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Using Low-Frequency Earthquake Families on the San Andreas Fault as Deep Creepmeters

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Abstract

The central section of the San Andreas Fault hosts tectonic tremor and lowfrequency earthquakes (LFEs) similar to subduction zone environments. LFEs are often interpreted as persistent regions that repeatedly fail during the aseismic shear of the surrounding fault allowing them to be used as creepmeters. We test this idea by using the recurrence intervals of individual LFEs within LFE families to estimate the timing, duration, recurrence interval, slip, and slip rate associated with inferred slow slip events. We formalize the definition of a creepmeter and determine whether this definition is consistent with our observations. We find that episodic families reflect surrounding creep over the interevent time, while the continuous families and the short time scale bursts that occur as part of the episodic families do not. However, when these families are evaluated on time scales longer than the interevent time these events can also be used to meter slip. A straightforward interpretation of episodic families is that they define sections of the fault where slip is distinctly episodic in well-defined slow slip events that slip 16 times the long-term rate. In contrast, the frequent short-term bursts of the continuous and short time scale episodic families likely do not represent individual creep events but rather are persistent asperities that are driven to failure by quasi-continuous creep on the surrounding fault. Finally, we find that the moment-duration scaling of our inferred creep events are inconsistent with the proposed linear moment-duration scaling. However, caution must be exercised when attempting to determine scaling with incomplete knowledge of scale.

1 Introduction

While many slow slip events (SSEs) are aseismic and can only be detected using geodetic techniques, some slow earthquakes do have a seismic manifestation. For example, long-duration, small-amplitude seismic signals, dubbed nonvolcanic tremor (NVT) or tectonic tremor, usually lack the obvious impulsive phase arrivals associated with regular earthquakes and are depleted in high-frequency content relative to conventional earthquakes of the same moment (Ide et al., 2007; Obara, 2002). Short-duration seismic signals known as low-frequency earthquakes (LFEs) more closely resemble conventional earthquakes and were initially found to occur as part of tremor episodes (Shelly et al., 2007). Shelly et al. (2007) demonstrated that the NVT

signal in Japan can be explained as a superposition of many LFEs. Similar analysis was later applied to tremor on the Parkfield section of the San Andreas Fault (SAF), which has produced a catalog of over one million LFEs detected between 2001 and 2016 grouped into 88 different families based on waveform similarity between events (Shelly, 2017). Locations and depths of these 88 LFE families are shown in Figure 1.

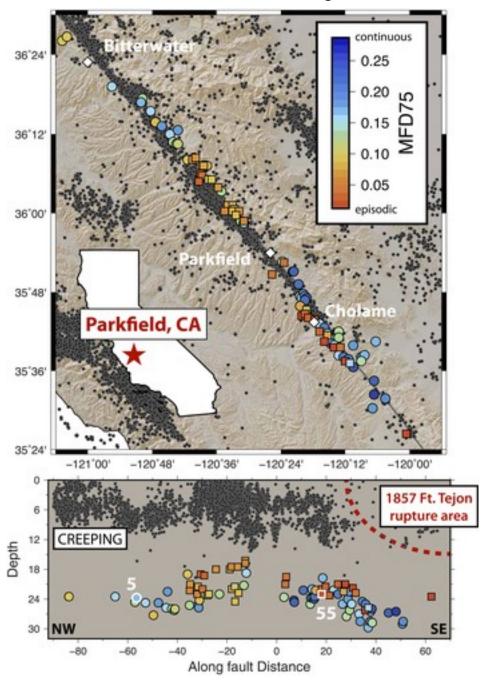


Figure 1 (top) Parkfield area location map with LFE locations are plotted as either circles (continuous families) or squares (episodic families) and color coded by MFD75 which is the minimum fraction of days required to contain 75% of the events in each family (Shelly & Johnson, 2011). Hypocenters of

earthquakes that occurred in the last decade (i.e., 2006–2016) are shown as gray dots. Inset shows location of Parkfield within the state of California. (bottom) Along fault cross section of the San Andreas viewed from the southwest (vertically exaggerated 2 times) showing locations of LFE families shown in the top and earthquakes within 10 km of the fault. The creeping and locked sections of the fault are annotated with approximate location of the 1857 Fort Tejon rupture area indicated by the dashed red line.

Within individual LFE families event occurrence is not steady. In some families, groups of a few events recur on time scales of days, while in other families there are nearly quiescent periods that often last for months followed by the occurrence of hundreds of events over the course of a few days (Shelly & Johnson, 2011; Thomas et al., 2012). These two end-member behaviors are shown in Figures 2a and 2b and are termed continuous and episodic, respectively. These styles of occurrence are not unique to Parkfield (Chamberlain et al., 2014; Frank et al., 2015; Royer et al., 2015; Wech & Creager, 2011). Though there is no geodetic signal associated with times of high LFE rate on the SAF (Smith & Gomberg, 2009), the cycle of guiescence followed by high-seismicity rate in the most episodic families is reminiscent of tremor accompanying SSEs in subduction zones. Shelly and Johnson (2011) quantified the episodicity of 88 LFE families on the deep SAF by measuring the minimum fraction of days necessary to contain 75% of all events (abbreviated MFD75). MFD75 scales inversely with family episodicity so that continuous families (Figure 2a) have high MFD75, while episodic families (Figure 2b) have low MFD75. MFD75 values for the 88 LFE families in Parkfield are shown in Figure 1. Shelly and Johnson (2011) also note a firstorder decrease of episodicity with depth. Similar changes in episodicity with depth have been observed using tremor in Cascadia (Wech & Creager, 2011) and low-frequency earthquakes in Japan (Obara, 2010) and Cascadia (Royer et al., 2015). Additionally, some LFE families have slip histories that closely resemble those of neighboring families suggesting that these distinct LFE families take part in the same underlying slip episode (Shelly, 2015; Trugman et al., 2015).

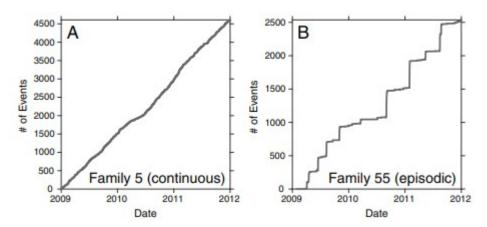


Figure 2

(a) The cumulative number of LFEs in family 5, a continuous family, as a function of time for the 3 year period from 2009 to 2012. (b) The same as Figure 2a but for episodic family 55. Locations of both families are shown in Figure 1.

One simple, popular conceptual model for LFEs is that like shallow repeating earthquakes, they represent radiation emanating from small, persistent regions that repeatedly fail during the aseismic shear of the larger-scale surrounding fault zone (Bufe et al., 1977; Schaff et al., 1998; Shelly et al., 2007; Nadeau & McEvilly, 1999). In this model, the earthquakes source itself is sufficiently small and its occurrence is a passive meter of the rate of fault creep. If this model is valid then the seismicity rate $\it R$ is proportional to the slip rate $\it V$ on the surrounding fault

$$R = V/d$$
. (1)

Here d is the characteristic slip per event. Equation 1 has the added implication that

$$V/V_L = R/R_L$$
. (2)

 R_L is the seismicity rate at a reference creep rate V_L . Equation 2 quantifies the relationship between the seismicity rate and the slip rate of the fault, and its application potentially allows each LFE source to be used as a fault creepmeter that could be monitored in near real time due to the large number of LFEs per family (Table 1) and the short interevent times.

Table 1 LFE Episode Properties

1C 24880 3,648 2C 28856 3,648 33C 53539 5,021 4C 32371 5,957 5C 30057 8,941 6C 41472 7,593 7C 53504 5,118 8C 24047 8,393 9C 36212 15,716 110C 34803 6,670	4 0.0972 8 0.0967 11 0.0703 7 0.0592 11 0.0395 3 0.0465 8 0.0689	546	5.0		ō	>	*	No.	Level.	,	P ₃		×
		546	2.0										
				5.3468	3.27e-02	5.21e-07	0.8857						
		538	2.0	5.8674	3.67e-02	2.23e-06	0.8580				,		
		734	5.0	3.2869	3.25e-02	9.51e-07	0.7572						ì
		111	0.9	4.6854	7.56e-02	7.38e-07	0.9481						
		1,123	7.0	2.4928	4.58e-02	3.67e-07	0.9129						,
		1,009	0.9	2.8294	3.86e-02	6.56e-07	0.9194						ì
		611	7.0	5.4479	6.03e-02	7.19e-07	0.9134					,	
		1,158	0.9	2.3212	4.25e-02	3.71e-07	0.8924						
		1,166	13.0	2.3384	7.33e-02	3.52e-07	0.9454						ì
	9 0.0333	1,530	2.0	1.0604	3.17e-02	5.44e-07	0.8049					,	
		970	2.0	2.9737	5.31e-02	6.92e-07	0.8388					,	
	6 0.0522	951	2.0	2.5415	4.42e-02	7.99e-07	0.7981					,	
19399 3,423		543	4.0	5.3994	3.83e-02	9.66e-07	9/69/0						
	1 0.0781	670	4.0	2.0269	1.91e-02	1.61e-06	0.6050					,	
40144 5,341		860	4.0	2,6792	1.81e-02	1.74e-06	0.7553						
14975 5,852		593	3.0	0.0594	1.28e-02	2.37e-06	0.5446	248	21.8	14.3472	1.15e+01	9.20e-09	0.9872
6861 5,230		404	4.0	0.1091	1.31e-02	2.77e-06	0.5021	278	17.6	13.3029	1.99e+01	6.20e-09	0.9763
		115	3.0	0.2727	1.05e-02	4.17e-06	0.2665	188	11.9	16.2357	1.75e+01	1.17e-08	0.9673
		639	4.0	0.1646	1.19e-02	2.10e-06	0.5725	286	17.5	13.0433	2.75e+01	6.12e-09	0.9851
40372 6,465		1,071	4.0	2.7783	2.31e-02	1.15e-06	0.7780					,	
25049 6,962		1,174	5.0	2.5639	2.11e-02	7.03e-07	0.8702					,	
83946 9,850		1,317	4.0	0.3012	2.50e-02	8.49e-07	0.6081	·					ŀ
		478	3.0	0.0459	1.33e-02	2.49e-06	0.3074	8	8.09	38.6832	2.90e+01	1.38e-08	0.9945
		154	3.0	0.2342	9.72e-03	4.31e-06	0.2730	183	15.8	17.6779	2.65e+01	9.83e-09	0.9692
	7 0.0413	716	4.0	0.0470	1.22e-02	1.96e-06	0.4983	105	75.8	39.8836	3.65e+01	1.69e-08	0.9911
45843 8,887		1,002	4.0	0.2895	1.46e-02	1.33e-06	0.6884	277	17.5	13.3737	3.34e+01	5.16e-09	0.9922
17268 8,453	3 0.0417	200	4.0	0.2898	1.08e-02	1.82e-06	0.5838	267	16.9	13.9104	3.34e+01	5.53e-09	0.9929
77401 7,468		1,036	4.0	0.1725	2.66e-02	7.66e-07	0.6575	127	45.1	28.5126	8.47e+01	6.49e-09	0.9949
18319 4,360		738	4.0	2.5551	1.12e-02	2.26e-06	99690						
31014 4,096		402	3.0	0.4063	1.61e-02	2.49e-06	0.4963	169	9.4	19.5979	2.96e+01	5.99e-09	0.9893
21253 3,056		224	3.0	0.3660	8.06e-03	90-e09'9	0.3514	139	10.3	25.7851	2.32e+01	7.94e-09	0.9921
		308	3.0	0.2428	1.39e-02	2.82e-06	0.5663	265	11.9	13.4903	2.34e+01	5.21e-09	0.9799
70316 7,962	2 0.0443	944	4.0	0.2994	1.53e-02	1.29e-06	0.8541	328	18.7	11.0103	3.63e+01	3.28e-09	0.9940
36319 4,262	2 0.0827	282	4.0	0.1420	1.43e-02	2.08e-06	0.7405	387	9.4	9.3987	1.20e+01	9.45e-09	0.9693
21462 7,092		869	4.0	0.1880	1.50e-02	1.68e-06	0.6128	171	17.9	19.6325	5.11e+01	4.90e-09	0.9937
9707 8,165		230	4.0	0.1387	1.75e-02	1.19e-06	0.8567	374	21.0	9.9300	2.05e+01	4.70e-09	0.9945
_		320	3.0	7.3823	1.32e-02	4.03e-06	0.4857						
37102 7,400		754	2.0	0.1681	1.64e-02	1.39e-06	0.7168	289	15.1	10.6611	1.69e+01	9.38e-09	0.9791

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	rein	2	OLFE.	Ne e	rues/eb.	Į.	P	١	×	e e	LrEs/ep.	2	P	>	×
39E	37140	4,173	0.0845	186	3.0	0.2674	7.88e-03	3.17e-06	0.2578	193	11.5	15.2903	2.79e+01	9.72e-09	0.9715
40C	27270	5,166	0.0683	803	4.0	2.8298	1.39e-02	2.38e-06	0.6597	í					
41C	42513	7,733	0.0456	834	6.0	4.3530	1.00e-01	4.15e-07	0.8477	i					
42E	47927	7,465	0.0471	22.7	4.0	0.0566	1.28e-02	2.02e-06	0.3928	236	31.6	12.0482	2.42e+01	1.35e-08	0.9412
43E	17171	5,780	0.0610	455	3.0	0.1043	1.06e-02	2.65e-06	0.3753	175	36.7	20.0123	3.19e+01	1.24e-08	0.9926
44C	54704	4,173	0.0845	612	4.0	4.1208	1.86e-02	1.13e-06	0.5806	ì	ì	ì		ì	
45C	68814	5,236	0.0674	811	4.0	3.4257	2.10e-02	1.03e-06	0.6646	ì					
46C	18406	11,324	0.0311	1,316	7.0	2.6257	3.00e-02	1.07e-06	0.8885	i					
47C	35503	4,675	0.0756	711	2.0	4.1542	4.64e-02	9.86e-07	0.8361	ì					
48C	21352	4,457	0.0792	869	4.0	3.9685	4.97e-02	8.54e-07	0.7402	ì					
49C	45768	6,339	0.0557	935	2.0	3.0669	3.42e-02	5.12e-07	0.8295	ì					
20C	30397	5,082	0.0695	292	4.0	3.7628	5.00e-02	7.85e-07	0.7721	ì					
51C	37811	9,122	0.0387	1,313	5.0	2.2783	6.44e-02	4.34e-07	0.8591	ì	ì		ì	ì	
52C	37796	11,877	0.0297	1,449	0.9	2.1473	5.33e-02	4.11e-07	0.8968	ì					
53C	15025	8,766	0.0401	1,105	2.0	0.3915	4.20e-02	7.35e-07	0.7886	i					
54E	34680	8,419	0.0418	339	5.0	0.3522	2.72e-02	7.49e-07	0.8626	222	12.3	11.4660	1.70e+01	8.03e-09	0.9614
35E	58668	11,435	0.0307	1,005	0.9	0.0689	8.03e-02	4.34e-07	0.8468	110	53.2	23.9833	4.00e+01	1.57e-08	0.9771
395	58755	11,090	0.0317	1,106	5.0	0.0870	5.78e-02	5.09e-07	0.8074	150	25.9	19.9325	3.68e+01	1.23e-08	0.9728
57C	15157	10,135	0.0348	1,129	7.0	2.9390	6.06e-02	4.94e-07	0.9054	ì					
28E	54021	10,505	0.0335	831	7.0	0.0626	8.11e-02	4.95e-07	0.8416	128	6.11	18.9769	1.90e+01	2.06e-08	0.9574
365	41767	12,596	0.0279	649	0.6	0.0851	1.33e-01	3.36e-07	0.9135	113	59.6	19.2511	1.17e+01	3.14e-08	0.9636
O00	16160	14,962	0.0236	1,187	10.0	2.8699	1.31e-01	2.06e-07	0.9563	,					
91E	32192	12,971	0.0272	655	11.0	0.1147	7.39e-02	6.12e-07	0.9413	113	59.1	25.0526	3.07e+01	1.80e-08	0.9823
97C	46177	20,726	0.0170	1,579	11.0	2.4012	1.17e-01	2.04e-07	0.9737	,					
93C	25753	11,263	0.0313	1,152	0.6	2.9830	5.29e-02	1.83e-07	0.9591	,					,
2 6	25879	8,062	0.0437	499	0.9	0.1656	3.61e-02	6.86e-07	0.8993	124	24.7	23.9669	1.76e+01	1.62e-08	0.9677
95E	68539	9,227	0.0378	808	7.0	0.0802	6.50e-02	6.17e-07	0.8207	106	67.3	28.2266	5.59e+01	1.56e-08	0.9806
299	19165	15,031	0.0235	286	15.0	3.7140	8.47e-02	2.45e-07	0.9773	ì					
92C	11612	7,856	0.0450	1,107	0.9	2.9868	4.22e-02	1.52e-07	0.8886	,					
98C	47706	9,287	0.0380	1,189	7.0	2.9488	3.67e-02	8.08e-07	0.9507	ì					
269	28381	6,731	0.0524	177	0.9	4.2596	1.14e-01	1.76e-07	0.9054	,					
70C	50672	7,253	0.0487	946	0.9	3.6957	3.36e-02	1.02e-06	0.9109	,					
71E	83647	7,819	0.0447	717	7.0	0.0764	6.97e-02	6.90e-07	0.8688	63	132.1	58.5354	1.60e+02	5.98e-09	0.9949
72E	9619	8,565	0.0407	1,075	6.0	0.1228	2.44e-02	1.05e-06	0.8697	73	129.2	49.3267	1.48e+02	6.74e-09	0.9968
73C	8893	7,160	0.0492	1,028	5.0	2.9007	2.62e-02	1.29e-06	0.8820	ì					
74C	38879	10,136	0.0349	1,150	8.0	3.2201	6.29e-02	4.50e-07	0.9717	,					
75C	61095	10,606	0.0333	1,347	7.0	2.5387	2.83e-02	1.22e-06	0.9414	ì					
76E	10824	7,021	0.0495	792	7.0	0.0681	4.44e-02	9.39e-07	0.8895	55	139.9	71.7628	8.07e+01	1.47e-08	0.9979

FEID LFEID N d _{LFE} N _e LFEs/ep.	33845 15842 58459	N 11,873 4,217 10,317	d _{LFE} 0.0297	N,	and the same of										
11,873 0.0297 1,324 8.0 2.594 3.53e-02 7.73e-07 0.9057 - - 4,217 0.0837 863 4.0 2.9850 1.06e-02 8.90e-06 0.9208 - - 10,317 0.0834 4.0 2.9850 1.06e-02 8.67e-07 0.9147 156 13.6 14.4646 1 20,843 0.0169 1,569 12.0 2.2521 1.04e-01 1.52e-07 0.9178 - - - 16,740 0.0211 1,197 14.0 3.3089 8.28e-02 4.23e-07 0.9880 - - - 15,999 0.0211 1,197 14.0 3.3813 1.70e-01 3.96e-07 0.9169 - - - 11,264 0.0214 1,712 11.0 3.46e-02 3.46e-07 0.9169 - - - - 11,264 0.0214 1,544 7.0 2.4473 4.6f-02 3.46e-07 0.9169	33845 15842 58459	11,873 4,217 10,317	0.0297	u	Lres/ep.	t,	t,	^	×	N	LFEs/ep.	t,	t _d	/	×
15842 4,217 0.0837 863 4.0 2.9850 1.06e-02 8.90e-06 0.9208 - - 58459 10,317 0.0342 406 5.0 0.2888 1.82e-02 8.67e-07 0.9147 156 13.6 14.4646 1 40527 20,843 0.0169 1,569 12.0 2.2521 1.04e-01 1.52e-07 0.9147 156 14.4646 1 37479 16,740 0.0211 1,197 14.0 3.3089 8.28e-02 4.23e-07 0.9880 - - - 40453 15,999 0.0221 1,197 14.0 3.36e-02 5.30e-07 0.9314 - - - 58966 12,659 0.0279 1,012 11.0 3.8513 1.70e-01 3.96e-07 0.9169 - - - - 40092 11,264 0.0314 1,374 7.0 2.4473 4.67e-02 3.46e-07 0.9169 - - -	15842 58459	4,217		1,324	8.0	2.5494	3.53e-02	7.73e-07	0.9057						٠
58459 10,317 0.0342 406 5.0 0.2888 1.82e-02 8.67e-07 0.9147 156 13.6 14.4646 40527 20,843 0.0169 1,569 12.0 2.2521 1.04e-01 1.52e-07 0.9778 - - 37479 16,740 0.0211 1,197 14.0 3.3089 8.28e-02 4.23e-07 0.9880 - - - 40453 15,999 0.0221 1,788 7.0 1.9539 3.81e-02 5.30e-07 0.9314 - - - 40492 11,264 0.0219 1,012 11.0 3.8513 1.70e-01 3.96e-07 0.9169 - - - 40492 11,264 0.0314 1,374 7.0 2.4473 4.67e-02 3.46e-07 0.9169 - - - 44437 12,974 0.0431 1,053 6.0 2.1058 3.04e-02 0.49e-07 0.8433 - - -	58459	10,317	0.0837	863	4.0	2.9850	1.06e-02	8.90e-06	0.9208						٠
40527 20,843 0.0169 1,569 12.0 2.2521 1.04e-01 1.52e-07 37479 16,740 0.0211 1,197 14.0 3.3089 8.28e-02 4.23e-07 40453 15,999 0.0221 1,788 7.0 1.9539 3.81e-02 5.30e-07 58966 12,659 0.0279 1,012 11.0 3.8513 1,70e-01 3.96e-07 40092 11,264 0.0314 1,374 7.0 2.4473 4.67e-02 3.46e-07 44437 12,974 0.0272 1,645 6.0 2.1058 3.04e-02 6.78e-07 41449 8,189 0.0431 1,053 6.0 2.9663 4.25e-02 9.49e-07			0.0342	406	2.0	0.2888	1.82e-02	8.67e-07	0.9147	156	13.6	14.4646	1.51e+01	7.46e-09	0.9661
37479 16,740 0.0211 1,197 14.0 3.3089 8.28e-02 4.23e-07 40453 15,999 0.0221 1,788 7.0 1.9539 3.81e-02 5.30e-07 58966 12,659 0.0279 1,012 11.0 3.8513 1.70e-01 3.96e-07 40092 11,264 0.0314 1,374 7.0 2.4473 4.67e-02 3.46e-07 44437 12,974 0.0272 1,645 6.0 2.1058 3.04e-02 6.78e-07 41449 8,189 0.0431 1,053 6.0 2.9663 4.25e-02 9.49e-07	40527	20,843	0.0169	1,569	12.0	2.2521	1.04e-01	1.52e-07	0.9778	,					•
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41449 8,189 0.0431 1,053 6.0 2.9563 4,25e-02 9,49e-07	44437	12,974	0.0272	1,645	0.9	2.1058	3.04e-02	6.78e-07	0.8959						1
	 41449	8,189	0.0431	1,053	0.9	2.9563	4.25e-02	9.49e-07	0.8433						1
87C 33861 19,091 0.0185 1,591 10.0 2.0856 4.97e-02 6.29e-07 0.9326	 33861	160'61	0.0185	1,591	10.0	2.0856	4.97e-02	6.29e-07	0.9326	,					٠
37752 4,306 0.0819 448 6.0 0.0715 3.88e—02 1.73e—06 0.8823 45 116.8 77.6959 5.1	 37752	4,306	0.0819	448	0.9	0.0715	3.83e-02	1.73e-06	0.8823	45	116.8	77.6959	5.15e+01	3.82e-08	0.9652

Table 1 (continued)

Accelerated deep slip is thought to have preceded a number of recent large subduction zone earthquakes, and repeating earthquake occurrence well documents both short-term and very long term precursory slip (Kato &

Nakagawa, 2014; Kato et al., 2012; Mavrommatis et al., 2015; Meng et al., 2015; Ruiz et al., 2014; Uchida et al., 2016). Accordingly, there is interest in monitoring deep plate motions worldwide for slip transients. The Parkfield section of the SAF is an ideal location to explore the use of LFEs as deep creepmeters for several reasons. First, LFE families in Parkfield extend beneath the probable nucleation zone of the last great San Andreas earthquake in Southern California, the 1857 M7.9 Fort Tejon earthquake (Sieh, 1978) (Figure 1). The proximity of LFEs to this hazardous earthquake source motivates using them for near real-time monitoring of fault slip. Additionally, there is evidence that the last M6 at Parkfield may have been preceded by accelerated deep slow slip (Shelly, 2009). Second, events in each LFE family in central California occur on average a few times per day which is advantageous because monitoring of the slip rate would be possible on daily or weekly basis and accelerated slip rates could be resolved on much shorter time scales. Third, the LFE catalog in Parkfield contains nearly one million earthquakes recorded since 2001. This amount of data allows for robust characterization of what "normal" behavior is, potentially allowing for detections of precursory transients that are abnormal.

Despite the simplicity of the idea and implementation of equation 2, in practice relating LFE rates to fault slip rate may not be so straightforward. LFE family cross-correlation detections are implemented using a forgiving correlation coefficient, typically as low as 0.16 (Shelly, 2017). How this loose definition of a family relates to a slip patch and whether family seismicity rates can be used without modification with the conceptual model in equation 2, remains to be seen. Additionally, equation 2 assumes that no aseismic slip occurs on the LFE patches whereas modeling studies have found that repeating earthquake asperities may accommodate a significant amount of aseismic slip (Chen & Lapusta, 2009). Finally, the seismicity rate, R, in equation 2 must be evaluated over some user defined time scale, and it is unclear which time scale is most appropriate.

Here we attempt to determine whether the occurrence of LFEs on the deep SAF provide a direct measure of the distribution of creep at depth and over what time scale. We do this by processing a catalog of 88 LFE families to determine average properties of periods of accelerated LFE occurrence and the SSEs they are through to reflect. Throughout the manuscript we use the terms SSE and creep episode interchangeably. Using the occurrence time and location of each LFE family, we estimate the average recurrence interval and duration of episodes. We then assume that equations 1 and 2 are valid and use the estimates of slip that can be derived from those assumptions to estimate additional properties such as the average total slip per episode, slip rate, fraction of interepisode LFEs, and relative episode moment. Finally, we explore the implications of these assumptions and determine whether they are physically realistic.

2 Methods

The data used in our analysis are the 88 LFE families identified by Shelly (2017). The catalog includes over one million earthquakes recorded since 2001; however, we limit our analysis to between 2006 and May of 2016 to minimize the effect of afterslip from the 2004 M6 Parkfield earthquake. LFE detections are identified by taking template waveforms recorded on many stations and channels and cross correlating them with continuous seismic data. The time series of cross correlations for each template are then summed over each station and channel to create a network cross-correlation time series. An LFE detection is registered when this network cross correlation exceeds a given threshold. Many studies use 8 times the median absolute deviation; however, Shelly (2017) instead required that the average cross correlation across all channels was 0.16 or greater and that the summed cross-correlations values exceeded 4.0. So defined, an LFE family represents events with similar waveforms, ensuring that they have similar mechanisms and similar source locations. However, it is uncertain whether these events are exact repeats of the same source at the same spot on the fault as nearby, as distinct sources can generate waveforms similar enough to meet the LFE detection criterion. Additionally, estimated LFE source dimensions of hundreds of meters (e.g., Bostock et al., 2015; Thomas et al., 2016) are typically less than LFE location uncertainties of 1-2 km (Shelly, 2017). Because of these uncertainties we apply equation 2 to slip episodes or periods in time when LFEs within a given family occur in rapid succession, as opposed to individual LFEs.

To define duration of slip episodes on the deep SAF, we take the distribution of recurrence intervals T_r , or the time between an LFE and its previous occurrence, for each individual LFE family and plot the logarithm of T_c as a function of time (see Figures 3a and 4a). For all LFE families, there is a clear separation into two or sometimes three populations of interevent times. To determine the time scale that separates populations, we first plot the smoothed histogram of the logarithm of recurrence intervals (for step sizes of 0.1 and a bin of width of 0.6, measured in log (days)). These histograms are shown in Figures 3b and 4b and have clear peaks corresponding to the different event populations. We then find the local minima in this distribution while requiring a minimum separation distance of 1 order of magnitude between successive minima. While these values are arbitrary, we find that they result in time scales that are consistent with identifying populations by eye. An example of continuous family 5 with two populations is shown in Figure 3a. We use the time scale corresponding to the minimum LFE frequency (vertical red line in Figure 3b) to assign each LFE to a population. In this case, and in most continuous families, the long recurrence interval population is interpreted to represent the first event in each episode, while the short recurrence interval populations are thought to represent LFEs that occur as part of an ongoing episode. This interpretation is consistent with observations of clustering behavior of LFEs in time. For example, Figure 3c shows the cumulative number of LFEs in family 5 versus time for a 1 week

period in 2012 with the LFE symbol corresponding to its population. Family 5 has episodes that tend to occur frequently (i.e., approximately every 3 days, see Table 1), and each episode begins with an event in the long population and often has several short events that follow. In episodic families, such as family 55, there are three populations (Figures 4a and 4b). The episode shown in Figure 4c initiates with a long event, in this case any LFE with recurrence interval greater than 1.5 days, and includes multiple groups of LFEs consisting of an intermediate followed by multiple short events. Like the continuous families, the long populations represent LFEs that initiate episodes while the short LFEs occur as part of an ongoing episode. The intermediate population reflects LFEs that initiate short-duration episodes, or "bursts," that occur within longer duration episodes. These bursts are reminiscent of the secondary slip fronts that have been observed in Cascadia and Japan (Houston et al., 2011; Obara et al., 2012).

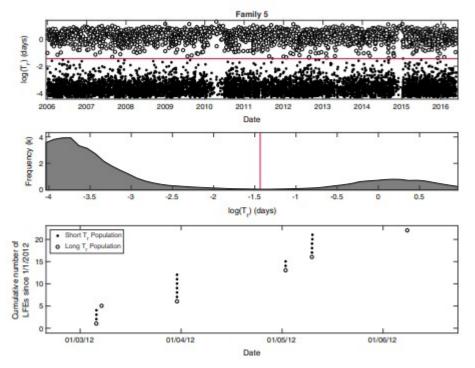


Figure 3

(a) Date versus $\log(T_r)$ for continuous family 5. Red horizontal lines mark boundaries between recurrence interval populations. (b) Smoothed histogram of $\log(T_r)$. Local minima are marked by vertical red lines. The $\log(T_r)$ values are used to separate each individual LFE in family 5 into populations of events with similar preceding recurrence intervals. (c) Cumulative number of events versus time plot for family 5 for 4 days in 2012. Each individual LFE occurrence is indicated by the symbol corresponding to the long and short $\log(T_r)$ populations. Note that family 5 has episodes lasting 2.75 min every 2.49 days (though there are a total of six episodes in the 6 week period shown). The inset in Figure 3c shows the definition of duration for a given episode.

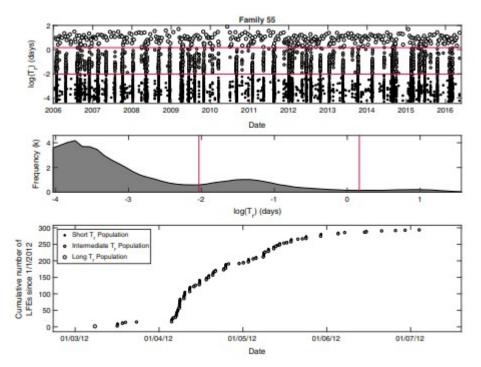


Figure 4

(a) Date versus $\log(T_r)$ for episodic family 55. Red horizontal lines mark boundaries between recurrence interval populations. (b) Smoothed histogram of $\log(T_r)$. Local minima are marked by vertical red lines. The $\log(T_r)$ values are used to separate each individual LFE in family 55 into populations of events with similar recurrence intervals. (c) Cumulative number of events versus time plot for family 55 for 5 days in 2012. Each individual LFE occurrence is indicated by the symbol corresponding to the long, intermediate, and short $\log(T_r)$ populations. Family 55 has an individual episodes that last 42 h every 13 days.

We define an episode as two or more successive recurrence intervals (a minimum of three LFEs) shorter than the time scale separating the $\log(T_r)$ populations. Because the episodic families have two relevant time scales, for each episodic family we explore the implications of defining episodes based on both the short and long recurrence interval time scales. In the remainder of the manuscript, each episodic family is represented twice: once for episodes defined using the short time scale (short time scale episodic families) and once for episodes defined using the long time scale (long time scale episodic families). Using this definition of episodes, we can also define individual slip episodes for each family and estimate their duration, t_d , as the time between the occurrence of the first and last LFE that takes part in the episode. The episode recurrence interval, t_r , is defined as the time between successive episode start times. For the episodic families with episodes defined using the long time scale, we consider only episodes that have durations greater than the short time scale (which ensures that they contain multiple bursts) when calculating the recurrence interval and duration. Similarly, since our analysis of the episodic families using the short

recurrence interval time scale is meant to better understand properties of bursts that occur as part of inferred creep episodes, we require that the burst recurrence interval be shorter than the long time scale when calculating the recurrence interval and duration. We also calculate a parameter, χ , which we define as the fraction of LFEs in each family that occur during episodes. We estimate the total slip per LFE, $d_{\rm LFE}$, by taking long-term slip rate of 34 mm/yr (Ryder & Bürgmann, 2008), multiplying by the catalog duration to determine a total slip and dividing by the total number of LFEs in that family, N. When $d_{\rm LFE}$ is combined with the number of LFEs per episode, this yields an estimate of the slip per episode, $d_{\rm e}$, and we also calculate the interepisode slip $d_{\rm ie}$. These calculations assume catalog completeness, that each LFE detection is an exact repeat and ruptures the same fault area and that all slip on that fault area is accommodated seismically. Finally, dividing the slip per episode by the episode duration results in an estimate of the episode slip velocity, V.

3 Results

The results of the procedure described above are summarized in Table 1.

3.1 Inferring Slow Slip Velocities

Assuming no interepisode slip (no appreciable LFE occurrence between episodes), one implication of equation 2 is that at constant loading rate, V_L , perfectly periodic slip should result in the ratio of episode recurrence to episode duration being proportional to the normalized episode slip velocity

$$t_r = t_d(V/V_L)$$
.(3)

Equation 3 has the advantage of having a clear time scale, t_r , over which the slip rate ratio V/V_L is evaluated. Figure 5 shows the median values of episode duration and recurrence interval for the 88 families color coded by their MFD75. There are three populations made up of the short time scale episodic families (lower left group), short time scale continuous families (lower right group), and the long time scale episodic families (upper right). When the episodic families are evaluated on the long time scales, most episodes have days-long durations and tens-of-days long recurrence intervals (top right group) while continuous families typically have recurrence intervals of days and durations of minutes. When the episodic families are evaluated on short time scales, they have durations that are similar to the continuous families but recurrence intervals that are approximately an order of magnitude shorter. These bursts of events occur multiple times as part of longer duration creep events as shown in Figure 4c. The episodes of continuous families and episodic families with episodes defined using the short time scale show no trend in duration versus recurrence interval. The mean ratio of t_r to t_d for this group of families implies V/V_L is of order 10² and 10³. Assuming V_L or a long-term deep slip rate of 34 mm/yr (Ryder & Bürgmann, 2008), this result implies a slip rate of 10^{-7} to 10^{-6} m/s during slip episodes for the continuous families. Finally, the longer duration episodes of the episodic

families show a systematic relationship with duration increasing with recurrence interval. Superimposed on Figure 5 is a zero-intercept line of slope 0.063, suggesting that the slip rate during episodes for episodic families is about 16 times the plate rate, or of order 10^{-8} m/s.

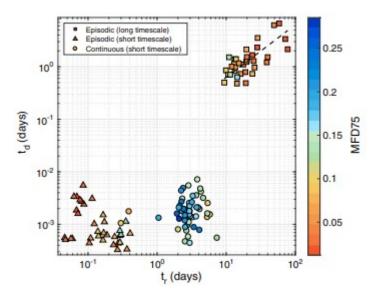


Figure 5

Median duration, t_d , versus recurrence interval t_r of slip episodes in the 88 LFE families color coded by their MFD75 value (high values correspond to continuous families, while low values correspond to episodic families). The squares and triangles represent episodes defined by the long and short time scales (shown in Figure 4), while circles represent continuous families. Events separate into three populations. The continuous and short time scale episodic families show no systematic trend, while episodic families with episodes defined by the long t_r time scale have t_d that increases as a function of t_r . The dashed line is the best fit to this group of families and has a slope of 0.063 corresponding to $V/V_r \approx 16$.

The slip estimates above are attractive in that they do not depend on an estimate of the slip per LFE (d_{LFE}). Figure 6 instead shows episode slip and slip rate determined using the average slip per LFE. Figure 6 suggests that while total slip increases as a function of episode duration, the slip rate in continuous and the short time scale episodic families is 2 orders of magnitude faster than the slip rate in the long time scale episodic families. Additionally, the specific slip velocities inferred using slip per LFE are largely consistent with those determined using equation 3.

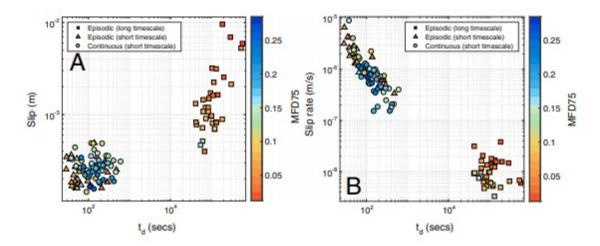


Figure 6

(a) The median duration, t_d , versus median slip per episode determined using the slip per LFE and LFEs per episode. (b) Median duration versus slip velocity measured over the duration of the episode.

3.2 Interepisode Creep

Equation 3 assumes that there is no slip between episodes. Whether this assumption is valid can be determined by using the fraction of intraepisode LFEs, χ , described above, which is the ratio of the number of LFEs that occur during episodes to the total number. This definition assumes that events that do not take place within episodes are representative of the total amount of interepisode slip, $1 - \chi$. χ reaches its maximum value, one, if there is no interepisode slip. γ provides a context for defining and perhaps understanding the differences between the continuous and episodic families. Figure 7 shows that the continuous and short time scale episodic families have similarly short durations and χ values that vary substantially whereas episodic families have large χ values and relatively long durations. χ exceeds 0.9 for all the episodic families; hence, they are well coupled between episodes whereas χ values for the short time scale episodic and continuous families range between near 0.5 and 1 and as a whole are not consistent with equation 3. This variable fraction of interepisode LFEs may explain why the long time scale episodic families have a clear increase in duration with recurrence interval, as shown in Figure 5, and are generally consistent with equation 3, while the continuous and short time scale episodic families show no such trend.

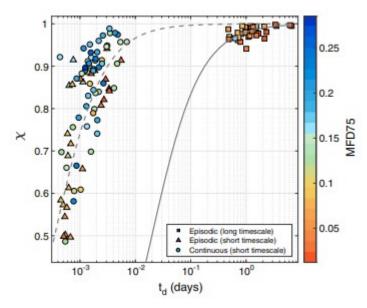


Figure 7

Median duration, t_a , versus χ of slip episodes in the 88 LFE families color coded by their MFD75 value. Once again LFE families separate into two populations. Episodic families generally have χ values near one and have long-duration episodes (around 1 day), whereas the continuous and short time scale families have strongly variable coupling that tends to increase as a function of episode duration. The dashed and solid lines are fits of equation 9 to all families and the episodic families alone.

Figures 8a and 8b show the median slip per episode and median interepisode slip as a function of χ for the continuous, short and long time scale episodic families. Similar to Figure 5, long time scale episodic families with large χ values have much larger slip per episode (and longer durations). In the continuous and short time scale episodic families, the per episode slip is lower, independent of χ , and does not overlap with the episodic families. In contrast, the average interepisode slip is similar for both episodic and continuous families (Figure 8) despite the variability in χ . The contrast in behavior, total slip, and duration suggests that the episodic and continuous families reflect mechanically different phenomena whereby the episodic families reflect periodic creep events, while continuous families may be driven by relatively continuous creep on surrounding fault. We further explore this idea in section 4.

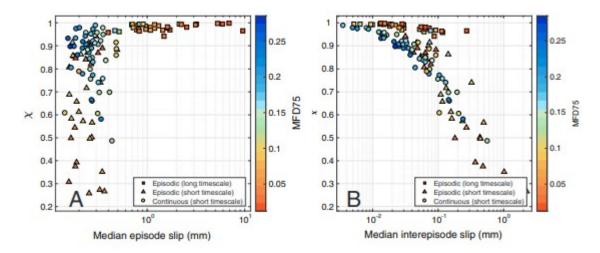


Figure 8 (a) χ versus median slip per episode. (b) χ versus median slip between episodes.

3.3 Moment-Duration Scaling of Inferred Creep Events

Seismic moment is defined as

$$M_0 = \mu A d$$
, (4)

where μ is the rigidity, A is the area of fault slip, and d is the average slip. Ide et al. (2007) suggested that all slow earthquake phenomena (i.e., SSEs, NVT, and LFEs) obey linear moment-duration scaling. In contrast, traditional earthquakes have moment that scales with the cube of duration Kanamori and Anderson (1975). More recent studies have suggested that smallermoment SSEs may scale more like regular earthquakes because they are not geometrically confined (Gomberg et al., 2016). Because the creep episodes we identify are likely smaller than those constrained geodetically or from tremor zone dimensions in other environments, knowing their momentduration scaling may inform the proposed scaling relationships. However, determining the moment of our inferred SSEs in Parkfield is challenging for a couple of reasons. First, while there is strong observational evidence for the occurrence of SSEs in Parkfield (Guilhem & Nadeau, 2012; Shelly, 2015), these SSEs are too small for individual events to be detectable with surface geodetic monitoring equipment (Smith & Gomberg, 2009). Delbridge (2015) showed that SSEs in Parkfield can be observed in strain meter records by stacking over multiple slip events; however, this does not allow for estimation of moments of individual SSEs. Second, knowing the slip alone does not allow for an estimate of the total moment; additional information is needed to estimate the area.

We estimate the relative difference in moment for these slip events in two different ways. We first assume constant rupture velocity, V_r , for all creep events identified using a given LFE family. Using this definition, the fault dimension $L = \sqrt{A} = t_d V_r$ and the relative moment is

$$\frac{M_o}{M^*} = \frac{d_e}{d_e^*} \left(\frac{t_d V_r}{t_d^* V_r^*} \right)^2,$$
 (5)

where the asterisks denote values for an arbitrarily chosen reference event. Alternatively, many slow earthquake phenomena are characterized by low stress drops of order 10 kPa (Bartlow et al., 2014; Bletery et al., 2017; Bostock et al., 2015; Brodsky & Mori, 2007; Hawthorne et al., 2016; Ide et al., 2007; Ito & Obara, 2006; Schmidt & Gao, 2010; Thomas et al., 2016). The stress drop is defined as the difference in stress before and after a slip event and is proportional to the displacement divided by the dimension of the slipping region or

$$\Delta \sigma = \alpha \mu \frac{d}{L} = \alpha \mu \frac{d}{\sqrt{A}}.$$
 (6)

If instead of taking $L=t_dV_r$ we assume that the Parkfield SSEs have similar stress drops and employ $L=\alpha\mu d/\Delta\sigma$ the relative moment is

$$\frac{M_o}{M^*} = \left(\frac{d_e}{d_e^*}\right)^3. \tag{7}$$

Figures 9a and 9b document the scaling that results from making these two assumptions. Figure 9a shows the moment-duration scaling assuming constant rupture velocity (equation 5), while Figure 9b shows the scaling resulting from assuming constant stress drop (equation 7). The best fit line (dashed) in Figure 9a has a slope of 0.44, close to the proposed 0.33 for regular earthquakes, while the fit to the moment-duration scaling shown in Figure 9b has a slope of 1.02, close to linear moment-duration scaling proposed by Ide et al. (2007).

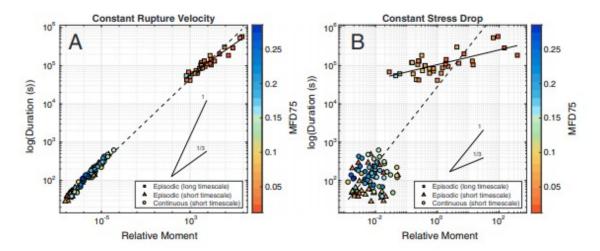


Figure 9

(a) The moment-duration scaling assuming constant rupture velocity (equation 5. (b) The moment-duration scaling resulting from assuming constant stress drop (equation 7). The best fit line to all families (dashed) in Figure 9a has a slope of 0.44, close to the proposed 0.33 for regular earthquakes, while the fit to the moment-duration scaling shown in Figure 9b has a slope of 1.02, close to linear

moment-duration scaling proposed by Ide et al. (2007). Fitting the episodic families only results moment-duration scaling of 0.32 and 0.19 for Figures 9a and 9b, respectively. Solid lines show slopes of 1/3 and 1 for reference.

4 Discussion

4.1 Velocity Estimates for Creep Events

SSEs around the world are observed to slip at speeds that are 1-2 orders of magnitude above the plate velocity. The near-constant slope of the episodic families evaluated on long time scales shown in Figure 5 suggests that equation 3 is valid and that these episodes represent creep events that slip ≈16 times faster than the long-term slip rate. The data shown in Figures 5 and 6 suggest that the episodic families are a passive indicator of large-scale aseismic slip on the surrounding creep patches that fail periodically in SSEs and hence can be used as creepmeters on the time scale of t_r (i.e., they are consistent with equation 3. The areas surrounding the LFE patches accommodate nearly 100% of their slip (as evidenced by large x values in the long time scale episodic families) during few-day-long SSEs that recur several times each year and come to a halt in the inter-SSE period. Equation 3 is attractive in that in the absence of aseismic creep on the LFE patch, both the duration and the recurrence interval are properties of the Parkfield creep events that can be measured with confidence and hence the ratio of the slip velocity during creep events to the plate rate can be measured without relying on more speculative estimates of slip per LFE. Despite this uncertainty, the slip rates for the long-duration episodic families shown in Figure 6 are surprisingly consistent with those derived from equation 3 supporting the idea that these families do reflect surrounding creep.

The lack of a clear trend in t_r versus t_d in Figure 5 for the continuous and episodic families evaluated on short time scales suggests that equation 3 is not applicable. Since equation 3 employs estimates of both the duration, t_d , and recurrence interval, t_r , of inferred creep events, the lack of a clear t_r versus t_d trend suggests that either t_r or t_d is not representative. From Figure 6 the inference of lower slip rates during larger creep events is surprising in that the continuous families have shorter recurrence intervals, as in the presence of a constant stressing rate they should have less strain energy available to accelerate slip. Hence, these families should slip at lower average speeds than the less frequent episodic events. One way to have spurious slip velocities for these families is to have durations that are not meaningful; that is, they are not representative of the duration of surrounding creep episodes. Our preferred interpretation of these results is that continuous and short time scale episodic families likely are persistent asperities driven to failure by essentially continuous surrounding fault slip, similar to shallow repeating earthquakes, and do not reflect surrounding creep when evaluated over the time scale of a single recurrence interval. While this suggests, at least initially, that these families are not appropriate for use as a creepmeter, this result is a direct consequence of the time scale on which they are evaluated. When evaluated on time scales shorter than

the burst recurrence time, t_r , there is no information on slip or slip rate and hence equation 3 is not applicable. Further support for this idea comes from the episodic families evaluated on short time scales shown in Figures 5 and 6 which, like the continuous families, show no trend in t_r versus t_d and have similar inferred slip rates. This suggests that for equation 3 to be applicable requires that they be evaluated on time scales that are longer than the fundamental interevent time. When evaluated on shorter time scales (as in the case of the short time scale episodic families), equation 3 yields unrealistic results.

Despite their inconsistency with equation 3, the continuous and short time scale episodic families are likely still useful creepmeters when their rates are evaluated on time scales much longer than a typical episode recurrence interval. To determine if this is true, we estimate the slip rate during the long time scale creep episodes by applying equation 2 to the short time scale episodic families over the median duration of a long time scale episode. Note that these two methods of estimating slip rate are independent, as the duration or recurrence interval of a long time scale episode need not correspond to the number of short time scale bursts it contains. If these families are useful creepmeters then we would expect the slip rates derived using equation 2 to be similar to those estimated by dividing the recurrence interval by the duration of the long time scale episodic families (i.e., equation 3 and Figure 5). We find that this is indeed the case, there is a very close correspondence between slip rates estimated using equations 2 and 3. While equation 3 yielded slip rate estimates of $V/V_L \approx 16$ for long time scale episodic families, equation 2 gives $V/V_{\perp} \approx 21$. Additionally, slip rates for the same family differ by 37% on average and by no more than a factor of 2.6 for any family. This result suggests that both continuous and short time scale episodic families can be used to monitor deep fault slip for transient increases that may precede large earthquakes; however, equation 2 must be evaluated over the appropriate time scale. For any recurring failure process, the assumption that time can be used as proxy for slip will break down at time scales shorter than the fundamental interevent time of the failure process. Because LFEs within a given family may not truly be repeating events (Bostock et al., 2015; Chestler & Creager, 2017) and may not necessarily reflect surrounding fault slip, the interevent time scale is the time between bursts in the short time scale episodic families as opposed to the time between individual LFEs. The time scale between episodes in continuous families appears to have the same physical significance. Accordingly, if the 88 LFE families in Parkfield were to be used as deep creepmeters the time scale to evaluate equation 2 over would be several short time scale recurrence intervals (listed in Table 1).

There are a few additional observations that are worthy of discussion. First, while the continuous families generally have fewer LFEs per episode than episodic families (see Table 1), they still have multiple LFEs per episode (typically 3–8 LFEs). This could occur because the size of the persistent

region is larger than an individual LFE asperity or because the slip accommodated when a continuous family experiences failure is larger than the maximum amount of slip any given LFE can accommodate (note that LFEs in Cascadia appear to have a maximum moment which they cannot exceed; see Bostock et al., 2015). Second, the continuous families have a larger fraction of interepisode LFEs than the episodic families many of which occur in isolation. These LFEs may be instances in which surrounding stress levels are too low to cause failure of the entire slip patch or in some cases they may represent false detections. Third, continuous and episodic families may be mechanically distinct; however, another possibility is that there simply are not regular slip transients in the locations of the continuous families. This idea is supported by the observations of Shelly (2017) that some families can switch between episodic and continuous deformation styles, suggesting that SSEs only sometimes reach their location. Fourth, if episodic families do meter creep that is approximately an order of magnitude faster than the long-term slip rate this provides a natural explanation for the recurrence intervals of the episodic families evaluated on short time scales being approximately an order of magnitude less than the continuous families as faster surrounding creep rates should produce correspondingly shorter recurrence intervals. Finally, previous studies have used analyses similar to that presented here to explore the spatial extent of interactions among families (Shelly, 2015; Trugman et al., 2015; Wu et al., 2015). In these studies, the continuous families do have occurrence patterns that are correlated over tens of kilometers which has been interpreted as long-range interaction among families (greater than 10 km in many cases). This observation appears to be inconsistent with our mechanical interpretation of the continuous families. Two possible explanations for this observation that still allow our hypothesis to hold are that LFEs in continuous families play an active role in propagating underlying creep fronts through a cascade-like failure process (as proposed by Shelly, 2015) or that the background driving stress, which includes contributions from long wavelength processes such as tectonics, tides, and hydrologic loads, pushes many families to failure nearly simultaneously manifesting as correlated failure of asperities separated by large distances.

4.2 Creep Events and Interepisode Slip

To better understand the observations in Figure 7, which shows χ , the fraction of intraepisode LFEs, as a function of episode duration t_d , we consider the hybrid stick- and creep-slip model of repeating earthquakes developed by Beeler et al. (2001). The model considers a fault patch of dimension L representing a region that undergoes episodic slip (i.e., earthquakes) and has material properties that are distinct from the fault patch surroundings. Slip on the surrounding fault drives slip on the patch; however, the patch is allowed to slip aseismically during the interseismic period as well as seismically while hosting repeating earthquakes. While Beeler et al. (2001) originally developed the model to study the moment-

recurrence interval behavior of shallow repeating earthquakes on the SAF, slight modification of the initial assumptions allows for application to the deep creep events studied here. Throughout this manuscript we have assumed that slip is completely metered by LFE occurrence, meaning we assume that aseismic slip on the LFE asperity is negligible; hence, direct application of the Beeler et al. (2001) model is inappropriate. However, replacing seismic and aseismic slip in the case of repeating earthquakes with intraepisode and interepisode slip makes the model appropriate for application to deep creep events we study here. The modified model derivation is shown in Appendix A and results in a relationship between χ , a strain hardening parameter, C, and the stiffness, k, of the fault patch hosting the creep event

$$\chi = \frac{d_e}{d_{\text{total}}} = \frac{1}{1 + k/C}.$$
 (8)

Equation 8 has a functional form that is consistent with the observations shown in Figure 7 provided that the ratio k/C approaches one for the short-duration continuous families and goes to zero at durations associated with the long-duration episodic families. While equation 8 is expressed in terms of physical parameters in the model, a quick sanity check shows that it can be derived directly from the expression for the total slip budget (i.e., $d_{ie}+d_e=d_{total}$) as

$$\chi = \frac{1}{1 + \frac{d_{ie}}{d_e}} = \frac{1}{1 + \frac{d_{ie}}{V_e t_d}}$$
 (9)

Assuming $d_{\rm ie}/V_e$ is constant allows equation 9 to be fit directly to the observations shown in Figure 7. This fit is shown as a dashed line in Figure 7. We obtain a median value of $3.48*10^{-4}$ days for $d_{\rm ie}/V_e$ and the fit captures some of the functional form of the observations. However, our calculated values of $d_{\rm ie}/V_e$ vary substantially with differences that exceed an order of magnitude between the episodic and continuous families. Additionally, as discussed in section 4.1, the velocity estimates for the continuous and short time scale episodic families are likely overestimated. Refitting equation 9 to the episodic families alone results in a value of $d_{\rm ie}/V_e$ that is 0.020 days. This value is in good agreement with the median measured value of $d_{\rm ie}/V_e$ of 0.039 days for the episodic families.

An alternative interpretation of the data shown in Figure 7 can be gleaned from using the functional form in equation 8 but by employing the definition of stiffness, k = G/L, where G is the rigidity of the surrounding rock and L is the SSE patch length.

$$\chi = \frac{1}{1 + \frac{G}{LC}}.$$
 (10)

In the context of this version of the Beeler et al. (2001) model, the variation in χ can be interpreted as being due to variations in the size of the slip events with families with smaller χ values having correspondingly smaller length scales and likely moments. The differences in inferred slip between long time scale episodic and continuous families further support this interpretation, as do numerical models of aseismic slip in repeating earthquakes (Chen & Lapusta, 2009). Laboratory studies of strain hardening in saturated fault gouge suggest that the strain hardening parameter C has an approximately linear pressure dependence (Morrow et al., 1982). Figure 10 shows measured values of C as a function of confining stress from Morrow et al. (1982). These data were originally collected in a triaxial press on samples with a saw cut fault inclined at 30° and have been converted from axial displacement to fault displacement for our purposes. Figure 10 shows that for the most extensively studied gouge from the Tejon Pass drilling project C lies in the range of 2 to 10 GPa/m for confining stresses between 50 and 200 MPa, which correspond to lithostatic pressures at shallow to midcrustal depths (Morrow et al., 1982). There is only a single measurement for Montmorillonite, and it implies a much weaker pressure dependence of the strain hardening parameter of 0.005 GPa/MPa-m. The Tejon Pass gouge is the strongest and most strongly strain hardening material in Morrow et al. (1982) and has a pressure dependence of 0.047 GPa/MPa-m. Pore fluid pressures in the LFE source region on the deep San Andreas Fault are thought to be near lithostatic (Beeler et al., 2018, 2013; Thomas et al., 2012). Using an effective normal stress of 1 MPa results in C = 0.047 GPa/m. Using equation 10, $\chi = 0.98$, the median χ value for the episodic families, and taking the shear modulus in the source region to be 30 GPa results in a creep patch dimension of ≈30 km, consistent with the estimates of Shelly (2015) and Trugman et al. (2015) deduced from the spatiotemporally coherent occurrence of the LFE families.

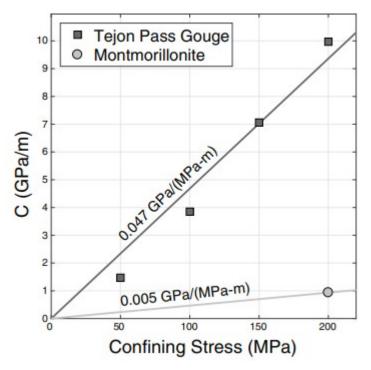


Figure 10

The strain hardening parameter C of saturated Tejon Pass fault gouge measured at between 50 and 200 MPa confining stress are shown as black squares, while C for Montmorillonite is shown in gray from Morrow et al. (1982). C is the rate of strengthening with fault slip measured in GPa/m. The regressions (black and gray lines) are constrained to go through zero and gives the pressure dependence of C. Since C is in GPa/m and confining stress is in MPa, the pressure dependence is measured in GPa/(MPa-m).

4.3 Moment-Duration Scaling of Creep Events

While it is fairly well accepted that large (i.e., M6 and above) SSEs are characterized by linear moment-duration scaling (Gao et al., 2012), whether smaller magnitude slow earthquakes or related phenomena (such as LFEs and VLFEs) have moment proportional to duration is unclear. Recently, Bostock et al. (2015) measured moments and durations of LFEs in Southern Vancouver Island and found that moment was proportional to duration to the tenth power reflecting the constant duration nature of LFEs. However, Bletery et al. (2017) estimate slip, area, and duration of secondary slip fronts in Cascadia, which are smaller-moment slip fronts that occur after the main slow slip front has passed, to show that such events obey linear momentduration scaling, similar to large magnitude SSEs. Gomberg et al. (2016) suggested that large SSEs might follow the Scholz (1982) W model and obey linear moment-duration scaling because they fall in a region of bounded growth, in which the geometry of the slipping region can only grow in one dimension. Those authors used observations of creep events in Cascadia that had smaller spatial extents than the inferred transition zone width to argue that smaller-moment creep events have scaling consistent with unbounded growth (i.e., moment proportional to the cube of duration). Our inferred

creep events may also have spatial extents that are equal to or less than the extent of the transition zone in Parkfield (Shelly, 2015); hence, estimates of moment and duration can inform the debate over how the moment of small magnitude creep events scale with duration.

Estimating the spatial extent of individual SSEs in Parkfield is challenging because individual SSEs are not geodetically detectable and LFE family locations are sparse (88 families spanning over 100 km along fault and 14 km in depth). As such, employing common (though not necessarily correct) assumptions, such as constant rupture velocity or constant stress drop, allows for estimates of relative SSE moments which may provide a useful constraint on the scaling. Because the frequent short-term bursts of the continuous families may not represent individual creep events, as proposed above, we consider only the moment duration trends of the episodic families alone. When we estimate relative moment assuming constant rupture velocity, the episodic families alone have a trend of 0.32 which is close to 0.33, implying that creep events on the SAF have moment-duration scaling similar to regular earthquakes. Assuming a constant stress drop results in a scaling of 0.19, inconsistent with either of the previously proposed scalings. Finally, the creep-slip model of Beeler et al. (2001) shown in equation 10 combined with laboratory estimates of the strain hardening parameter C provide another means for estimating the length scale of creep events. We determine length scales of creep events by taking the χ values shown in Table 1, C = 0.047 GPa/m (assuming an effective stress of 1 MPa), and $\mu =$ 30 GPa. Doing this results in the moment-duration scaling shown in Figure 11 that yields inferred scalings 0.22 episodic families and 0.24 for continuous and short time scale episodic families, respectively. One issue with using the Beeler et al. (2001) model to estimate spatial scale is that having χ values that approach one requires $K \ll C$. Very small stiffnesses can result in inferred length scales that are unrealistically large. For example, for the C value we adopted the largest family, which has $\chi > 0.99$ and has an inferred length scale of ≈300 km. This problem could be alleviated by choosing a different value of C for the episodic and continuous families. Thomas et al. (2012) found that more episodic families located at shallower depths are generally less correlated with small magnitude tidal shear stress fluctuations than deeper, more continuous families. They suggested that these variations in sensitivity to tidal stresses result from variations in effective stress and frictional properties. If such variations do reflect variations in pore fluid pressure then the episodic families may operate at larger effective stresses than the continuous families which justifies adopting different values of C for the episodic and continuous families. Increasing C by a factor of 5 for the episodic families (which corresponds to an effective stress of 5 MPa) results in maximum length scales on the order of tens of kilometers, which is consistent with the spatial extents inferred from other studies (Shelly, 2015; Trugman et al., 2015; Wu et al., 2015).

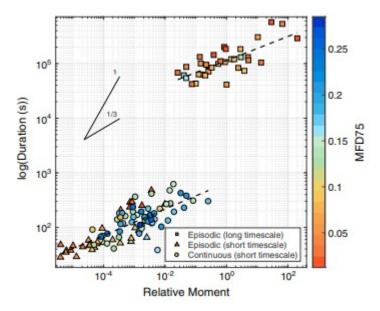


Figure 11 Moment-duration scaling determined using a length scaled derived from the model of Beeler et al. (2001). The slope for the continuous and short time scale episodic families is 0.24. The slope for the episodic families is 0.22. Solid lines show slopes of 1/3 and 1 for reference.

In summary, moments of SSEs in Parkfield are challenging to estimate due to the lack of knowledge of their spatial extents. The spatial extent of creep events in Parkfield are difficult to constrain reliably due to the sparseness of LFE locations. We instead determine relative moment, which can constrain the moment-duration scaling of SSEs in Parkfield, by employing our measurements of slip and duration (see equations 5 and 7). We estimate moment-duration scaling in three different ways: assuming constant rupture velocity, assuming constant stress drop, and employing the model of Beeler et al. (2001) to get spatial extents which we combine with our estimates of slip. None of these methods yields linear moment-duration scaling. While it is encouraging to find consistent results using different techniques to estimate the spatial extents of creep events in Parkfield, extreme caution should be exercised when attempting to determine scaling with incomplete knowledge of spatial scale.

5 Conclusions

Our analysis of creep events on the deep SAF yields the following results:

1. We find that the distribution of the logarithm of recurrence intervals of LFEs within a given family are either bimodal or trimodal. We call families with a bimodal distribution continuous while those with a trimodal distribution are episodic. We use the time scales between populations to identify episodes. In continuous families, the short and long recurrence interval populations represent LFEs that occur within episodes and LFEs that initiate episodes, respectively. Episodes in continuous families recur every few days. In the episodic families, the long recurrence interval

populations are events that initiate episodes, the intermediate recurrence intervals are events that initiate bursts of events that occur within episodes, and the short recurrence intervals represent LFEs that occur within bursts of events. Episodic families recur on time scales of tens of days.

- 2. We formalized the definition of a creepmeter (i.e., equation 2 and determined its applicability to LFE families on the deep SAF). Because equation 2 has no inherent time scale, we recast it as equation 3 which suggests that the ratio of the recurrence interval to the duration can be used to estimate slip speeds during SSEs, which appear to be ≈ 16 times the long-term plate slip rate in Parkfield. We find that continuous families and the short time scale episodic families are inconsistent with equation 3. However, when the short time scale episodic families are evaluated using 2 on time scales longer than the interevent time t_r they can be used to determine meaningful slip rate estimates. Given the many similarities between the continuous and short time scale episodic families, this result likely extends to the continuous families as well.
- 3. A straightforward interpretation of episodic families is that they define sections of the fault where slip is distinctly episodic in well-defined SSEs. In contrast, the frequent short-term bursts of the continuous and short time scale episodic families likely do not represent individual creep events but rather are persistent asperities that are driven to failure by quasicontinuous slip on the surrounding fault.
- 4. A slightly modified version of the hybrid stick and creep-slip model of Beeler et al. (2001) provides a framework to interpret the observation that different families have variable coupling. The functional form of the model also suggests that the episodic families reflect episodic creep events with correspondingly larger moment, slip, duration, and, likely, scale.
- 5. We estimated moment-duration scaling of creep events assuming constant stress drop and constant rupture velocity and also estimated the spatial extent of the SSEs from the Beeler et al. (2001) model. All of the resulting moment-duration scalings are inconsistent with the proposed linear moment-duration scaling. However, caution must be exercised when attempting to determine scaling with incomplete knowledge of scale.

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Appendix A: Derivation of Hybrid Stick- and Creep-Slip Model for Deep Creep Events

Beeler et al. (2001) derived a hybrid stick- and creep-slip model to study moment-recurrence interval relationships of shallow repeating earthquakes on the San Andreas Fault. Their model considers a fault patch of dimension L representing a region that undergoes episodic slip and has material properties that are distinct from the fault patch surroundings. Slip on the surrounding fault drives slip on the patch. Stress on the patch is assumed to be uniform implying that it can be well characterized by a spatial average. To account for the total slip budget, the Beeler et al. (2001) model considers both seismic slip, d_{seis} , that occurs during repeating earthquakes, and aseismic slip, d_{aseis} , that occurs between repeating earthquakes such that $d_{\text{seis}}+d_{\text{aseis}}=d_{\text{total}}$. To modify their original model, we replace d_{seis} with the slip that occurs within episodes, d_e , and d_{aseis} with the slip that occur between episodes, d_{ie} , such that sum of the interepisode and intraepisode slip is the total slip, $d_{ie}+d_e=d_{total}$. Otherwise, the derivation follows that of Beeler et al. (2001). During the interseismic period the patch is loaded by elastic stress transfer from the surroundings and the shear stress on the patch, τ , can be represented by

$$\tau = k (d_L - d_{ie}) = k (d_0 + V_L t - d_{ie}) . (A1)$$

where t is time, and d_L , d_{L0} , and V_L are the displacement, the initial displacement, and the slip (or loading) velocity of the surroundings, respectively. Here k is the stiffness k = G/L, where G is the shear modulus, or equivalently the unloading stiffness, $k = \Delta \tau_s/d_e$, where $\Delta \tau_s$ is the static stress drop due to slip during an episode, d_e . The model considers a fault strength relation for the patch that allows for interseismic slip because in some families LFEs do not always occur as part of episodes, implying nonzero d_{ie} . One relationship that satisfies this requirement is to allow patch strength prior to failure to be strain hardening, or an increasing function of the interepisode fault slip (e.g., Morrow et al., 1982). For simplicity we, like Beeler et al. (2001), assume this relationship is linear

$$\tau_{\text{strength}} = \tau_0 + Cd_{\text{ie}}, (A2)$$

where C is a slip hardening coefficient and τ_0 is the strength at the onset of loading. C is intended to represent a ductile component to the region of interest and allows strain to accumulate without loss of strength. Because LFEs are thought to occur at the base of the crust, below the nominal depth of the brittle-ductile transition in California, it is appropriate to employ a model that allows for both brittle and ductile creep behaviors.

Equating A1 with A2 and noting that $\tau_0=kd_0$ results in an equation for the interseismic slip

$$d_{\rm ie} = \frac{kV_L t}{C + k}.$$
 (A3)

If the loading rate is constant, the slip rate of the patch is constant during the interepisode time:

$$V_{\rm ie} = \frac{kV_L}{C+k}.$$
 (A4)

When τ reaches a threshold strength τ_f , a slip episode occurs and stress drops over some duration, t_d , to τ_0 . The static stress drop is then $\Delta \tau_s = \tau_f - \tau_0$. Combining this definition of stress drop with equation A2 results in $\Delta \tau_s = Cd_{ie}$. Equation A3 can be adapted to apply to a single interepisode time period by replacing the total interepisode slip d_{ie} with the interepisode slip of a single earthquake cycle d_{ie} and total time t with the recurrence interval, t_r . Then the episode recurrence interval can be written as

$$t_r = \frac{\Delta \tau_s}{V_L} \left(\frac{1}{k} + \frac{1}{C} \right). \tag{A5}$$

To determine the ratio of slip during an episode to the total slip, χ , the "coupling" coefficient, we use the slip resulting from elastic unloading of the fault during an episode, given by $d_e = \Delta \tau_s/k$, and the total slip $d_{\text{total}} = V_L t_r$. Combining these definitions with equation A5 leads to

$$\chi = \frac{d_e}{d_{\text{total}}} = \frac{1}{1 + k/C} \cdot (A6)$$

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