | .84986E+01 |
| 30 | 8.50000 | .50000 | 4.50000 | .52090E+01 | .962401E+01 | 4.50000 | .52090E+01 | .962401E+01 | 4.50000 | .62550E+01 |
| 31 | 7.50000 | .50000 | 5.50000 | .29052E+01 | .99360E+01 | 5.50000 | .29052E+01 | .99360E+01 | 5.50000 | .61831E+01 |
| 32 | 7.50000 | .50000 | 1.50000 | .34841E+01 | .15116E+02 | 1.50000 | .34841E+01 | .15116E+02 | 1.50000 | .86364E+01 |
| 33 | 7.50000 | .50000 | 2.50000 | .41673E+01 | .17221E+02 | 2.50000 | .41673E+01 | .17221E+02 | 2.50000 | .92595E+01 |
| 34 | 7.50000 | .50000 | 3.50000 | .45252E+01 | .18494E+02 | 3.50000 | .45252E+01 | .18494E+02 | 3.50000 | .94671E+01 |
| 35 | 7.50000 | .50000 | 4.50000 | .47616E+01 | .19807E+02 | 4.50000 | .47616E+01 | .19807E+02 | 4.50000 | .92202E+01 |
| 36 | 7.50000 | .50000 | 5.50000 | .40318E+01 | .23409E+02 | 5.50000 | .40318E+01 | .23409E+02 | 5.50000 | .71777E+01 |
| 37 | 7.50000 | .50000 | 1.50000 | .46742E+01 | .91989E+01 | 1.50000 | .46742E+01 | .91989E+01 | 1.50000 | .23002E+01 |
| 38 | 7.50000 | .50000 | 2.50000 | .58642E+01 | .88966E+01 | 2.50000 | .58642E+01 | .88966E+01 | 2.50000 | .66411E+01 |
| 39 | 7.50000 | .50000 | 3.50000 | .73207E+01 | .9488E+01 | 3.50000 | .73207E+01 | .9488E+01 | 3.50000 | .80984E+01 |
| 40 | 7.50000 | .50000 | 4.50000 | .81982E+01 | .10784E+02 | 4.50000 | .81982E+01 | .10784E+02 | 4.50000 | .85199E+01 |

FIPM3D FLOW UNDER DAM SUPPORTED ON TWO MEDIA FOUNDATION
 LOAD CASE 1

| ELEMENT | COORDINATES | | | VFLOCITIES | | |
|---------|-------------|---------|---------|------------|-----------|-----------|
| | X | Y | Z | X | Y | Z |
| 41 | 7.50000 | 1.50000 | 4.50000 | 88639E+01 | 11839E+02 | 77997E+01 |
| 42 | 7.50000 | 1.50000 | 5.50000 | 79528E+01 | 12853E+02 | 39804E+01 |
| 43 | 7.50000 | 2.50000 | 5.50000 | 24083E+01 | 67274E+01 | 21430E+01 |
| 44 | 7.50000 | 2.50000 | 1.50000 | 36964E+01 | 69967E+01 | 58312E+01 |
| 45 | 7.50000 | 2.50000 | 2.50000 | 53522E+01 | 74316E+01 | 74213E+01 |
| 46 | 7.50000 | 2.50000 | 3.50000 | 65402E+01 | 79829E+01 | 78108E+01 |
| 47 | 7.50000 | 2.50000 | 4.50000 | 76018E+01 | 85735E+01 | 68632E+01 |
| 48 | 7.50000 | 2.50000 | 5.50000 | 74422E+01 | 90675E+01 | 34084E+01 |
| 49 | 7.50000 | 3.50000 | 5.50000 | 54857E+01 | 50489E+01 | 20222E+01 |
| 50 | 7.50000 | 3.50000 | 1.50000 | 13332E+01 | 51676E+01 | 55640E+01 |
| 51 | 7.50000 | 3.50000 | 2.50000 | 31633E+01 | 53861E+01 | 70351E+01 |
| 52 | 7.50000 | 3.50000 | 3.50000 | 45910E+01 | 56727E+01 | 73591E+01 |
| 53 | 7.50000 | 3.50000 | 4.50000 | 59602E+01 | 59854E+01 | 64117E+01 |
| 54 | 7.50000 | 3.50000 | 5.50000 | 61344E+01 | 62521E+01 | 30992E+01 |
| 55 | 7.50000 | 4.50000 | 5.50000 | 18294E+01 | 18009E+01 | 19828E+01 |
| 56 | 7.50000 | 4.50000 | 1.50000 | 39578E+01 | 18374E+01 | 54482E+01 |
| 57 | 7.50000 | 4.50000 | 2.50000 | 15210E+01 | 19052E+01 | 68646E+01 |
| 58 | 7.50000 | 4.50000 | 3.50000 | 30695E+01 | 19956E+01 | 71527E+01 |
| 59 | 7.50000 | 4.50000 | 4.50000 | 45795E+01 | 20962E+01 | 62047E+01 |
| 60 | 7.50000 | 4.50000 | 5.50000 | 49345E+01 | 21882E+01 | 29474E+01 |
| 61 | 6.50000 | 5.00000 | 5.00000 | 17336E+02 | 71865E+01 | 39943E+01 |
| 62 | 6.50000 | 5.00000 | 1.50000 | 20642E+02 | 10012E+02 | 69401E+01 |
| 63 | 6.50000 | 5.00000 | 2.50000 | 22529E+02 | 11595E+02 | 83856E+01 |
| 64 | 6.50000 | 5.00000 | 3.50000 | 23308E+02 | 12644E+02 | 92038E+01 |
| 65 | 6.50000 | 5.00000 | 4.50000 | 22786E+02 | 13562E+02 | 97698E+01 |
| 66 | 6.50000 | 5.00000 | 5.00000 | 10242E+02 | 56232E+01 | 19793E+01 |
| 67 | 6.50000 | 1.50000 | 1.50000 | 10627E+02 | 63655E+01 | 53868E+01 |
| 68 | 6.50000 | 1.50000 | 2.50000 | 11203E+02 | 74012E+01 | 73206E+01 |
| 69 | 6.50000 | 1.50000 | 3.50000 | 11445E+02 | 84434E+01 | 81781E+01 |
| 70 | 6.50000 | 1.50000 | 4.50000 | 10654E+02 | 10055E+02 | 82660E+01 |
| 71 | 6.50000 | 2.50000 | 5.00000 | 75542E+01 | 43497E+01 | 16894E+01 |
| 72 | 6.50000 | 2.50000 | 1.50000 | 79657E+01 | 46989E+01 | 45853E+01 |
| 73 | 6.50000 | 2.50000 | 2.50000 | 84952E+01 | 53033E+01 | 64819E+01 |
| 74 | 6.50000 | 2.50000 | 3.50000 | 88903E+01 | 61108E+01 | 71671E+01 |
| 75 | 6.50000 | 2.50000 | 4.50000 | 86419E+01 | 70829E+01 | 66938E+01 |
| 76 | 6.50000 | 3.50000 | 5.00000 | 54424E+01 | 28516E+01 | 15419E+01 |
| 77 | 6.50000 | 3.50000 | 1.50000 | 59008E+01 | 30372E+01 | 41979E+01 |
| 78 | 6.50000 | 3.50000 | 2.50000 | 65514E+01 | 33816E+01 | 59205E+01 |
| 79 | 6.50000 | 3.50000 | 3.50000 | 71399E+01 | 38452E+01 | 64575E+01 |
| 80 | 6.50000 | 3.50000 | 4.50000 | 71893E+01 | 43818E+01 | 58947E+01 |

FIPM3D FLOW UNDER DAM SUPPORTED ON TWO MEDIA FOUNDATION
 LOAD CASE 1

| ELEMENT | X | Y | Z | X | Y | Z | X | Y | Z |
|---------|---------|---------|---------|------------|------------|------------|---|---|---|
| 81 | 6.50000 | 4.50000 | 1.50000 | 1.50000 | 1.0227E+01 | 1.4775E+01 | | | |
| 82 | 6.50000 | 4.50000 | 1.50000 | 1.50000 | 1.0833E+01 | 1.4016E+01 | | | |
| 83 | 6.50000 | 4.50000 | 2.50000 | 1.50000 | 1.1962E+01 | 1.5645E+01 | | | |
| 84 | 6.50000 | 4.50000 | 3.50000 | 1.50000 | 1.3469E+01 | 1.6118E+01 | | | |
| 85 | 6.50000 | 4.50000 | 4.50000 | 1.50000 | 1.5231E+01 | 1.5520E+01 | | | |
| 86 | 5.50000 | 5.00000 | 1.50000 | 1.7565E+02 | 1.9962E+01 | 1.5695E+01 | | | |
| 87 | 5.50000 | 5.00000 | 1.50000 | 1.7501E+02 | 1.9224E+01 | 1.5695E+01 | | | |
| 88 | 5.50000 | 5.00000 | 2.50000 | 1.7282E+02 | 1.2749E+01 | 1.7962E+01 | | | |
| 89 | 5.50000 | 5.00000 | 3.50000 | 1.6631E+02 | 1.7723E+01 | 1.9498E+01 | | | |
| 90 | 5.50000 | 5.00000 | 4.50000 | 1.4967E+02 | 1.2252E+01 | 1.1905E+01 | | | |
| 91 | 5.50000 | 5.00000 | 1.50000 | 1.4911E+02 | 1.2849E+01 | 1.5137E+01 | | | |
| 92 | 5.50000 | 5.00000 | 2.50000 | 1.4614E+02 | 1.7268E+01 | 1.7291E+01 | | | |
| 93 | 5.50000 | 5.00000 | 3.50000 | 1.4004E+02 | 1.8239E+01 | 1.8574E+01 | | | |
| 94 | 5.50000 | 5.00000 | 4.50000 | 1.1684E+02 | 1.7502E+01 | 1.1587E+01 | | | |
| 95 | 5.50000 | 2.50000 | 1.50000 | 1.1534E+02 | 1.2177E+01 | 1.4258E+01 | | | |
| 96 | 5.50000 | 2.50000 | 2.50000 | 1.1284E+02 | 1.2940E+01 | 1.6362E+01 | | | |
| 97 | 5.50000 | 2.50000 | 3.50000 | 1.0832E+02 | 1.4003E+01 | 1.7343E+01 | | | |
| 98 | 5.50000 | 3.50000 | 1.50000 | 9.4570E+01 | 1.1119E+01 | 1.4026E+01 | | | |
| 99 | 5.50000 | 3.50000 | 2.50000 | 9.4244E+01 | 1.3843E+01 | 1.3911E+01 | | | |
| 00 | 5.50000 | 3.50000 | 3.50000 | 9.3631E+01 | 1.8803E+01 | 1.5617E+01 | | | |
| 101 | 5.50000 | 3.50000 | 4.50000 | 9.1693E+01 | 1.2539E+01 | 1.6365E+01 | | | |
| 102 | 5.50000 | 4.50000 | 1.50000 | 8.2904E+01 | 1.2948E+01 | 1.1306E+01 | | | |
| 103 | 5.50000 | 4.50000 | 2.50000 | 8.3288E+01 | 1.4851E+01 | 1.3644E+01 | | | |
| 104 | 5.50000 | 4.50000 | 3.50000 | 8.3875E+01 | 1.6506E+01 | 1.5223E+01 | | | |
| 105 | 5.50000 | 4.50000 | 4.50000 | 8.3415E+01 | 1.8700E+01 | 1.5881E+01 | | | |
| 106 | 4.50000 | 5.00000 | 1.50000 | 2.1610E+02 | 1.8042E+01 | 1.2584E+01 | | | |
| 107 | 4.50000 | 5.00000 | 2.50000 | 2.0072E+02 | 1.4231E+01 | 1.6709E+01 | | | |
| 108 | 4.50000 | 5.00000 | 3.50000 | 1.7633E+02 | 1.1053E+01 | 1.9606E+01 | | | |
| 109 | 4.50000 | 5.00000 | 4.50000 | 1.8785E+02 | 1.4999E+01 | 1.2250E+01 | | | |
| 110 | 4.50000 | 5.00000 | 1.50000 | 1.7607E+02 | 1.4062E+01 | 1.6021E+01 | | | |
| 111 | 4.50000 | 5.00000 | 2.50000 | 1.5731E+02 | 1.3257E+01 | 1.8580E+01 | | | |
| 112 | 4.50000 | 5.00000 | 3.50000 | 1.5102E+02 | 1.4629E+01 | 1.1841E+01 | | | |
| 113 | 4.50000 | 5.00000 | 4.50000 | 1.4384E+02 | 1.7324E+01 | 1.5040E+01 | | | |
| 114 | 4.50000 | 5.00000 | 1.50000 | 1.3204E+02 | 1.4843E+01 | 1.7179E+01 | | | |
| 115 | 4.50000 | 5.00000 | 2.50000 | 1.2307E+02 | 1.6982E+01 | 1.1527E+01 | | | |
| 116 | 4.50000 | 5.00000 | 3.50000 | 1.1912E+02 | 1.2875E+01 | 1.4213E+01 | | | |
| 117 | 4.50000 | 5.00000 | 4.50000 | 1.1229E+02 | 1.4406E+01 | 1.6060E+01 | | | |
| 118 | 4.50000 | 4.50000 | 1.50000 | 1.1080E+02 | 1.8780E+01 | 1.1381E+01 | | | |
| 119 | 4.50000 | 4.50000 | 2.50000 | 1.0795E+02 | 1.5538E+01 | 1.3816E+01 | | | |
| 120 | 4.50000 | 4.50000 | 3.50000 | 1.0295E+02 | 1.1811E+01 | 1.5492E+01 | | | |

FIPM3D FLOW UNDER DAM SUPPORTED ON TWO MEDIA FOUNDATION
 LOAD CASE 1

| ELEMENT | COORDINATES | | | VFLOCITIES | | |
|---------|-------------|---------|--------|------------|------------|------------|
| | X | Y | Z | X | Y | Z |
| 121 | 3.50000 | .50000 | .50000 | .32022E+02 | .29621E+01 | .44938F+01 |
| 122 | 3.50000 | .50000 | .50000 | .26243E+02 | .20027E+01 | .12117E+02 |
| 123 | 3.50000 | 1.50000 | .50000 | .24964E+02 | .92259E+01 | .35384E+01 |
| 124 | 3.50000 | 1.50000 | .50000 | .21494E+02 | .64936E+01 | .93804E+01 |
| 125 | 3.50000 | 2.50000 | .50000 | .17077E+02 | .53056E+01 | .24331F+01 |
| 126 | 3.50000 | 2.50000 | .50000 | .15776E+02 | .40214E+01 | .64691F+01 |
| 127 | 3.50000 | 3.50000 | .50000 | .14195E+02 | .25331E+01 | .18661F+01 |
| 128 | 3.50000 | 3.50000 | .50000 | .13331E+02 | .19155E+01 | .51344F+01 |
| 129 | 3.50000 | 4.50000 | .50000 | .13049E+02 | .72512E+00 | .16440F+01 |
| 130 | 3.50000 | 4.50000 | .50000 | .12330E+02 | .54510E+00 | .45588E+01 |
| 131 | 2.50000 | .50000 | .50000 | .64897E+02 | .42208E+02 | .77602F+01 |
| 132 | 2.50000 | 1.50000 | .50000 | .23102E+02 | .18833E+02 | .56536E+01 |
| 133 | 2.50000 | 2.50000 | .50000 | .17667E+02 | .90198E+01 | .36075F+01 |
| 134 | 2.50000 | 3.50000 | .50000 | .15465E+02 | .19033E+01 | .27360E+01 |
| 135 | 2.50000 | 4.50000 | .50000 | .14886E+02 | .10795E+01 | .24996F+01 |
| 136 | 1.62500 | .50000 | .37500 | .13923E+02 | .70005E+02 | .94146F+01 |
| 137 | 1.62500 | 1.50000 | .37500 | .23384E+02 | .26266E+02 | .72918F+01 |
| 138 | 1.62500 | 2.50000 | .37500 | .19321E+02 | .10582E+02 | .52403F+01 |
| 139 | 1.62500 | 3.50000 | .37500 | .20028E+02 | .41486E+01 | .47010F+01 |
| 140 | 1.62500 | 4.50000 | .37500 | .20499E+02 | .10726E+01 | .46487E+01 |
| 141 | 2.62500 | .50000 | .37500 | .53777E+02 | .26308E+02 | .25749F+02 |
| 142 | 2.62500 | 1.50000 | .37500 | .22007E+02 | .14245E+02 | .11829F+02 |
| 143 | 2.62500 | 2.50000 | .37500 | .16463E+02 | .71046E+01 | .80001E+01 |
| 144 | 2.62500 | 3.50000 | .37500 | .14505E+02 | .92240E+01 | .60887F+01 |
| 145 | 2.62500 | 4.50000 | .37500 | .13848E+02 | .98704E+00 | .54605F+01 |
| 146 | 3.62500 | .50000 | .37500 | .20756E+02 | .93315E+00 | .12124E+02 |
| 147 | 3.62500 | 1.50000 | .37500 | .18111E+02 | .29333E+01 | .10481E+02 |
| 148 | 3.62500 | 2.50000 | .37500 | .14503E+02 | .20598E+01 | .82033F+01 |
| 149 | 3.62500 | 3.50000 | .37500 | .12463E+02 | .99784E+00 | .66902F+01 |
| 150 | 3.62500 | 4.50000 | .37500 | .11602E+02 | .23801E+00 | .59784E+01 |
| 151 | 4.62500 | .50000 | .37500 | .15917E+02 | .79787E+00 | .10221E+02 |
| 152 | 4.62500 | 1.50000 | .37500 | .14400E+02 | .17846E+01 | .92269E+01 |
| 153 | 4.62500 | 2.50000 | .37500 | .12350E+02 | .19853E+01 | .78335F+01 |
| 154 | 4.62500 | 3.50000 | .37500 | .10692E+02 | .13569E+01 | .66535E+01 |
| 155 | 4.62500 | 4.50000 | .37500 | .98976E+01 | .47978E+00 | .60555E+01 |
| 156 | 5.62500 | .50000 | .37500 | .16015E+02 | .22774E+01 | .10614E+02 |
| 157 | 5.62500 | 1.50000 | .37500 | .13463E+02 | .69402E+01 | .92005E+01 |
| 158 | 5.62500 | 2.50000 | .37500 | .10346E+02 | .53596E+01 | .72521E+01 |
| 159 | 5.62500 | 3.50000 | .37500 | .89124E+01 | .33132E+01 | .61942E+01 |
| 160 | 5.62500 | 4.50000 | .37500 | .81859E+01 | .11287E+01 | .57055F+01 |

FLPM3D FLOW UNDER DAM SUPPORTED ON TWO MEDIA FOUNDATION
 LOAD CASE 1

| ELEMENT | X | Y | Z | X | Y | Z | X | Y | Z | VFLOCITIES | Z |
|---------|---------|---------|---------|------------|------------|---------|---------|---------|---------|-------------|------------|
| 161 | 6.62500 | 5.50000 | 5.37500 | 2.0673E+02 | 1.8396E+02 | 5.37500 | 6.62500 | 5.50000 | 5.37500 | 1.94700E+01 | 9.4700E+01 |
| 162 | 6.62500 | 1.50000 | 5.37500 | 8.8966E+01 | 1.2133E+02 | 5.37500 | 6.62500 | 5.50000 | 5.37500 | 6.1830E+01 | 6.1830E+01 |
| 163 | 6.62500 | 2.50000 | 5.37500 | 7.7039E+01 | 8.0053E+01 | 5.37500 | 6.62500 | 5.50000 | 5.37500 | 4.6754E+01 | 4.6754E+01 |
| 164 | 6.62500 | 3.50000 | 5.37500 | 6.4852E+01 | 6.4960E+01 | 5.37500 | 6.62500 | 5.50000 | 5.37500 | 4.1461E+01 | 4.1461E+01 |
| 165 | 6.62500 | 4.50000 | 5.37500 | 5.8573E+01 | 5.8573E+01 | 5.37500 | 6.62500 | 5.50000 | 5.37500 | 3.8125E+01 | 3.8125E+01 |
| 166 | 1.37500 | 5.00000 | 6.25000 | 2.5891E+01 | 2.5891E+01 | 6.25000 | 1.37500 | 5.00000 | 6.25000 | 2.5532E+00 | 2.5532E+00 |
| 167 | 1.37500 | 1.50000 | 6.25000 | 5.4952E+01 | 5.4952E+01 | 6.25000 | 1.37500 | 1.50000 | 6.25000 | 2.4276E+01 | 2.4276E+01 |
| 168 | 1.37500 | 2.50000 | 6.25000 | 6.1445E+01 | 6.1445E+01 | 6.25000 | 1.37500 | 2.50000 | 6.25000 | 3.6883E+01 | 3.6883E+01 |
| 169 | 1.37500 | 3.50000 | 6.25000 | 6.7513E+01 | 6.7513E+01 | 6.25000 | 1.37500 | 3.50000 | 6.25000 | 4.2784E+01 | 4.2784E+01 |
| 170 | 1.37500 | 4.50000 | 6.25000 | 7.1132E+01 | 7.1132E+01 | 6.25000 | 1.37500 | 4.50000 | 6.25000 | 4.5984E+01 | 4.5984E+01 |
| 171 | 2.37500 | 5.00000 | 1.62500 | 8.9298E+01 | 8.9298E+01 | 1.62500 | 2.37500 | 5.00000 | 1.62500 | 9.7719E+00 | 9.7719E+00 |
| 172 | 2.37500 | 1.50000 | 1.62500 | 4.8067E+01 | 4.8067E+01 | 1.62500 | 2.37500 | 1.50000 | 1.62500 | 1.4230E+01 | 1.4230E+01 |
| 173 | 2.37500 | 2.50000 | 1.62500 | 4.5226E+01 | 4.5226E+01 | 1.62500 | 2.37500 | 2.50000 | 1.62500 | 2.0763E+01 | 2.0763E+01 |
| 174 | 2.37500 | 3.50000 | 1.62500 | 4.4914E+01 | 4.4914E+01 | 1.62500 | 2.37500 | 3.50000 | 1.62500 | 2.4321E+01 | 2.4321E+01 |
| 175 | 2.37500 | 4.50000 | 1.62500 | 5.475E+01 | 5.475E+01 | 1.62500 | 2.37500 | 4.50000 | 1.62500 | 2.6167E+01 | 2.6167E+01 |
| 176 | 3.37500 | 5.00000 | 2.62500 | 4.7797E+01 | 4.7797E+01 | 2.62500 | 3.37500 | 5.00000 | 2.62500 | 1.4916E+01 | 1.4916E+01 |
| 177 | 3.37500 | 1.50000 | 2.62500 | 4.2638E+01 | 4.2638E+01 | 2.62500 | 3.37500 | 1.50000 | 2.62500 | 1.4046E+01 | 1.4046E+01 |
| 178 | 3.37500 | 2.50000 | 2.62500 | 3.6837E+01 | 3.6837E+01 | 2.62500 | 3.37500 | 2.50000 | 2.62500 | 1.4132E+01 | 1.4132E+01 |
| 179 | 3.37500 | 3.50000 | 2.62500 | 3.4803E+01 | 3.4803E+01 | 2.62500 | 3.37500 | 3.50000 | 2.62500 | 1.5650E+01 | 1.5650E+01 |
| 180 | 3.37500 | 4.50000 | 2.62500 | 3.4083E+01 | 3.4083E+01 | 2.62500 | 3.37500 | 4.50000 | 2.62500 | 1.6503E+01 | 1.6503E+01 |
| 181 | 4.37500 | 5.00000 | 3.62500 | 3.6665E+01 | 3.6665E+01 | 3.62500 | 4.37500 | 5.00000 | 3.62500 | 1.0527E+01 | 1.0527E+01 |
| 182 | 4.37500 | 1.50000 | 3.62500 | 3.4007E+01 | 3.4007E+01 | 3.62500 | 4.37500 | 1.50000 | 3.62500 | 1.0380E+01 | 1.0380E+01 |
| 183 | 4.37500 | 2.50000 | 3.62500 | 3.0558E+01 | 3.0558E+01 | 3.62500 | 4.37500 | 2.50000 | 3.62500 | 1.0374E+01 | 1.0374E+01 |
| 184 | 4.37500 | 3.50000 | 3.62500 | 2.7952E+01 | 2.7952E+01 | 3.62500 | 4.37500 | 3.50000 | 3.62500 | 1.0607E+01 | 1.0607E+01 |
| 185 | 4.37500 | 4.50000 | 3.62500 | 2.6816E+01 | 2.6816E+01 | 3.62500 | 4.37500 | 4.50000 | 3.62500 | 1.0863E+01 | 1.0863E+01 |
| 186 | 5.37500 | 5.00000 | 4.62500 | 3.3408E+01 | 3.3408E+01 | 4.62500 | 5.37500 | 5.00000 | 4.62500 | 1.6779E+00 | 1.6779E+00 |
| 187 | 5.37500 | 1.50000 | 4.62500 | 2.9413E+01 | 2.9413E+01 | 4.62500 | 5.37500 | 1.50000 | 4.62500 | 6.7492E+00 | 6.7492E+00 |
| 188 | 5.37500 | 2.50000 | 4.62500 | 2.4331E+01 | 2.4331E+01 | 4.62500 | 5.37500 | 2.50000 | 4.62500 | 6.7329E+00 | 6.7329E+00 |
| 189 | 5.37500 | 3.50000 | 4.62500 | 2.1678E+01 | 2.1678E+01 | 4.62500 | 5.37500 | 3.50000 | 4.62500 | 6.5710E+00 | 6.5710E+00 |
| 190 | 5.37500 | 4.50000 | 4.62500 | 2.0421E+01 | 2.0421E+01 | 4.62500 | 5.37500 | 4.50000 | 4.62500 | 6.5339E+00 | 6.5339E+00 |
| 191 | 6.37500 | 5.00000 | 5.62500 | 3.4216E+01 | 3.4216E+01 | 5.62500 | 6.37500 | 5.00000 | 5.62500 | 4.0729E+00 | 4.0729E+00 |
| 192 | 6.37500 | 1.50000 | 5.62500 | 1.9492E+01 | 1.9492E+01 | 5.62500 | 6.37500 | 1.50000 | 5.62500 | 4.4125E+00 | 4.4125E+00 |
| 193 | 6.37500 | 2.50000 | 5.62500 | 1.5695E+01 | 1.5695E+01 | 5.62500 | 6.37500 | 2.50000 | 5.62500 | 3.3154E+00 | 3.3154E+00 |
| 194 | 6.37500 | 3.50000 | 5.62500 | 1.3719E+01 | 1.3719E+01 | 5.62500 | 6.37500 | 3.50000 | 5.62500 | 3.0879E+00 | 3.0879E+00 |
| 195 | 6.37500 | 4.50000 | 5.62500 | 1.2591E+01 | 1.2591E+01 | 5.62500 | 6.37500 | 4.50000 | 5.62500 | 2.9213E+00 | 2.9213E+00 |
| 196 | 5.00000 | 5.00000 | 5.00000 | 2.5244E+01 | 2.5244E+01 | 5.00000 | 5.00000 | 5.00000 | 5.00000 | 3.6054E+00 | 3.6054E+00 |
| 197 | 5.00000 | 5.00000 | 1.50000 | 1.6216E+01 | 1.6216E+01 | 1.50000 | 5.00000 | 5.00000 | 1.50000 | 7.3667E+00 | 7.3667E+00 |
| 198 | 5.00000 | 5.00000 | 2.50000 | 1.2145E+01 | 1.2145E+01 | 2.50000 | 5.00000 | 5.00000 | 2.50000 | 8.5627E+00 | 8.5627E+00 |
| 199 | 5.00000 | 5.00000 | 3.50000 | 9.7214E+00 | 9.7214E+00 | 3.50000 | 5.00000 | 5.00000 | 3.50000 | 9.0136E+00 | 9.0136E+00 |
| 200 | 5.00000 | 5.00000 | 4.50000 | 7.8774E+00 | 7.8774E+00 | 4.50000 | 5.00000 | 5.00000 | 4.50000 | 9.1423E+00 | 9.1423E+00 |

FIPM3D FLOW UNDER DAM SUPPORTED ON TWO MEDIA FOUNDATION
 LOAD CASE 1

| ELEMENT | X | Y | Z | X | Y | Z | VFLOCITIES | Z |
|---------|--------|---------|---------|------------|--------|---------|------------|------------|
| 201 | .50000 | .50000 | 5.50000 | .50547E+00 | .50000 | 5.50000 | .49453E+00 | .80350F+00 |
| 202 | .50000 | 1.50000 | 5.50000 | .67400E+01 | .50000 | 5.50000 | .69131E+00 | .69273E+00 |
| 203 | .50000 | 1.50000 | 1.50000 | .43567E+01 | .50000 | 1.50000 | .11352E+00 | .30937E+00 |
| 204 | .50000 | 1.50000 | 2.50000 | .32797E+01 | .50000 | 2.50000 | .14933E+00 | .61366F+00 |
| 205 | .50000 | 1.50000 | 3.50000 | .26312E+01 | .50000 | 3.50000 | .21312E+00 | .73782F+00 |
| 206 | .50000 | 1.50000 | 4.50000 | .21419E+01 | .50000 | 4.50000 | .43358E+00 | .77292F+00 |
| 207 | .50000 | 1.50000 | 5.50000 | .15109E+01 | .50000 | 5.50000 | .50007E+00 | .59605F+00 |
| 208 | .50000 | 2.50000 | 5.50000 | .92829E+01 | .50000 | 5.50000 | .14843E+00 | .12822F+01 |
| 209 | .50000 | 2.50000 | 1.50000 | .60600E+01 | .50000 | 1.50000 | .61020E+00 | .59264F+01 |
| 210 | .50000 | 2.50000 | 2.50000 | .45876E+01 | .50000 | 2.50000 | .54273E+00 | .46838F+00 |
| 211 | .50000 | 2.50000 | 3.50000 | .37000E+01 | .50000 | 3.50000 | .61807E+00 | .64397E+00 |
| 212 | .50000 | 2.50000 | 4.50000 | .30449E+01 | .50000 | 4.50000 | .66346E+00 | .70092F+00 |
| 213 | .50000 | 2.50000 | 5.50000 | .23242E+01 | .50000 | 5.50000 | .68661E+00 | .57840F+00 |
| 214 | .50000 | 3.50000 | 5.50000 | .10700E+02 | .50000 | 5.50000 | .43405E+00 | .15736F+01 |
| 215 | .50000 | 3.50000 | 1.50000 | .70549E+01 | .50000 | 1.50000 | .59290E+00 | .69969F+01 |
| 216 | .50000 | 3.50000 | 2.50000 | .53846E+01 | .50000 | 2.50000 | .66036E+00 | .39763F+00 |
| 217 | .50000 | 3.50000 | 3.50000 | .43839E+01 | .50000 | 3.50000 | .69797E+00 | .60176F+00 |
| 218 | .50000 | 3.50000 | 4.50000 | .36629E+01 | .50000 | 4.50000 | .71854E+00 | .67717F+00 |
| 219 | .50000 | 3.50000 | 5.50000 | .29094E+01 | .50000 | 5.50000 | .72814E+00 | .56941F+00 |
| 220 | .50000 | 4.50000 | 5.50000 | .11774E+02 | .50000 | 5.50000 | .49234E+00 | .17258E+01 |
| 221 | .50000 | 4.50000 | 1.50000 | .79203E+01 | .50000 | 1.50000 | .54366E+00 | .12789F+00 |
| 222 | .50000 | 4.50000 | 2.50000 | .61582E+01 | .50000 | 2.50000 | .56595E+00 | .36580F+00 |
| 223 | .50000 | 4.50000 | 3.50000 | .51084E+01 | .50000 | 3.50000 | .57754E+00 | .58438E+00 |
| 224 | .50000 | 4.50000 | 4.50000 | .43606E+01 | .50000 | 4.50000 | .58373E+00 | .66779F+00 |
| 225 | .50000 | 4.50000 | 5.50000 | .35948E+01 | .50000 | 5.50000 | .58646E+00 | .56645F+00 |
| 226 | .50000 | 5.50000 | 5.50000 | .23488E+01 | .50000 | 5.50000 | .45920E+01 | .20954F+00 |
| 227 | .50000 | 5.50000 | 1.50000 | .18851E+01 | .50000 | 1.50000 | .33141E+01 | .51258F+00 |
| 228 | .50000 | 5.50000 | 2.50000 | .15434E+01 | .50000 | 2.50000 | .24877E+01 | .66103F+00 |
| 229 | .50000 | 5.50000 | 3.50000 | .12952E+01 | .50000 | 3.50000 | .18706E+01 | .72187E+00 |
| 230 | .50000 | 5.50000 | 4.50000 | .11546E+01 | .50000 | 4.50000 | .11656E+01 | .57306E+00 |
| 231 | .50000 | 5.50000 | 5.50000 | .49261E+01 | .50000 | 5.50000 | .14554E+01 | .90822E+00 |
| 232 | .50000 | 1.50000 | 5.50000 | .40011E+01 | .50000 | 5.50000 | .93229E+00 | .17064E+00 |
| 233 | .50000 | 1.50000 | 1.50000 | .33139E+01 | .50000 | 1.50000 | .60072E+00 | .18631E+00 |
| 234 | .50000 | 1.50000 | 2.50000 | .28058E+01 | .50000 | 2.50000 | .34836E+00 | .32713E+00 |
| 235 | .50000 | 1.50000 | 3.50000 | .25176E+01 | .50000 | 3.50000 | .20821E+00 | .12258E+00 |
| 236 | .50000 | 1.50000 | 4.50000 | .54537E+01 | .50000 | 4.50000 | .47886E+00 | .14483F+01 |
| 237 | .50000 | 1.50000 | 5.50000 | .44760E+01 | .50000 | 5.50000 | .15847E+00 | .47405F+00 |
| 238 | .50000 | 2.50000 | 5.50000 | .37612E+01 | .50000 | 5.50000 | .15749E+01 | .16068F+01 |
| 239 | .50000 | 2.50000 | 1.50000 | .32262E+01 | .50000 | 1.50000 | .12202E+00 | .17086F+00 |
| 240 | .50000 | 2.50000 | 2.50000 | .29214E+01 | .50000 | 2.50000 | .17779E+00 | .82925F+01 |

FILPM3D FLOW UNDER DAM SUPPORTED ON TWO MEDIA FOUNDATION
LOAD CASE 1

| ELEMENT | X | Y | Z | X | Y | Z | X | Y | Z | VFLOCITIES |
|---------|---------|---------|---------|------------|------------|---------|------------|------------|---------|-------------|
| 241 | 1.50000 | 3.50000 | 1.50000 | .59894E+01 | .50613E-01 | .50000 | .59894E+01 | .50613E-01 | .50000 | .17706E+01 |
| 242 | 1.50000 | 3.50000 | 2.50000 | .49215E+01 | .11911E+00 | 2.50000 | .49215E+01 | .11911E+00 | 2.50000 | .64188E+00 |
| 243 | 1.50000 | 3.50000 | 3.50000 | .41655E+01 | .21209E+00 | 3.50000 | .41655E+01 | .21209E+00 | 3.50000 | .11544E+00 |
| 244 | 1.50000 | 3.50000 | 4.50000 | .36055E+01 | .26266E+00 | 4.50000 | .36055E+01 | .26266E+00 | 4.50000 | .11338E+00 |
| 245 | 1.50000 | 3.50000 | 5.50000 | .32869E+01 | .28611E+00 | 5.50000 | .32869E+01 | .28611E+00 | 5.50000 | .61188E-01 |
| 246 | 1.50000 | 4.50000 | 1.50000 | .63038E+01 | .92994E-02 | 1.50000 | .63038E+01 | .92994E-02 | 1.50000 | .19184E+01 |
| 247 | 1.50000 | 4.50000 | 2.50000 | .51886E+01 | .66478E-01 | 2.50000 | .51886E+01 | .66478E-01 | 2.50000 | .72101E+00 |
| 248 | 1.50000 | 4.50000 | 3.50000 | .44086E+01 | .95838E-01 | 3.50000 | .44086E+01 | .95838E-01 | 3.50000 | .15864E+00 |
| 249 | 1.50000 | 4.50000 | 4.50000 | .38359E+01 | .11152E+00 | 4.50000 | .38359E+01 | .11152E+00 | 4.50000 | .90319E-01 |
| 250 | 1.50000 | 4.50000 | 5.50000 | .35116E+01 | .11842E+00 | 5.50000 | .35116E+01 | .11842E+00 | 5.50000 | .53903E-01 |
| 251 | 2.50000 | .50000 | 2.50000 | .71589E+01 | .26878E+01 | 2.50000 | .71589E+01 | .26878E+01 | 2.50000 | .53532E+00 |
| 252 | 2.50000 | .50000 | 3.50000 | .58079E+01 | .21012E+01 | 3.50000 | .58079E+01 | .21012E+01 | 3.50000 | .16276E-01 |
| 253 | 2.50000 | .50000 | 4.50000 | .49273E+01 | .16445E+01 | 4.50000 | .49273E+01 | .16445E+01 | 4.50000 | .23778E+00 |
| 254 | 2.50000 | .50000 | 5.50000 | .42627E+01 | .12218E+01 | 5.50000 | .42627E+01 | .12218E+01 | 5.50000 | .25197E+00 |
| 255 | 2.50000 | 1.50000 | 2.50000 | .44415E+01 | .95718E+00 | 2.50000 | .44415E+01 | .95718E+00 | 2.50000 | .94594E+00 |
| 256 | 2.50000 | 1.50000 | 3.50000 | .38117E+01 | .76148E+00 | 3.50000 | .38117E+01 | .76148E+00 | 3.50000 | .35546E+00 |
| 257 | 2.50000 | 1.50000 | 4.50000 | .33838E+01 | .54161E+00 | 4.50000 | .33838E+01 | .54161E+00 | 4.50000 | .67037E-01 |
| 258 | 2.50000 | 1.50000 | 5.50000 | .31577E+01 | .41000E+00 | 5.50000 | .31577E+01 | .41000E+00 | 5.50000 | .24356E-02 |
| 259 | 2.50000 | 2.50000 | 2.50000 | .42150E+01 | .38198E+00 | 2.50000 | .42150E+01 | .38198E+00 | 2.50000 | .11313E+01 |
| 260 | 2.50000 | 2.50000 | 3.50000 | .37509E+01 | .21002E+00 | 3.50000 | .37509E+01 | .21002E+00 | 3.50000 | .53773E+00 |
| 261 | 2.50000 | 2.50000 | 4.50000 | .33867E+01 | .10805E+00 | 4.50000 | .33867E+01 | .10805E+00 | 4.50000 | .20660E+00 |
| 262 | 2.50000 | 2.50000 | 5.50000 | .31853E+01 | .51752E-01 | 5.50000 | .31853E+01 | .51752E-01 | 5.50000 | .45910E-01 |
| 263 | 2.50000 | 3.50000 | 2.50000 | .42287E+01 | .11661E+00 | 2.50000 | .42287E+01 | .11661E+00 | 2.50000 | .13109E+01 |
| 264 | 2.50000 | 3.50000 | 3.50000 | .37954E+01 | .10909E-01 | 3.50000 | .37954E+01 | .10909E-01 | 3.50000 | .63578E+00 |
| 265 | 2.50000 | 3.50000 | 4.50000 | .34546E+01 | .45593E-01 | 4.50000 | .34546E+01 | .45593E-01 | 4.50000 | .26703E+00 |
| 266 | 2.50000 | 3.50000 | 5.50000 | .32641E+01 | .71250E-01 | 5.50000 | .32641E+01 | .71250E-01 | 5.50000 | .67437E-01 |
| 267 | 2.50000 | 4.50000 | 2.50000 | .42826E+01 | .18750E-01 | 2.50000 | .42826E+01 | .18750E-01 | 2.50000 | .14028E+01 |
| 268 | 2.50000 | 4.50000 | 3.50000 | .38541E+01 | .17053E-01 | 3.50000 | .38541E+01 | .17053E-01 | 3.50000 | .68541E+00 |
| 269 | 2.50000 | 4.50000 | 4.50000 | .35173E+01 | .15521E-01 | 4.50000 | .35173E+01 | .15521E-01 | 4.50000 | .29236E+00 |
| 270 | 2.50000 | 4.50000 | 5.50000 | .33292E+01 | .43487E-01 | 5.50000 | .33292E+01 | .43487E-01 | 5.50000 | .75725E-01 |
| 271 | 3.50000 | .50000 | 3.50000 | .44025E+01 | .95350E-01 | 3.50000 | .44025E+01 | .95350E-01 | 3.50000 | .755561E+00 |
| 272 | 3.50000 | .50000 | 4.50000 | .39577E+01 | .72907E-01 | 4.50000 | .39577E+01 | .72907E-01 | 4.50000 | .31570E+00 |
| 273 | 3.50000 | .50000 | 5.50000 | .37260E+01 | .65599E-01 | 5.50000 | .37260E+01 | .65599E-01 | 5.50000 | .90894E-01 |
| 274 | 3.50000 | 1.50000 | 3.50000 | .39796E+01 | .34821E+00 | 3.50000 | .39796E+01 | .34821E+00 | 3.50000 | .81077E+00 |
| 275 | 3.50000 | 1.50000 | 4.50000 | .36435E+01 | .25547E+00 | 4.50000 | .36435E+01 | .25547E+00 | 4.50000 | .37571E+00 |
| 276 | 3.50000 | 1.50000 | 5.50000 | .34547E+01 | .18992E+00 | 5.50000 | .34547E+01 | .18992E+00 | 5.50000 | .10375E+00 |
| 277 | 3.50000 | 2.50000 | 3.50000 | .35164E+01 | .99304E-01 | 3.50000 | .35164E+01 | .99304E-01 | 3.50000 | .88727E+00 |
| 278 | 3.50000 | 2.50000 | 4.50000 | .32929E+01 | .65507E-01 | 4.50000 | .32929E+01 | .65507E-01 | 4.50000 | .44475E+00 |
| 279 | 3.50000 | 2.50000 | 5.50000 | .31673E+01 | .11934E-01 | 5.50000 | .31673E+01 | .11934E-01 | 5.50000 | .13488E+00 |
| 280 | 3.50000 | 3.50000 | 3.50000 | .33529E+01 | .25521E-02 | 3.50000 | .33529E+01 | .25521E-02 | 3.50000 | .94252E+00 |

FIPM3D FLOW UNDER DAM SUPPORTED ON TWO MEDIA FOUNDATION
 LOAD CASE 1

| ELEMENT | COORDINATES | | | VFLOCITIES | | |
|---------|-------------|---------|---------|------------|-------------|--------------|
| | X | Y | Z | X | Y | Z |
| 281 | 3.50000 | 3.50000 | 4.50000 | .31704E+01 | -.38697E-01 | -.4A354F+00 |
| 282 | 3.50000 | 3.50000 | 5.50000 | .30635E+01 | -.56406E-01 | -.14833E+00 |
| 283 | 3.50000 | 4.50000 | 3.50000 | .32940E+01 | -.88650E-02 | -.98080F+00 |
| 284 | 3.50000 | 4.50000 | 4.50000 | .31262E+01 | -.23902E-01 | -.50155F+00 |
| 285 | 3.50000 | 4.50000 | 5.50000 | .30267E+01 | -.20021E-01 | -.15415E+00 |
| 286 | 4.50000 | .50000 | 4.50000 | .35539E+01 | -.69299E-01 | -.57607F+00 |
| 287 | 4.50000 | .50000 | 5.50000 | .34311E+01 | -.68195E-01 | -.1A502F+00 |
| 288 | 4.50000 | 1.50000 | 4.50000 | .33000E+01 | -.17046E+00 | -.5A529F+00 |
| 289 | 4.50000 | 1.50000 | 5.50000 | .31995E+01 | -.17912E+00 | -.183335F+00 |
| 290 | 4.50000 | 2.50000 | 4.50000 | .29780E+01 | -.20012E+00 | -.59594F+00 |
| 291 | 4.50000 | 2.50000 | 5.50000 | .28995E+01 | -.20659E+00 | -.18783E+00 |
| 292 | 4.50000 | 3.50000 | 4.50000 | .27390E+01 | -.15356E+00 | -.60405F+00 |
| 293 | 4.50000 | 3.50000 | 5.50000 | .26826E+01 | -.15859E+00 | -.19122F+00 |
| 294 | 4.50000 | 4.50000 | 4.50000 | .26356E+01 | -.56584E-01 | -.60980F+00 |
| 295 | 4.50000 | 4.50000 | 5.50000 | .258A2E+01 | -.58970E-01 | -.19288F+00 |
| 296 | 5.50000 | .50000 | 5.50000 | .33036E+01 | -.27148E+00 | -.24318F+00 |
| 297 | 5.50000 | 1.50000 | 5.50000 | .28599E+01 | -.65212E+00 | -.27652E+00 |
| 298 | 5.50000 | 2.50000 | 5.50000 | .23808E+01 | -.51178E+00 | -.24130F+00 |
| 299 | 5.50000 | 3.50000 | 5.50000 | .21309E+01 | -.32014E+00 | -.23142E+00 |
| 300 | 5.50000 | 4.50000 | 5.50000 | .20127E+01 | -.11002E+00 | -.22658F+00 |

FI PM3D FLOW UNDER DAM SUPPORTED ON TWO MEDIA FOUNDATION
 LOAD CASE 1

| NODE | RESIDUAL |
|------|------------|
| 1 | 0. |
| 2 | 0. |
| 3 | 0. |
| 4 | 0. |
| 5 | 0. |
| 6 | 0. |
| 7 | 0. |
| 8 | 0. |
| 9 | 0. |
| 10 | 0. |
| 11 | 0. |
| 12 | 0. |
| 13 | 0. |
| 14 | 0. |
| 15 | 0. |
| 16 | 0. |
| 17 | 0. |
| 18 | 0. |
| 19 | 0. |
| 20 | 0. |
| 21 | 0. |
| 22 | 0. |
| 23 | 0. |
| 24 | 0. |
| 25 | 0. |
| 26 | 0. |
| 27 | 0. |
| 28 | 0. |
| 29 | 0. |
| 30 | 0. |
| 31 | 0. |
| 32 | 0. |
| 33 | 0. |
| 34 | 0. |
| 35 | 0. |
| 36 | 0. |
| 37 | 0. |
| 38 | 0. |
| 39 | 0. |
| 40 | 0. |
| 41 | 0. |
| 42 | 0. |
| 43 | .11369E-12 |
| 44 | .85265E-12 |
| 45 | .78167E-12 |
| 46 | .12232E-11 |
| 47 | .10090E-11 |
| 48 | .11084E-11 |
| 49 | 0. |
| 50 | .17337E-11 |

FI PM3D FLOW UNDER DAM SUPPORTED ON TWO MEDIA FOUNDATION
 LOAD CASE 1

| NODE | RESIDUAL |
|------|-------------|
| 51 | .13927E-11 |
| 52 | .11937E-11 |
| 53 | .85265E-12 |
| 54 | .13074E-11 |
| 55 | 0. |
| 56 | .28848E-11 |
| 57 | .31974E-11 |
| 58 | .19327E-11 |
| 59 | .16769E-11 |
| 60 | .11546E-11 |
| 61 | 0. |
| 62 | .18900E-11 |
| 63 | .27569E-11 |
| 64 | .23448E-11 |
| 65 | .26006E-11 |
| 66 | .13252E-11 |
| 67 | 0. |
| 68 | .23377E-11 |
| 69 | .29061E-11 |
| 70 | .22098E-11 |
| 71 | .37659E-11 |
| 72 | .13287E-11 |
| 73 | 0. |
| 74 | .33751E-11 |
| 75 | .30198E-11 |
| 76 | .31051E-11 |
| 77 | .36309E-11 |
| 78 | .13571E-11 |
| 79 | 0. |
| 80 | .22808E-11 |
| 81 | .57554E-12 |
| 82 | .11866E-11 |
| 83 | .94502E-12 |
| 84 | .66791E-12 |
| 85 | 0. |
| 86 | .14239E-11 |
| 87 | .10687E-10 |
| 88 | .94786E-11 |
| 89 | .99192E-11 |
| 90 | .37517E-11 |
| 91 | 0. |
| 92 | .23022E-11 |
| 93 | -.27853E-11 |
| 94 | -.51159E-12 |
| 95 | 0. |
| 96 | -.11369E-11 |
| 97 | 0. |
| 98 | -.11987E-10 |
| 99 | -.10616E-10 |
| 100 | -.18062E-10 |

FIPM3D FLOW UNDER DAM SUPPORTED ON TWO MEDIA FOUNDATION
 LOAD CASE 1

| NODE | RESIDUAL |
|------|-------------|
| 1-1 | -.15135E-10 |
| 1-2 | -.75744E-11 |
| 1-3 | 0. |
| 1-4 | .15490E-11 |
| 1-5 | .92371E-13 |
| 1-6 | .84555E-12 |
| 1-7 | .58265E-12 |
| 1-8 | .99476E-13 |
| 1-9 | 0. |
| 1-10 | .25722E-11 |
| 1-11 | -.42633E-13 |
| 1-12 | -.17621E-11 |
| 1-13 | -.92371E-12 |
| 1-14 | -.14566E-12 |
| 1-15 | 0. |
| 1-16 | .22169E-11 |
| 1-17 | -.97344E-12 |
| 1-18 | -.13145E-11 |
| 1-19 | -.67512E-12 |
| 1-20 | -.43343E-12 |
| 1-21 | 0. |
| 1-22 | .12861E-11 |
| 1-23 | -.49738E-13 |
| 1-24 | -.33396E-12 |
| 1-25 | -.29132E-12 |
| 1-26 | -.32685E-12 |
| 1-27 | 0. |
| 1-28 | .78160E-13 |
| 1-29 | -.48317E-12 |
| 1-30 | -.13145E-11 |
| 1-31 | -.10871E-11 |
| 1-32 | -.54712E-12 |
| 1-33 | .55707E-11 |
| 1-34 | .17394E-10 |
| 1-35 | .10942E-10 |
| 1-36 | .56133E-11 |
| 1-37 | .51159E-11 |
| 1-38 | .37659E-11 |
| 1-39 | .39222E-11 |
| 1-40 | .27285E-11 |
| 1-41 | -.11653E-11 |
| 1-42 | -.15916E-11 |
| 1-43 | .21032E-11 |
| 1-44 | .93792E-12 |
| 1-45 | .18190E-11 |
| 1-46 | -.32685E-11 |
| 1-47 | -.12534E-10 |
| 1-48 | -.28422E-11 |
| 1-49 | -.39790E-11 |
| 1-50 | -.19043E-11 |

FI PM3D FLOW UNDER DAM SUPPORTED ON TWO MEDIA FOUNDATION
 LOAD CASE 1

| NODE | RESIDUAL |
|------|-------------|
| 151 | -.87255E-11 |
| 152 | -.14637E-10 |
| 153 | -.13372E-10 |
| 154 | -.11092E-10 |
| 155 | -.13188E-10 |
| 156 | -.84412E-11 |
| 157 | -.43343E-12 |
| 158 | .14921E-12 |
| 159 | -.13323E-11 |
| 160 | -.50093E-12 |
| 161 | -.11973E-11 |
| 162 | -.24869E-13 |
| 163 | -.14211E-13 |
| 164 | .51159E-12 |
| 165 | -.86686E-12 |
| 166 | -.75318E-12 |
| 167 | -.19895E-11 |
| 168 | -.11369E-12 |
| 169 | -.11369E-12 |
| 170 | -.59686E-12 |
| 171 | -.83844E-12 |
| 172 | -.17764E-11 |
| 173 | -.49738E-12 |
| 174 | -.16165E-12 |
| 175 | -.42633E-12 |
| 176 | .99476E-13 |
| 177 | -.65370E-12 |
| 178 | -.83844E-12 |
| 179 | -.13642E-11 |
| 180 | -.32685E-12 |
| 181 | .21743E-11 |
| 182 | .34106E-11 |
| 183 | .39719E-11 |
| 184 | .24727E-11 |
| 185 | .42490E-11 |
| 186 | .30695E-11 |
| 187 | -.39790E-12 |
| 188 | -.88107E-12 |
| 189 | -.68212E-12 |
| 190 | -.31264E-12 |
| 191 | -.88107E-12 |
| 192 | -.45475E-12 |
| 193 | -.34106E-12 |
| 194 | -.42633E-12 |
| 195 | -.13927E-11 |
| 196 | .48317E-12 |
| 197 | -.44906E-11 |
| 198 | -.16200E-11 |
| 199 | -.19327E-11 |
| 200 | .18758E-11 |

FI PM3D FLOW UNDER DAM SUPPORTED ON TWO MEDIA FOUNDATION
 LOAD CASE 1

| NODE | RESIDUAL |
|------|-------------|
| 201 | .13358E-11 |
| 202 | -.17053E-12 |
| 203 | -.63665E-11 |
| 204 | -.32827E-11 |
| 205 | -.62741E-11 |
| 206 | -.14268E-10 |
| 207 | -.12555E-10 |
| 208 | -.12790E-10 |
| 209 | -.12875E-10 |
| 210 | -.50377E-11 |
| 211 | -.54001E-12 |
| 212 | -.12186E-11 |
| 213 | -.52580E-12 |
| 214 | -.17337E-11 |
| 215 | -.11653E-11 |
| 216 | .23093E-13 |
| 217 | -.99476E-13 |
| 218 | -.10161E-11 |
| 219 | -.10374E-11 |
| 220 | -.11795E-11 |
| 221 | -.10800E-11 |
| 222 | -.72120E-12 |
| 223 | -.39790E-12 |
| 224 | -.11653E-11 |
| 225 | -.84199E-12 |
| 226 | -.11759E-11 |
| 227 | -.11475E-11 |
| 228 | -.25224E-12 |
| 229 | .43343E-12 |
| 230 | .34319E-11 |
| 231 | .10161E-11 |
| 232 | .11795E-11 |
| 233 | .54712E-12 |
| 234 | .11440E-11 |
| 235 | -.25580E-12 |
| 236 | -.14211E-11 |
| 237 | -.68212E-12 |
| 238 | -.31264E-12 |
| 239 | .34106E-12 |
| 240 | -.36948E-12 |
| 241 | -.39790E-12 |
| 242 | -.14779E-11 |
| 243 | -.30980E-11 |
| 244 | -.19611E-11 |
| 245 | -.35243E-11 |
| 246 | -.88107E-12 |
| 247 | -.19895E-12 |
| 248 | -.31264E-12 |
| 249 | -.13642E-11 |
| 250 | -.21885E-11 |

FI PM3D FLOW UNDER DAM SUPPORTED ON TWO MEDIA FOUNDATION
LOAD CASE 1

| NODE | RESIDUAL |
|------|-------------|
| 251 | -.29843E-12 |
| 252 | -.71054E-12 |
| 253 | -.85265E-13 |
| 254 | -.49170E-11 |
| 255 | -.27285E-11 |
| 256 | -.34390E-11 |
| 257 | -.19327E-11 |
| 258 | -.19327E-11 |
| 259 | -.34888E-11 |
| 260 | -.10374E-10 |
| 261 | -.11489E-10 |
| 262 | -.73115E-11 |
| 263 | -.11219E-10 |
| 264 | -.39293E-11 |
| 265 | -.78160E-13 |
| 266 | -.56133E-12 |
| 267 | -.49738E-13 |
| 268 | -.67751E-12 |
| 269 | -.57979E-12 |
| 270 | -.67235E-12 |
| 271 | -.22737E-12 |
| 272 | -.57554E-12 |
| 273 | -.68567E-12 |
| 274 | -.48672E-12 |
| 275 | -.65015E-12 |
| 276 | -.85265E-13 |
| 277 | -.19185E-12 |
| 278 | -.36238E-12 |
| 279 | -.24158E-12 |
| 280 | -.18048E-11 |
| 281 | -.54001E-12 |
| 282 | -.42633E-13 |
| 283 | -.62528E-12 |
| 284 | -.11653E-11 |
| 285 | -.17337E-11 |
| 286 | -.20179E-11 |
| 287 | -.85265E-12 |
| 288 | -.19895E-12 |
| 289 | -.28422E-13 |
| 290 | -.15064E-11 |
| 291 | -.40643E-11 |
| 292 | -.30127E-11 |
| 293 | -.25437E-11 |
| 294 | -.61107E-12 |
| 295 | -.56843E-12 |
| 296 | -.14211E-11 |
| 297 | -.23306E-11 |
| 298 | -.73896E-12 |
| 299 | -.23022E-11 |
| 300 | -.12790E-11 |

FIPM3D FLOW UNDER DAM SUPPORTED ON TWO MEDIA FOUNDATION
 LOAD CASE 1

| NODE | RESIDUAL |
|------|-------------|
| 301 | -.85265E-12 |
| 302 | .11084E-11 |
| 303 | -.25011E-11 |
| 304 | -.44622E-11 |
| 305 | -.48033E-11 |
| 306 | -.11084E-11 |
| 307 | .62528E-12 |
| 308 | -.68212E-12 |
| 309 | -.25580E-12 |
| 310 | -.21885E-11 |
| 311 | -.47748E-11 |
| 312 | -.34106E-12 |
| 313 | -.27711E-11 |
| 314 | -.55280E-11 |
| 315 | -.74891E-11 |
| 316 | -.70557E-11 |
| 317 | -.10974E-10 |
| 318 | -.40679E-11 |
| 319 | -.15277E-12 |
| 320 | -.20250E-12 |
| 321 | -.41922E-12 |
| 322 | -.65015E-12 |
| 323 | -.47251E-12 |
| 324 | -.11369E-12 |
| 325 | -.60396E-12 |
| 326 | -.15774E-11 |
| 327 | -.16271E-11 |
| 328 | -.22098E-11 |
| 329 | -.13927E-11 |
| 330 | -.10090E-11 |
| 331 | 0. |
| 332 | -.17053E-11 |
| 333 | -.14779E-11 |
| 334 | -.20179E-11 |
| 335 | -.68212E-12 |
| 336 | -.72475E-12 |
| 337 | 0. |
| 338 | -.12790E-11 |
| 339 | -.25295E-11 |
| 340 | -.24158E-12 |
| 341 | -.21316E-11 |
| 342 | -.46896E-12 |
| 343 | 0. |
| 344 | -.15916E-11 |
| 345 | -.11653E-11 |
| 346 | -.26432E-11 |
| 347 | -.15632E-12 |
| 348 | -.24301E-11 |
| 349 | 0. |
| 350 | -.45475E-12 |

FI-PM3D FLOW UNDER DAM SUPPORTED ON TWO MEDIA FOUNDATION
 LOAD CASE 1

| NODE | RESIDUAL |
|------|------------|
| 351 | .12221E-11 |
| 352 | .16200E-11 |
| 353 | .38796E-11 |
| 354 | .20179E-11 |
| 355 | 0. |
| 356 | .24727E-11 |
| 357 | .23874E-11 |
| 358 | .24727E-11 |
| 359 | .35385E-11 |
| 360 | .16200E-11 |
| 361 | 0. |
| 362 | .76739E-12 |
| 363 | .79581E-12 |
| 364 | .11937E-11 |
| 365 | .54001E-12 |
| 366 | .10090E-11 |
| 367 | 0. |
| 368 | .47073E-13 |
| 369 | .15765E-11 |
| 370 | .27178E-11 |
| 371 | .11133E-11 |
| 372 | .15157E-11 |
| 373 | 0. |
| 374 | .39791E-12 |
| 375 | .14211E-12 |
| 376 | .95213E-12 |
| 377 | .15632E-11 |
| 378 | .85265E-12 |
| 379 | 0. |
| 380 | .88107E-12 |
| 381 | .21743E-11 |
| 382 | .85265E-12 |
| 383 | .38867E-11 |
| 384 | .20179E-11 |
| 385 | 0. |
| 386 | .34106E-12 |
| 387 | .17053E-12 |
| 388 | .24158E-12 |
| 389 | .93792E-12 |
| 390 | .65370E-12 |
| 391 | 0. |
| 392 | .28422E-12 |
| 393 | .76739E-12 |
| 394 | .24158E-12 |
| 395 | .14566E-11 |
| 396 | .42633E-13 |
| 397 | 0. |
| 398 | .54001E-12 |
| 399 | .17053E-12 |
| 400 | 0. |

FIPM3D FLOW UNDER DAM SUPPORTED ON TWO MEDIA FOUNDATION
 LOAD CASE 1

| NODE | RESIDUAL |
|------|-------------|
| 41 | .27001E-12 |
| 42 | -.10090E-11 |
| 43 | 0. |
| 44 | .22737E-12 |
| 45 | -.11369E-12 |
| 46 | -.28422E-12 |
| 47 | -.54001E-12 |
| 48 | .36948E-12 |
| 49 | 0. |
| 410 | .17053E-12 |
| 411 | -.34106E-12 |
| 412 | .61107E-12 |
| 413 | .48317E-12 |
| 414 | .28422E-13 |
| 415 | 0. |
| 416 | 0. |
| 417 | 0. |
| 418 | 0. |
| 419 | 0. |
| 420 | 0. |
| 421 | 0. |
| 422 | 0. |
| 423 | 0. |
| 424 | 0. |
| 425 | 0. |
| 426 | 0. |
| 427 | 0. |
| 428 | 0. |
| 429 | 0. |
| 430 | 0. |
| 431 | 0. |
| 432 | 0. |
| 433 | 0. |
| 434 | 0. |
| 435 | 0. |
| 436 | 0. |
| 437 | 0. |
| 438 | 0. |
| 439 | 0. |
| 440 | 0. |
| 441 | 0. |
| 442 | 0. |
| 443 | 0. |
| 444 | 0. |
| 445 | 0. |
| 446 | 0. |
| 447 | 0. |
| 448 | 0. |
| 449 | 0. |
| 450 | 0. |

FI PM3D FLOW UNDER DAM SUPPORTED ON TWO MEDIA FOUNDATION
LOAD CASE 1

| NODE | RESIDUAL |
|------|----------|
| 451 | 0. |
| 452 | 0. |
| 453 | 0. |
| 454 | 0. |
| 455 | 0. |
| 456 | 0. |

FI PM3D FLOW UNDER DAM SUPPORTED ON TWO MEDIA FOUNDATION

TIME LOG

| | | | | | |
|---------------------|---|--------|------------------|---|----------|
| TIME IN FPIN | = | 1.768 | TIME PER NODE | = | .388E-02 |
| TIME IN FPEL | = | 4.400 | TIME PER ELEMENT | = | .147E-01 |
| TIME IN FPST | = | 14.810 | TIME PER NODE | = | .325E-01 |
| TIME IN GAUSS | = | 15.968 | TIME PER NODE | = | .350E-01 |
| TIME IN FPRE | = | 6.426 | TIME PER NODE | = | .141E-01 |
| TOTAL TIME = 43.372 | | | | | |

| | | |
|-------------------------------|-------|--------|
| NUMBER OF EQUATIONS | | 456 |
| HALF BAND WIDTH | | 56 |
| NUMBER OF EQUATIONS PER BLOCK | | 39 |
| NUMBER OF BLOCKS | | 12 |
| EQUATION SOLVER | | GAUSS2 |
| LENGTH OF BLANK COMMON (MTOT) | | 5000 |

APPENDIX D

LISTING FOR COMPUTER PROGRAM FLPM3D

```

PROGRAM FPM3D
C
C DIRECT SOLUTION OF THREE DIMENSIONAL FLOW OF INCOMPRESSIBLE FLUID
C IN ORTHOTROPICALLY PERMEABLE POROUS MEDIA USING 8 POINT F.O.E.
C
1 (INPUT,OUTPUT,TAPES=INPUT,TAPE6=OUTPUT,
2 TAPE1,TAPE2,TAPE3,TAPE7,TAPE8,TAPE9)
C
COMMON / GENCON /
1 HED(13),WORD(2),NUMEL,NUMNP,NUMMAT,ISTOP,MAXBAN,NSTRES,NPT
2,LNSTOR,NUMJC,NST
COMMON / GAUSEQ /
1 NJ,MM,LL,NR,NC,NSET,NRNC
2,NTAPE2,NTAPE3,NTAPE4,NTAPE5,NTAPE6
COMMON / BUFFER /
1 LNREC,LNBUFF,NTAPE1,BUFF(2640)
COMMON A(12000)
C
C ASSIGN LENGTH OF BLANK COMMON - MTOT
C ASSIGN LENGTH OF ONE RECORD ON INTERNAL BUFFER - LNREC
C ASSIGN NUMBER OF RECORDS ON INTERNAL BUFFER - LNREC
C ASSIGN LENGTH OF ELEMENT STORAGE BLOCKS - LNSTOR
C ASSIGN TEMPORARY STORAGE UNITS - NTAPE1,NTAPE2,NTAPE3
C NTAPE4,NTAPE5
NTAPE1=1
NTAPE2=2
NTAPE3=3
NTAPE4=7
NTAPE5=8
NTAPE6=9
MTOT=12000
LNREC=132
LNSTOR=99
NUMREC=20

```

1 FPM
2 FPM
3 FPM
4 FPM
5 FPM
6 FPM
7 FPM
8 FPM
9 FPM
10 FPM
11 FPM
12 FPM
13 FPM
14 FPM
15 FPM
16 FPM
17 FPM
18 FPM
19 FPM
20 FPM
21 FPM
22 FPM
23 FPM
24 FPM
25 FPM
26 FPM
27 FPM
28 FPM
29 FPM
30 FPM
31 FPM
32 FPM
33 FPM
34 FPM
35 FPM

LNBUFF=NUMREC*LNREC
CALL FPCALL (A,MTOT)
STOP
END

FPM 36
FPM 37
FPM 38
FPM 39


```

NNPL=NNPL+NPLO(L)
30 CONTINUE
C
C DIMENSION BLANK COMMON
C
M1=1
M2=M1+LL*NG
M3=M2+NUMNP
M4=M3+NUMNP
M5=M4+NUMNP
M6=M5+NUMNP
M7=M6+NUMNP
M8=M7+6*NUMDC
M9=M8+4*NUMPC
M10=M9+4*NNEL
M11=M10+LNSIOR*NSIOR1
M12=M11+LNSIOR*NSIOR2
M13=M12+LNSIOR*NSIOR3
IF ( M13 .LE. MTOT ) GO TO 50
WRITE (6,4001) MTOT,M13
GO TO 10
50 CONTINUE
C
C INPUT ALL DATA EXCEPT ELEMENT IDENTIFICATION
C
CALL FPIN
1 (A(M1),A(M2),A(M3),A(M4),A(M5),A(M6),A(M7),A(M8),A(M9)
2,NG,NUMPC,NNEL,NUMDC)
IF ( ISTOP .EQ. 1 ) GO TO 10
CALL OPTIME(SEC(2))
C
C INPUT ELEMENT IDENTIFICATION
C
CALL FPEL
1 (A(M1),A(M2),A(M3),A(M4),A(M5),A(M6),A(M7),A(M8),A(M9),A(M10)

```

```

CALL 71
CALL 72
CALL 73
CALL 74
CALL 75
CALL 76
CALL 77
CALL 78
CALL 79
CALL 80
CALL 81
CALL 82
CALL 83
CALL 84
CALL 85
CALL 86
CALL 87
CALL 88
CALL 89
CALL 90
CALL 91
CALL 92
CALL 93
CALL 94
CALL 95
CALL 96
CALL 97
CALL 98
CALL 99
CALL 100
CALL 101
CALL 102
CALL 103
CALL 104
CALL 105

```

```

2  ,A(M11),A(M12),NQ,NUMPC,MNEL,NUMDC)
  IF ( ISIOP .EQ. 1 ) GO TO 10
  CALL CPTIME(SEC(3))

C
C   DETERMINE OPTIMAL NUMBER OF EQUATIONS IN ONE SET AND CHOOSE
C   CORRESPONDING EQUATION SOLVER
C
  IC=MM+LL
  NCJ=NC+1
  MRRES=LL*NQ
  MAVC=MTOT-MRES
  NR2=MAVC/NCJ
  NR=NR2/2
  IF ( NR2 .GE. NQ ) NR=NQ
  IF ( NR .LT. MM ) GO TO 60
  ITYPE=1
  GO TO 70
60  ITYPE=2
  70  NSET=(NQ-1)/NR+1
      IF ( NR .GE. 2 ) GO TO 90
      WRITE (6,3003) NQ,MM,NR,NSET,ITYPE,MTOT
      WRITE (6,4002) MM
      GO TO 10
90  CONTINUE
  NRNC=NR*NC
  IF ( NQ .LE. NRNC ) GO TO 100
  WRITE (6,4003) NQ,NRNC
  GO TO 10
100 CONTINUE
  N1=MRRES+1
  N2=N1+NRNC
  N3=N2+NRNC
  IF ( ( ITYPE .EQ. 1 ) .AND. ( NR .EQ. NQ ) ) N3=N2
  N4=N3+NR
  IF ( N4 .LE. MTOT ) GO TO 110
  CALL 106
  CALL 107
  CALL 108
  CALL 109
  CALL 110
  CALL 111
  CALL 112
  CALL 113
  CALL 114
  CALL 115
  CALL 116
  CALL 117
  CALL 118
  CALL 119
  CALL 120
  CALL 121
  CALL 122
  CALL 123
  CALL 124
  CALL 125
  CALL 126
  CALL 127
  CALL 128
  CALL 129
  CALL 130
  CALL 131
  CALL 132
  CALL 133
  CALL 134
  CALL 135
  CALL 136
  CALL 137
  CALL 138
  CALL 139
  CALL 140

```



```

WRITE (6,4001) MTOT,N4
GO TO 10
110 CONTINUE
L1=1
L2=L1+MRES
L3=L2+NQ
L4=L3+NUMNP*NSTRES
L5=L4+3*NUMNP*NSTRES
IF ( L5 .LE. MTOT ) GO TO 115
WRITE (6,4004) L5
GO TO 10
115 CONTINUE
C
C RE-DIMENSION BLANK COMMON
C FORM DISPLACEMENT EQUATIONS OF EQUILIBRIUM BY DIRECT STIFFNESS
C
C REWIND NTAPE2
CALL FPST
1 (A(M1),A(M2),NQ,NR,NC)
CALL CPTIME(SEC(4))
C
C RE-DIMENSION BLANK COMMON
C SOLVE EQUATIONS
IF ( ITYPE .EQ. 1 ) CALL GAUSS1
1 (A(N1),A(N2),A(N3),NR,NC,NQ,MM,LL,NTAPE2,NTAPE3)
C
IF ( ITYPE .EQ. 2 ) CALL GAUSS2
1 (A(N1),A(N2),A(N3),NR,NC,NQ,MM,LL,NTAPE2,NTAPE3,NTAPE4,NTAPE5)
CALL CPTIME(SEC(5))
C
C RE-DIMENSION
C ASSIGN NATURAL COORDINATES OF VELOCITY POINTS
C EXTRACT FLOW VELOCITIES FROM PRESSURE FIELD

```

```

CALL 141
CALL 142
CALL 143
CALL 144
CALL 145
CALL 146
CALL 147
CALL 148
CALL 149
CALL 150
CALL 151
CALL 152
CALL 153
CALL 154
CALL 155
CALL 156
CALL 157
CALL 158
CALL 159
CALL 160
CALL 161
CALL 162
CALL 163
CALL 164
CALL 165
CALL 166
CALL 167
CALL 168
CALL 169
CALL 170
CALL 171
CALL 172
CALL 173
CALL 174
CALL 175

```

```

PPT(1)=0.0
SPT(1)=0.0
TPT(1)=0.0
DO 120 I=2,9
PPT(I)=1.0
SPT(I)=1.0
TPT(I)=1.0
120 CONTINUE
DO 130 I=1,4
J=2*I
PPT(I+5)=1.0
SPT(I+3)=1.0
TPT(J)=1.0
130 CONTINUE
CALL FPRE
1 (A(L1),A(L2),A(L3),A(L4),NUMNP)
CALL CPTIME(SEC(6))
PRINT TIME LOG
DO 140 I=1,5
J=6-I
140 TIME(J)=SEC(J+1)-SEC(J)
DO 150 I=1,5
150 TIME(I+5)=TIME(I)/NUMNP
TIME(7)=TIME(2)/NUMEL
TIME(11)=TIME(1)+TIME(2)+TIME(3)+TIME(4)+TIME(5)
WRITE (6,3000) HEU
WRITE (6,3001) (TIME(I),TIME(I+5),I=1,5),TIME(11)
WRITE (6,3003) NO,MM,NR,NSET,ITYPE,MTOT
C
C
C GO TO NEXT PROBLEM
C
C

```

```

CALL 176
CALL 177
CALL 178
CALL 179
CALL 180
CALL 181
CALL 182
CALL 183
CALL 184
CALL 185
CALL 186
CALL 187
CALL 188
CALL 189
CALL 190
CALL 191
CALL 192
CALL 193
CALL 194
CALL 195
CALL 196
CALL 197
CALL 198
CALL 199
CALL 200
CALL 201
CALL 202
CALL 203
CALL 204
CALL 205
CALL 206
CALL 207
CALL 208
CALL 209
CALL 210

```

CALL 211
 CALL 212
 CALL 213
 CALL 214
 CALL 215
 CALL 216
 CALL 217
 CALL 218
 CALL 219
 CALL 220
 CALL 221
 CALL 222
 CALL 223
 CALL 224
 CALL 225
 CALL 226
 CALL 227
 CALL 228
 CALL 229
 CALL 230
 CALL 231
 CALL 232
 CALL 233
 CALL 234
 CALL 235
 CALL 236
 CALL 237
 CALL 238
 CALL 239
 CALL 240
 CALL 241
 CALL 242
 CALL 243
 CALL 244
 CALL 245

GO TO 10
 C
 1000 FORMAT(13A6)
 1001 FORMAT(9I5)
 1002 FORMAT(2I5)
 1003 FORMAT(4F10.0)
 2001 FORMAT(/
 1/10X,46H NUMBER OF NODAL POINTSI5
 2/10X,46H NUMBER OF ELEMENTSI5
 3/10X,46H NUMBER OF MATERIALSI5
 4/10X,46H NUMBER OF SURFACE FLOW TYPESI5
 5/10X,46H NUMBER OF SETS OF DIRECTION RATIOSI5
 6/10X,46H NUMBER OF LOADING CASESI5
 7/10X,46H ELEMENT VELOCITY OPTIONI5
 8/10X,46H LIMIT ON ALLOWABLE HALF BAND WIDTHI5
 9/10X,46H NUMBER OF ELEMENT STORAGE BLOCKSI5
 1/10X,46H CONSTANT ACCELERATION IN X DIRECTIONF12.5
 2/10X,46H CONSTANT ACCELERATION IN Y DIRECTIONF12.5
 3/10X,46H CONSTANT ACCELERATION IN Z DIRECTIONF12.5
 4/10X,46H ACCELERATION DUE TO GRAVITYF12.5
 5/10X,46H UNIT WEIGHT OF FLUIDF12.5)
 2002 FORMAT(//
 1/10X,46H LOAD CASEI5
 2/10X,46H NUMBER OF NODES WITH PRESCRIBED FLOWI5
 3/10X,46H NUMBER OF ELEMENT FACES WITH
 4/10X,46H PRESCRIBED SURFACE FLOWSI5)
 3000 FORMAT(1H1,10X,13A6)
 3001 FORMAT(/20X,9H TIME LOG /
 1/10X,16H TIME IN FPIN =,F9.3,10X,19H TIME PER NODE =,E10.3
 2/10X,16H TIME IN FPEL =,F9.3,10X,19H TIME PER ELEMENT =,E10.3
 3/10X,16H TIME IN FPST =,F9.3,10X,19H TIME PER NODE =,E10.3
 4/10X,16H TIME IN GAUSS =,F9.3,10X,19H TIME PER NODE =,E10.3
 5/10X,16H TIME IN FPRE =,F9.3,10X,19H TIME PER NODE =,E10.3
 6//10X,13H TOTAL TIME =,F9.3)
 3003 FORMAT(//

```

1/10X,46H NUMBER OF EQUATIONS .....I6          CALL 246
2/10X,46H HALF BAND WIDTH .....I6              CALL 247
3/10X,46H NUMBER OF EQUATIONS PER BLOCK .....I6  CALL 248
4/10X,46H NUMBER OF BLOCKS .....I6             CALL 249
5/10X,51H EQUATION SOLVER .....I6             CALL 250
6/10X,46H LENGTH OF BLANK COMMON (MTUT) .....GAUSS,I6) CALL 251
4000 FORMAT(20H0 CONTROL CARD ERROR )          CALL 252
4001 FORMAT(36H DIMENSIONED LENGTH OF BLANK COMMON=I6// CALL 253
      1 34H REQUESTED LENGTH OF BLANK COMMON=I6//  CALL 254
      2 36H EXECUTION TERMINATED                CALL 255
4002 1 15H AVAILABLE BANDWIDTH OF ,I5,I7H IS TOO LARGE FOR CALL 256
      1 15H AVAILABLE CORE)                     CALL 257
4003 1 15H/31H ALLOWABLE STORAGE CAPACITY EXCEEDED,/20HNUMBER OF EQUATIONS=, CALL 258
      1 15H/31H ALLOWABLE NUMBER OF EQUATIONS=,I5) CALL 259
4004 1/53H CONTAIN ONE LOAD VECTOR AFTER SOLUTION OF EQUATIONS TO CALL 260
      END                                       ) CALL 261

```



```

5 CONTINUE
  READ (5,1008) N,E(N,1),E(N,2),E(N,3)
  WRITE (6,2008) N,E(N,1),E(N,2),E(N,3)
10 CONTINUE
C
C
C
  READ AND PRINT REFERENCE SET OF DIRECTION COSINES
  IF ( NUMDC .EQ. 0 ) GO TO 30
  MPRINT=0
  WRITE (6,3000) HED
  WRITE (6,3001)
  DO 25 I=1,NUMDC
  MPRINT=MPRINT+1
  IF ( MPRINT .LE. 40 ) GO TO 15
  WRITE (6,3000) HED
  WRITE (6,3001)
  MPRINT=1
15 CONTINUE
  READ (5,1001) N,(DC(N,J),J=1,6)
  WRITE (6,2001) N,(DC(N,J),J=1,6)
  DJ=0.0
  DK=0.0
  DO 20 J=1,3
  K=J+3
  DJ=DJ+DC(N,J)*DC(N,J)
  DK=DK+DC(N,K)*DC(N,K)
20 CONTINUE
  DJ=SQRT(DJ)
  DK=SQRT(DK)
  DO 21 J=1,3
  K=J+3
  DY(N,J)=DC(N,J)/DJ
  DC(N,K)=DC(N,K)/DK
21 CONTINUE
25 CONTINUE

```

```

FPIN 36
FPIN 37
FPIN 38
FPIN 39
FPIN 40
FPIN 41
FPIN 42
FPIN 43
FPIN 44
FPIN 45
FPIN 46
FPIN 47
FPIN 48
FPIN 49
FPIN 50
FPIN 51
FPIN 52
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FPIN 56
FPIN 57
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FPIN 63
FPIN 64
FPIN 65
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FPIN 67
FPIN 68
FPIN 69
FPIN 70

```

```

30 CONTINUE
C
C READ AND PRINT NODAL POINT IDENTIFICATION
C
WRITE (6,3000) MED
WRITE (6,3003)
ICOUNT=0
40 READ (5,10J3) NL,INCL,KONE(NL),X(NL),Y(NL),Z(NL),BC(NL),IBCL
IF ( INCL .EQ. 0 ) INCL=1
ICOUNT=ICOUNT+1
IF ( ICOUNT .EQ. 1 ) GO TO 60
DEN=(NL=NF)/INCF
IF ( DEN .LE. 0.0 ) GO TO 60
DX=(X(NL)-X(NF))/DEN
DY=(Y(NL)-Y(NF))/DEN
DZ=(Z(NL)-Z(NF))/DEN
DP=(BC(NL)-BC(NF))/DEN
N=NF
50 N=N+INCF
IF ( N .EQ. NL ) GO TO 60
IF ( N .GT. NUMNP ) GO TO 70
M=N-INCF
X(N)=X(M)+DX
Y(N)=Y(M)+DY
Z(N)=Z(M)+DZ
KONE(N)=0
IF ( IBCF .NE. 0 ) KODE(N)=KODE(M)
BC(N)=0.0
IF ( IBCF .EQ. 1 ) BC(N)=BC(M)
IF ( IBCF .EQ. 2 ) BC(N)=BC(M)+DP
ICOUNT=ICOUNT+1
GO TO 50
60 NF=NL
INCF=INCL
I0CF=IBCL

```

FPIN 71
FPIN 72
FPIN 73
FPIN 74
FPIN 75
FPIN 76
FPIN 77
FPIN 78
FPIN 79
FPIN 80
FPIN 81
FPIN 82
FPIN 83
FPIN 84
FPIN 85
FPIN 86
FPIN 87
FPIN 88
FPIN 89
FPIN 90
FPIN 91
FPIN 92
FPIN 93
FPIN 94
FPIN 95
FPIN 96
FPIN 97
FPIN 98
FPIN 99
FPIN 100
FPIN 101
FPIN 102
FPIN 103
FPIN 104
FPIN 105

```

IF ( ICOUNT .LT. NUMNP ) GO TO 40
GO TO 80
70 WRITE (6,4001) N
   ISTOP=1
80 MPRINT=0
   DO 90 K=1,NUMNP
   MPRINT=MPRINT+1
   IF ( MPRINT .LE. 50 ) GO TO 85
   MPRINT=1
   WRITE (6,3000) HEU
   WRITE (6,3003)
85 CONTINUE
   IF ( KODE(K) .EQ. 0 ) WRITE (6,2003) K,X(K),Y(K),Z(K)
   IF ( KODE(K) .EQ. 1 ) WRITE (6,2003) K,X(K),Y(K),Z(K),BC(K)
90 CONTINUE
C
C
C
READ AND PRINT NON-ZERO NODAL POINT FLOWS FOR EACH LOAD CASE
UU 120 L=1,LL
DU 120 I=1,NG
120 BCF(I,L)=0.0
   IF ( NNPL .EQ. 0 ) GO TO 140
   WRITE (6,3000) HEU
   MPRINT=0
   DO 135 L=1,LL
   J=NPLD(L)
   IF ( J .EQ. 0 ) GO TO 135
   WRITE (6,3004) L
   DO 130 I=1,J
   READ (5,1004) N,BCF(N,L)
   MPRINT=MPRINT+1
   IF ( MPRINT .LE. 50 ) GO TO 125
   MPRINT=1
   WRITE (6,3000) HEU
   WRITE (6,3004) L

```

FFIN 106
 FFIN 107
 FFIN 108
 FFIN 109
 FFIN 110
 FFIN 111
 FFIN 112
 FFIN 113
 FFIN 114
 FFIN 115
 FFIN 116
 FFIN 117
 FFIN 118
 FFIN 119
 FFIN 120
 FFIN 121
 FFIN 122
 FFIN 123
 FFIN 124
 FFIN 125
 FFIN 126
 FFIN 127
 FFIN 128
 FFIN 129
 FFIN 130
 FFIN 131
 FFIN 132
 FFIN 133
 FFIN 134
 FFIN 135
 FFIN 136
 FFIN 137
 FFIN 138
 FFIN 139
 FFIN 140

FPIN 141
 FPIN 142
 FPIN 143
 FPIN 144
 FPIN 145
 FPIN 146
 FPIN 147
 FPIN 148
 FPIN 149
 FPIN 150
 FPIN 151
 FPIN 152
 FPIN 153
 FPIN 154
 FPIN 155
 FPIN 156
 FPIN 157
 FPIN 158
 FPIN 159
 FPIN 160
 FPIN 161
 FPIN 162
 FPIN 163
 FPIN 164
 FPIN 165
 FPIN 166
 FPIN 167
 FPIN 168
 FPIN 169
 FPIN 170
 FPIN 171
 FPIN 172
 FPIN 173
 FPIN 174
 FPIN 175

```

125 CONTINUE
130 WRITE (6,2004) N,BCF(N,L)
135 CONTINUE
140 CONTINUE
C
C READ AND PRINT SURFACE FLOW TYPES
C
IF ( NUMPC .EQ. 0 ) GO TO 160
PI=180.0/(4.0*ATAN(1.0))
WRITE (6,3000) HEU
WRITE (6,3005)
MPRINT=0
DO 150 N=1,NUMPC
HEAD (5,1005) N,(PBC(N,J),J=1,4)
MPRINT=MPRINT+1
IF ( MPRINT .LE. 50 ) GO TO 145
MPRINT=1
WRITE (6,3000) HEU
WRITE (6,3005)
145 CONTINUE
WRITE (6,2005) N,(PBC(N,J),J=1,4)
150 CONTINUE
160 CONTINUE
C
C READ AND PRINT SURFACE FLOW LOADING CASES
C
IF ( NNEL .EQ. 0 ) GO TO 170
WRITE (6,3000) HEU
WRITE (6,3006)
MPRINT=0
DO 165 I=1,NNEL
HEAD (5,1006) (IDL(I,J),J=1,4)
MPRINT=MPRINT+1
IF ( MPRINT .LE. 50 ) GO TO 164
MPRINT=1
  
```


FPIN 211

END

FPEL 36
 FPEL 37
 FPEL 38
 FPEL 39
 FPEL 40
 FPEL 41
 FPEL 42
 FPEL 43
 FPEL 44
 FPEL 45
 FPEL 46
 FPEL 47
 FPEL 48
 FPEL 49
 FPEL 50
 FPEL 51
 FPEL 52
 FPEL 53
 FPEL 54
 FPEL 55
 FPEL 56
 FPEL 57
 FPEL 58
 FPEL 59
 FPEL 60
 FPEL 61
 FPEL 62
 FPEL 63
 FPEL 64
 FPEL 65
 FPEL 66
 FPEL 67
 FPEL 68
 FPEL 69
 FPEL 70

```

MMS=0
1STOR=C
DO 10 I=1,3
DO 10 J=1,3
D(I,J)=0.0
TO CONTINUE

C READ ELEMENT IDENTIFICATION
C
C WRITE (6,3000) HFU
WRITE (6,3001)
100 READ (5,1000) MML,(NODL(Y),I=1,9),NDCL,GFTL,STORE
      ,INCL1,INCL2,INCL3,JUMPL2,JUMPL3
      IF ( INCL1 .EQ. 0 ) INCL1=1
      IF ( INCL2 .EQ. 0 ) INCL2=1
      IF ( INCL3 .EQ. 0 ) INCL3=1
      ICNT2=0
      ICNT3=0
      IF ( NODL(9) .EQ. 0 ) NODL(9)=1
      IF ( STORE .NE. 0 ) MMS=MML
110 MMF=MMF+1
      INCF=INCF1
      ICNT2=ICNT2+1
      ICNT3=ICNT3+1
      IF ( ICNT2 .NE. JUMPF2 ) GO TO 101
      ICNT2=0
      INCF=INCF2
121 CONTINUE
      IF ( ICNT3 .NE. JUMPF3 ) GO TO 102
      ICNT2=0
      ICNT3=0
      INCF=INCF3
122 CONTINUE
      IF (MML=MMF) GO,120,140
400 WRITE (6,4000) MML
  
```

```

120 ISTOP=1
    GETF=GETL
    NDCF=NDCL
    DO 130 I=1,9
130  NOUF(I)=NODL(I)
    GO TO 160
140  DO 150 I=1,8
150  NOUF(I)=NOUF(I)+INCF
160  CONTINUE
C
C
C      OBTAIN ELEMENT PERMEABILITY FROM PREVIOUS COMPUTATIONS
      IF ( (ISTOP.EQ.1).OR.(GETF.EQ.0).OR.(STORE.NE.0) ) GO TO 116
      IF ( GETF.NE.1 ) GO TO 112
      DO 111 I=1,LNSTOR
111  Q(I)=STORE1(I)
112  CONTINUE
      IF ( GETF.NE.2 ) GO TO 114
      DO 113 I=1,LNSTOR
113  Q(I)=STORE2(I)
114  CONTINUE
      IF ( GETF.NE.3 ) GO TO 116
      DO 115 I=1,LNSTOR
115  Q(I)=STORE3(I)
116  CONTINUE
      DO 170 I=1,8
          J=NOUF(I)
          XX(I)=X(J)
          YY(I)=Y(J)
          ZZ(I)=Z(J)
170
C
C      TRANSFORM MATERIAL PERMEABILITY FROM PRINCIPAL TO GLOBAL COORDS
      IF ( ( GETF.NE.0 ) .AND. ( STORE.EQ.0 ) ) GO TO 275
      HTYPE=NOUF(9)

```

```

71  FPPEL
72  FPPEL
73  FPPEL
74  FPPEL
75  FPPEL
76  FPPEL
77  FPPEL
78  FPPEL
79  FPPEL
80  FPPEL
81  FPPEL
82  FPPEL
83  FPPEL
84  FPPEL
85  FPPEL
86  FPPEL
87  FPPEL
88  FPPEL
89  FPPEL
90  FPPEL
91  FPPEL
92  FPPEL
93  FPPEL
94  FPPEL
95  FPPEL
96  FPPEL
97  FPPEL
98  FPPEL
99  FPPEL
100 FPPEL
101 FPPEL
102 FPPEL
103 FPPEL
104 FPPEL
105 FPPEL

```

```

RH0=UWT/ACCG
D(1,1)=E(MTYPE,1)
D(2,2)=E(MTYPE,2)
D(3,3)=E(MTYPE,3)
IF ( NDCF .EQ. 0 ) GO TO 255
Q1=DC(NDCF,1)
Q4=DC(NDCF,2)
Q7=UC(NDCF,3)
Q2=DC(NDCF,4)
Q5=DC(NDCF,5)
Q8=DC(NDCF,6)
Q3=Q4*Q8-Q5*Q7
Q6=Q2*Q7-Q1*Q8
Q9=Q1*Q5-Q2*Q4
QM=SQRT(Q3*Q3+Q6*Q6+Q9*Q9)
QJ=Q3/QM
QO=Q6/QM
QY=Q9/QM
D1=D(1,1)
D2=D(2,2)
D3=D(3,3)
P1=D1*Q1
P2=D2*Q2
P3=D3*Q3
P4=D1*Q4
P5=D2*Q5
P6=D3*Q6
P7=D1*Q7
P8=D2*Q8
P9=D3*Q9
U(1,1)=Q1*P1+Q2*P2+Q3*P3
U(2,1)=Q4*P1+Q5*P2+Q6*P3
U(3,1)=Q7*P1+Q8*P2+Q9*P3
U(2,2)=Q4*P4+Q5*P5+Q6*P6
U(3,2)=Q7*P4+Q8*P5+Q9*P6

```

```

FPFL 106
FPFL 107
FPFL 108
FPFL 109
FPFL 110
FPFL 111
FPFL 112
FPFL 113
FPFL 114
FPFL 115
FPFL 116
FPFL 117
FPFL 118
FPFL 119
FPFL 120
FPFL 121
FPFL 122
FPFL 123
FPFL 124
FPFL 125
FPFL 126
FPFL 127
FPFL 128
FPFL 129
FPFL 130
FPFL 131
FPFL 132
FPFL 133
FPFL 134
FPFL 135
FPFL 136
FPFL 137
FPFL 138
FPFL 139
FPFL 140

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FPFL 176
 FPFL 177
 FPFL 178
 FPFL 179
 FPFL 180
 FPFL 181
 FPFL 182
 FPFL 183
 FPFL 184
 FPFL 185
 FPFL 186
 FPFL 187
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 FPFL 200
 FPFL 201
 FPFL 202
 FPFL 203
 FPFL 204
 FPFL 205
 FPFL 206
 FPFL 207
 FPFL 208
 FPFL 209
 FPFL 210

```

NST=1
L=IDL(I,1)
J=IDL(I,3)
IULDFC(L,J)=IDL(I,4)
298 CONTINUE
299 CONTINUE
IF ( ( GETF .NE. 0 ) .AND. ( STORE .EQ. 0 ) ) GO TO 500
C
C
C
FORM PARALLELPIPED PERMEARILITY MATRIX (IF ISTOP=0)
IF ( ISTOP .EQ. 1 ) GO TO 390
CALL PIPED (IND,NST,PBC,NIMPC,NPT)
IF ( VOL .GT. 0.0 ) GO TO 500
ISTOP=1
WRITE (6,4001) MMF
GO TO 390
C
C
C
STORE ELEMENT PERMEABILITY FOR FUTURE REFERENCE
500 CONTINUE
ISTOP=0
IF ( STORE .EQ. 0 ) GO TO 600
IF ( MMS .NE. MMF ) GO TO 600
IF ( STORE .NE. 1 ) GO TO 510
DO 505 I=1,LNSTOR
505 STORE(I)=J(I)
ISTOP=1
510 CONTINUE
IF ( STORE .NE. 2 ) GO TO 520
DO 515 I=1,LNSTOR
515 STORE2(I)=J(I)
ISTOP=2
520 CONTINUE
IF ( STORE .NE. 3 ) GO TO 530
DO 525 I=1,LNSTOR
  
```

FPEL 211
 FPEL 212
 FPEL 213
 FPEL 214
 FPEL 215
 FPFL 216
 FPEL 217
 FPEL 218
 FPEL 219
 FPEL 220
 FPEL 221
 FPEL 222
 FPEL 223
 FPEL 224
 FPEL 225
 FPFL 226
 FPEL 227
 FPEL 228
 FPEL 229
 FPEL 230
 FPEL 231
 FPEL 232
 FPEL 233
 FPEL 234
 FPEL 235
 FPEL 236
 FPEL 237
 FPEL 238
 FPEL 239
 FPEL 240
 FPEL 241
 FPEL 242
 FPEL 243
 FPEL 244
 FPEL 245

```

525 STORE3(I)=Q(I)
      ISTORE=3
530 CONTINUE
540 CONTINUE
      TVL=TVL+VOL
C
C   MODIFY ELEMENT PERMEABILITY FOR PRESSURE R.C.
C   ADD ELEMENT GENERALIZED FLOWS TO NODAL FLOW VECTOR
C
      DO 300 I=1,8
      J=NODF(I)
      JK(I)=KODE(J)
      DO 380 N=1,8
      KU=1
      II=NODF(N)
      KK=JK(N)
      IF (KK-KD) 335,340,340
C
C       1.0  ADD GENERALIZED FLOWS
C
      DO 336 L=1,LL
      IV=N+8*(L-1)
      BCF(II,L)=BCF(II,L)+Q(IQ)
      GO TO 380
C
C       2.0  PRESSURE BOUNDARY CONDITIONS
C
      DISP=BC(II)
      DO 370 K=1,8
      JJ=NODF(K)
      IF (JJ-II) 345,355,345
      345 CONTINUE
      IF ( JK(K) .EQ. 1 ) GO TO 365
      DO 350 L=1,LL
      350 BCF(JJ,L)=BCF(JJ,L)-QK(K,N)*DISP

```

FPPEL 246
 FPPEL 247
 FPPEL 248
 FPPEL 249
 FPPEL 250
 FPPEL 251
 FPPEL 252
 FPPEL 253
 FPPEL 254
 FPPEL 255
 FPPEL 256
 FPPEL 257
 FPPEL 258
 FPPEL 259
 FPPEL 260
 FPPEL 261
 FPPEL 262
 FPPEL 263
 FPPEL 264
 FPPEL 265
 FPPEL 266
 FPPEL 267
 FPPEL 268
 FPPEL 269
 FPPEL 270
 FPPEL 271
 FPPEL 272
 FPPEL 273
 FPPEL 274
 FPPEL 275
 FPPEL 276
 FPPEL 277
 FPPEL 278
 FPPEL 279
 FPPEL 280

```

    GO TO 365
    355 DO 360 L=1,LL
    360 BPF(JJ,L)=BPF(JJ,L)*DISP
    365 QK(N,K)=0.0
    370 QK(K,N)=0.0
    380 QK(N,N)=1.0
    390 CONTINUE
    395 CONTINUE
    C
    C PRINT ELEMENT DATA
    C
    MPRINT=MPRINT+1
    IF ( MPRINT .LE. 40 ) GO TO 395
    MPRINT=1
    WRITE (6,3000) HED
    WRITE (6,3001)
    395 CONTINUE
    IGET=GETF
    IF ( ISTOP .NE. 0 ) IGET=0
    WRITE (6,2000) MMF, (NODF(I), I=1,9), VOI, ISTOP, IGET
    ISTOP=0
    C
    C STORE ELEMENT TRANSFORMATIONS AND IDENTIFICATION ON NTAPF1
    C
    IF ( ISTOP .EQ. 1 ) GO TO 399
    CALL WRITEB (4,BUFF,LNREC,LNBUFF,MMF,NUMEI,NTAPEI)
    399 CONTINUE
    IF ( MMF .EQ. NUMEL ) GO TO 420
    IF ( MMF .NE. MML ) GO TO 110
    INCF1=INCL1
    INCF2=INCL2
    INCF3=INCL3
    JUMPF2=JUMPL2
    JUMPF3=JUMPL3
    GO TO 100
  
```

```

420 CONTINUE
IF ( ISIOP .EQ. 1 ) RETURN
WRITE (6,30J2) TVL
RETURN
1000 FORMAT(18I4)
2000 FORMAT(10X,15,18,7I5,17,4X, E13.5,17,112)
3000 FORMAT(1H1,10X,13A6)
3001 FORMAT(/83X,23H STORE IN OBTAIN FROM
1/10X,58H ELEMENT N1 N2 N3 N4 N5 N6 N7 NR MATERIAL
2,35H VOLUME BLOCK BLOCK )
3002 FORMAT(10X,15H TOTAL VOLUME=,E15.5)
4000 FORMAT(49H0 ERROR IN ELEMENT DATA CARD SEQUENCE ELEMENT...I3)
4001 FORMAT(40H0 NEGATIVE OR ZERO VOLUME ELEMENT...I3)
4002 FORMAT(14H0 BANDWIDTH OF,18,12H FOR ELEMENT,I5/
1 42H EXCEEDS UPPER LIMIT GIVEN ON CONTROL CARD )
END
FPEL 281
FPEL 282
FPEL 283
FPEL 284
FPEL 285
FPEL 286
FPEL 287
FPEL 288
FPEL 289
FPEL 290
FPEL 291
FPEL 292
FPEL 293
FPEL 294
FPEL 295
FPEL 296

```

```

SUBROUTINE PIPED
C
C 1 (IND,NST,PBC,NN1,NPT)
C
C EIGHT POINT TRILINEAR FINITE ELEMENT
C EIGHT POINT GAUSSIAN INTEGRATION
C IF IND=1 COMPUTES ELEMENT PERMEABILITY
C IF IND=2 COMPUTES FLOW VELOCITIES (QV) AT NPT POINTS OF THE
C ELEMENT GIVEN THE EIGHT NODAL POINT PRESSURES (RB)
C IF NST=1 ELEMENT HAS SURFACE FLOW B.C. OTHERWISE NST=0
C
COMMON / ELARG /
1 4(24),QK(8,8),D(3,3),RHO,VOL,NOIDF(9),XX(A),YY(8),ZZ(8)
COMMON / LOUARG /
1 NUMPC,ACCX,ACCY,ACCZ,NPLN(3),NELD(3),NVEI,NNPL,IDLDFC(3,6)
COMMON / GAUSEQ /
1 NUM,MM,LL,NR,NC,NSET,NRNC
2,NTAPE2,NTAPE3,NTAPE4,NTAPE5,NTAPE6
COMMON / ELFLOW /
1 PPT(9),SPT(9),TPT(9),XPT(9),YPT(9),ZPT(9),QV(6,9),BB(8)
DIMENSION H(8),HD(24),B(24),DB(24),DF(3)
DIMENSION PINT(8),SINT(8),TINT(8)
DATA PINT / 1.0, 1.0, 1.0, 1.0, -1.0, -1.0, -1.0, -1.0 /
DATA SINT / -1.0, -1.0, 1.0, 1.0, 1.0, 1.0, -1.0, -1.0 /
DATA TINT / -1.0, 1.0, -1.0, 1.0, -1.0, 1.0, -1.0, 1.0 /
WT=1.0
SRJ=1.0/SURT(3.0)
F1=ACCX*RHO
F2=-ACCY*RHO
F3=-ACCZ*RHO
DO 1 I=1,3
1 DF(I)=D(I,1)*F1+D(I,2)*F2+D(I,3)*F3
DO 2 I=1,24
Q(I)=0.0

```

```

1 FP8
2 FP8
3 FP8
4 FP8
5 FP8
6 FP8
7 FP8
8 FP8
9 FP8
10 FP8
11 FP8
12 FP8
13 FP8
14 FP8
15 FP8
16 FP8
17 FP8
18 FP8
19 FP8
20 FP8
21 FP8
22 FP8
23 FP8
24 FP8
25 FP8
26 FP8
27 FP8
28 FP8
29 FP8
30 FP8
31 FP8
32 FP8
33 FP8
34 FP8
35 FP8

```

```

2 B(I)=0.0
  IF ( IND .EQ. 2 ) GO TO 6
  DO 3 I=1,d
  DO 3 J=1,b
  3 WK(I,J)=0.0
  VOL=0.0
  DO 110 II=1,b
  P=PIII(II)*SR3
  S=SINT(II)*SR3
  T=TINT(II)*SR3
  GO TO 7
  6 JJ=0
  500 JJ=JJ+1
  P=PII(JJ)
  S=SPT(JJ)
  T=TPT(JJ)
  C
  7 CONTINUE
  C
  PM=1.0-P
  SM=1.0-S
  TM=1.0-T
  PP=1.0+P
  SP=1.0+S
  TP=1.0+T
  PMSM=PM*SM*U.125
  PMSP=PM*SP*0.125
  PMTM=PM*TM*0.125
  PMTP=PM*TP*0.125
  PPSM=PP*SM*0.125
  PPSP=PP*SP*0.125
  PPTM=PP*TM*0.125
  PPTP=PP*TP*0.125
  SMTM=SM*TM*0.125
  SMTP=SM*TP*0.125

```

```

FP8 36
FP8 37
FP8 38
FP8 39
FP8 40
FP8 41
FP8 42
FP8 43
FP8 44
FP8 45
FP8 46
FP8 47
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FP8 49
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FP8 68
FP8 69
FP8 70

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FP8 106
 FP8 107
 FP8 108
 FP8 109
 FP8 110
 FP8 111
 FP8 112
 FP8 113
 FP8 114
 FP8 115
 FP8 116
 FP8 117
 FP8 118
 FP8 119
 FPA 120
 FP8 121
 FP8 122
 FP8 123
 FP8 124
 FP8 125
 FP8 126
 FPA 127
 FP8 128
 FP8 129
 FP8 130
 FPA 131
 FP8 132
 FP8 133
 FP8 134
 FP8 135
 FPA 136
 FP8 137
 FP8 138
 FP8 139
 FP8 140

HU(5)=-PPTP
 HU(6)=PPSM
 HU(7)=SPTM
 HU(8)=PPTM
 HU(9)=PPSP
 HU(10)=SPTP
 HU(11)=PPTP
 HU(12)=PPSP
 HU(13)=SPTM
 HU(14)=PMTM
 HU(15)=PMSP
 HU(16)=SPTP
 HU(17)=PMTP
 HU(18)=PMSP
 HU(19)=SMTM
 HU(20)=PMTM
 HU(21)=PMSM
 HU(22)=SMTP
 HU(23)=PMTP
 HU(24)=PMSM

C
 C FURH AND INVERT JACOBIAN
 C

XP=0.0
 XZ=0.0
 XI=0.0
 YP=0.0
 YZ=0.0
 YI=0.0
 ZP=0.0
 ZZ=0.0
 ZI=0.0
 DU 10 K=1.0
 K3=3*K
 XK=AX(K)

FP8 211
 FP8 212
 FP8 213
 FP8 214
 FP8 215
 FP8 216
 FP8 217
 FP8 218
 FP8 219
 FP8 220
 FP8 221
 FP8 222
 FP8 223
 FP8 224
 FP8 225
 FP8 226
 FP8 227
 FP8 228

```

    UJ=DR(3+I)
    DO 80 K=1,J
      L=3*(K-1)
      80 Q(K,J)=Q(K,N,J)+(U1*B(1+L)+U2*B(2+L)+U3*B(3+L))*FAC
      DO 85 I=1,8
        J=(I-1)*3
        85 Q(I)=Q(I)+(UB(1+J)*ACCX+DR(2+J)*ACCY+UB(3+J)*ACCZ)*FAC*RH0
      110 CONTINUE
    C
    DO 120 J=1,8
      Q(J+8)=Q(J)
      Q(J+16)=Q(J)
      DO 120 K=1,J
        120 QK(J,K)=QK(K,J)
      IF (NST .NE. 0) CALL SQLOAD(PBC,NN1,LL)
    400 RETURN
    END
  
```



```

36 SQL
37 SQL
38 SQL
39 SQL
40 SQL
41 SQL
42 SQL
43 SQL
44 SQL
45 SQL
46 SQL
47 SQL
48 SQL
49 SQL
50 SQL
51 SQL
52 SQL
53 SQL
54 SQL
55 SQL
56 SQL
57 SQL
58 SQL
59 SQL
60 SQL
61 SQL
62 SQL
63 SQL
64 SQL
65 SQL
66 SQL
67 SQL
68 SQL
69 SQL
70 SQL

```

```

D(1)=XG(4)-XG(1)
D(2)=YG(4)-YG(1)
D(3)=ZG(4)-ZG(1)
C(1)=A(2)*B(3)-B(2)*A(3)
C(2)=A(3)*B(1)-B(3)*A(1)
C(3)=A(1)*B(2)-B(1)*A(2)
B(1)=C(2)*A(3)-A(2)*C(3)
B(2)=C(3)*A(1)-A(3)*C(1)
B(3)=C(1)*A(2)-A(1)*C(2)
AM=0.0
BM=0.0
CM=0.0
DO 30 I=1,3
AM=AM+A(I)*H(I)
BM=BM+H(I)*B(I)
CM=CM+C(I)*C(I)
30 CONTINUE
DO 40 I=1,3
A(I)=A(I)/SQRT(AM)
B(I)=B(I)/SQRT(BM)
C(I)=C(I)/SQRT(CM)
40 CONTINUE
DO 50 I=1,4
XL(I)=A(I)*XG(I)+A(2)*YG(I)+A(3)*ZG(I)
YL(I)=B(I)*XG(I)+B(2)*YG(I)+B(3)*ZG(I)
ZL(I)=C(I)*XG(I)+C(2)*YG(I)+C(3)*ZG(I)
50 CONTINUE
C
C
C
OBTAIN INTERPOLATION FUNCTIONS AND JACOBIAN DETERMINANT
DO 200 II=1,4
S=SIGNT(II)*SR3
T=INT(II)*SR3
SM=1.0-S
SP=1.0+S

```

SQL 71
 SQL 72
 SQL 73
 SQL 74
 SQL 75
 SQL 76
 SQL 77
 SQL 78
 SQL 79
 SQL 80
 SQL 81
 SQL 82
 SQL 83
 SQL 84
 SQL 85
 SQL 86
 SQL 87
 SQL 88
 SQL 89
 SQL 90
 SQL 91
 SQL 92
 SQL 93
 SQL 94
 SQL 95
 SQL 96
 SQL 97
 SQL 98
 SQL 99

```

  TM=1.0-T
  TP=1.0*I
  H(1)=0.25*SM*TM
  H(2)=0.25*SP*TM
  H(3)=0.25*SP*TP
  H(4)=0.25*SM*TP
  X2=0.25*(TM*(XL(2)-XL(1)) + TP*(XL(3)-XL(4)) )
  Y2=0.25*(TM*(YL(2)-YL(1)) + TP*(YL(3)-YL(4)) )
  XT=0.25*(SM*(XL(4)-XL(1)) + SP*(XL(3)-XL(2)) )
  YT=0.25*(SM*(YL(4)-YL(1)) + SP*(YL(3)-YL(2)) )
  XJAC=1.0/(XS*YT-XT*YS)

  C
  C OBTAIN GENERALIZED FLOWS FOR EACH LOADING CASE
  C
  DO 100 L=1,LL
  LD=LDLDFC(L,IFACE)
  IF ( LD .EQ. 0 ) GO TO 100
  WL=PBC(LD,1)*H(1)+PBC(LD,2)*H(2)+PBC(LD,3)*H(3)+PBC(LD,4)*H(4)
  FAC=RH0*WT*XJAC*QL
  DO 90 I=1,4
  J=IFACE(IFACE,I)+8*(L-1)
  WJ=-FAC*H(I)
  W(J)=W(J)+WJ
  90 CONTINUE
  100 CONTINUE
  200 CONTINUE
  300 CONTINUE
  RETURN
  END
  
```



```

IF ( (II.LI.NR1) .OR. (II.GI.NR2) ) GO TO 30
IJ=II-NRS
DO 20 J=1,8
JJ=NODF(J)-II+1
IF (JJ.LE.0) GO TO 20
A(IJ,JJ)=A(IJ,JJ) + QK(I, I)
20 CONTINUE
30 CONTINUE
35 CONTINUE
C
C
C
ADD FLOW VECTORS
DO 60 I=1, NR
IN=I+NRS
IF ( IN.GT. MW ) GO TO 65
DO 60 L=1, LL
A(I,L+MM)=BCF(IN,L)
60 WRITE (NTAPE2) A
70 CONTINUE
RETURN
END

```

```

FPST 36
FPST 37
FPST 38
FPST 39
FPST 40
FPST 41
FPST 42
FPST 43
FPST 44
FPST 45
FPST 46
FPST 47
FPST 48
FPST 49
FPST 50
FPST 51
FPST 52
FPST 53
FPST 54
FPST 55
FPST 56

```



```

1  FPFE
2  FPFE
3  FPFE
4  FPFE
5  FPFE
6  FPFE
7  FPFE
8  FPFE
9  FPFE
10 FPFE
11 FPFE
12 FPFE
13 FPFE
14 FPFE
15 FPFE
16 FPFE
17 FPFE
18 FPFE
19 FPFE
20 FPFE
21 FPFE
22 FPFE
23 FPFE
24 FPFE
25 FPFE
26 FPFE
27 FPFE
28 FPFE
29 FPFE
30 FPFE
31 FPFE
32 FPFE
33 FPFE
34 FPFE
35 FPFE

```

```

SUBROUTINE FPFE
C THIS SUBROUTINE PRINTS RESULTS
C
C
C
C
COMMON / GENCUN /
1 HED(13),WORD(2),NUMEL,NUMNP,NUMMAI,ISTOP,MAXBAN,NSTRES,NPT
2,LNSTOR,NUMDC,NST
COMMON / GAUSEL /
1 NU,MM,LL,NR,NC,NSET,NRNC
2,NTAPE2,NTAPE3,NTAPE4,NTAPE5,NTAPE6
COMMON / ELARG /
1 J(24),QK(8,8),D(3,3),RHO,VUL,NODF(9),XX(R),YY(8),ZZ(8)
COMMON / BUFFER /
1 LNREC,LNBUFF,NTAPE1,BUFF(2040)
COMMON / ELFLOW /
1 PPT(9),SPT(9),TPT(9),XPT(9),YPT(9),ZPT(9),QV(6,9),BR(8)
DIMENSION RE(NI,1),B(1),ICOUNT(1),AVGQV(NI,1)
C
C NST=0
C IND=2
C NUMPC=0
C MPRINT=0
C
C FOR EACH LOAD CASE
C DO 300 L=1,LL
C
C INITIALIZE
C IF ( NSTRES .EQ. 0 ) GO TO 7
C DO 6 I=1,NUMNP
C ICOUNT(I)=0
C DO 6 J=1,3
C AVGQV(I,J)=0.0

```

```

FPRE 36
FPRE 37
FPRE 38
FPRE 39
FPRE 40
FPRE 41
FPRE 42
FPRE 43
FPRE 44
FPRE 45
FPRE 46
FPRE 47
FPRE 48
FPRE 49
FPRE 50
FPRE 51
FPRE 52
FPRE 53
FPRE 54
FPRE 55
FPRE 56
FPRE 57
FPRE 58
FPRE 59
FPRE 60
FPRE 61
FPRE 62
FPRE 63
FPRE 64
FPRE 65
FPRE 66
FPRE 67
FPRE 68
FPRE 69
FPRE 70

```

```

6 CONTINUE
7 CONTINUE
C
C PRINT NODAL PRESSURES
C
WRITE (6,3000) HED
WRITE (6,3005) L
WRITE (6,3001)
ITAPE=L+6
READ (ITAPE) (B(I),I=1,NG)
DO 10 I=1,NUMNP
MPRINT=MPRINT+1
IF ( MPRINT .LE. 50 ) GO TO 20
MPRINT=1
WRITE (6,3000) HED
WRITE (6,3005) L
WRITE (6,3001)
20 CONTINUE
30 CONTINUE
C
C EVALUATE AND PRINT ELEMENT VELOCITIES
C
WRITE (6,3000) HED
WRITE (6,3005) L
WRITE (6,3002)
MPRINT=0
DO 50 N=1,NUMEL
CALL READBF (Q,BUFF,LNREC,LINEBUFF,N,NUMEL,NTAPE1)
DO 30 I=1,8
J=NOOF(I)
30 BB(I)=B(J)
DO 40 I=1,d
M=NOOF(I)
S=U.0

```

```

71 FPPE
72 FPPE
73 FPPE
74 FPPE
75 FPPE
76 FPPE
77 FPPE
78 FPPE
79 FPPE
80 FPPE
81 FPPE
82 FPPE
83 FPPE
84 FPPE
85 FPPE
86 FPPE
87 FPPE
88 FPPE
89 FPPE
90 FPPE
91 FPPE
92 FPPE
93 FPPE
94 FPPE
95 FPPE
96 FPPE
97 FPPE
98 FPPE
99 FPPE
100 FPPE
101 FPPE
102 FPPE
103 FPPE
104 FPPE
105 FPPE

```

```

DU 35 K=1,8
35 S=S+QK(I,K)*BB(K)
R=(M,L)/RE(M,L)=S
40 CONTINUE
CALL PIPEU (IND,NST,PBC,NUMMPC,NPT)
MPRINT=MPRINT+1
IF ( MPRINT .LE. 40 ) GO TO 41
MPRINT=1
WRITE (6,3000) HD
WRITE (6,3001) L
WRITE (6,3002)
41 CONTINUE
WRITE (6,2002) N,XPT(1),YPT(1),ZPT(1),(JV(I,1),I=1,3)
IF ( NSTRES .EQ. 0 ) GO TO 50
DU 45 I=1,8
J=NOZF(I)
ICOUNT(J)=ICOUNT(J)+1
DU 45 K=1,3
AVGQV(J,K)=AVGQV(J,K)+QV(K,I+1)
45 CONTINUE
50 CONTINUE
C
C
C
AVERAGE NODAL POINT VELOCITIES ( IF NSTRES=1)
IF ( NSTRES .EQ. 0 ) GO TO 85
DU 60 I=1,NUMNP
DEN=ICOUNT(I)
DU 60 J=1,3
AVGQV(I,J)=AVGQV(I,J)/DEN
60 CONTINUE
WRITE (6,3000) HD
WRITE (6,3005) L
WRITE (6,3003)
MPRINT=0
DU 80 I=1,NUMNP

```



```

2002 FORMAT(10X, I5, 5X, 3F15.5, 3F15.5)
2003 FORMAT(10X, I4, X, 4E15.5)
2004 FORMAT(10X, I4, X, E15.5)
3000 FORMAT(1H, I3, X, 13A6)
3001 FORMAT(12X, 20H NODE
3002 FORMAT(
1/10X, 2HX, 12H COORDINATES, 34X, 11H VELOCITIES
2/10X, 8H ELEMENT, 11X, 1HX, 14X, 1HY, 14X, 1HZ, 10X, 1HX, 14X, 1HY, 14X, 1HZ)
3003 FORMAT(22X, 26H AVERAGED NODAL VELOCITIES, 16X, 10H RESULTANT
1/10X, 5H NODE, 5X, 1HX, 14X, 1HY, 14X, 1HZ)
3004 FORMAT(/10X, 20H NODE
3005 FORMAT(10X, 10H LOAD CASE, 73)
END
FPRE 141
FPRE 142
FPRE 143
FPRE 144
FPRE 145
FPRE 146
FPRE 147
FPRE 148
FPRE 149
FPRE 150
FPRE 151
FPRE 152
FPRE 153

```



```

BACKSPACE NPKCSB
190 CONTINUE
C
C      3.0 STORE SOLUTIONS ON TAPE ITAPE
C
200 CONTINUE
DO 220 L=1,LL
ITAPE=L*6
REWIND ITAPE
DO 210 N=1,NSET
M1=(NSET-N)*NR+1
M2=M1+NR-1
210 READ (ITAPE) (AT(M),M=M1,M2)
REWIND ITAPE
WRITE (ITAPE) (AT(I),I=1,NQ)
REWIND ITAPE
220 CONTINUE
240 RETURN
END

```

```

GSI 106
GSI 107
GSI 108
GSI 109
GSI 110
GSI 111
GSI 112
GSI 113
GSI 114
GSI 115
GSI 116
GSI 117
GSI 118
GSI 119
GSI 120
GSI 121
GSI 122
GSI 123
GSI 124

```



```

DO 40 J=1,J2
40 AT(I,J)=AT(I,J)-C*AT(KK,IK+J)
50 CONTINUE
60 CONTINUE
D=AT(I2,I)
IF ( D .EQ. 0.0 ) GO TO 65
DD=SQRT(D)
DO 61 I=1,NC
61 AT(I2,I)=AT(I2,I)/DD
62 CONTINUE
IF ( N .EQ. NSET ) GO TO 730
WRITE (NBCKSB) AT
READ (NT1) AB
C
C
C
NRR=NR
DO 110 I=NR1,NQLF
110 I=I-NRR
IF ( II .LE. NR ) GO TO 7A
WRITE (NT2) AB
READ (NT1) AB
NRR=NRR+NR
II=1
70 CONTINUE
KKMIN=I-MMM1
IF ( KKMIN .LT. 1 ) KKMIN=1
DO 100 KK=KKMIN,NR
100 U=AT(KK,I)
IF ( U .EQ. 0.0 ) GO TO 1A0
IK=I-KK
C=AT(KK,IK+1)
IF ( C .EQ. 0.0 ) GO TO 1A0
K=KK+1
KM=KK+MM

```

```

71 GS2
72 GS2
73 GS2
74 GS2
75 GS2
76 GS2
77 GS2
78 GS2
79 GS2
80 GS2
81 GS2
82 GS2
83 GS2
84 GS2
85 GS2
86 GS2
87 GS2
88 GS2
89 GS2
90 GS2
91 GS2
92 GS2
93 GS2
94 GS2
95 GS2
96 GS2
97 GS2
98 GS2
99 GS2
100 GS2
101 GS2
102 GS2
103 GS2
104 GS2
105 GS2

```



```

160 AB(NR+J)=AB(J)
DO 165 I=1,NR
165 AB(I+MNL)=AT(I,ML)
DO 175 II=1,NR
JJ=NR-II
I=JJ+1
JM=JJ+MNL
IF ( AT(I,1) .EQ. 0.0 ) GO TO 175
S=AB(I+MNL)
DO 170 J=2,MM
170 S=S-AT(I,J)*AB(J+JM)
AB(I+MNL)=S/AT(I,1)
175 B(I)=AB(I+MNL)
WRITE (ITAPE) B
190 CONTINUE
C
C
C
3.0 STORE SOLUTIONS ON TAPE ITAPE
DO 220 L=1,LL
ITAPE=L+6
REWIND ITAPE
DO 210 N=1,NSET
M1=(NSET-N)*NR+1
M2=M1+NR-1
210 READ (ITAPE) (AT(M),M=M1,M2)
REWIND ITAPE
WRITE (ITAPE) (AT(I),I=1,NQ)
REWIND ITAPE
220 CONTINUE
240 RETURN
END

```

```

GS2 141
GS2 142
GS2 143
GS2 144
GS2 145
GS2 146
GS2 147
GS2 148
GS2 149
GS2 150
GS2 151
GS2 152
GS2 153
GS2 154
GS2 155
GS2 156
GS2 157
GS2 158
GS2 159
GS2 160
GS2 161
GS2 162
GS2 163
GS2 164
GS2 165
GS2 166
GS2 167
GS2 168
GS2 169
GS2 170
GS2 171

```

SUBROUTINE CPTIME(T)
CALL SECOND(T)
RETURN
END

CPT
CPT
CPT
CPT

1 2 3 4

```

SUBROUTINE WRITBF (REC,BUFF,LNREC,LNBUFF,N,NUMEL,NTAPE)
DIMENSION REC(LNREC),BUFF(LNBUFF)
IF ( N .NE. 1 ) GO TO 10
REWIND NTAPE
M=0
10 MM=M+LNREC
DO 20 I=1, LNREC
  11=I+M
  20 BUFF(11)=REC(I)
  M=MM
  IF ( N .EQ. NUMEL ) GO TO 30
  IF ( (M+LNREC) .LE. LNBUFF ) GO TO 40
  30 WRITE (NTAPE) BUFF
  M=0
  40 RETURN
END

```

```

WRB
WRB
WRB
WRB
WRB
WRB
WRB
WRB
WRB
WRB
WRB
WRB
WRB
WRB
WRB
WRB

```

```

1
2
3
4
5
6
7
8
9
10
11
12
13
14
15
16

```