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Chemical Sciences Division

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# Vapor-Liquid Equilibria for Binary Solutions of Polyisobutylene in C<sub>6</sub> through C<sub>9</sub> n-Alkanes

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## ABSTRACT

Vapor-liquid equilibria for binary solutions of polyisobutylene in C<sub>6</sub> through C<sub>9</sub> n-alkanes were obtained at 65°C. Using a classic gravimetric-sorption method, the amount of solvent absorbed by polyisobutylene was measured as a function of solvent vapor pressure. The data are interpreted with the Flory-Huggins theory and the Prigogine-Flory-Patterson theory.

## INTRODUCTION

Vapor-liquid-equilibrium (VLE) data for polymer solutions are useful for a variety of applications including surface acoustic-wave sensors, polymer devolatilization, polymeric membrane-separation processes, pervaporation, and vapor-phase photografting<sup>1-6</sup>. Efficient design of such processes requires characterizing VLE behavior of polymer solutions through experimental data or molecular-thermodynamic models.

Modeling polymer-solution properties is traditionally done by lattice theory or by equation-of-state theory; the Flory-Huggins lattice theory<sup>7</sup> and the Prigogine-Flory-Patterson equation-of-state theory<sup>8-11</sup> provide classical examples. In general, an equation-of-state theory gives a more complete and accurate description of real polymer solutions than lattice theory. For example, the excess volume upon mixing is accessible through an equation-of-state model but not through an incompressible lattice model. On the other hand, whereas the Flory-Huggins lattice theory requires only one adjustable interaction

parameter, the Prigogine-Flory-Patterson theory requires an adjustable interaction parameter in addition to three pure-component parameters for the solvent and for the polymer.

This work reports vapor-liquid-equilibrium data for binary solutions of polyisobutylene (PIB) in C<sub>6</sub> through C<sub>9</sub> n-alkanes. Data are interpreted with the Flory-Huggins theory and with the Prigogine-Flory-Patterson theory.

## EXPERIMENTAL

### *Materials*

Solvents were degassed with a standard freeze-thaw procedure described by Panayiotou and Vera<sup>12</sup> and used without further purification.

The polyisobutylene sample was a white, rubbery solid with a glass-transition temperature at about 29°C. The viscosity-average molecular weight was in the range  $4.2 \times 10^6$  to  $5.2 \times 10^6$ . The average value  $4.7 \times 10^6$  is assumed in our calculations.

*Table 1* gives properties of solvents and polyisobutylene.

### *Apparatus*

Vapor-liquid-equilibrium data were collected using a gravimetric-sorption method previously described by several authors (see, for example, Gupta and Prausnitz<sup>13</sup>). *Figure 1* shows a schematic diagram of the apparatus. The entire system is submerged in an isothermal water bath maintained at  $\pm 0.1^\circ\text{C}$ .

Each glass chamber contains one aluminum pan suspended from a quartz spring (Ruska Instruments Corp., Houston, TX). The calibrated springs have a sensitivity of

about 1 mg/mm and a maximum load of 250 mg. Within this range, the elongation of each spring is linear with respect to change in mass.

A cathetometer (Gaertner Scientific Corp., Chicago) is used to measure the extension of the springs and the mercury levels of the manometer.

### *Experimental Procedure*

Polymer samples of known mass (20–25 mg) are placed into previously weighed aluminum pans. The system is then vacuum-dried for 12 to 24 hours to remove residual moisture and solvent. After obtaining the mass of dry polymer, solvent is introduced by opening and then closing the valve between the solvent flask and the evacuated glass chambers.

The system is allowed to equilibrate anywhere from 12 hours to a few days after each solvent injection. Equilibrium is assumed when measurements in spring length do not change more than  $\pm 0.03$  mm over a 12-hour period.

Because the polymer is nonvolatile, the total pressure is equal to the vapor pressure of solvent above the polymer solution. Because experimental pressures are low (less than 0.9 bar), the solvent vapor is considered to be an ideal gas. Solvent activity  $a_1$  is given by the ratio of the measured pressure to the pure-solvent saturation pressure at system temperature.

The vernier scale on the cathetometer allows measurements to be made to the nearest 0.01 millimeter; therefore, pressure and mass readings have a precision of 0.02 torr and 0.02 mg, respectively. Uncertainty in solvent activity is less than 1% for the pressures used here. Solvent weight fraction  $w_1$  uncertainty is less than 1% above

$w_1 = 0.1$  and 1–10% below  $w_1 = 0.1$ . Reliability of the apparatus and experimental procedure were established by reproducing published experimental vapor-liquid-equilibrium data for polystyrene in chloroform at 50°C<sup>14</sup>.

## RESULTS AND DISCUSSION

*Table 2* presents vapor-liquid-equilibrium data for polyisobutylene in C<sub>6</sub> through C<sub>9</sub> n-alkanes.

The data were fitted using the Flory-Huggins lattice theory<sup>7</sup> and the Prigogine-Flory-Patterson equation-of-state theory<sup>8-11</sup>.

### *Flory-Huggins Theory*

The activity of the solvent is given by

$$\ln a_1 = \ln \Phi_1 + \left(1 - \frac{r_1}{r_2}\right) \Phi_2 + \chi_{FH} \Phi_2^2. \quad (1)$$

Solvent and polymer segment fractions,  $\Phi_1$  and  $\Phi_2$ , are defined by

$$\Phi_2 = 1 - \Phi_1 = \frac{r_2 N_2}{r_1 N_1 + r_2 N_2} \quad (2)$$

where  $N_1$  and  $N_2$  are the number of molecules and  $r_1$  and  $r_2$  are the number of segments per molecule of solvent and polymer, respectively. We set  $r_1$  equal to unity and calculate  $r_2$  by

$$r_2 = \frac{M_2 \rho_1}{M_1 \rho_2} = \frac{\text{molar volume of polymer}}{\text{molar volume of solvent}} \quad (3)$$

where  $M_1$  and  $M_2$  are molecular weights and  $\rho_1$  and  $\rho_2$  are mass densities of solvent



and polymer, respectively. The dimensionless Flory-Huggins parameter  $\chi_{FH}$  characterizes the solvent-polymer interaction energy; the lower this parameter, the stronger the attraction between solvent and polymer. *Figure 2* shows that our vapor-liquid-equilibrium data are fit reasonably well by adjusting  $\chi_{FH}$ . *Table 3* gives fitted  $\chi_{FH}$  values and indicates that the solvent power of n-alkanes decreases (increasing  $\chi_{FH}$ ) with rising alkane carbon number.

### *Prigogine-Flory-Patterson Theory*

The Prigogine-Flory-Patterson theory gives a reduced equation of state

$$\frac{\tilde{P}\tilde{v}}{\tilde{T}} = \frac{\tilde{v}^{1/3}}{\tilde{v}^{1/3} - 1} - \frac{1}{\tilde{v}\tilde{T}} \quad (4)$$

where temperature  $T$ , pressure  $P$ , and specific volume  $v$ , are reduced, respectively, by characteristic parameters  $T^*$ ,  $P^*$ , and  $v^*$  such that

$$\tilde{T} = \frac{T}{T^*} \quad (5); \quad \tilde{v} = \frac{v}{v^*} \quad (6); \quad \tilde{P} = \frac{P}{P^*}. \quad (7)$$

A binary mixture requires six pure-component parameters:  $T_1^*$ ,  $T_2^*$ ,  $v_1^*$ ,  $v_2^*$ ,  $P_1^*$ , and  $P_2^*$ . For pure solvents and polymers, these parameters are found from volumetric data. *Table 4* shows pure-component parameters for PIB and n-alkanes; we define  $T^*$  in Kelvin,  $v^*$  in  $\text{cm}^3/\text{g}$ , and  $P^*$  in  $\text{cal}/\text{cm}^3$ .

For the mixture,  $T^*$  and  $P^*$  depend on composition according to

$$T^* = \frac{P^*}{\left(\frac{P_1^*}{T_1^*}\right)\Phi_1^* + \left(\frac{P_2^*}{T_2^*}\right)\Phi_2^*} \quad (8)$$

and

$$P^* = P_1^* \Phi_1^* + P_2^* \Phi_2^* - \Phi_1^* \theta_2 X_{12} \quad (9)$$

where  $\Phi_1^*$ ,  $\Phi_2^*$ ,  $\theta_1$ , and  $\theta_2$  are, respectively, the segment fractions and surface fractions of the solvent and polymer and given by

$$\Phi_2^* = 1 - \Phi_1^* = \frac{m_2 v_2^*}{m_1 v_1^* + m_2 v_2^*} \quad (10)$$

and

$$\theta_2 = 1 - \theta_1 = \frac{(s_2/s_1)\Phi_2^*}{\Phi_1^* + (s_2/s_1)\Phi_2^*} \quad (11)$$

where  $m_1$  and  $m_2$  are the masses of solvent and polymer, respectively. Because solvent and polymer segments are chosen to have the same core volume, the segment-surface ratio  $s_2/s_1$  is the ratio of surfaces per unit core volume and can be estimated from structural data, as tabulated, for example, by Bondi<sup>15</sup>. However, Flory and Höcker<sup>16</sup> note that using group surface-area increments by Bondi overestimates the available surface area of polymers because it ignores shielding of constituent groups by intramolecular contacts between near-neighbors in the polymer chain. Thus, we follow Flory et al.<sup>17</sup> and calculate  $s_2/s_1$  from crystallographic data as follows. We consider n-alkanes to be right cylinders with length  $L_1 = 1.19n + 1.32 \text{ \AA}$ , mean radius  $R_1 = 2.49 \text{ \AA}$ , molecular surface area  $A_1$ , and core molar volume  $V_1^*$ . Similarly, we consider polyisobutylene to be a right cylinder divided into repeat units with length  $L_u = 2.325 \text{ \AA}$ , radius  $R_u = 3.48 \text{ \AA}$ , molecular surface area  $A_u$ , and core molar volume  $V_u^*$ . The ratio  $s_2/s_1$  is then calculated by

$$\frac{s_2}{s_1} = \frac{A_u}{A_1} \frac{V_1^*}{V_u^*}. \quad (12)$$

Molecular surface areas are defined by

$$A_1 = 2\pi R_1 L_1 + 2\pi R_1^2 \quad (13) \quad \text{and} \quad A_u = 2\pi R_u L_u \quad (14)$$

and core molar volumes are defined by

$$V_1^* = \pi R_1^2 L_1 N_{av} \quad (15) \quad \text{and} \quad V_u^* = \pi R_u^2 L_u N_{av} \quad (16)$$

where  $N_{av}$  is Avogadro's number.

For the mixture, the reduced volume  $\tilde{v}$  can be conveniently determined by following the procedure of Flory et al.<sup>18</sup>. First, we define an ideal reduced volume

$$\tilde{v}^0 = \Phi_1^* \tilde{v}_1 + \Phi_2^* \tilde{v}_2 \quad (17)$$

where

$$\tilde{v}_1 = \frac{v_1}{v_1^*} \quad (18) \quad \text{and} \quad \tilde{v}_2 = \frac{v_2}{v_2^*}. \quad (19)$$

The reduced volume of the real mixture is given by

$$\tilde{v} = \tilde{v}^0 + \tilde{v}^E. \quad (20)$$

The excess volume is calculated from

$$\tilde{v}^E = \left( \frac{\partial \tilde{v}}{\partial \tilde{T}} \right) (\tilde{T} - \tilde{T}^0) = \frac{3(\tilde{v}^0)^{7/3}}{4 - 3(\tilde{v}^0)^{1/3}} (\tilde{T} - \tilde{T}^0) \quad (21)$$

where the reduced temperature corresponding to  $\tilde{v}^0$  is found by rearranging Equation (4)

for  $P = 0$  such that

$$\tilde{T}^0 = \frac{(\tilde{v}^0)^{1/3} - 1}{(\tilde{v}^0)^{4/3}}. \quad (22)$$

Equation (21) provides an excellent approximation for polymer solutions at low or moderate pressures where pressure has a negligible effect on thermodynamic properties.

The solvent activity is then given by

$$\ln a_1 = \ln \Phi_1^* + \left(1 - \frac{r_1}{r_2}\right) \Phi_2^* + \frac{P_1^* M_1 v_1^*}{RT} \left[ 3\tilde{T}_1 \ln \frac{\tilde{v}_1^{1/3} - 1}{\tilde{v}^{1/3} - 1} + \left(\frac{1}{\tilde{v}_1} - \frac{1}{\tilde{v}}\right) \right] + \frac{M_1 v_1^*}{RT} \left(\frac{X_{12}}{\tilde{v}}\right) \theta_2^2 \quad (23)$$

where  $M_1$  is the solvent molecular weight and  $R$  is the universal gas constant. The interchange-interaction parameter,  $X_{12}$ , measures the energy change upon formation of a solvent-polymer segment contact from a solvent-solvent and a polymer segment-polymer segment contact. The lower the value of  $X_{12}$ , the stronger the attraction between solvent and polymer.

*Figure 3* shows solvent-activity data fitted with the Prigogine-Flory-Patterson theory. As shown in *Table 5*,  $X_{12}$  increases from  $C_6$  to  $C_8$ , but surprisingly decreases from  $C_8$  to  $C_9$ . Similar results for  $X_{12}$ , however, have been reported by Kasprzycka-Guttman et al.<sup>19,20</sup> who measured heats of mixing for  $\gamma$ -picoline in  $C_6$  through  $C_{10}$  n-alkanes and found that  $X_{12}$  is not monotonic with alkane carbon number.

A significant advantage of the Prigogine-Flory-Patterson theory is its ability to account for negative enthalpies of mixing without necessarily assigning negative interchange energies. Instead, observed negative enthalpies of mixing are accounted for with equation-of-state contributions, e.g. negative excess volumes upon mixing. Delmas et al.<sup>21</sup> obtained enthalpy-of-mixing data for mixtures of PIB and n-alkanes and found them to be negative and to decrease in magnitude from  $C_6$  to  $C_{10}$  n-alkanes. Using the

Prigogine-Flory-Patterson theory, Flory et al.<sup>17</sup> calculated  $X_{12}$  from these enthalpy-of-mixing data and showed that  $X_{12}$  is positive and decreases with rising alkane carbon number, as shown in *Table 6*. For mixtures of nonpolar molecules, such as PIB and n-alkanes, the interchange energy should be small and positive. Further, it is expected that the interchange energy decreases with alkane carbon number; as carbon number  $\rightarrow \infty$ , the contact energy for mixing polymethylene segments and PIB should decline to a small value.

As Eichinger and Flory<sup>22</sup> pointed out, however,  $X_{12}$  found from enthalpy-of-mixing data does not agree well with  $X_{12}$  found from solvent-activity data. Therefore, we follow the proposed extension of the Prigogine-Flory-Patterson theory by Orwoll and Flory<sup>23</sup> and express solvent activity by

$$\ln a_1 = \ln \Phi_1^* + \left(1 - \frac{r_1}{r_2}\right) \Phi_2^* + \frac{P_1^* M_1 v_1^*}{RT} \left[ 3\tilde{T}_1 \ln \frac{\tilde{v}_1^{1/3} - 1}{\tilde{v}^{1/3} - 1} + \left(\frac{1}{\tilde{v}_1} - \frac{1}{\tilde{v}}\right) \right] + \frac{M_1 v_1^*}{RT} \left( \frac{X_{12}}{\tilde{v}} - TQ_{12} \right) \theta_2^2 \quad (24)$$

where parameter  $Q_{12}$  accounts for the interaction entropy. *Figure 4* shows that upon introducing  $Q_{12}$ , vapor-liquid-equilibrium data measured here can be fitted using Flory's  $X_{12}$  values obtained from enthalpy-of-mixing data. *Table 6* lists fitted  $TQ_{12}$ .

A deficiency of the Prigogine-Flory-Patterson theory may follow from overestimating the magnitude of  $\tilde{v}^E$ , thereby underestimating  $X_{12}$ . A larger negative  $\tilde{v}^E$  causes  $X_{12}$  to become less positive. *Table 7* shows that the Prigogine-Flory-Patterson theory significantly overestimates the magnitude of  $\tilde{v}^E$  in mixtures of PIB and

n-alkanes investigated by Flory et al.<sup>17</sup>.

A comparison of results shown in *Figures 2-4* indicates that our data are not fit better with the Prigogine-Flory-Patterson theory than with the Flory-Huggins theory. Application of the Prigogine-Flory-Patterson theory may be less successful than hoped because pure-component parameters for polyisobutylene vary with molecular weight. We used pure-component parameters reported by Eichinger and Flory<sup>24</sup> based on a viscosity-average molecular weight of ca.  $4 \times 10^4$ , whereas the molecular weight of the sample used here is ca.  $4.7 \times 10^6$ , two orders of magnitude larger. Although theory predicts that VLE behavior should converge at high polymer molecular weights, experimental data do not always agree with this prediction. For example, Wang et al.<sup>25</sup> showed that diethyl-ether solubility significantly depended on polymer molecular weight in high-molecular-weight poly(butyl methacrylate).

## CONCLUSIONS

New vapor-liquid-equilibrium data for polyisobutylene in n-alkanes indicate that alkane solubility decreases as alkane carbon number rises. Data were reduced using the Flory-Huggins theory and the Prigogine-Flory-Patterson theory. Both theories give a fair representation of the data. An extended Prigogine-Flory-Patterson theory correlates the vapor-liquid-equilibrium data using Flory's  $X_{12}$  parameters calculated from enthalpy-of-mixing data.

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**Table 1** Solvent and polymer properties

Substance	Supplier	Lot Number	Purity
n-hexane	Aldrich Chemical Co., Inc.	13004CR	99+%
n-heptane	Sigma-Aldrich	06438LQ	99+%
n-octane	Aldrich Chemical Co., Inc.	JR01557HR	99+%
n-nonane	Aldrich Chemical Co., Inc.	ER10504PQ	99%
polyisobutylene	Aldrich Chemical Co., Inc.	AF03243TZ	

**Table 2** Vapor-liquid-equilibrium data for polyisobutylene in n-alkanes at 65°C

$w_1$  = solvent weight fraction in the liquid phase

$\Phi_1$  = solvent segment fraction in the liquid phase

$a_1 = P / P_1^{\text{sat}}$  = solvent activity

$P$  = vapor pressure in Torr

$P_1^{\text{sat}}$  = pure-solvent saturation pressure (calculated from equations suggested by Daubert and Danner<sup>26</sup>) in Torr

Solvent: n-Hexane; $P_1^{\text{sat}} = 671$ Torr			Solvent: n-Heptane; $P_1^{\text{sat}} = 255$ Torr		
$w_1$	$\Phi_1$	$a_1$	$w_1$	$\Phi_1$	$a_1$
0.011	0.016	0.117	0.017	0.023	0.122
0.030	0.043	0.232	0.040	0.055	0.243
0.060	0.085	0.343	0.067	0.091	0.367
0.087	0.122	0.464	0.097	0.130	0.487
0.121	0.167	0.580	0.135	0.178	0.604
0.162	0.219	0.694	0.179	0.232	0.720
0.217	0.287	0.792	0.237	0.301	0.829
0.292	0.374	0.890	0.292	0.364	0.904
0.401	0.493	0.967	0.350	0.428	0.972
			0.451	0.533	1.000
Solvent: n-Octane; $P_1^{\text{sat}} = 96$ Torr			Solvent: n-Nonane; $P_1^{\text{sat}} = 37$ Torr		
$w_1$	$\Phi_1$	$a_1$	$w_1$	$\Phi_1$	$a_1$
0.021	0.028	0.171	0.021	0.027	0.137
0.040	0.053	0.276	0.053	0.068	0.320
0.065	0.085	0.427	0.073	0.094	0.453
0.091	0.119	0.550	0.104	0.132	0.591
0.122	0.157	0.670	0.134	0.169	0.720
0.156	0.199	0.777	0.167	0.208	0.863
0.199	0.250	0.879			

**Table 3** Flory-Huggins interaction parameter for polyisobutylene in n-alkanes at 65°C

n-Alkane	$\chi_{FH}$
C <sub>6</sub>	0.612
C <sub>7</sub>	0.637
C <sub>8</sub>	0.860
C <sub>9</sub>	0.877

**Table 4** Pure-component parameters for the Prigogine-Flory-Patterson theoryParameters for polyisobutylene estimated from Eichinger and Flory<sup>24</sup> $v_1$  and  $P_1^*$  for n-alkanes estimated from Orwoll and Flory<sup>27</sup> $T_1^*$  and  $v_1^*$  for n-alkanes estimated from Flory et al.<sup>28</sup> $s_2/s_1$  calculated from structural data following Flory et al.<sup>17</sup>

Substance	$v_i$ (cm <sup>3</sup> /g)	$v_i^*$ (cm <sup>3</sup> /g)	$T_i^*$ (K)	$P_i^*$ (cal/cm <sup>3</sup> )	$s_2/s_1$
n-hexane	1.620	1.162	4510	97	0.549
n-heptane	1.551	1.144	4757	99	0.565
n-octane	1.503	1.126	4946	100	0.577
n-nonane	1.465	1.115	5096	102	0.587
polyisobutylene	1.114	0.952	7820	105	

**Table 5** Interchange-interaction parameter  $X_{12}$  fitted to solvent-activity data

n-Alkane	$X_{12}$ (cal/cm <sup>3</sup> )
C <sub>6</sub>	2.00
C <sub>7</sub>	2.21
C <sub>8</sub>	3.69
C <sub>9</sub>	3.36

**Table 6** Flory's  $X_{12}$  from enthalpy-of-mixing data and fitted  $TQ_{12}$  using an extended Prigogine-Flory-Patterson theory;  $T = 338.15$  K

n-alkane	$X_{12}$ (cal/cm <sup>3</sup> )	$TQ_{12}$ (cal/cm <sup>3</sup> )
C <sub>6</sub>	1.75	-0.205
C <sub>7</sub>	1.28	-0.770
C <sub>8</sub>	1.05	-2.191
C <sub>9</sub>	0.91*	-2.045

\* estimated

**Table 7** Calculated and observed  $\tilde{v}^E$  for binary solutions of polyisobutylene in n-alkanes investigated by Flory et al.<sup>17</sup>

n-Alkane	$\tilde{v}_{\text{observed}}^E \times 100$	$\tilde{v}_{\text{calculated}}^E \times 100$	% Overestimation*
C <sub>5</sub>	-1.583	-1.920	21.3
C <sub>6</sub>	-1.043	-1.214	16.4
	-1.053	-1.191	13.2
	-0.995	-1.066	7.1
C <sub>7</sub>	-0.749	-0.902	20.3
C <sub>8</sub>	-0.578	-0.661	14.4
	-0.582	-0.653	12.3
	-0.564	-0.624	10.6
C <sub>10</sub>	-0.342	-0.399	16.6
	-0.349	-0.396	13.4
	-0.330	-0.428	30.0
C <sub>16</sub>	-0.092	-0.131	42.9
	-0.095	-0.131	37.5
	-0.092	-0.118	28.2

\* 
$$\frac{(\tilde{v}_{\text{observed}}^E - \tilde{v}_{\text{calculated}}^E)}{\tilde{v}_{\text{observed}}^E} \times 100\%$$



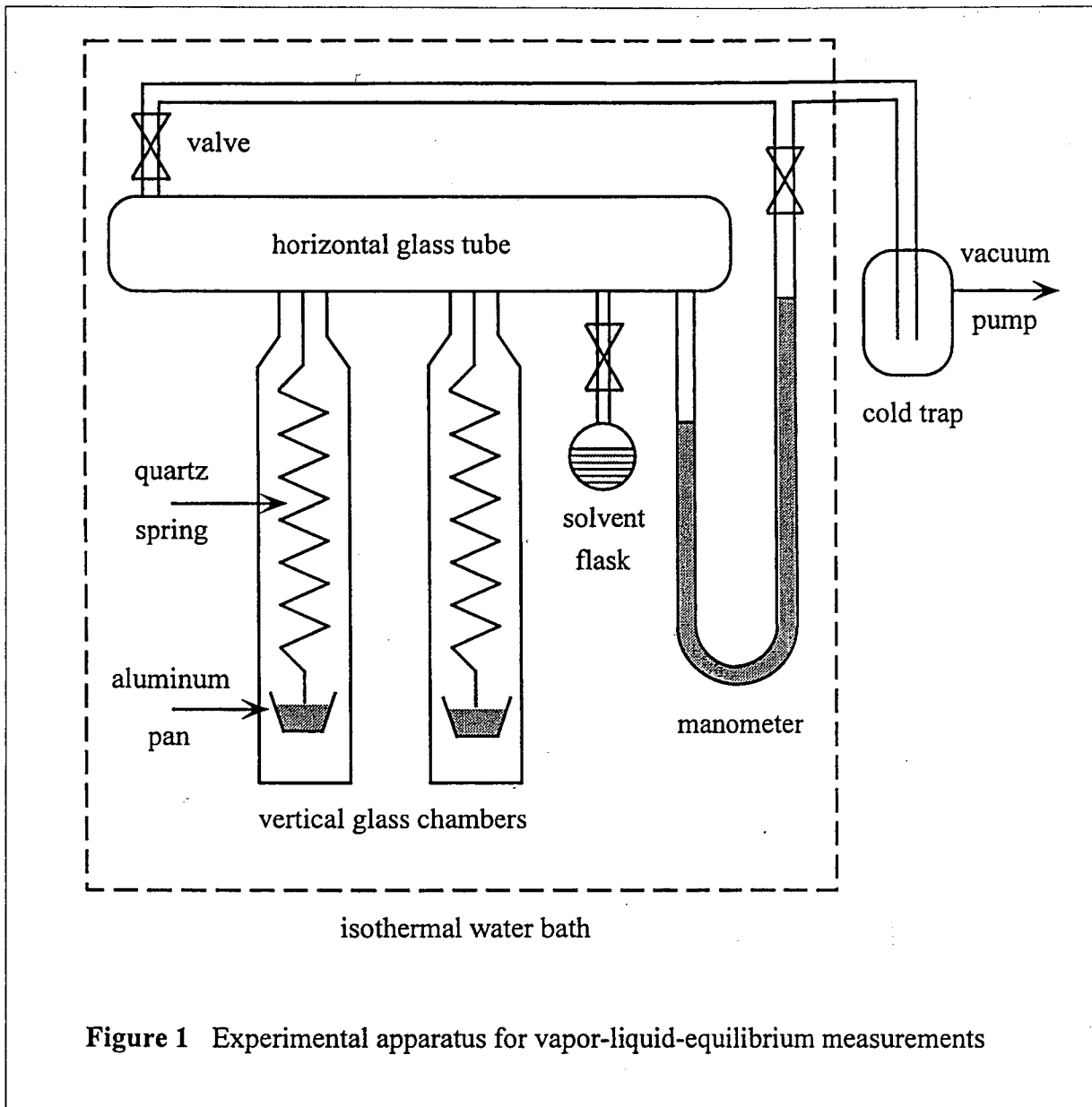
## Figure Captions

**Figure 1** Experimental apparatus for vapor-liquid equilibrium measurements.

**Figure 2** Calculated solvent activities (solid lines) for binary solutions of polyisobutylene in n-alkanes at 65°C; data fitted with the Flory-Huggins equation; points are experimental

**Figure 3** Calculated solvent activities (solid lines) for binary solutions of polyisobutylene in n-alkanes at 65°C; data fitted with the Prigogine-Flory-Patterson equation of state; points are experimental

**Figure 4** Calculated solvent activities (solid lines) for binary solutions of polyisobutylene in n-alkanes at 65°C; data fitted with an extended Prigogine-Flory-Patterson equation of state; points are experimental



**Figure 1** Experimental apparatus for vapor-liquid-equilibrium measurements

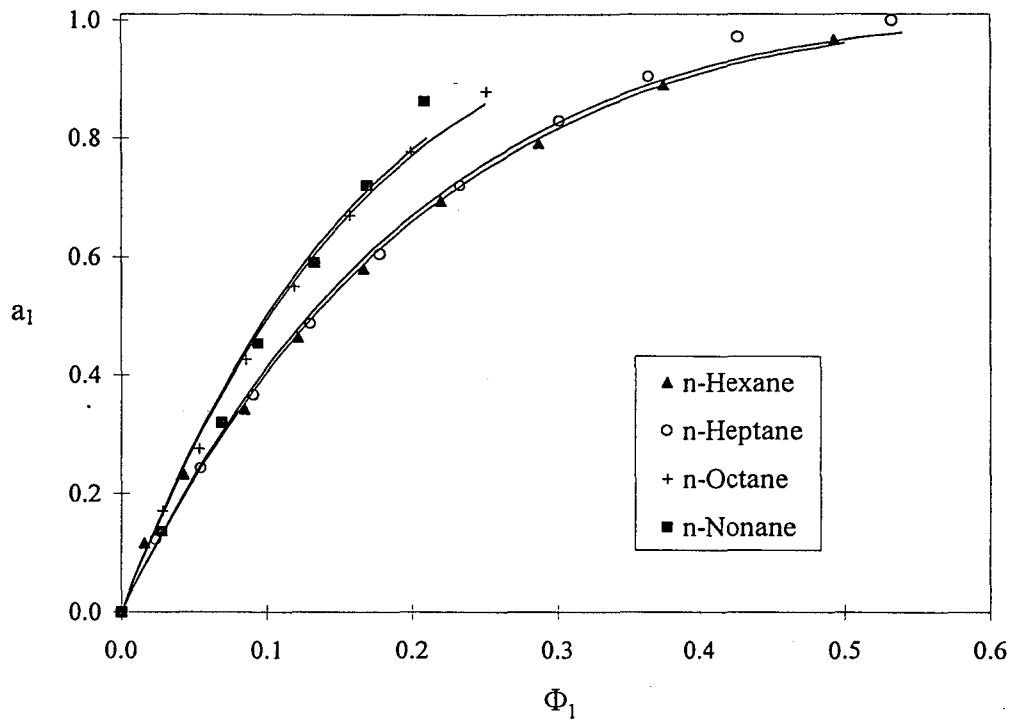


Figure 2

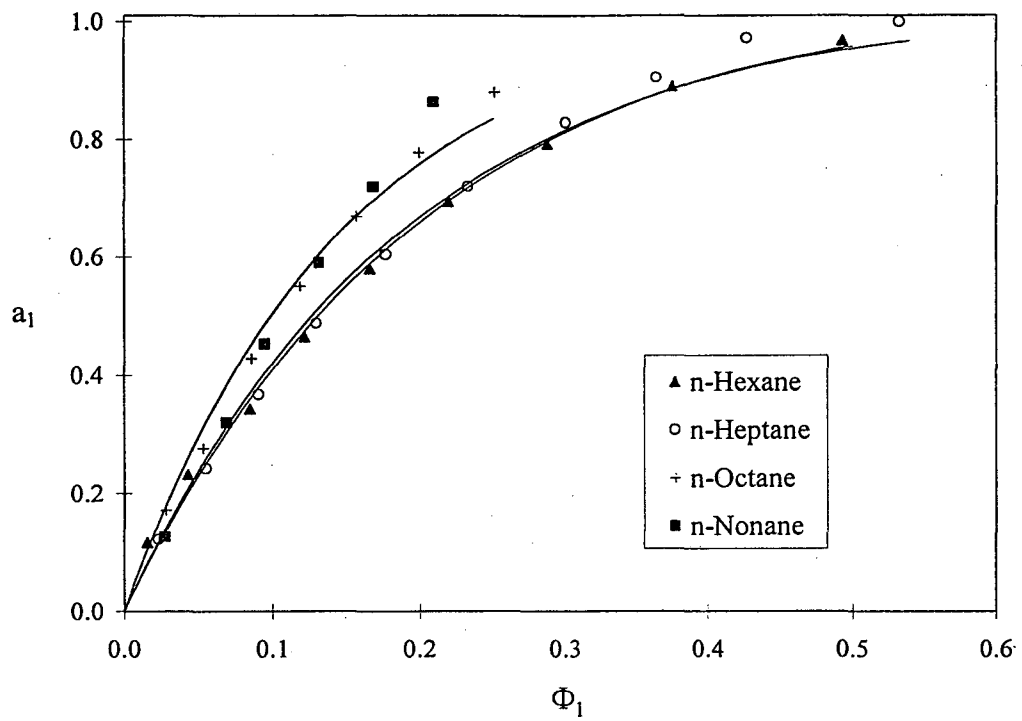


Figure 3

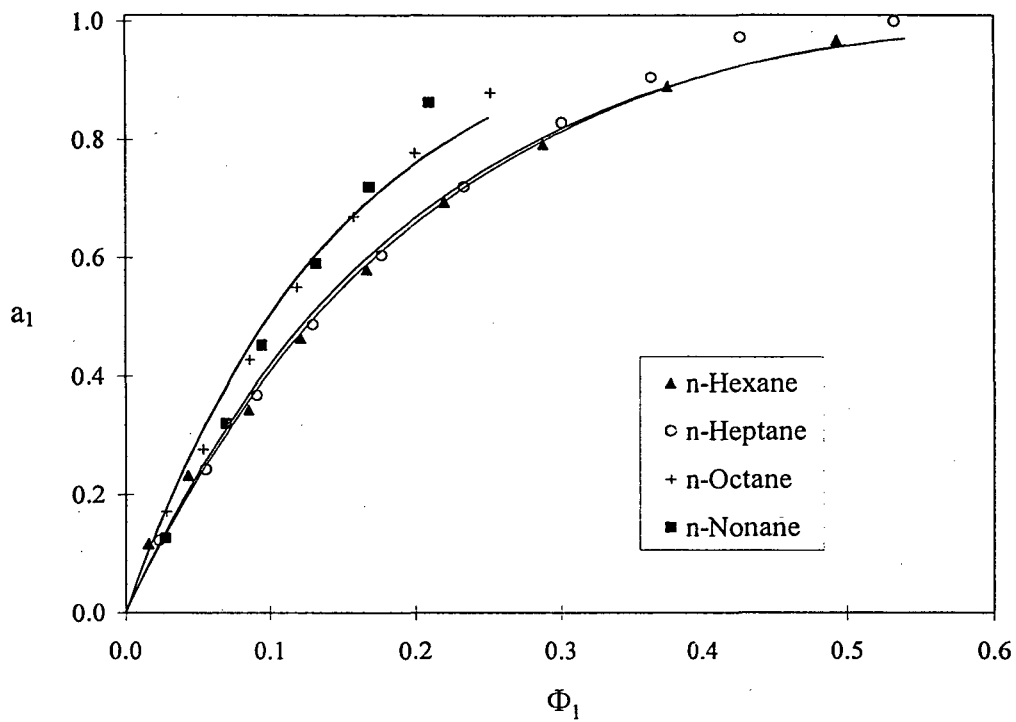


Figure 4

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