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A PARTIAL WAVE ANALYSIS OF THE REACTION  $nN \rightarrow Nnn$  IN THE CMS ENERGY RANGE 1.6 BeV TO 2.0 BeV

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UNIVERSITY OF CALIFORNIA

A PARTIAL WAVE ANALYSIS OF THE REACTION  $\pi N \rightarrow N\pi\pi$  IN  
THE CMS ENERGY RANGE 1.6 BeV TO 2.0 BeV

David J. Herndon  
(Ph. D. thesis)

May 30, 1972



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A Partial Wave Analysis of the Reaction  $\pi N \rightarrow N \pi \pi$   
in the CMS Energy Range 1.6 BeV to 2.0 BeV

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May 30, 1972

ABSTRACT

We present the results of an energy independent partial-wave analysis of the single-pion production reactions at nine center of mass energies from 1.6 to 2.0 GeV. This maximum likelihood analysis was based upon the Isobar Model. We use the results of a preliminary K-matrix analysis to remove the overall phase ambiguity at each of our energies. The Argand plots confirm the S11(2100) and P13(1850) resonances and show no evidence for the P31(1900) in our channels. There are indications of the existence of the D13(1700), badly needed by the quark model, and for a new P11 resonance around 2100 MeV.

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INTRODUCTION

The  $\pi N$  elastic partial-wave analyses done during the middle 1960's generated great interest in a partial-wave analysis of the inelastic channels. These elastic analyses predicted a large number of new resonances with large couplings to the inelastic channels. The inelastic analyses would determine the couplings to the various inelastic channels and would determine the relative signs of the couplings.

This analysis concerns the single-pion production reactions. Of the five possible reactions,

$$\pi^- p \rightarrow n \pi^0 \pi^0 \quad (1)$$

$$\rightarrow n \pi^- \pi^+ \quad (2)$$

$$\rightarrow p \pi^- \pi^0 \quad (3)$$

$$\pi^+ p \rightarrow p \pi^+ \pi^0 \quad (4)$$

$$\rightarrow n \pi^+ \pi^+ \quad (5)$$

we decided to look at reactions (2) and (3) in the region of the 1688 resonances. There are at least two dominant resonances, the D15 and F15, as well as other smaller resonances in this region. By using two channels, we hoped to be able to separate the  $I_{spin} = \frac{1}{2}$  from the  $I_{spin} = \frac{3}{2}$  contributions. At these energies we are far from threshold and many waves should be present, but we felt that with enough events we could separate the different waves. The practical reason for choosing this region was the large amount of LBL 72" hydrogen bubble chamber film already exposed by others doing

strange-particle analyses.

Looking at the data from the available 72" HBC film (fig 1), we see that it adequately covers only the lower half of the 1688 region. We proposed and were granted a run using the 30" MURA HBC at Argonne National Lab to fill in the gap in the 1688 data. Although the original proposal was expanded to include data from 1.4 to 2.0 GeV (fig 2), the data below 1.63 GeV was not sufficient to be used in the fitting. For a complete discussion of the data and its reduction see the paper by Brody et. al.<sup>1</sup>

After starting the analysis, we found that the  $\pi^-$  data alone was insufficient and that we also needed  $\pi^+$  data. Bernard Deler was in Berkeley at that time and gave us  $\approx 20000 \pi^+$  events<sup>2</sup> covering our entire energy region. We later obtained  $\approx 25000 \pi^+$  events in the region 1.83 to 2.0 GeV from a UCR - LBL collaboration.<sup>3</sup> Table I and figures 3 - 6 give the breakdown by energy and reaction of all the data used. Mark numbers correspond to the reactions in equations 1 - 5, i.e. Mark 2 corresponds to  $\pi^- p \rightarrow n \pi^- \pi^+$ .

The analysis has progressed in three stages; program development, energy independent fitting, and energy dependent analysis. Because none of the available fitting programs could handle either the amount of data or the number of parameters ( $\leq 120$ ) necessary for the analysis, Larry Miller wrote a new maximum likelihood fitting program.<sup>4</sup> While this work was going on, we developed as a framework for the analysis a generalized Isobar Model formalism<sup>5</sup> (hereafter called HSC) which allows arbitrary spins on all five particles.

8 2 1 0 0 3 7 0 1 2 8

Ronald Longacre<sup>6</sup> has written a program based upon the K-matrix formalism to do an energy dependent analysis of our final amplitudes. This report deals with the energy independent fitting and with the addition of an appendix on errors will appear as LBL-544. In the first section we develop the actual equations used in the analysis and discuss the fitting procedure. Section two is a discussion of our final amplitudes.

I. EQUATIONS AND PROCEDURES

We summarize the formalism of HSC for the general case of  $a + b \rightarrow 1 + 2 + 3$  where  $a$  is the beam,  $b$  the target, and 1, 2, 3 are the three outgoing particles. We let  $j, k, l$  represent any cyclic permutation of 1, 2, 3. The diparticle (fig 7) is always composed of particles  $k$  and  $l$  with all diparticle quantities indexed by a subscript  $j$ . Figure 7 illustrates the following quantities and equation 6 relates the different angular momenta.

- a. Total CMS energy and angular momentum -  $W, J$
- b. Four-momenta in CMS -  $p_a p_b Q_j Q_k Q_l$
- c. Particle spins -  $\sigma_a \sigma_b \sigma_j \sigma_k \sigma_l$
- d. Helicities in CMS -  $\mu_a \mu_b \mu_j \mu_k \mu_l$
- e. Mass of diparticle -  $w_j$
- f. Spin and CMS helicity of the diparticle -  $j_j \lambda_j$
- g. Incident orbital angular momentum and total spin -  $L S$
- h. Outgoing orbital angular momentum and total spin -  $L_j S_j$

In the diparticle rest-frame we have the quantities

- i. Four-momenta of the decay particles -  $q_k q_l$
- j. Helicities of the decay particles -  $\nu_k \nu_l$
- k. Orbital angular momentum and total spin of decay particles -  $l_j s_j$

The angular momenta are coupled in the following manner:

$$\begin{aligned}
 \vec{S} &= \vec{\sigma}_a + \vec{\sigma}_b \\
 \vec{J} &= \vec{L} + \vec{S} \\
 \vec{s}_j &= \vec{\sigma}_k + \vec{\sigma}_l \\
 \vec{j}_j &= \vec{l}_j + \vec{s}_j \\
 \vec{S}_j &= \vec{\sigma}_j + \vec{j}_j \\
 \vec{J}_j &= \vec{L}_j + \vec{S}_j
 \end{aligned}
 \tag{6}$$

We assume that  $L, L_j,$  and  $l_j$  are chosen so as to conserve parity. We use  $\mu$  with no subscript to represent a fixed set of all five helicities. The index  $n$  represents the set of quantities

$$n = (j; J; L S; L_j S_j; j_j l_j s_j).
 \tag{7}$$

The differential cross-section is written as

$$d\sigma = \frac{\pi^2}{F} \bar{\Sigma}_{\mu} |f_{\mu}|^2 dp
 \tag{8}$$

where

$$\bar{\Sigma}_{\mu} = \frac{1}{(2\pi_{in})(2\pi_{out})} \Sigma_{\mu}
 \tag{9}$$

and

$$f_{\mu} = \sum_n g_n^{\mu} T_n(W, w_j)
 \tag{10}$$

The  $T_n(W, w_j)$  are such that at a fixed energy  $W_0$

$$\int |T_n(W_0, w_j)|^2 dw_j \leq 1/2 \quad (11)$$

Letting  $p$  and  $Q_j$  be the magnitude of the incoming and outgoing momenta in the center of mass and  $q_k$  be the decay momentum in the diparticle rest-frame,

$$g_n^\mu = \frac{W}{\pi} \sqrt{\frac{w_j}{\pi p \rho_j \beta_k}} \sqrt{(2L+1)(2L_j+1)(2L_j+1)} \\ C(\sigma_a, \sigma_b, S | \mu_a, \mu_b) C(L, S, J | 0, \mu_a - \mu_b) \\ \sum_{\lambda_j} C(\sigma_j, \delta_j, S_j | \mu_j, -\lambda_j) C(L_j, S_j, J | 0, \mu_j - \lambda_j) D_{\mu_j - \lambda_j}^J(\alpha_j, \beta_j, \gamma_j) \\ \sum_{\mu_k} C(\sigma_k, \sigma_c, S_j | \mu_k, \mu_c) C(L_j, S_j, J | 0, \mu_k - \mu_c) d_{\mu_k - \mu_c}^{L_j}(\theta_j) \\ d_{\mu_k - \mu_c}^{L_j}(\theta_j) d_{\mu_k - \mu_c}^{L_j}(\theta_j) d_{\mu_k - \mu_c}^{L_j}(\theta_j) (-1)^{\mu_k - \mu_c}$$

Although not exact, we use the Watson final-state interaction term for the final-state enhancement factor. Since the Watson form includes the barrier factor for the decay, we only need to include the incoming and outgoing barrier terms. We used  $p^L$  and  $Q_j^{L_j}$ , but these are inadequate and should be corrected.<sup>7</sup> Explicitly writing the isospin vector addition coefficients and assuming no other  $w_j$  dependence,  $T_n$  can be written as

$$T_n(W, w_j) = C(I^a, I^b, I | I_2^a, I_2^b) C(I^c, I^d, I | I_2^c, I_2^d + I_2^e) \\ C(I^k, I^l, I^0 | I_2^k, I_2^l) \frac{1}{4W} P_{Q_j}^{L+L_j+L_j} \quad (13) \\ \frac{e^{i\delta}}{q_k^{L_j+1}} \sqrt{\frac{q_k}{4W_j}} A_n(W)$$

Absorbing the factor  $\frac{\pi^2}{F} \frac{1}{(2\sigma_a+1)(2\sigma_b+1)}^{1/2}$  into  $f_\mu$ , we have

$$d\sigma = \sum_{\mu} |f_\mu'|^2 dp \quad (14)$$

where

$$f_\mu' = \sum_n X_{n\mu} A_n(W) \quad (15)$$

and

$$X_{n\mu} = C(I^a, I^b, I | I_2^a, I_2^b) C(I^c, I^d, I | I_2^c, I_2^d + I_2^e) \\ C(I^k, I^l, I^0 | I_2^k, I_2^l) \frac{4}{\sqrt{W\rho\pi}} [(2\sigma_a+1)(2\sigma_b+1)]^{-1/2} \\ p^L Q_j^{L_j} \frac{e^{i\delta} \sin \delta}{q_k^{L_j+1}}$$

$$[(2L+1)(2L_j+1)(2L_j+1)]^{1/2} C(\sigma_a, \sigma_b, S | \mu_a, \mu_b) C(L, S, J | 0, \mu_a - \mu_b) \quad (16)$$

$$\sum_{\lambda_j} C(\sigma_j, \delta_j, S_j | \mu_j, -\lambda_j) C(L_j, S_j, J | 0, \mu_j - \lambda_j) \\ D_{\mu_j - \lambda_j}^J(\alpha_j, \beta_j, \gamma_j)$$

$$\sum_{\mu_k} C(\sigma_k, \sigma_c, S_j | \mu_k, \mu_c) C(L_j, S_j, J | 0, \mu_k - \mu_c)$$

$$d_{\mu_k - \mu_c}^{L_j}(\theta_j) d_{\mu_k - \mu_c}^{L_j}(\theta_j) d_{\mu_k - \mu_c}^{L_j}(\theta_j) (-1)^{\mu_k - \mu_c}$$

For our case with three of the five particles having zero spin, the expression for  $X_{n\mu}$  is much simpler. Since we have divided the data into energy bins and are doing an energy independent analysis, we removed the term  $p^L$  as being constant over each bin and assumed that  $A_n(W)$  is a constant for each bin. It is these constant  $A_n$  that are the actual fitting parameters.

Types of Diparticles We consider three final-state resonances:

the  $\Delta(1236)$  ( $L=1, l=\frac{3}{2}, J=\frac{3}{2}$ )  $\pi N$  resonance, the  $\rho(760)$  ( $L=I=J=1$ ) resonance, and the  $\sigma(800)$  ( $L=I=J=0$ )  $\pi\pi$  enhancement. In the case of the  $\rho$  there are two possible values for  $S_j, \frac{1}{2}$  and  $\frac{3}{2}$ ; these will be denoted by  $\rho_1$  and  $\rho_3$  respectively. We consider all waves with  $L$  and  $L_j$  less than 4 which meant 60 possible waves.

|  |   |  |   |   |   |  |
|--|---|--|---|---|---|--|
| LL <sub>j</sub> (2J)   |   |  |   |   |   |  |
| $\left. \begin{array}{l} \text{PP 1} \\ \text{SD 1} \\ \text{DS 3} \\ \text{PP 3} \\ \text{DD 3} \\ \text{PF 3} \\ \text{FP 5} \\ \text{DD 5} \\ \text{FF 5} \\ \text{FF 7} \end{array} \right\} \Delta$ | + | $\left. \begin{array}{l} \text{PP 1} \\ \text{SD 1} \\ \text{DS 3} \\ \text{PP 3} \\ \text{DD 3} \\ \text{PF 3} \\ \text{FP 5} \\ \text{DD 5} \\ \text{FF 5} \\ \text{FF 7} \end{array} \right\} \rho_3$ | + | $\left. \begin{array}{l} \text{SS 1} \\ \text{PP 1} \\ \text{PP 3} \\ \text{DD 3} \\ \text{DD 5} \\ \text{FF 5} \\ \text{FF 7} \end{array} \right\} \rho_1$ | + | $\left. \begin{array}{l} \text{PS 1} \\ \text{SP 1} \\ \text{DP 3} \\ \text{PD 3} \\ \text{FD 5} \\ \text{DF 5} \end{array} \right\} \sigma$ |
| 10 waves x   |   | 10 waves x   |   | 7 waves x   |   | 6 waves x  |
| 2 isospins =   | + | 2 isospins =   | + | 2 isospins =  | + | 1 isospin =  |
| 20   |   | 20   |   | 14  |   | 6  |

We use a seven-character label for each wave. The first three characters designate the type of diparticle, P33, RH3, RH1, SIG; the last four characters are  $L, L_j, (2I),$  and  $(2J)$ . Thus an incoming F15

wave going to a  $\Delta\pi$  final state with  $L_j = 1$  is denoted by P33 FP15. These labels appear at the lower left of each Argand plot.

For the Delta phase in the Watson final-state interaction term, we used a table look-up from CERN-TH<sup>8</sup> with linear interpolation (quadratic interpolation from threshold to 1.089 GeV.) For energies above 1.794 GeV, we fixed  $\delta = 180^\circ$ . Figure 8 gives  $\delta$  and  $e^{i\delta} \sin \delta / g^{2l+1}$  for the Delta. Figure 9 shows the same plots for the Rho. The Rho phases come from the parametrization of Morgan,<sup>9</sup>

$$\cot \delta = \frac{(m_\pi^2 - 0.1536 g^2)(m_\pi^2 + 0.028 g^2) \sqrt{m_\pi^2 + g^2}}{0.035 m_\pi^2 g^3} \quad (17)$$

For the Sigma (now called the  $\epsilon$ ), we split the energy region into three parts. For energies above 0.66 GeV, we used the phase from a Breit-Wigner with  $E_r = 0.9$  GeV and  $\Gamma_r = 0.74$  GeV.

$$\cot \delta = 2(0.9 - \omega) / 0.74 \quad (18)$$

This form was chosen to correspond to the old "up-down" solution.

For energies below 0.4 GeV, we used a scattering length approximation,

$$\frac{g}{\omega} \cot \delta = \frac{1}{0.32} - 109.5 g^2 + 1114.0 g^4 \quad (19)$$

The constant term corresponds to a scattering length  $a_0 = 0.16$ .<sup>9</sup> The other two terms were added to give a smooth joining of equations 18 and 19 at 0.53 GeV. Rather than actually extending each form to 0.53 GeV, we drew a hand-drawn curve between 0.4 and 0.66 GeV and used a table look-up with linear interpolation from points on this curve.





$i^{\text{th}}$  event is

$$P_i = \sum_{\mu} |f_{\mu}'|^2 \quad (23)$$

When  $p_i / p_{\text{max}}$  was greater than a generated random number, the event was kept as part of the artificial data. In this manner we generated 4733 Mark 2 events and 2850 Mark 3 events.

To obtain a set of reasonable starting values for fitting the artificial data, we randomly generated 2000 sets of A's and kept the twenty sets with the highest likelihood. These twenty sets typically reduced to five separate solutions after fitting. Any wave, for which the modulus was within one standard deviation of zero in at least three of the five solutions, was considered statistically insignificant and eliminated. After elimination, we refit with fewer waves and again tried to eliminate waves. In the end the five separate solutions has coalesced into one solution, and the number of waves had reduced from 60 to 24. These 24 waves consisted of the original eleven waves and another thirteen extra waves each of which had  $|T| < 0.028$ .

Figure 12a shows the fitted amplitudes corresponding to the original eleven waves and figure 12b shows the extra thirteen waves. On all Argand plots, the scale maximum is given at the lower right.

Fitting For our first attempts at fitting the data we chose energy bins 20 MeV wide. We were unable to get satisfactory fits as discussed by Miller.<sup>4</sup> We recombined the data into bins 40 MeV wide and we label each bin by its midpoint, eg. 1650.

Initially we worked with just the five lowest bins, 1650 - 1810. At each energy we generated 2000 random sets of starting A's and, using

those with the highest likelihood, fit with as many sets as necessary to generate five distinct 60-wave solutions. At each energy, we then made a list of all waves whose modulus was within 1.25 standard deviations of zero in any of the five solutions. Any wave which was considered statistically insignificant in a majority (3/5) of the energy bins was then eliminated and the whole procedure repeated. In the case of the rho waves, we have the problem of the two types of waves, RH1 and RH3. In all cases in which the different types also had different  $L_j$  values, the program chose the wave with the lower value of  $L_j$ . In the three cases, P13, P31, and F37, in which both rho waves have the same value of  $L_j$ , we fit with only one wave and then with only the other wave choosing that wave giving the higher likelihood in a majority of the energy bins. In all cases the difference in likelihoods was insignificant and the fits would be unchanged if the other wave was used. Using this technique we reduced the number of waves from 60 to 30.

At this point we still had three or four solutions at each energy. To look for continuity, we used each solution as a starting value in the energy bin above and below its own. In this manner we were able to find a continuous chain over all five energies. Except for 1730 which had two solutions (one when going up from 1690 and one when coming down from 1770) each energy had just one solution which fit into the chain.

We were now ready to try the four highest energies, 1850 - 1970. Again we generated 2000 random sets of A's but, because of computer

time, kept only enough sets to give four separate solutions after fitting. Rather than again going through the procedure of eliminating waves, we tried to use the 30 waves from the lower energies plus the F35 and F37 waves which had not been used at the lower energies. By eliminating some waves and extending the new waves down to the lower bins, we were able to get a 28 wave chain that included eight of the nine bins. It was impossible to include 1930 in the chain. By looking at plots of the amplitudes we removed any wave which seemed small at all energies and any wave whose behaviour was erratic. We also removed the F35 and F37 waves from the lowest two bins. This reduced the number of waves to 24 (23 at 1730 and 20 at 1650 and 1690.) We were now able to include 1930 in the chain and to resolve the ambiguity at 1730. The chain was completely continuous upwards and downwards in energy.

We need to check our judgement in removing the waves. The effect on both  $\chi^2$  and the likelihood are discussed in detail in ref. 6, but here we give brief re-assurance. Taking the log of the likelihood, we have

$$\ln L = F = -\frac{\chi^2}{2} + \text{Constant} \quad (24)$$

Thus any wave (2 parameters) that is statistically insignificant should cause a change in F of  $\approx 1$  when removed. We find that the change from 30 waves to 28 waves caused a change in F of about 10 or 5/wave. On the other hand, the reduction of 24 waves caused a change in F of 25/wave at 1650 up to 50/wave at 1970. Clearly we are removing waves which the program feels are needed. As a check to see how important these changes really are, we removed the

P33 DD15 wave at 1650 and the P33 FP15 wave at 1690. Since the P33 DD15 wave is the only D15 wave and since it is large at 1650, one would expect a drastic change in F. The P33 FP15, however, is one of three F15 waves and is only "medium" in size, and one would expect a smaller change in F. The changes were 584 and 186 respectively. Thus it appears that we did not remove any waves that were really needed by the fit.

During the fitting, we imposed a unitarity constraint. We added for each incoming partial wave an extra term in the likelihood of the form

$$e^{-\alpha^2 \left( \frac{\sigma_{INEL} - \sigma_{CALC}}{\delta\sigma_{INEL}} \right)^2} \quad (25)$$

$\sigma_{inel}$  and  $\delta\sigma_{inel}$  came from averaging the inelastic cross-sections predicted by the different elastic phase-shift analyses<sup>8</sup> and using their external error. The parameter  $\alpha$  was taken to be zero if  $\sigma_{inel} > \sigma_{calc}$ , and for  $\sigma_{inel} < \sigma_{calc}$ , we adjusted  $\alpha$  so that  $\delta\sigma_{inel} = \alpha \delta\sigma_{calc}$ . When we removed the small F35 waves at 1650 and 1690, the F15 cross-section increased and at 1690 it just violates unitarity.

The fitting program, RUMBLE, is designed to be invariant to overall scale changes in the amplitudes.<sup>4</sup> After fitting, we must normalize the final fitted amplitudes to the known cross-sections. For our fits, RUMBLE adjusts the scale factor so that the sum of the calculated cross-sections for channels 2, 3, and 4 equals the sum of the experimental cross-sections for these channels. Table II

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gives the values of the input cross-sections and the final calculated values. Figures 13 - 17 give the experimental cross-sections for each channel with our calculated cross-sections,  $\sigma_{calc}$ , marked by x's. We are always low in our calculated value of the  $\pi^+ p \rightarrow n\pi^+ \pi^+$  cross-section, and it gets worse as the energy increases. This is probably due to an increasing contribution to the cross-section from the  $N\pi$  channels.

## II. RESULTS

To get a feeling for the quality of our fits, Larry Miller wrote a program<sup>15</sup> that allows one to bin the data in up to four variables and to then compare the actual bin population to a predicted bin population. The predicted population is obtained by binning Monte Carlo events, each weighted by  $p_i$  (see eq. 21.) For our four variables, we chose  $\phi$ ,  $\cos\theta$ ,  $M(N\pi)$ , and  $M(\pi\pi)$  where  $(\theta, \phi)$  are the angles of the beam and the  $\pi$  in the  $(N\pi)$  combination has the same sign as the beam. Figures 18 - 23 show these comparisons for Marks 2, 3, and 4 at 1690 and 1930. Figure a is always the four-dimensional plot and figures b and c are the two two-dimensional plots. To ensure enough statistics in each bin, the four-dimensional plots have each variable divided into only four bins and the two-dimensional plots have each variable divided into ten bins. In each bin the dashed tombstone indicates the real event population and the solid tombstone indicates the predicted population. The population is proportional not to the area but to the height (or width) of the tombstone. To the

top and right of each two-dimensional plot are the projections of what is below and to the left. With the increase in statistics due to making projections, the number of bins is increased. From the figures, we see that our solution predicts the distribution of events well in all areas of the four-dimensional kinematic space in all three channels.

By doing an energy independent analysis, one is unable to determine the relative phase between fits at different energies. Thus one is unable to make Argand plots and to look for resonances. One can, however, use the less reliable method of plotting  $|T|^2$  and looking for resonance bumps. One can also compare the calculated inelastic cross-section,  $\sigma_{calc}$ , with the cross-section predicted by the elastic analyses,  $\sigma_{inel}$ . We have included both types of plots in figures 29 - 40.

Since Argand plots are so useful, one looks for different methods to fix the relative phase between the different energies. One can make the phase of a particular wave constant with energy, but trying to guess which wave is difficult. (with hindsight, we could fix the phase of the RH3 DS33 wave in our case.) One can assume that one wave is resonating and give that wave the appropriate phase at each energy. Still another method is the least path method. Here one adjusts the relative phase between the amplitudes at energy  $E_n$  and energy  $E_{n+1}$  so as to minimize the quantity  $\sum_j |T_j(E_n) - T_j(E_{n+1})|$ . This was the method used by Miller.<sup>4</sup> When most of the waves are moving with energy, this method tends to remove the motion. A more sophisticated method,

and therefore more open to discussion, is to try and relate the inelastic phases to the elastic phases using the K-matrix formalism. Longacre's program fits each incoming partial wave with a factorizable pole and a constant non-factorizable background. He adjusts the overall phase at each energy to give the best combined fit to the four partial waves D15, F15, F35, and F37. Figures 24 - 28 are our final amplitudes with this phase adjustment. The errors are approximately the size of the letter representing each point and have been suppressed for legibility. Tables III - XI give our final 24 amplitudes and the parameters of the two-dimensional error ellipse<sup>16</sup> at each energy. The appendix in LBL-544 will be a more detailed discussion of the errors.

There are two general features of our amplitudes. The Delta in general is coupled to the resonances in the lower part of our energy region and the Rho is coupled to those resonances in the upper part of our energy region and to those resonances just above our energy region. This probably reflects the opening of the Rho channel at a CM energy of 1700 MeV.

Figures 29 - 40 give our amplitudes rearranged by incoming partial wave. In each figure we give the Argand plot and  $|T|^2$  plot for each of our amplitudes along with a plot of the calculated inelastic cross-section,  $\sigma_{calc}$ . On the cross-section plots, we show the predicted inelastic cross-sections,  $\sigma_{inel}$  and  $\delta\sigma_{inel}$ , as vertical lines slightly offset. For the following discussion we use the new

$\pi N$  phase-shift analysis of Almeded and Lovelace<sup>17</sup> as the "elastic analysis." Table XII is a copy of their Table 3 with an extra column added showing which diparticle couples to each resonance.

S11 We clearly see the elastic S11(1670) in the  $\sigma N$  channel; in the  $\rho N$  channel the S11(1670) seems to be there but not strongly. The  $\rho N$  channel also gives evidence for a resonance above our energy region corresponding to the S11(2100).

P11 The P11(1720) seems to be mostly  $\Delta\pi$  whereas the  $\sigma N$  channel suggests a new resonance at about 2100 MeV.

P13 We definitely have a resonance at about 1900 in the  $\rho N$  channel with a width of  $\approx 300$  MeV.

D13 Both the  $\Delta\pi$ (DS13) and the  $\sigma N$  channels suggest that the D13(1700), badly needed by the quark model,<sup>18</sup> does exist. Point H in the RH3 DS13 wave is probably a bad point and should be out with G and I. In which case, this channel is coupled to the D13(2075).

D15 As we should, we see the D15(1683) but only in the  $\Delta\pi$  channel. We see no evidence for the D15(2100); probably because we have not included the  $\rho N$  channel in the final fit.

F15 The F15(1688) appears in all three channels and about equally in each. No indication of the F15(2175) but it is probably too far above our energies.

F17 We found that the F17 waves were insignificant at our energies.

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S31 Both the  $\Delta\pi$  and  $\rho N$  channels indicate the presence of the S31(1620) just below our energy region.

P31 We see nothing in the P31 channel.

P33 The  $\Delta\pi$  amplitude is consistent with just a decreasing background.

D33 We see the D33(1700) in the  $\Delta\pi$  channel with no structure in the  $\rho N$  channel.

D35 We found the D35 channels insignificant.

F35 The F35(1875) is clearly shown by the  $\rho N$  channel. No apparent structure in the  $\Delta\pi$  channel.

F37 The F37(1925) is clearly seen in both the  $\Delta\pi$  and  $\rho N$  channels.

In looking at the large  $\Delta\pi$  F15 and D15 channels, we find that solution B of our earlier paper<sup>19</sup> can be discarded. We find that the relative sign of the couplings of these resonances to the  $\Delta\pi$  channel is negative, and that the F15 is coupled about equally to the  $\Delta\pi$ ,  $\rho N$ , and  $\sigma N$  channels.

\* \* \* \* \*

We have presented the results of an energy independent partial wave analysis of the single-pion production reactions at nine energies. Using the results of a K-matrix analysis, we have removed the arbitrary overall phase at each energy. The Argand plots confirm the two resonances S11(2100) and P13(1850) observed only weakly in the elastic channel. We also see evidence for a new resonance around 2100 VeV in P11, and no evidence for the P31(1900). We also see some evidence for the D13(1700). Further study<sup>6</sup> is planned of each incoming partial wave using the K-matrix to give the proportion of background to resonance and the resonance parameters.

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TABLE I: Events per channel for each energy bin

| Energy Range | Bin Name | Mark 2 Events<br>(n-+) | Mark 3 Events<br>(p-0) | Mark 4 Events<br>(p+0) | Total Events |
|--------------|----------|------------------------|------------------------|------------------------|--------------|
| 1630 - 1670  | 1650     | 6061                   | 3757                   | 2467                   | 12285        |
| 1670 - 1710  | 1690     | 5901                   | 3689                   | 1139                   | 10729        |
| 1710 - 1750  | 1730     | 3455                   | 2630                   | 4061                   | 10146        |
| 1750 - 1790  | 1770     | 3214                   | 2352                   | 2853                   | 8419         |
| 1790 - 1830  | 1810     | 2447                   | 1541                   | 3855                   | 7843         |
| 1830 - 1870  | 1850     | 3931                   | 3183                   | 6372                   | 13486        |
| 1870 - 1910  | 1890     | 5072                   | 3170                   | 12690                  | 20932        |
| 1910 - 1950  | 1930     | 5817                   | 4080                   | 4298                   | 14195        |
| 1950 - 1990  | 1970     | 5277                   | 3544                   | 7744                   | 16565        |

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TABLE II: Input and calculated cross-sections for each channel

| ENERGY<br>Bin | MARK 1<br>(n00) |      | MARK 2<br>(n-+) |       | MARK 3<br>(p-0) |      | MARK 4<br>(p+0) |       | MARK 5<br>(n++) |      |
|---------------|-----------------|------|-----------------|-------|-----------------|------|-----------------|-------|-----------------|------|
|               | INPUT           | CALC | INPUT           | CALC  | INPUT           | CALC | INPUT           | CALC  | INPUT           | CALC |
| 1650          |                 | 3.54 | 10.10           | 10.40 | 6.21            | 5.81 | 9.90            | 10.00 |                 | 0.93 |
| 1690          |                 | 3.96 | 11.81           | 12.21 | 7.29            | 6.86 | 10.10           | 10.13 |                 | 1.01 |
| 1730          |                 | 2.57 | 8.07            | 8.37  | 5.93            | 5.68 | 9.70            | 9.66  |                 | 0.91 |
| 1770          |                 | 2.14 | 7.75            | 8.00  | 5.68            | 5.40 | 10.20           | 10.22 |                 | 0.72 |
| 1810          |                 | 2.13 | 8.30            | 8.42  | 4.79            | 4.75 | 10.90           | 10.82 |                 | 0.74 |
| 1850          |                 | 1.86 | 8.00            | 7.99  | 4.50            | 4.50 | 11.50           | 11.52 |                 | 0.74 |
| 1890          |                 | 1.81 | 8.70            | 8.51  | 4.90            | 4.86 | 11.20           | 11.43 |                 | 0.76 |
| 1930          |                 | 1.68 | 7.50            | 7.40  | 4.80            | 4.75 | 11.50           | 11.65 |                 | 0.67 |
| 1970          |                 | 1.29 | 6.60            | 6.44  | 4.50            | 4.36 | 8.60            | 8.91  |                 | 0.49 |

TABLE III: 1650 Partial-wave amplitudes with error ellipse parameters (semi-major axis, semi-minor axis, and angle of semi-major axis wrt the x-axis.)

| WAVE LABEL | AMPLITUDE |        | ERROR ELLIPSE |       |          |
|------------|-----------|--------|---------------|-------|----------|
|            | REAL      | IMAG   | MAJOR         | MINOR | ANGLE(°) |
| P33 PP11   | -0.288    | 0.063  | 0.037         | 0.037 | -41.28   |
| P33 DS13   | 0.225     | -0.054 | 0.032         | 0.029 | 55.31    |
| P33 DD13   | -0.083    | -0.103 | 0.028         | 0.024 | 43.40    |
| P33 FP15   | -0.035    | 0.266  | 0.025         | 0.020 | - 0.85   |
| P33 DD15   | -0.200    | -0.346 | 0.024         | 0.018 | 43.53    |
| P33 PP31   | 0.084     | -0.061 | 0.035         | 0.030 | 75.07    |
| P33 SD31   | 0.123     | -0.338 | 0.038         | 0.023 | 5.02     |
| P33 DS33   | 0.177     | 0.168  | 0.029         | 0.023 | -59.67   |
| P33 PP33   | 0.086     | 0.306  | 0.041         | 0.012 | 55.85    |
| P33 FF35   |           |        |               |       |          |
| P33 FF37   |           |        |               |       |          |
| RH3 DS13   | 0.033     | -0.070 | 0.026         | 0.022 | -80.63   |
| RH3 FP15   | 0.132     | 0.234  | 0.018         | 0.016 | 41.19    |
| RH3 DS33   | 0.192     | 0.007  | 0.025         | 0.024 | 74.20    |
| RH3 FP35   |           |        |               |       |          |
| RH3 FF37   |           |        |               |       |          |
| RH1 SS11   | 0.171     | 0.074  | 0.035         | 0.028 | -86.15   |
| RH1 PP13   | -0.073    | 0.040  | 0.024         | 0.021 | -61.18   |
| RH1 SS31   | 0.222     | 0.207  | 0.041         | 0.025 | -69.73   |
| RH1 PP31   | 0.087     | -0.027 | 0.037         | 0.037 | -54.88   |
| SIG PS11   | 0.153     | 0.022  | 0.043         | 0.035 | -67.75   |
| SIG SP11   | -0.178    | -0.133 | 0.047         | 0.040 | -58.69   |
| SIG DP13   | -0.214    | -0.041 | 0.034         | 0.026 | -71.04   |
| SIG FD15   | 0.131     | 0.202  | 0.018         | 0.014 | -42.71   |

TABLE IV: 1690 Partial-wave amplitudes with error ellipse parameters (semi-major axis, semi-minor axis, and angle of semi-major axis wrt the x-axis.)

| WAVE LABEL | AMPLITUDE |        | ERROR ELLIPSE |       |          |
|------------|-----------|--------|---------------|-------|----------|
|            | REAL      | IMAG   | MAJOR         | MINOR | ANGLE(°) |
| P33 PP11   | -0.248    | -0.145 | 0.044         | 0.042 | -39.20   |
| P33 DS13   | 0.254     | 0.105  | 0.032         | 0.031 | -56.26   |
| P33 DD13   | 0.011     | -0.080 | 0.032         | 0.027 | -33.87   |
| P33 FP15   | -0.214    | 0.256  | 0.026         | 0.023 | -74.10   |
| P33 DD15   | -0.033    | -0.447 | 0.033         | 0.018 | -37.25   |
| P33 PP31   | 0.094     | 0.051  | 0.051         | 0.037 | 82.08    |
| P33 SD31   | 0.281     | -0.213 | 0.041         | 0.037 | -75.08   |
| P33 DS33   | 0.014     | 0.268  | 0.033         | 0.028 | -31.74   |
| P33 PP33   | -0.138    | 0.337  | 0.039         | 0.017 | 76.08    |
| P33 FF35   |           |        |               |       |          |
| P33 FF37   |           |        |               |       |          |
| RH3 DS13   | -0.035    | -0.040 | 0.032         | 0.024 | -43.50   |
| RH3 FP15   | -0.069    | 0.306  | 0.023         | 0.018 | 69.54    |
| RH3 DS33   | 0.137     | 0.071  | 0.031         | 0.029 | -51.53   |
| RH3 FP35   |           |        |               |       |          |
| RH3 FF37   |           |        |               |       |          |
| RH1 SS11   | 0.196     | 0.207  | 0.038         | 0.032 | -66.11   |
| RH1 PP13   | -0.160    | -0.059 | 0.027         | 0.026 | -35.27   |
| RH1 SS31   | 0.073     | 0.303  | 0.054         | 0.034 | -45.73   |
| RH1 PP31   | 0.036     | -0.038 | 0.050         | 0.044 | 73.20    |
| SIG PS11   | 0.077     | 0.163  | 0.050         | 0.043 | -38.76   |
| SIG SP11   | 0.016     | -0.266 | 0.042         | 0.041 | -27.49   |
| SIG DP13   | -0.233    | -0.163 | 0.030         | 0.029 | -69.67   |
| SIG FD15   | -0.025    | 0.250  | 0.018         | 0.018 | 61.25    |



TABLE V: 1730 Partial-wave amplitudes with error ellipse parameters (semi-major axis, semi-minor axis, and angle of semi-major axis wrt the x-axis.)

| WAVE LABEL | AMPLITUDE |        | ERROR ELLIPSE |       |          |
|------------|-----------|--------|---------------|-------|----------|
|            | REAL      | IMAG   | MAJOR         | MINOR | ANGLE(°) |
| P33 PP11   | -0.098    | -0.329 | 0.048         | 0.048 | 68.91    |
| P33 DS13   | 0.089     | 0.163  | 0.040         | 0.029 | - 2.41   |
| P33 DD13   | 0.052     | -0.037 | 0.041         | 0.028 | 5.76     |
| P33 FP15   | -0.263    | 0.152  | 0.035         | 0.023 | -46.10   |
| P33 DD15   | 0.206     | -0.193 | 0.036         | 0.023 | 10.88    |
| P33 PP31   | 0.077     | -0.030 | 0.035         | 0.034 | -65.24   |
| P33 SD31   | 0.252     | -0.122 | 0.042         | 0.032 | -51.97   |
| P33 DS33   | -0.077    | 0.216  | 0.032         | 0.022 | - 7.32   |
| P33 PP33   | -0.058    | 0.338  | 0.021         | 0.015 | -14.93   |
| P33 FF35   | 0.004     | 0.120  | 0.026         | 0.019 | 1.11     |
| P33 FF37   | 0.087     | 0.088  | 0.015         | 0.013 | 28.07    |
| RH3 DS13   | 0.003     | 0.054  | 0.030         | 0.029 | 23.00    |
| RH3 FP15   | -0.243    | 0.106  | 0.033         | 0.018 | -46.51   |
| RH3 DS33   | 0.168     | 0.103  | 0.028         | 0.020 | -82.98   |
| RH3 FP35   | -0.167    | -0.014 | 0.020         | 0.016 | -29.29   |
| RH3 FF37   |           |        |               |       |          |
| RH1 SS11   | -0.049    | 0.238  | 0.051         | 0.040 | 1.36     |
| RH1 PP13   | -0.063    | -0.214 | 0.034         | 0.031 | -28.71   |
| RH1 SS31   | -0.004    | 0.124  | 0.034         | 0.033 | 84.07    |
| RH1 PP31   | 0.049     | 0.147  | 0.037         | 0.035 | 82.09    |
| SIG PS11   | 0.063     | 0.177  | 0.058         | 0.049 | 9.02     |
| SIG SP11   | 0.169     | -0.221 | 0.059         | 0.053 | 17.22    |
| SIG DP13   | -0.148    | -0.179 | 0.034         | 0.031 | 34.39    |
| SIG FD15   | -0.177    | 0.194  | 0.022         | 0.019 | -74.91   |

TABLE VI: 1770 Partial-wave amplitudes with error ellipse parameters (semi-major axis, semi-minor axis, and angle of semi-major axis wrt the x-axis.)

| WAVE LABEL | AMPLITUDE |        | ERROR ELLIPSE |       |          |
|------------|-----------|--------|---------------|-------|----------|
|            | REAL      | IMAG   | MAJOR         | MINOR | ANGLE(°) |
| P33 PP11   | 0.156     | -0.296 | 0.055         | 0.040 | 35.08    |
| P33 DS13   | 0.083     | 0.210  | 0.038         | 0.036 | -89.13   |
| P33 DD13   | 0.105     | -0.010 | 0.038         | 0.037 | 9.76     |
| P33 FP15   | -0.294    | -0.005 | 0.029         | 0.026 | -79.01   |
| P33 DD15   | 0.067     | -0.116 | 0.032         | 0.027 | 89.52    |
| P33 PP31   | 0.113     | 0.029  | 0.042         | 0.040 | 12.78    |
| P33 SD31   | 0.263     | -0.095 | 0.044         | 0.030 | - 7.41   |
| P33 DS33   | -0.028    | 0.114  | 0.031         | 0.029 | -57.76   |
| P33 PP33   | 0.089     | 0.300  | 0.044         | 0.016 | 74.29    |
| P33 FF35   | -0.033    | 0.083  | 0.027         | 0.024 | 17.24    |
| P33 FF37   | 0.055     | 0.161  | 0.029         | 0.016 | 75.93    |
| RH3 DS13   | -0.104    | -0.008 | 0.033         | 0.030 | -24.47   |
| RH3 FP15   | -0.212    | 0.037  | 0.029         | 0.023 | - 4.07   |
| RH3 DS33   | 0.250     | 0.039  | 0.032         | 0.023 | -71.41   |
| RH3 FP35   | -0.228    | -0.108 | 0.026         | 0.013 | -68.20   |
| RH3 FF37   | -0.031    | 0.037  | 0.022         | 0.016 | -68.71   |
| RH1 SS11   | -0.020    | 0.311  | 0.045         | 0.042 | -84.60   |
| RH1 PP13   | -0.013    | -0.359 | 0.040         | 0.030 | 76.72    |
| RH1 SS31   | 0.009     | 0.150  | 0.040         | 0.037 | 58.86    |
| RH1 PP31   | 0.033     | 0.120  | 0.048         | 0.040 | -69.82   |
| SIG PS11   | 0.032     | 0.307  | 0.051         | 0.047 | -87.22   |
| SIG SP11   | 0.238     | -0.147 | 0.061         | 0.041 | -19.78   |
| SIG D013   | -0.081    | -0.241 | 0.036         | 0.031 | 79.17    |
| SIG FD15   | -0.178    | 0.086  | 0.027         | 0.025 | 77.04    |

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TABLE VII: 1810 Partial-wave amplitudes with error ellipse parameters (semi-major axis, semi-minor axis, and angle of semi-major axis wrt the x-axis.)

| WAVE LABEL | AMPLITUDE |        | ERROR ELLIPSE |       |          |
|------------|-----------|--------|---------------|-------|----------|
|            | REAL      | IMAG   | MAJOR         | MINOR | ANGLE(°) |
| P33 PP11   | 0.119     | -0.292 | 0.066         | 0.049 | -73.52   |
| P33 DS13   | 0.041     | 0.160  | 0.044         | 0.040 | -86.23   |
| P33 DD13   | 0.018     | -0.195 | 0.042         | 0.040 | 80.74    |
| P33 FP15   | -0.242    | -0.003 | 0.036         | 0.033 | - 1.82   |
| P33 DD15   | 0.143     | 0.026  | 0.035         | 0.033 | -17.57   |
| P33 PP31   | 0.079     | 0.059  | 0.043         | 0.037 | -82.92   |
| P33 SD31   | 0.218     | -0.034 | 0.035         | 0.034 | - 0.08   |
| P33 DS33   | -0.088    | 0.079  | 0.029         | 0.027 | -87.59   |
| P33 PP33   | -0.036    | 0.285  | 0.017         | 0.011 | 84.73    |
| P33 FF35   | 0.053     | 0.102  | 0.026         | 0.023 | -22.10   |
| P33 FF37   | 0.070     | 0.218  | 0.025         | 0.011 | -27.50   |
| RH3 DS13   | -0.178    | -0.049 | 0.038         | 0.035 | 56.88    |
| RH3 FP15   | -0.137    | 0.090  | 0.032         | 0.026 | 49.00    |
| RH3 DS33   | 0.224     | 0.072  | 0.034         | 0.020 | 15.32    |
| RH3 FP35   | -0.185    | -0.206 | 0.021         | 0.019 | -54.75   |
| RH3 FF37   | -0.074    | 0.043  | 0.018         | 0.016 | - 8.07   |
| RH1 SS11   | -0.091    | 0.224  | 0.067         | 0.045 | -78.10   |
| RH1 PP13   | 0.112     | -0.411 | 0.039         | 0.021 | -89.45   |
| RH1 SS31   | -0.058    | 0.169  | 0.038         | 0.038 | 77.93    |
| RH1 PP31   | 0.083     | 0.096  | 0.045         | 0.043 | 30.87    |
| SIG PS11   | -0.058    | 0.342  | 0.064         | 0.054 | 85.54    |
| SIG SP11   | 0.294     | -0.035 | 0.071         | 0.071 | 32.44    |
| SIG DP13   | -0.021    | -0.236 | 0.042         | 0.041 | 78.82    |
| SIG FD15   | -0.238    | 0.096  | 0.037         | 0.028 | -27.23   |

TABLE VIII: 1850 Partial-wave amplitudes with error ellipse parameters (semi-major axis, semi-minor axis, and angle of semi-major axis wrt the x-axis.)

| WAVE LABEL | AMPLITUDE |        | ERROR ELLIPSE |       |          |
|------------|-----------|--------|---------------|-------|----------|
|            | REAL      | IMAG   | MAJOR         | MINOR | ANGLE(°) |
| P33 PP11   | 0.154     | -0.291 | 0.046         | 0.037 | 67.33    |
| P33 DS13   | -0.022    | 0.210  | 0.032         | 0.030 | 77.72    |
| P33 DD13   | 0.079     | -0.045 | 0.037         | 0.032 | 60.50    |
| P33 FP15   | -0.231    | -0.067 | 0.028         | 0.024 | -37.63   |
| P33 DD15   | -0.037    | 0.020  | 0.026         | 0.026 | -52.01   |
| P33 PP31   | 0.104     | 0.172  | 0.031         | 0.030 | 47.94    |
| P33 SD31   | 0.247     | 0.064  | 0.031         | 0.021 | -37.79   |
| P33 DS33   | -0.080    | 0.085  | 0.020         | 0.020 | 46.53    |
| P33 PP33   | 0.010     | 0.242  | 0.024         | 0.024 | -51.32   |
| P33 FF35   | -0.008    | 0.127  | 0.023         | 0.017 | 56.30    |
| P33 FF37   | -0.073    | 0.230  | 0.022         | 0.013 | 52.09    |
| RH3 DS13   | -0.143    | -0.094 | 0.029         | 0.025 | 9.52     |
| RH3 FP15   | -0.136    | 0.040  | 0.022         | 0.020 | 26.46    |
| RH3 DS33   | 0.240     | 0.033  | 0.021         | 0.017 | -39.34   |
| RH3 FP35   | -0.143    | -0.289 | 0.020         | 0.012 | -82.47   |
| RH3 FF37   | -0.131    | 0.063  | 0.013         | 0.012 | 24.15    |
| RH1 SS11   | -0.182    | 0.229  | 0.043         | 0.029 | 72.12    |
| RH1 PP13   | 0.289     | -0.329 | 0.013         | 0.006 | 74.42    |
| RH1 SS31   | -0.044    | 0.043  | 0.035         | 0.030 | -79.57   |
| RH1 PP31   | 0.013     | -0.022 | 0.037         | 0.032 | -78.11   |
| SIG PS11   | -0.215    | 0.272  | 0.050         | 0.038 | 65.47    |
| SIG SP11   | 0.282     | -0.041 | 0.049         | 0.045 | 33.56    |
| SIG DP13   | 0.092     | -0.291 | 0.036         | 0.028 | 56.62    |
| SIG FD15   | -0.210    | 0.048  | 0.027         | 0.026 | -55.18   |

TABLE IX: 1890 Partial-wave amplitudes with error ellipse parameters (semi-major axis, semi-minor axis, and angle of semi-major axis wrt the x-axis.)

| WAVE LABEL | AMPLITUDE |        | ERROR ELLIPSE |       |          |
|------------|-----------|--------|---------------|-------|----------|
|            | REAL      | IMAG   | MAJOR         | MINOR | ANGLE(°) |
| P33 PP11   | 0.130     | -0.350 | 0.044         | 0.033 | -57.58   |
| P33 DS13   | -0.089    | 0.096  | 0.031         | 0.028 | 52.02    |
| P33 DD13   | 0.123     | -0.063 | 0.036         | 0.031 | 69.32    |
| P33 FP15   | -0.223    | 0.006  | 0.024         | 0.023 | 85.49    |
| P33 DD15   | -0.162    | -0.066 | 0.026         | 0.025 | 53.70    |
| P33 PP31   | 0.116     | 0.185  | 0.026         | 0.026 | 1.40     |
| P33 SD31   | 0.230     | 0.124  | 0.027         | 0.020 | 30.23    |
| P33 DS33   | -0.118    | 0.077  | 0.017         | 0.015 | 56.16    |
| P33 PP33   | -0.066    | 0.150  | 0.018         | 0.017 | -46.77   |
| P33 FF35   | -0.001    | 0.180  | 0.018         | 0.016 | 50.64    |
| P33 FF37   | -0.193    | 0.173  | 0.014         | 0.012 | 47.37    |
| RH3 DS13   | -0.167    | -0.212 | 0.025         | 0.025 | 6.01     |
| RH3 FP15   | -0.087    | 0.112  | 0.024         | 0.018 | 59.66    |
| RH3 DS33   | 0.210     | 0.057  | 0.017         | 0.013 | 26.79    |
| RH3 FP35   | -0.064    | -0.299 | 0.015         | 0.013 | -6.43    |
| RH3 FF37   | -0.195    | 0.040  | 0.010         | 0.010 | 86.20    |
| RH1 SS11   | -0.270    | 0.241  | 0.041         | 0.025 | 55.91    |
| RH1 PP13   | 0.411     | -0.240 | 0.033         | 0.014 | 61.18    |
| RH1 SS31   | -0.072    | 0.045  | 0.026         | 0.025 | -4.66    |
| RH1 PP31   | -0.024    | -0.068 | 0.028         | 0.027 | -82.71   |
| SIG PS11   | -0.199    | 0.258  | 0.042         | 0.037 | -53.12   |
| SIG SP11   | 0.222     | 0.010  | 0.046         | 0.042 | 85.82    |
| SIG DP13   | 0.142     | -0.213 | 0.033         | 0.029 | 51.49    |
| SIG FD15   | -0.286    | 0.031  | 0.021         | 0.020 | -50.53   |

TABLE X: 1930 Partial-wave amplitudes with error ellipse parameters (semi-major axis, semi-minor axis, and angle of semi-major axis wrt the x-axis.)

| WAVE LABEL | AMPLITUDE |        | ERROR ELLIPSE |       |          |
|------------|-----------|--------|---------------|-------|----------|
|            | REAL      | IMAG   | MAJOR         | MINOR | ANGLE(°) |
| P33 PP11   | 0.236     | -0.098 | 0.047         | 0.036 | -77.48   |
| P33 DS13   | -0.133    | 0.227  | 0.028         | 0.027 | 80.78    |
| P33 DD13   | 0.077     | -0.168 | 0.030         | 0.030 | 80.23    |
| P33 FP15   | -0.171    | -0.084 | 0.026         | 0.022 | 59.43    |
| P33 DD15   | -0.094    | -0.019 | 0.027         | 0.022 | 88.13    |
| P33 PP31   | 0.059     | -0.006 | 0.033         | 0.033 | -60.46   |
| P33 SD31   | 0.197     | 0.265  | 0.029         | 0.025 | -6.35    |
| P33 DS33   | -0.076    | -0.102 | 0.023         | 0.022 | 2.19     |
| P33 PP33   | -0.061    | 0.044  | 0.030         | 0.021 | -88.89   |
| P33 FF35   | -0.076    | 0.153  | 0.023         | 0.021 | 85.33    |
| P33 FF37   | -0.241    | 0.139  | 0.025         | 0.014 | -84.75   |
| RH3 DS13   | -0.033    | -0.056 | 0.031         | 0.022 | -74.11   |
| RH3 FP15   | -0.150    | -0.007 | 0.020         | 0.019 | -57.34   |
| RH3 DS33   | 0.226     | 0.151  | 0.022         | 0.020 | 74.62    |
| RH3 FP35   | -0.033    | -0.314 | 0.018         | 0.015 | 27.93    |
| RH3 FF37   | -0.207    | -0.094 | 0.017         | 0.013 | 65.13    |
| RH1 SS11   | -0.281    | 0.253  | 0.042         | 0.029 | -86.43   |
| RH1 PP13   | 0.437     | -0.200 | 0.035         | 0.013 | -81.04   |
| RH1 SS31   | 0.165     | 0.002  | 0.038         | 0.035 | 69.89    |
| RH1 PP31   | 0.101     | -0.033 | 0.039         | 0.038 | 14.08    |
| SIG PS11   | -0.396    | 0.037  | 0.043         | 0.030 | -66.80   |
| SIG SP11   | 0.295     | 0.064  | 0.043         | 0.038 | 48.93    |
| SIG DP13   | 0.162     | -0.220 | 0.029         | 0.027 | 84.64    |
| SIG FD15   | -0.225    | 0.046  | 0.025         | 0.024 | -89.14   |

TABLE XI: 1970 Partial-wave amplitudes with error ellipse parameters (semi-major axis, semi-minor axis, and angle of semi-major axis wrt the x-axis.)

| WAVE LABEL | AMPLITUDE |        | ERROR ELLIPSE |       |          |
|------------|-----------|--------|---------------|-------|----------|
|            | REAL      | IMAG   | MAJOR         | MINOR | ANGLE(°) |
| P33 PP11   | 0.160     | -0.260 | 0.042         | 0.030 | -46.79   |
| P33 DS13   | -0.126    | -0.062 | 0.030         | 0.028 | -85.96   |
| P33 DD13   | 0.097     | 0.097  | 0.034         | 0.030 | 55.62    |
| P33 FP15   | -0.181    | -0.039 | 0.024         | 0.020 | 35.71    |
| P33 DD15   | -0.098    | -0.098 | 0.027         | 0.026 | 29.86    |
| P33 PP31   | -0.033    | 0.110  | 0.028         | 0.026 | 30.12    |
| P33 SD31   | 0.211     | 0.214  | 0.025         | 0.019 | 60.88    |
| P33 DS33   | -0.115    | -0.080 | 0.020         | 0.016 | 43.73    |
| P33 PP33   | 0.012     | -0.035 | 0.026         | 0.015 | -89.20   |
| P33 FF35   | -0.107    | 0.150  | 0.019         | 0.016 | 78.64    |
| P33 FF37   | -0.211    | 0.018  | 0.018         | 0.012 | -79.83   |
| RH3 DS13   | 0.041     | -0.293 | 0.022         | 0.022 | -66.04   |
| RH3 FP15   | -0.089    | 0.029  | 0.021         | 0.018 | -76.57   |
| RH3 DS33   | 0.146     | 0.177  | 0.016         | 0.015 | 65.81    |
| RH3 FP35   | 0.069     | -0.263 | 0.015         | 0.012 | -58.78   |
| RH3 FF37   | -0.199    | -0.121 | 0.015         | 0.009 | 48.92    |
| RH1 SS11   | -0.415    | -0.016 | 0.038         | 0.025 | -78.19   |
| RH1 PP13   | 0.467     | 0.035  | 0.017         | 0.013 | -72.40   |
| RH1 SS31   | -0.087    | 0.047  | 0.028         | 0.027 | -58.52   |
| RH1 PP31   | 0.088     | -0.112 | 0.032         | 0.030 | -9.06    |
| SIG PS11   | -0.342    | 0.141  | 0.038         | 0.027 | 78.39    |
| SIG SP11   | 0.169     | -0.108 | 0.047         | 0.037 | -81.45   |
| SIG DP13   | 0.183     | 0.040  | 0.036         | 0.025 | 87.69    |
| SIG FD15   | -0.262    | 0.040  | 0.022         | 0.016 | 80.62    |

TABLE XII This is Table 3 of Almeded and Lovelace<sup>17</sup> with the addition of an extra column giving our channel to which the resonance couples.\*

| Approximate resonance parameters(MeV) |      |                |                            |       |                          |
|---------------------------------------|------|----------------|----------------------------|-------|--------------------------|
| Wave                                  | Mass | $\Gamma_{tot}$ | $\Gamma_{el}/\Gamma_{tot}$ | Grade | Inel. Wave               |
| S31                                   | 1620 | 140            | 0.35                       | A     | $\Delta$ $\rho$          |
| P31                                   | 1900 | 200            | 0.33                       | B     |                          |
| P33(i)                                | 1235 | 129            | 1.0                        | A     |                          |
| P33(ii)                               | 1680 | 220            | 0.1                        | D     |                          |
| P33(iii)                              | 2150 | 200            | 0.3                        | C     |                          |
| D33                                   | 1700 | 260            | 0.16                       | A     | $\Delta$                 |
| D35                                   | 2200 | 260            | 0.25                       | D     |                          |
| F35                                   | 1875 | 250            | 0.18                       | A     | $\rho$                   |
| F37                                   | 1925 | 200            | 0.4                        | A     | $\Delta$ $\rho$          |
| S11(i)                                | 1500 | 50             | 0.25                       | A     |                          |
| S11(ii)                               | 1670 | 120            | 0.5                        | A     | $\rho$ $\sigma$          |
| S11(iii)                              | 2100 | 200            | 0.5                        | D     | $\rho$                   |
| P11(i)                                | 1470 | 220            | 0.65                       | A     |                          |
| P11(ii)                               | 1720 | 160            | 0.2                        | A     | $\Delta$                 |
| P13                                   | 1850 | 300            | 0.25                       | C     | $\rho$                   |
| D13(i)                                | 1520 | 120            | 0.58                       | A     | $\Delta$ $\rho$ $\sigma$ |
| D13(ii)                               | 2075 | 150            | 0.3                        | B     | $\rho$                   |
| D15(i)                                | 1683 | 150            | 0.45                       | A     | $\Delta$                 |
| D15(ii)                               | 2100 | 150            | 0.2                        | C     |                          |
| F15(i)                                | 1688 | 140            | 0.65                       | A     | $\Delta$ $\rho$ $\sigma$ |
| F15(ii)                               | 2175 | 150            | 0.25                       | D     |                          |
| F17                                   | 2000 | 200            | 0.15                       | C     |                          |
| G17                                   | 2225 | 150            | 0.35                       | C     |                          |

\* We have inserted the D13(1700) which is not seen in the elastic channels.

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## FIGURE CAPTIONS

1. 72" HBC  $\pi^- p \rightarrow N \pi \pi$  events per 10 MeV, arrows indicate the energies 1690-70 and 1690+70 (half-widths above and below 1690.) Total of 28111 events.
2. 30" HBC  $\pi^- p \rightarrow N \pi \pi$  events per 10 MeV. Total of 59510 events.
3. Total  $\pi^- p \rightarrow n \pi^- \pi^+$  events per 10 MeV. Total of 41210 events.
4. Total  $\pi^- p \rightarrow p \pi^- \pi^0$  events per 10 MeV. Total of 27306 events.
5. Total  $\pi^+ p \rightarrow p \pi^+ \pi^0$  events per 10 MeV. Total of 45474 events.
6. All events per 10 MeV. Total of 113990 events
7. Summary of kinematic quantities for the general Isobar Model.
8. Final-state factor for the Delta.
9. Final-state factor for the Rho.
10. Final-state factor for the Sigma. Dashed line on  $\delta$  plot from reference 10.
11. Generating amplitudes for the artificial data.
12. Final fitted amplitudes from the artificial data. 12a contains the amplitudes corresponding to the generating set, 12b contains the extra thirteen waves. The box about the origin in figure 12a shows the relative size of figure 12b.
13. Mark 1 cross-sections - experimental values from ref. 14
14. Mark 2 cross-sections - experimental values from ref. 1
15. Mark 3 cross-sections - experimental values from ref. 1
16. Mark 4 cross-sections - experimental values from ref. 14
17. Mark 5 cross-sections - experimental values from ref. 14
18. Comparison of data to prediction for Mark 2 events at 1690
19. Comparison of data to prediction for Mark 3 events at 1690
20. Comparison of data to prediction for Mark 4 events at 1690
21. Comparison of data to prediction for Mark 2 events at 1930

22. Comparison of data to prediction for Mark 3 events at 1930
23. Comparison of data to prediction for Mark 4 events at 1930

All Argand plots have the wave label in the lower left and the scale maximum in the lower right. The number after the energy in the legend is the identification number for that set of waves. These plots also appear in figures 29 - 40 but in a different order.

24. Argand plots for Delta waves with incoming Ispin =  $\frac{1}{2}$
25. Argand plots for Delta waves with incoming Ispin =  $\frac{3}{2}$
26. Argand plots for Rho waves with  $S_j = \frac{3}{2}$
27. Argand plots for Rho waves with  $S_j = \frac{1}{2}$
28. Argand plots for Sigma waves.
29. Argand plots,  $|T|^2$  plots and cross-section plot for S11
30. Argand plots,  $|T|^2$  plots and cross-section plot for P11
31. Argand plots,  $|T|^2$  plots and cross-section plot for P13
32. Argand plots,  $|T|^2$  plots and cross-section plot for D13
33. Argand plots,  $|T|^2$  plots and cross-section plot for D15
34. Argand plots,  $|T|^2$  plots and cross-section plot for F15
35. Argand plots,  $|T|^2$  plots and cross-section plot for S31
36. Argand plots,  $|T|^2$  plots and cross-section plot for P31
37. Argand plots,  $|T|^2$  plots and cross-section plot for P33
38. Argand plots,  $|T|^2$  plots and cross-section plot for D33
39. Argand plots,  $|T|^2$  plots and cross-section plot for F35
40. Argand plots,  $|T|^2$  plots and cross-section plot for F37

-37-

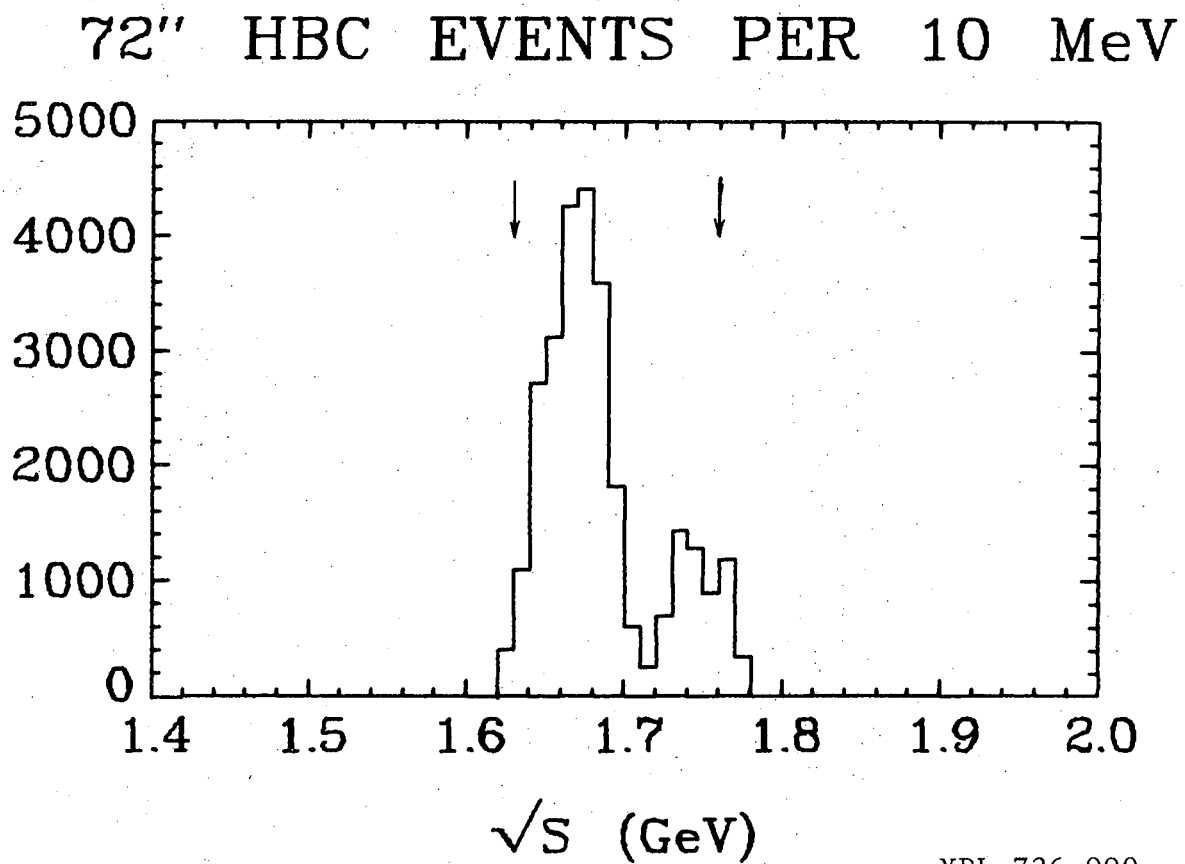
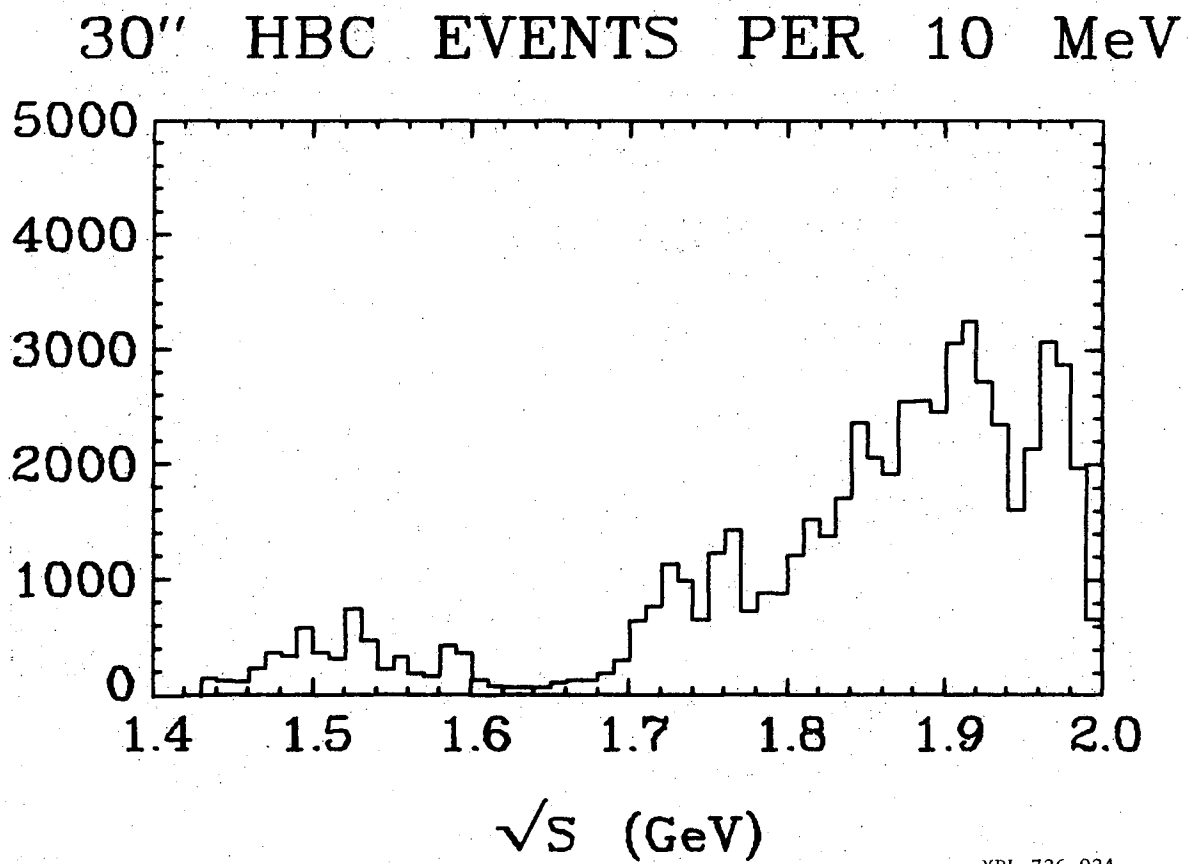


Fig. 1.

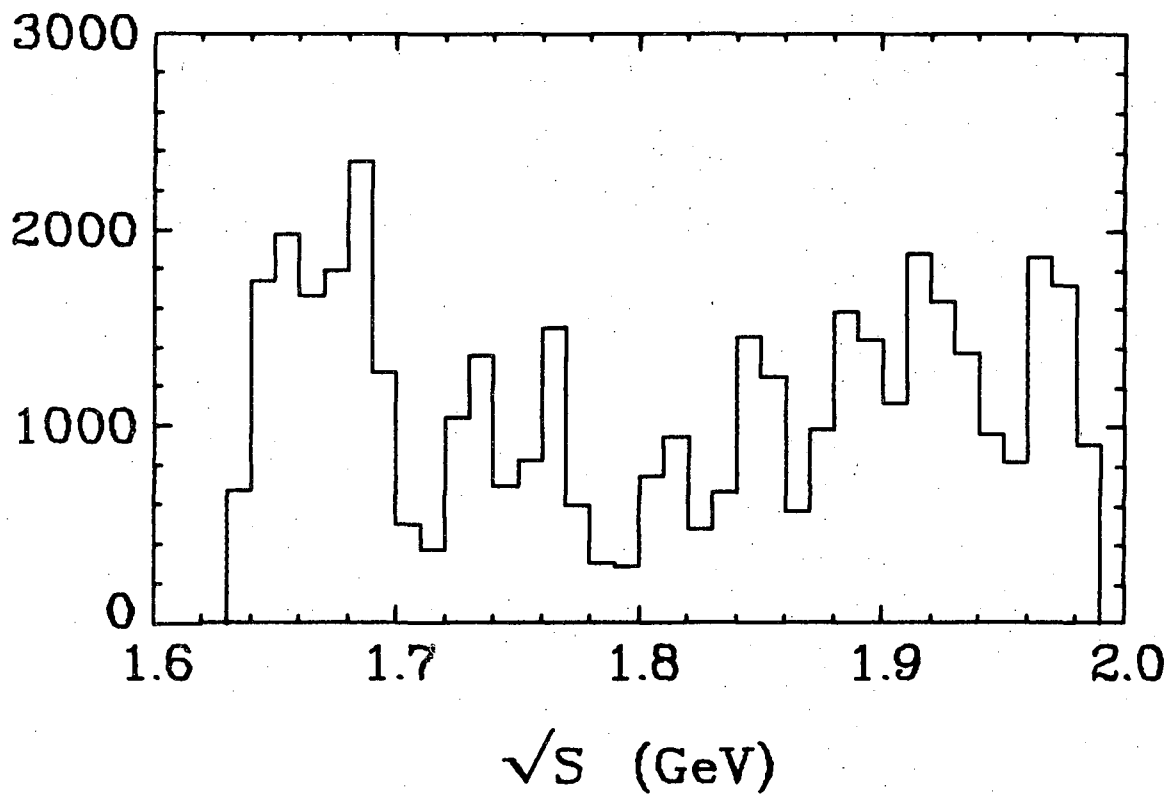


XBL 726-924

Fig. 2.



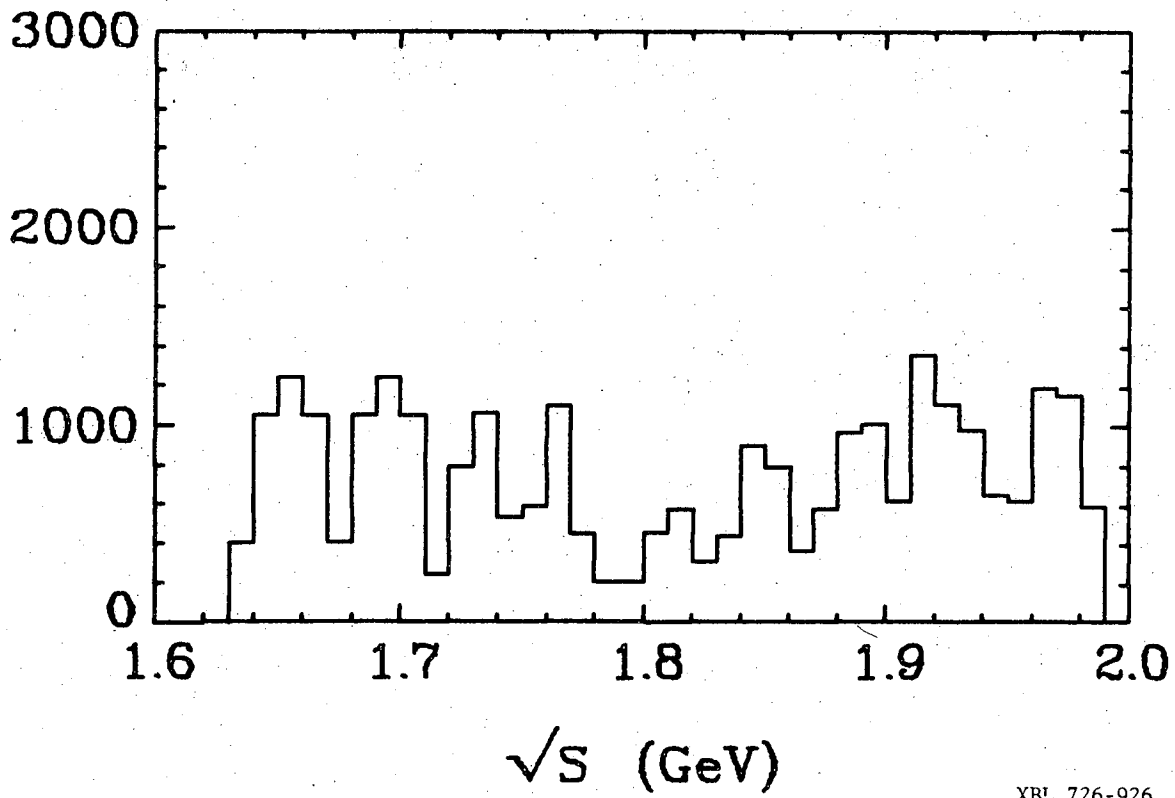
# MARK 2 EVENTS PER 10 MeV



XBL 726-925

Fig. 3.

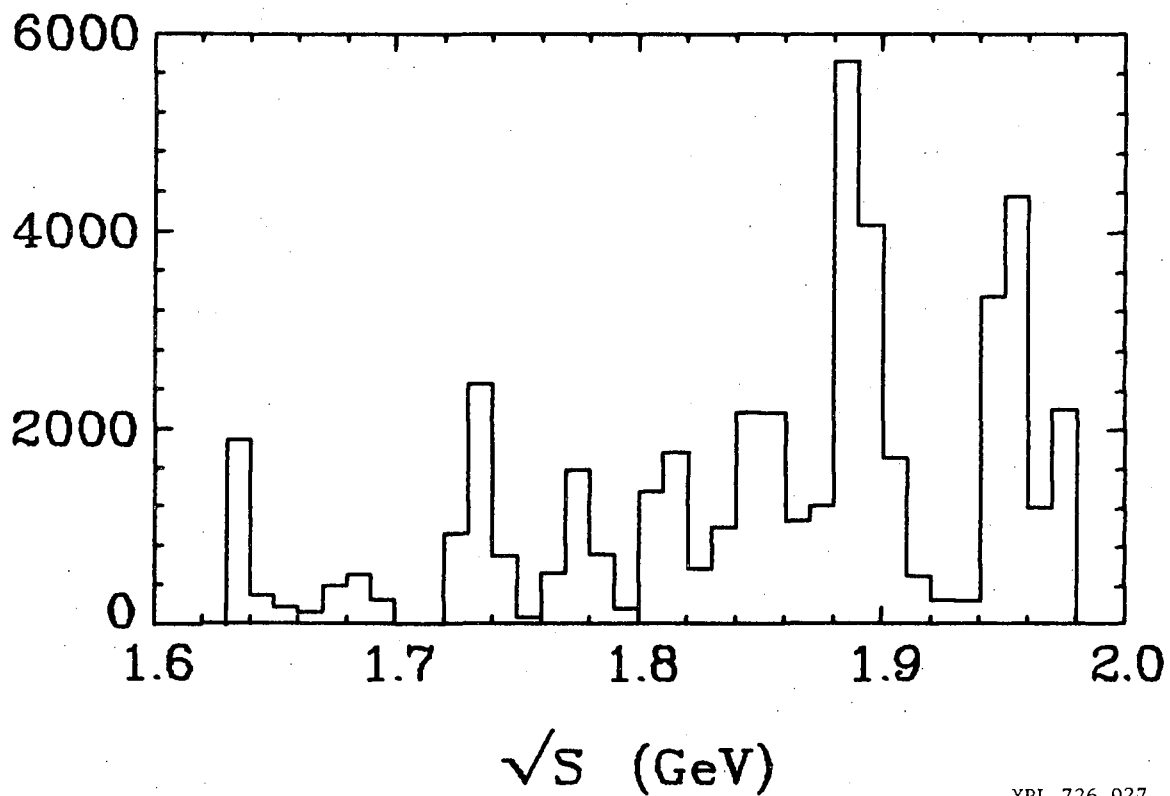
# MARK 3 EVENTS PER 10 MeV



XBL 726-926

Fig. 4.

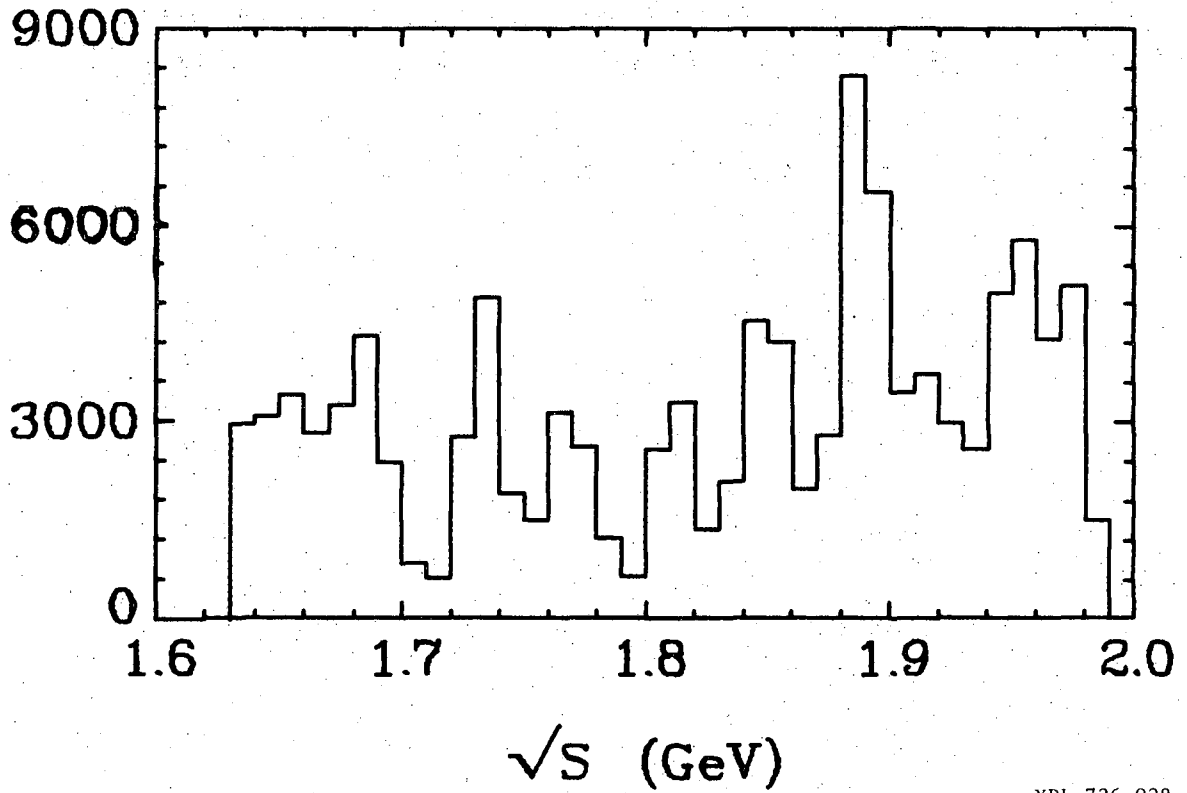
### MARK 4 EVENTS PER 10 MeV



XBL 726-927

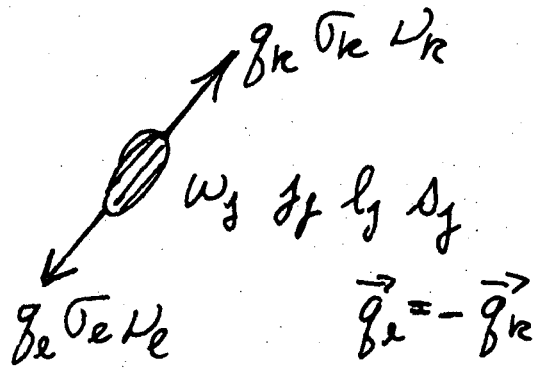
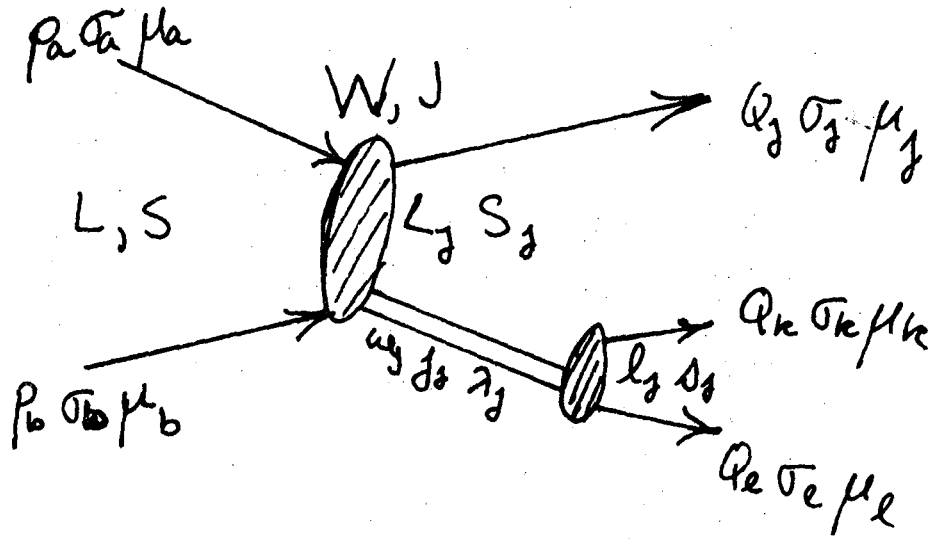
Fig. 5.

### TOTAL EVENTS PER 10 MeV



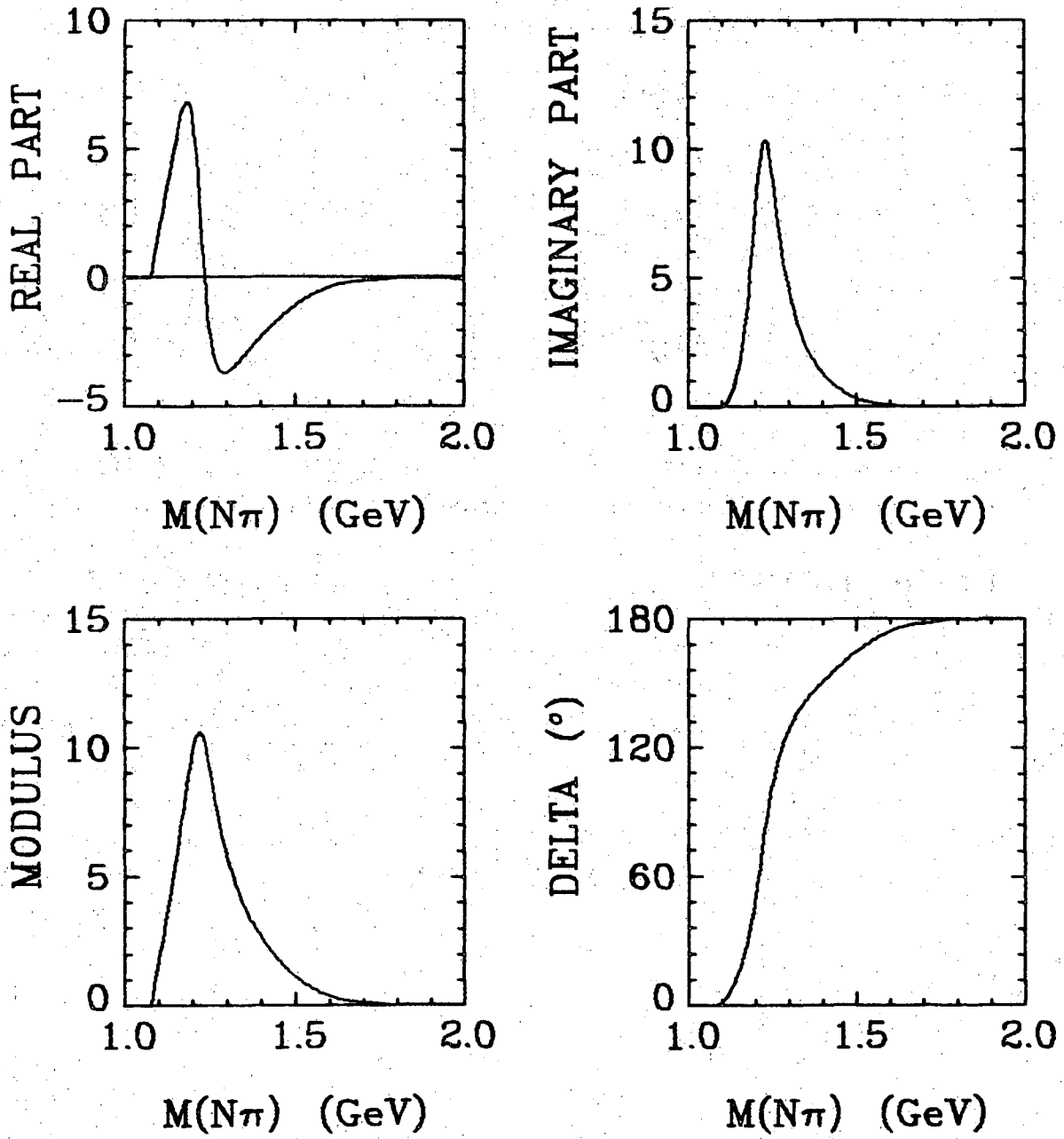
XBL 726-928

Fig. 6.



XBL 726-929

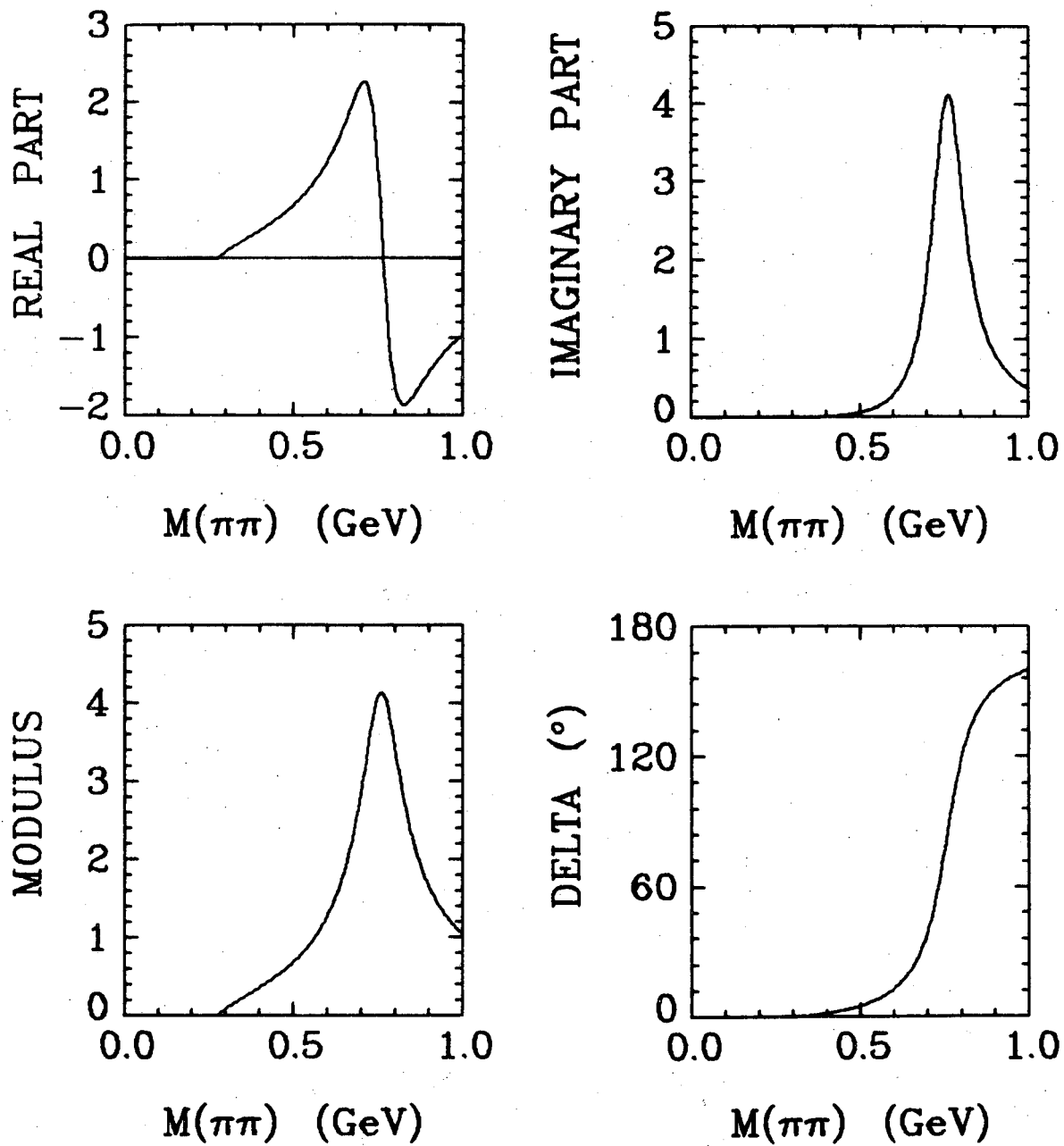
Fig. 7.



XBL 726-930

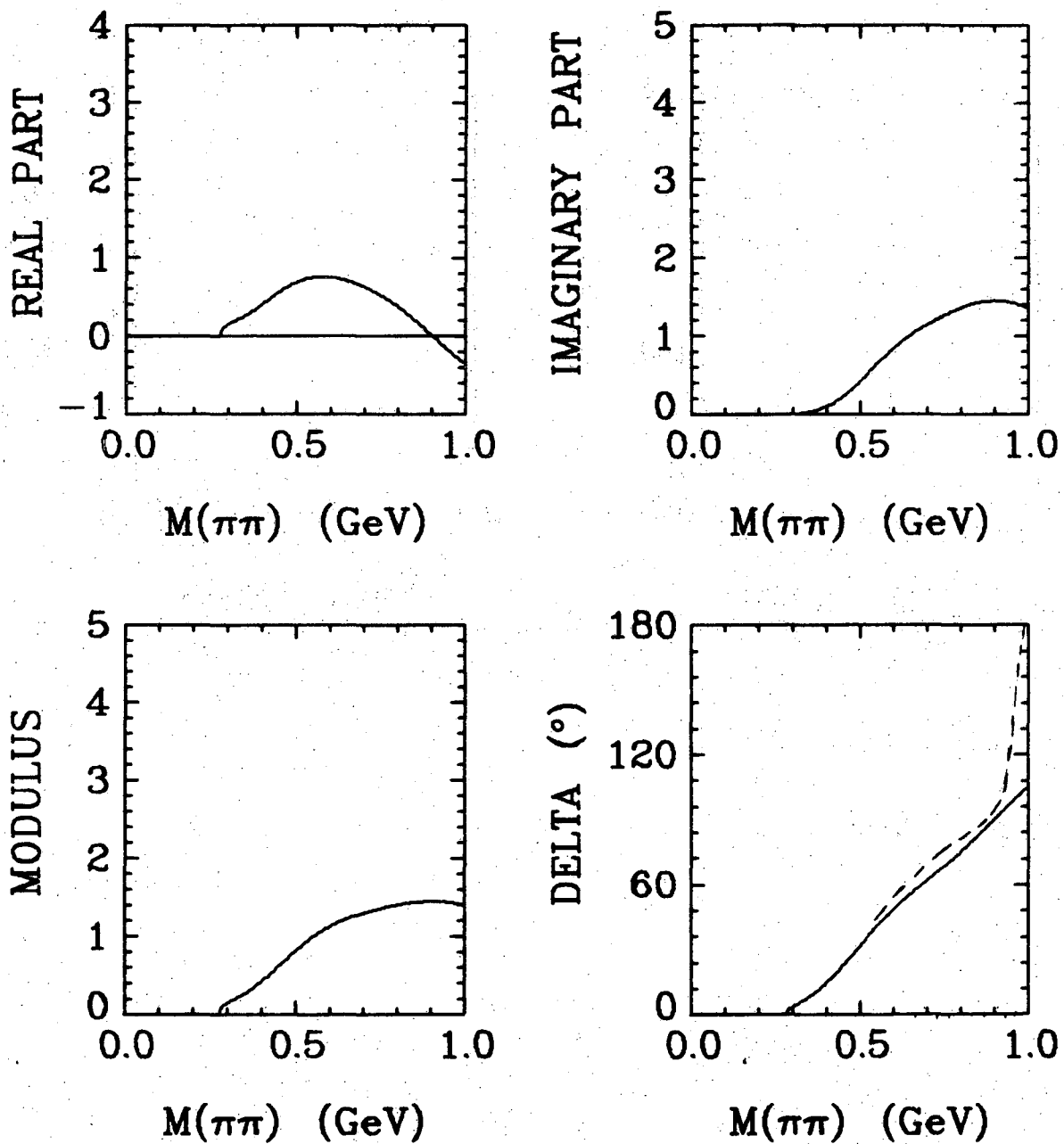
Fig. 8.

-45-



XBL 726-931

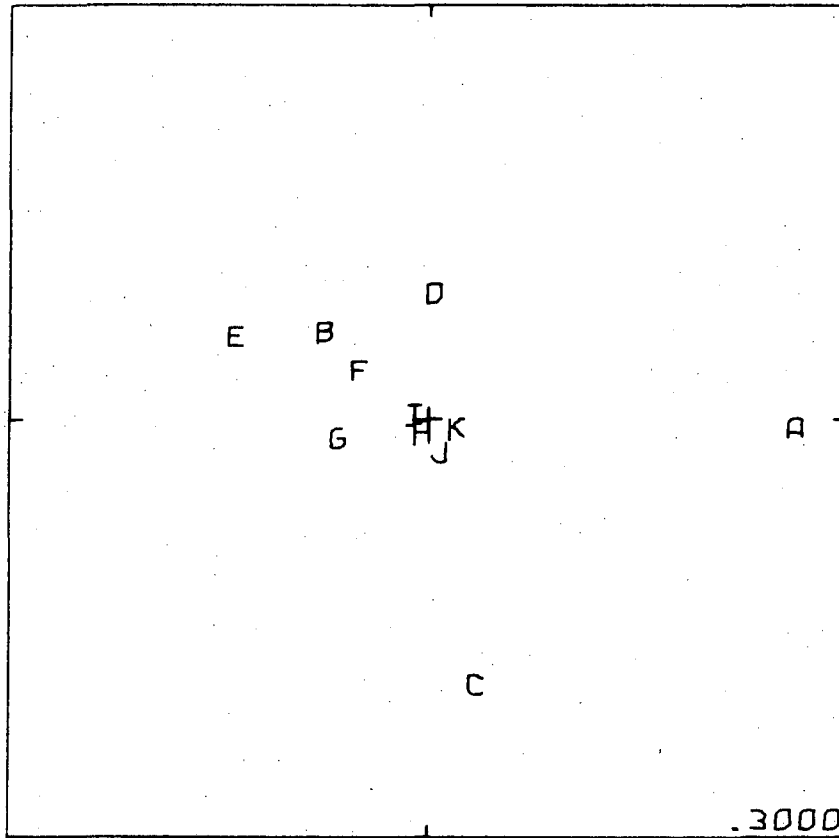
Fig. 9.



XBL 726-932

Fig. 10.



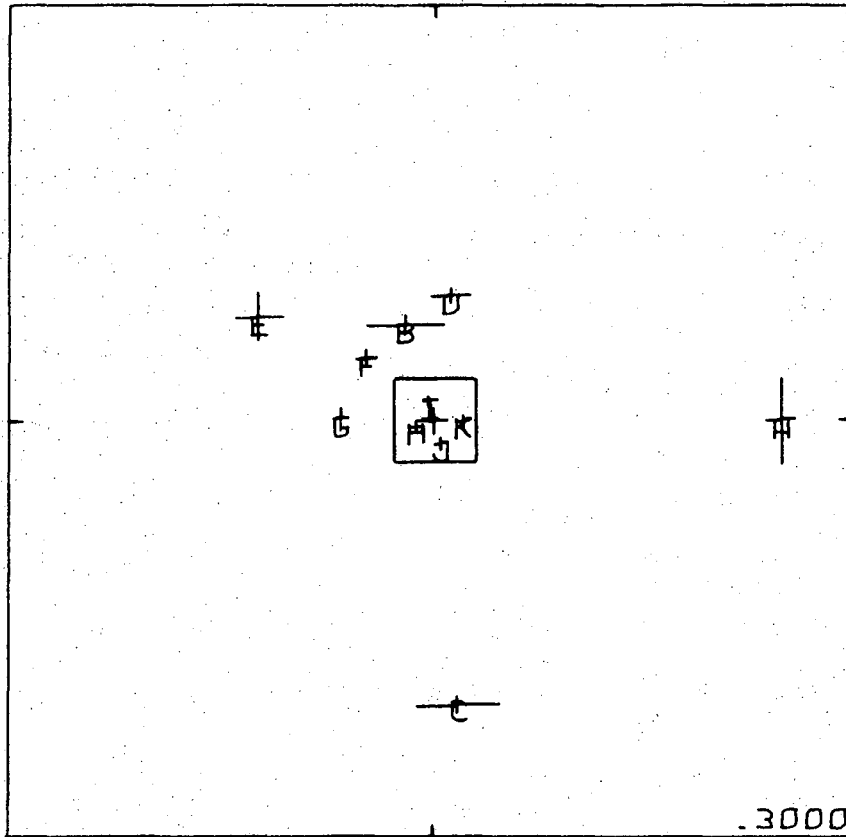


|   |     |      |
|---|-----|------|
| A | P33 | PP11 |
| B | P33 | SD11 |
| C | P33 | DD13 |
| D | P33 | DD15 |
| E | P33 | SD31 |
| F | RH3 | DS13 |
| G | RH3 | PP13 |
| H | RH3 | DD13 |
| I | RH3 | PF13 |
| J | SIG | FD15 |
| K | SIG | DF15 |

GENERATING AMPLITUDES

XBL 726-933

Fig. 11.

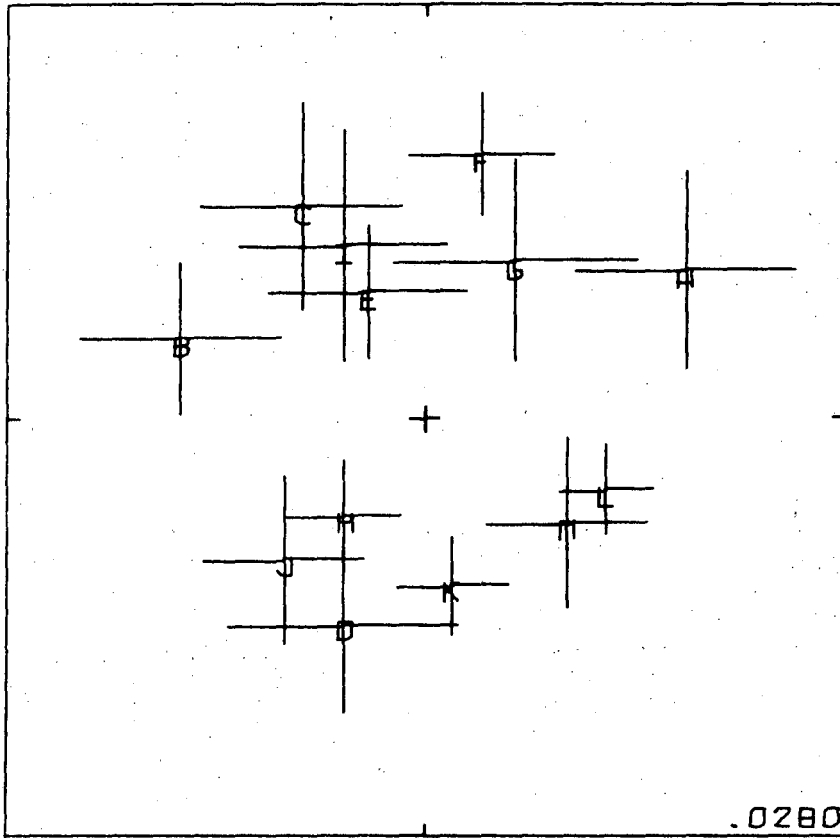


|   |     |      |
|---|-----|------|
| A | P33 | PP11 |
| B | P33 | SD11 |
| C | P33 | DD13 |
| D | P33 | DD15 |
| E | P33 | SD31 |
| F | RH3 | DS13 |
| G | RH3 | PP13 |
| H | RH3 | DD13 |
| I | RH3 | PF13 |
| J | SIG | FD15 |
| K | SIG | DF15 |

FITTED AMPLITUDES

XBL 726-934

Fig. 12a.



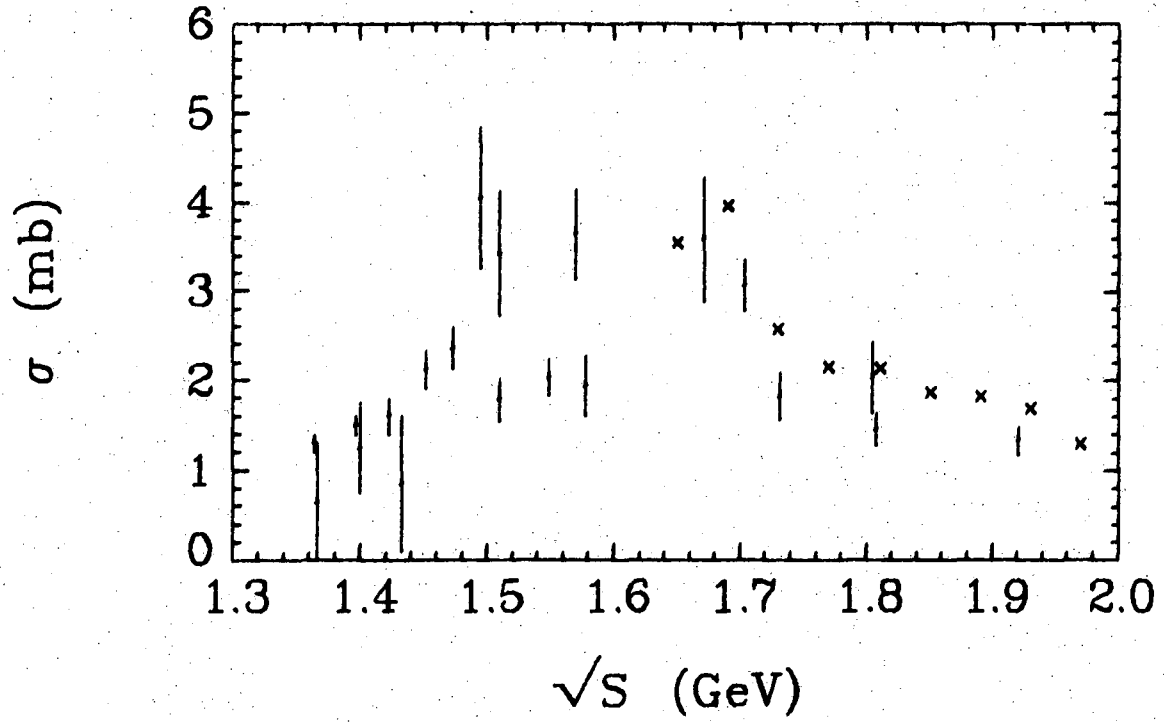
- A P33 DS13
- B P33 FF15
- C P33 DS33
- D P33 DD33
- E P33 FF35
- F P33 FF37
- G RH3 SD11
- H RH3 FP15
- I RH3 PP31
- J RH3 DS33
- K RH3 FF35
- L RH1 FF37
- M SIG PD13

FITTED AMPLITUDES

XBL 726-935

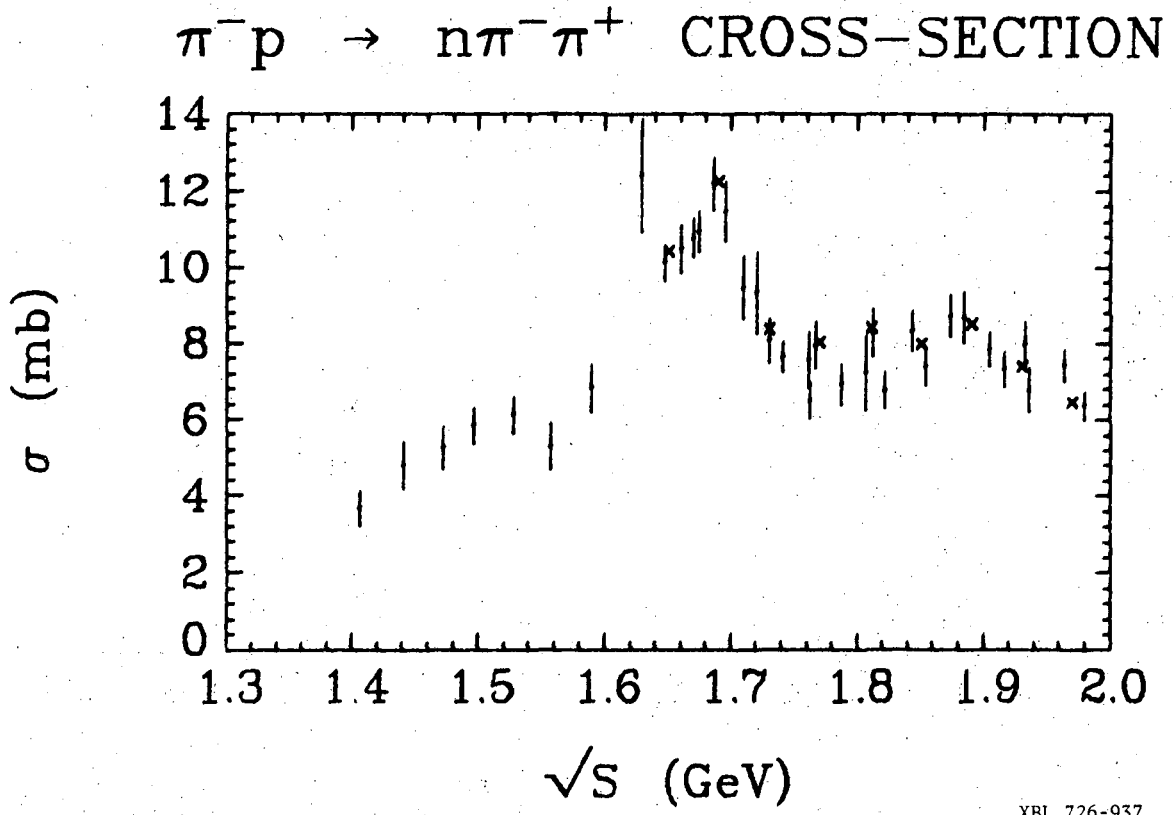
Fig. 12b.

$\pi^- p \rightarrow n\pi^0\pi^0$  CROSS-SECTION



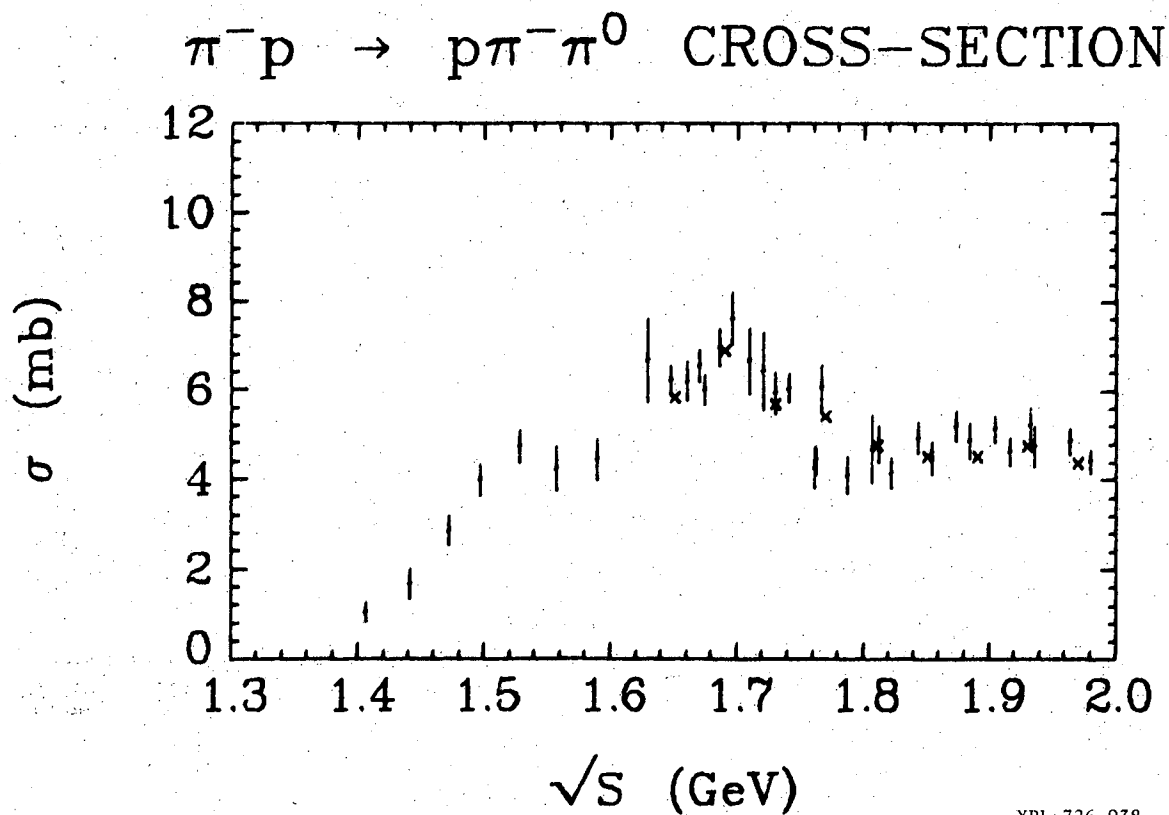
XBL 726-936

Fig. 13.



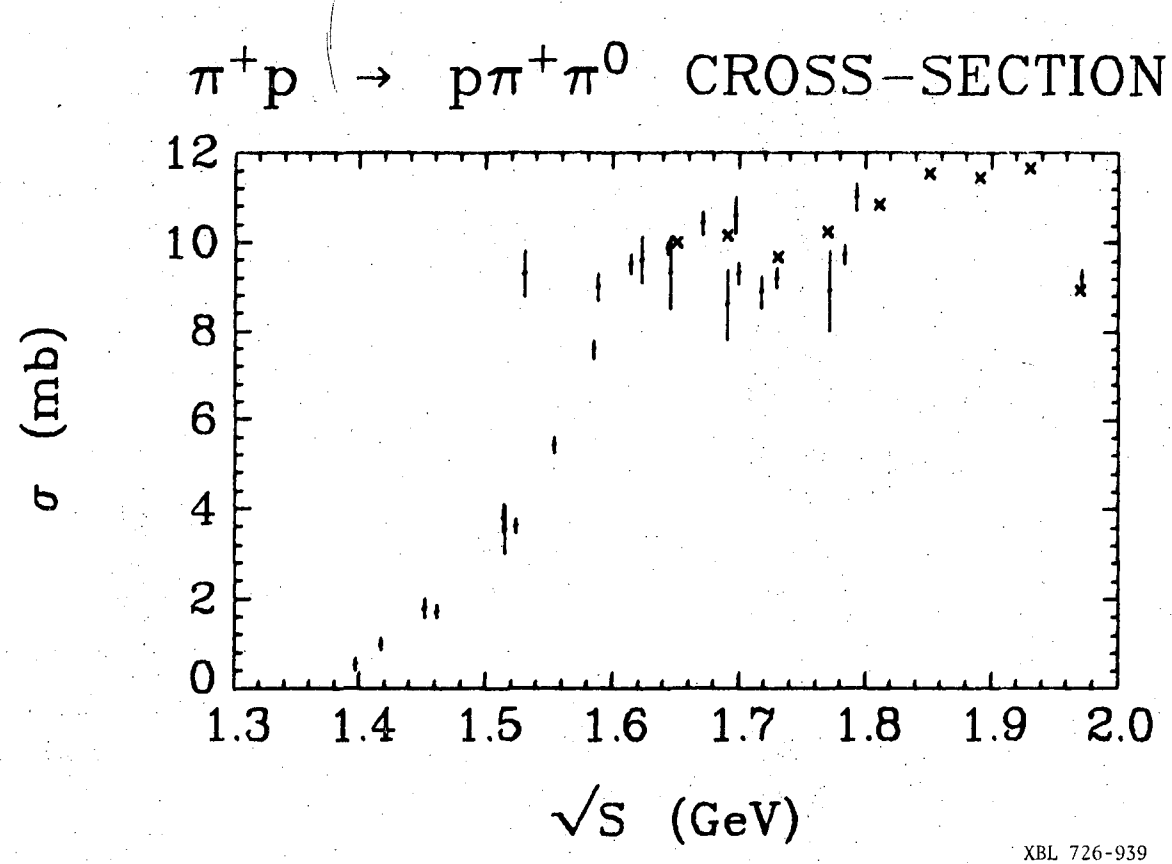
XBL 726-937

Fig. 14.



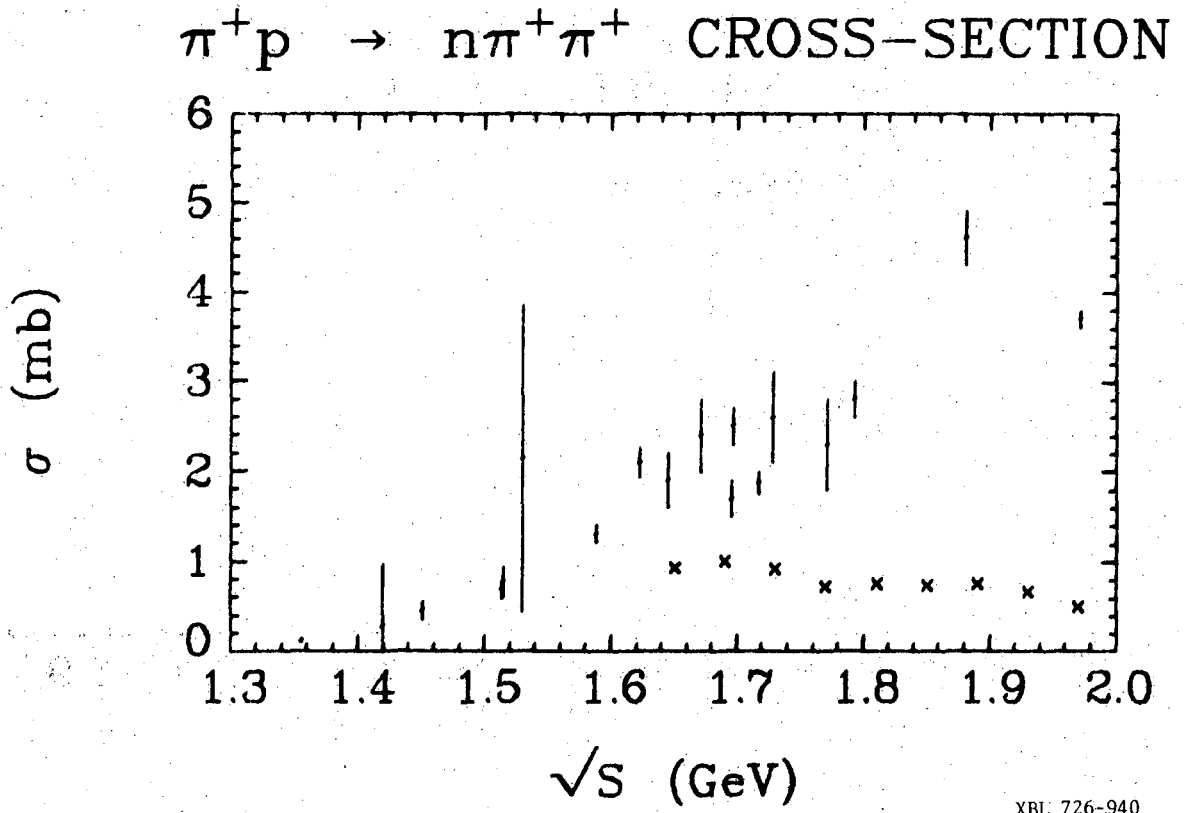
XBL 726-938

Fig. 15.



XBL 726-939

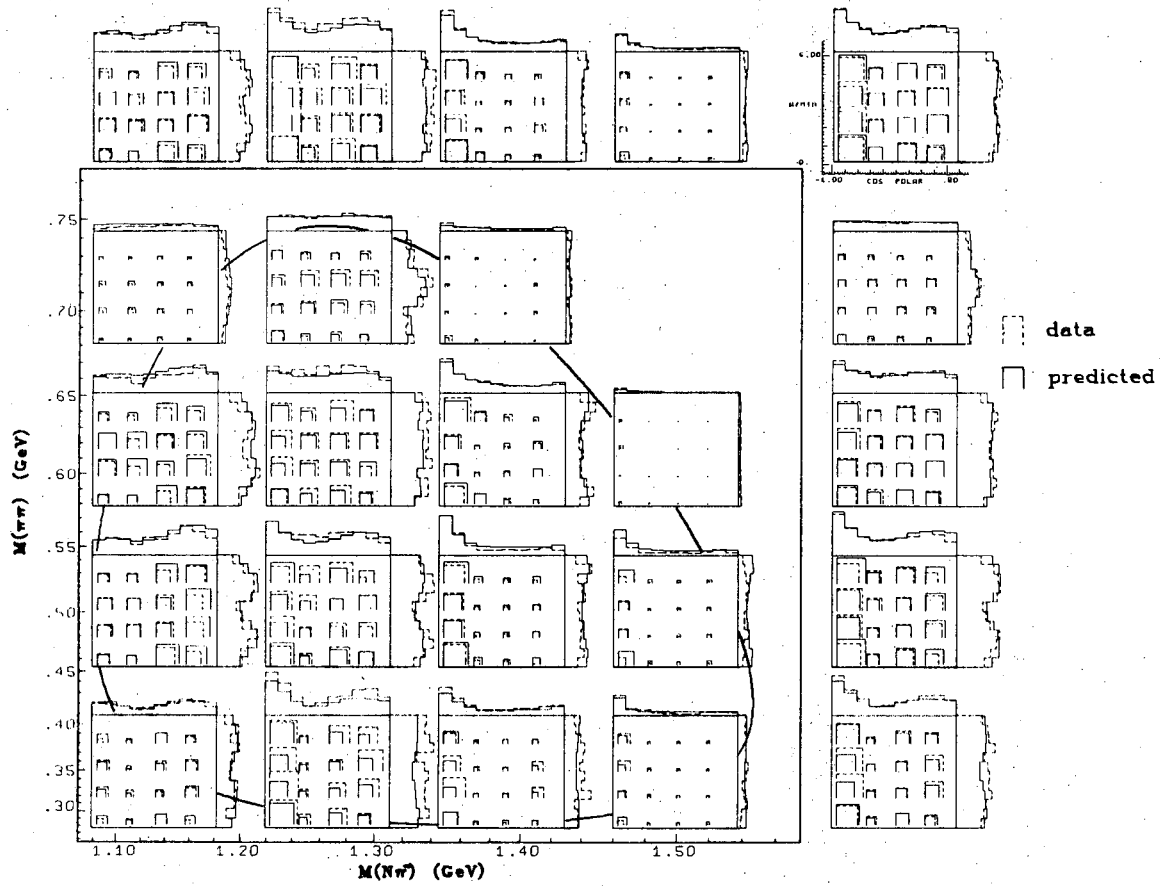
Fig. 16.



XBL 726-940

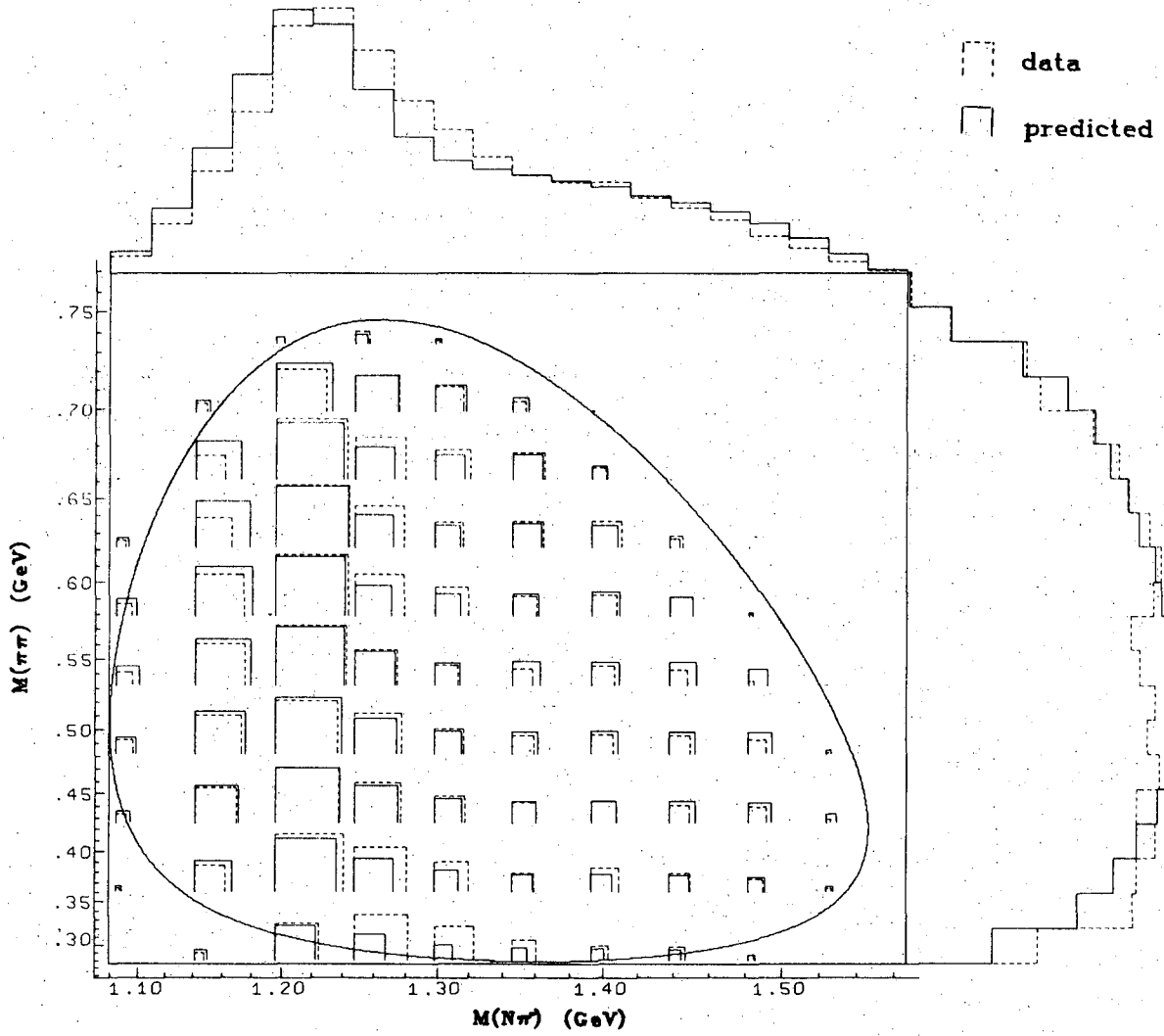
Fig. 17.





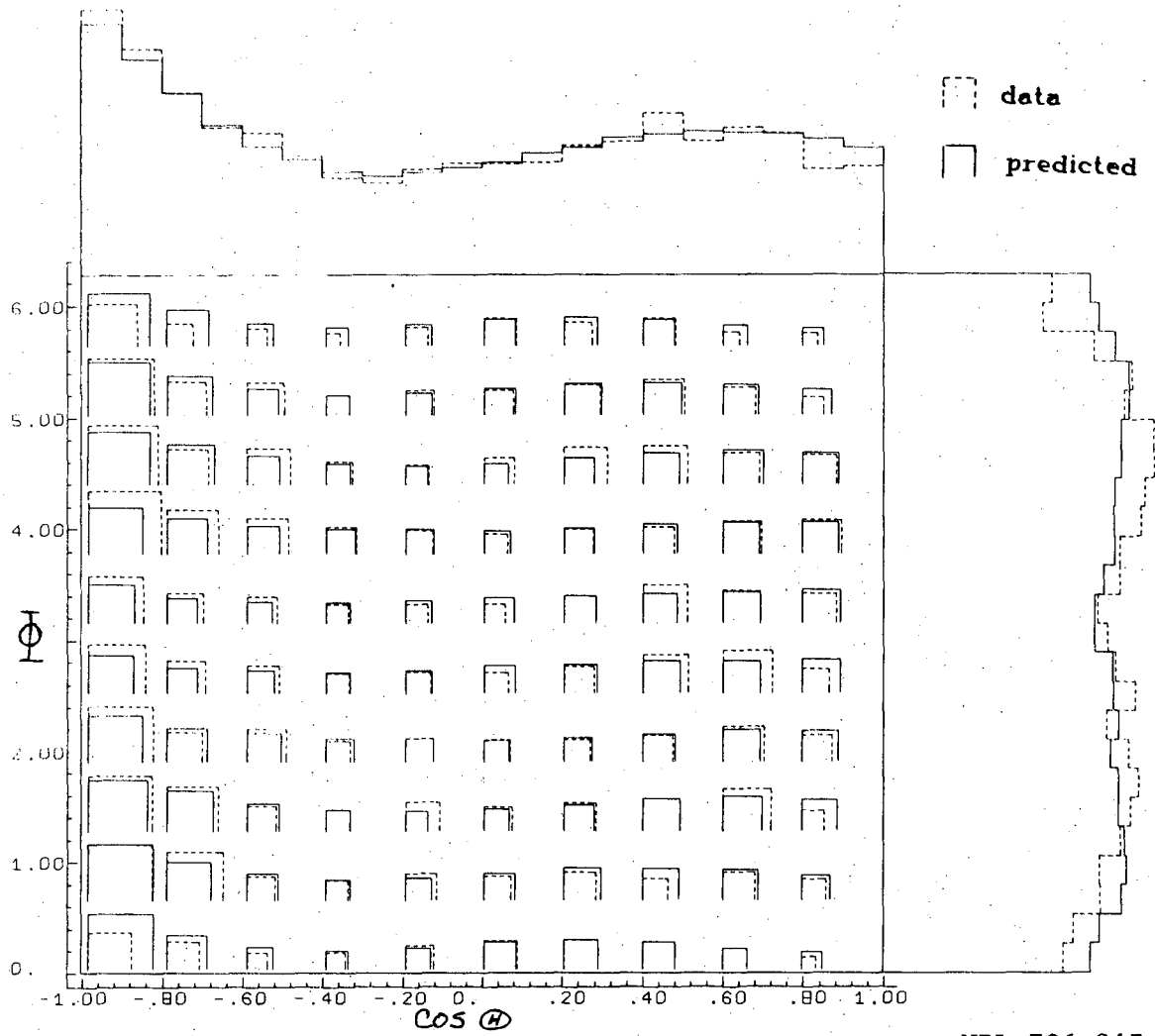
XBL 726-941

Fig.18a.



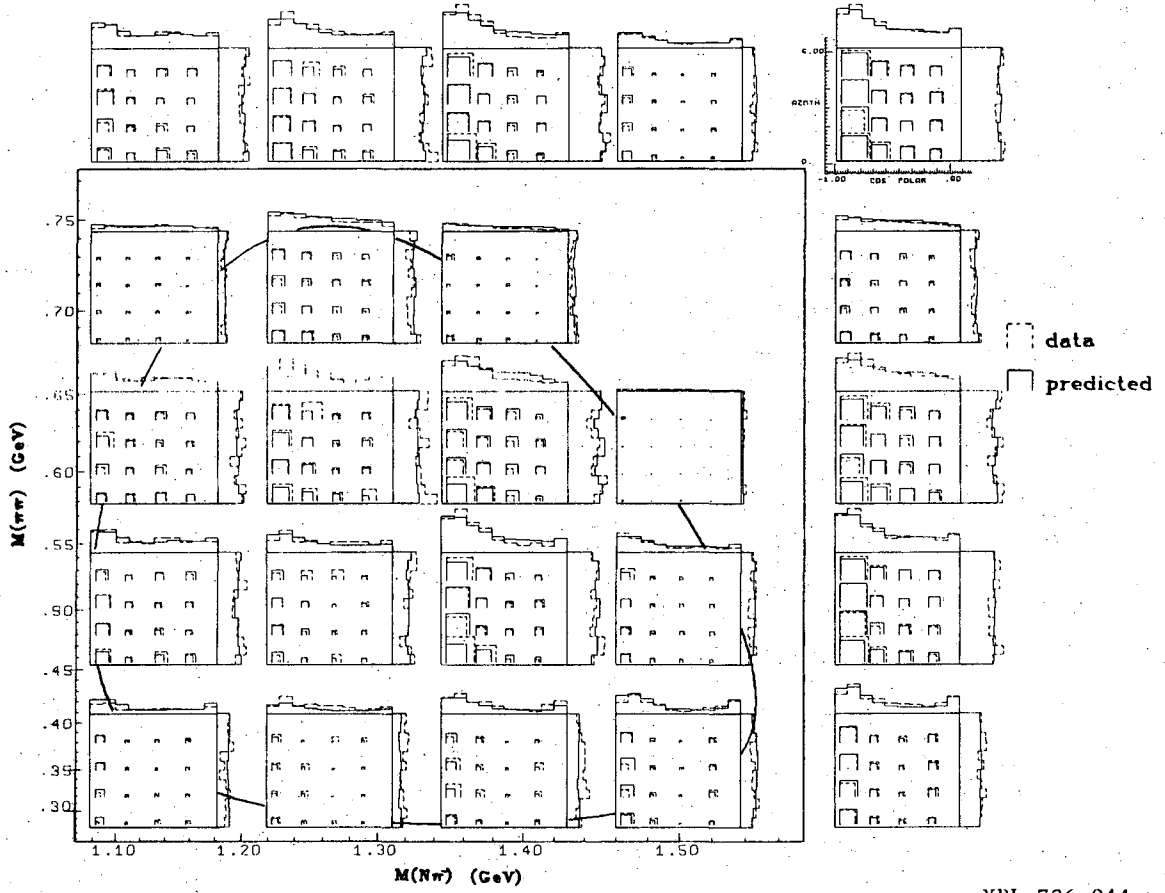
XBL 726-942

Fig. 18b.



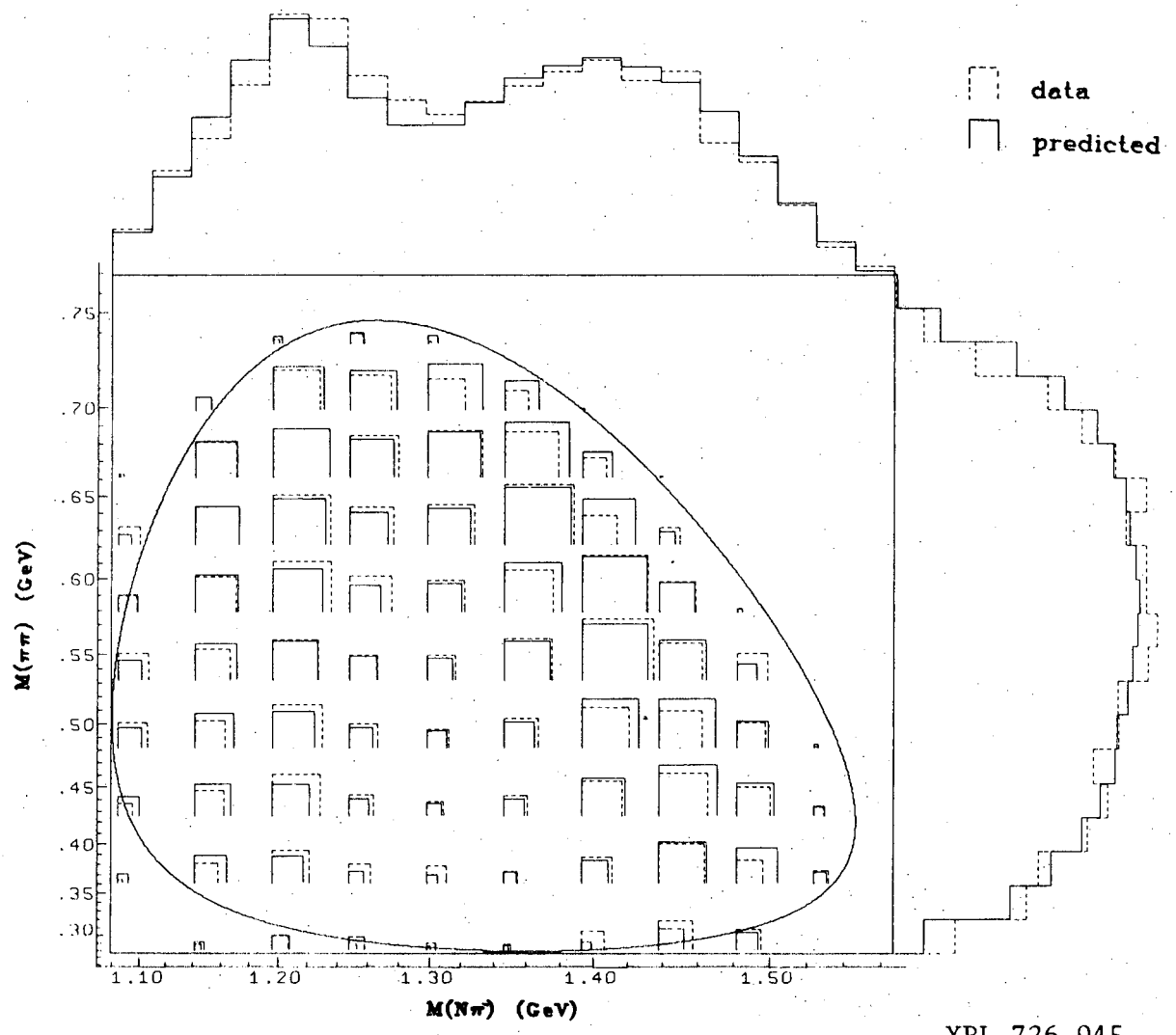
XBL 726-943

Fig. 18c.



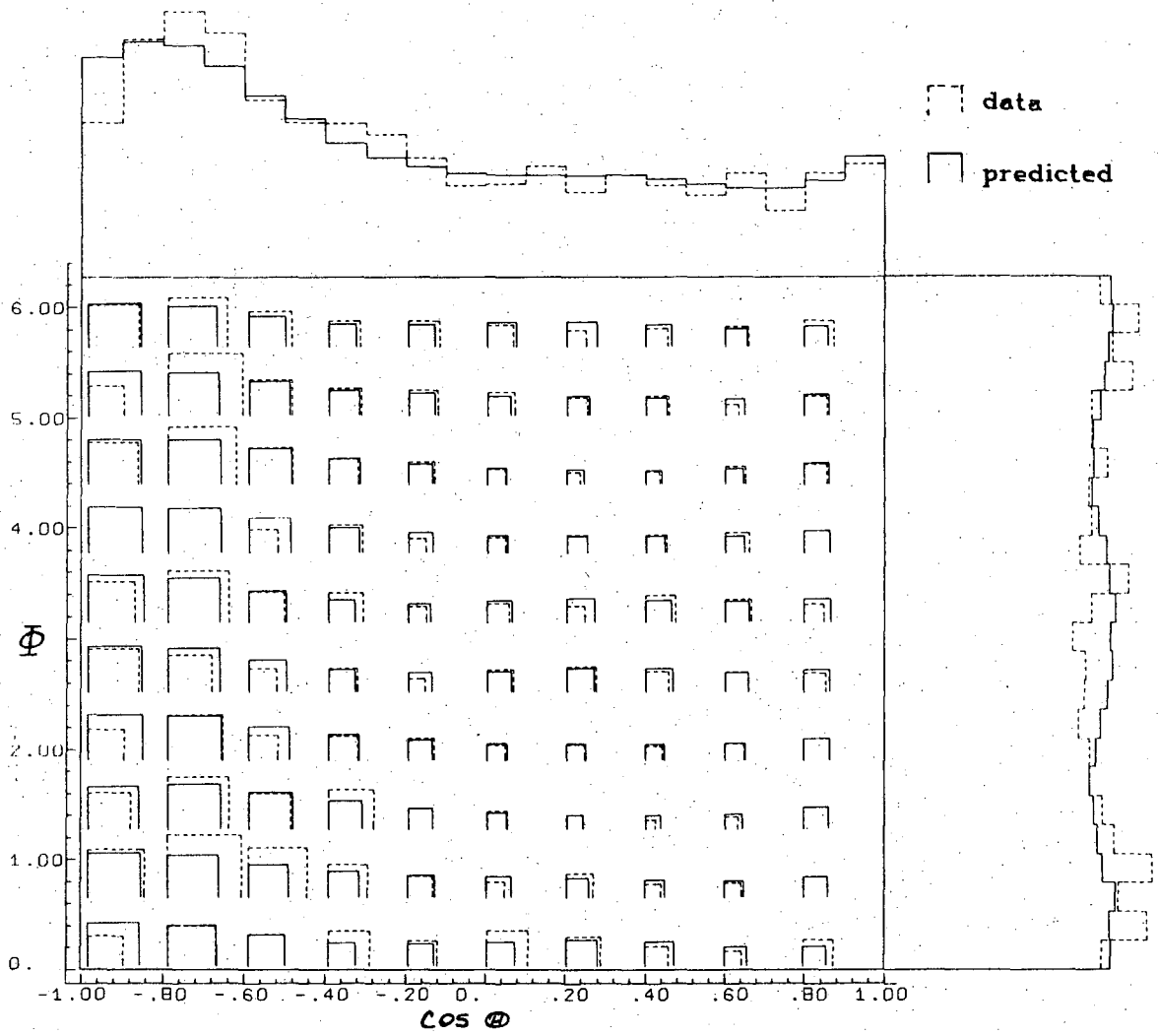
XBL 726-944

Fig. 19a.



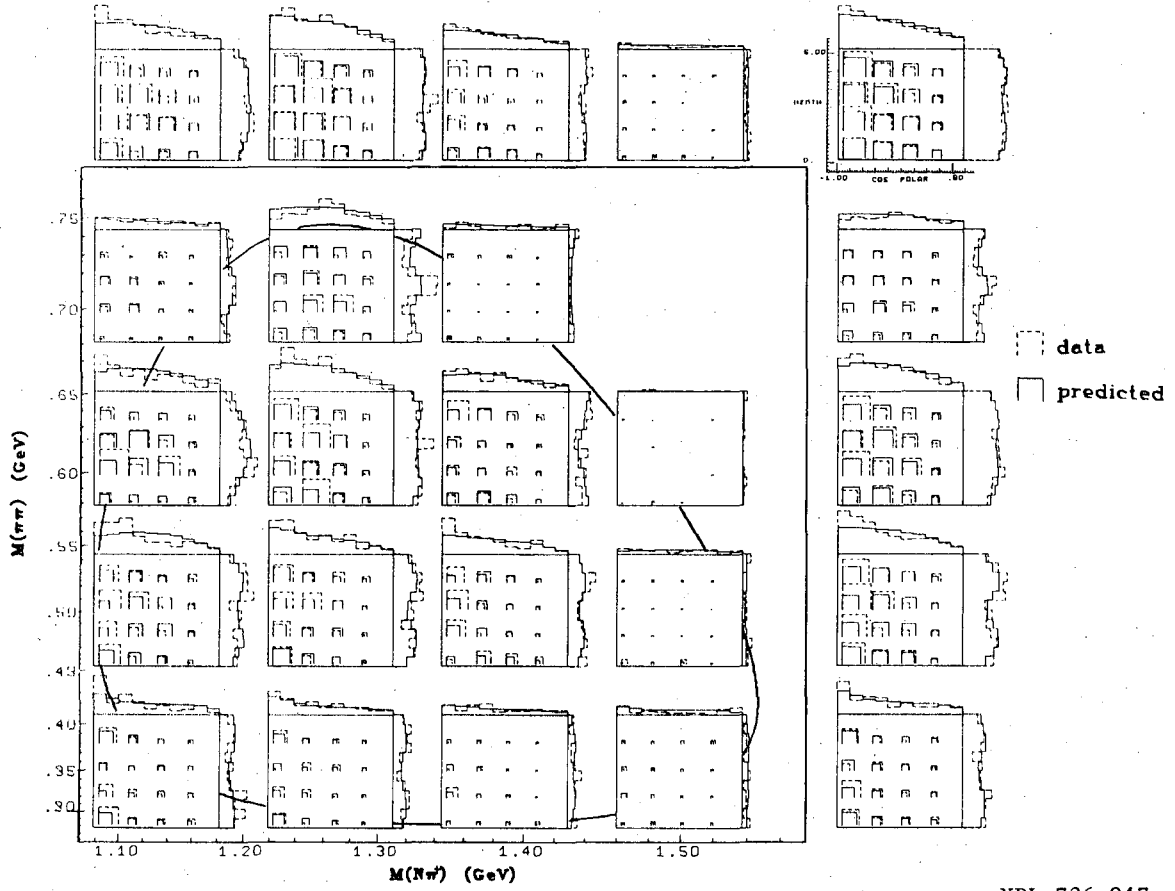
XBL 726-945

Fig. 19b.



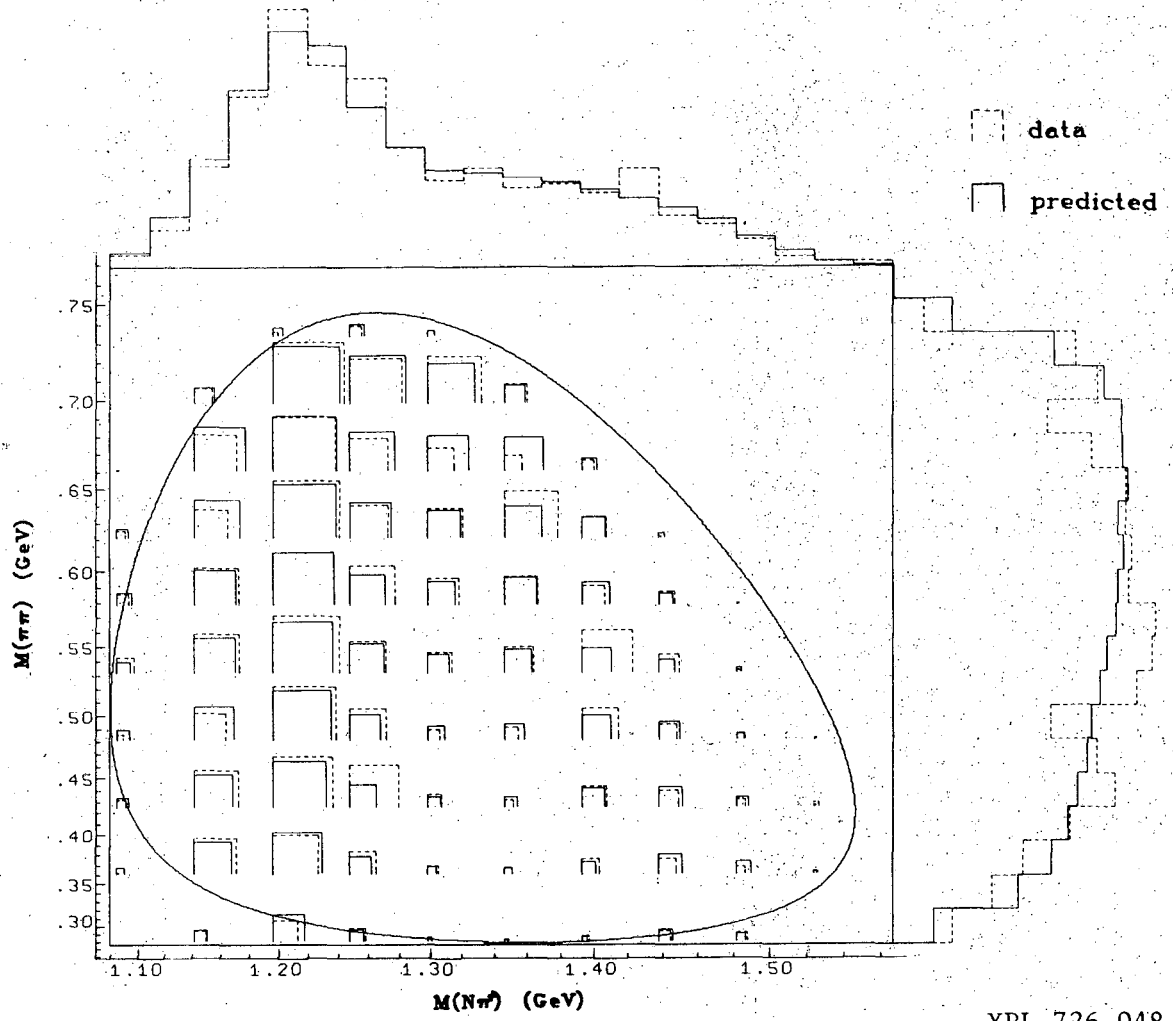
XBL 726-946

Fig. 19c.



XBL 726-947

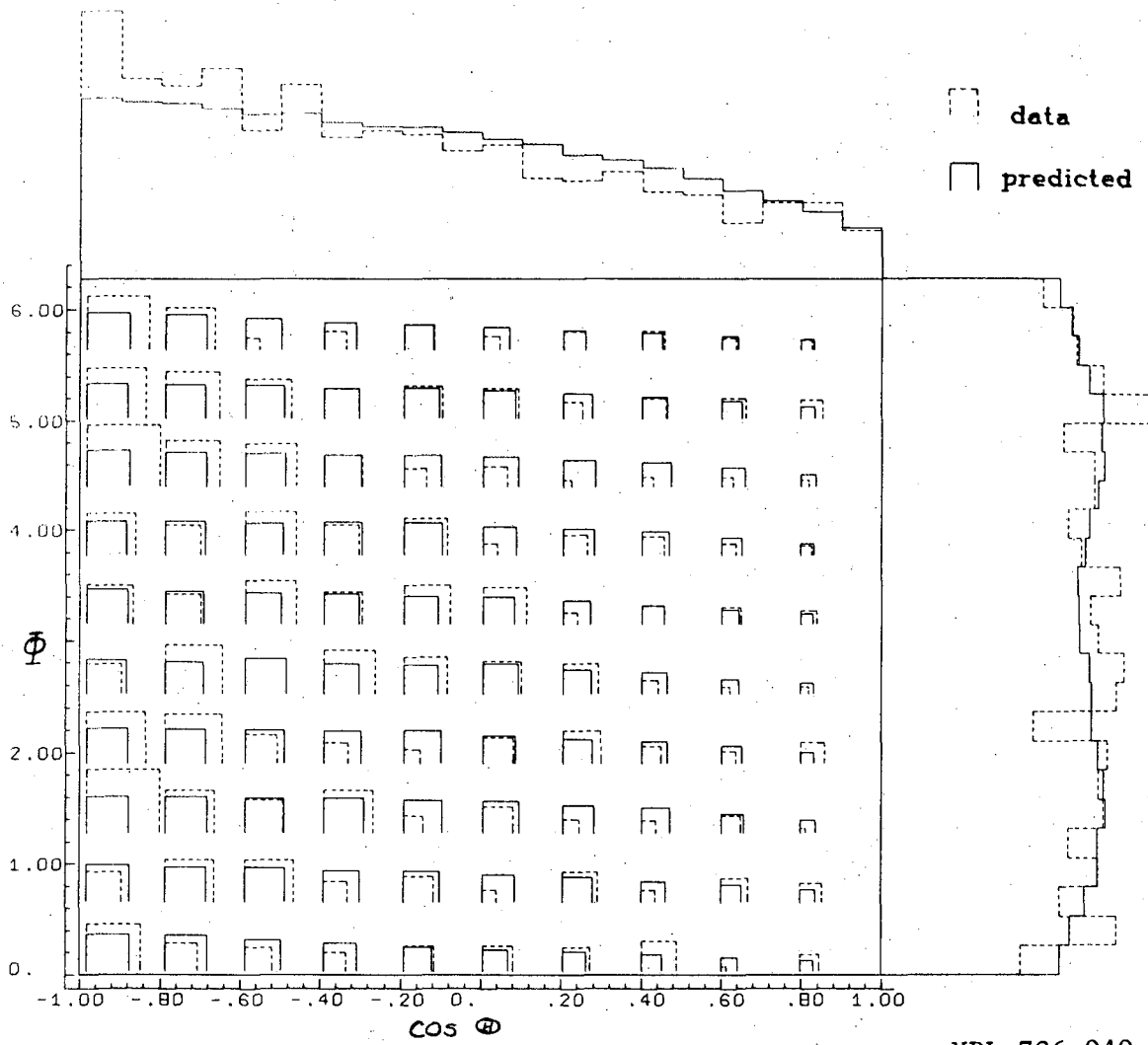
Fig. 20a.



XBL 726-948

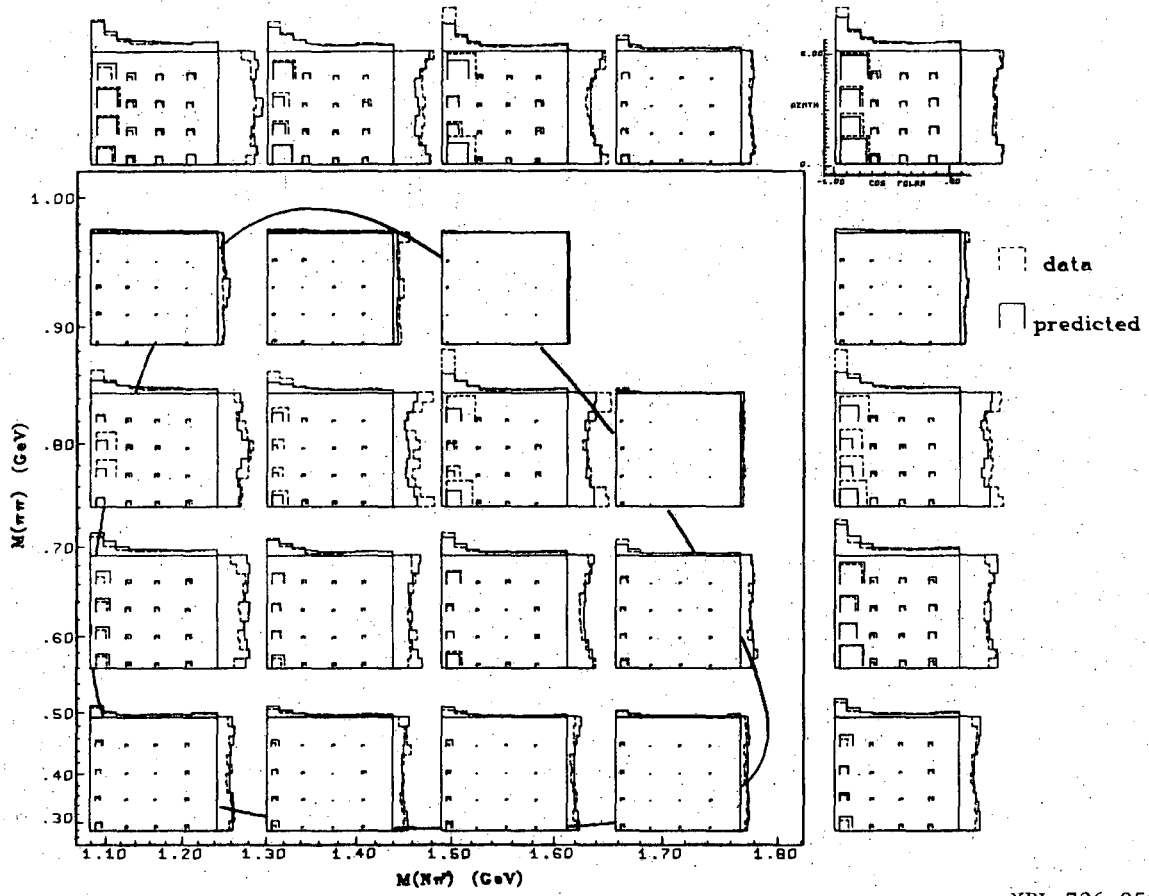
Fig. 20b.





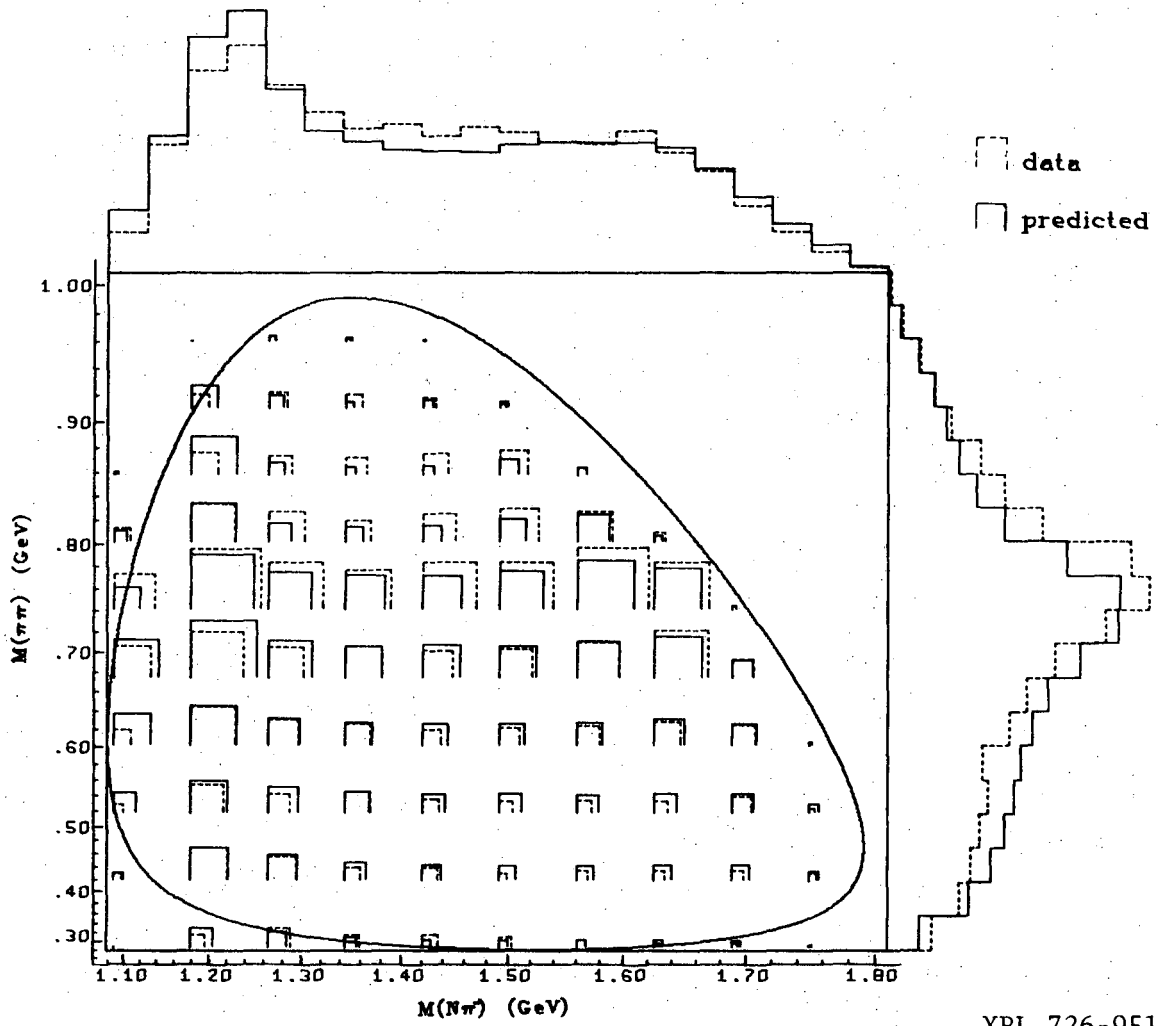
XBL 726-949

Fig. 20c.



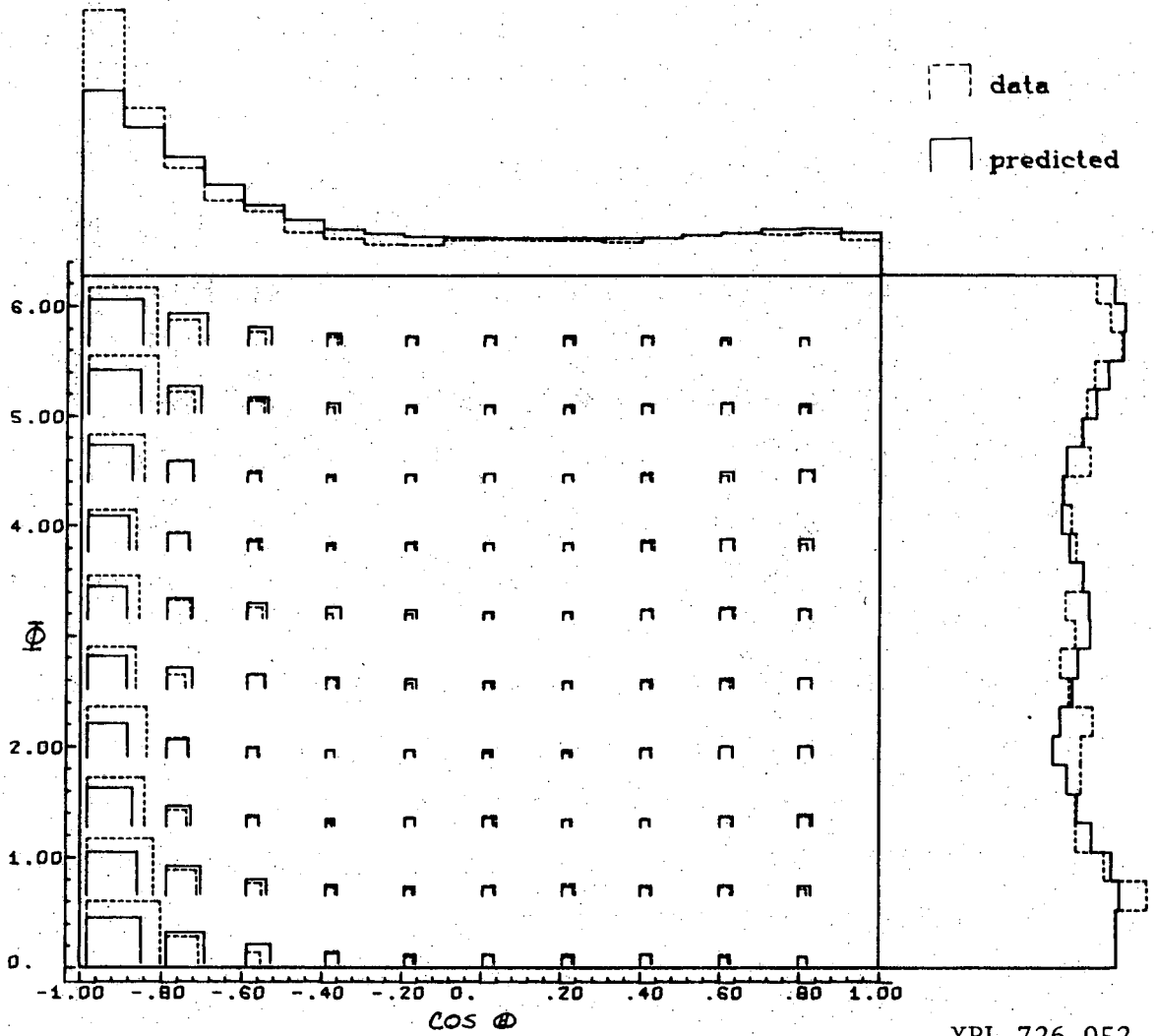
XBL 726-950

Fig. 21a.



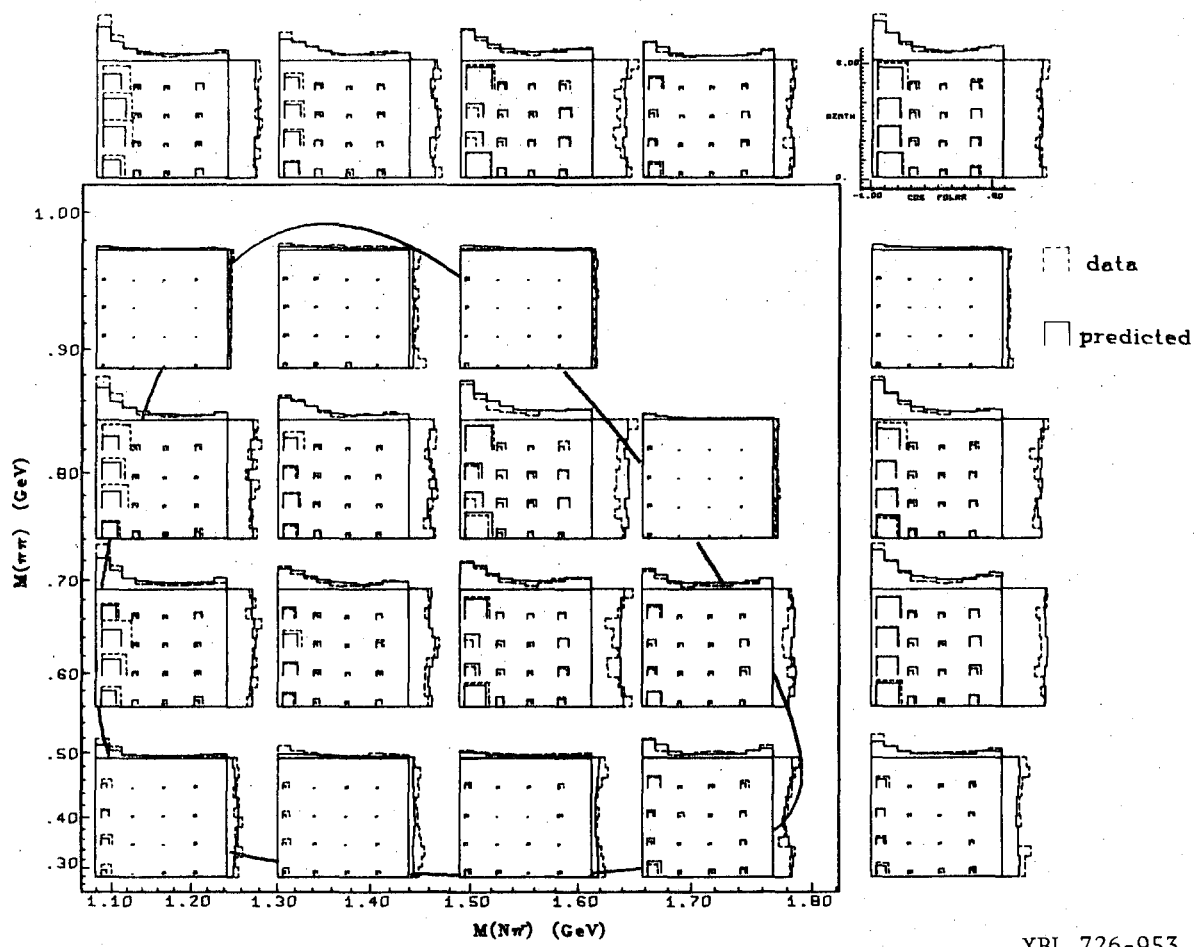
XBL 726-951

Fig. 21b.



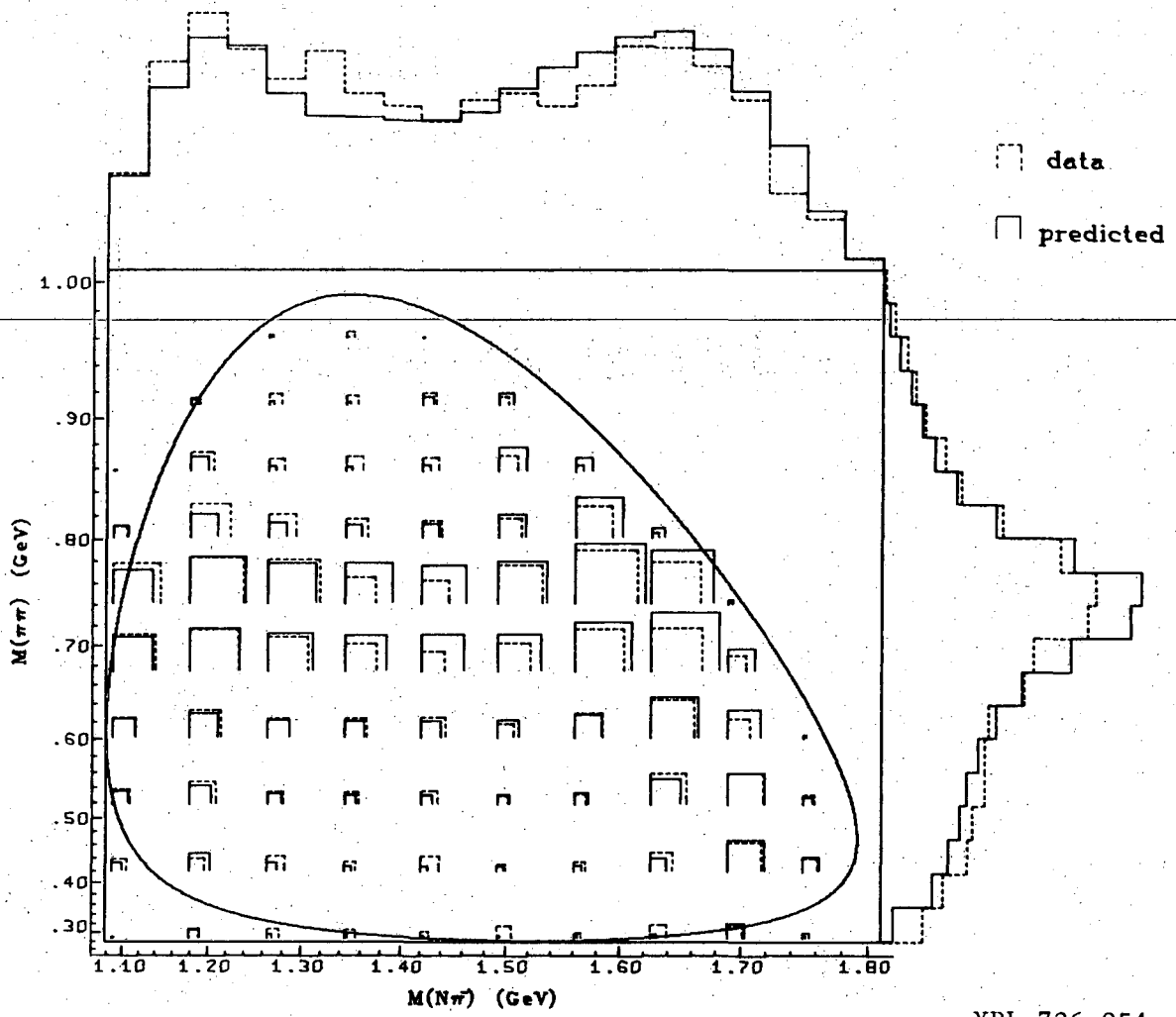
XBL 726-952

Fig. 21c.



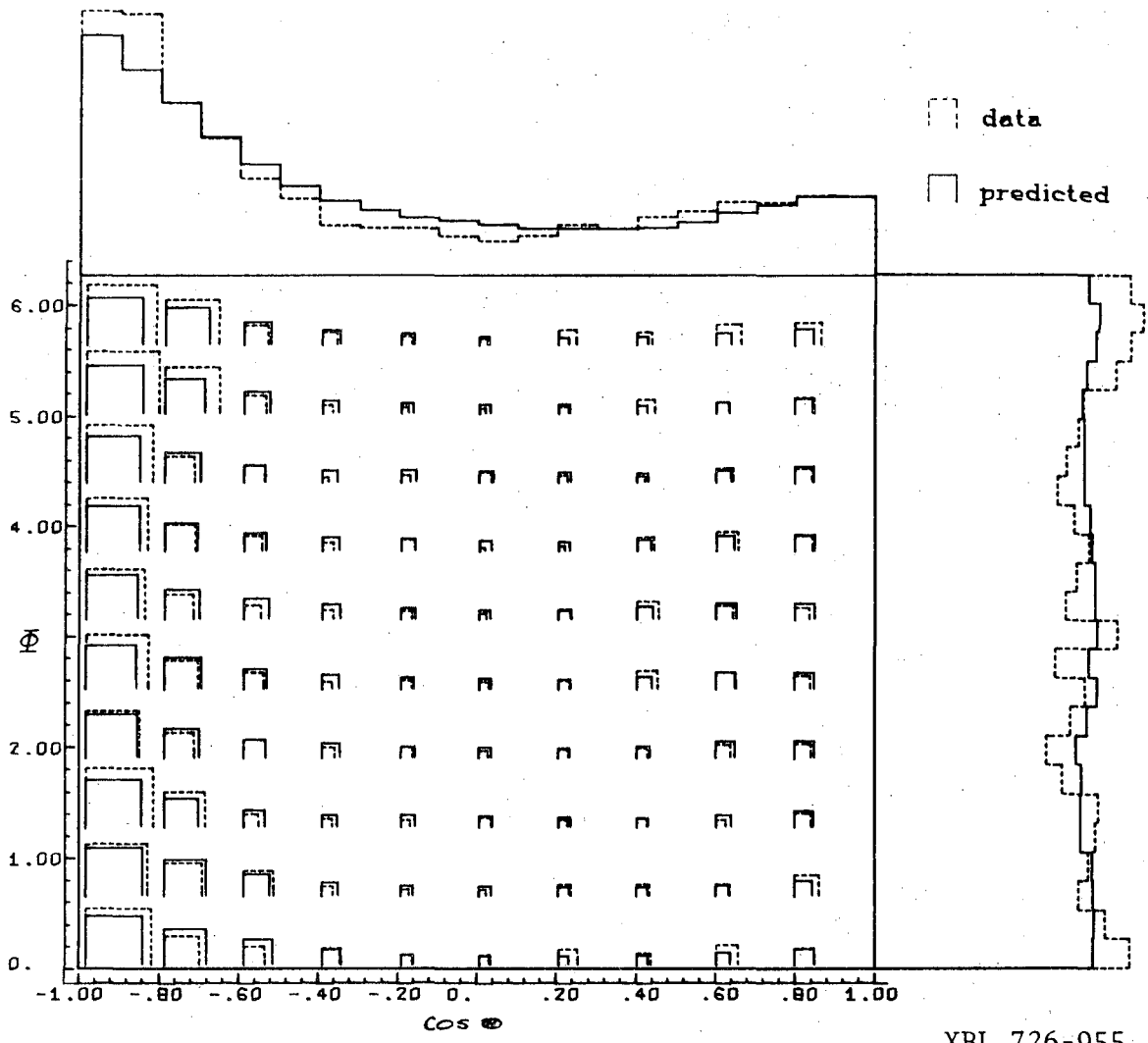
XBL 726-953

Fig. 22a.



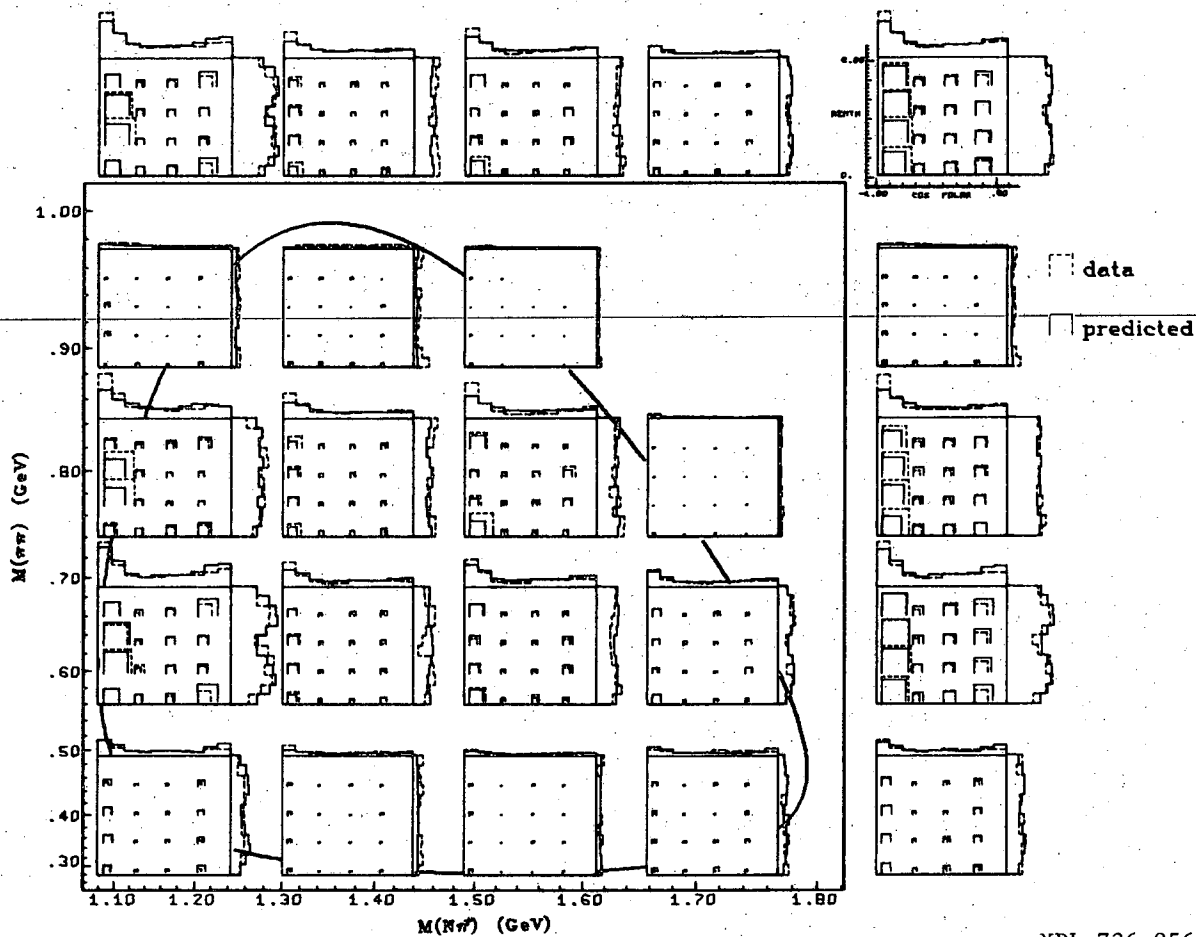
XBL 726-954

Fig. 22b.



XBL 726-955

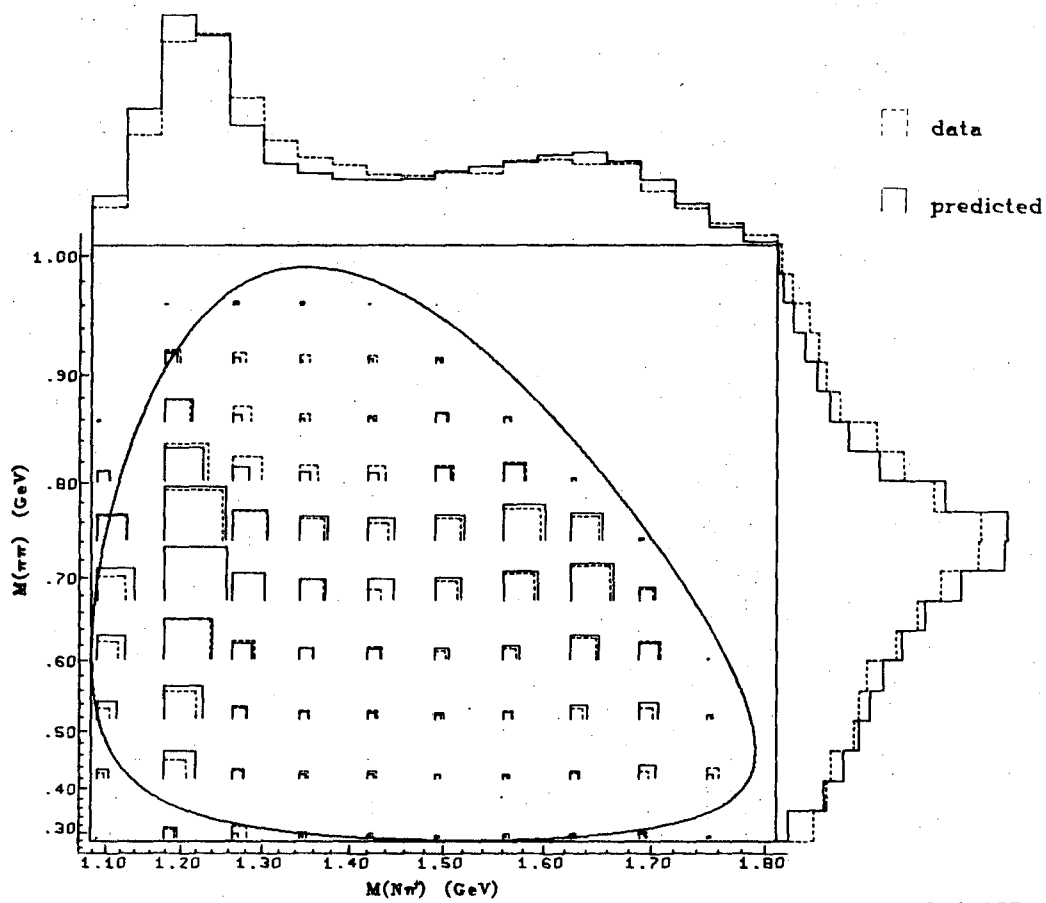
Fig. 22c.



XBL 726-956

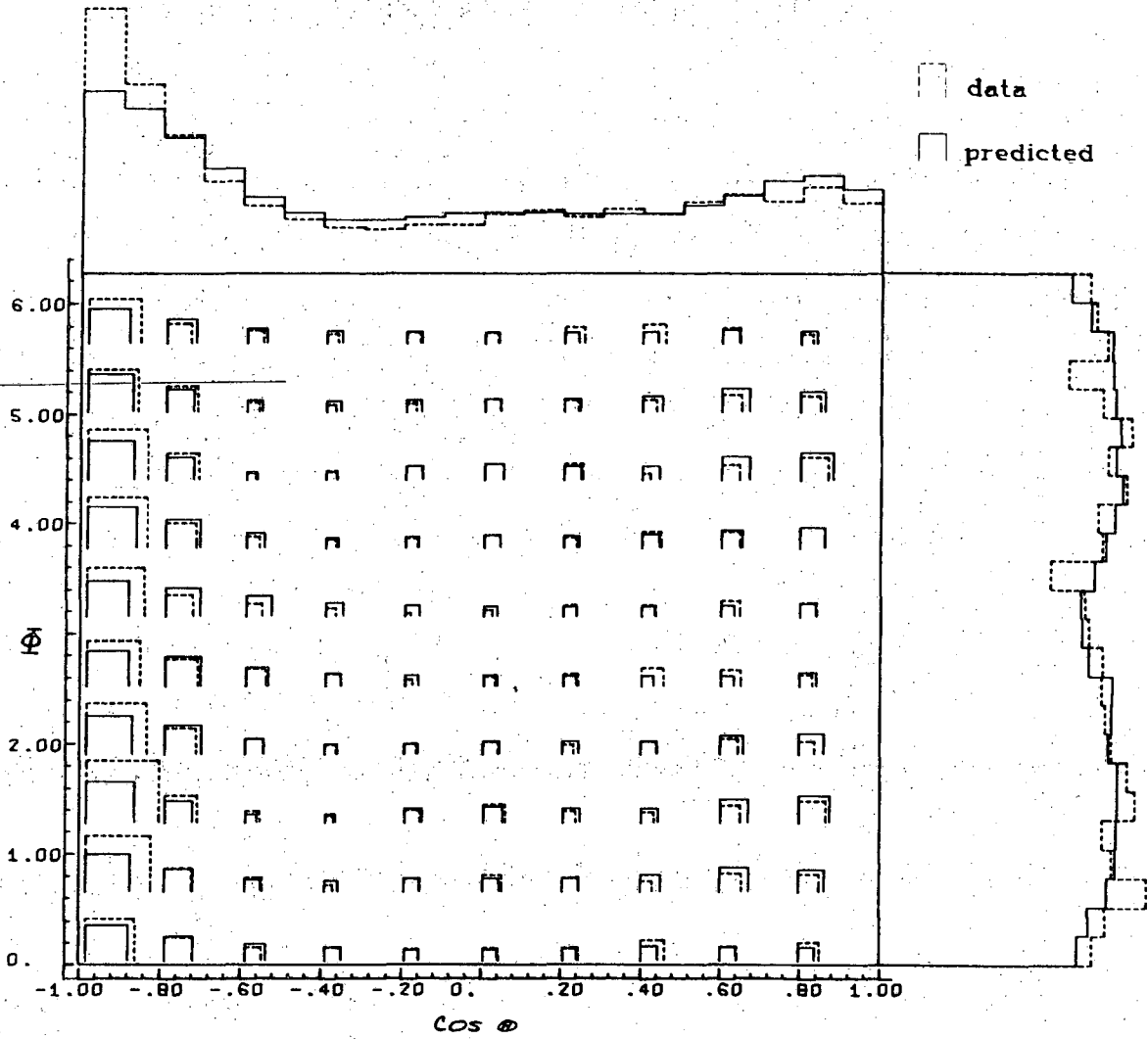
Fig. 23a.





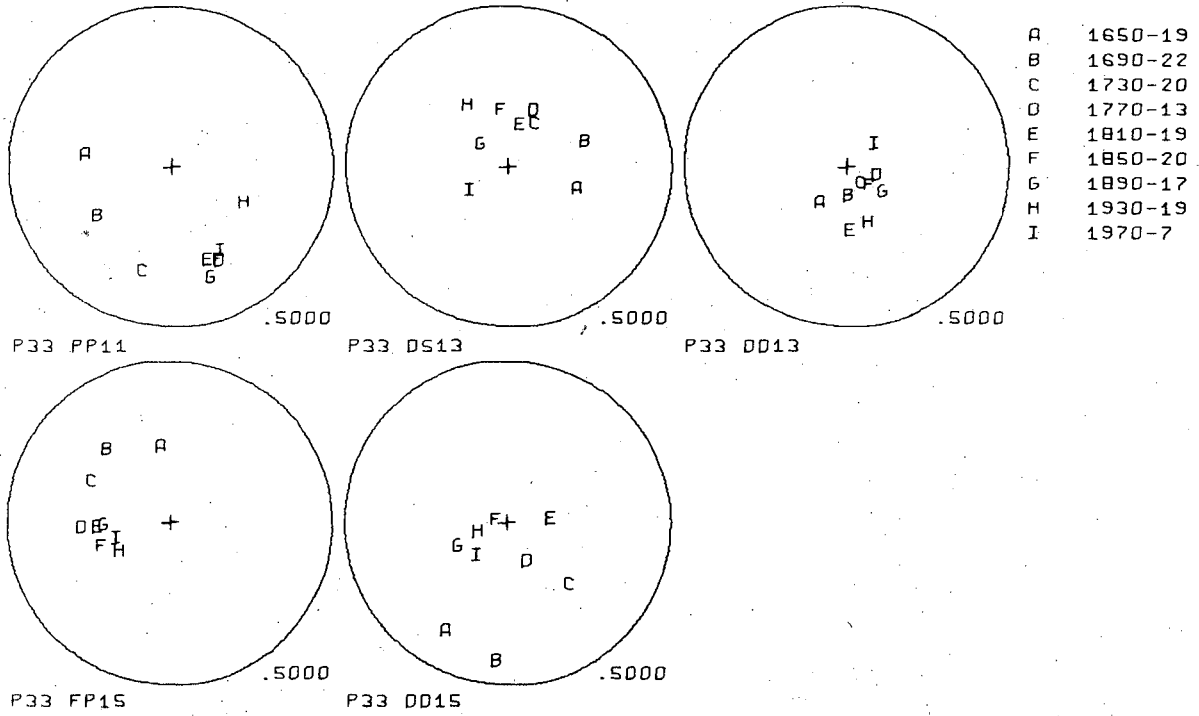
XBL 726-957

Fig. 23b.



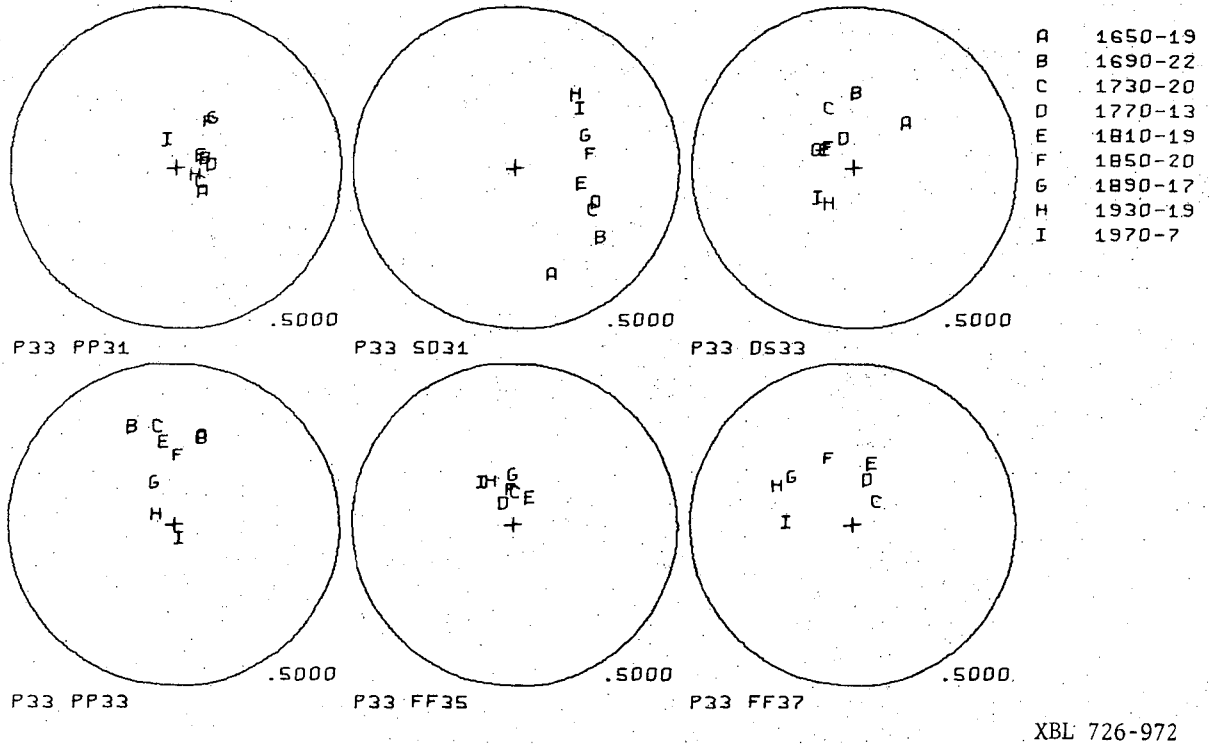
XBL 726-970

Fig. 23c.



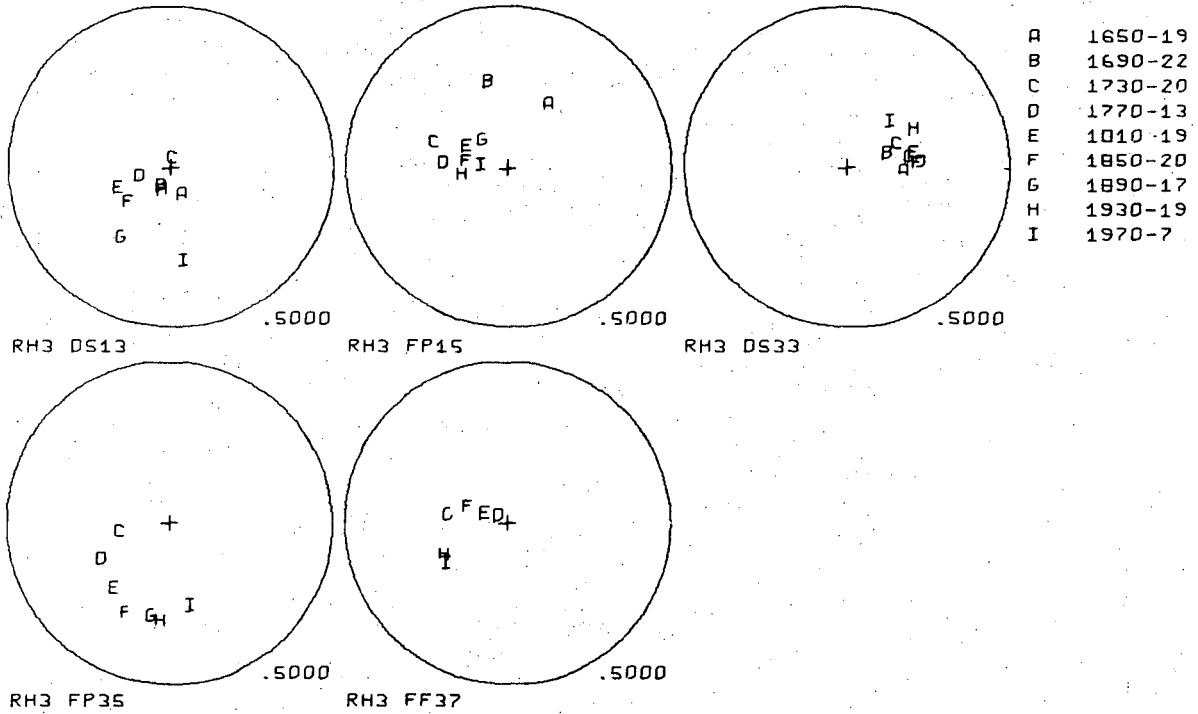
XBL 726-971

Fig. 24.



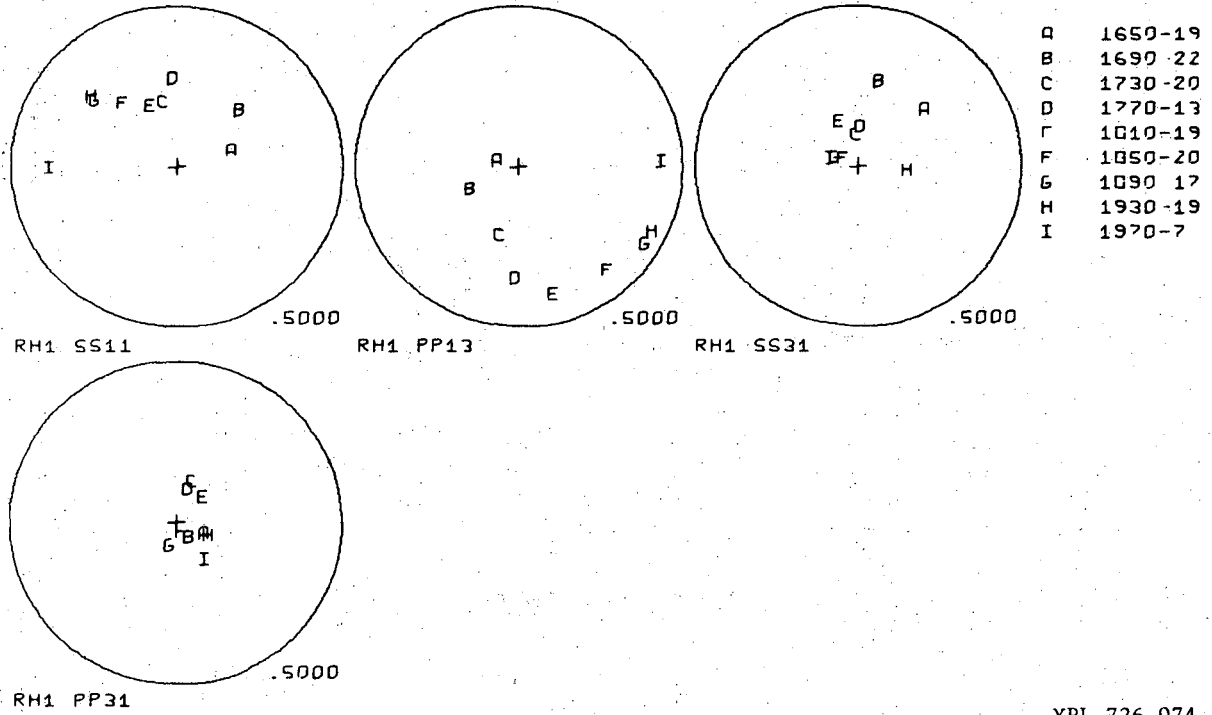
XBL 726-972

Fig. 25.



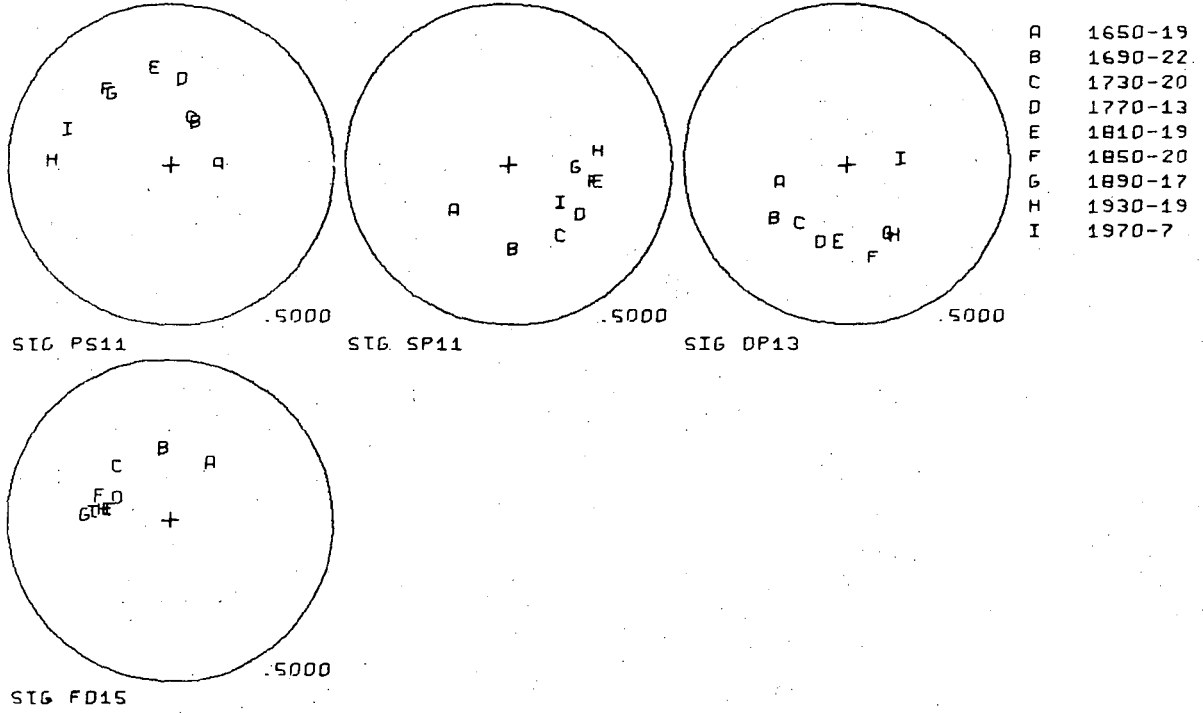
XBL 726-973

Fig. 26.



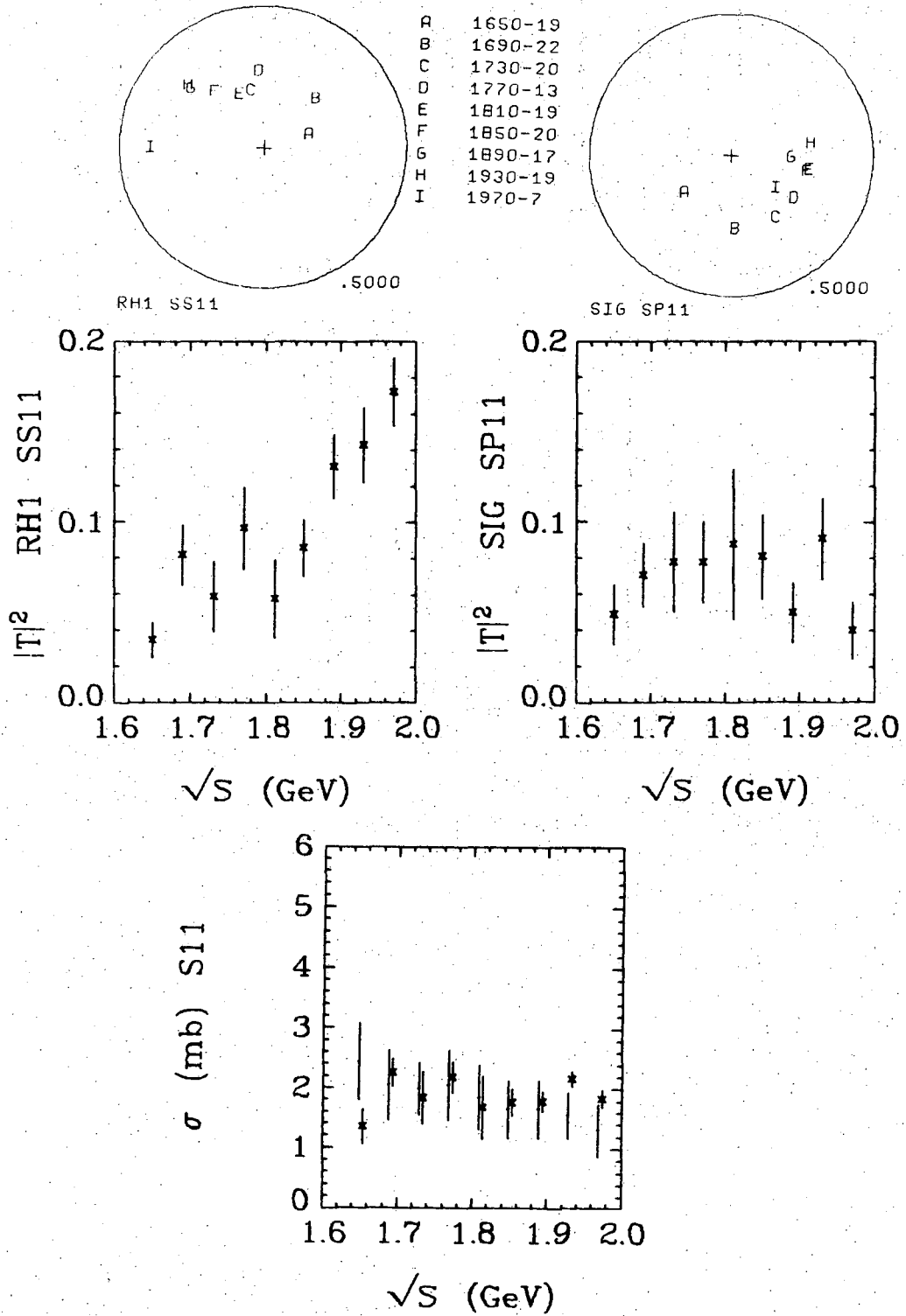
XBL 726-974

Fig. 27.



XBL 726-975

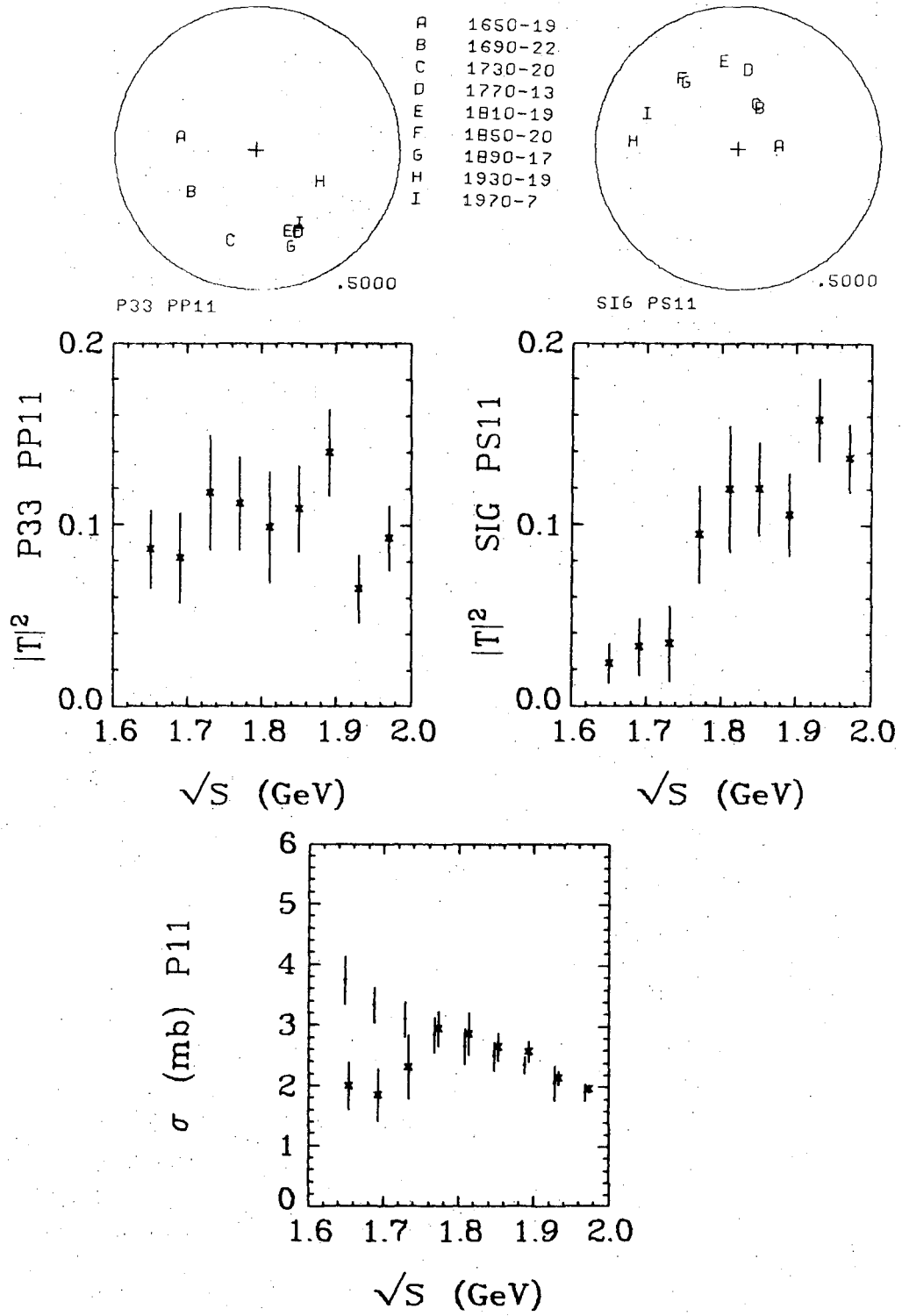
Fig. 28.



XBL 726-976

Fig. 29.

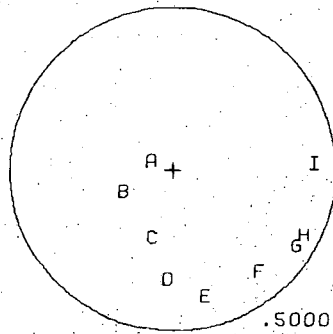




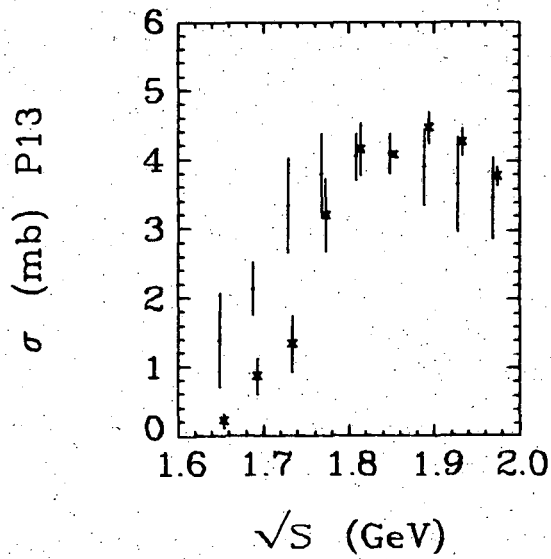
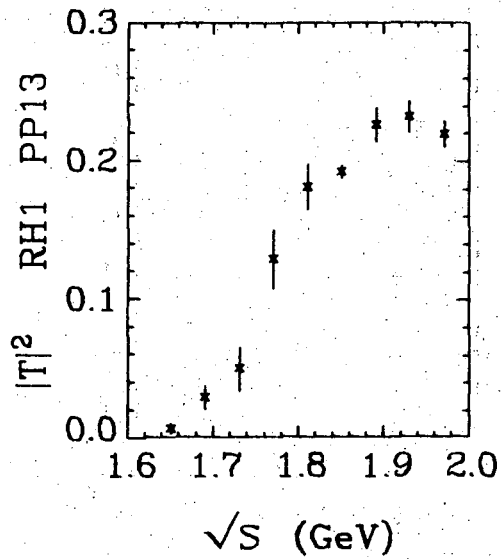
XBL 726-977

Fig. 30.

- A 1650-19
- B 1690-22
- C 1730-20
- D 1770-13
- E 1810-19
- F 1850-20
- G 1890-17
- H 1930-19
- I 1970-7

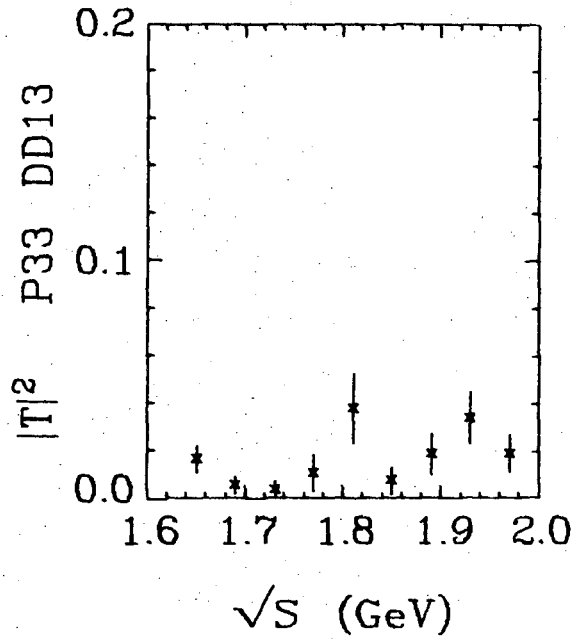
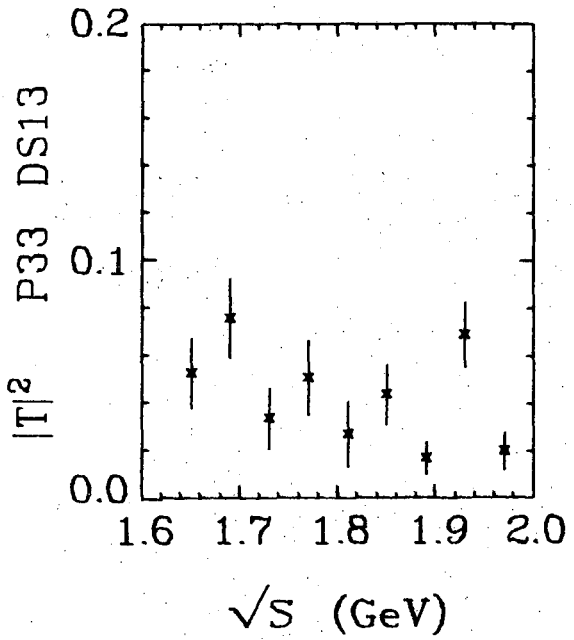
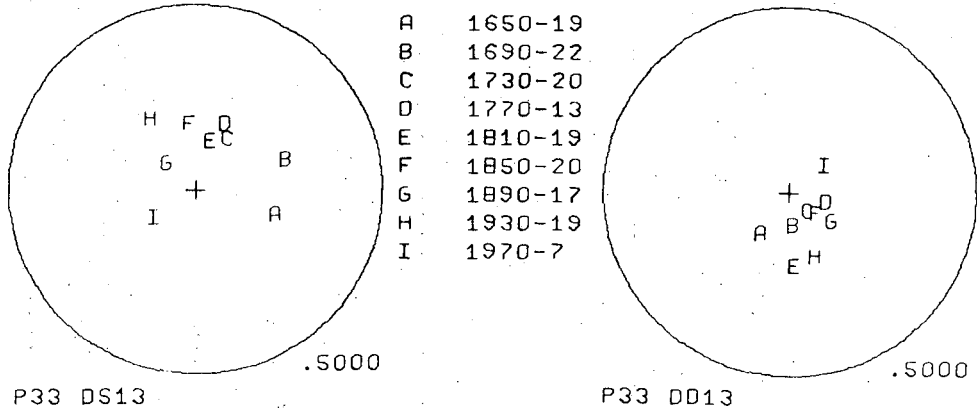


RH1 PP13



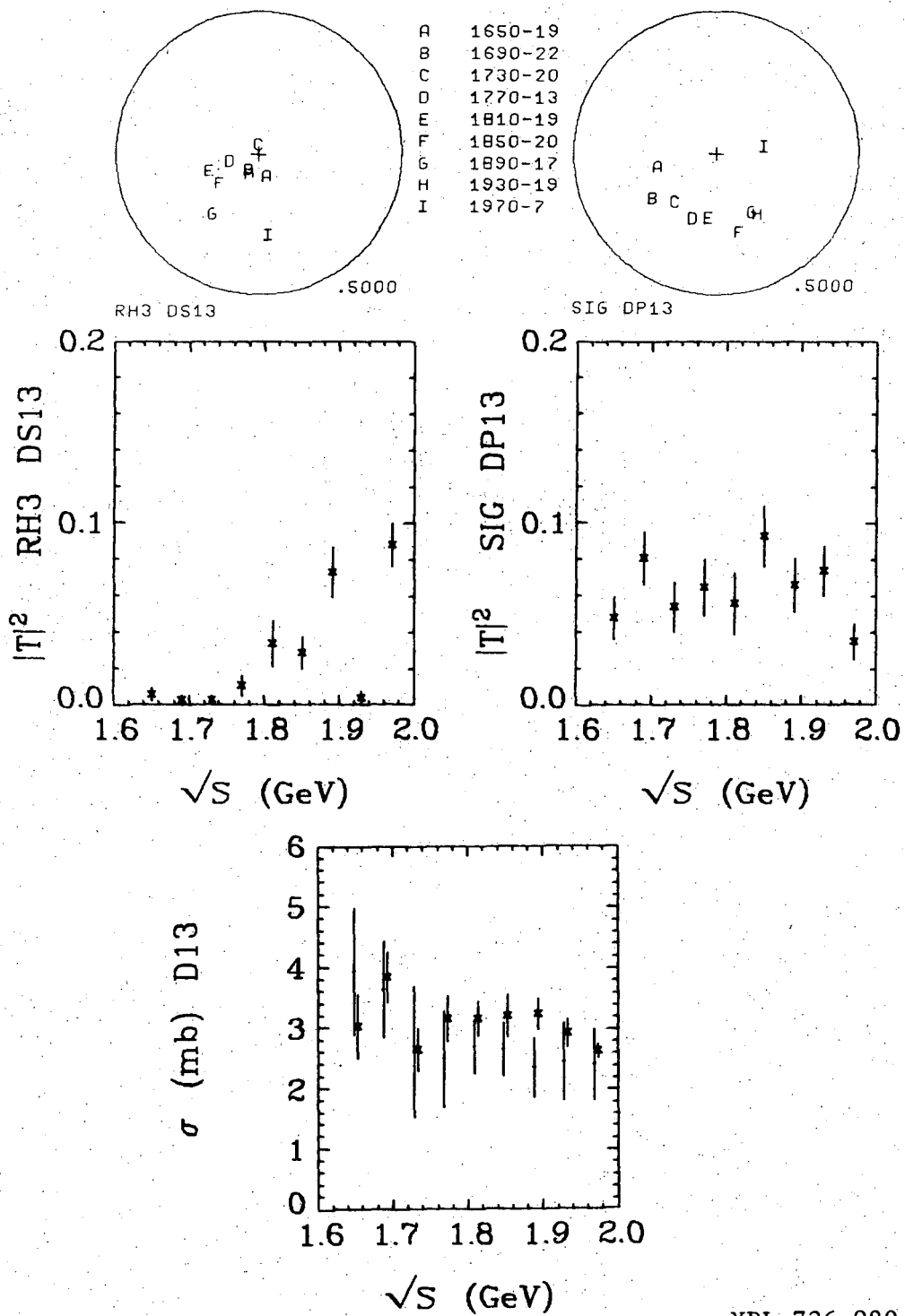
XBL 726-978

Fig. 31.



XBL 726-979

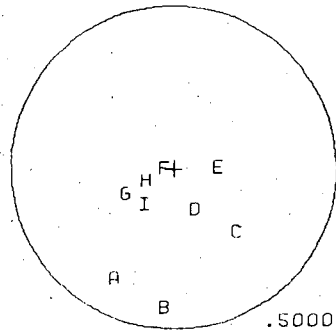
Fig. 32a.



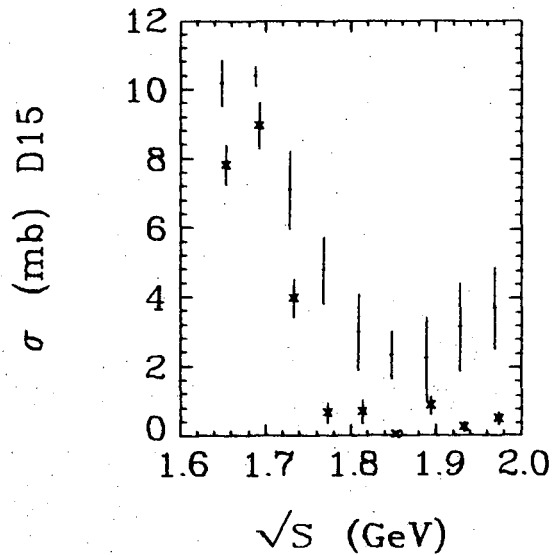
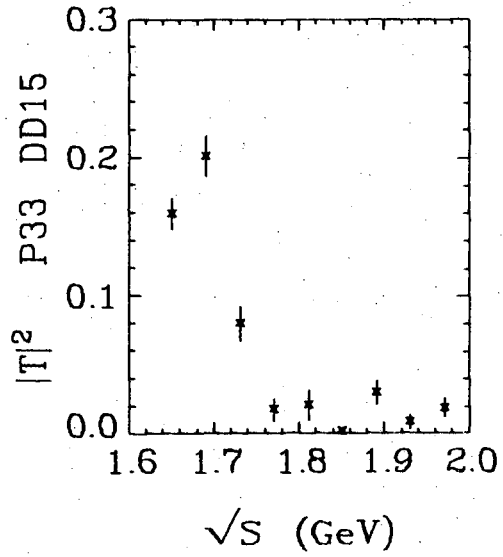
XBL 726-980

Fig. 32b.

- A 1650-19
- B 1690-22
- C 1730-20
- D 1770-13
- E 1810-19
- F 1850-20
- G 1890-17
- H 1930-19
- I 1970-7

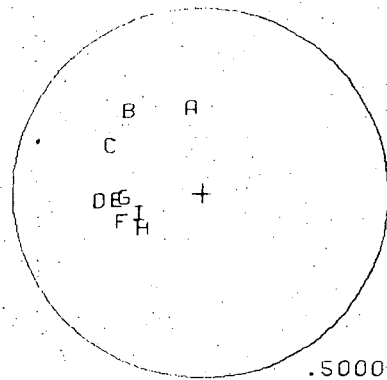


P33 DD15

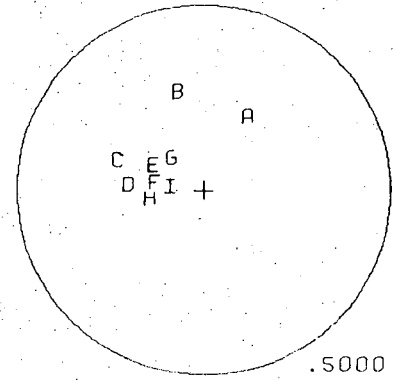


XBL 726-981

Fig. 33.

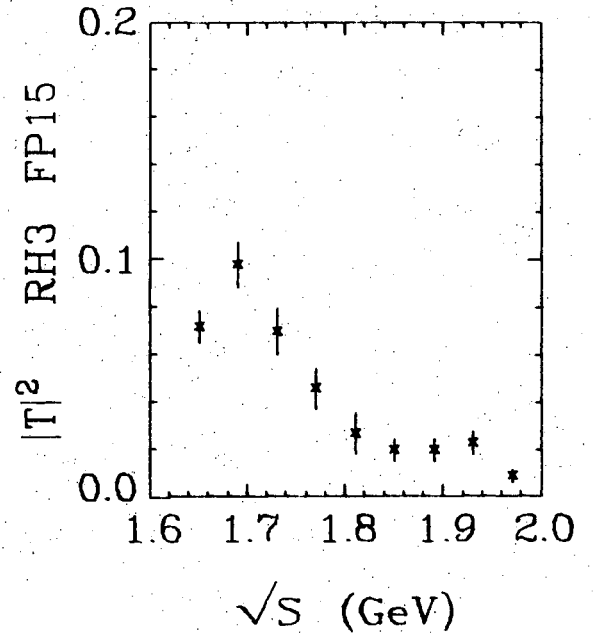
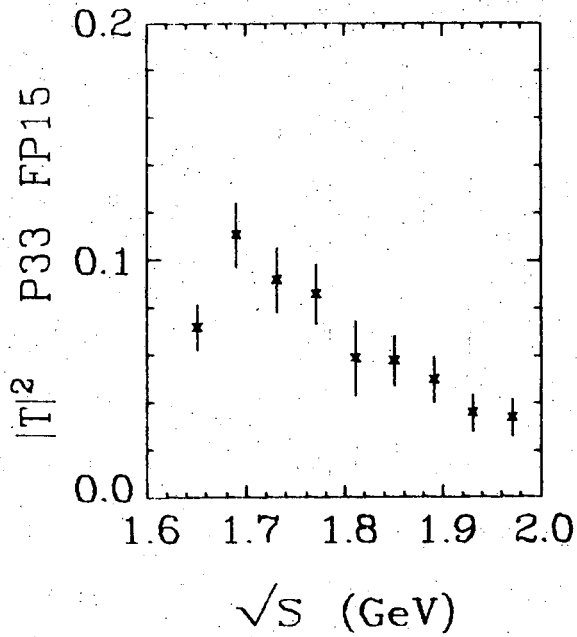


- A 1650-19
- B 1690-22
- C 1730-20
- D 1770-13
- E 1810-19
- F 1850-20
- G 1890-17
- H 1930-19
- I 1970-7



P33 FP15

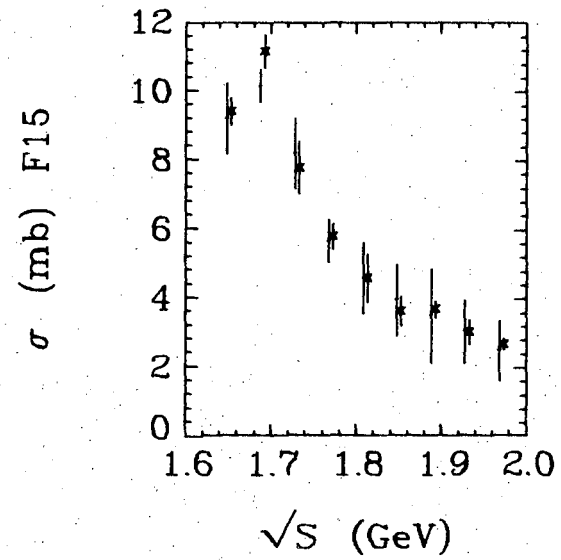
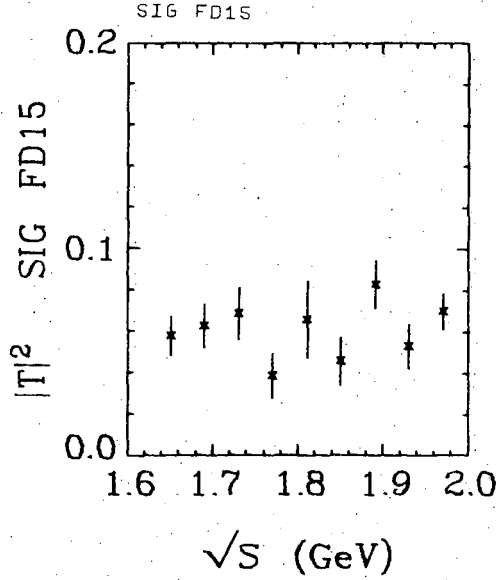
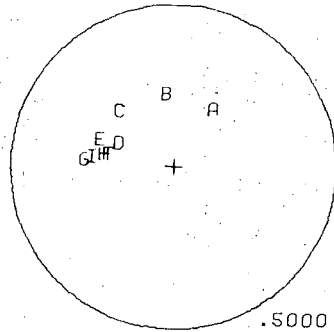
RH3 FP15



XBL 726-982

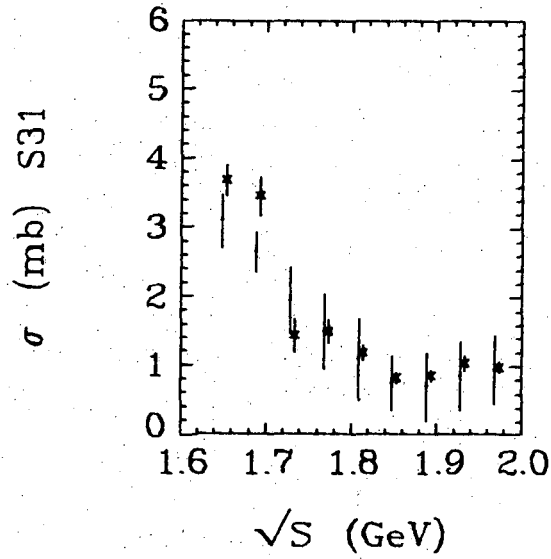
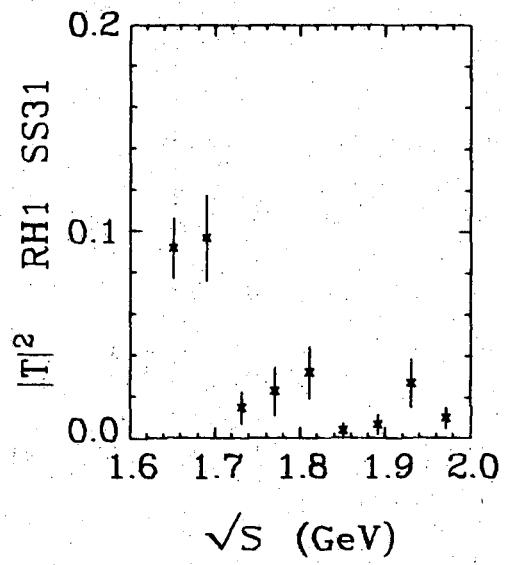
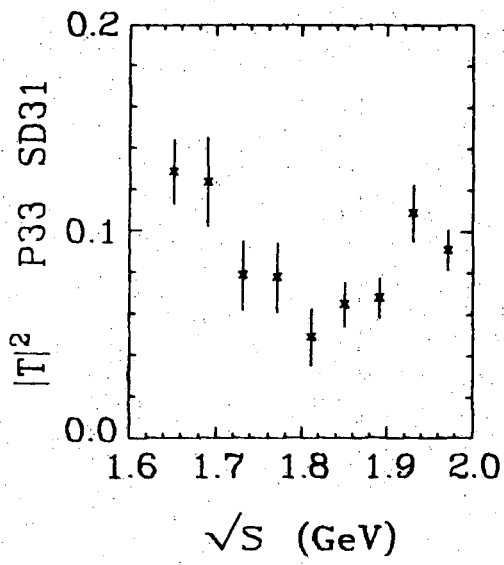
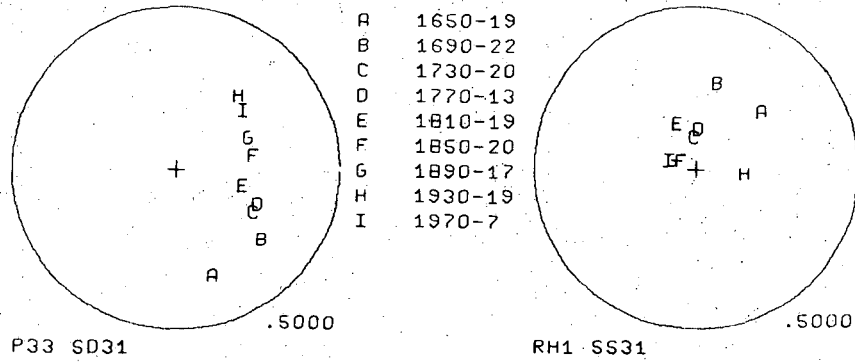
Fig. 34a.

- A 1650-19
- B 1690-22
- C 1730-20
- D 1770-13
- E 1810-19
- F 1850-20
- G 1890-17
- H 1930-19
- I 1970-7



XBL 726-983

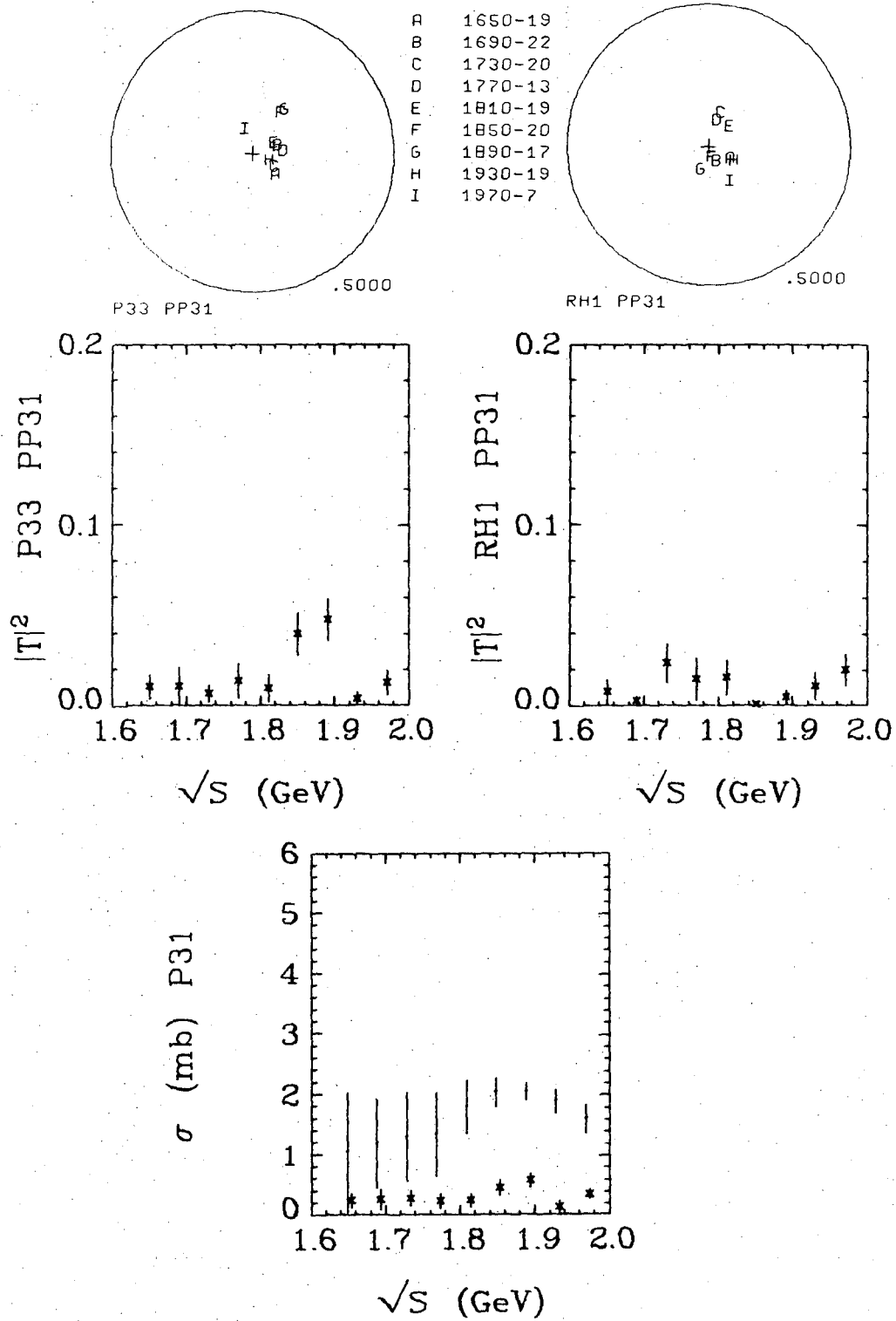
Fig. 34b.



XBL 726-984

Fig. 35.

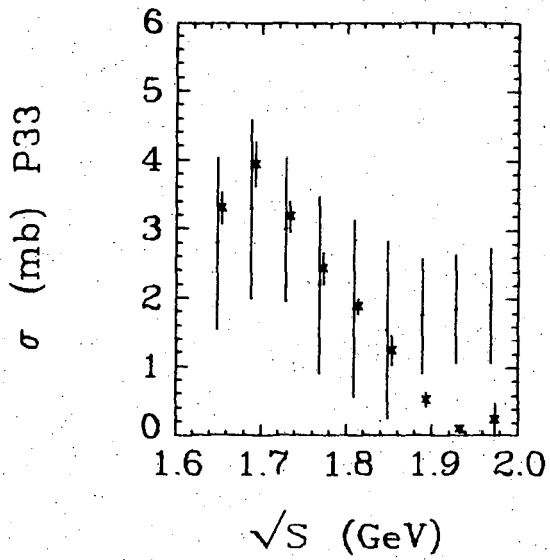
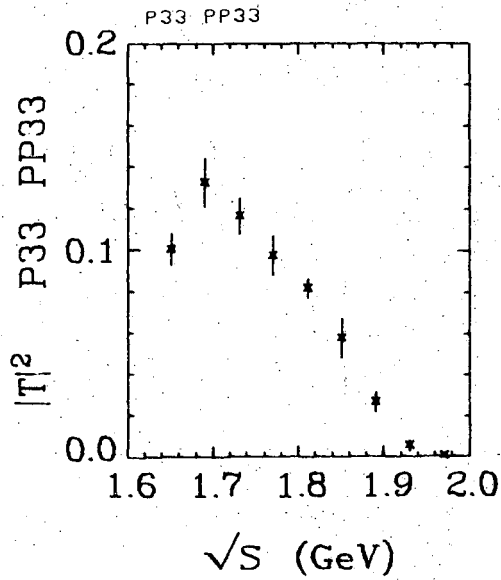
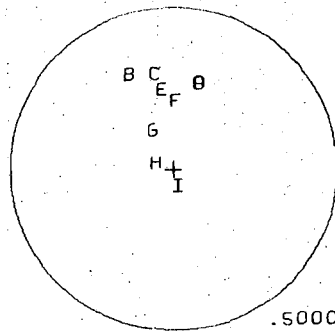




XBL 726-985

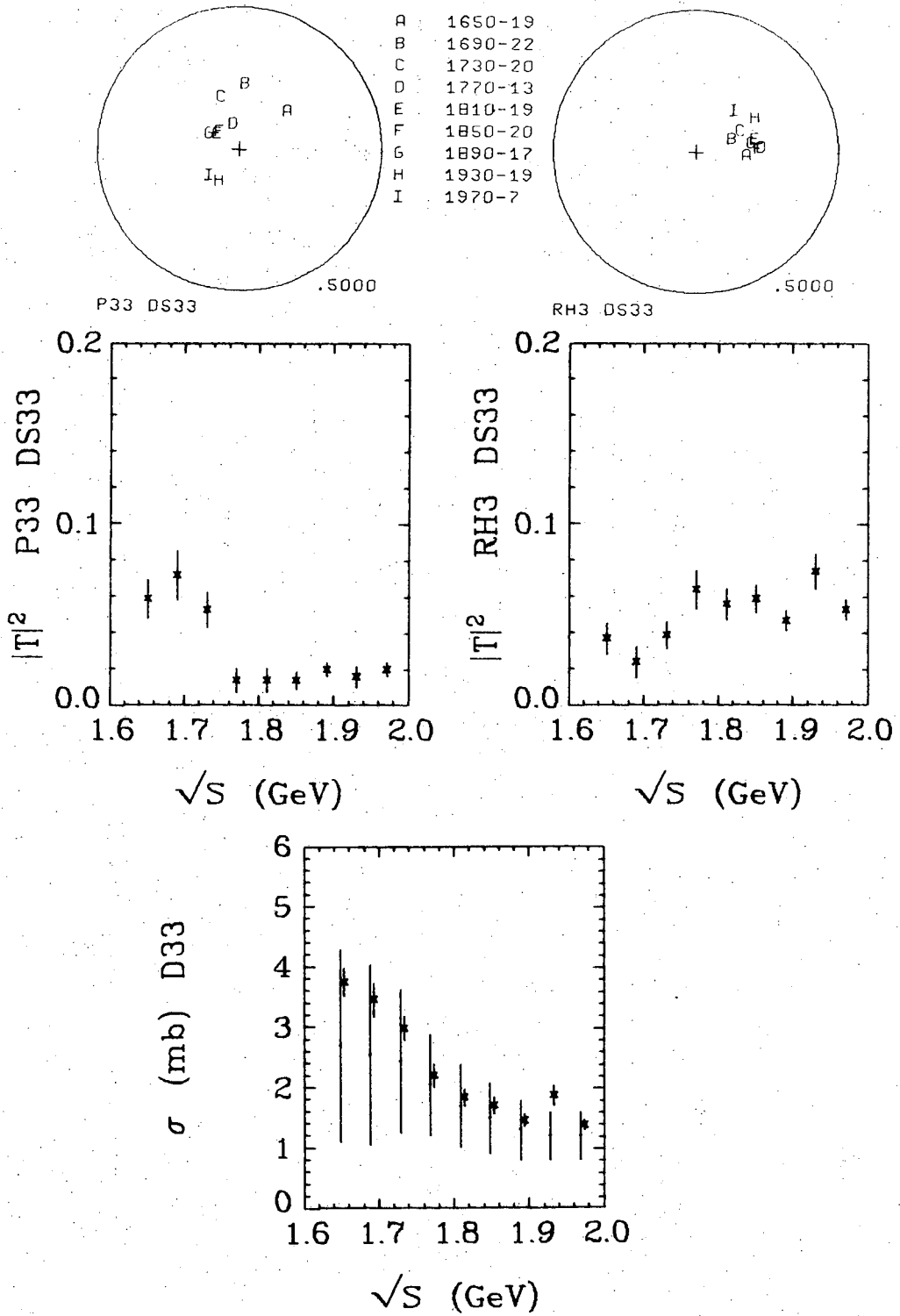
Fig. 36.

- A 1650-19
- B 1690-22
- C 1730-20
- D 1770-13
- E 1810-19
- F 1850-20
- G 1890-17
- H 1930-19
- I 1970-7



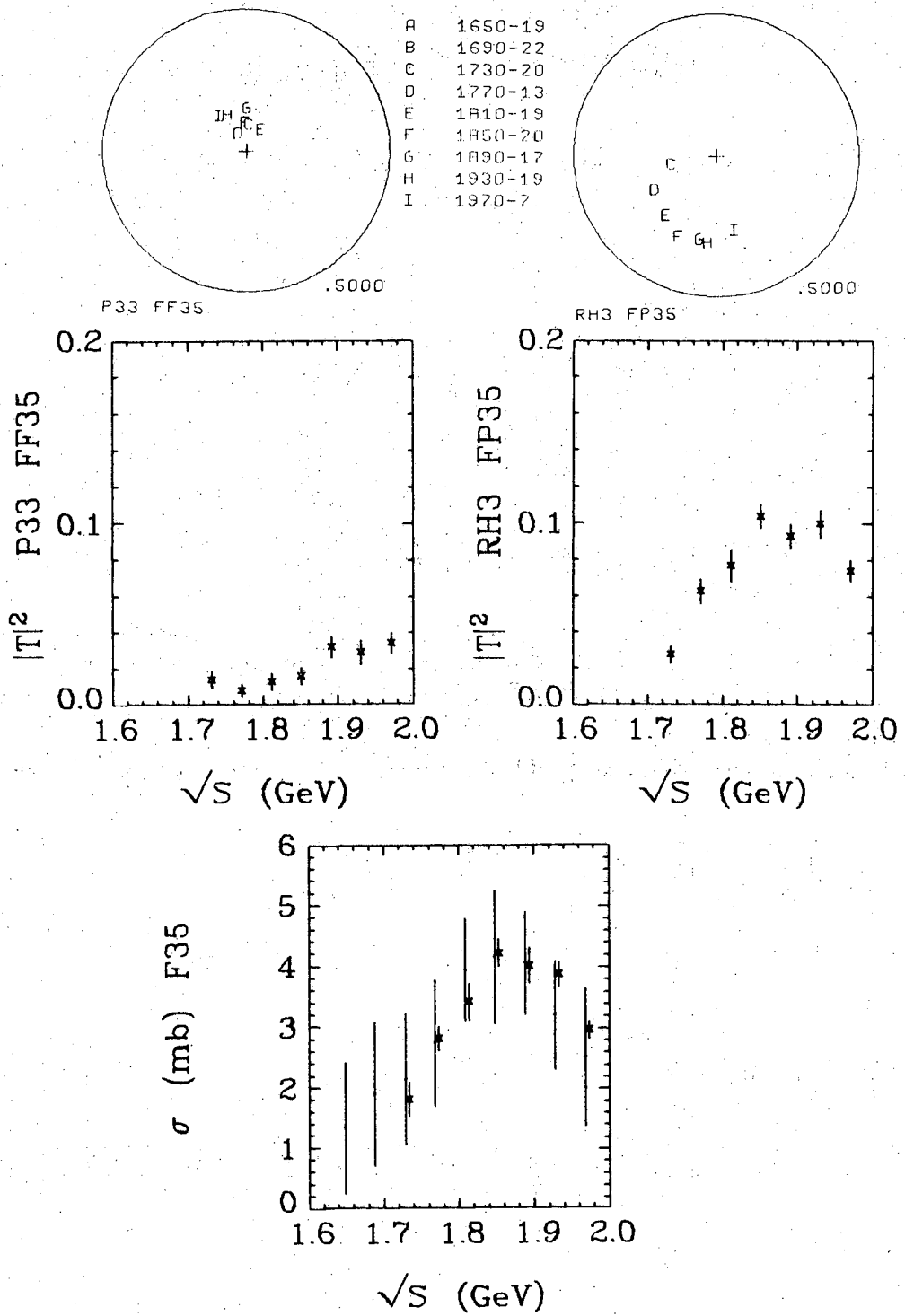
XBL 726-986

Fig. 37.



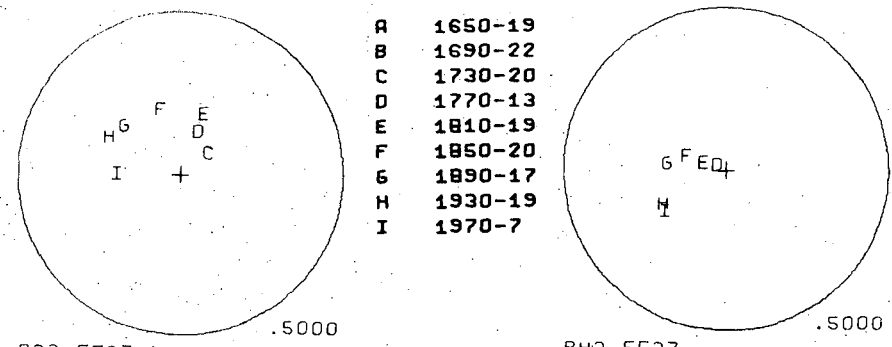
XBL 726-987

Fig. 38.

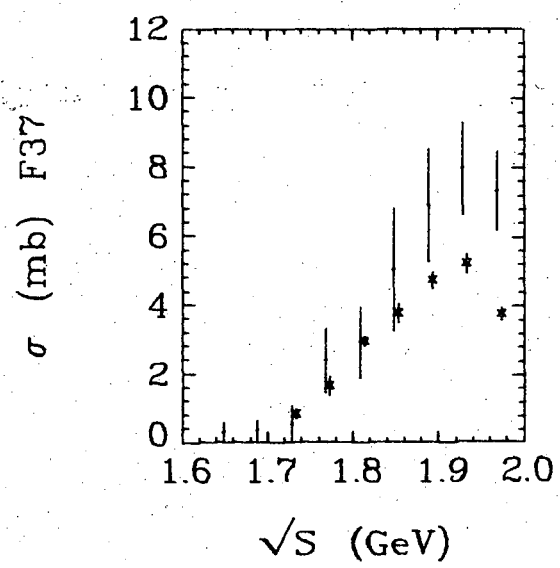
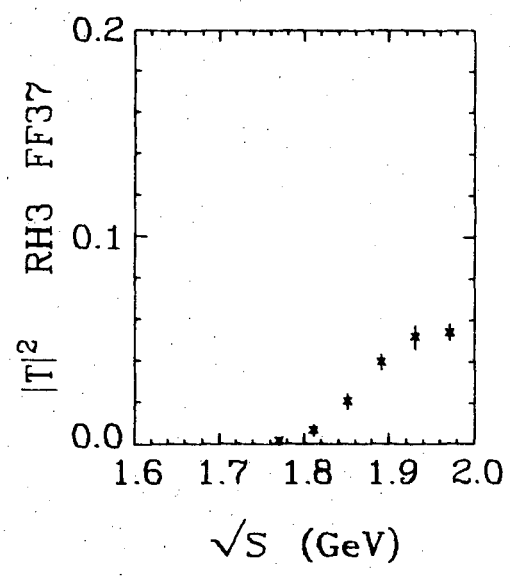
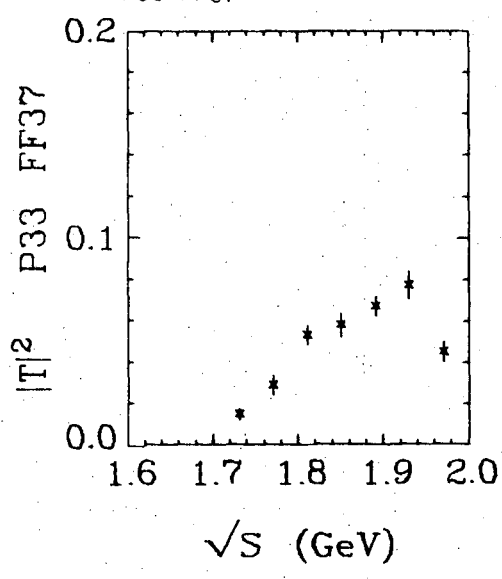


XBL 726-988

Fig. 39.



|   |         |
|---|---------|
| A | 1650-19 |
| B | 1690-22 |
| C | 1730-20 |
| D | 1770-13 |
| E | 1810-19 |
| F | 1850-20 |
| G | 1890-17 |
| H | 1930-19 |
| I | 1970-7  |



XBL 726-989

Fig. 40.

APPENDIX I

In this Appendix, we wish to review another property of the variance matrix,  $E$ , and the second derivative matrix,  $D$ , where  $D$  is  $E^{-1}$ .  $E$  (or  $D$ ) is positive definite. This is necessary to insure a maximum in the likelihood,  $\mathcal{L}$ , rather than a saddle point or a minimum.

Defining the origin of the parameter space to be at the maximum, we can write

$$\mathcal{F} = \ln \mathcal{L} = \ln \mathcal{L}_0 - 1/2 \chi^2 \quad (\text{A.1})$$

and near the origin we can expand  $\chi^2$  as

$$\chi^2 = \underline{\underline{A}} \cdot \underline{\underline{D}} \cdot \underline{\underline{A}} \quad (\text{A.2})$$

The surface, enclosing the origin, defined by  $1 = \underline{\underline{A}} \cdot \underline{\underline{D}} \cdot \underline{\underline{A}}$  is known as the error ellipsoid. This surface intercepts each axis at the points  $A_i^{\text{int}} = (D_{ii})^{-1/2}$ .

$$(\text{A.3})$$

This is sketched, in two dimensions, in Fig. A.1. It can be shown\* that the planes defining the circumscribed box intercept the axes at the points  $A_i^{\text{max}}$ , given by

$$A_i^{\text{max}} = (E_{ii})^{1/2} \equiv \delta A_i. \quad (\text{A.4})$$

(The plane  $A_1 = A_1^{\text{max}} = \delta A_1$  is the dashed line of Fig. A.1). In A.4 we have written

$$E = \begin{pmatrix} \delta A_1 \delta A_1 & \delta A_1 \delta A_2 c_{12} & \dots & \delta A_1 \delta A_n c_{1n} \\ \delta A_1 \delta A_2 c_{12} & \delta A_2 \delta A_2 & \dots & \delta A_2 \delta A_n c_{2n} \\ \vdots & \vdots & \ddots & \vdots \\ \delta A_1 \delta A_n c_{1n} & \delta A_2 \delta A_n c_{2n} & \dots & \delta A_n \delta A_n \end{pmatrix} \quad (\text{A.5})$$

\* Rosenfeld, A.H. and Solmitz, F.T. Lawrence Berkeley Laboratory Group A Memo 753 (unpublished, 1972).

and  $|c_{ij}| < 1$  and are the correlation coefficients. Now (as is evident from Fig. A.1)

$$(D_{ii})^{-1/2} \leq \delta A_i \quad (\text{A.6})$$

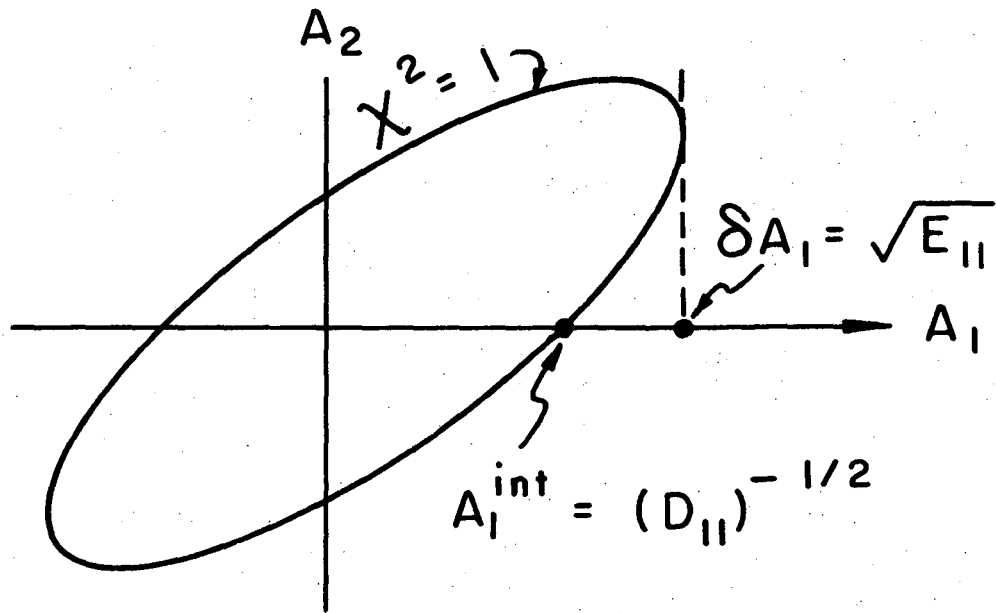
and the equality holds if and only if  $c_{ij} = 0$  for all  $j \neq i$ . Thus one can get a measure of how strong the correlations are by comparing  $(D_{ii})^{-1/2}$  with  $\delta A_i$ .

In Table AI we compare  $\delta A_i$  and  $(D_{ii})^{-1/2}$  for all the waves at a typical energy,  $\sqrt{s} = 1690$  MeV. Note that there are three entries for  $(D_{ii})^{-1/2}/\delta A_i$ , which exceed 1.0, one of them by 20%! This difficulty presumably has to do with invalid approximations in the inversion of D. Remember that we fit in a space of two too many variables; i. e., we use the real and imaginary part of all amplitudes, even though the overall amplitude and phase are undetermined. Therefore, D is singular, and we have to subtract two eigenvalues -- see Eq. 14 of Miller's thesis, Ref. 4. Apparently approximations in this procedure can introduce errors at the 10-20% level.

Table AI. Comparison of  $\delta A_1$  and  $(D_{ii})^{-1/2}$  for all the waves at a typical energy,  $\sqrt{s} = 1690$  MeV.

|     |              | Re           |                   |                              | Im           |                   |                              |
|-----|--------------|--------------|-------------------|------------------------------|--------------|-------------------|------------------------------|
|     |              | $\delta A_i$ | $(D_{ii})^{-1/2}$ | $(D_{ii})^{-1/2}/\delta A_i$ | $\delta A_i$ | $(D_{ii})^{-1/2}$ | $(D_{ii})^{-1/2}/\delta A_i$ |
| P33 | PP11         | 0.0755       | 0.0630            | 0.834                        | 0.0734       | 0.0528            | 0.719                        |
|     | DS13         | 0.0206       | 0.0162            | 0.786                        | 0.0208       | 0.0144            | 0.692                        |
|     | DD13         | 0.1520       | 0.1281            | 0.843                        | 0.1223       | 0.1036            | 0.847                        |
|     | FP15         | 0.0589       | 0.0382            | 0.649                        | 0.0392       | 0.0288            | 0.735                        |
|     | DD15         | 0.1916       | 0.1021            | 0.533                        | 0.1269       | 0.1269            | 0.551                        |
|     | PP31         | 0.0913       | 0.0745            | 0.816                        | 0.0642       | 0.0533            | 0.830                        |
|     | SD31         | 0.2283       | 0.1944            | 0.852                        | 0.1589       | 0.1346            | 0.847                        |
|     | DS33         | 0.0264       | 0.0194            | 0.735                        | 0.0189       | 0.0134            | 0.709                        |
|     | FP33         | 0.1006       | 0.0689            | 0.685                        | 0.0295       | 0.0327            | > 1                          |
|     | FF35<br>FF37 |              |                   |                              |              |                   |                              |
| RH3 | DS13         | 0.0973       | 0.0767            | 0.788                        | 0.0882       | 0.0647            | 0.734                        |
|     | FP15         | 0.3184       | 0.2347            | 0.737                        | 0.1910       | 0.1493            | 0.782                        |
|     | DS33         | 0.980        | 0.0742            | 0.757                        | 0.0979       | 0.0701            | 0.716                        |
|     | FP35<br>FF37 |              |                   |                              |              |                   |                              |
|     |              |              |                   |                              |              |                   |                              |
| RH1 | SS11         | 0.1111       | 0.0976            | 0.878                        | 0.1356       | 0.0974            | 0.718                        |
|     | PP13         | 0.3066       | 0.2297            | 0.749                        | 0.2924       | 0.2474            | 0.846                        |
|     | SS31         | 0.1549       | 0.1198            | 0.773                        | 0.1414       | 0.1037            | 0.733                        |
|     | PP31         | 0.5790       | 0.4471            | 0.772                        | 0.4885       | 0.4268            | 0.874                        |
| SIG | PS11         | 0.2106       | 0.1559            | 0.740                        | 0.1927       | 0.1675            | 0.869                        |
|     | SP11         | 0.6360       | 0.5678            | 0.893                        | 0.4441       | 0.4621            | > 1                          |
|     | DP13         | 0.3282       | 0.2855            | 0.870                        | 0.3741       | 0.3107            | 0.831                        |
|     | FD15         | 0.4801       | 0.5859            | > 1                          | 0.6085       | 0.5367            | 0.882                        |





XBL727-3577

Fig. A.1

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