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1 **Closed-Form Analytic Solution of Cloud Dissipation for a Mixed Layer**

2 **Model**

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ABSTRACT

8 Stratocumulus clouds play an important role in climate cooling and are hard
9 to predict using global climate and weather forecast models. Thus, previ-
10 ous studies in the literature use observations and numerical simulation tools,
11 such as Large Eddy Simulation (LES), to solve the governing equations for
12 the evolution of stratocumulus clouds. In contrast to the previous works, this
13 work provides an analytic closed-form solution to the cloud thickness evolu-
14 tion of stratocumulus clouds in a mixed layer model framework. With a focus
15 on application over coastal lands, the diurnal cycle of cloud thickness and
16 whether or not clouds dissipate are of particular interest. An analytic solu-
17 tion enables the sensitivity analysis of implicitly interdependent variables and
18 extrema analysis of cloud variables that are hard to achieve using numerical
19 solutions. In this work, the sensitivity of inversion height, cloud base height
20 and cloud thickness with respect to initial and boundary conditions such as
21 Bowen Ratio, subsidence, surface temperature and initial inversion height are
22 studied. A critical initial cloud thickness value that can be dissipated pre
23 and post-sunrise is provided. Furthermore, an extrema analysis is provided
24 to obtain the minima and maxima of the inversion height and cloud thickness
25 within 24 hours. The proposed solution is validated against LES results under
26 the same initial and boundary conditions.

27 **1. Introduction**

28 Stratocumulus clouds (Sc) cover 21% of the earth's surface on average annually and have a
29 relatively high albedo resulting in a cooling contribution to climate (Klein and Hartmann (1993);
30 Eastman and Warren (2014)). Sc also impact Photovoltaic (PV) generation output in coastal areas
31 such as Southern California (Jamaly et al. (2013)). Sc are prevalent over the ocean and the coast
32 line, but less so inland, yet there are also studies focusing on continental Sc (e.g. Kollias and Al-
33 brecht (2000)). Their global abundance and the increase in coastal populations make it important
34 to accurately model and forecast their behavior. However, global forecast models fail to accurately
35 represent and forecast Sc (Bony (2005)).

36 Sc generally form under a strong inversion layer and the resulting boundary layer (BL) is spa-
37 tially homogeneous and well mixed day and night due to buoyant turbulence forcing from long-
38 wave cooling at the cloud top (Lilly (1968); Bretherton and Wyant (1997)). In observational stud-
39 ies, it has been shown that Sc can also form during the day under decoupled conditions, especially
40 for deeper BLs and stronger winds, temperature and moisture gradients, yet they are less preva-
41 lent to the well-mixed cases (Serpetzoglou et al. (2008); Rémillard et al. (2012)). Mixed layer
42 models (MLM) are therefore an appropriate tool and have been widely applied to Sc since the
43 groundbreaking work of Lilly (1968). Many studies improved physical model components such
44 as entrainment (Stevens (2002); Fang et al. (2014); Caldwell et al. (2005)), radiation (Larson et al.
45 (2007); Duynkerke (1999)), surface fluxes (Bretherton and Wyant (1997)), and advection (Seager
46 et al. (1995)). MLM are typically numerically integrated, validated against other numerical simu-
47 lations such as Large Eddy Simulation (LES), and applied to study specific cases or sensitivities in
48 the Sc topped BL (Stevens et al. (2005) and references within). Numerical integration is required
49 due to the fact that the MLM integro-differential equations are often very complex with multiple

50 feedback loops (Ghonima et al. (2016)). However, to understand interdependencies between vari-
51 ables or sensitivity of the system to a parameter, multiple case studies and simulations need to be
52 performed. Even then, hidden interdependencies or feedback effects may not be discovered using
53 trial and error methods.

54 There are also studies that use analytic models to understand the underlying behaviors (van der
55 Dussen et al. (2014); Duynkerke et al. (2004); Stevens (2002)). However, these studies focus on
56 the modeling of the physical phenomena with better analytic equations, rather than solving the
57 time evolution of cloud variables analytically.

58 In this work, we build up a physical MLM with radiation, buoyancy flux, and surface schemes
59 and use mathematical approximations to obtain a closed-form analytic solution to inversion height,
60 cloud base height, and ultimately cloud dissipation. The advantage of an analytic solution is that
61 the dependencies and sensitivities are observable directly from equations. For example, and re-
62 lated to our application of solar forecasting over coastal lands, the dependence of cloud thickness
63 on Bowen ratio can be directly inferred, given the initial conditions of the system. The tempo-
64 ral evolution of the system can be described without numerical approximations and steady state
65 conditions or attraction points can be detected.

66 We provide sensitivity and extrema analysis for inversion height, cloud base height and cloud
67 thickness, to infer how they depend on the initial and boundary conditions, and understand when
68 their minima and maxima occur during the diurnal cycle.

69 This paper is structured as follows. Section 2 provides a background on the models that consti-
70 tute the system of equations. In Section 3 the analytic solution is derived. In Section 4, closed-form
71 analytic solution is verified against LES and is shown to closely follow the numerical results. Sec-
72 tion 5 contains detailed analysis on the sensitivity of inversion height, cloud base height and cloud

73 thickness evolution in time with respect to the system parameters and initial conditions, and the
 74 timing of their extrema during the diurnal cycle.

75 The radiation and surface models used in this work are similar as in Ghonima et al. (2016), who
 76 use numerical time-stepping to solve a similar single-column mixed layer model. Even though the
 77 authors show that the MLM results are close to a more complex simulation method (LES), the un-
 78 derlying connections and interdependencies between the cloud variables and the initial conditions
 79 are not analyzed. Such an analysis using numerical solution techniques is impractical due to the
 80 vast number of variables in the solution space as shown in Figure 2 later, motivating our analytic
 81 solution to this problem.

82 2. Background

83 In this section, we define the models that approximate the physical processes. Consider a well
 84 mixed single vertical column with a single cloud layer bounded by its base height, z_b , and the
 85 inversion height, z_i . An illustration is shown in Figure 1. We assume constant air density ρ_{air} and
 86 constant values for the jumps at the inversion layer for total water mixing ratio, $\Delta q_{T, i}$, and liquid
 87 potential temperature, $\Delta \theta_{l, i}$, (Lilly (1968)).

88 The cloud thickness h is the primary parameter of interest and its tendency can be defined as:

$$\frac{dh(t)}{dt} = \frac{dz_i(t)}{dt} - \frac{dz_b(t)}{dt} \quad (1)$$

89 We use the inversion tendency definition from Caldwell et al. (2005) and Duynkerke et al.
 90 (2004), where the inversion height changes with the entrainment parameter, w_e and the subsi-
 91 dence, $w_s(z_i)$. Subsidence is further approximated by a divergence (Caldwell et al. (2005)):

$$\frac{dz_i}{dt} = w_e(t) + \mathbf{v}_H \nabla z_i = w_e(t) + w_s(z_i) = w_e(t) + D z_i(t) \quad (2)$$

92 The cloud base height tendency expression (Ghonima et al. (2015)) depends on the conserved
 93 variables of liquid potential temperature, θ_l and total moisture, q_T :

$$\frac{dz_b(t)}{dt} = \frac{R_d T_{\text{base}}}{g q_T(t)} \left(1 - \frac{L_v R_d}{c_p R_v T_{\text{base}}}\right)^{-1} \frac{dq_T(t)}{dt} + \frac{c_p \pi_{\text{base}}}{g} \left(1 - \frac{c_p R_v T_{\text{base}}}{R_d L_v}\right)^{-1} \frac{d\theta_l(t)}{dt} \quad (3)$$

94 R_d and R_v represent the gas constants for dry air and water vapor, respectively, L_v is the latent heat
 95 of evaporation, c_p is the specific heat, g is the gravitational acceleration, T_{base} is the temperature
 96 at the cloud base, π_{base} is the Exner function evaluated at the cloud base. In the following sections
 97 the inversion height and cloud base height tendencies are derived based on the budget equations
 98 for heat and moisture.

99 *a. Budget Equations for Conserved Moisture and Temperature Variables*

100 The MLM budget conservation equations are given for the liquid potential temperature and the
 101 total moisture as (Lilly (1968)):

$$\frac{d\theta_l(t)}{dt} = -\frac{\partial}{\partial z} \left(\overline{w'\theta_l'}(z,t) + \frac{F_{\text{rad}}(z,t)}{c_p \rho_{\text{air}}} \right) - \theta_{l, \text{adv}}, \quad \frac{dq_T(t)}{dt} = -\frac{\partial \overline{w'q_T'}}{\partial z} - q_{T, \text{adv}} \quad (4)$$

102 The large scale advection values of total moisture $q_{T, \text{adv}}$ and liquid potential temperature $\theta_{l, \text{adv}}$
 103 are assumed to be zero throughout this work. While advection effects are important for the MBL
 104 over coastal lands, the advection terms complicate the integration of the equations and are left for
 105 future study. $\overline{w'\theta_l'}(z,t)$ and $\overline{w'q_T'}(z,t)$ represent the average liquid potential temperature flux and
 106 average total moisture flux, respectively. F_{rad} represents the net radiation flux. Due to the well-
 107 mixed assumption, both conserved variables can be assumed to be independent of height. This
 108 forces the right hand side of the equations to be also independent of height, resulting in a linear
 109 height dependency for the partial derivatives. Representing the partial derivatives as E and W ,
 110 respectively, we can derive the full expressions using the boundary conditions at $z = 0$ and $z = z_i$,

111 as given in Bretherton and Wyant (1997):

$$\frac{d\theta_l}{dt} = -\frac{\partial E}{\partial z} \quad \frac{dq_T}{dt} = -\frac{\partial W}{\partial z} \quad (5)$$

$$E(z) = (1 - z/z_i)E(0) + (z/z_i)E(z_i) \quad W(z) = (1 - z/z_i)W(0) + (z/z_i)W(z_i) \quad (6)$$

112 The boundary conditions at the surface and inversion height are obtained as:

$$E(0) = \overline{w'\theta'_l}(0,t) + F_{\text{rad}}(0,t)/(\rho_{\text{air}}c_p) \quad E(z_i) = -w_e\Delta\theta_{l,i} + F_{\text{rad}}(z_i,t)/(\rho_{\text{air}}c_p) \quad (7)$$

$$W(0) = \overline{w'q'_T}(0,t) \quad W(z_i) = -w_e\Delta q_{T,i} \quad (8)$$

113 The final expressions for θ_l and q_T tendencies are obtained as:

$$\frac{d\theta_l(t)}{dt} = \frac{\overline{w'\theta'_l}(0,t)}{z_i(t)} + \frac{F_{\text{rad}}(0,t)}{\rho_{\text{air}}c_p z_i(t)} + \frac{w_e(t)\Delta\theta_{l,i}}{z_i(t)} - \frac{F_{\text{rad}}(z_i(t),t)}{\rho_{\text{air}}c_p z_i(t)} \quad (9)$$

$$\frac{dq_T(t)}{dt} = \frac{\overline{w'q'_T}(0,t)}{z_i(t)} + \frac{w_e(t)\Delta q_{T,i}}{z_i(t)} \quad (10)$$

114 *b. Radiation Model*

115 In this section we derive equations for the components of the net radiation flux and their at-
 116 tenuation through the cloud layer. Net radiation flux is decomposed into net longwave and net
 117 shortwave components:

$$F_{\text{rad}}(z,t) = F_{\text{lw}}(z,t) - F_{\text{sw}}(z,t) \quad (11)$$

118 1) LIQUID WATER PATH AND OPTICAL DEPTH

119 Both radiation terms are attenuated by an optical depth term designated as τ . This term depends
 120 on the total columnar liquid water content. We assume that the liquid water mixing ratio q_l within
 121 the cloud increases linearly with height proportional to a constant Γ_l , which can be calculated from

122 thermodynamics or observations:

$$q_l(z, t) = \begin{cases} \Gamma_l(z - z_b(t)), & z_b(t) \leq z \leq z_i(t) \\ 0, & \text{otherwise} \end{cases} \quad (12)$$

123 The liquid water path (LWP) then becomes:

$$\text{LWP}(z, t) = \int_{z'=z}^{z_i(t)} \rho_{\text{air}} q_l(z', t) dz' = \begin{cases} 0, & z > z_i(t) \\ \rho_{\text{air}} \Gamma_l ((z_i(t) - z_b(t))^2 - (z - z_b(t))^2) / 2, & z_b(t) \leq z \leq z_i(t) \\ \rho_{\text{air}} \Gamma_l (z_i(t) - z_b(t))^2 / 2, & z < z_b(t) \end{cases} \quad (13)$$

124 The optical depth τ is defined with respect to the optical depth at the cloud top which is assumed
125 to be zero. τ_b is the optical depth at and below the cloud base:

$$\tau(z, t) = \begin{cases} 0, & z > z_i(t) \\ \frac{3\rho_{\text{air}} \text{LWP}}{2R_e \rho_W} = \frac{3\rho_{\text{air}} \Gamma_l (h(t)^2 - (z - z_b(t))^2)}{4R_e \rho_W}, & z_b(t) \leq z \leq z_i(t) \\ \tau_b(t) \triangleq \frac{3\rho_{\text{air}} \Gamma_l h^2}{4R_e \rho_W}, & z < z_b(t) \end{cases} \quad (14)$$

126 ρ_W is the density of water and R_e is the effective droplet radius.

127 2) LONGWAVE RADIATION

128 For the longwave radiation, we utilize the model in Larson et al. (2007) which assumes isother-
129 mal blackbody radiation and single scattering. The net radiative longwave flux is defined as:

$$F_{\text{lw}}(z, t) = L_{\text{lw}}(t) e^{\alpha_{\text{lw}} \tau(z, t)} + M_{\text{lw}}(t) e^{-\alpha_{\text{lw}} \tau(z, t)} \quad (15)$$

130 α_{lw} represents the optical depth scale for longwave radiation. The coefficients L and M are ob-
 131 tained by solving the second order radiation differential equation in Goody (1995):

$$L_{lw}(t) = \gamma(t) \left((B_{cld}(t) - B_{sky}(t))c_{1, lw}e^{-\alpha_{lw}\tau_b(t)} + (B_{srf}(t) - B_{cld}(t))c_{2, lw} \right) \quad (16)$$

$$M_{lw}(t) = \gamma(t) \left((B_{cld}(t) - B_{sky}(t))c_{2, lw}e^{\alpha_{lw}\tau_b(t)} + (B_{srf}(t) - B_{cld}(t))c_{1, lw} \right) \quad (17)$$

132 The coefficients are defined as:

$$\gamma(t) = \frac{-4\pi(1 - \omega_{lw})}{c_{1, lw}^2 e^{-\alpha_{lw}\tau_b(t)} - c_{2, lw}^2 e^{\alpha_{lw}\tau_b(t)}} \quad (18)$$

$$c_{1, lw} = \alpha_{lw} - 2(1 - \omega_{lw}) \quad (19)$$

$$c_{2, lw} = \alpha_{lw} + 2(1 - \omega_{lw}) \quad (20)$$

$$\alpha_{lw} = \sqrt{3(1 - \omega_{lw})(1 - \omega_{lw}g_{lw})} \quad (21)$$

133 ω_{lw} designates the single scattering albedo and g_{lw} is the asymmetry factor. The B_{cld} , B_{sky} and B_{srf}
 134 terms are blackbody radiation arising from T_{cld} , T_{sky} and T_{srf} .

$$B_{cld}(t) = \frac{\sigma}{\pi} T_{cld}(t)^4, \quad B_{sky}(t) = \frac{\sigma}{\pi} T_{sky}(t)^4, \quad B_{srf}(t) = \frac{\sigma}{\pi} T_{srf}(t)^4 \quad (22)$$

135 T_{cld} and T_{srf} designate the effective radiation temperatures of the cloud base and ground surface,
 136 respectively. T_{sky} is the effective radiation temperature of the column above the cloud top.

137 3) SHORTWAVE RADIATION

138 We utilize the Delta-Eddington approximation in Duynkerke et al. (2004) and Shettle and Wein-
 139 man (1970) as shortwave radiation model. Using the Eddington approximation, the diffuse radi-
 140 ance can be divided into a linear combination of a term independent of the solar zenith angle (θ_0)
 141 and a solar zenith angle dependent term, yielding the analytic solution for the net shortwave radi-
 142 ation flux as:

$$F_{ls}(z, t) = F_0 \mu_0(t) \left(\frac{4p}{3} L_{sw}(t) e^{k\tau(z, t)} + \frac{4p}{3} M_{sw}(t) e^{-k\tau(z, t)} + e^{-\tau(z, t)/\mu_0(t)} \left(1 - \frac{4}{3} \beta_{sw}(t) \right) \right) \quad (23)$$

143 ω_{sw} designates the single scattering albedo for shortwave radiation, g_{sw} is the asymmetry factor,
 144 $\mu_0 = \cos(\theta_0)$, A is the surface albedo and k is the optical depth scale for shortwave radiation. Note
 145 that the incoming downward shortwave radiation F_0 is different from the net shortwave radiation
 146 at the cloud top ($F_{l_s}(z_i, t)$) as the net radiation includes radiation reflected from clouds and/or the
 147 ground surface. The coefficients are:

$$\beta_{\text{sw}}(t) = 3\omega_{\text{sw}} \frac{1 + 3g_{\text{sw}}(1 - \omega_{\text{sw}})\mu_0(t)^2}{4(1 - k^2\mu_0(t)^2)} \quad (24)$$

$$L_{\text{sw}}(t) = \frac{e^{-k\tau_b(t)} (\alpha_{\text{sw}} + 2\beta_{\text{sw}}/3) m_1}{e^{k\tau_b(t)} m_2 (1 + 2p/3) - e^{-k\tau_b(t)} m_1 (1 - 2p/3)} - \frac{(1 + 2p/3)e^{-\tau_b(t)/\mu_0(t)} (A(\alpha_{\text{sw}} + 2\beta_{\text{sw}}/3 - 1) - (\alpha_{\text{sw}} - 2\beta_{\text{sw}}/3))}{e^{k\tau_b(t)} m_2 (1 + 2p/3) - e^{-k\tau_b(t)} m_1 (1 - 2p/3)} \quad (25)$$

$$M_{\text{sw}}(t) = \frac{e^{k\tau_b(t)} (\alpha_{\text{sw}} + 2\beta_{\text{sw}}/3) m_2}{e^{k\tau_b(t)} m_2 (1 + 2p/3) - e^{-k\tau_b(t)} m_1 (1 - 2p/3)} - \frac{(1 - 2p/3)e^{-\tau_b(t)/\mu_0(t)} (A(\alpha_{\text{sw}} + 2\beta_{\text{sw}}/3 - 1) - (\alpha_{\text{sw}} - 2\beta_{\text{sw}}/3))}{e^{k\tau_b(t)} m_2 (1 + 2p/3) - e^{-k\tau_b(t)} m_1 (1 - 2p/3)} \quad (26)$$

$$m_1 = A(1 + 2p/3) - (1 - 2p/3), \quad m_2 = A(1 - 2p/3) - (1 + 2p/3) \quad (27)$$

$$k = \sqrt{3(1 - \omega_{\text{sw}})(1 - \omega_{\text{sw}}g_{\text{sw}})}, \quad p = \sqrt{\frac{3(1 - \omega_{\text{sw}})}{1 - \omega_{\text{sw}}g_{\text{sw}}}} \quad (28)$$

$$\alpha_{\text{sw}}(t) = 3\omega_{\text{sw}}\mu_0(t) \frac{1 + g_{\text{sw}}(1 - \omega_{\text{sw}})}{4(1 - k^2\mu_0(t)^2)} \quad (29)$$

148 c. Boundary Conditions

149 To close the system of budget equations the boundary conditions at the ground surface and
 150 inversion are needed. Entrainment at the top can be expressed as a function of the virtual potential
 151 temperature flux, $\overline{w'\theta'_v}$, through a convective velocity scale w^* defined as in Turton and Nicholls
 152 (1987), Caldwell et al. (2005) and Bretherton et al. (1999):

$$w^{*3} = \frac{2.5g}{\theta_{v,0}} \int_{z=0}^{z=z_i} \overline{w'\theta'_v}(z, t) dz, \quad w_e(t) = w^* \frac{A_w}{\text{Ri}}, \quad \text{Ri} = \frac{gz_i \Delta\theta_{v,i}}{\theta_{v,0} w^{*2}} \quad (30)$$

153 A_w is a tuning parameter, $\theta_{v,0}$ is a reference virtual potential temperature and Ri is the Richardson
 154 number. Combining the velocity scale equations and the Richardson number, we obtain:

$$w_e(t) = \frac{2.5A_w}{z_i(t)\Delta\theta_{v,i}} \int_{z=0}^{z_i(t)} \overline{w'\theta'_v}(z,t) dz \quad (31)$$

155 Finally, we need the surface boundary conditions to close the system of equations. Surface
 156 fluxes of heat and water are connected to the net surface radiation through surface flux efficiency,
 157 α_{srf} and the Bowen Ratio, β as (Ghonima et al. (2016)):

$$\text{SHF}(t) = \overline{w'\theta'_1}(0,t)c_p\rho_{\text{air}} = -\alpha_{\text{srf}} \left(\frac{\beta}{\beta + 1} \right) F_{\text{rad}}(0,t) \quad (32)$$

$$\text{LHF}(t) = \overline{w'q'_T}(0,t)L_v\rho_{\text{air}} = -\alpha_{\text{srf}} \left(\frac{1}{\beta + 1} \right) F_{\text{rad}}(0,t) \quad (33)$$

158
 159 $\alpha_{\text{srf}} = 0.88$ is applied in all simulations while Bowen Ratio is also constant for a particular simu-
 160 lation, but will vary from simulation to simulation to investigate effects of soil moisture content.

161 Interdependencies of atmospheric variables are abundant as illustrated in Figure 2 through a
 162 automatically generated dependency graph.

163 3. Analytic Closed-Form Solution

164 a. Inversion Height Tendency

165 The objective of this section is to obtain a closed form solution for Eq. (2). This requires the
 166 entrainment velocity in Eq. (31) which depends on the virtual potential temperature flux $\overline{w'\theta'_v}(z,t)$.
 167 The virtual potential temperature flux depends on the surface heat fluxes as (Bretherton and Wyant
 168 (1997)):

$$\overline{w'\theta'_v}(z,t) = c_{1,3}\overline{w'\theta'_1}(z,t) + c_{2,4}\overline{w'q'_T}(z,t) \quad (34)$$

169 From the surface to the cloud base height the coefficients $c_{1,3} = c_1$ and $c_{2,4} = c_2$ are used. For
 170 the cloud layer, spanning from the cloud base height to the inversion height, $c_{1,3} = c_3$ and $c_{2,4} =$
 171 c_4 (Bretherton and Wyant (1997)).

172 We start by scaling Eq. (9) and Eq. (10) by $c_{1,3}$ and $c_{2,4}$, respectively and summing them up:

$$c_{1,3} \frac{d\theta_1}{dt} + c_{2,4} \frac{dq_T}{dt} = \frac{\overline{w'\theta'_v}(0,t) + c_3 w_e(t) \Delta\theta_{1,i} + c_4 w_e(t) \Delta q_{T,i}}{z_i(t)} + \frac{c_1 F_{\text{rad}}(0,t) - c_3 F_{\text{rad}}(z_i,t)}{\rho_{\text{air}} c_p z_i(t)} \quad (35)$$

173 The left hand side can also be expressed using Eq. (4):

$$\begin{aligned} c_{1,3} \frac{d\theta_1}{dt} + c_{2,4} \frac{dq_T}{dt} &= -c_{1,3} \frac{\partial}{\partial z} \left(\overline{w'\theta'_1}(z,t) + \frac{F_{\text{rad}}(z,t)}{c_p \rho_{\text{air}}} \right) - c_{2,4} \frac{\partial \overline{w'q'_T}(z,t)}{\partial z} \\ &= -c_{1,3} \frac{\partial}{\partial z} \left(\frac{F_{\text{rad}}(z,t)}{c_p \rho_{\text{air}}} \right) - \frac{\partial \overline{w'\theta'_v}(z,t)}{\partial z} \end{aligned} \quad (36)$$

174 Eq. (35) and Eq. (36) are equal to each other. We use the fact that the left side of both Eq. (35)
 175 and Eq. (36) are independent of z due to the well mixed assumption, to take the integral of both
 176 equations from $z = 0$ to an arbitrary z . Leaving the virtual potential temperature flux on the left
 177 side of the equation, the expression becomes:

$$\begin{aligned} \overline{w'\theta'_v}(z,t) &= c_1 \frac{F_{\text{rad}}(0,t)}{c_p \rho_{\text{air}}} - c_{1,3} \frac{F_{\text{rad}}(z,t)}{c_p \rho_{\text{air}}} + \overline{w'\theta'_v}(0,t) \\ &+ \frac{z}{z_i(t)} \left(\frac{c_3 F_{\text{rad}}(z_i,t) - c_1 F_{\text{rad}}(0,t)}{\rho_{\text{air}} c_p} - \overline{w'\theta'_v}(0,t) - w_e(t) (c_3 \Delta\theta_{1,i} + c_4 \Delta q_{T,i}) \right) \end{aligned} \quad (37)$$

178 Utilizing the same scaling operation as in Eq. (35) for the surface flux definitions from Eq. (33)
 179 and Eq. (32):

$$\begin{aligned} \frac{c_1}{c_p \rho_{\text{air}}} \text{SHF} + \frac{c_2}{L_v \rho_{\text{air}}} \text{LHF} &= c_1 \overline{w'\theta'_1}(0,t) + c_2 \overline{w'q'_T}(0,t) = \overline{w'\theta'_v}(0,t) \\ &= -\frac{F_{\text{rad}}(0,t)}{\beta + 1} \left(\frac{\alpha_{\text{srf}} \beta c_1}{c_p \rho_{\text{air}}} + \frac{c_2 \alpha_{\text{srf}}}{\rho_{\text{air}} L_v} \right) \end{aligned} \quad (38)$$

180 Substituting Eq. (38) into Eq. (37), we obtain:

$$\begin{aligned} \overline{w'\theta'_v}(z,t) &= \frac{F_{\text{rad}}(0,t)}{c_p \rho_{\text{air}}} \left(c_1 - \frac{\alpha_{\text{srf}} \beta c_1}{\beta + 1} - \frac{c_2 \alpha_{\text{srf}} c_p}{L_v (\beta + 1)} \right) - c_{1,3} \frac{F_{\text{rad}}(z,t)}{c_p \rho_{\text{air}}} \\ &+ \frac{z}{z_i(t)} \left(\frac{c_3 F_{\text{rad}}(z_i,t)}{\rho_{\text{air}} c_p} - \frac{F_{\text{rad}}(0,t)}{\rho_{\text{air}} c_p} \left(c_1 - \frac{\alpha_{\text{srf}} \beta c_1}{\beta + 1} - \frac{c_2 \alpha_{\text{srf}} c_p}{L_v (\beta + 1)} \right) - w_e(t) (c_3 \Delta\theta_{1,i} + c_4 \Delta q_{T,i}) \right) \end{aligned} \quad (39)$$

181 Next, we integrate $\overline{w'\theta'_v}(z, t)$ over the boundary layer depth to obtain the entrainment velocity w_e
 182 in Eq. (31):

$$w_e(t) = \frac{2.5A_w}{z_i \Delta\theta_{v,i}} \left[\int_{z=0}^{z=z_i} \left(1 - \frac{z}{z_i}\right) F_{\text{rad}}(0, t) \left(\frac{c_1}{c_p \rho_{\text{air}}} - \frac{\alpha_{\text{srf}} \beta c_1}{c_p \rho_{\text{air}} (\beta + 1)} - \frac{c_2 \alpha_{\text{srf}}}{\rho_{\text{air}} L_v (\beta + 1)} \right) dz \right. \\ \left. - \int_{z=0}^{z=z_i} \frac{c_{1,3}}{c_p \rho_{\text{air}}} F_{\text{rad}}(z, t) dz + \int_{z=0}^{z=z_i} \frac{z}{z_i} \left(\frac{c_3 F_{\text{rad}}(z_i, t)}{c_p \rho_{\text{air}}} - w_e (c_3 \Delta\theta_{1,i} + c_4 \Delta q_{T,i}) \right) dz \right] \quad (40)$$

183 Combining all w_e terms on the left side, we obtain:

$$w_e(t) \left(\frac{0.8 \Delta\theta_{v,i}}{A_w} + c_3 \Delta\theta_{1,i} + c_4 \Delta q_{T,i} \right) = F_{\text{rad}}(0, t) \left(\frac{c_1}{c_p \rho_{\text{air}}} - \frac{\alpha_{\text{srf}} \beta c_1}{c_p \rho_{\text{air}} (\beta + 1)} - \frac{c_2 \alpha_{\text{srf}}}{\rho_{\text{air}} L_v (\beta + 1)} \right) \\ + \frac{c_3}{c_p \rho_{\text{air}}} F_{\text{rad}}(z_i, t) - \frac{2}{z_i c_p \rho_{\text{air}}} \int_{z=0}^{z=z_i} c_{1,3} F_{\text{rad}}(z, t) dz \quad (41)$$

184 Substituting this result in Eq. (2) we obtain the inversion height tendency:

$$\frac{dz_i(t)}{dt} - D z_i = \zeta_1 F_{\text{rad}}(0, t) + \zeta_2 F_{\text{rad}}(z_i, t) + \frac{\zeta_3}{z_i} \int_{z=0}^{z=z_i} c_{1,3} F_{\text{rad}}(z, t) dz \quad (42)$$

185 where ζ coefficients are employed to simplify the equation. This is a nonlinear differential equa-
 186 tion. Each net radiation term depends on the cloud thickness through the optical depth term.
 187 Furthermore, the columnar integral of the net radiation is called a Dawson function and is not an
 188 analytic function. Thus, an analytic solution requires approximations as explained in Section 3c.

189 *b. Cloud Thickness Tendency*

190 In addition to the inversion height tendency the cloud thickness tendency requires the cloud base
 191 height tendency. The solution strategy is to manipulate Eq. (3) into simpler variables analogous to
 192 the derivation of the inversion height tendency. The total moisture and liquid potential temperature
 193 tendencies appear in Eq. (3), but their tendencies given in Eq. (9) and Eq. (10), depend on z_i^{-1} .
 194 Since inversion height is a complex expression itself, it would be difficult to solve the tendencies
 195 in their current form. To simplify the inversion height dependency, we multiply both differential

196 equations by z_i and add $\theta_1 \frac{dz_i}{dt}$ and $q_T \frac{dz_i}{dt}$, respectively, so that the resulting expressions are the
 197 derivatives of the product of the conserved variables with the inversion height:

$$\begin{aligned} \frac{d(\theta_1(t)z_i(t))}{dt} &= \overline{w'\theta_1'}(0,t) + \frac{F_{\text{rad}}(0,t)}{\rho_{\text{air}}c_p} + w_e(t)\theta_{1,\text{inv}} - w_e(t)\theta_1(t) - \frac{F_{\text{rad}}(z_i(t),t)}{\rho_{\text{air}}c_p} + \theta_1(t)\frac{dz_i}{dt} \\ \frac{d(q_T(t)z_i(t))}{dt} &= \overline{w'q_T'}(0,t) + w_e(t)q_{T,\text{inv}} - w_e(t)q_T(t) + q_T(t)\frac{dz_i}{dt} \end{aligned}$$

198 This manipulation simplifies the right side of the differential equation by eliminating the inversion
 199 height term. Only its tendency remains. Using the inversion tendency (Eq. (2)) and the surface
 200 fluxes (Eq. (32), Eq. (33)) we obtain:

$$\frac{d(\theta_1(t)z_i(t))}{dt} - D(\theta_1(t)z_i(t)) = \left(\frac{\beta + 1 - \alpha_{\text{srf}}\beta}{\rho_{\text{air}}c_p(\beta + 1)} \right) F_{\text{rad}}(0,t) - \frac{F_{\text{rad}}(z_i(t),t)}{\rho_{\text{air}}c_p} + w_e(t)\theta_{1,\text{inv}} \quad (43)$$

$$\frac{d(q_T(t)z_i(t))}{dt} - D(q_T(t)z_i(t)) = -\frac{\alpha_{\text{srf}}}{L_v\rho_{\text{air}}(\beta + 1)} F_{\text{rad}}(0,t) + w_e(t)q_{T,\text{inv}} \quad (44)$$

201 Note that we again need the net radiation expressions as in the inversion height expression to solve
 202 these differential equations. Finally, we use the cloud thickness tendency in Ghonima et al. (2015)
 203 to obtain the cloud thickness:

$$\frac{dh}{dt} = \frac{dz_i(t)}{dt} - \frac{R_d T_{\text{base}}}{g q_T(t)} \left(1 - \frac{L_v R_d}{c_p R_v T_{\text{base}}} \right)^{-1} \frac{dq_T(t)}{dt} - \frac{c_p \Pi_b}{g} \left(1 - \frac{c_p R_v T_{\text{base}}}{R_d L_v} \right)^{-1} \frac{d\theta_1(t)}{dt} \quad (45)$$

204 *c. Approximation of Net Radiation Flux Term*

205 The net radiation flux appears in three forms: 1) surface $F_{\text{rad}}(0,t)$, 2) inversion height
 206 $F_{\text{rad}}(z_i(t),t)$, and 3) columnar average $\frac{1}{z_i(t)} \int_{z=0}^{z=z_i(t)} F_{\text{rad}}(z,t) dz$. We start with the approximations
 207 for the net longwave expressions at $z = 0$ and z_i based on Eq. (15). Then we continue with the
 208 net shortwave expressions at $z = 0$ and z_i . Finally, we approximate the columnar integral of net
 209 radiation as a linear combination of the net radiation at $z = 0$ and z_i .

$$F_{\text{lw}}(z = 0, t) = L_{\text{lw}}(t)e^{\alpha_{\text{lw}}\tau_b(t)} + M_{\text{lw}}(t)e^{-\alpha_{\text{lw}}\tau_b(t)} \quad (46)$$

210

$$F_{\text{lw}}(z = z_i, t) = L_{\text{lw}}(t) + M_{\text{lw}}(t) \quad (47)$$

211 We simplify these expressions by neglecting higher order (< -1) exponential optical depth terms
 212 ($\exp(-\alpha_{lw}\tau_b)$) as follows:

$$F_{lw}(z, t) \simeq \frac{4\pi(1 - \omega_{lw})(B_{srf} - B_{cld})}{c_2} + \frac{8\pi\alpha_{lw}(1 - \omega_{lw})(B_{cld} - B_{sky})}{c_2^2} e^{-\alpha_{lw}\tau_b} \quad (48)$$

$$F_{lw}(z_i(t), t) \simeq \frac{4\pi(1 - \omega_{lw})(B_{cld} - B_{sky})}{c_2} + \frac{8\pi\alpha_{lw}(1 - \omega_{lw})(B_{srf} - B_{cld})}{c_2^2} e^{-\alpha_{lw}\tau_b} \quad (49)$$

213 Even though this simplification is not required for the analytic solution, it simplifies the sensitivity
 214 analysis in Section 5 and the error is less than 1%. Specifics for the error estimation are provided
 215 in Appendix B.b

216 To permit integration of net shortwave radiation into the cloud tendency expressions, we need
 217 to simplify solar zenith angle dependent terms, since solar zenith angle changes with time in
 218 a sinusoidal shape and complex nonlinear dependencies on μ_0 such as in Eq. (29) or the third
 219 exponential in Eq. (23) are difficult to integrate. We use the following approximations for α_{sw} and
 220 β_{sw} in Eq. (29) and Eq. (24), with less than 2% and 1% error, respectively (see Appendix B.c).

$$\alpha_{sw} \simeq 3\mu_0\omega_{sw} \frac{1 + g_{sw}(1 - \omega_{sw})}{4}, \quad \beta_{sw} \simeq 3\omega_{sw}/4 \quad (50)$$

221 To approximate the net shortwave radiation at the inversion height, we use its mathematical
 222 bounds at: clear sky, $\tau = 0$, and infinite depth, $\tau \rightarrow \infty$.

$$F_{ls}(z = z_i, \tau_b = 0) = F_0\mu_0(1 - A), \quad F_{ls}(z = z_i, \tau_b \rightarrow \infty) = F_0\mu_0\left(1 - \frac{4\beta_{sw}}{3 + 2p}\right) + F_0\mu_0\frac{4p\alpha_{sw}}{3 + 2p} \quad (51)$$

223 The following approximation assumes an exponential dependence of net shortwave radiation on
 224 optical depth between these limits. The error of approximation is less than 6% (see Appendix B.c):

$$F_{ls}(z = z_i) \simeq F_{ls}(z = z_i, \tau_b \rightarrow \infty) + (F_{ls}(z = z_i, \tau_b \rightarrow \infty) - F_{ls}(z = z_i, \tau_b = 0)) e^{-2k\tau_b} \quad (52)$$

225 The net shortwave radiation at the surface is approximated in terms of the value at the inversion
 226 height scaled by a factor of attenuation depending on the optical depth, with an error of less than

227 7% (see Appendix B.c):

$$F_{ls}(z=0) \simeq F_{ls}(z=z_i)e^{-k\tau_b} \quad (53)$$

228 The columnar integral of net (shortwave and longwave) radiation flux can be approximated by
 229 a linear combination of net radiation values at the surface and inversion height with an error of
 230 6% (see Appendix B.d):

$$\frac{1}{z_i} \int_{z=0}^{z_i} F_{rad}(z,t) dz \simeq s_1 F_{rad}(z=0) + s_2 F_{rad}(z=z_i), \quad s_1 = 0.99, s_2 = 0.04 \quad (54)$$

231 *d. Inversion Height Solution*

232 Using the simplified, integrable approximations for the net radiation terms a closed-form so-
 233 lution for the inversion height in Eq. (42) can be obtained. The columnar integral expression in
 234 Eq. (54) is employed to write Eq. (42) as a combination of net radiation terms at the surface and
 235 inversion height.

$$\frac{dz_i(t)}{dt} - Dz_i(t) = \psi_1(t)F_{rad}(0,t) + \psi_2(t)F_{rad}(z_i,t) \quad (55)$$

$$\psi_1 \triangleq \frac{\frac{c_1}{c_p \rho_{air}} - \frac{\alpha_{srf} \beta c_1}{c_p \rho_{air} (\beta + 1)} - \frac{c_2 \alpha_{srf}}{\rho_{air} L_v (\beta + 1)} - \frac{2s_1}{c_p \rho_{air}}}{\frac{0.8 \Delta \theta_{v,i}}{A_w} + c_3 \Delta \theta_{l,i} + c_4 \Delta q_{T,i}}, \quad \psi_2 \triangleq \frac{\frac{c_3 - 2s_2}{c_p \rho_{air}}}{\frac{0.8 \Delta \theta_{v,i}}{A_w} + c_3 \Delta \theta_{l,i} + c_4 \Delta q_{T,i}} \quad (56)$$

236 The solution strategy is to find all time dependent variables inside the net radiation expressions
 237 and then solve the differential equation. For net longwave (Eq. (15)) the blackbody radiations are
 238 time dependent and for net shortwave (Eq. (52) and (53)) the solar zenith angle is time dependent.
 239 Furthermore, both radiation terms depend on the optical depth exponentially and optical depth
 240 depends on the square of the cloud thickness given in Eq. (14). We use two approximations, which
 241 are further discussed in the following paragraphs: 1) Surface, cloud base, and cloud top effective
 242 temperatures are constant over a 24 hour period. As a result the blackbody radiation terms are
 243 constants. 2) The change in cloud thickness h is negligible compared to the radiation length
 244 scales. This means that the effect of change in optical depth can be ignored *only* for radiation

245 terms resulting in constant exponential optical depth terms. The actual cloud thickness solution,
 246 $h(t)$, is not a constant and the actual time-dependent expression is presented in Section 3e.

247 The first approximation can be supported as follows: 1) The model is only valid in overcast
 248 conditions. In overcast conditions, the daily range in surface temperature compared to the ac-
 249 tual temperature is small, where the root mean square error (RMSE) of the constant temperature
 250 assumption is about 6%, 2) Surface and cloud base temperatures follow similar diurnal patterns
 251 decreasing the error of the difference of blackbody radiation differences in Eq. (16) and Eq. (17).
 252 The RMSE of a constant blackbody difference assumption is about 4%. 3) The change in surface
 253 and cloud base temperatures is largest near solar noon due to the peak in net shortwave irradiance
 254 at small solar zenith angle. However, at noon the net longwave radiation is only $\sim 10\%$ of the
 255 net shortwave radiation and therefore the longwave balance does not contribute significantly to the
 256 overall net radiation. In conclusion, it is justifiable to approximate the differences in blackbody
 257 radiations as constant. To further reduce the error, rather than using the initial temperatures at
 258 midnight, the mean temperatures of the previous day are used.

259 For the second approximation, we need to investigate the exponential optical depth terms for
 260 net longwave ($\exp(\alpha_{lw}\tau_b)$) and net shortwave ($\exp(k\tau_b)$) expressions separately. Using the optical
 261 depth expression in Eq. (14), the exponent of the shortwave radiation can be written in the form of:
 262 $(h(t)/h_{sw})^2$, where $h_{sw} \triangleq \sqrt{(4R_e\rho_w)/(3\rho_{air}\Gamma_l k)}$, and $h_{sw} \sim [250, 500]$ m for k taken from Shettle
 263 and Weinman (1970), R_e from Larson et al. (2007), and for Γ_l between $[0.5, 2] \times 10^{-6} \text{ m}^{-1}$. The
 264 cloud thickness has to change on the order of h_{sw} to cause a significant change in the value of the
 265 exponent. The same notation for longwave yields the exponent in the form of: $(h(t)/h_{lw})^2$ with
 266 $h_{lw} = \sqrt{(4R_e\rho_w)/(3\rho_{air}\Gamma_l\alpha_{lw})}$. $h_{lw} \gg h_{sw}$, resulting in an even smaller exponent value than the
 267 shortwave. For a cloud thickness of 250 m, the RMSE of keeping the exponential optical depth
 268 term constant with respect to a varying numerical optical depth solution is $\sim 7\%$ as demonstrated

269 in Appendix B.e. The appendix also provides comparisons of daily model runs for constant and
 270 variable optical thickness under different Bowen Ratios and Γ_l values. The constant optical thick-
 271 ness results follows the variable optical thickness results, but differences increase for greater Γ_l
 272 and smaller Bowen Ratios. Large Γ_l result in smaller h_{SW} scales, causing larger deviation from
 273 the constant optical thickness assumption, whereas smaller Bowen Ratios delay cloud dissipation
 274 resulting in the accumulation of errors over longer time horizons.

275 Using both approximations, the only time dependent terms are the solar zenith angle terms, $\mu_0(t)$
 276 and $\mu_0^2(t)$, and the inversion height tendency equation simplifies into:

$$\frac{dz_i(t)}{dt} - Dz_i(t) = a_1 + a_2\mu_0(t) + a_3\mu_0^2(t). \quad (57)$$

277 The solution of differential equations of type $\frac{dy}{dx} - Dy = f(x)$ is:

$$y(x) = y(0)e^{Dx} + e^{Dx} \int_{x'=0}^x e^{-Dx'} f(x') dx' \quad (58)$$

278 Assuming that $u_1(t)$, $u_2(t)$ and $u_3(t)$ are the solutions of

$$\frac{du_1}{dt} - Du_1 = 1, \quad \frac{du_2}{dt} - Du_2 = \mu_0, \quad \frac{du_3}{dt} - Du_3 = \mu_0^2 \quad (59)$$

279 we can write the inversion height as:

$$z_i(t) = z_i(0)e^{Dt} + a_1u_1(t) + a_2u_2(t) + a_3u_3(t) \quad (60)$$

280 We use the solar zenith angle definition of $\mu_0 = \max(\mu_1 + \mu_2 \cos(t\pi/H - \pi), 0)$, where $\mu_1 =$
 281 $\sin(\text{lat}) \sin(\text{dec})$, $\mu_2 = \cos(\text{lat}) \cos(\text{dec})$, lat is the local latitude, dec is the declination and H is 12
 282 hours. We solve for the functions u_1 , u_2 and u_3 using Eq. (58). The equations for a single day are

283 given below. The general forms for multiple days are more complex and provided in Appendix C.

$$u_1(t) = \frac{e^{Dt} - 1}{D} \quad (61)$$

$$u_2(t) = \mu_2 \frac{\pi H^{-1} \sin(t\pi/H - \pi) - D \cos(t\pi/H - \pi)}{D^2 + \pi^2 H^{-2}} + e^{Dt-Dt_1} \frac{\pi H^{-1} \left(\sqrt{\mu_2^2 - \mu_1^2} \right) + \mu_1 D^{-1} \pi^2 H^{-2}}{D^2 + \pi^2 H^{-2}} - \mu_1 D^{-1} \quad (62)$$

$$u_3(t) = 2\mu_1\mu_2 \frac{\pi H^{-1} \sin(t\pi/H - \pi) - D \cos(t\pi/H - \pi)}{D^2 + \pi^2 H^{-2}} + 2\mu_1 e^{Dt-Dt_1} \frac{\pi H^{-1} \sqrt{\mu_2^2 - \mu_1^2} - \mu_1 D}{D^2 + \pi^2 H^{-2}} + \frac{\mu_2^2}{2} \frac{2\pi H^{-1} \sin(2t\pi/H) - D \cos(2t\pi/H)}{D^2 + 4\pi^2 H^{-2}} + e^{Dt-Dt_1} \frac{\pi D(\mu_1^2 - \mu_2^2/2) - 2\mu_1 \pi H^{-1} \sqrt{\mu_2^2 - \mu_1^2}}{D^2 + 4\pi^2 H^{-2}} \quad (63)$$

284 The unit of these functions is seconds due to the time-integration. Using these functions, the
 285 inversion height can be calculated for any t without numerical integrations that would be required
 286 in mixed-layer models. The functional forms as plotted in Figure 3 directly reveal the following.
 287 At night time, when $\mu_0 = 0$, u_2 and u_3 follow the same exponential trend as u_1 as in $\exp(Dt)$
 288 with additional oscillatory terms, therefore u_2 and u_3 decrease during the night. u_1 also follows
 289 a negative exponential trend due to the negative sign of D . This means that the combined effect
 290 of all three functions causes the inversion height to change exponentially and the exponent is the
 291 subsidence divergence parameter, D . D is hard to determine and difficult to measure; it typically
 292 assumes values on the order of $-[10^{-6}, 10^{-5}] \text{ s}^{-1}$. During the day, u_2 and u_3 increase, dominate
 293 over u_1 and behave like a sigmoid function. The signs and magnitudes of the coefficients for the u
 294 functions also determine the trends for the cloud base height as will be shown in Section 5.

295 Since the initial condition $z_i(0)$ is scaled by $\exp(Dt)$, the analytic solution also shows that the
 296 e-folding time for the effect of the initial condition $z_i(0)$ on the inversion height to approach zero

297 is $1/D \sim 3$ days. This means that the initial inversion height has a negligible effect on the solution
 298 in ~ 3 days. Furthermore, since all u functions have the same exponential trend of $\exp(Dt)$,
 299 $z_i(t)$ converges within 5% of steady state in approximately $1/3D \sim 9$ days. Once $z_i(t)$ reaches
 300 the steady state solution, the inversion height oscillates with sinusoids of periods 12 hours and
 301 24 hours. However, in practice this finding is largely irrelevant as the synoptic meteorological
 302 conditions induce change over shorter time scales rendering the mixed layer model results not
 303 applicable.

304 *e. Cloud Thickness Solution*

305 In order to obtain the final cloud thickness expression, the cloud base height expression is sub-
 306 tracted from the inversion height expression. In Eq. (3) only q_T and θ_1 tendencies vary in time as
 307 the other terms are either constant or assumed constant due to the assumption of constant effective
 308 radiative temperature. We integrate Eq. (3) to obtain:

$$z_b(t) - z_b(0) = \frac{R_d T_{\text{base}}}{g} \left(1 - \frac{L_v R_d}{c_p R_v T_{\text{base}}} \right)^{-1} \ln \left(\frac{q_T(t)}{q_T(0)} \right) + \frac{c_p \Pi_b}{g} \left(1 - \frac{c_p R_v T_{\text{base}}}{R_d L_v} \right)^{-1} \theta_1(t) \quad (64)$$

309 Assuming the change in $q_T(t)$ to be small compared to its initial value, we use $\ln(x+1) \simeq x$ to
 310 linearize the expression and denote the coefficients of the time-varying terms as δ_1 and δ_2 :

$$z_b(t) - z_b(0) = \delta_1 (q_T(t) - q_T(0)) + \delta_2 (\theta_1(t) - \theta_1(0)) \quad (65)$$

$$\frac{dz_b(t)}{dt} = \delta_1 \frac{dq_T(t)}{dt} + \delta_2 \frac{d\theta_1(t)}{dt} \quad (66)$$

311 In Eq. (43) and Eq. (44) the $z_i q_T$ and $z_i \theta_1$ differentials are of the same functional form as the
 312 inversion height tendency. Thus, we manipulate the cloud base height expressions to obtain the
 313 same format so that the total moisture and liquid potential temperature results can be substituted
 314 directly. To achieve this, we multiply Eq. (65) by dz_i/dt and Eq. (66) by z_i and sum them up to

315 obtain:

$$\frac{d(z_i z_b)}{dt} = \delta_1 \frac{d(z_i q_T)}{dt} + \delta_2 \frac{d(z_i \theta_1)}{dt} + \frac{dz_i}{dt} (z_b(0) - \delta_1 q_T(0) - \delta_2 \theta_1(0)) \quad (67)$$

316 Scaling Eq. (65) by Dz_i and subtracting it from Eq. (67) yields:

$$\frac{dz_i z_b}{dt} - Dz_i z_b = \delta_1 \left(\frac{d(z_i q_T)}{dt} - Dz_i q_T \right) + \delta_2 \left(\frac{d(z_i \theta_1)}{dt} - Dz_i \theta_1 \right) \quad (68)$$

$$+ \left(\frac{dz_i}{dt} - Dz_i \right) (z_b(0) - \delta_1 q_T(0) - \delta_2 \theta_1(0)) \quad (69)$$

317 The $z_i q_T$ and $z_i \theta_1$ differentials can be substituted from Eq. (43) and Eq. (44):

$$\frac{dz_i(z_b - z_{adj})}{dt} - Dz_i(z_b - z_{adj}) = \frac{\delta_2(\beta + 1 - \alpha_{srf}\beta)L_v - \delta_1\alpha_{srf}c_p}{\rho_{air}c_p L_v(\beta + 1)} F_{rad}(0, t) - \frac{\delta_2 F_{rad}(z_i(t), t)}{\rho_{air}c_p} \quad (70)$$

318 where $z_{adj} \triangleq z_b(0) + \delta_1 \Delta \theta_{l,i} + \delta_2 \Delta q_{T,i}$. Aggregating all constant coefficients in ψ_3 and ψ_4 we

319 obtain:

$$\frac{dz_i(z_b - z_{adj})}{dt} - Dz_i(z_b - z_{adj}) = \psi_3 F_{rad}(0, t) + \psi_4 F_{rad}(z_i(t), t) \quad (71)$$

$$\psi_3 \triangleq \frac{\delta_2(1 - \alpha_{srf})}{\rho_{air}c_p} + \frac{\delta_2\alpha_{srf}L_v - \delta_1\alpha_{srf}c_p}{\rho_{air}c_p L_v(\beta + 1)}, \quad \psi_4 \triangleq -\frac{\delta_2}{\rho_{air}c_p} \quad (72)$$

320 Eq. (70) depends only on the radiation terms which already had been derived for the inversion

321 height expression:

$$z_i(t)(z_b(t) - z_{adj}) = z_i(0)(z_b(0) - z_{adj})e^{Dt} + b_0 u_1(t) + b_1 u_2(t) + b_2 u_3(t) \quad (73)$$

322 where the constants are combined into b_1 , b_2 and b_3 for convenience. Solving for the cloud base

323 height, we obtain:

$$z_b(t) = \frac{b_1 u_1(t) + b_2 u_2(t) + b_3 u_3(t) + z_i(0)(z_b(0) - z_{adj})e^{Dt}}{a_1 u_1(t) + a_2 u_2(t) + a_3 u_3(t) + z_i(0)e^{Dt}} + z_{adj} \quad (74)$$

324 And finally, the cloud thickness is obtained from $h(t) = z_i(t) - z_b(t)$.

325 4. Validation against LES

326 We verify our solution against Large Eddy Simulation (LES) specifically the UCLA-

327 LES (Stevens et al. (2005)) on a 100×100 grid with 193 vertical levels. The horizontal reso-

328 lution is 25 m and the vertical resolution is 5 m resulting in a domain of $2.5 \text{ km} \times 2.5 \text{ km} \times 960 \text{ m}$.
 329 The LES land surface model is a constant Bowen Ratio model that converts the incoming net
 330 radiation into SHF and LHF according to Eqs. (32) and Eq. (33). Initial conditions are CGILS
 331 s12 from Zhang et al. (2012) and initial profiles of q_T and θ_1 are shown in Figure 4. The initial
 332 inversion height is 677 m, the initial cloud thickness is 238 m and LWP is 72.4 g m^{-2} . LES is
 333 initialized at 03:00 LST. The results for the first hour of integrations are considered spin-up time
 334 and not shown. LES is run for 23 more hours with samples taken every 20 seconds and averaged
 335 over 10 minutes. LES inversion height, cloud base height, inversion jumps for total moisture and
 336 liquid potential temperature, total moisture at the surface, and the effective radiative temperatures
 337 at the surface (T_{srf}) and the cloud base (T_{clld}) at 04:00 LST serve as initial conditions for the ana-
 338 lytic model. The effective cloud top temperature (T_{sky}) is obtained from the LES longwave flux,
 339 the constant value of the exponential optical depth ($\exp(k\tau_b)$) is calculated from LES shortwave
 340 flux and the subsidence divergence (D) is extracted from LES using Eq. (2).

341 The validation consisted of two sets of sensitivity experiments: 1) Varying Bowen Ratio and 2)
 342 Varying $\Delta q_{T, i}$ jump at the inversion. Bowen Ratio sensitivity results in Figure 5 show agreement
 343 in the inversion height and cloud thickness time series, and cloud dissipation time; the inversion
 344 height RMSE compared to LES is less than 1.5% and the cloud thickness RMSE is less than 9%.

345 At this time, the cloud base height can also be compared against the *lifting condensation*
 346 *level* (LCL) - the level, where the moisture in air is expected to saturate based on surface tem-
 347 perature and relative humidity (Bolton (1980)). The LCL results for $\beta = 0.1$ and $\beta = 0.2$ in
 348 Figure 5 agree with our cloud thickness formulation. The small difference is due to the approx-
 349 imate nature of the LCL formulation. We use the current formulation (Ghonima et al. (2015))
 350 for the rest of this paper, since it is integrated with the simulated MLM profiles. In contrast, the

351 LCL formulation depends on near-surface temperature and relative humidity, which would require
352 additional equations to obtain the closed-form results.

353 Both inversion height (Eq. (56)) and cloud base height (Eq. (73)) were shown to depend on the
354 inversion jump, including the total moisture jump, $\Delta q_{T,i}$. Furthermore, the inversion jump also
355 affects entrainment and the turbulent fluxes through the boundary conditions (Eqs. (7), (8)). Even
356 though multiple interdependent variables depend on $\Delta q_{T,i}$, we are able to infer how $\Delta q_{T,i}$ affects
357 the cloud thickness through our analytic solution. A detailed sensitivity analysis is presented
358 in Section 5, where the analytic solution suggests that the inversion height decreases and cloud
359 thickness increases with smaller magnitude inversion jumps. For the validation, LES were run for
360 Bowen Ratios of 0.3 and 1 and the q_T jump was varied by $\mp 0.5 \text{ g kg}^{-1}$ (moister and drier air in
361 the free troposphere), while keeping the boundary layer value at 9.43 g kg^{-1} . Figure 6 shows that
362 the analytic solution closely follows LES results in both trend and dissipation times. The inversion
363 height RMSE compared to LES is again less than 1.5% and the cloud thickness RMSE is less than
364 5%. The cloud dissipates only for $\beta = 1$ and the time of dissipation differs only by 5 minutes.

365 5. Sensitivity Analysis

366 a. Inversion Height Sensitivity

367 In section 3, we found that the inversion height tendency is a linear combination of 3 functions:
368 u_1, u_2 and u_3 . The common property of these functions is that they generally increase exponentially
369 and the exponent is the subsidence divergence (D). The evolution of the inversion height in time
370 then depends on the coefficients of these functions given in Eq. (57), where the coefficients were
371 kept in their compact forms to emphasize the linear combination of the three functions. Now, we

372 write out these coefficients and analyze their dependence on the initial and boundary conditions.

$$a_1 = \frac{4\pi(1 - \omega_{lw})}{c_{2, lw}^2} ((c_{2, lw} \psi_1 + 2e_{lw} \alpha_{lw} \psi_2)(B_{srf} - B_{cld}) + (c_{2, lw} \psi_2 + 2e_{lw} \alpha_{lw} \psi_1)(B_{cld} - B_{sky})) \quad (75)$$

$$a_2 = -(\psi_2 + e_1 \psi_1) F_0 \left(1 - \frac{4\beta_{sw}}{3 + 2p} + e_2 \left(\frac{4\beta_{sw}}{3 + 2p} - A \right) \right) \quad (76)$$

$$a_3 = -(1 - e_2)(\psi_2 + e_1 \psi_1) F_0 \left(\frac{3p\omega_{sw}(1 + g_{sw}(1 - \omega_{sw}))}{3 + 2p} \right) \quad (77)$$

$$\psi_1 \triangleq \frac{\frac{c_1 - \alpha_{srf} c_1 - 2s_1}{c_p \rho_{air}} + \frac{\alpha_{srf}(c_1 L_v - c_2 c_p)}{c_p \rho_{air} L_v (\beta + 1)}}{\frac{0.8\Delta\theta_{v,i}}{A_w} + c_3 \Delta\theta_{1,i} + c_4 \Delta q_{T,i}}, \quad \psi_2 \triangleq \frac{\frac{c_3 - 2s_2}{c_p \rho_{air}}}{\frac{0.8\Delta\theta_{v,i}}{A_w} + c_3 \Delta\theta_{1,i} + c_4 \Delta q_{T,i}} \quad (78)$$

373 where for convenience, we defined $e_m \triangleq \exp(-mk\tau_b)$ and $e_{lw} \triangleq \exp(-\alpha_{lw}\tau_b)$ and remember that
374 the exponential optical depth value ($\exp(-k\tau_b)$) was assumed to be constant in Section 3d.

375 The turbulent flux coefficients in Eq. (34), $c_1 = 1, c_2 = 108 \text{ K}, c_3 = 0.5, c_4 = 970 \text{ K}$, and the
376 convective surface efficiency of $\alpha_{srf} = 0.9$ in Eq. (32) and Eq. (33) are obtained from Ghonima
377 et al. (2016). $A_w = 0.2$ in Eq. (30) is from Turton and Nicholls (1987). Constants related to
378 longwave radiation are from Larson et al. (2007) and shortwave radiation from Duynkerke et al.
379 (2004). The coefficients become:

$$a_1 \simeq \frac{(39.55 \times 10^{-12} \text{ m s}^{-1} \text{ K}^{-3})}{\zeta_D} \left(\left(\frac{1}{\beta + 1} - 2.29 + 0.52e_{lw} \right) (T_{srf}^4 - T_{cld}^4) + \left(\frac{e_{lw}}{\beta + 1} - 2.31e_{lw} + 0.51 \right) (T_{cld}^4 - T_{sky}^4) \right) \quad (79)$$

$$a_2 \simeq \frac{(0.23 \text{ m s}^{-1} \text{ K})(0.23 + e_2)}{\zeta_D} \left(2.3e_1 - 0.52 - \frac{e_1}{\beta + 1} \right), \quad a_3 \simeq (1 - e_2) \frac{a_2}{1.53} \quad (80)$$

$$\zeta_D \triangleq 4\Delta\theta_{v,i} + 0.5\Delta\theta_{1,i} + (970 \text{ K})\Delta q_{T,i} \quad (81)$$

380 where ζ_D aggregates the inversion jumps and has been defined for notational convenience. The
381 unit of ζ_D is K , $[\psi_1] = [\psi_2] = \text{W}^{-1} \text{ s}^{-1} \text{ m}^3$, and $[a_1] = [a_2] = [a_3] = \text{m s}^{-1}$.

382 Furthermore, a_2 is a scalar multiple of a_3 , so we can combine the $u_2(t)$ and $u_3(t)$ functions
383 into a new function $u_4(t) = u_2(t) + u_3(t) \frac{1 - e_2}{1.53}$. Combining the coefficients, the inversion height

384 expression becomes:

$$z_i(t) = z_i(0)e^{Dt} + a_1u_1(t) + a_2u_4(t) \quad (82)$$

385 The functions u_1 and u_4 are always positive. Thus, their combined tendency in time depends
386 on the sign and magnitude of their coefficients. ζ_D is the common denominator of all coefficients
387 and its only negative term is the inversion jump in total moisture. However, given the strong
388 temperature inversions for the stratocumulus-topped marine boundary layer, the total moisture
389 jump would have to be unrealistically large to create a negative sign for ζ_D . For example, if
390 $\Delta\theta_{v,i} = \Delta\theta_{l,i} = 10$ K, the jump in total moisture would have to be 33 g kg^{-1} to reverse the sign,
391 but typical values of q_T in the boundary layer are only 10 g kg^{-1} . Thus let us assume that $\zeta_D > 0$ K.

392 For the optical depth exponentials, e_1 and e_{lw} , a thinner cloud ranging between $[0,200]$ m
393 thickness and a thicker cloud in the interval $[200,400]$ m are analyzed. For the thinner cloud,
394 the optical depth variables are calculated as: $e_1 = 0.9, e_{lw} = 0.39$; and for the thicker cloud:
395 $e_1 = 0.7, e_{lw} = 0.03$. For the thin cloud case, a_2 is positive for all Bowen Ratios. For a_1 , there is a
396 balance between the cloud base-cloud top and surface-cloud base blackbody radiation differences,
397 slightly weighted towards the latter. The effect of Bowen Ratio is small due to its coefficient being
398 small relative to the rest of the terms. A low radiative temperature for the cloud base favors positive
399 a_1 , whereas high surface or effective cloud top temperatures favor negative a_1 . Using the standard
400 atmospheric lapse rate of -6.5 K km^{-1} and assuming that effective radiative temperature equals
401 air temperature, a_1 is always negative for the thin cloud case. A negative a_1 means that the in-
402 version height increases proportionally with the cloud top temperature and inversely proportional
403 with the surface temperature. This sounds counter-intuitive at first, as a large cloud top tempera-
404 ture would lead to a higher upwelling longwave radiation and thus faster cooling. However, for a
405 thin cloud with low optical depth, a large proportion of the downwelling longwave radiation from
406 the cloud top reaches the surface and contributes to the sensible heat flux. This leads to a tempera-

407 ture increase in the boundary layer, increasing the turbulent fluxes and entrainment, which results
408 in increased inversion height.

409 For the thick cloud case, a_2 is positive for all Bowen Ratios. The sign of a_1 depends on both
410 the Bowen Ratio and the radiative temperature balance. However, only the sign of the cloud top
411 temperature term (T_{sky}) is negative for all Bowen Ratios, thus the inversion height is inversely
412 proportional to cloud top temperature. The change in the direction of the effect for a thicker cloud
413 emerges since the cloud top net longwave radiation is attenuated through the cloud's high optical
414 thickness and only a negligible fraction reaches the surface.

415 To infer the combined effect of the oscillating terms in Eq. (82), we need the numerical values
416 of u_1 and u_4 . For $D = -3.75 \times 10^{-6} \text{ s}^{-1}$, Julian day of 196 and latitude 32.85° N , $u_4 \approx 8.2u_1$ in
417 magnitude on average. For typical effective radiative temperatures, it is physically impossible for
418 the weighted summation ($a_1u_1 + a_2u_4$) to be negative. For example, for thin clouds if $T_{\text{cld}} = T_{\text{sky}}$,
419 T_{srf} would have to be more than 560 K to cause a negative trend. Increasing Bowen Ratio increases
420 a_2 . Since u_4 is the dominant term, the combined trend increases with Bowen Ratio. To show this,
421 we fix T_{srf} , T_{cld} , ζ_D , D and vary the Bowen Ratio and T_{sky} , as shown in Figure 7.

422 Before sunrise $u_4 = 0$ such that the results represent only u_1 and all lines for both thin and
423 thick clouds show a downward slope since the negative term of a_1 is dominant. This comes from
424 the fact that a_1 includes only net longwave radiation terms. During the night, the net longwave
425 radiation causes the boundary layer to cool decreasing the inversion height. For the thin cloud
426 case, throughout the day higher cloud top temperatures are associated with larger inversion height
427 since the cloud's optical thickness is small enough to admit net longwave radiation to the surface,
428 which is converted into sensible heat flux and warms up the boundary layer. For the thick case, we
429 see exactly the opposite, where higher cloud top temperature lead to lower inversion heights. A

430 large optical thickness attenuates the cloud top radiation before it reaches the land surface, which
 431 results in a cooler mixing layer and reduces surface turbulent fluxes.

432 Larger Bowen Ratio causes z_i to increase by a factor of $1/(\beta + 1)$ as is illustrated by the spacing
 433 between the gray lines of constant Bowen Ratios for $T_{\text{sky}} = 280$ K. Decreased moisture content
 434 in the soil associated with larger Bowen Ratio increases the sensible heat flux and the warming
 435 increases the inversion height. Since the ratio of radiation flux converted into turbulent fluxes is
 436 fixed through α_{srf} , the rate of the increases in the sensible heat flux and inversion height slow with
 437 increasing Bowen Ratio as reflected in the closer line spacing. Finally, the trend of the inversion
 438 height is also affected inversely by ζ_D . A larger jump in potential temperature results in a smaller
 439 change in inversion height, whereas a larger jump in the magnitude of total water mixing ratio
 440 causes in contrast a greater change. This arises mainly from the fact that the turbulent fluxes are
 441 bounded by the negative of the inversion jumps at the inversion layer, as presented in Eqs. (7), (8).

442 *b. Cloud Base Height Sensitivity*

443 For the sensitivity analysis of the cloud base height from Eq. (74) it is enlightening to analyze
 444 $z_i(z_b - z_{\text{adj}})$ as – similar to z_i – its functional form is a linear combination of the three u functions
 445 in Eq. (73). The coefficients of u_1 , u_2 , and u_3 are:

$$b_1 = \frac{4\pi(1 - \omega_{\text{lw}})}{c_{2, \text{lw}}^2} ((c_{2, \text{lw}}\psi_3 + 2e_{\text{lw}}\alpha_{\text{lw}}\psi_4)(B_{\text{srf}} - B_{\text{cld}}) + (c_{2, \text{lw}}\psi_4 + 2e_{\text{lw}}\alpha_{\text{lw}}\psi_3)(B_{\text{cld}} - B_{\text{sky}})) \quad (83)$$

$$b_2 = -(\psi_4 + e_1\psi_3)F_0 \left(1 - \frac{4\beta_{\text{sw}}}{3 + 2p} + e_2 \left(\frac{4\beta_{\text{sw}}}{3 + 2p} - A \right) \right) \quad (84)$$

$$b_3 = -(1 - e_2)(\psi_4 + e_1\psi_3)F_0 \left(\frac{3p\omega_{\text{sw}}(1 + g_{\text{sw}}(1 - \omega_{\text{sw}}))\alpha_{\text{sw}}}{3 + 2p} \right) \quad (85)$$

446 with

$$\psi_3 \triangleq \frac{\delta_2(1 - \alpha_{\text{srf}})}{\rho_{\text{air}}c_p} + \frac{\delta_2\alpha_{\text{srf}}L_v - \delta_1\alpha_{\text{srf}}c_p}{\rho_{\text{air}}c_pL_v(\beta + 1)}, \quad \psi_4 \triangleq -\frac{\delta_2}{\rho_{\text{air}}c_p} \quad (86)$$

447 δ_1 and δ_2 from Eq. (66) are calculated using $q_T(0) = 9 \text{ g kg}^{-1}$ as -211590 m K^{-1} and
 448 125 m K^{-1} , respectively. The coefficients become:

$$b_1 \simeq (9.2 \times 10^{-9} \text{ m}^2 \text{ s}^{-1} \text{ K}^{-4}) \left(\left(\frac{1}{\beta + 1} + 1.88 - 2.21e_{lw} \right) (T_{srf}^4 - T_{cld}^4) \right. \\ \left. + \left(\frac{e_{lw}}{\beta + 1} + 1.88e_{lw} - 2.22 \right) (T_{cld}^4 - T_{sky}^4) \right) \quad (87)$$

$$b_2 \simeq (11 \text{ m}^2 \text{ s}^{-1})(0.235 + e_2) \left(7.33 - e_1 - \frac{12.43e_1}{\beta + 1} \right), \quad b_3 = (1 - e_2)b_2/1.53 \quad (88)$$

449 The units of ψ_3 and ψ_4 are $\text{W}^{-1} \text{ s}^{-1} \text{ m}^4$, and $[b_1] = [b_2] = [b_3] = \text{m}^2 \text{ s}^{-1}$. As for the inversion
 450 height (Eq. (82)), u_2 and u_3 are combined into u_4 :

$$z_i(z_b - z_{adj}) = z_i(0)(z_b(0) - z_{adj})e^{Dt} + b_1u_1(t) + b_2u_4(t) \quad (89)$$

451 As in the inversion height analysis in Section 5a, we consider two cases of thin and thick clouds
 452 with $e_1 = 0.9$, $e_{lw} = 0.39$ and $e_1 = 0.7$, $e_{lw} = 0.03$, respectively.

453 As with the coefficient of inversion height a_1 , for b_1 there is a balance between the surface-cloud
 454 base and cloud base-cloud top radiation differences. Using a lapse rate for a standard atmosphere
 455 b_1 is negative for any Bowen Ratio. The equation for b_2 is very similar to a_2 , except that for Bowen
 456 Ratios $\beta \geq 0.74$ for the thin cloud case and $\beta \geq 0.31$ for the thick cloud case, b_2 changes sign
 457 and becomes positive. The combined trend depends on the u_1 and u_4 functions. Since $u_4 \approx 8.2u_1$
 458 and b_2 is much greater than b_1 , b_2 is the dominant term in the equality. Therefore the sign of
 459 $z_i(z_b - z_{adj})$ changes with the sign of b_2 during daytime. To show this, similar to the inversion
 460 height analysis, the sensitivity of β and T_{sky} is shown in Figure 8. The results for the daytime
 461 reflect sign and magnitude variation in u_4 with Bowen Ratio. As expected, cloud base height starts
 462 to increase during daytime at a Bowen Ratio of 0.47 and the cloud base height increases with
 463 increasing Bowen Ratio. The sensitivity to cloud top temperature is small due to the dominance
 464 of u_4 . $z_i(z_b - z_{adj})$ is only an intermediate expression that allows understanding cloud base height

465 trends, but it does not have a physical meaning; instead Eq. (74) is considered now:

$$z_b(t) = z_b(0) + \frac{(b_1 + a_1(\delta_1 \Delta q_{T,i} + \delta_2 \Delta \theta_{l,i}))u_1(t) + (b_2 + a_2(\delta_1 \Delta q_{T,i} + \delta_2 \Delta \theta_{l,i}))u_4(t)}{z_i(0)e^{Dt} + a_1 u_1(t) + a_2 u_4(t)} \quad (90)$$

466 Using the values from the sensitivity analysis for $z_i(z_b - z_{adj})$ and z_i , and neglecting the u_1 terms
467 as u_4 is the dominant term during daytime:

$$z_b(t) \simeq z_b(0) + (4.34 \text{ m}^2)(0.23 + e_2) \left(15.6 + 13e_1 - \frac{38.6e_1}{\beta + 1} \right) \frac{u_4(t)}{z_i(0)e^{Dt}} \quad (91)$$

468 For the thin cloud case, cloud base height changes direction for $\beta \geq 0.27$, whereas for the thick
469 cloud case, the direction change occurs for $\beta \geq 0.1$. The cloud base height for different Bowen
470 Ratios is plotted in Figure 9. This result shows that the cloud base height trend changes direction
471 depending on the Bowen Ratio. Only a single cloud top temperature is shown as the effect of u_1 is
472 negligible. Increasing Bowen Ratio causes a decrease in the latent heat flux and an increase in the
473 sensible heat flux. The resulting drying and heating of the boundary layer increases the cloud base
474 height more than the inversion height. The cloud then dissipates faster with increasing Bowen
475 Ratios. The effect of Bowen Ratio decreases with increasing cloud optical thickness, as more
476 radiation is absorbed or reflected within the cloud resulting in smaller surface turbulent fluxes.

477 Furthermore, note that the cloud base height converges to a steady state:

$$z_b(t \rightarrow \infty) \simeq z_b(0) + \delta_1 \Delta \theta_{l,i} + \delta_2 \Delta q_{T,i} + \frac{b_2}{a_2} = z_{adj} + \frac{b_2}{a_2} \quad (92)$$

478 As shown earlier in this section, a_2 is positive and b_2 changes from negative to positive with higher
479 Bowen Ratios. Therefore, larger Bowen Ratios lead to larger steady state cloud base height.

480 *c. Cloud Thickness Sensitivity*

481 Using inversion height and cloud base height trends, we can directly infer the cloud thickness
482 sensitivity. In this section we study the maximum initial cloud thickness that can be dissipated 1)
483 before sunrise, 2) before sunset or whether the cloud dissipates within 24 hours at all.

484 1) CLOUD THICKNESS EVOLUTION

485 Fig. 10 shows the thickness evolution of a cloud with 200 m initial thickness (top) and the
 486 resulting surface shortwave radiative fluxes, especially important from the solar forecasting aspect
 487 (bottom). The expected dissipation times using Eq. (94) and Eq. (96), later presented in this
 488 section, are tabulated in Table 1 for the cases in Fig. 10. The initial conditions used for the cases
 489 are also shown in Fig. 4.

490 The dashed lines compare the effect of Bowen Ratio under normal subsidence for an initial
 491 inversion height of 1500 m. Under these conditions, Eq. (94) predicts that the cloud does not
 492 dissipate before sunrise, but Eq. (96) predicts that the cloud dissipates during the day if $\beta > 0.3$.
 493 As expected in the figure only $\beta = 0.2$ does not dissipate. The lines with markers compare the
 494 same Bowen Ratio scenarios for a lower initial inversion height of 500 m. Under these conditions,
 495 the cloud dissipates at about the same time as for the initial inversion height of 1500 m for $\beta = 0.6$
 496 and $\beta = 5$. Finally, the thick solid lines compare the effect of a strong subsidence for different
 497 initial inversion heights. As expected stronger subsidence decreases cloud thickness. For strong
 498 subsidence ($-1.875 \times 10^{-5} \text{ s}^{-1}$), Eq. (94) predicts that for $z_i(0) > 1050 \text{ m}$, the cloud dissipates
 499 before sunrise and Eq. (96) predicts that $z_i(0) = 500 \text{ m}$ and $\beta > 0.16$ dissipates during the day.
 500 The results validate the analytically derived conditions.

501 2) DISSIPATION BEFORE SUNRISE

502 The expression for dissipation at t_{sunrise} will be derived to determine the critical initial cloud
 503 thickness, h_{crit} . In order for the cloud to dissipate, the initial cloud thickness must be less than
 504 h_{crit} . Before sunrise, $u_4 = 0$ and a_1 is negligible compared to b_1 such that:

$$h(t) = z_i(0)e^{Dt} - z_b(0) - \frac{b_1(e^{Dt} - 1)}{z_i(0)De^{Dt}} = h(0)e^{Dt} - (1 - e^{Dt}) \left(z_b(0) - \frac{b_1}{e^{Dt}Dz_i(0)} \right) \quad (93)$$

505 Since cloud thickness either monotonically increases or decreases during the night, the critical
 506 cloud thickness would dissipate exactly at sunrise. We manipulate Eq. (93) to obtain the maximum
 507 allowable initial cloud thickness for the dissipation condition to be satisfied:

$$h_{\text{crit}} \leq (1 - e^{Dt_{\text{sunrise}}}) \left(z_i(0) - \frac{b_1}{e^{Dt} D z_i(0)} \right) \simeq -t_{\text{sunrise}} \left(z_i(0) D - \frac{b_1}{e^{Dt} z_i(0)} \right) \quad (94)$$

508 We infer the following points from this condition: 1) Deeper boundary layers can dissipate thicker
 509 clouds. This comes from the fact that the contribution of the initial inversion height ($z_i(0)$) de-
 510 creases in time through subsidence (Eq. (82)), whereas the initial cloud base height ($z_b(0)$) is not
 511 multiplied by a subsidence term in Eq. (90). For example, if surface, cloud base, and cloud top
 512 radiative temperatures were the same such that the net longwave radiation and related coefficients
 513 (a_1, b_1) are zero, the inversion height would still decrease in time due to subsidence, whereas cloud
 514 base height would stay constant as shown in Eq. (90). Thus, a larger inversion height subsides
 515 faster, resulting in more dissipation. The physical mechanism behind this is a faster subsidence
 516 rate due to a high inversion height. A faster subsidence rate results in a faster decrease in the cloud
 517 thickness; 2) Stronger subsidence dissipates thicker clouds. This is expected due to the faster
 518 decrease in the inversion height. The physical process is the same as the previous item. As the
 519 subsidence divergence increases, the subsidence rate of the cloud top also increases, resulting in a
 520 thinner cloud; 3) The cloud base analysis showed that b_1 is proportional to the cloud top tempera-
 521 ture. Thus, a higher cloud top temperature increases the maximum "dissipatable" cloud thickness
 522 before sunrise. However, a 1 K increase in T_{sky} only leads to approximately a 7.5 m increase in
 523 h_{crit} , thus T_{sky} has a smaller effect compared to the initial inversion height. The maximum dissi-
 524 patable cloud thickness before sunrise for various cloud top temperatures, subsidence values, and
 525 initial inversion heights is presented in Figure 11.

526 3) DISSIPATION AFTER SUNRISE

527 The second dissipation option materializes through a closing of the gap between inversion height
 528 and cloud base height during the day due to a faster increase in cloud base height. Previously,
 529 we observed that the dominant daytime term is u_4 . Dropping the u_1 terms, the cloud thickness
 530 expression can be written as:

$$h(t) = z_i(0)e^{Dt} + a_2u_4(t) - z_b(0) - \frac{(b_2 + a_2(\delta_1\Delta q_{T,i} + \delta_2\Delta\theta_{l,i}))u_4(t)}{z_i(0)e^{Dt} + a_2u_4(t)} \quad (95)$$

531 The maximum dissipatable or critical initial cloud thickness at sunset is obtained as:

$$h_{\text{crit}} \leq z_i(0)(1 - e^{Dt_{\text{sunset}}}) - a_2u_4(t_{\text{sunset}}) + \frac{(b_2 + a_2(\delta_1\Delta q_{T,i} + \delta_2\Delta\theta_{l,i}))u_4(t_{\text{sunset}})}{z_i(0)e^{Dt_{\text{sunset}}} + a_2u_4(t_{\text{sunset}})} \quad (96)$$

532 Using $\Delta q_{T,i} = -5 \text{ g kg}^{-1}$, $\Delta\theta_{l,i} = 10 \text{ K}$, $\Delta\theta_{v,i} = 10 \text{ K}$, the critical thickness is obtained as:

$$h_{\text{crit}} = 0.23z_i(0) + \frac{(13.96 \times 10^6 \text{ m}^2)(0.14 + 0.6e_2) \left(0.4 + 0.32e_1 - \frac{e_1}{\beta+1}\right)}{1.31z_i(0) + (10^3 \text{ m})(0.14 + 0.6e_2) \left(2.3e_1 - 0.52 - \frac{e_1}{\beta+1}\right)} - (586 \text{ m})(0.14 + 0.6e_2) \left(2.3e_1 - 0.52 - \frac{e_1}{\beta+1}\right) \quad (97)$$

533 For the thin cloud case, the critical thickness expression becomes:

$$h_{\text{crit}} = \frac{0.23 \left(z_i(0) + (500 \text{ m}) \left(1.74 + \frac{1}{\beta+1}\right)\right)^2 + (5.61 \times 10^6 \text{ m}^2) \left(0.72 - \frac{1}{\beta+1}\right)}{z_i(0) + (430 \text{ m}) \left(1.72 - \frac{1}{\beta+1}\right)} \quad (98)$$

534 We infer the following points based on this condition: 1) The dominant term is the negative Bowen
 535 Ratio dependent term in the numerator of Eq. (98). h_{crit} increases with increasing Bowen Ratio.
 536 However, the dependence on Bowen Ratio weakens as $1/\beta$ consistent with Section 5a. When
 537 the Bowen Ratio increases the positive feedback on the inversion height is weaker compared to
 538 the positive feedback on the cloud base height and the combined effect is an increase in h_{crit} .
 539 Since the net radiation flux that is converted into turbulent fluxes is constant, the sensitivity to
 540 Bowen Ratio decreases for high Bowen Ratios. 2) The dominant term changes sign with Bowen

541 Ratio, making dissipation impossible for small Bowen Ratios and possible for larger Bowen Ra-
542 tios. Therefore there is a region of the parameter space without dissipation before sunset. The
543 Bowen Ratio threshold that causes dissipation before sunset, is inversely proportional to the initial
544 inversion height. 3) Larger initial inversion heights enhance dissipation (first quadratic term). As
545 explained in the previous section for dissipation before sunrise, the term that contains the initial
546 inversion height decreases exponentially with subsidence, whereas the term with the initial cloud
547 base height persists in time. 4) Larger potential temperature inversion jumps and smaller magni-
548 tudes of total moisture inversion jumps enable dissipation as they have been shown in Section 5a
549 to limit inversion height growth (Eq. (96)). 5) Stronger subsidence enables dissipation, resulting
550 directly from the decrease in inversion height. We plot the maximum cloud thickness that can
551 be dissipated during the day for various Bowen Ratios, subsidence values, and initial inversion
552 heights in Figure 12. Combining both night and day results, stronger subsidence, larger inversion
553 height and higher Bowen Ratio enable dissipation and result in higher h_{crit} values.

554 *d. Extrema Analysis*

555 One of the advantages of an analytic solution is the ability to analyze derivatives for extrema
556 determination. Extrema may be of interest, e.g. in solar forecasting where the thickest cloud con-
557 ditions determine the maximum required amount of back-up generation. We performed extrema
558 analysis on inversion height and cloud thickness to find out where their minima and maxima occur.
559 To find the extrema points, we take the first and second derivative of the inversion height Eq. (82):

$$\frac{dz_i(t)}{dt} = z_i(0)De^{Dt} + a_1e^{Dt} + a_2u_4'(t) \quad (99)$$

$$\frac{d^2z_i(t)}{dt^2} = z_i(0)D^2e^{Dt} + a_1De^{Dt} + a_2u_4''(t) = a_2(u_4''(t) - Du_4'(t)) \quad (100)$$

560 The extrema points are obtained by solving the equation:

$$\frac{dz_i(t)}{dt} = 0 \rightarrow \frac{z_i(0)D}{a_2} + \frac{a_1}{a_2} = -\frac{u_4'(t)}{e^{Dt}} \quad (101)$$

561 The terms of the equality are plotted in Figure 13. The extrema are close to sunrise and sun-
 562 set. A greater initial inversion height leads to extrema moving towards mid-day. Furthermore,
 563 since $a_1/a_2 \ll 1$, the effect of Bowen Ratio and longwave and shortwave radiation terms is small
 564 compared to the initial inversion height.

565 The second derivative determines whether these points are maxima or minima. We know that
 566 $a_2 > 0, D < 0$ and $u_4''(t) \gg Du_4'(t)$. So the sign is determined by the sign of the second derivative
 567 of u_4 . The sign is positive until mid-day as the cosine of the solar zenith angle is increasing
 568 and it is negative after mid-day. This means that the first extremum after sunrise is a minimum
 569 and the second extrema before sunset is a maximum. This is an expected result as during night
 570 time longwave cooling decreases the inversion height. A minimum occurs when after sunrise net
 571 shortwave radiation counteracts longwave cooling and eventually becomes dominant to increase
 572 z_i . Similarly in the afternoon, net shortwave radiation results in an increase in inversion height
 573 until longwave cooling dominates closer to sunset.

574 We continue with the cloud thickness expression. The cloud base height was (Eq. (90)):

$$z_b(t) = \frac{z_i(t)z_{adj} + b_1u_1(t) + b_2u_4(t) + z_i(0)(z_b(0) - z_{adj})e^{Dt}}{z_i(t)} \quad (102)$$

575 The cloud thickness is obtained by subtracting cloud base height in Eq. (102) from $z_i(t)$:

$$h(t) = \frac{z_i^2(t) - z_i(t)z_{adj} - b_1u_1(t) - b_2u_4(t) - z_i(0)(z_b(0) - z_{adj})e^{Dt}}{z_i(t)} = \frac{z_i^2(t) + bz_i(t) + c(t)}{z_i(t)} \quad (103)$$

576 The derivatives are:

$$\frac{dh(t)}{dt} = \left(1 - \frac{c(t)}{z_i^2(t)}\right) \frac{dz_i(t)}{dt} + \frac{dc(t)}{dt} \frac{1}{z_i(t)} = 0 \quad (104)$$

$$\frac{d^2h(t)}{dt^2} = \frac{2c(t)}{z_i(t)^3} \left(\frac{dz_i(t)}{dt}\right)^2 + \left(1 - \frac{c(t)}{z_i(t)^2}\right) \frac{d^2z_i(t)}{dt^2} + \frac{d^2c(t)}{dt^2} \frac{1}{z_i(t)} - 2\frac{dc(t)}{dt} \frac{1}{z_i^2(t)} \frac{dz_i(t)}{dt} \quad (105)$$

577 The cloud thickness derivative contains the inversion height derivative. We expand the inversion
 578 height expression from Eq. (82) for the first derivative as:

$$\begin{aligned} \frac{dz_i}{dt} z_i^2 = & (b_1 u'_1 + b_2 u'_2 + b_3 u'_3 + Dz_i(0)(z_b(0) - z_{adj})e^{Dt})(a_1 u_1 + a_2 u_2 + a_3 u_3 + z_i(0)e^{Dt}) \\ & - (b_1 u_1 + b_2 u_2 + b_3 u_3 + z_i(0)(z_b(0) - z_{adj})e^{Dt})(a_1 u'_1 + a_2 u'_2 + a_3 u'_3 + Dz_i(0)e^{Dt}) \end{aligned} \quad (106)$$

579 Using the fact that $u'_1 - Du_1 = 1$, $u'_2 - Du_2 = \mu_0$ and $u'_3 - Du_3 = \mu_0^2$, the expression becomes:

$$\frac{dz_i}{dt} = \frac{(a_1 b_2 - a_2 b_1)u_4(t) - z_i(0)e^{Dt} \left((b_1 + b_2 \mu_0(t)) + (a_1 + a_2 \mu_0(t))(z_{adj} - z_b(0)) \right)}{z_i^2} \Bigg|_{t=t_{\text{ext}}} \quad (107)$$

580 Eq. (107) states that the cloud thickness extrema points exist when the derivative of the inversion
 581 height is equal to the right hand side (RHS) of the expression. We utilize the sensitivity results
 582 presented previously in this section for all coefficients to assess the extrema of cloud thickness.
 583 During night time for $\mu_0 = u_4 = 0$ the RHS is positive. Therefore, no extremum is present before
 584 sunrise as the derivative of the inversion height was shown to be negative.

585 During daytime for large Bowen Ratios that lead to the dissipation of the cloud before sunset, the
 586 RHS has a small negative value close to zero due to the quadratic term in the denominator, $b_2 > 0$
 587 and $a_2 > 0$. This means that the extrema, if they exist, are close to the extrema of the inversion
 588 height - right after sunrise and right before sunset - since the inversion height extrema are when the
 589 inversion height derivative is zero. Inversion height is increasing during the day, except between
 590 sunrise and the inversion height minimum and between the inversion height maximum and sunset.
 591 The extremum for cloud thickness must occur during these two intervals when the inversion height
 592 decreases and the RHS is negative.

593 When smaller Bowen Ratios lead to persistence of the cloud, the RHS changes sign during
 594 the day from negative to positive. Since the initial sign of RHS is negative, the first extremum
 595 between sunrise and the minimum inversion height still exists, however the other extremum shifts

596 to the interval between the minimum inversion height and maximum inversion height, where the
597 inversion height derivative is positive and matches the sign of the RHS.

598 We check for cloud thickness minima and maxima conditions for the inversion height extrema
599 points. The sign of the following expression determines the extrema condition:

$$\left(1 - \frac{c(t)}{z_i(t)^2}\right) \frac{d^2 z_i(t)}{dt^2} + \frac{d^2 c(t)}{dt^2} \frac{1}{z_i(t)}$$

600 The sign depends on the initial inversion height. The sign is the opposite of the second derivative
601 of the inversion height for small initial inversion heights and the same for large initial inversion
602 heights. Therefore for shallow boundary layers, the morning cloud thickness extremum is a maxi-
603 mum and occurs between sunrise and the minimum inversion height and the afternoon extremum
604 is a minimum. For higher boundary layers, the morning cloud thickness extremum is a minimum
605 and the afternoon extremum is a maximum. However, since larger inversion heights were shown to
606 increase h_{crit} in Section 5c, the afternoon maximum may not be observed as the cloud may already
607 have dissipated before the extremum depending on the Bowen Ratio. Two examples are shown in
608 Figure 14, where $\beta = 0.2$ and the only difference is the initial inversion height. As expected, the
609 minimum and maximum switch intervals between the two examples.

610 Combining this extrema result with the inversion height extrema, we have three scenarios for
611 dissipation: 1) Cloud dissipation occurs before the minimum inversion height and then no cloud
612 thickness maximum occurs as e.g. for the high subsidence and $z_i(0) \geq 1000$ m cases in Figure 10.
613 2) For larger initial inversion height, dissipation occurs after sunrise. 3) For small initial inversion
614 height, dissipation occurs after sunrise and before sunset with a maximum after sunrise depending
615 on the Bowen Ratio. Since the extrema analysis can only give the extrema of the cloud thickness
616 and not the values at those points, it is possible that the cloud may dissipate before the minimum.

617 **6. Conclusions**

618 We have provided an analytic closed-form solution to the cloud thickness evolution of stratocu-
619 mulus clouds in a mixed layer model framework with a focus on application over coastal lands.
620 This solution enabled sensitivity studies for inversion height, cloud base height and cloud thick-
621 ness. While the parameter space was not explored exhaustively, for the typical base case chosen
622 here, the following parameters influenced cloud thickness: Bowen Ratio, subsidence, and initial
623 inversion height. Critical initial cloud thicknesses, that can be dissipated pre and post-sunrise
624 were derived. Furthermore, we provided extrema analyses for inversion height and cloud thick-
625 ness expressions to show when these variables reach their maximum and minimum values. Cloud
626 dissipation can occur pre-sunrise, but this situation is unlikely in practice as such adverse condi-
627 tions would likely have prevented cloud formation in the first place. If cloud does not dissipate
628 pre-sunrise, then a morning maximum and afternoon minimum in cloud thickness is observed.
629 For large initial inversion heights, this observation is reversed as a morning minimum for cloud
630 thickness. If this minimum is associated with a cloud thickness of zero then the cloud deck breaks
631 up during the day. If the minimum is associated with a cloud thickness greater than zero, then
632 clouds are guaranteed to be maintained throughout the day.

633 The work in this paper will be used as the fundamental building block for future research on
634 physical effect on cloud lifetime. In the present analysis that does not consider advection, clouds
635 are sustained only for unrealistically small Bowen Ratios. Even though our solution provided a
636 good match against LES results, the models and assumptions that were required to solve the equa-
637 tions, limit its application compared to the variable meteorological conditions in the real world.
638 Examples include soil moisture change, precipitation, wind profiles, advection, and decoupling.
639 Future work will include large scale advection effects to analyze more realistic scenarios over

640 coastal lands. We plan to create a multi-column structure, where the columns are coupled through
641 large scale advection. The addition of moisture and cooling from the ocean is expected to increase
642 the sustenance of the clouds over the coast, creating more realistic dissipation times. Furthermore,
643 our current model does not consider the decoupling process. Even though decoupling occurs less
644 frequently than the well-mixed conditions, multi-layer clouds can form in deep boundary layers
645 that can result in the vertical column deviating from well-mixed conditions. Decoupling can occur
646 under stronger winds and, stronger temperature and moisture gradients. We plan to extend our cur-
647 rent model to study multiple cloud layers in a single column to observe the effects of decoupling
648 on cloud dissipation.

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652 **APPENDIX A**

653 **Nomenclature**

654 α_{lw} Optical depth scale for longwave radiation

655 α_{srf} Surface turbulent efficiency

656 A_w Entrainment tuning parameter

657 B_{cld} Cloud blackbody radiation

658 β Bowen Ratio

659 B_{srf} Surface blackbody radiation

660 B_{sky} Cloud top blackbody radiation

661 c_p Specific heat constant

662 $\Delta q_{T, i}$ Total water vapor mixing ratio jump at the inversion

663 $\Delta \theta_{l, i}$ Liquid potential temperature jump at the inversion

664 $\Delta \theta_{v, i}$ Virtual potential temperature jump at the inversion

665 F_{lw} Net longwave radiation flux

666 F_{rad} Net radiation flux

667 F_{ls} Net shortwave radiation flux

668 g_{lw} Asymmetry factor for longwave radiation

669 g_{sw} Asymmetry factor for shortwave radiation

670 L_v Latent heat of evaporation

671 μ_0 Cosine of the solar zenith angle

672 ω_{lw} Single scattering albedo for longwave radiation

673 ω_{sw} Single scattering albedo for shortwave radiation

674 q_l Liquid water mixing ratio

675 q_T Total water vapor mixing ratio

676 $q_{T, \text{adv}}$ Horizontal advection of water vapor mixing ratio

677 $q_{T, \text{inv}}$ Total water vapor mixing ratio at the inversion

678 R_d Gas constant for dry air

679 R_e Effective droplet radius

680 ρ_{air} Density of air

681 ρ_W Density of water

682 Ri Richardson number

683 R_v Gas constant for moist air

684 τ_b Optical depth of the cloud

685 T_{base} Cloud base temperature

686 T_{cld} Effective cloud temperature

687 θ_l Liquid potential temperature

688 $\theta_{l, \text{adv}}$ Horizontal advection of liquid potential temperature

689 $\theta_{l, \text{inv}}$ Liquid potential temperature at the inversion

690 θ_v Virtual potential temperature

691 $\theta_{v, 0}$ Virtual potential temperature reference

692 T_{srf} Surface temperature

693 T_{sky} Effective cloud top cooling temperature

694 \mathbf{v}_H Horizontal wind speed

695 w_e Entrainment velocity

696 $\overline{w'q'_T}$ Mean turbulent flux for total water vapor mixing ratio

697 w_s Subsidence velocity

698 $\overline{w'\theta'_l}$ Mean turbulent flux for liquid potential temperature

699 $\overline{w'\theta'_v}$ Mean turbulent flux for virtual potential temperature

700 z_b Cloud base height

701 z_i Inversion height

702 D Subsidence divergence

703 g Gravitational acceleration

704 t Time

705 APPENDIX B

706 Error Calculations

707 a. Error Calculation Methods and Metrics

708 We use the root mean square error (RMSE) definition as:

$$\text{RMSE} \triangleq \sqrt{\frac{1}{N} \sum_{i=1}^N (x_{\text{model}}(i) - x_{\text{ref}}(i))^2} \quad (\text{B1})$$

709 $x_{\text{model}}(i)$ represents the i^{th} point generated by our model, whereas $x_{\text{ref}}(i)$ is the i^{th} point associ-
710 ated with a reference (usually the ground truth). The percentage error is defined by normalizing
711 the RMSE by the mean reference value:

$$\% \text{Error} = \frac{\text{RMSE}}{\frac{1}{N} \sum_{i=1}^N x_{\text{ref}}(i)} \quad (\text{B2})$$

712 This percentage error model is only used for positive valued variables.

713 Throughout this section, errors are assessed by comparing the results of our approximations
714 with their original forms. For longwave calculations, we use the parameters from Larson et al.
715 (2007) and for shortwave calculations we use the parameters from Duynkerke (1999). The errors
716 are calculated numerically over a range of parameter values and then averaged. For inversion
717 height, the interval of $z_i \in [500 \text{ m}, 1000 \text{ m}]$ with 50 m resolution is used, whereas for the cloud
718 thickness $h \in [50 \text{ m}, 400 \text{ m}]$ is used. Since optical thickness depends on Γ_l , we use the interval
719 $\Gamma_l \in [0.1 \times 10^{-6} \text{ m}^{-1}, 2 \times 10^{-6} \text{ m}^{-1}]$ with a resolution of 10^{-7} m^{-1} . Longwave radiation depends
720 on the surface, cloud, and cloud top effective radiative temperatures. The standard atmosphere
721 adiabatic lapse rate of -6.5 K m^{-1} allows calculating the cloud and cloud top temperatures from
722 the surface temperature. We use the interval $T_{\text{srf}} \in [285 \text{ K}, 295 \text{ K}]$ with 1 K resolution. For solar
723 zenith angle calculations, we use daytime with 100 s resolution.

724 *b. Longwave Error Calculations for the approximations in Eqs. (46) and (47)*

725 We set $\omega_{\text{lw}} = 0.694$ and $g_{\text{lw}} = 0.83$ for all longwave calculations. We performed more than 35
726 million experiments, where we calculated the percentage error of our approximation in Eq. (49)
727 and (48) with respect to the original formulation in Eq. (47) and (46). The maximum RMSE
728 observed is 0.53 and the maximum percentage error is 0.05%, while the mean percentage error
729 is 0.03%. The maximum error is observed for Eq. (47), $z_i = 500 \text{ m}$, $\Gamma_l = 2 \times 10^{-6} \text{ m}^{-1}$ and
730 $T_{\text{srf}} = 285 \text{ K}$.

731 *c. Shortwave Error Calculations for the approximations in Eqs. (53) and (52)*

732 We set $\omega_{\text{sw}} = 0.993$ and $g_{\text{sw}} = 0.83$ for all shortwave calculations. We calculate α_{sw} and
733 β_{sw} (Eq. 50) and compare against Eq. (29) and Eq. (24), respectively to obtain the error per-
734 formance. We performed more than 32 million experiments. The resulting mean percentage error

735 is 2%. The percentage error of our approximation at the inversion height in Eq. (52) is 6% and
736 the maximum RMSE observed is 43 W m^{-2} . The maximum error is observed for the $z_i = 500 \text{ m}$,
737 $\Gamma_l = 10^{-6} \text{ m}^{-1}$ and $z_b = 335 \text{ m}$ case. For the shortwave approximation at the surface in Eq. (53),
738 the percentage error is 7% and the maximum RMSE is 44 W m^{-2} . The maximum error is ob-
739 served for the $z_i = 500 \text{ m}$, $\Gamma_l = 10^{-6} \text{ m}^{-1}$ and $z_b = 325 \text{ m}$ case.

740 *d. Net Radiation Error Calculations for the approximations in Eq. (54)*

741 We use the same configurations as in the previous sections b, c. The mean percentage error of
742 the columnar integral linear approximation in Eq. (54) is 6% and the RMSE is 41 W m^{-2} .

743 *e. Constant Assumption Validations*

744 The first assumption states that the surface, cloud base and cloud top temperature variations
745 are small compared to the actual temperature. Assuming a 30 K sinusoidal variation during the
746 day from 265 K to 295 K and back to 265 K, the RMSE of assuming a fixed temperature is only
747 4.5 K corresponding to less than 2% error. The errors are amplified to 6% in the black body radi-
748 ation calculation due to the fourth-order temperature dependence. The second assumption states
749 that similar trends in temperature will decrease the effective error since the equations depend on
750 the difference of the black body radiations. To verify this claim we create a second tempera-
751 ture timeseries at a height of 1 km. Under the standard atmosphere assumption, the lapse rate is
752 -6.5 K km^{-1}] so the second temperature timeseries therefore varies sinusoidally from 256.5 K
753 to 286.5 K instead. The error of the difference of black body radiation drops to 5%. The third
754 assumption states that the net shortwave radiation is greater than the net longwave radiation in the
755 cloud layer during the day. Using the assumptions in the previous example, the average ratio of
756 net shortwave to net longwave during the day is 8.7.

757 The constant optical depth assumption with τ_b calculated once using the initial thickness and
758 then set constant is validated against a model run with a variable (real) optical depth that is solved
759 iteratively at every minute. Different optical depth variation were created through two scenarios
760 with different Bowen Ratios of 0.2 and 1. Furthermore, since the optical depth depends on Γ_l , we
761 analyzed two scenarios with $\Gamma_l = 10^{-7} \text{ m}^{-1}$ (Figure B1 - top) and $\Gamma_l = 5 \times 10^{-7} \text{ m}^{-1}$ (Figure B1
762 - bottom). The results in Figure B1 show that the iterative and constant solutions are close in all
763 Bowen Ratio cases. In the case of $\Gamma_l = 5 \times 10^{-7} \text{ m}^{-1}$, the distance between the solutions increase
764 relative to the $\Gamma_l = 10^{-7} \text{ m}^{-1}$ case. The main reason is that the LWP and the cloud optical depth are
765 5 times higher, resulting in the optical thickness scale (h_{sw}) that is 5 times smaller. The difference
766 is largest for $\beta = 0.2$, since the cloud does not dissipate within 24 hours and the error accumulates
767 over a longer time.

768 APPENDIX C

769 Derivation of u_1, u_2, u_3 functions

770 We start the solution from $u_1(t)$:

$$u_1(t) = e^{Dt} \int_{t'=0}^t e^{-Dt'} dt' \quad (C1)$$

$$= \frac{e^{Dt} - 1}{D} \quad (C2)$$

771 We continue with $u_2(t)$. This function involves the solar zenith angle and can be written in a
772 general form as: $\mu_0(t) = \max \left\{ \mu_1 + \mu_2 \cos \left(\frac{t\pi}{H} - \pi \right), 0 \right\}$. The solution is as follows:

$$u_2(t) = e^{Dt} \int_{t'=0}^t e^{-Dt'} \max \left\{ \mu_1 + \mu_2 \cos \left(\frac{t'\pi}{H} - \pi \right), 0 \right\} dt' \quad (C3)$$

773 Note that the expression in the maximum is a periodic expression. The non-zero region within
774 a day spans from t_1 , sunrise, to t_2 , sunset. If t is greater than 1 day, then the solar zenith angle

775 expression will be repeated. The general solution for a time t on following days is:

$$\begin{aligned}
u_2(t) &= e^{Dt} \left(\int_{t_1}^{t_2} e^{-Dt'} \mu_0(t') dt' + \dots + \int_{t_1+2(n-1)H}^{t_2+2(n-1)H} e^{-Dt'} \mu_0(t') dt' + \int_{t_1+2nH}^t e^{-Dt'} \mu_0(t') dt' \right) \\
&= e^{Dt} \sum_{j=0}^{n-1} e^{-2DHj} \int_{t_1}^{t_2} e^{-Dt'} \mu_0(t') dt' + e^{Dt-2DHn} \int_{t_1}^{t-2nH} e^{-Dt'} \mu_0(t') dt' \quad (C4)
\end{aligned}$$

$$= e^{Dt} \left(\frac{1 - e^{-2DHn}}{1 - e^{-2DH}} \right) \int_{t_1}^{t_2} e^{-Dt'} \mu_0(t') dt' + e^{Dt-2DHn} \int_{t_1}^{t-2nH} e^{-Dt'} \mu_0(t') dt' \quad (C5)$$

776 We start with the solution of the integral with a general bound:

$$\int_{t_1}^x e^{Dx-Dt'} \mu_0(t') dt' = \mu_1 e^{Dx} \int_{t_1}^x e^{-Dt'} dt' + \mu_2 e^{Dx} \int_{t_1}^x e^{-Dt'} \cos(t' \pi/H - \pi) dt' \quad (C6)$$

$$= \frac{\mu_1}{D} (e^{Dx-Dt_1} - 1) + \mu_2 e^{Dx} \int_{t'=t_1}^x \frac{e^{it'\pi/H - i\pi - Dt'} + e^{-it'\pi/H + i\pi - Dt'}}{2} dt' \quad (C7)$$

$$\begin{aligned}
&= \frac{\mu_1}{D} (e^{Dx-Dt_1} - 1) \\
&+ \mu_2 e^{Dx} \frac{e^{ix\pi/H - i\pi - Dx} - e^{it_1\pi/H - i\pi - Dt_1}}{2i\pi/H - 2D} \\
&+ \mu_2 e^{Dx} \frac{e^{-ix\pi/H + i\pi - Dx} - e^{-it_1\pi/H + i\pi - Dt_1}}{-2i\pi/H - 2D} \quad (C8)
\end{aligned}$$

$$\begin{aligned}
&= \mu_2 \frac{\pi H^{-1} \sin(x\pi/H - \pi) - D \cos(x\pi/H - \pi)}{D^2 + \pi^2 H^{-2}} \\
&+ e^{Dx-Dt_1} \frac{\pi H^{-1} \left(\sqrt{\mu_2^2 - \mu_1^2} \right) - \mu_1 D}{D^2 + \pi^2 H^{-2}} \\
&+ \mu_1 D^{-1} e^{Dx-Dt_1} - \mu_1 D^{-1} \quad (C9)
\end{aligned}$$

$$\begin{aligned}
&= \mu_2 \frac{\pi H^{-1} \sin(x\pi/H - \pi) - D \cos(x\pi/H - \pi)}{D^2 + \pi^2 H^{-2}} \\
&+ e^{Dx-Dt_1} \frac{\pi H^{-1} \left(\sqrt{\mu_2^2 - \mu_1^2} \right) + \mu_1 D^{-1} \pi^2 H^{-2}}{D^2 + \pi^2 H^{-2}} - \mu_1 D^{-1} \quad (C10)
\end{aligned}$$

777 Using this result, we construct u_2 :

$$\begin{aligned}
u_2(t) = & e^{Dt-Dt_2} \left(\frac{1-e^{-2DHn}}{1-e^{-2DH}} \right) \frac{\pi H^{-1} \left(\sqrt{\mu_2^2 - \mu_1^2} \right) - \mu_1 D^{-1} \pi^2 H^{-2}}{D^2 + \pi^2 H^{-2}} \\
& + e^{Dt-Dt_1} \left(\frac{1-e^{-2DHn}}{1-e^{-2DH}} \right) \frac{\pi H^{-1} \left(\sqrt{\mu_2^2 - \mu_1^2} \right) + \mu_1 D^{-1} \pi^2 H^{-2}}{D^2 + \pi^2 H^{-2}} \\
& + \mu_2 \frac{\pi H^{-1} \sin(t\pi/H - \pi) - D \cos(t\pi/H - \pi)}{D^2 + \pi^2 H^{-2}} \\
& + e^{Dt-2DHn-Dt_1} \frac{\pi H^{-1} \left(\sqrt{\mu_2^2 - \mu_1^2} \right) + \mu_1 D^{-1} \pi^2 H^{-2}}{D^2 + \pi^2 H^{-2}} - \mu_1 D^{-1} \quad (C11)
\end{aligned}$$

778 The resulting equation has three components: a constant, an oscillatory component with a pe-
779 riodicity of 24 hours and an exponentially decreasing component, which has subsidence as its
780 exponent. As in the previous component, this means that the exponential term will vanish after
781 roughly 10 days.

782 We continue with $u_3(t)$. We now deal with the square of the solar zenith angle. Taking the
783 square of the expression, we obtain a very similar expression as before:

$$\begin{aligned}
\mu_0^2 = & \mu_1^2 + 2\mu_1\mu_2 \cos(t\pi/H - \pi) + \mu_2^2 \cos^2(t\pi/H - \pi) \\
= & (\mu_1^2 + \mu_2^2/2) + (2\mu_1\mu_2 \cos(t\pi/H - \pi)) + (\mu_2^2/2) \cos(2t\pi/H) \quad (C12)
\end{aligned}$$

We again start with the solution of the integral with a general bound for μ_0^2 :

$$\begin{aligned}
&= (\mu_1^2 + \mu_2^2/2) e^{Dx} \int_{t_1}^x e^{-Dt'} dt' + 2\mu_1\mu_2 e^{Dx} \int_{t_1}^x e^{-Dt'} \cos(t' \pi/H - \pi) dt' \\
&+ (\mu_2^2/2) e^{Dx} \int_{t_1}^x e^{-Dt'} \cos(2t' \pi/H) dt' \tag{C13}
\end{aligned}$$

$$\begin{aligned}
&= \frac{(\mu_1^2 - \mu_2^2/2)}{D} (e^{Dx-Dt_1} - 1) + 2\mu_1\mu_2 e^{Dx} \int_{t'=t_1}^x \frac{e^{it' \pi/H - i\pi - Dt'} + e^{-it' \pi/H + i\pi - Dt'}}{2} dt' \\
&+ (\mu_2^2/2) e^{Dx} \int_{t'=t_1}^x \frac{e^{2it' \pi/H - Dt'} + e^{-2it' \pi/H - Dt'}}{2} dt' \tag{C14}
\end{aligned}$$

$$\begin{aligned}
&= \frac{(\mu_1^2 + \mu_2^2/2)}{D} (e^{Dx-Dt_1} - 1) \\
&+ 2\mu_1\mu_2 e^{Dx} \frac{e^{ix\pi/H - i\pi - Dx} - e^{it_1 \pi/H - i\pi - Dt_1}}{2i\pi/H - 2D} \\
&+ 2\mu_1\mu_2 e^{Dx} \frac{e^{-ix\pi/H + i\pi - Dx} - e^{-it_1 \pi/H + i\pi - Dt_1}}{-2i\pi/H - 2D} \\
&+ (\mu_2^2/2) e^{Dx} \frac{e^{2ix\pi/H - Dx} - e^{2it_1 \pi/H - Dt_1}}{4i\pi/H - 2D} \\
&+ (\mu_2^2/2) e^{Dx} \frac{e^{-2ix\pi/H - Dx} - e^{-2it_1 \pi/H - Dt_1}}{-4i\pi/H - 2D} \tag{C15}
\end{aligned}$$

$$\begin{aligned}
&= \frac{(\mu_1^2 - \mu_2^2/2)}{D} (e^{Dx-Dt_1} - 1) \\
&+ 2\mu_1\mu_2 \frac{\pi H^{-1} \sin(x\pi/H - \pi) - D \cos(x\pi/H - \pi)}{D^2 + \pi^2 H^{-2}} \\
&+ 2\mu_1 e^{Dx-Dt_1} \frac{\pi H^{-1} \sqrt{\mu_2^2 - \mu_1^2} - \mu_1 D}{D^2 + \pi^2 H^{-2}} \\
&+ \frac{\mu_2^2}{2} \frac{2\pi H^{-1} \sin(2x\pi/H) - D \cos(2x\pi/H)}{D^2 + 4\pi^2 H^{-2}} \\
&+ e^{Dx-Dt_1} \frac{D(\mu_1^2 - \mu_2^2/2) - 2\mu_1 \pi H^{-1} \sqrt{\mu_2^2 - \mu_1^2}}{D^2 + 4\pi^2 H^{-2}} \tag{C16}
\end{aligned}$$

786 Using the respective x values we obtain:

$$\begin{aligned}
 & 2\mu_1 \left(\frac{1 - e^{-2DHn}}{1 - e^{-2DH}} \right) \left(e^{Dt-Dt_2} \frac{\pi H^{-1} \sqrt{\mu_2^2 - \mu_1^2} - \mu_1 \pi^2 H^{-2}}{D^2 + \pi^2 H^{-2}} \right. \\
 & \quad \left. + e^{Dt-Dt_1} \frac{\pi H^{-1} \sqrt{\mu_2^2 - \mu_1^2} + \mu_1 \pi^2 H^{-2}}{D^2 + \pi^2 H^{-2}} \right) \\
 & - \left(\frac{1 - e^{-2DHn}}{1 - e^{-2DH}} \right) \left(e^{Dt-Dt_2} \frac{2\pi H^{-1} \mu_1 \sqrt{\mu_2^2 - \mu_1^2} + D(\mu_1^2 - \mu_2^2)}{D^2 + 4\pi^2 H^{-2}} \right. \\
 & \quad \left. - e^{Dt-Dt_1} \frac{D(\mu_1^2 - \mu_2^2) - 2\mu_1 \pi H^{-1} \sqrt{\mu_2^2 - \mu_1^2}}{D^2 + 4\pi^2 H^{-2}} \right) \\
 & \quad + \frac{(\mu_1^2 - \mu_2^2/2)}{D} (e^{Dt-2DnH-Dt_1} - 1) + \\
 & 2\mu_1 \mu_2 \frac{\pi H^{-1} \sin(t\pi/H - \pi) - D \cos(t\pi/H - \pi)}{D^2 + \pi^2 H^{-2}} \\
 & \quad + 2\mu_1 e^{Dt-2DnH-Dt_1} \frac{\pi H^{-1} \sqrt{\mu_2^2 - \mu_1^2} - \mu_1 D}{D^2 + \pi^2 H^{-2}} \\
 & \quad + \frac{\mu_2^2}{2} \frac{2\pi H^{-1} \sin(2t\pi/H) - D \cos(2t\pi/H)}{D^2 + 4\pi^2 H^{-2}} \\
 & \quad + e^{Dt-2DnH-Dt_1} \frac{D(\mu_1^2 - \mu_2^2/2) - 2\mu_1 \pi H^{-1} \sqrt{\mu_2^2 - \mu_1^2}}{D^2 + 4\pi^2 H^{-2}} \tag{C17}
 \end{aligned}$$

787 This is similar to the previous result and results in 3 different components: a constant, oscillatory
 788 and exponential component with subsidence as its exponent.

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TABLE 1. Projected critical cloud thickness values for the cases in Fig. 10.

	$\beta = 0.2, z_i(0) = 1500 \text{ m}, D_n$	$\beta = 0.6, z_i(0) = 1500 \text{ m}, D_n$	$\beta = 5, z_i(0) = 1500 \text{ m}, D_n$
Before sunrise	75 m	56 m	13 m
Before sunset	19 m	506 m	1401 m
Dissipation Time	none	9.7 hours	7.9 hours
	$\beta = 0.2, z_i(0) = 500 \text{ m}, D_n$	$\beta = 0.6, z_i(0) = 500 \text{ m}, D_n$	$\beta = 5, z_i(0) = 500 \text{ m}, D_n$
Before sunrise	0 m	0 m	0 m
Before sunset	0 m	500 m	500 m
Dissipation Time	none	9.2 hours	7.7 hours
	$\beta = 0.2, z_i(0) = 500 \text{ m}, 5D_n$	$\beta = 0.6, z_i(0) = 1000 \text{ m}, 5D_n$	$\beta = 5, z_i(0) = 1500 \text{ m}, 5D_n$
Before sunrise	26 m	190 m	330 m
Before sunset	211 m	1000 m	1500 m
Dissipation Time	16.7 hours	5.3 hours	2.8 hours

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916		Simulations with $T_{\text{sky}} = 265 \text{ K}$ (solid) and $T_{\text{sky}} = 280 \text{ K}$ (dashed) are shown. Simulations
917		for Bowen Ratios between 0.1 and 5 are shown as thin gray lines for the $T_{\text{sky}} = 280 \text{ K}$ case
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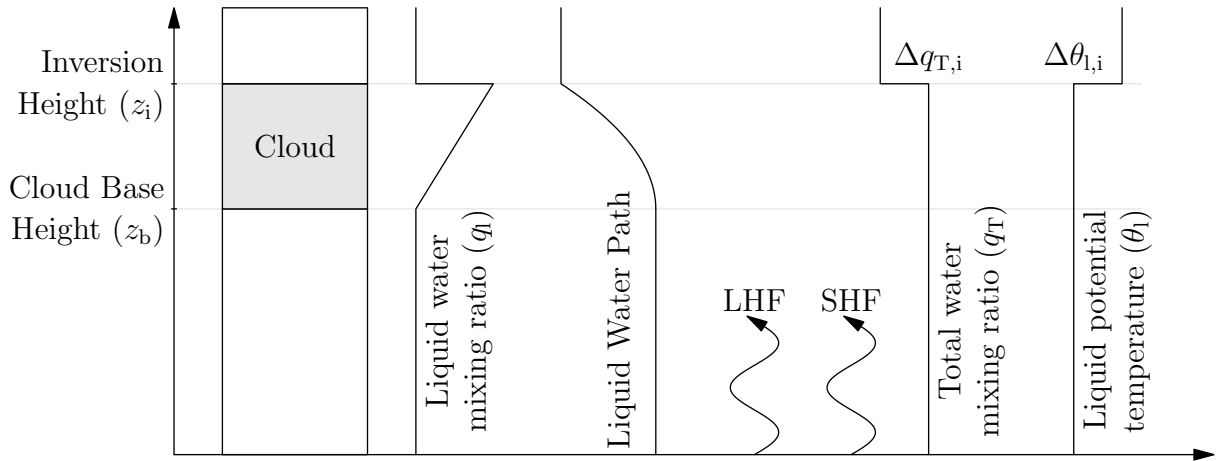
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946 10 K 68

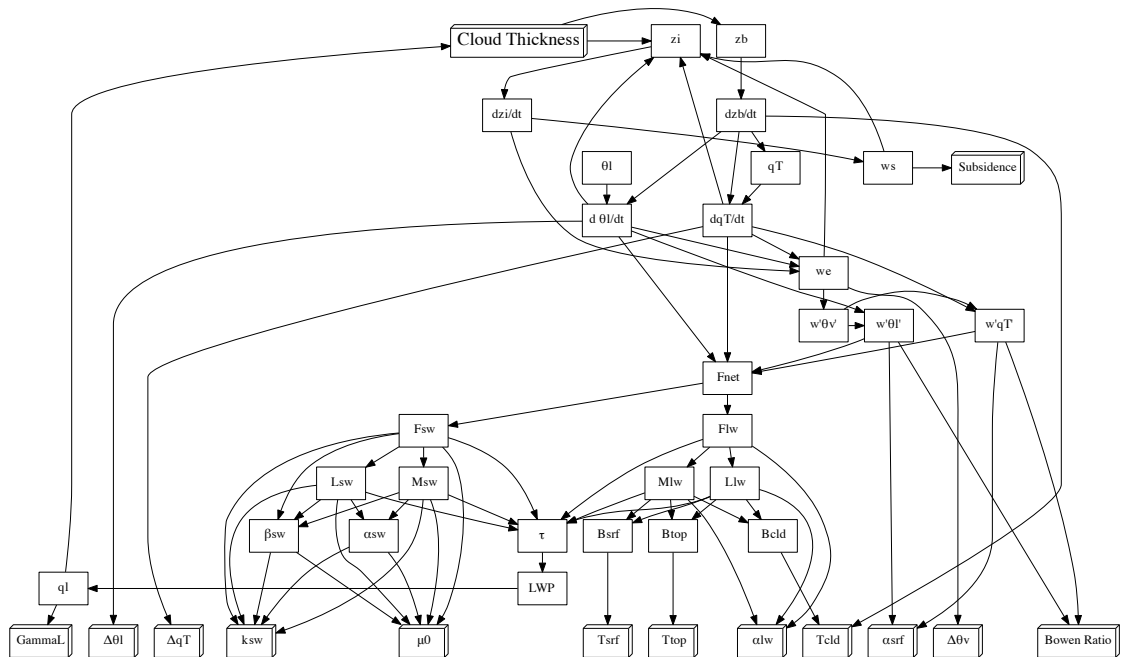
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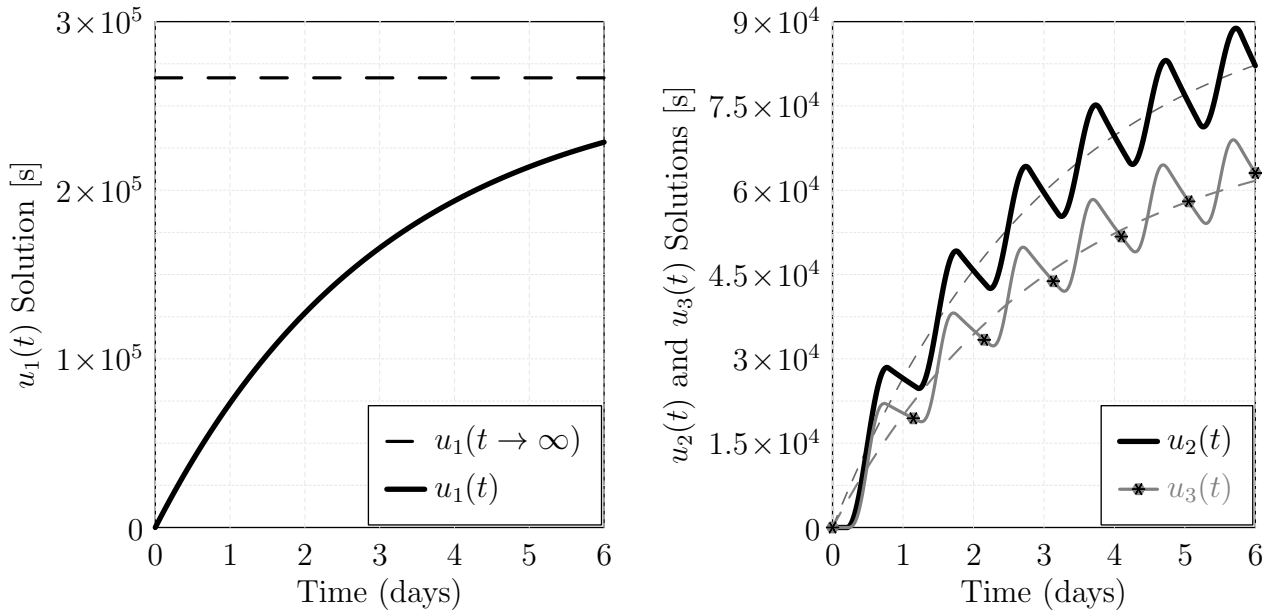
952 **Fig. B1.** The constant optical depth solution (solid) follows the iterative optical depth solution
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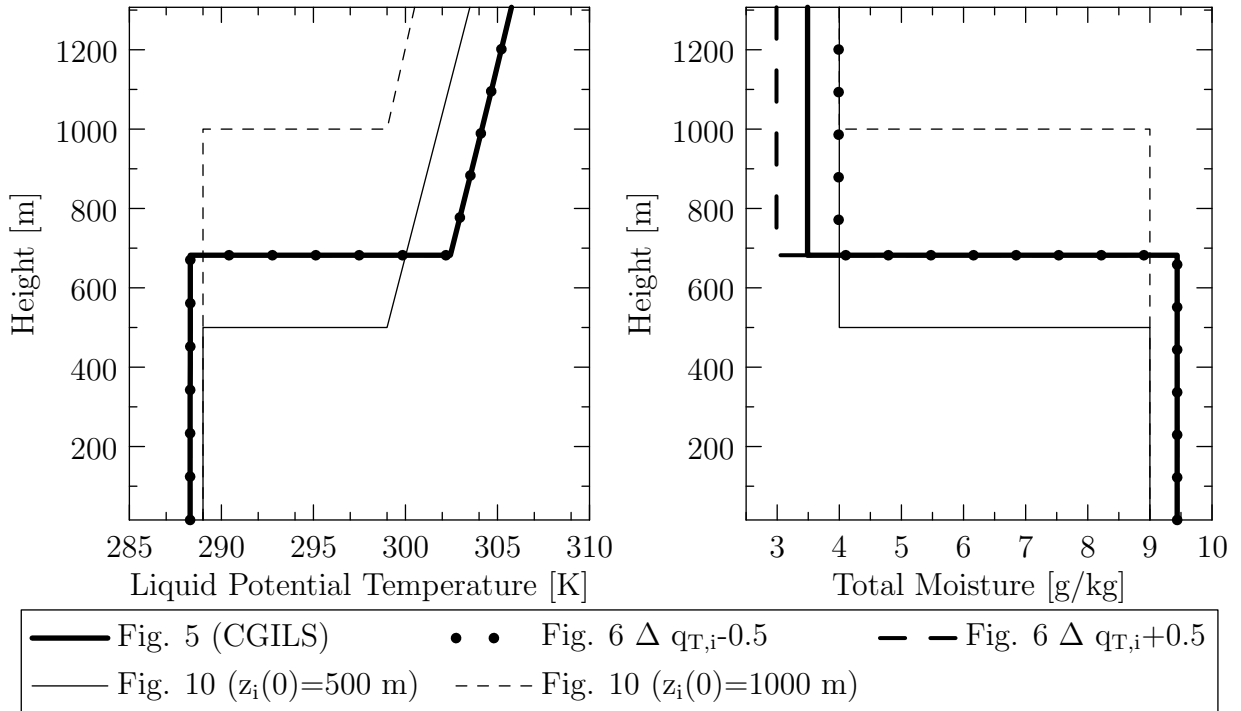
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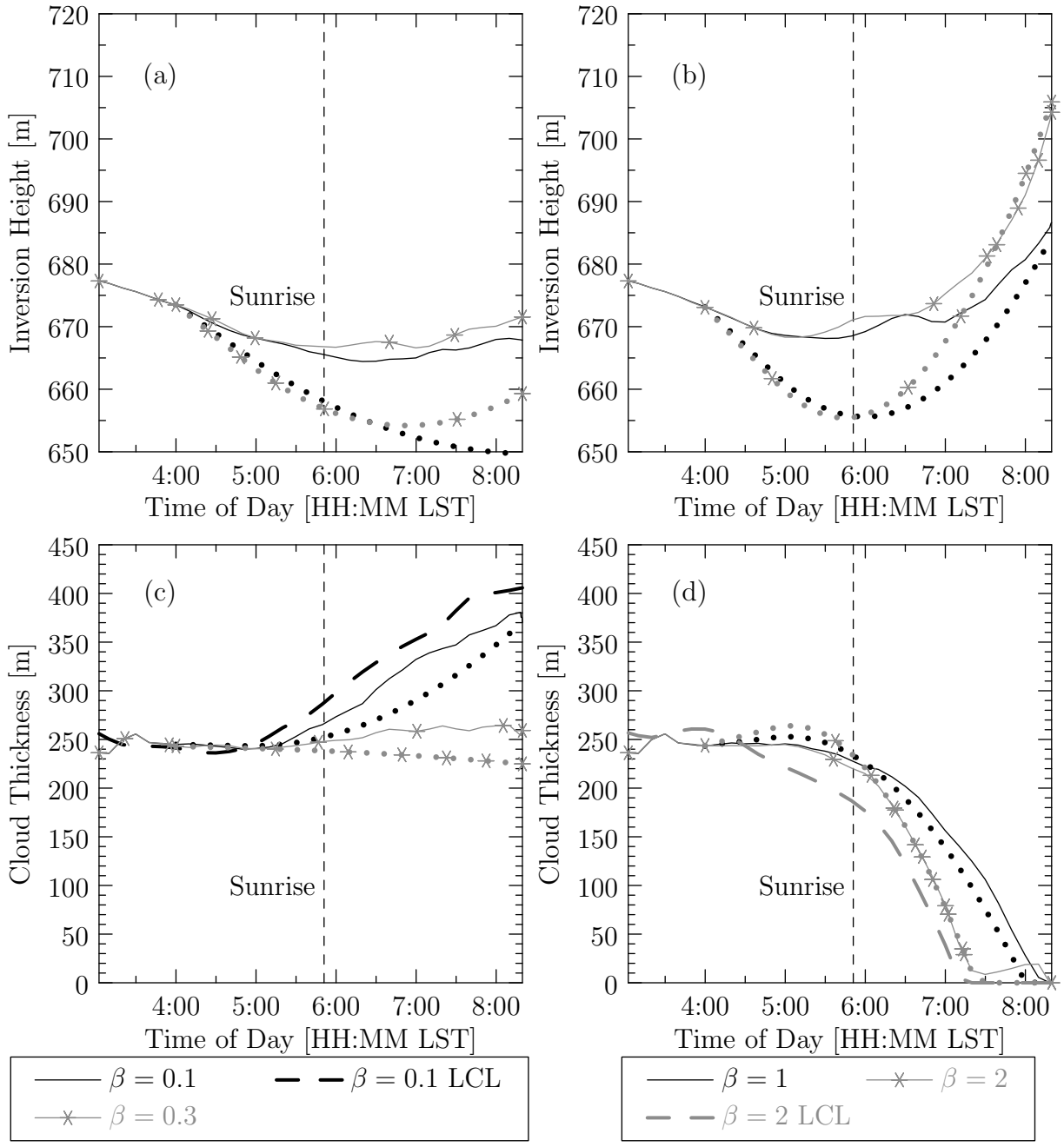
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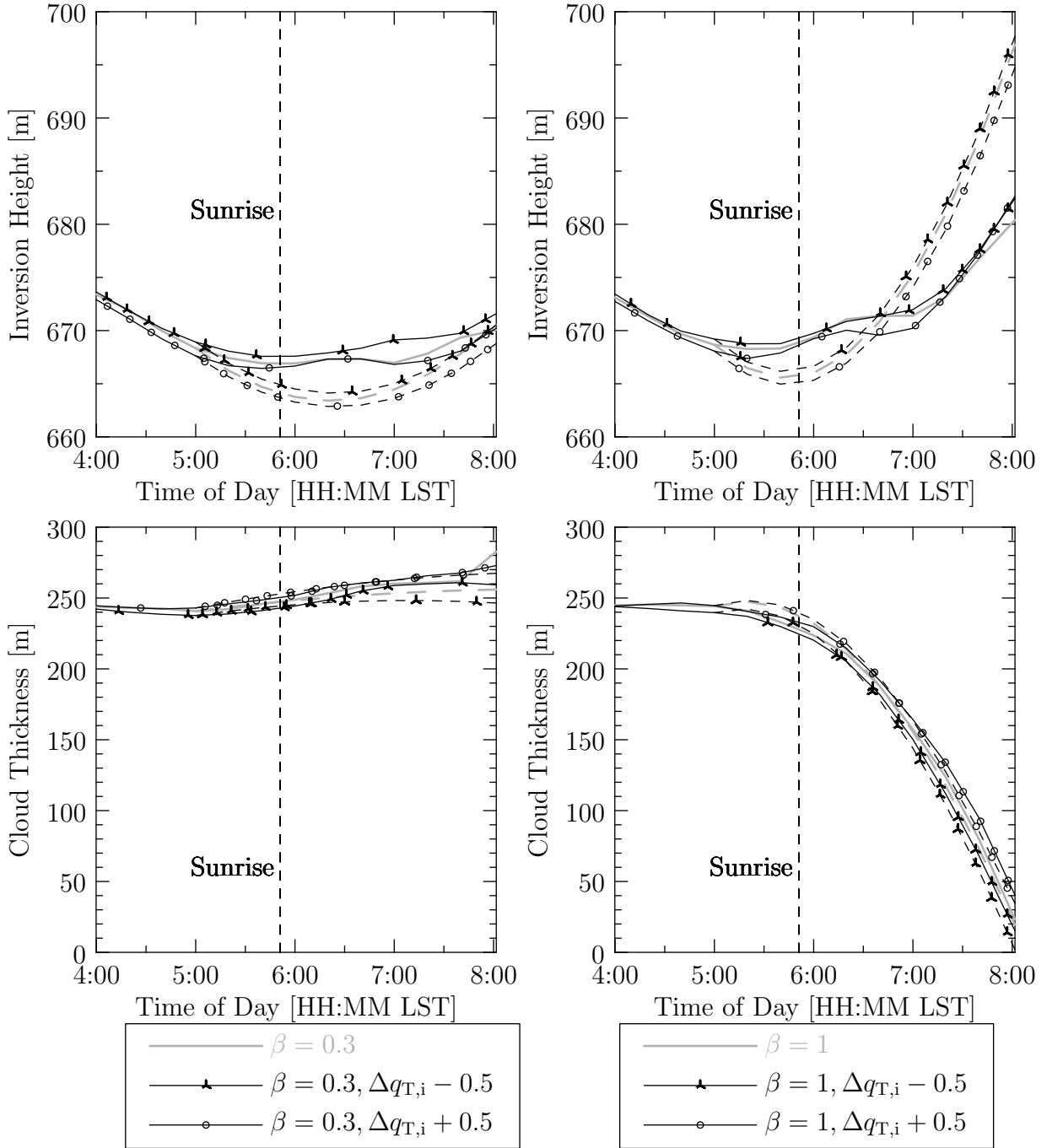
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 965 in Eq. (60). For subsidence, $D = -3.75 \times 10^{-6} \text{ s}^{-1}$ is used. Solar zenith angle is calculated for a latitude of
 966 32.85° N and the 196^{th} day of the year.



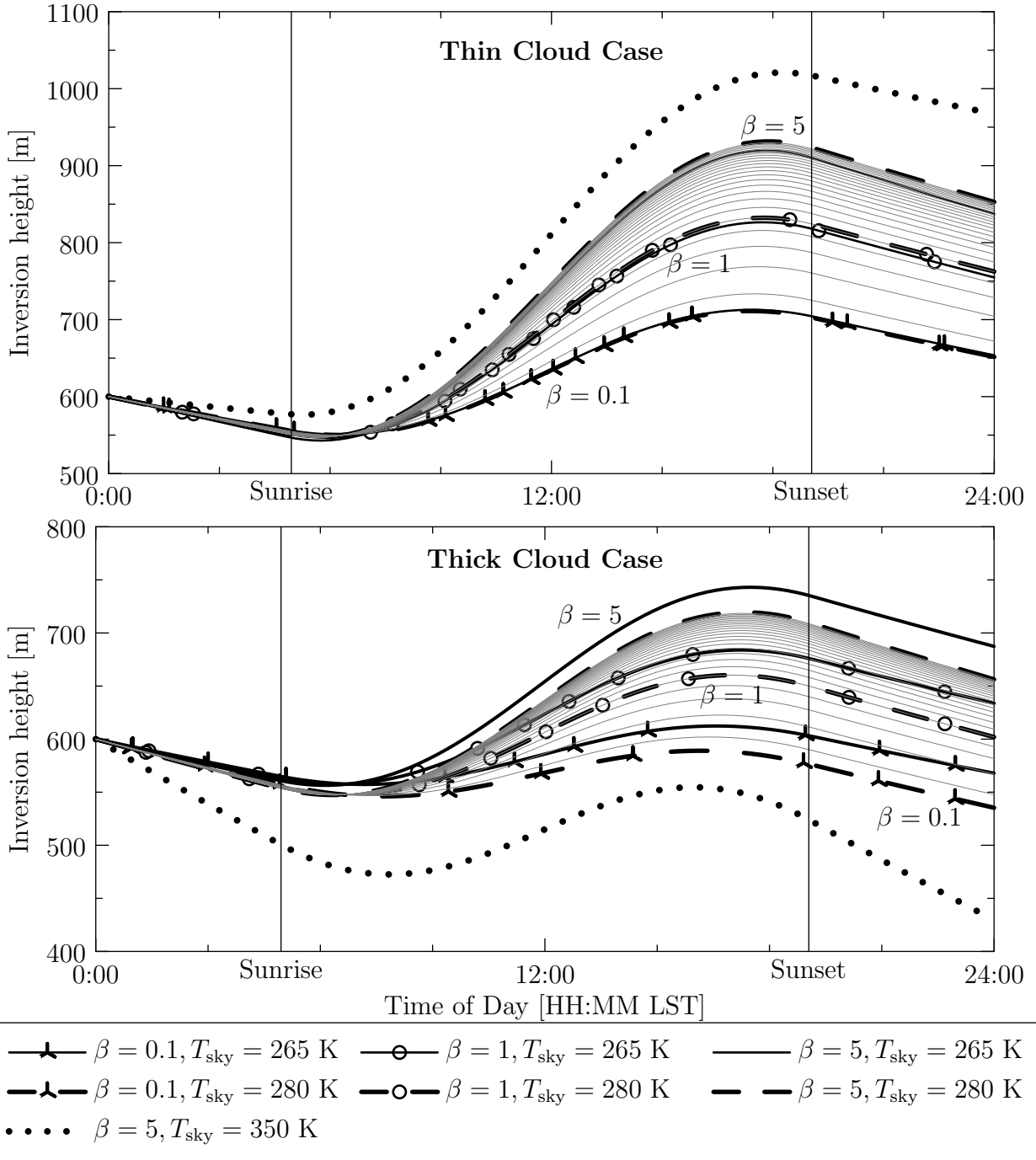
967 FIG. 4. Initial profiles of liquid potential temperature and total water mixing ratio used for LES are taken from
 968 CGILS s12 data (thick solid line). Throughout this work, the initial profiles have been slightly modified to study
 969 various conditions, such as total moisture jump sensitivity in Fig. 6 (dotted and thick dashed lines) and initial
 970 inversion height sensitivity in Fig. 10 (thin solid and dashed lines).



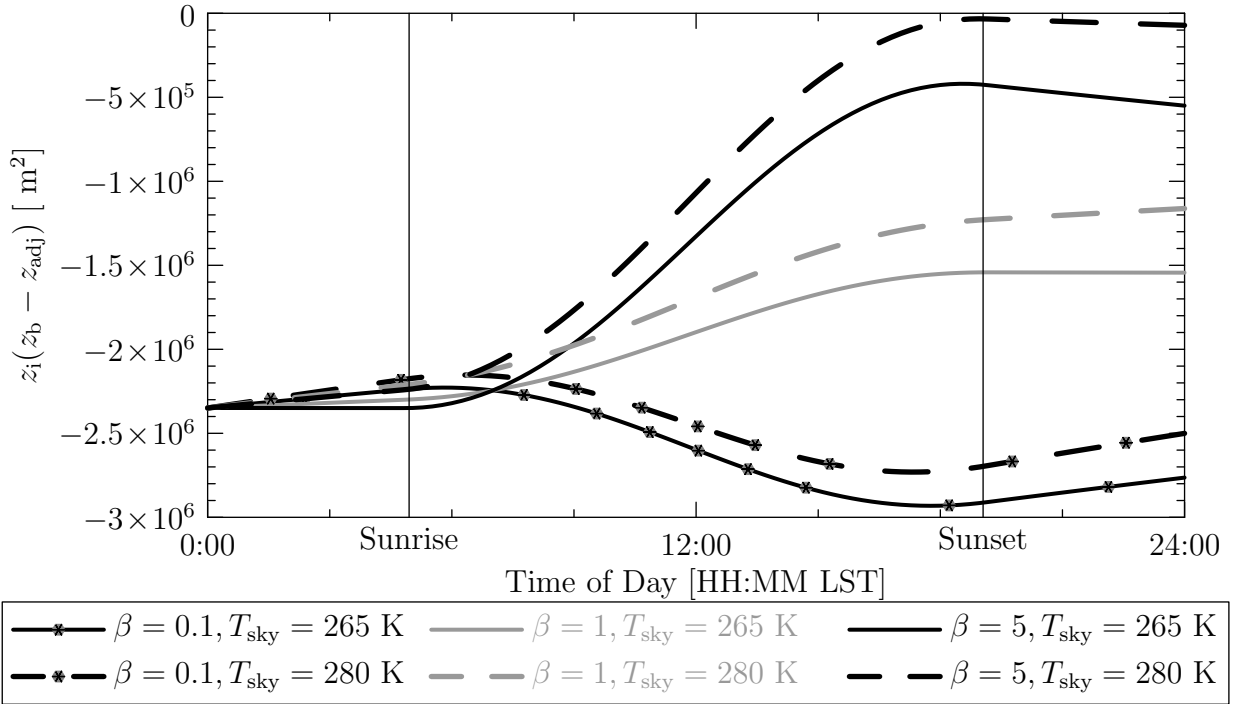
971 FIG. 5. Bowen Ratio sensitivity comparison between the analytic solution (dotted) and LES simulations (solid
 972 lines). Simulations are shown until the cloud dissipated for the largest Bowen Ratio, i.e. until 0800 LST, because
 973 the analytic model is not valid in clear conditions. Inversion height, z_i , is plotted for (a) $\beta = \{0.1, 0.3\}$ and (b)
 974 $\beta = \{1, 2\}$. Cloud thickness, h , is plotted for (c) $\beta = \{0.1, 0.3\}$ and (d) $\beta = \{1, 2\}$. Cloud thickness was also
 975 calculated using LCL for the $\beta = 0.1$ and $\beta = 2$ cases (dashed). The vertical dashed lines mark sunrise.



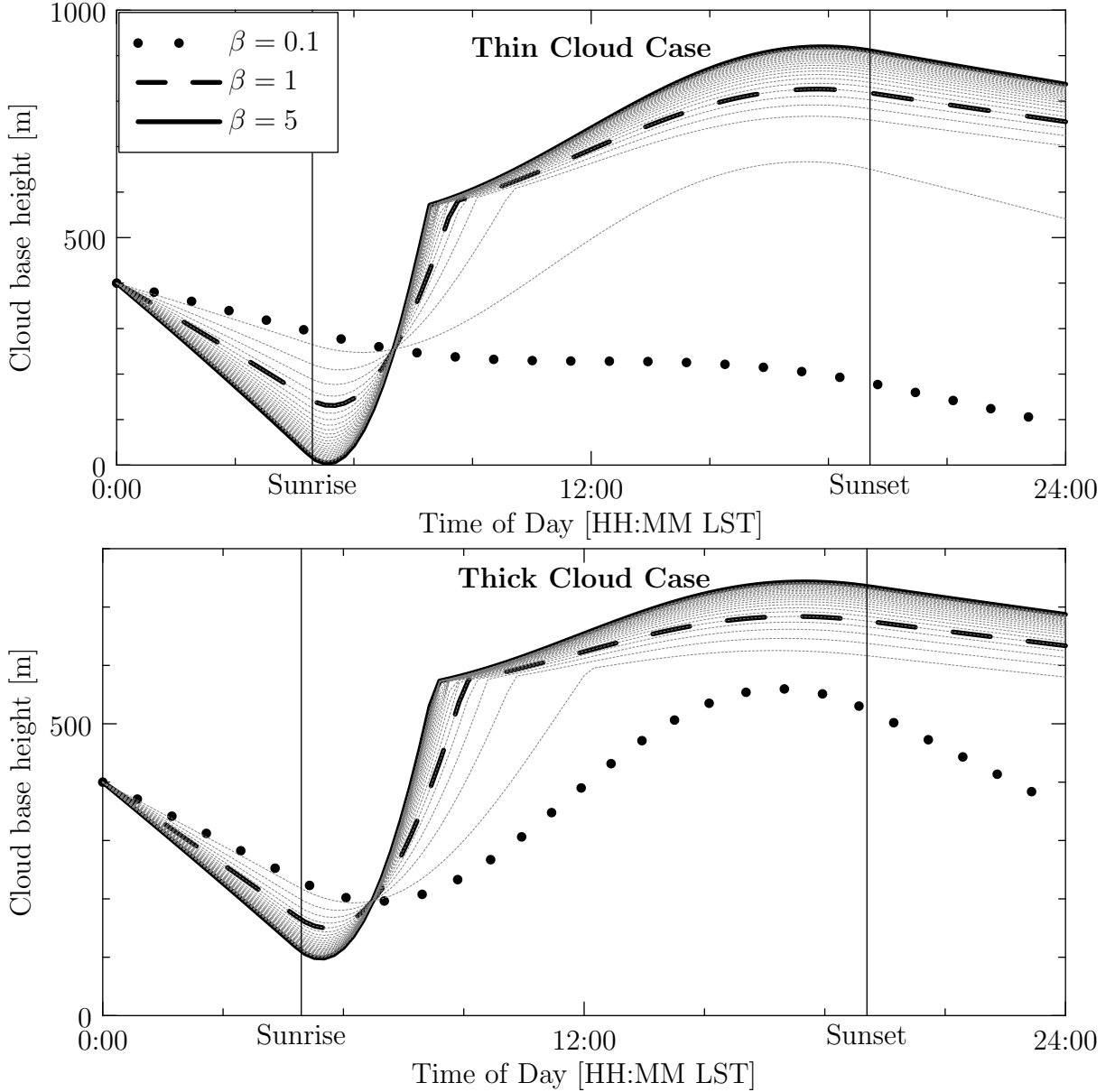
976 FIG. 6. Sensitivity of inversion height (top), and cloud thickness (bottom) to total moisture jump at the
 977 inversion and initial cloud base height, computed by the analytic solution (dashed) and the LES simulation
 978 (solid lines). Results for Bowen Ratios of 0.3 (left) and 1 (right) are shown. The original total moisture jump is
 979 colored gray, reduced case is marked with triangle and the increased case is marked with a circle.



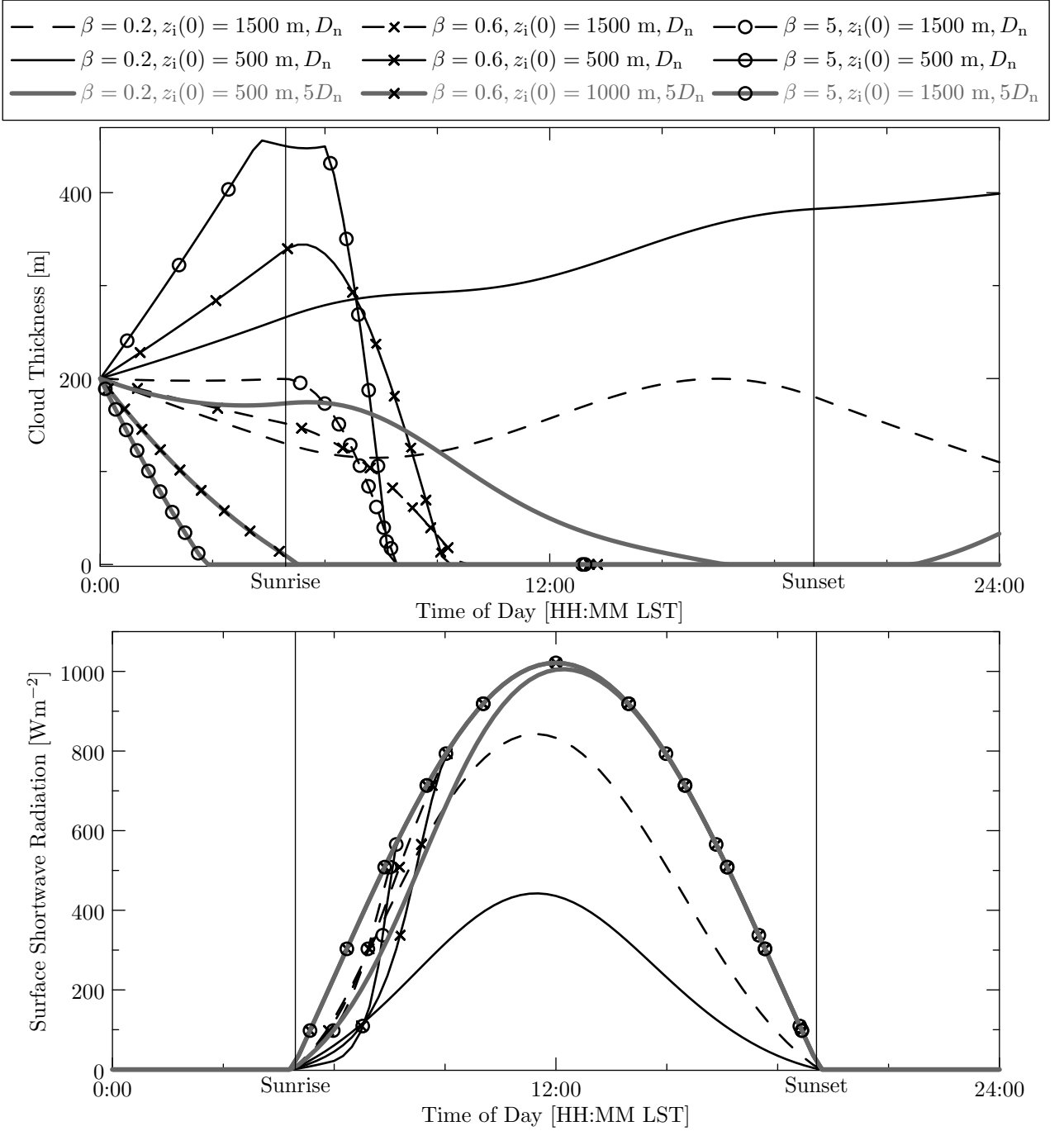
980 FIG. 7. Inversion height trend ($z_i(t)$) with respect to different Bowen Ratios and cloud top temperatures for
 981 the thin cloud case ($[0, 200]$ m, top) and the thick cloud case ($[200, 400]$ m, bottom). Other variables are fixed
 982 at $T_{\text{srf}} = 289 \text{ K}$, $T_{\text{cld}} = 285 \text{ K}$, $\zeta_D = 51 \text{ K}$, $D = -3.75 \times 10^{-6} \text{ s}^{-1}$. Simulations with $T_{\text{sky}} = 265 \text{ K}$ (solid) and
 983 $T_{\text{sky}} = 280 \text{ K}$ (dashed) are shown. Simulations for Bowen Ratios between 0.1 and 5 are shown as thin gray lines
 984 for the $T_{\text{sky}} = 280 \text{ K}$ case with 0.2 increments. The dotted line is an admittedly unrealistic parameter choice to
 985 show a case where $z_i(t)$ decreases. For this and all future graphs a latitude equal to 32.85° N and Julian day of
 986 196 were used for solar zenith angle calculations. 63



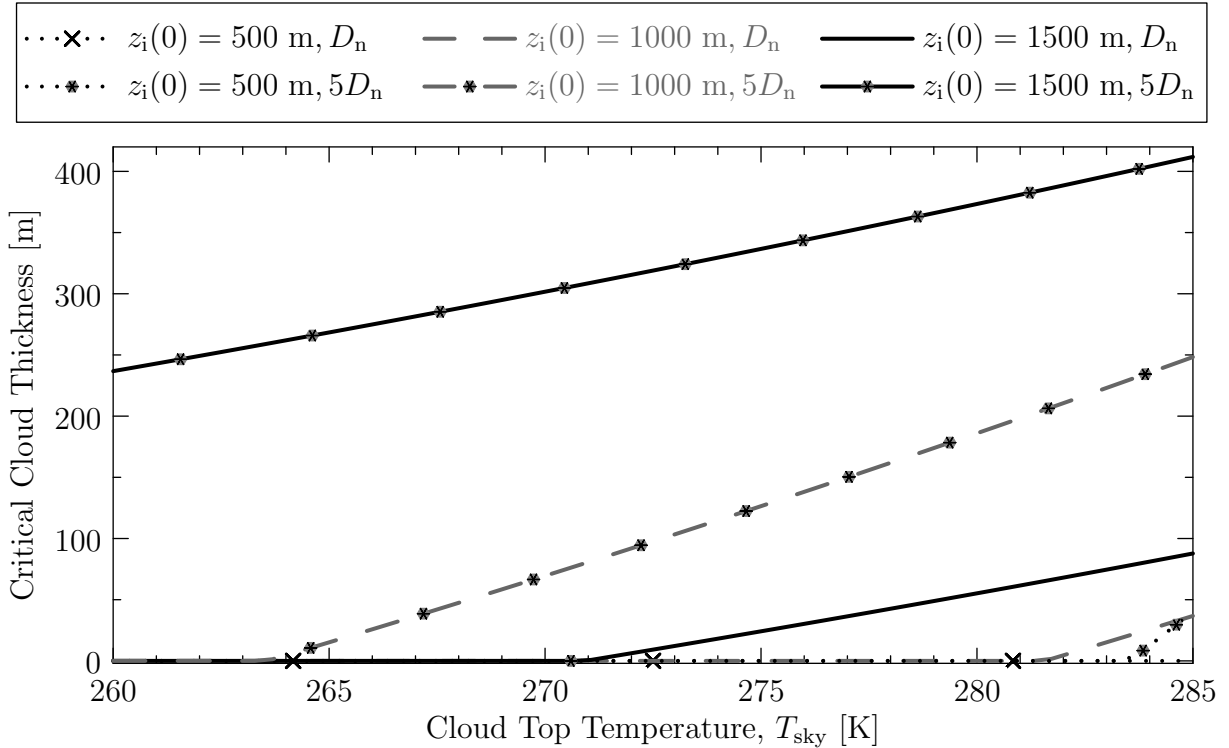
987 FIG. 8. $z_i(z_b - z_{\text{adj}})$ (proxy for cloud base height) timeseries for different Bowen Ratios and cloud top tem-
 988 peratures. Cases for $T_{\text{sky}} = 265 \text{ K}$ (solid) and $T_{\text{sky}} = 280 \text{ K}$ (dashed) are shown. Other variables are fixed at
 989 $T_{\text{srf}} = 289 \text{ K}, T_{\text{cld}} = 285 \text{ K}, \zeta_D = 51 \text{ K}, D = -3.75 \times 10^{-6} \text{ s}^{-1}$.



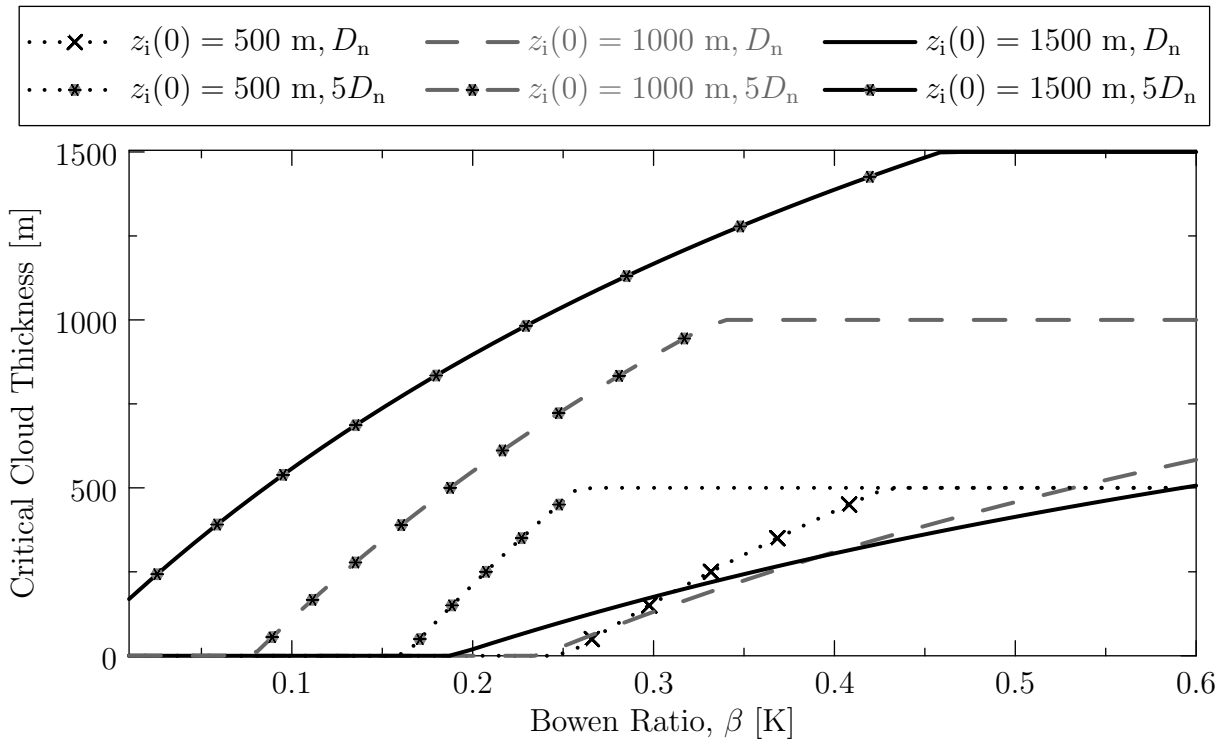
990 FIG. 9. Cloud Base Height timeseries ($z_b(t)$) for different Bowen Ratios for the thin cloud case ($[0, 200]$ m,
 991 top) and the thick cloud case ($[200, 400]$ m, bottom). The kink in the line occurs when the cloud base height
 992 reaches the inversion height. The thin gray lines represent Bowen Ratios from 0.1 to 5 with 0.2 increments. Other
 993 variables are fixed at $T_{\text{srf}} = 289$ K, $T_{\text{clid}} = 285$ K, $\zeta_D = 51$, $D = -3.75 \times 10^{-6} \text{ s}^{-1}$, $z_{\text{adj}} = 1600$ m, $z_i(0) = 600$ m,
 994 $T_{\text{sky}} = 265$ K.



995 FIG. 10. Cloud thickness evolution (top) and resulting surface shortwave radiative fluxes (bottom) for different
 996 Bowen Ratios, initial inversion heights, and subsidence values. High initial inversion height cases of $z_i =$
 997 1500 m are represented by dashed lines, $z_i = 500$ m cases are represented by solid lines and high subsidence
 998 cases are represented by thick lines. $D_n = -3.75 \times 10^{-6} \text{ s}^{-1}$, $T_{\text{srf}} = 289 \text{ K}$, $T_{\text{cld}} = 285 \text{ K}$, $T_{\text{sky}} = 270 \text{ K}$, $\zeta_D =$
 999 51 K, $\Delta q_{T,i} = -10 \text{ g kg}^{-1}$, $\Delta \theta_{l,i} = 10 \text{ K}$.



1000 FIG. 11. Maximum cloud thickness that can be dissipated by sunrise for different cloud top temperatures,
 1001 initial inversion heights and subsidence values. For normal subsidence values of D_n , only a very thin cloud
 1002 dissipates for the $z_i(0) = 1000$ m and $z_i(0) = 1500$ m cases. A zero result means that the cloud will not dissipate
 1003 before sunrise for the given conditions. $D_n = -3.75 \times 10^{-6} \text{ s}^{-1}$. Other variables are fixed at $\beta = 1$, $T_{\text{srf}} = 289$ K,
 1004 $T_{\text{cld}} = 285$ K, $\zeta_D = 51$ K.



1005 FIG. 12. Maximum cloud thickness that can be dissipated by sunset for different Bowen Ratios, initial inver-
 1006 sion heights and subsidence values. A zero result means that the cloud will not dissipate before sunset for the
 1007 given conditions. Horizontal lines result when the "dissipatable" cloud thickness reaches the initial inversion
 1008 height. Parameters are $D_n = -3.75 \times 10^{-6} \text{ s}^{-1}$, $T_{\text{srf}} = 289 \text{ K}$, $T_{\text{cld}} = 285 \text{ K}$, $T_{\text{sky}} = 270 \text{ K}$, $\zeta_D = 51 \text{ K}$, $\Delta q_{T,i} =$
 1009 -5 g kg^{-1} , $\Delta\theta_{l,i} = 10 \text{ K}$, $\Delta\theta_{v,i} = 10 \text{ K}$.

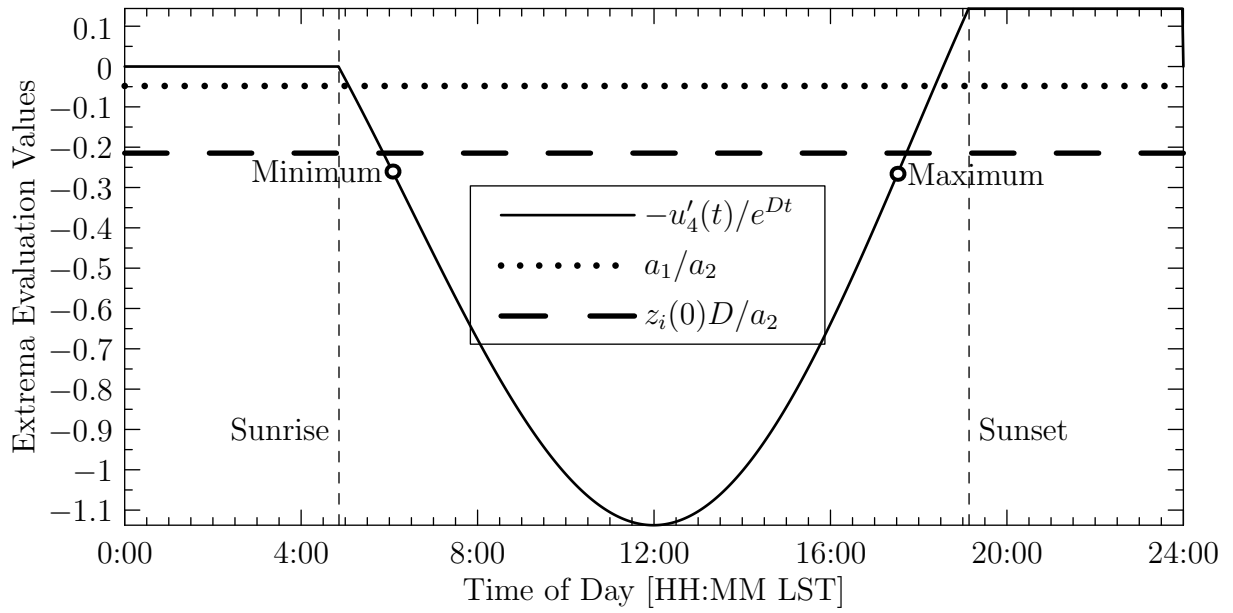
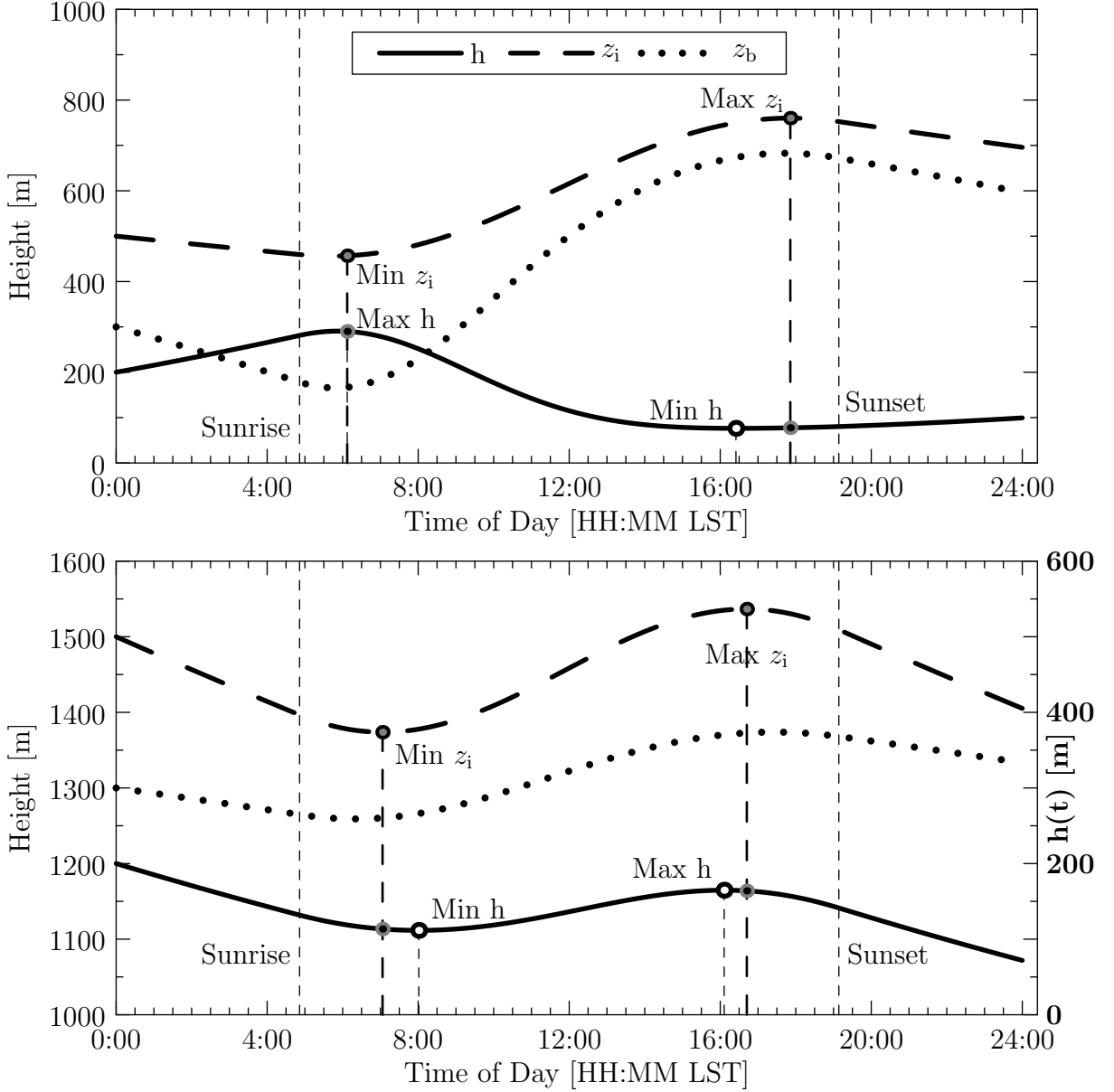
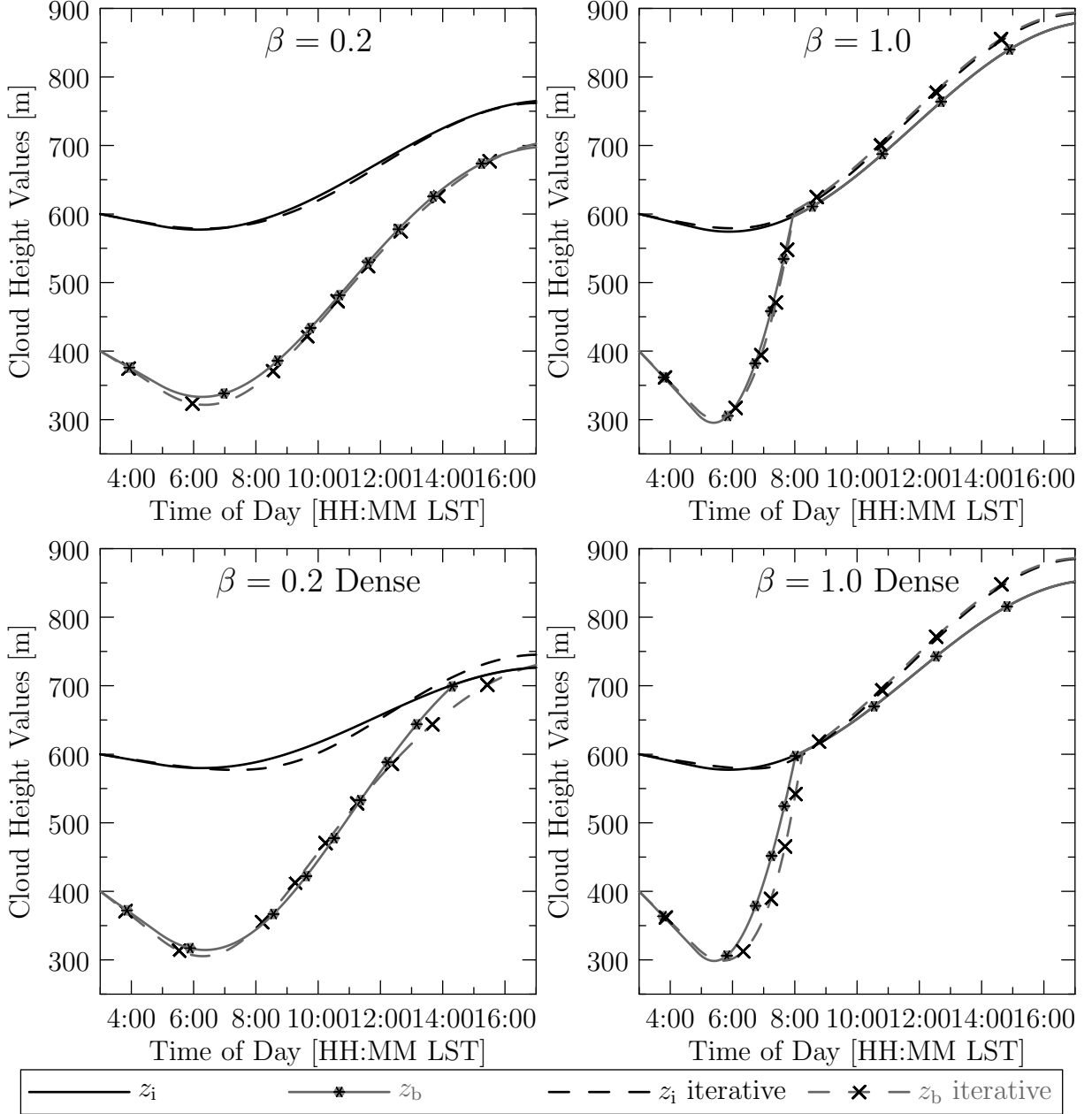


FIG. 13. Evaluation of the terms in Eq. (101) to find the inversion height extrema points.



1010 FIG. 14. Evaluation of the cloud thickness and its extrema values. Both cases have an initial cloud thickness of
 1011 200 m, but the top figure has $z_i(0) = 500$ m and the bottom figure has $z_i(0) = 1500$ m. The remaining parameters
 1012 are the same, i.e. $\beta = 0.2$, $T_{\text{srf}} = 289$ K, $T_{\text{cld}} = 285$ K, $T_{\text{sky}} = 270$ K, $\zeta_D = 51$ K.



1013 Fig. B1. The constant optical depth solution (solid) follows the iterative optical depth solution (dashed)
 1014 closely, showing that our constant optical depth assumption is valid. $\Gamma_l = 5 \times 10^{-7} \text{ m}^{-1}$ for the normal case,
 1015 and $\Gamma_l = 10^{-7} \text{ m}^{-1}$ for the dense case. Rest of the simulation parameters are $z_i(0) = 600 \text{ m}$, $z_b(0) = 400 \text{ m}$,
 1016 $T_{\text{srf}} = 289 \text{ K}$, $T_{\text{cld}} = 285 \text{ K}$, $T_{\text{sky}} = 265 \text{ K}$, $D = -3.75 \times 10^{-6} \text{ s}^{-1}$.