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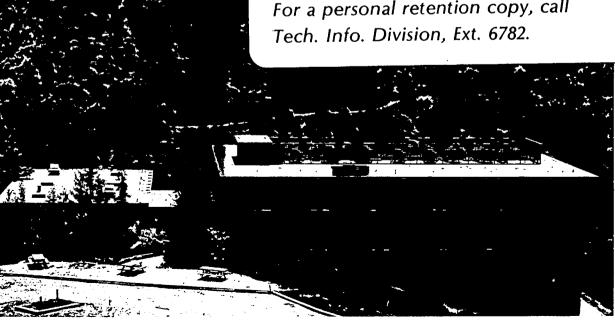
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## MASS TRANSFER LIMITING CURRENTS OF ZINC DEPOSITION IN ACIDIC ZnCl $_2$ and ZnSO $_4$ SOLUTIONS

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#### INTRODUCTION

The zinc chlorine battery system is under development for load-leveling and electric vehicle applications. This secondary battery consists of a zinc electrode and a Cl<sub>2</sub> electrode in an aqueous solution of ZnCl<sub>2</sub> and KCl. During the charging process, Zn is deposited on the cathode and Cl<sub>2</sub> evolves on a porous flow-through graphite anode. The Cl<sub>2</sub> containing electrolyte flows into another chamber where it is chilled and stored in the form of solid chlorine hydrate (Cl<sub>2</sub>·6H<sub>2</sub>O). During the discharge process zinc dissolves and the chlorine gas produced by heating the hydrate passes through the porous graphite electrode and forms chloride ions yielding aqueous ZnCl<sub>2</sub> [1]:

The cycle life, reliability, and coulombic efficiency of this battery depends on the quality of the zinc deposit. The macromorphology of the zinc deposit obtained from acidic  $\operatorname{ZnCl}_2$  solutions has been a subject of recent studies [1,5,8]. In this laboratory efforts have been concentrated on the evaluation of the effect of hydrodynamic flow on the macromorphology of zinc deposits. The influence of current density, pH, hydrodynamic conditions, deposition time, electrolyte composition, including impurities, have been examined. For the development of an understanding of the complex phenomena involved in zinc deposition, the mass transfer conditions near the electrode must be fully characterized.

The present work concerns the determination of limiting currents of zinc deposition from acidic  ${\rm ZnCl}_2$  and  ${\rm ZnSO}_4$  solutions. A rotating disk electrode has been used for this purpose.

For simple laminar flow at a rotating disk electrode, the dependence of mass transfer rate on relevant proven variables is expressed in the dimensionless equation:

$$Sh = 0.62 \text{ Re}^{1/2} \text{ Sc}^{1/3} \qquad [1]$$
 for 
$$Re < 2.7 \times 10^5$$
 where 
$$Sh = rk/D$$
 
$$Sc = v/D$$
 
$$Re = r^2 \Omega/v$$
 
$$k = i_L/nFC_b, \text{ mass transfer coefficient, cm/sec}$$

This equation is the dimensionless form of Levich's rotating disk limiting current equation [13]:

$$i_L = 0.62 \text{ n F D}^{2/3} \Omega^{1/2} \nu^{-1/6} C_b$$
 [2]  
 $\nu = \text{kinematic viscosity, cm}^2/\text{sec}$   
 $\Omega = \text{angular velocity, rad/sec}$   
 $r = \text{disk radius, cm}$ 

c<sub>b</sub> = bulk concentration of the reacting species, moles/cm<sup>3</sup>

#### EXPERIMENTAL

#### Experimental Setup

The solutions were prepared from Analytical Reagent (AR) grade  ${\rm ZnCl}_2$ ,  ${\rm ZnSO}_4$ , KCl, and  ${\rm Na}_2{\rm SO}_4$  manufactured by Mallinckrodt. The rotating disk electrodes were made of 99.99% zinc. The 1.0 cm diameter zinc disk was attached to a brass core using silver-epoxy adhesive. brass core was tapped on one end to screw onto the spindle shaft of the rotating disk assembly. Epoxy resin was cast around this brass core and zinc disk. The RDE was then machined to cylindrical shape, with a final outer diameter of 3.5 cm (Figures 1a and 1b). A one-compartment electrolyte cell with a 99.99% zinc circular anode located at the bottom of the cell was used in this investigation. This same cell (Figures 2a and 2b) was used in the previous investigations by Jaksic and Komnenic. reference electrode was a saturated calomel electrode. Ohmic resistance was minimized by locating the Luggin capillary as close as possible to the disk in the plane of the disk, 3-4 cm from its center. The zinc disk study was carried out under potentiostatic control; the circuit diagram is shown in Figure 3a. Potentiostat-galvanostat, Princeton Applied Research Co. (PAR) Model 371, with a PAR Model 178 Electrometer Probe and PAR Model 175 Universal Programmer were used in the potentiostatic experiments. The rotator was a Pines Instrument ASR-2 rotator. Cathodic polarization curves were recorded on a Hewlett-Packard Model 7001A X-Y recorder (Figure 3b).

#### Experimental Procedure

The pretreatment of the zinc disk electrode was as follows:

- a) polishing with waterproof SiC paper, (grit size 400, followed by 600)
- b) polish with 1 micron-size diamond paste
- c) washing with soap, rinsing with ethyl alcohol and acetone
- d) before the experiment, dipping for 1 second in conc HNO3, and then rinsing with distilled water

Cathodic polarization of the zinc RDE was carried out in five different solutions:

0.05 M ZnCl<sub>2</sub> + 1 M KCl

0.10 M ZnCl<sub>2</sub> + 1 M KCl

0.50 M ZnCl + 1 M KCl

 $0.05 \text{ M ZnSO}_{4} + 1 \text{ M Na}_{2}\text{SO}_{4}$ 

 $0.10 \text{ M } \text{ZnSO}_{4} + 1 \text{ M } \text{Na}_{2}\text{SO}_{4}$ 

The following six rotational speeds were used in this study: 200, 400, 800, 1200, 1600, 2000 revolutions per minute (rpm). The polarization curves were obtained by sweeping the potential range, -1.050 V to -2.550 V vs. SCE at scan rates of 10, 100, and 200 mV/s.

Half-cell reactions were:

$$Zn^{+2} + 2e^{-} = Zn$$
 Eo = -0.763 V (working cathode)

$$2Hg + 2 Cl^- = Hg_2Cl_2 + 2e^-$$
 Eo = +0.242 V (reference electrode)

The viscosity of the solutions was measured with a Cannon-Fenske viscosimeter [4].

#### RESULTS

Cathodic polarization curves were obtained with the zinc disk at different rotational speeds, different concentrations of ZnCl<sub>2</sub> and ZnSO<sub>4</sub> solutions and using 3 different potential sweep rates. Each cathodic polarization curve was obtained with a freshly polished electrode surface. Supporting electrolyte was used to minimize potential variations in the solution and to keep the concentration of zinc at a low level in order to prevent large limiting currents. Zinc is highly complexed in chloride solutions even at the 0.05 M zinc concentrations used in these experiments [9,14]. The measured limiting current in chloride solution is actually a net quantity resulting from zinc transport by convective diffusion to the electrode and from additive or subtractive migrational contributions of the zinc ionic species.

### Rotating Disk Studies in ZnCl<sub>2</sub> + KCl Solutions

Figure 4 shows the polarization curves at a scan rate of 10 mV/sec, in 0.05 M ZnCl<sub>2</sub> + 1 M KCl solution, pH = 2.48, T = 22°C. At all rotational speeds a well defined limiting current plateau was reached within the potential sweep. The steep rise in the current which appears at about -1.870 V vs. SCE is due to hydrogen evolution. Hydrogen bubbles could be observed near the electrode surface after this potential was reached. This potential is in good agreement with a result reported by Kim and Jorne in 0.05 M ZnCl<sub>2</sub> solution [5]. The zinc reaction is diffusion controlled; the current is proportional to the square root of the rotational speed in good agreement with Levich theory [2], as shown in Figure 5. This can be seen from the plot of the current vs. square root of the rotational speed under a fixed potential on the limiting current

plateau, E = -1.746 V vs. SCE. At higher rotational speeds (1600 and 2000 rpm) accurate limiting current plateaus could not be obtained.

Increase in surface area due to surface roughening is the most probable explanation for this behavior [6].

After sweeping the potential at 10 mV/sec to just above the limiting current plateau, evidenced by the onset of hydrogen evolution, the electrodes were removed, washed, and dried, and Scanning Electron Microscopy (SEM) images of the zinc deposits were taken for the various rotational speeds. At the three lower rotational speeds (Figures 6, 7, 8) the dendritic growth covers the entire surface. The dendrites seen in these Figures are whiskery in shape and extend normal from the surface into the bulk solution. At the higher rotational speeds the dendritic growth was observed only near the disk edge (Figures 9, 10, 11) and was of layered and spiral form. This behavior is due to the secondary current distribution becoming more nonuniform at higher rotational speeds below the limiting current. At the same fraction of limiting current, the current density near the disk edge is higher at higher rpms, and the surface near the edge becomes more rough. At limiting current the current distribution is uniform over the electrode, but a dendritic zinc deposit with a high surface area has already been formed.

Substantial surface roughening can prevent obtaining a limiting current plateau because the surface area increases during the measurement, causing a corresponding increase in limiting current [6]. In order to avoid the rapid development of surface roughness during measurement, higher potential scan rates were used. The results for a high scan rate of 200 mV/sec is shown in Figure 12 for 0.05 M ZnCl<sub>2</sub> + 1 M

KCl. Accurate limiting current plateaus at the higher rotational speeds were obtained using these higher scan rates. The diffusion coefficient for  $\mathrm{Zn}^{+2}$  was calculated from the limiting currents obtained in Figures 5 and 12, and is tabulated in Table 1. At the lower potential scan rate, 10 mV/sec, the calculated diffusion coefficient for  $\mathrm{Zn}^{+2}$  is lower than literature values (Table 3), but the experimental result at the higher scan rates is in good agreement with values of  $\mathrm{Zn}^{+2}$  diffusion coefficients reported previously [5,7]. The zinc deposition is shown to be diffusion controlled and the limiting current is proportional to the square root of the rotational speed for the higher scan rates in Figure 13. Using 200 mV/sec scan rate data, the average diffusion coefficient for  $\mathrm{Zn}^{+2}$  at  $\mathrm{22^{O}C}$  in 0.05 M  $\mathrm{ZnCl}_2$  + 1 M KCl is D = 0.981  $\pm$  0.050 x  $\mathrm{10}^{-5}$  cm<sup>2</sup>/sec.

Numerous experiments in 0.10 M  $\rm ZnCl^2 + 1$  M KCl at various rotational speeds and potential sweep rates were made in order to study the effect of concentration on the diffusion coefficient of  $\rm Zn^{+2}$ . Results are shown in Figure 14. Accurate limiting current plateaus were obtained only at the potential scan rate of 200 mV/sec. At the higher rotational speeds, the current becomes independent of the rotational speed and the zinc electrodeposition reaction is no longer diffusion controlled (Figure 13). The average diffusion coefficient for  $\rm Zn^{+2}$  in 0.10 M  $\rm ZnCl_2 + 1$  M KCl at  $\rm 22^{\circ}C$  is D = 0.892  $\pm$  0.067 x  $\rm 10^{-5}$  cm<sup>2</sup>/sec. Experimental data are summarized in Table 1. The experimental results show that more accurate limiting current plateaus for the higher rotational speeds and scan rates can be obtained at lower zinc concentrations.

In 0.50 M  $\rm ZnCl_2$  + 1 M KCl solution a limiting current plateau could only be obtained with 200 and 400 rpm and at the highest scan rate, 200 mV/sec (Figure 15). The average diffusion coefficient obtained was 0.583 x  $10^{-5}$  cm<sup>2</sup>/sec. At higher rotational speeds and lower sweep rates limiting current plateaus were not discernible.

## Rotating Disk Studies in ZnSO4 + Na2SO4 Solutions

In acidic chloride solutions, zinc forms various chloride complexes in addition to the simple cation:  $\operatorname{ZnCl}_4^-$ ,  $\operatorname{ZnCl}_3^-$ ,  $\operatorname{ZnCl}_2$ ,  $\operatorname{ZnCl}^+$  [9,14]. In order to demonstrate the influence of zinc chloride complexes in the foregoing limiting current measurements, experiments in acidic  $\operatorname{ZnSO}_4^+$  +  $\operatorname{Na}_2\operatorname{SO}_4^-$  solutions were also performed. No reference to sulfate complexes of zinc were found in the literature [9].

Figure 16 shows the polarization curves at scan rate 200 mV/sec in  $0.05 \text{ M ZnSO}_{\text{$\mbox{$\mbo$ 

The plot of current vs. square root of the rotational speed is shown in Figure 17 at a fixed potential on the limiting current plateau E = -2.300 V vs. SCE. The zinc deposition reaction is diffusion controlled and the average diffusion coefficient for  $Zn^{+2}$  at  $22^{\circ}C$  in 0.05 M  $ZnSO_{4}$  + 1 M  $Na_{2}SO_{4}$  is  $D = 0.786 \pm 0.038 \times 10^{-5}$  cm<sup>2</sup>/sec.

Several experiments were performed in 0.10 M  $\rm ZnSO_4$  + 1 M  $\rm Na_2SO_4$ , pH = 2.5, T = 22°C at various rotational speeds. Figure 18 shows the polarization curves at a scan rate of 200 mV/sec. At the higher rpms, accurate limiting current plateaus could not be obtained, just as in the chloride system.

From Figure 17, at E = -2.404 V vs. SCE, it can be seen that the current at higher rpms is still proportional to the square root of the rotational speed, thus the reaction is diffusion controlled. The average diffusion coefficient for  $\rm Zn^{+2}$  at 22°C in 0.10 M  $\rm ZnSO_4$  + 1 M  $\rm Na_2SO_4$  is D = 0.565  $\pm$  0.023 x  $\rm 10^{-5}$  cm<sup>2</sup>/sec. The zinc sulfate experimental data are summarized in Table 2.

#### DISCUSSION

The experimental diffusivity data show slightly higher values of the zinc diffusion coefficient in 0.05 M ZnSO<sub>4</sub> than in 0.05 M ZnCl<sub>2</sub>, and show a dependence upon both the rotational speed and sweep rate. The average diffusion coefficient decreases as the concentration of zinc increases. Experiments with higher zinc concentrations were attempted, but limiting current plateaus could not be obtained. The higher currents needed in more concentrated solutions caused even more rapid increase in the surface area of the zinc deposit.

The diffusion coefficients obtained in this study are compared with other available diffusion data in Table 3. Substantial differences exist between the diffusion coefficients reported for ZnCl<sub>2</sub> solutions by the interferometric measurements and those obtained by electrochemical measurements. These differences arise from the diffusional quantities measured by the two experimental techniques. The interferometric methods use a free-diffusion, stagnant cell to measure zinc diffusivities, while the electrochemical methods yield effective diffusion coefficients under forced-convection conditions. The formation of zinc-chloro-complex ions may also influence the two types of diffusion coefficients to different degrees in the ZnCl<sub>2</sub> solutions. Miller and Rard [10,15] also present component diffusion coefficients for the ternary (ZnCl<sub>2</sub>-KCl-H<sub>2</sub>0) system.

The  ${\rm ZnSO}_{\downarrow\downarrow}$  results are more ambiguous in that they show a large decrease in the diffusion coefficient with increasing concentration. Surface roughening arguments cannot justify such a large decline in diffusion coefficient. The results by Albright and Miller [11] show a

similar but smaller dependence on concentration than this work; the authors suggest that the decline is due to ion-pair formation, which causes greater structuring in more concentrated solutions.

#### SUMMARY

Mass transfer limiting currents in acidic  ${\rm ZnCl}_2$  and  ${\rm ZnSO}_4$  solutions were investigated. Cathodic polarization curves were obtained by potential scans at various rotational speeds of a zinc disk electrode. The surface roughness of zinc during slow potential scan rates (10 mV/sec) and high rotational speeds (1600,2000 rpm) prevented obtaining limiting current plateaus. However, at higher scan rates, distinct limiting current plateaus were defined. From the limiting current, the diffusion coefficient was calculated, D = 0.98  $\pm$  0.05 x 10<sup>-5</sup> cm<sup>2</sup>/sec (0.05 M ZnCl<sub>2</sub> + 1 M KCl). In 0.10  ${\rm ZnCl}_2$  + 1 M KCl at the higher rotational speeds a limiting current plateau could not be observed at the higher potential scan rates. Experiments in acidic  ${\rm ZnSO}_4$  solution showed similar results. The zinc diffusion coefficient obtained from these experiments was D = 0.78  $\pm$  0.04 x 10<sup>-5</sup> cm<sup>2</sup>/sec (0.05 M ZnSO<sub>4</sub> + 1 M Na<sub>2</sub>SO<sub>4</sub>).

#### ACKNOWLEDGEMENT

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Table 1. Experimental Data and Results for Deposition of Zinc from ZnCl<sub>2</sub> + 1 M KCl Solution

|        |               |                    |                   |                      |             |       |                      | <del></del> |      |
|--------|---------------|--------------------|-------------------|----------------------|-------------|-------|----------------------|-------------|------|
|        | ZnCl<br>Conc. |                    |                   | _                    | 0           | Sweep | ••                   |             | _    |
|        | cone.         | 1 <sub>L</sub>     | k                 | D .                  | Ω           | Rate  | ν                    | Se          | Re   |
|        |               |                    | ×10 <sup>-3</sup> | ×10 <sup>-5</sup>    |             | mV/   | ×10 <sup>-2</sup>    |             |      |
| Expt.  | M             | mA/cm <sup>2</sup> | cm/sec            | cm <sup>2</sup> /sec | rpm         | sec   | cm <sup>2</sup> /sec |             |      |
|        |               |                    |                   |                      | <del></del> |       |                      |             |      |
| 1      | 0.05          | 15.3               | 1.6               | 0.419                | 200         | 10    | 0.9969               | 2380        | 525  |
| 2      | 0.05          | 12.9               | 1.3               | 0.324                | 200         | 10    | 0.9969               | 3080        | 525  |
| 3<br>4 | 0.05          | 20.2               | 2.1               | 0.376                | 400         | 10    | 0.9969               | 2650        | 1050 |
| 4      | 0.05          | 20.9               | 2.2               | 0.399                | 400         | 10    | 0.9969               | 2500        | 1050 |
| 5<br>6 | 0.05          | 28.2               | 2.9               | 0.371                | 800         | 10    | 0.9969               | 2690        | 2100 |
|        | 0.05          | 26.6               | 2.8               | 0.339                | 800         | 10    | 0.9969               | 2940        | 2100 |
| 7 .    | 0.05          | 34.6               | 3.6               | 0.372                | 1200        | 10    | 0.9969               | 2680        | 3150 |
| 8      | 0.05          | 33.0               | 3.4               | 0.347                | 1200        | 10    | 0.9969               | 2870        | 3150 |
| 9 .    | 0.05          | 41.3               | 4.3               | 0.388                | 1600        | 10    | 0.9969               | 2570        | 4200 |
| 10     | 0.05          | 37.9               | 3.9               | 0.343                | 1600        | 10    | 0.9969               | 2910        | 4200 |
| 11     | 0.05          | 44.3               | 4.6               | 0.367                | 2000        | 10    | 0.9969               | 2720        | 5250 |
| 12     | 0.05          | 41.9               | 4.3               | 0.337                | 2000        | 10    | 0.9969               | 2960        | 5250 |
| 13     | 0.05          | 25.8               | 2.7               | 0.916                | 200         | 100   | 0.9969               | 1090        | 525  |
| 14     | 0.05          | 22.5               | 2.3               | 0.746                | 200         | 100   | 0.9969               | 1340        | 525  |
| 15     | 0.05          | 24.2               | 2.5               | 0.832                | 200         | 100   | 0.9969               | 1220        | 525  |
| 16     | 0.05          | . 26.8             | 2.8               | 0.966                | 200         | 200   | 0.9969               | 1030        | 525  |
| 17     | 0.05          | 28.0               | 2.9               | 1.032                | 200         | 200   | 0.9969               | 970         | 525  |
| 18     | 0.05          | 38.2               | 4.0               | 0.980                | 400         | 200   | 0.9969               | 1020        | 1050 |
| 19     | 0.05          | 40.8               | 4.3               | 1.081                | 400         | 200   | 0.9969               | 920         | 1050 |
| 20     | 0.05          | 53.5               | 5.5               | 0.965                | 800         | 200   | 0.9969               | 1030        | 2100 |
| 21     | 0.05          | 53.5               | 5.5               | 0.965                | 800         | 200   | 0.9969               | 1030        | 2100 |
| 22     | 0.05          | 65.0               | 6.7               | 0.953                | 1200        | 200   | 0.9969               | 1050        | 3150 |
| 23     | 0.05          | 63.7               | 6.6               | 0.925                | 1200        | 200   | 0,9969               | 1080        | 3150 |
| 24     | 0.05          | 80.3               | 8.3               | 1.055                | 1600        | 200   | 0.9969               | 940         | 4200 |
| 25     | 0.05          | 73.9               | 7.7               | 0.932                | 1600        | 200   | 0.9969               | 1070        | 4200 |
| 26     | 0.05          | 85.4               | 8.8               | 0.979                | 2000        | 200   | 0.9969               | 1020        | 5250 |
| 27     | 0.05          | 82.8               | 8.6               | 0.935                | 2000        | 200   | 0.9969               | 1070        | 5250 |
| 28     | 0.10          | 48.4               | 2.5               | 0.846                | 200         | 200   | 1.011                | 1200        | 518  |
| 29     | 0.10          | 53.5               | 2.8               | 0.983                | 200         | 200   | 1.011                | 1030        | 518  |
| 30     | 0.10          | 79.0               | 4.1               | 1.033                | 400         | 200   | 1.011                | 980         | 1036 |
| 31     | 0.10          | 70.1               | 3.6               | 0.878                | 400         | 200   | 1.011                | 1150        | 1036 |
| 32     | 0.10          | 98.1               | 5.1               | 0.850                | 800         | 200   | 1.011                | 1190        | 2072 |
| 33     | 0.10          | 98.1               | 5.1               | 0.850                | 800         | 200   | 1.011                | 1190        | 2072 |
| 34     | 0.10          | 118.5              | 6.1               | 0.832                | 1200        | 200   | 1.011                | 1220        | 3108 |
| 36     | 0.10          | 124.8              | 6.5               | 0.914                | 1200        | 200   | 1.011                | 1110        | 3108 |
| 37     | 0.10          | 137.6              | 7.1               | 0.854                | 1600        | 200   | 1.011                | 1180        | 4144 |
| 38     | 0.10          | 99.1               | 5.1               | 0.877                | 800         | 100   | 1.011                | 1150        | 2072 |
| 39     | 0.50          | 191.0              | 2.0               | 0.593                | 200         | 200   | 1.080                | 1820        | 485  |
| 40     | 0.50          | 188.0              | 1.9               | 0.580                | 200         | 200   | 1.080                | 1860        | 485  |
| 41     | 0.50          | 188.0              | 1.9               | 0.580                | 200         | 200   | 1.080                | 1860        | 485  |
| 42     | 0.50          | 265.0              | 2.7               | 0.577                | 400         | 200   | 1.080                | 1870        | 970  |
| 43     | 0.50          | 268.0              | 2.8               | 0.584                | 400         | 200   | 1.080                | 1850        | 970  |

Experimental Data and Results for Deposition of Zinc from  ${
m ZnSO}_{f u}$  + 1 M  ${
m Na}_2{
m SO}_{f u}$  Solution æ Sc x10<sup>-2</sup> cm<sup>2</sup>/sec Sweep Rate mV/ sec r C; x10<sup>-5</sup> cm<sup>2</sup>/sec 0.852 0.765 0.765 0.768 0.758 0.758 0.758 0.812 0.758 0.758 0.559 0.559 0.559 0.559 0.559 0.558 x10<sup>-3</sup> mA/cm<sup>2</sup> ZnSO4 Σ Table 2. Expt. 

Table 3. Comparison of Diffusion Coefficients of Zinc with Literature Data

|                                       |                               |                | (D in 10 <sup>-5</sup> cm <sup>2</sup> /sec) | <sup>2</sup> /sec) |       |      |       |                    |       |      |      |
|---------------------------------------|-------------------------------|----------------|--|--------------------|-------|------|-------|--------------------|-------|------|------|
| Reference                             | Solution                      | Method         | Temp. (OC)                                   | Ħ                  |       |      | Conce | Concentrations (M) | (M)   |      |      |
| -                                     |                               |                |  |                    | 0.05  | 0.1  | 0.2   | 4.0                | 0.5   | 1.0  | 1.6  |
| Present Study ZnCl <sub>2</sub> + 1 M | ZnCl <sub>2</sub> + 1 M KCl   | RDE            | 55   | 2.4                | 0.98  | 0.89 |       |                    | 0.58  |      |      |
| 5                                     | $ZnCl_2 + 1 M KCl$            | RDE            | 25   |                    | 0.89  |      |       |                    |       |      |      |
| 7                                     | ZnCl <sub>2</sub> + 3.5 M KCl | Capillary      | 26.5   |                    |       |      |       | 0.82               |       |      | 0.88 |
| 8                                     | ZnC1 <sub>2</sub> + 3 M KC1   | Polarography   | . 52   | 3.5                |       | 0.52 | -     |                    | 0.45  | 0.41 |      |
| 10                                    | 2nc1 <sub>2</sub>             | Interferometry | 22   |                    |       |      | 1.027 | 1.007              | ,     |      |      |
| 12                                    | ZnC1 <sub>2</sub>             | Interferometry | 52   |                    | 1.048 |      |       |                    |       |      |      |
| 15                                    | ZnC1 <sub>2</sub>             | Interferometry | 25   | ٠                  |       |      |       | 1.003              | 0.991 |      |      |
| Present Study                         | ZnSO4 + 1 M Na2SO4            | RDE            | 55   | 2.5                | 0.78  | 0.57 |       |                    |       |      |      |
| 11                                    | η OSuz                        | Interferometry | 25   |                    | 09.0  | 0.56 | 0.51  | •                  | 0.43  | 0.37 |      |

#### FIGURE CAPTIONS

- Fig. 1a. Rotating disc zinc electrode.
- Fig. 1b. RDE electrolysis cell.
- Fig. 2a. Cell for Zn-RDE studies.
- Fig. 2b. Experimental apparatus.
- Fig. 3a. Circuit for potentiostatic deposition of zinc.
- Fig. 4. Limiting current plateaus in 0.05 M ZnCl<sub>2</sub> + 1 M KCl.
- Fig. 5. Dependence of  $i_L$  on rpm (Levich plot).
- Fig. 6. SEM micrographs of zinc deposits on RDE in 0.5 M ZnCl<sub>2</sub> + 1 M KCl, above the limiting current at rotation speed 200 rpm.

  Magnification: (A) 10x, (B) 500x, (C) original RDE surface before zinc deposition, 500x, (D) 2000x.
- Fig. 7. SEM micrographs of zinc deposits on RDE in 0.05 M ZnCl<sub>2</sub> + 1 M KCl, above the limiting current at rotation speed 400 rpm.

  Magnification: (A) 10x, (B) 500x, (C) 2000x.
- Fig. 8. SEM micrographs of zinc deposits on RDE in 0.05 M ZnCl<sub>2</sub> + 1 M KCl, above the limiting current at rotation speed 800 rpm.

  Magnification: (A) 10x, (B) 500x, (C) 2000x.
- Fig. 9. SEM micrographs of zinc deposits on RDE in 0.05 M ZnCl<sub>2</sub> + 1 M KCl, above the limiting current at rotation speed 1200 rpm.

  Magnification: (A) 10x, (B) 500x, (C) 2000x.
- Fig. 10. SEM micrographs of zinc deposits on RDE in 0.05 M ZnCl<sub>2</sub> + 1 M KCl, above the limiting current at rotation speed 1600 rpm.

  Magnification: (A) 10x, (B) 500x, (C) 2000x.

- Fig. 11. SEM micrographs of zinc deposits on RDE in 0.05 M ZnCl<sub>2</sub> + 1 M KCl, above the limiting current at rotation speed 2000 rpm.

  Magnification: (A) 10x, (B) 500x, (C) 2000x.
- Fig. 12. Limiting current plateaus in 0.05 M ZnCl<sub>2</sub> + 1 M KCl.
- Fig. 13. Dependence of  $i_L$  on rpm (Levich plot).
- Fig. 14. Limiting current plateaus in 0.10 M ZnCl<sub>2</sub> + 1 M KCl.
- Fig. 15. Limiting current plateaus in 0.50 M ZnCl<sub>2</sub> + 1 M KCl.
- Fig. 16. Limiting current plateaus in  $0.05 \text{ ZnSO}_4 + 1 \text{ M Na}_2 \text{SO}_4$ .
- Fig. 17. Dependence of  $i_L$  on rpm (Levich plot).
- Fig. 18. Limiting current plateaus in 0.10  $ZnSO_4 + 1 M Na_2SO_4$ .

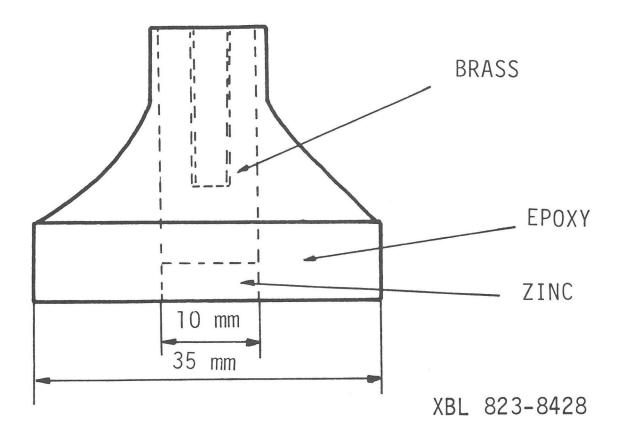


Fig. la

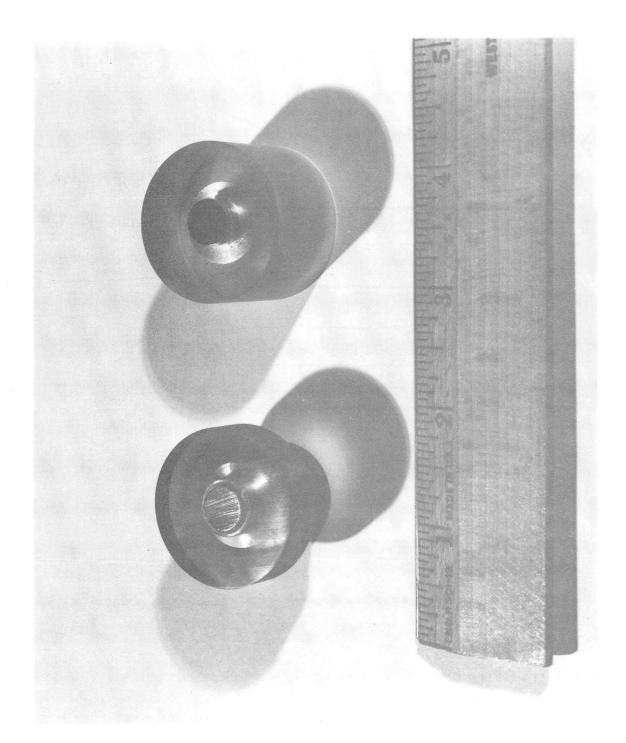


Fig. 1b

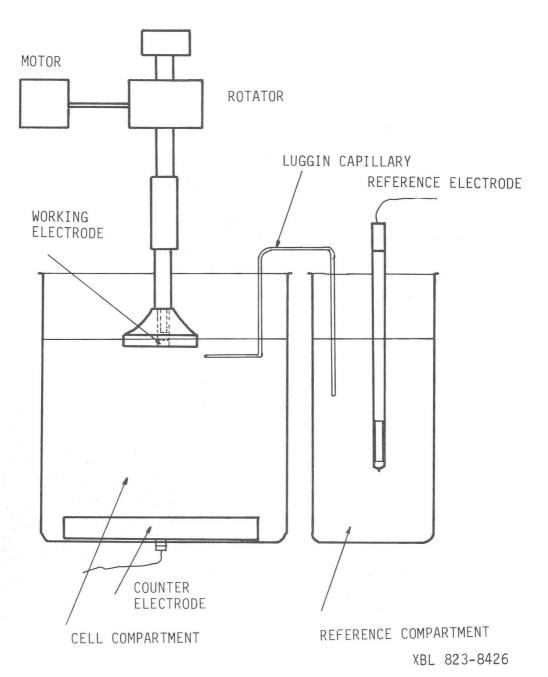
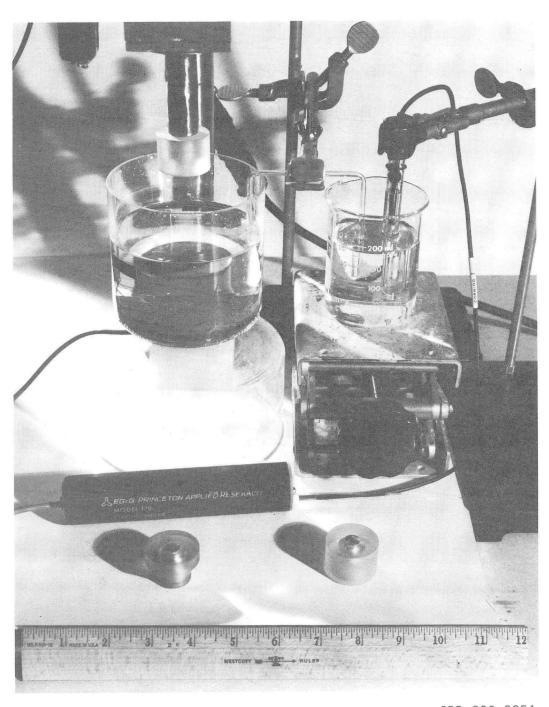


Fig. 2a.



CBB 823-2854

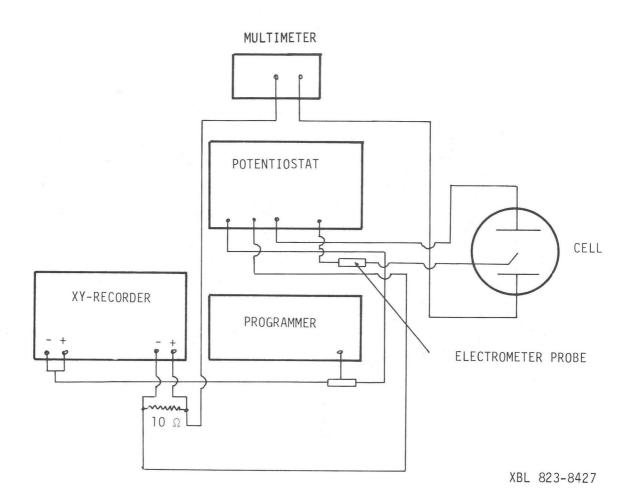
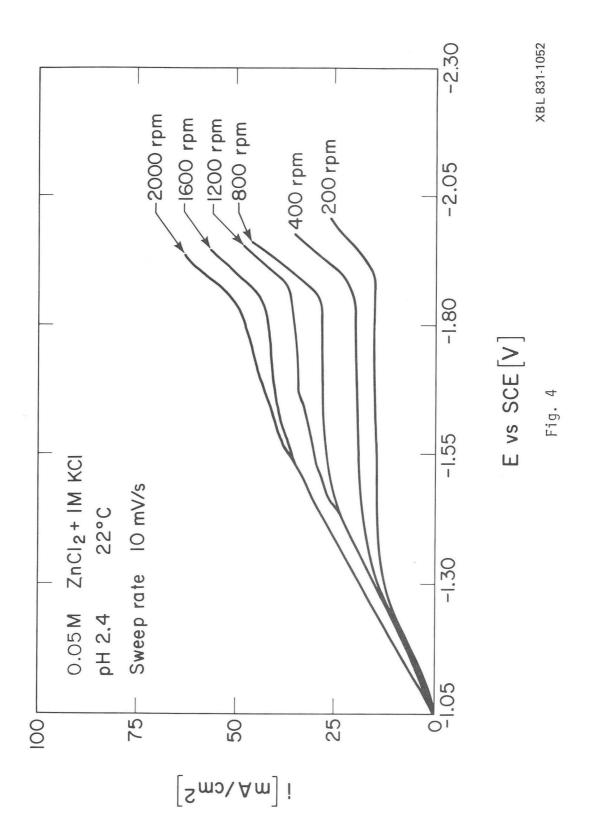


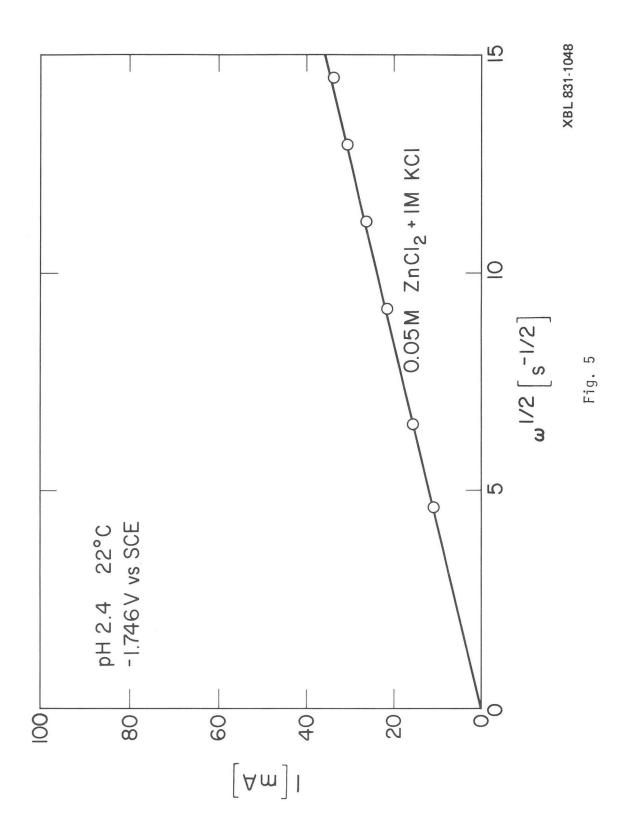
Fig. 3a



Fig. 3b

CBB 823-2850





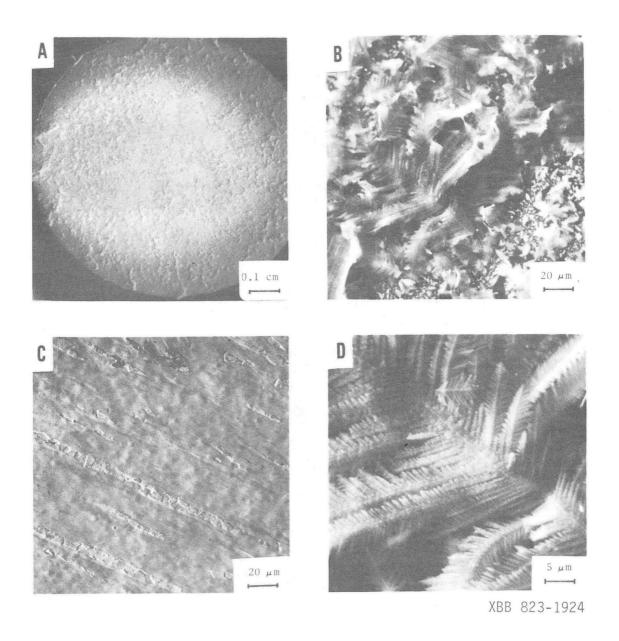


Fig. 6

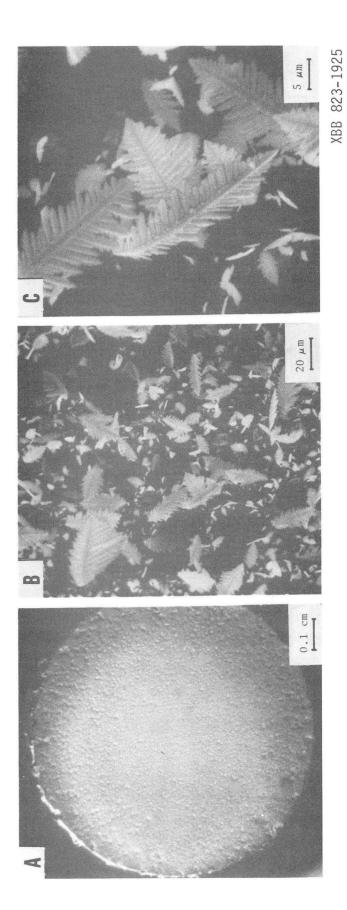


Fig. 7

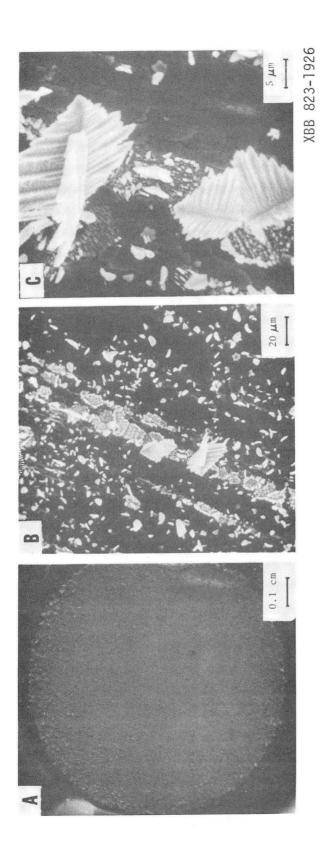


Fig. 8

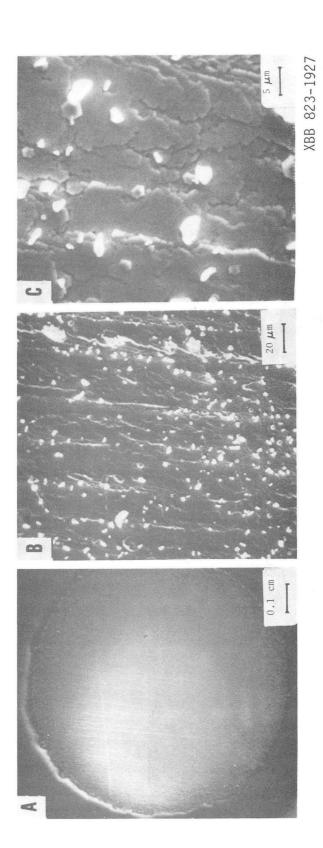


Fig. 9

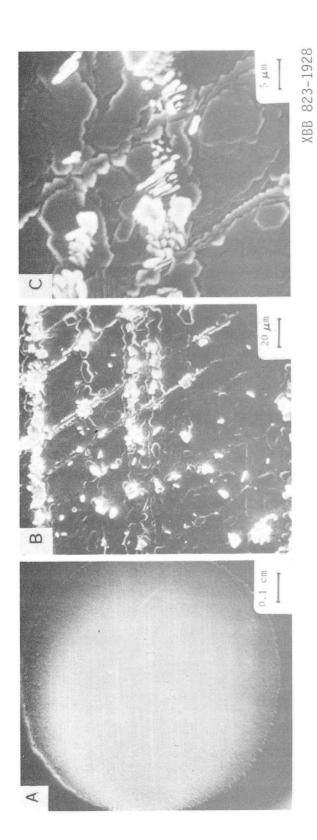


Fig. 10

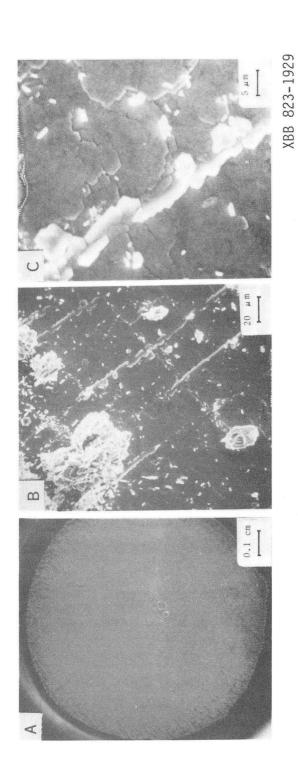
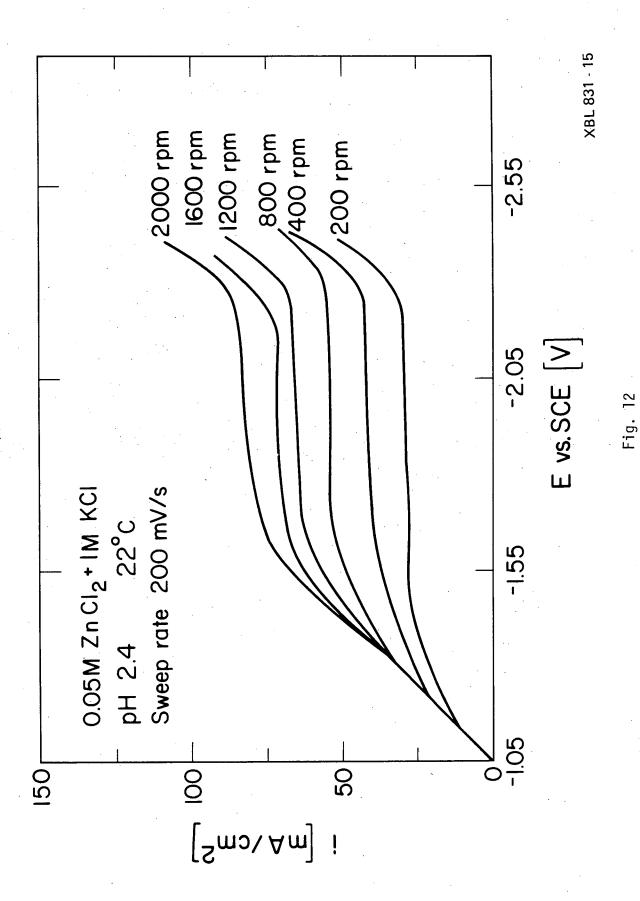
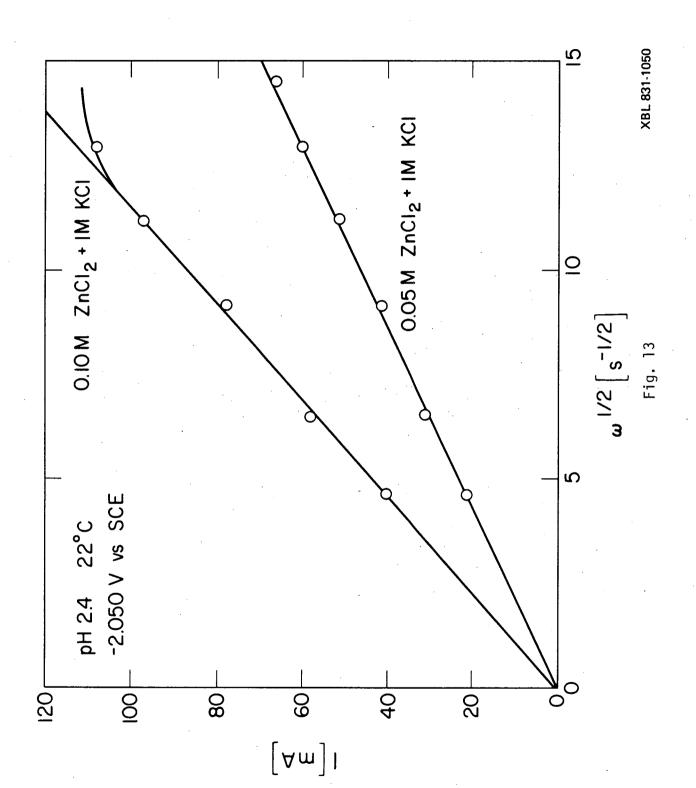
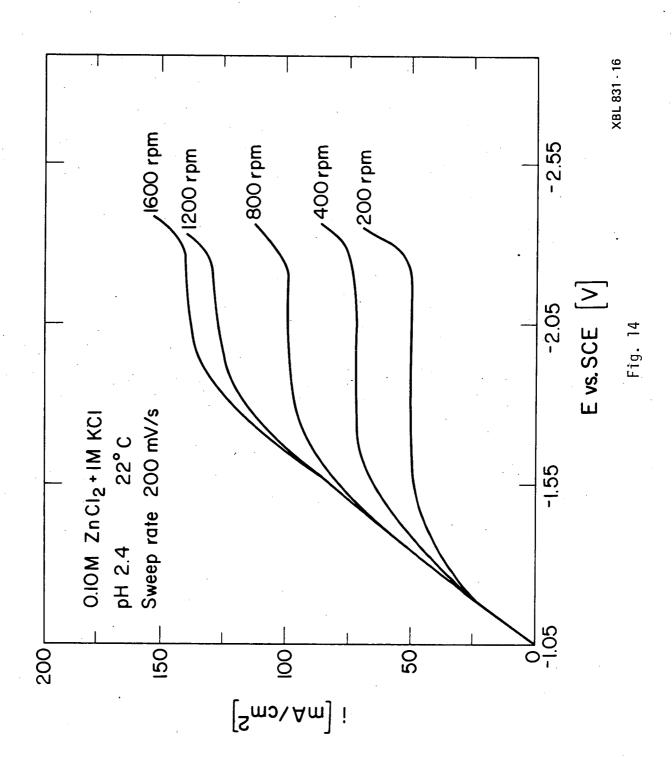
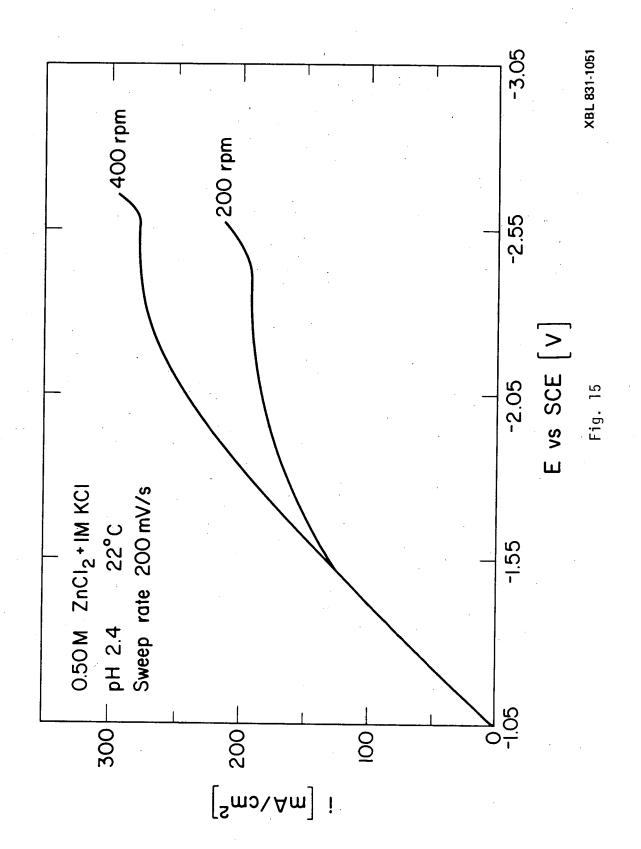


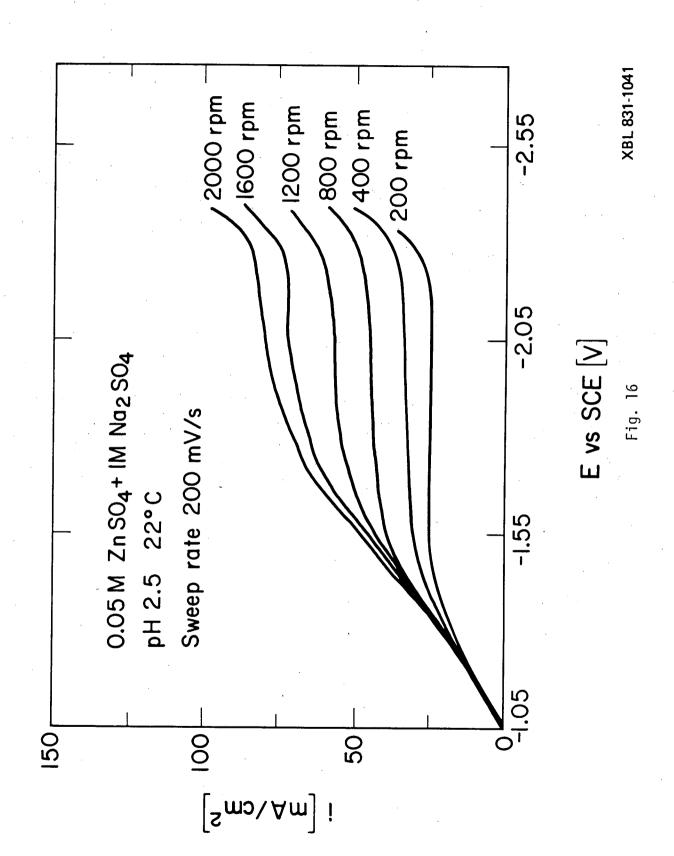
Fig. 11

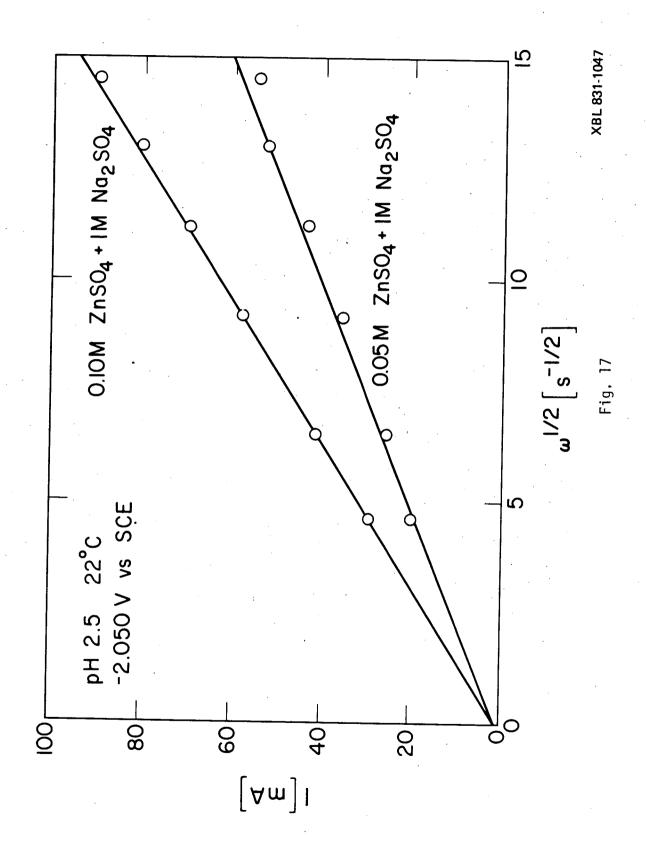












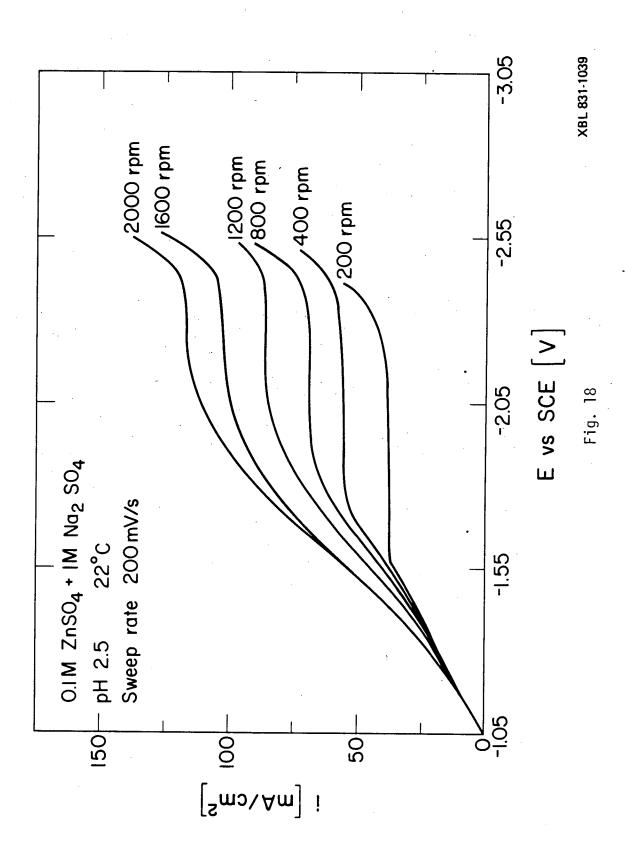


Table 1. Experimental Data and Results for Deposition of Zinc from  ${\rm ZnCl}_2$  + 1 M KCl Solution

|             | ZnCl<br>Conc. | i <sub>L</sub>     | k                           | D   | Ω    | Sweep<br>Rate | ν   | Sc   | Re   |
|-------------|---------------|--------------------|-----------------------------|---|------|---------------|---|------|------|
| Expt.       | М             | mA/cm <sup>2</sup> | x10 <sup>-3</sup><br>cm/sec | x10 <sup>-5</sup><br>cm <sup>2</sup> /sec | rpm  | mV/<br>sec    | x10 <sup>-2</sup><br>cm <sup>2</sup> /sec |      |      |
| 1.          | 0.05          | 15.3               | 1.6                         | 0.419                                     | 200  | 10            | 0.9969                                    | 2380 | 525  |
|             | 0.05          | 12.9               | 1.3                         | 0.324                                     | 200  | 10            | 0.9969                                    | 3080 | 525  |
| 2<br>3<br>4 | 0.05          | 20.2               | 2.1                         | 0.376                                     | 400  | 10            | 0.9969                                    | 2650 | 1050 |
| 7           | 0.05          | 20.9               | 2.2                         | 0.399                                     | 400  | 10            | 0.9969                                    | 2500 | 1050 |
| 5           | 0.05          | 28.2               | 2.9                         | 0.371                                     | 800  | 10            | 0.9969                                    | 2690 | 2100 |
| 5<br>6      | 0.05          | 26.6               | 2.8                         | 0.339                                     | 800  | 10            | 0.9969                                    | 2940 | 2100 |
| 7           | 0.05          | 34.6               | 3.6                         | 0.372                                     | 1200 | 10            | 0.9969                                    | 2680 | 3150 |
| 8           | 0.05          | 33.0               | 3.4                         | 0.347                                     | 1200 | 10            | 0.9969                                    | 2870 | 3150 |
| 9.          | 0.05          | 41.3               | 4.3                         | 0.388                                     | 1600 | 10            | 0.9969                                    | 2570 | 4200 |
| 10          | 0.05          | 37.9               | 3.9                         | 0.343                                     | 1600 | 10            | 0.9969                                    | 2910 | 4200 |
| 11          | 0.05          | 44.3               | 4.6                         | 0.367                                     | 2000 | 10            | 0.9969                                    | 2720 | 5250 |
| 12          | 0.05          | 41.9               | 4.3                         | 0.337                                     | 2000 | 10            | 0.9969                                    | 2960 | 5250 |
| 13          | 0.05          | 25.8               | 2.7                         | 0.916                                     | 200  | 100           | 0.9969                                    | 1090 | 525  |
| 14          | 0.05          | 22.5               | 2.3                         | 0.746                                     | 200  | 100           | 0.9969                                    | 1340 | 525  |
| 15          | 0.05          | 24.2               | 2.5                         | 0.832                                     | 200  | 100           | 0.9969                                    | 1220 | 525  |
| 16          | 0.05          | 26.8               | 2.8                         | 0.966                                     | 200  | 200           | 0.9969                                    | 1030 | 525  |
| 17          | 0.05          | 28.0               | 2.9                         | 1.032                                     | 200  | 200           | 0.9969                                    | 970  | 525  |
| 18          | 0.05          | 38.2               | 4.0                         | 0.980                                     | 400  | 200           | 0.9969                                    | 1020 | 1050 |
| 19          | 0.05          | 40.8               | 4.3                         | 1.081                                     | 400  | 200           | 0.9969                                    | 920  | 1050 |
| 20          | 0.05          | 53.5               | 5.5                         | 0.965                                     | 800  | 200           | 0.9969                                    | 1030 | 2100 |
| 21          | 0.05          | 53.5               | 5.5                         | 0.965                                     | 800  | 200           | 0.9969                                    | 1030 | 2100 |
| 22          | 0.05          | 65.0               | 6.7                         | 0.953                                     | 1200 | 200           | 0.9969                                    | 1050 | 3150 |
| 23          | 0.05          | 63.7               | 6.6                         | 0.925                                     | 1200 | 200           | 0.9969                                    | 1080 | 3150 |
| 24          | 0.05          | 80.3               | 8.3                         | 1.055                                     | 1600 | 200           | 0.9969                                    | 940  | 4200 |
| 25          | 0.05          | 73.9               | 7.7                         | 0.932                                     | 1600 | 200           | 0.9969                                    | 1070 | 4200 |
| 26          | 0.05          | 85.4               | 8.8                         | 0.979                                     | 2000 | 200           | 0.9969                                    | 1020 | 5250 |
| 27          | 0.05          | 82.8               | 8.6                         | 0.935                                     | 2000 | 200           | 0.9969                                    | 1070 | 5250 |
| 28          | 0.10          | 48.4               | 2.5                         | 0.846                                     | 200  | 200           | 1.011                                     | 1200 | 518  |
| 29          | 0.10          | 53.5               | 2.8                         | 0.983                                     | 200  | 200           | 1.011                                     | 1030 | 518  |
| 30          | 0.10          | 79.0               | 4.1                         | 1.033                                     | 400  | 200           | 1.011                                     | 980  | 1036 |
| 31          | 0.10          | 70.1               | 3.6                         | 0.878                                     | 400  | 200           | 1.011                                     | 1150 | 1036 |
| 32          | 0.10          | 98.1               | 5.1                         | 0.850                                     | 800  | 200           | 1.011                                     | 1190 | 2072 |
| 33          | 0.10          | 98.1               | 5.1                         | 0.850                                     | 800  | 200           | 1.011                                     | 1190 | 2072 |
| 34          | 0.10          | 118.5              | 6.1                         | 0.832                                     | 1200 | 200           | 1.011                                     | 1220 | 3108 |
| 36          | 0.10          | 124.8              | 6.5                         | 0.914                                     | 1200 | 200           | 1.011                                     | 1110 | 3108 |
| 37          | 0.10          | 137.6              | 7.1                         | 0.854                                     | 1600 | 200           | 1.011                                     | 1180 | 4144 |
| 38          | 0.10          | 99.1               | 5.1                         | 0.877                                     | 800  | 100           | 1.011                                     | 1150 | 2072 |
| 39          | 0.50          | 191.0              | 2.0                         | 0.593                                     | 200  | 200           | 1.080                                     | 1820 | 485  |
| 40          | 0.50          | 188.0              | 1.9                         | 0.580                                     | 200  | 200           | 1.080                                     | 1860 | 485  |
| 41          | 0.50          | 188.0              | 1.9                         | 0.580                                     | 200  | 200           | 1.080                                     | 1860 | 485  |
| 42          | 0.50          | 265.0              | 2.7                         | 0.577                                     | 400  | 200           | 1.080                                     | 1870 | 970  |
| 43          | 0.50          | 268.0              | 2.8                         | 0.584                                     | 400  | 200           | 1.080                                     | 1850 | 970  |

Experimental Data and Results for Deposition of Zinc from  ${\rm ZnSO}_{\rm L}$  + 1 M  ${\rm Na}_{\rm 2}{\rm SO}_{\rm L}$  Solution Table 2.

| Expt. M mA/cm <sup>2</sup> cm/sec cm <sup>2</sup> /sec rpm sec cm <sup>2</sup> /sec cm <sup>2</sup> /sec cm |            | ZnSO <sub>4</sub><br>Conc. | i<br>L             | ᅶ                        | Д               | Ci ·  | Sweep      | >                                      | Sc   | Re   |
|--|------------|----------------------------|--------------------|--------------------------|-----------------|-------|------------|--|------|------|
| 0.05       24.2       2.5       0.852       200         0.05       34.4       3.6       0.860       400         0.05       34.4       3.6       0.860       400         0.05       31.8       3.3       0.765       400         0.05       45.9       4.8       0.788       800         0.05       44.6       4.6       0.788       800         0.05       44.6       4.6       0.788       800         0.05       44.6       4.6       0.788       800         0.05       54.8       5.7       0.758       1200         0.05       67.5       7.0       0.758       1200         0.05       68.8       7.1       0.758       200         0.05       68.8       7.1       0.768       200         0.10       36.9       1.9       0.569       200         0.10       36.9       1.9       0.569       200         0.10       34.4       1.8       0.590       400         0.10       34.4       1.8       0.590       400         0.10       53.5       2.8       0.590       400         0.10 <th>kpt.</th> <th>Σ</th> <th>mA/cm<sup>2</sup></th> <th>x10<sup>-3</sup> cm/sec</th> <th><sup>2</sup>/2</th> <th>rpm</th> <th>mV/<br/>sec</th> <th>x10<sup>-2</sup> cm<sup>2</sup>/sec</th> <th></th> <th></th>   | kpt.       | Σ                          | mA/cm <sup>2</sup> | x10 <sup>-3</sup> cm/sec | <sup>2</sup> /2 | rpm   | mV/<br>sec | x10 <sup>-2</sup> cm <sup>2</sup> /sec |      |      |
| 0.05       22.9       2.4       0.765       400         0.05       34.4       3.6       0.860       400         0.05       31.8       3.3       0.765       400         0.05       45.9       4.8       0.788       800         0.05       44.6       4.8       0.788       800         0.05       44.6       4.8       0.758       800         0.05       54.8       5.7       0.758       1200         0.05       67.5       7.0       0.836       1600         0.05       66.2       6.9       0.758       1200         0.05       67.5       7.0       0.788       1600         0.05       66.2       6.9       0.756       1600         0.05       66.2       6.9       0.768       200         0.05       66.2       6.9       0.768       200         0.05       66.2       6.9       0.768       200         0.05       66.2       6.9       0.768       200         0.10       34.4       1.8       0.599       400         0.10       53.5       2.8       0.590       400         0.10  |            | 0.05                       |                    |                          |                 | 200 . | 100        | 1.112                                  | 1310 | 471  |
| 0.05       34.4       3.6       0.860       400         0.05       31.8       3.3       0.765       400         0.05       45.9       4.8       0.788       800         0.05       44.6       4.8       0.788       800         0.05       44.6       4.8       0.758       800         0.05       54.8       5.7       0.758       1200         0.05       67.5       7.0       0.836       1600         0.05       66.2       6.9       0.812       1600         0.05       66.2       6.9       0.836       1600         0.05       66.2       6.9       0.768       200         0.05       66.2       6.9       0.768       200         0.05       66.2       6.9       0.768       200         0.05       66.2       6.9       0.768       200         0.05       66.2       6.9       0.768       200         0.05       68.8       7.1       0.768       200         0.10       33.4       1.8       0.590       400         0.10       53.5       2.8       0.590       400         0.10<  | 0.1        | 0.05                       | _                  | •                        | •               | 200   | 200        | 1.112                                  | 1420 | 471  |
| 0.05       31.8       3.3       0.765       400         0.05       31.8       3.3       0.765       400         0.05       45.9       4.8       0.788       800         0.05       44.6       4.8       0.788       800         0.05       54.8       5.7       0.758       1200         0.05       67.5       7.0       0.788       1200         0.05       67.5       7.0       0.788       1200         0.05       67.5       7.0       0.783       1200         0.05       66.2       6.9       0.812       1600         0.05       68.8       7.1       0.768       200         0.05       68.8       7.1       0.768       200         0.10       36.9       1.9       0.569       200         0.10       34.4       1.8       0.590       400         0.10       33.5       2.8       0.590       400         0.10       77.2       3.9       0.540       400         0.10       77.3       3.8       0.540       400         0.10       77.2       3.9       0.540       400         0.10  |            | 0.05                       | _                  | •                        | •               | 100   | 100        | 1.112                                  | 1290 | 942  |
| 0.05       31.8       3.3       0.765       400         0.05       45.9       4.8       0.788       800         0.05       44.6       4.6       0.758       800         0.05       54.8       5.7       0.758       1200         0.05       67.5       7.0       0.783       1200         0.05       67.5       7.0       0.836       1600         0.05       66.2       6.9       0.812       1600         0.05       66.2       6.9       0.812       1600         0.05       68.8       7.1       0.768       2000         0.05       68.8       7.1       0.768       2000         0.10       36.9       1.9       0.569       200         0.10       34.4       1.8       0.590       400         0.10       34.4       1.8       0.590       400         0.10       53.5       2.8       0.590       400         0.10       77.3       3.8       0.540       800         0.10       77.3       3.8       0.540       800         0.10       77.3       3.8       0.540       800         0.  |            | 0.05                       | _                  | •                        | •               | 400   | 100        | 1.112                                  | 1450 | 942  |
| 0.05       45.9       4.8       0.788       800         0.05       44.6       4.8       0.788       800         0.05       54.8       5.7       0.758       1200         0.05       54.8       5.7       0.758       1200         0.05       66.2       6.9       0.812       1600         0.05       66.2       6.9       0.812       1600         0.05       66.2       6.9       0.812       1600         0.05       66.2       6.9       0.812       1600         0.05       68.8       7.1       0.768       200         0.10       36.9       1.9       0.768       200         0.10       36.9       1.9       0.569       200         0.10       34.4       1.8       0.559       400         0.10       33.9       1.9       0.569       400         0.10       53.5       2.8       0.590       400         0.10       53.5       2.8       0.540       400         0.10       77.2       3.9       0.540       400         0.10       89.2       4.6       0.558       1200         0.  |            | 0.05                       | _                  | •                        | •               | 001   | 200        | 1.112                                  | 1450 | 942  |
| 0.05       45.9       4.8       0.788       800         0.05       44.6       4.6       0.755       800         0.05       54.8       5.7       0.758       1200         0.05       67.5       7.0       0.836       1600         0.05       66.2       6.9       0.812       1600         0.05       68.8       7.1       0.768       2000         0.05       68.8       7.1       0.768       2000         0.05       68.8       7.1       0.768       2000         0.05       68.8       7.1       0.768       2000         0.10       36.9       1.9       0.569       200         0.10       34.4       1.8       0.559       400         0.10       53.5       2.8       0.590       400         0.10       53.5       2.8       0.590       400         0.10       77.2       3.9       0.540       800         0.10       77.3       3.7       0.540       800         0.10       89.2       4.6       0.558       1200         0.10       101.9       5.3       0.548       1600 <td< td=""><td></td><td>0:05</td><td>_</td><td>•</td><td>•</td><td>800</td><td>100</td><td>1.112</td><td>1410</td><td>1884</td></td<>  |            | 0:05                       | _                  | •                        | •               | 800   | 100        | 1.112                                  | 1410 | 1884 |
| 0.05       44.6       4.6       0.755       800         0.05       54.8       5.7       0.758       1200         0.05       67.5       7.0       0.836       1600         0.05       66.2       6.9       0.812       1600         0.05       68.8       7.1       0.766       1600         0.05       71.3       7.4       0.768       2000         0.05       68.8       7.1       0.728       2000         0.10       36.9       1.9       0.569       200         0.10       34.4       1.8       0.569       200         0.10       34.4       1.8       0.590       400         0.10       33.5       2.8       0.590       400         0.10       53.5       2.8       0.590       400         0.10       77.2       3.9       0.590       400         0.10       77.3       3.7       0.540       800         0.10       77.3       3.9       0.590       400         0.10       89.2       4.6       0.58       1200         0.10       89.2       4.6       0.59       1600         0.1  |            | 0.05                       | _                  | •                        | •               | 800   | 100        | 1.112                                  | 1410 | 1884 |
| 0.05       54.8       5.7       0.758       1200         0.05       67.5       7.0       0.836       1600         0.05       66.2       6.9       0.812       1600         0.05       66.2       6.9       0.766       1600         0.05       71.3       7.4       0.768       2000         0.05       71.3       7.4       0.768       2000         0.05       68.8       7.1       0.768       200         0.05       68.8       7.1       0.768       200         0.10       36.9       1.9       0.569       200         0.10       34.4       1.8       0.569       200         0.10       34.4       1.8       0.599       400         0.10       53.5       2.8       0.599       400         0.10       53.5       2.8       0.590       400         0.10       77.3       3.8       0.590       400         0.10       77.3       3.8       0.590       400         0.10       89.2       4.6       0.585       1200         0.10       89.2       4.6       0.599       1600         0  |            | 0.05                       | _                  | •                        | •               | 800   | 200        | 1.112                                  | 1470 | 1884 |
| 0.05       54.8       5.7       0.758       1200         0.05       67.5       7.0       0.836       1600         0.05       66.2       6.9       0.812       1600         0.05       63.7       6.6       0.766       1600         0.05       71.3       7.4       0.768       2000         0.05       77.1       0.768       2000         0.10       36.9       1.9       0.569       200         0.10       36.9       1.9       0.569       200         0.10       34.4       1.8       0.569       200         0.10       34.4       1.8       0.569       200         0.10       34.4       1.8       0.590       400         0.10       53.5       2.8       0.590       400         0.10       75.2       3.8       0.590       400         0.10       77.3       3.8       0.540       800         0.10       77.3       3.8       0.590       400         0.10       89.2       4.6       0.58       1200         0.10       89.2       4.6       0.58       1200         0.10       10  |            | 0.05                       | _                  | 5.7                      | •               | 1200  | 100        | 1.112                                  | 1470 | 2826 |
| 0.05       67.5       7.0       0.836       1600         0.05       66.2       6.9       0.812       1600         0.05       63.7       6.6       0.766       1600         0.05       71.3       7.4       0.768       2000         0.05       68.8       7.1       0.728       2000         0.10       36.9       1.9       0.569       200         0.10       34.4       1.8       0.569       200         0.10       34.4       1.8       0.569       200         0.10       53.5       2.8       0.590       400         0.10       53.5       2.8       0.590       400         0.10       75.2       3.9       0.590       400         0.10       77.3       3.7       0.540       800         0.10       89.2       4.6       0.558       1200         0.10       89.2       4.6       0.558       1200         0.10       101.9       5.3       0.548       1600         0.10       114.6       5.9       0.599       1600         0.10       114.6       5.9       0.594       200         <  | 0          | 0.05                       | _                  | 5.7                      | •               | 1200  | 200        | 1.112                                  | 1470 | 2826 |
| 0.05       66.2       6.9       0.812       1600         0.05       63.7       6.6       0.766       1600         0.05       71.3       7.4       0.768       2000         0.05       68.8       7.1       0.728       2000         0.10       36.9       1.9       0.569       200         0.10       34.4       1.8       0.569       200         0.10       53.5       2.8       0.590       400         0.10       73.9       3.8       0.590       400         0.10       75.2       3.9       0.585       800         0.10       77.3       3.7       0.540       800         0.10       77.3       3.7       0.540       800         0.10       89.2       4.6       0.558       1200         0.10       89.2       4.6       0.558       1200         0.10       101.9       5.3       0.558       1200         0.10       101.9       5.3       0.599       1600         0.10       114.6       5.9       0.599       1600         0.10       114.6       5.9       0.599       1600  | _          | 0.05                       | •                  | •                        | •               | 1600  | 100        | 1.112                                  | 1330 | 3768 |
| 0.05       63.7       6.6       0.766       1600         0.05       71.3       7.4       0.768       2000         0.05       68.8       7.1       0.728       2000         0.10       36.9       1.9       0.569       200         0.10       34.4       1.8       0.569       200         0.10       53.5       2.8       0.590       400         0.10       73.9       3.8       0.590       400         0.10       75.2       3.9       0.590       400         0.10       77.3       3.7       0.540       800         0.10       77.3       3.7       0.540       800         0.10       77.3       3.7       0.540       800         0.10       89.2       4.6       0.558       1200         0.10       89.2       4.6       0.558       1200         0.10       101.9       5.3       0.558       1200         0.10       103.2       5.3       0.599       1600         0.10       114.6       5.9       0.599       1600         0.10       114.6       5.9       0.594       2000 <td>2</td> <td>0.05</td> <td>•</td> <td>•</td> <td>•</td> <td>1600</td> <td>100</td> <td>1.112</td> <td>1370</td> <td>3768</td>   | 2          | 0.05                       | •                  | •                        | •               | 1600  | 100        | 1.112                                  | 1370 | 3768 |
| 0.05       71.3       7.4       0.768       2000         0.05       68.8       7.1       0.728       2000         0.10       36.9       1.9       0.569       200         0.10       34.4       1.8       0.569       200         0.10       33.5       2.8       0.590       400         0.10       53.5       2.8       0.590       400         0.10       53.5       2.8       0.590       400         0.10       53.5       2.8       0.590       400         0.10       75.2       3.9       0.590       400         0.10       77.3       3.7       0.540       800         0.10       89.2       4.6       0.585       1200         0.10       89.2       4.6       0.558       1200         0.10       89.2       4.6       0.558       1200         0.10       101.9       5.3       0.548       1600         0.10       114.6       5.9       0.554       2000         0.10       114.6       5.9       0.554       2000   | ٣          | 0.05                       |                    | •                        |                 | 1600  | 200        | 1.112                                  | 1450 | 3768 |
| 0.05       68.8       7.1       0.728       2000         0.10       36.9       1.9       0.569       200         0.10       34.4       1.8       0.569       200         0.10       53.5       2.8       0.590       400         0.10       53.5       2.8       0.590       400         0.10       73.9       3.8       0.590       400         0.10       75.2       3.9       0.590       400         0.10       75.2       3.9       0.585       800         0.10       75.2       3.9       0.585       800         0.10       89.2       4.6       0.558       1200         0.10       89.2       4.6       0.558       1200         0.10       101.9       5.3       0.548       1600         0.10       103.2       5.3       0.548       1600         0.10       114.6       5.9       0.554       2000   | <b>†</b>   | 0.05                       |                    | •                        | •               | 2000  | 100        | 1.112                                  | 1450 | 4710 |
| 0.10       36.9       1.9       0.569       200         0.10       34.4       1.8       0.512       200         0.10       34.4       1.8       0.590       400         0.10       53.5       2.8       0.590       400         0.10       73.9       3.8       0.590       400         0.10       75.2       3.9       0.590       400         0.10       77.2       3.9       0.585       800         0.10       71.3       3.7       0.540       800         0.10       89.2       4.6       0.558       1200         0.10       89.2       4.6       0.558       1200         0.10       101.9       5.3       0.548       1600         0.10       103.2       5.3       0.599       1600         0.10       114.6       5.9       0.554       2000  | 2          | 0.05                       | -                  | •                        | •               | 2000  | 100        | 1.112                                  | 1530 | 4710 |
| 0.10       36.9       1.9       0.569       200         0.10       34.4       1.8       0.512       200         0.10       53.5       2.8       0.590       400         0.10       53.5       2.8       0.590       400         0.10       73.9       3.8       0.590       400         0.10       75.2       3.9       0.570       800         0.10       71.3       3.7       0.540       800         0.10       89.2       4.6       0.558       1200         0.10       89.2       4.6       0.558       1200         0.10       101.9       5.3       0.548       1600         0.10       103.2       5.3       0.599       1600         0.10       114.6       5.9       0.554       2000  | 9          | 0.10                       | -                  | 1.9                      | •               | 200   | 200        | 1.118                                  | 1960 | 7468 |
| 0.10       34.4       1.8       0.512       200         0.10       53.5       2.8       0.590       400         0.10       53.5       2.8       0.590       400         0.10       73.9       3.8       0.590       400         0.10       75.2       3.9       0.570       800         0.10       71.3       3.7       0.540       800         0.10       89.2       4.6       0.558       1200         0.10       89.2       4.6       0.558       1200         0.10       89.2       4.6       0.558       1200         0.10       101.9       5.3       0.548       1600         0.10       103.2       5.3       0.599       1600         0.10       114.6       5.9       0.554       2000   | 7          | 0.10                       | •                  | 1.9                      | •               | 200   | 200        | 1.118                                  | 1960 | 468  |
| 0.10       53.5       2.8       0.590       400         0.10       53.5       2.8       0.590       400         0.10       73.9       3.8       0.570       800         0.10       75.2       3.9       0.585       800         0.10       71.3       3.7       0.540       800         0.10       89.2       4.6       0.558       1200         0.10       89.2       4.6       0.558       1200         0.10       101.9       5.3       0.548       1600         0.10       103.2       5.3       0.599       1600         0.10       114.6       5.9       0.554       2000  | 8          | 0.10                       | -                  | •                        | •               | 200   | 100        | 1.118                                  | 2180 | 468  |
| 0.10       53.5       2.8       0.590       400         0.10       73.9       3.8       0.570       400         0.10       75.2       3.9       0.585       800         0.10       71.3       3.7       0.540       800         0.10       89.2       4.6       0.558       1200         0.10       89.2       4.6       0.558       1200         0.10       101.9       5.3       0.548       1600         0.10       103.2       5.3       0.548       1600         0.10       114.6       5.9       0.554       2000         0.10       114.6       5.9       0.554       2000  | ę.         | 0.10                       |                    | •                        | •               | 00h   | 200        | 1.118                                  | 1890 | 936  |
| 0.10       53.5       2.8       0.590       400         0.10       75.2       3.9       0.570       800         0.10       71.3       3.7       0.540       800         0.10       89.2       4.6       0.558       1200         0.10       89.2       4.6       0.558       1200         0.10       89.2       4.6       0.558       1200         0.10       101.9       5.3       0.548       1600         0.10       103.2       5.3       0.548       1600         0.10       114.6       5.9       0.554       2000         0.10       114.6       5.9       0.554       2000   | 0.         | 0.10                       |                    | •                        | •               | 400   | 200        | 1.118                                  | 1890 | 936  |
| 0.10       73.9       3.8       0.570       800         0.10       75.2       3.9       0.585       800         0.10       71.3       3.7       0.540       800         0.10       89.2       4.6       0.558       1200         0.10       89.2       4.6       0.558       1200         0.10       101.9       5.3       0.548       1600         0.10       114.6       5.9       0.599       1600         0.10       114.6       5.9       0.554       2000  | 7.         | 0.10                       | •                  | •                        | •               | 400   | 200        | 1.118                                  | 1890 | 936  |
| 0.10       75.2       3.9       0.585       800         0.10       71.3       3.7       0.540       800         0.10       89.2       4.6       0.558       1200         0.10       89.2       4.6       0.558       1200         0.10       101.9       5.3       0.548       1600         0.10       103.2       5.3       0.599       1600         0.10       114.6       5.9       0.554       2000         0.10       114.6       5.9       0.554       2000  | 22         | 0.10                       |                    | •                        | •               | 800   | 200        | 1.118                                  | 1960 | 1872 |
| 0.10       71.3       3.7       0.540       800         0.10       89.2       4.6       0.558       1200         0.10       89.2       4.6       0.558       1200         0.10       101.9       5.3       0.548       1600         0.10       103.2       5.3       0.599       1600         0.10       114.6       5.9       0.554       2000         0.10       114.6       5.9       0.554       2000  | 33         | 0.10                       |                    | •                        | •               | 800   | 200        | 1.118                                  | 1910 | 1872 |
| 0.10       89.2       4.6       0.558       1200         0.10       89.2       4.6       0.558       1200         0.10       101.9       5.3       0.548       1600         0.10       103.2       5.3       0.599       1600         0.10       114.6       5.9       0.554       2000         0.10       114.6       5.9       0.554       2000  | <b>π</b> ζ | 0.10                       |                    | •                        | •               | 800   | 200        | 1.118                                  | 2070 | 1872 |
| 0.10 89.2 4.6 0.558 1200 0.10 89.2 4.6 0.558 1200 0.10 101.9 5.3 0.548 1600 0.10 103.2 5.3 0.599 1600 0.10 114.6 5.9 0.554 2000 0.10 114.6 5.9 0.554 2000  | 55         | 0.10                       | •                  | •                        | •               | 1200  | 200        | 1.118                                  | 2000 | 2808 |
| 0.10 89.2 4.6 0.558 1200<br>0.10 101.9 5.3 0.548 1600<br>0.10 103.2 5.3 0.599 1600<br>0.10 114.6 5.9 0.554 2000<br>0.10 114.6 5.9 0.554 2000   | 9          | 0.10                       | •                  | •                        | •               | 1200  | 200        | 1.118                                  | 2000 | 2808 |
| 0.10 101.9 5.3 0.548 1600 0.10 103.2 5.3 0.599 1600 0.10 114.6 5.9 0.554 2000 0.10 114.6 5.9 0.554 2000  | 27         | 0.10                       |                    | •                        | •               | 1200  | 200        | 1.118                                  | 2000 | 2808 |
| 0.10 103.2 5.3 0.599 1600<br>0.10 114.6 5.9 0.554 2000<br>0.10 114.6 5.9 0.554 2000  | 82         | 0.10                       | 01.                | •                        | •               | 1600  | 200        | 1.118                                  | 2040 | 3744 |
| 0.10 114.6 5.9 0.554 2000 0.10 114.6 5.9 0.554 2000  | 53         | Ξ.                         | 03.                | •                        | •               | 1600  | 200        | 1.118                                  | 1870 | 3744 |
| 0.10 114.6 5.9 0.554 2000  | 30         | -                          | 14.                | •                        | •               | 2000  | 200        | 1.118                                  | 2020 | 4680 |
|  | 31         | <b>.</b>                   |                    | •                        | •               | 2000  | 200        | 1.118                                  | 2020 | 4680 |

Table 3. Comparison of Diffusion Coefficients of Zinc with Literature Data

|               |                               |                | (D in $10^{-5}$ cm <sup>2</sup> /sec) | 2/sec) |        |      |        |                    |       |      |      |
|---------------|-------------------------------|----------------|---------------------------------------|--------|--------|------|--------|--------------------|-------|------|------|
| Reference     | Solution                      | Method         | Temp. (OC)                            | Hd     | *      | -    | Concen | Concentrations (M) | (M)   |      |      |
|               |                               |                |                                       |        | 0.05   | 0.1  | 0.2    | ħ.0                | 0.5   | 1.0  | 1.6  |
| Present Study | ZnCl <sub>2</sub> + 1 M KCl   | RDE            | 22                                    | 2.4    | . 86.0 | 0.89 |        |                    | 0.58  |      |      |
| 5             | ZnCl <sub>2</sub> + 1 M KCl   | RDE            | 25                                    | :      | 0.89   |      |        |                    |       | · .  | -    |
| 7             | ZnCl <sub>2</sub> + 3.5 M KCl | Capillary      | 26.5                                  |        |        |      |        | 0.82               |       | ·    | 0.88 |
| 80            | $2ncl_2 + 3 M Kcl$            | Polarography   | 25                                    | 3.5    |        | 0.52 |        |                    | 0.45  | 0.41 |      |
| 10            | ZnC1 <sub>2</sub>             | Interferometry | 25                                    |        |        |      | 1.027  | 1.007              |       |      |      |
| 12            | ZnC1 <sub>2</sub>             | Interferometry | . 55                                  |        | 1.048  |      |        |                    |       |      |      |
| 15            | 2nc1 <sub>2</sub>             | Interferometry | 52                                    |        |        |      |        | 1.003              | 0.991 |      |      |
| Present Study | $2nSO_{4} + 1 M Na_{2}SO_{4}$ | RDE            | 22                                    | 2.5    | 0.78   | 0.57 |        |                    |       |      | •    |
| 11            | znS0 <sub>4</sub>             | Interferometry | 25                                    |        | 09.0   | 0.56 | 0.51   |                    | 0.43  | 0.37 |      |
|               |                               |                |                                       |        |        |      |        |                    |       |      |      |

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