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March 16, 1964

Berkeley, California

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ABSTRACT

The design and use of parallel-channel collimators with the scintillation camera are described. Equations for calculating the optimum hole diameter, length, and septal thickness are given, together with parameters of a number of collimators designed for a given resolution and maximum gamma-ray energy. Examples are shown of their performance with the scintillation camera in clinical use.

INTRODUCTION

The scintillation camera is a sensitive electronic instrument for taking pictures of the distribution of gamma-ray- and positron-emitting isotopes in vivo. The pictures are similar to those obtained from mechanical scanners, but they are produced in much less time. No scanning is employed because the scintillation camera is sensitive to all parts of its field of view during the entire exposure time.

To obtain an image of activity distribution a collimator first projects a gamma-ray image of the subject onto a scintillator. The instrument described here uses a single sodium iodide crystal 11.5 inches in diameter by 0.5 inch thick. Coupled to the crystal through an optical light guide is a close-packed hexagonal array of 19 multiplier phototubes. The phototubes view overlapping areas in the scintillator so that light from each scintillation divides among the 19 tubes. The combination of scintillator, light guide, and phototubes is called an image detector (1). The phototubes are connected to an analog computer that identifies the X and Y coordinates and the brightness of each scintillation occurring in the crystal. All photopeak scintillations are reproduced on an oscilloscope as point flashes of light in the same relative positions in which they occurred in the scintillator. The flashes are photographed over a period of time, and an image of the subject results.

To obtain the best combination of sensitivity and resolution for a given subject and radionuclide, the optimum collimation method should be used. A brief account of the three collimating methods--pinhole, multichannel, and positron coincidence--has been given (2). For positron emitters, coincidence collimation gives excellent sensitivity and resolution for both large and small subjects. For small subjects containing gamma-ray emitters, pinhole

collimation is the method of choice. It is used to obtain high-resolution pictures of small subjects such as the thyroid gland.

However, for large gamma-ray-emitting subjects, such as the brain or liver, collimators with large numbers of parallel holes (2 through 9) give the best combination of sensitivity and resolution. A drawing of this type of collimator is shown with the scintillation camera image detector in Fig. 1.

Parallel-channel collimators have properties that are different from those of other collimators. One characteristic is the one-to-one size relationship between the subject and the image produced in the scintillator. In addition the size is independent of the distance between the subject and the collimator. This is an advantage in diagnostic situations where an organ lies at an unknown depth and its size is to be determined.

Sharpest image resolution is obtained in the parts of the subject lying closest to the collimator. However, parallel-channel collimators can be designed to provide resolution equal to focused collimators in the deeper parts of the subject. The "depth of focus" of parallel-channel collimators can be much greater than that provided by focused collimators.

Parallel-channel collimators have substantially uniform "depth response," or in other words, equal sensitivity to activity at different depths in air. In tissue the depth response is of course modified by tissue attenuation.

Many combinations of hole diameter, length, and septal thickness are possible in multichannel collimators. Formulas are given in the next section to assist in designing collimators that have maximum efficiency for a given resolution and maximum gamma-ray energy. The collimators are most efficient when they can be designed for use with low-energy gamma rays,

because the septa can be thinner and more holes can be packed into a given area. However, even when the collimators are designed for use with gamma rays of 0.4 MeV or more, the overall sensitivity camera is still considerably higher than that of focused-collimator mechanical scanners.

DESIGN OF PARALLEL-CHANNEL COLLIMATORS

Mathematical analysis of the image produced by a parallel-channel collimator is rather complex compared with pinhole collimation or positron coincidence collimation. In the latter two methods, a point source in the subject is imaged as a disc on the image detector. With multichannel collimators, gamma rays from a point source may strike the image detector in several areas, because they may travel through more than one of the holes to reach the scintillator. The shape of the irradiated areas depends on the shape of the holes, their distribution pattern, and the placement of the point source relative to the holes.

The mathematical analysis of this type of collimator is simplified if the assumption is made that the collimator moves sideways in the manner of a Bucky filter during the exposure time. Formulas have been derived that give the sensitivity and resolution as a function of hole diameter, length, and septal thickness. They have been derived by (a) assuming that the collimator moves relative to the subject and image detector during the entire exposure time, (b) determining the fraction of the time that a point source in the subject is visible to each element in the image detector and the solid angle of each element, and (c) integrating to determine the overall counting efficiency.

For example, consider a collimator consisting of a rectangular array of square holes as shown in Fig. 2. This section view shows a plane through the

center of a row of holes. The width of the holes is d , the length is a , and the septal thickness is t . The distance from the radioactive subject to the near end of the collimator is b , and the distance from the central plane of the scintillator to the other end of the collimator is c .

If the collimator is stationary, the distribution of gamma rays has the irregular shape shown at the top of Fig. 2, but if the collimator moves in the direction shown, the average distribution of gamma rays that strike the scintillator has a triangular shape. The intensity is then a maximum at point o directly above the point source, and it falls linearly to zero, assuming opaque septa, at points q and q' . The distance oq , which is approximately equal to the full width of the gamma-ray intensity curve at half maximum, is defined as the geometric resolution-distance R .

From geometric considerations, it can be shown that

$$R = \frac{d(a + b + c)}{a} . \tag{1}$$

As expected, the resolution-distance R is smallest, or in other words the image is sharpest, when the distances b and c are small.

The geometric efficiency of the collimator is given by the formula

$$g = \left[\frac{Kd^2}{a(d + t)} \right]^2 , \tag{2}$$

where g is defined as the number of gamma rays that impinge on the scintillator divided by the total number emitted by the subject. Scattered gamma rays and any that travel through the septa are not included. It should be noted that g is independent of b , the distance between the subject and the collimator, providing the subject is completely imaged within the boundaries

of the scintillator. Therefore the counting rate of a subject in air should be independent of the distance from the collimator to the subject. This has been found by experiment to be approximately true. The value of the constant K depends on the shape of the holes and their distribution pattern. It has been determined mathematically and confirmed approximately by experiment that $K = 0.282$ for square holes in a square array and $K = 0.238$ for round holes in a hexagonal array.

The shortest distance a gamma ray can travel through septal material when taking the unwanted path of minimum attenuation pr , shown in Fig. 3, is w . From geometric considerations,

$$w = \frac{at}{2d + t} \quad \text{or} \quad t = \frac{2dw}{a - w} \quad (3)$$

From experimental studies, it has been determined that acceptable images result when the narrow-beam (Compton + photoelectric) attenuation of gamma rays taking the path pr is 95% or more. Assuming a given collimator material and gamma-ray energy, the distance w can be calculated. With w known, the minimum permissible septal thickness can be calculated for any hole diameter and length.

The sensitivity S in terms of dots per minute recorded on the picture per microcurie of activity in the subject is given by

$$S = 2.2 \times 10^6 \epsilon f_a \frac{Kd^2}{a^2 (d + t)^2} \quad (4)$$

where f_a is the abundance factor of the gamma ray, or the average number of gamma rays of a given energy emitted per disintegration. The photopeak counting efficiency ϵ is defined as the fraction of gamma rays incident on the scintillator that produce a dot on the picture when the pulse-height selector

window is adjusted to accept nearly all the photopeak scintillations. Values of ϵ are given in other papers. (1, 2, 10). With the above equations, collimators can be designed that have optimum hole diameter, length, and septal thickness for a given subject-to-collimator distance, maximum gamma-ray energy, and desired resolution.

DEPTH OF FOCUS AND DEPTH RESPONSE

Since clinical subjects are nearly always several inches thick, the "depth of focus," or the depth over which a relatively sharp image is obtained, must be taken into account when evaluating any collimation method. The resolution of focused collimators is best for the parts of the subject at the geometric focus, which is usually 3 inches from the collimator. Its depth of focus is limited, and planes closer and farther away are less sharply resolved (11, 12).

In comparison, the resolution of parallel-channel collimators is best for the parts of the subject closest to the collimator, and the resolution decreases with increasing distance. However, a parallel-channel collimator can be designed to give as good resolution as desired at any depth. For instance, it can be designed to have the same resolution at 3-inch distance as a focused collimator. Then it will have greater depth of focus because it will sharply resolve all the closer planes, whereas the focused collimator will not.

Both collimating methods have "uniform depth response" in air, or equal counting sensitivity for activity at different depths. However, neither has uniform depth response in tissue because of gamma-ray scattering and absorption. It might be thought that because a stationary focused collimator

has a maximum response to a point source on the axis at a distance of 3 inches (13), it would be more sensitive to activity lying on that plane in an actual scanning situation. This is not the case, as indicated by others (12, 14, 15) and confirmed experimentally by the author. Under working conditions, the "depth response" of the two collimating methods is the same, and each decreases with distance only because of tissue attenuation.

PARAMETERS OF TYPICAL COLLIMATORS

Parallel-channel collimators with hexagonal arrays of round holes can be made by (a) drilling holes in a plate, (b) cementing together lengths of tubing, or (c) casting the entire collimator in a suitable mold. Rectangular arrays of square holes have been made by (d) cementing together strips of lead or tungsten, (e) pressing sheet lead into W-shaped sections and cementing them together, and (f) cementing alternate strips of lead foil and balsa wood, cutting them crosswise into strips, and cementing these alternately with lead foil. This last technique is used to make low-energy collimators.

The parameters of eight typical collimators designed for maximum efficiency consistent with the stated geometric resolution and maximum gamma-ray energy are given in Table 1. The material is lead, and all have hexagonal arrays of round holes. The calculated overall sensitivity in terms of dots/minute/ μc takes into account the abundance factors of the principal gamma rays. The contribution of the high-energy components of I^{131} was not included.

The parameters of a ninth collimator, designated as "A," are also included. This collimator was constructed before the formulas were derived,

and has parameters that are slightly less than optimum, though its characteristics are similar to those of collimator No. 6. Collimator "A" has a nominal maximum gamma-ray energy of 0.36 MeV. It was used for all the liver, kidney, and thyroid-area examples that follow.

A collimator identical to No. 3 has also been constructed and tested in clinical use. It was designed for a maximum gamma-ray energy of 0.28 MeV and was used to take the brain pictures in the examples that follow. It was not used for the kidney pictures because collimator "A" has greater depth of focus and gives better results in this application. Collimator "A" was made by technique (b) above, and No. 3 was made by technique (a). Both have about 1,400 holes in an 11-inch-diameter area.

A collimator designed for gamma rays less than 0.20 MeV has been made by technique (f) above. It has a rectangular array of 4000 square holes 0.11 inch wide by 1 inch long. It has performed satisfactorily with phantoms containing Ce^{139} (0.166 MeV) but has not yet been tested clinically.

Calculations indicate that higher sensitivity can be achieved if the collimators are made of tungsten alloy. The improvement results from having thinner septa and therefore more holes of the same diameter per unit area. The increase in sensitivity varies from 21% for collimators designed for 0.28 MeV maximum to 30% for those designed for 0.41 MeV.

PERFORMANCE OF COLLIMATORS

Since no material is completely opaque to gamma rays, the performance of the collimators is not exactly as predicted. The measured dots per minute per microcurie of radionuclide obtained from the existing collimators is larger than the calculated values at the higher gamma-ray energies. The increased count is caused by (a) gamma rays that travel through collimator material near the ends of the holes, (b) small-angle scattering of gamma rays by the channel walls, and (c) septal penetration. With some nuclides, part of the excess is caused by high-energy components in the gamma-ray spectra that produce Compton events in the crystal.

When collimator "A" is used with I^{131} , about 85% more than the theoretical number of counts are detected. Calculations indicate that about 1/3 of the excess is due to reason (a) above. This calculation was made by assuming that the effective length of the collimator is equal to its geometric length less twice the mean free path of the gamma ray in the collimator material (16). Probably only a small amount of the excess is due to reason (b) (16). The rest is presumably due to (c). When Hg^{203} is used with the "A" collimator, the excess count is about 25%, nearly all of which is caused by reason (a). Collimator No. 3 at its nominal maximum gamma-ray energy of 0.28 MeV gives an excess count of 35%. Over 3/4 of the excess in this case is calculated to be due to reason (a).

Although there is apparently a large amount of septal penetration at the higher gamma-ray energies, its effects are not normally visible in clinical pictures. The effect has been seen with the "A" collimator when small hot areas, such as the thyroid gland, are greatly overexposed. Then the "starfish" effect seen in focused collimators is visible (17).

Septal penetration can of course be reduced by making the collimators of tungsten alloy. Calculations indicate that for most collimators the number of gamma rays taking the path pr in Fig. 3 would be $1/3$ as great with the denser material if the dimensions in Table 1 are not changed.

The equations and calculations can serve only as guides in the design of collimators. Their merit should be judged by the clinical results obtained.

In the derivation of Eqs. (1) through (4), it was assumed that the collimator moved during the exposure time to provide a smooth distribution of gamma rays at the scintillator. This technique has not been used in taking pictures, however. The "collimator pattern" produced by stationary collimators is visible occasionally when small sources are imaged. With subjects larger than the thyroid gland, the effect has not been visible with the existing collimators.

Up to this point, only the theoretical geometric resolution of the collimator has been discussed. The overall resolution of the scintillation camera depends on the following factors: (a) the actual resolution of the gamma-ray image projected by the collimator, (b) the translation of this image into a light image by the scintillator, and (c) the reproduction of the scintillator image on the oscilloscope and the subsequent photographic image. The resolution lost in step (b) has been calculated to be very small for $1/2$ -inch-thick sodium iodide (10). Some resolution is lost in step (c), but the amount is not large for gamma rays with more than 0.15 MeV (1). The major factor that determines the overall resolution of the scintillation camera is the performance of the particular collimator used.

A demonstration of the overall resolution is shown in Fig. 4A. Five point sources of Ba^{133} were placed 1 inch from the "A" collimator and on the

axis of certain holes shown in Fig. 4B. An enlargement of the central portion of the resulting picture shows the resolution obtained. Gamma rays traveling through adjacent holes produced adjacent white areas on the picture, while those separated by a blank hole in the collimator produced clearly separated spots.

CLINICAL ILLUSTRATIONS

The following examples of clinical pictures were taken with the scintillation camera and two of the parallel-channel collimators.

Three views of an adult patient with a brain lesion are shown in Fig. 5. The pictures, showing (A) left lateral, (B) frontal, and (C) back views, were taken 4 hours after the administration of 700 microcuries of Hg^{203} Neohydrin. The lesion is clearly visible in (A) and (B), and is less clearly visible in (C). The exposure time was 5 minutes with the No. 3 collimator for each of the three views. Marker sources of Ba^{133} were placed at the corner of the eye and the lower margin of the ear lobe in the lateral view, and at the ear canals in the frontal and back views. The six images with graded density were obtained simultaneously with a six-lens oscilloscope camera (2, 18).

A picture of an apparently normal adult liver, taken with the "A" collimator, is shown in Fig. 6A. It was taken 2 hours after the administration of 250 microcuries of I^{131} rose bengal. The exposure time was 10 minutes. The gall bladder is shown at the center, and bowel loops are shown at the lower right. In Fig. 6B, the liver of another patient shows an apparent defect at the upper left. The exposure time in this example was 5 minutes, and the dose was 200 microcuries.

Multichannel collimators are used with the scintillation camera to take neck survey pictures of thyroid patients. The purpose is to show all active thyroid tissue within a 9- to 10-inch-diameter circle. Following the survey, a high-resolution close-up picture of the thyroid gland is taken with a triple-aperture pinhole collimator (2). Pictures of the neck area of two patients, taken 24 hours after the ingestion of 50 microcuries of I^{131} , are shown in Fig. 7A and B. The three graded-density images in each example were obtained with a three-lens oscilloscope camera. Exposure time was 5 minutes with the "A" collimator. A short extension of the upper part of the right lobe is visible in Fig. 7A, but otherwise the pictures show that the area around the thyroid is clear of radioactive lymph nodes and sub-sternal and thyroglossal extensions. The "collimator pattern" is visible in the left image of Fig. 7A.

A 10-minute exposure of a thyroid phantom containing 5.9 microcuries of mock I^{131} is shown in Fig. 7C. A suggestion of two cold nodules can be seen. These nodules are very clearly outlined in a 10-minute triple-aperture picture of the same phantom shown in an earlier publication (2).

Pictures of human kidneys taken with collimator "A" are shown in Fig. 8. All these examples were taken from the back with the patient lying face down. The first two show a normal subject with an estimated 50 microcuries of Hg^{203} Neohydrin in the kidneys. The exposure times were 10 and 2 minutes respectively. Part of the liver appears to the right in each of the examples. The picture shown in Fig. 8C was taken 20 minutes after the intravenous injection of 200 microcuries of I^{131} hippuran. In this 5-minute exposure, the hippuran is shown to be in the renal pelvis of both

kidneys. The patient had bilateral kidney disease, resulting in a slow clearing time. The high body background is due to hippuran that had not been cleared from the blood. The two small spots between the kidneys are radioactive marker sources at the eleventh thoracic and second lumbar vertebrae.

Two sequences from a time-lapse motion picture of a patient with stenosis of the left renal artery are shown in Fig. 9A. Two hundred microcuries of I^{131} hippuran were given intravenously, and pictures were taken at the rate of two frames per minute with the "A" collimator. Though the degree of stenosis was mild, some delay in the filling of the left kidney is apparent, as well as a reduction in the peak uptake.

The time-lapse sequence in Fig. 9B shows I^{131} rose bengal in the liver and intestine of a 3-month old girl. She had previous surgery for biliary atresia in which a fistula was created between the liver and duodenum. Later she had recurrent fever and jaundice, and it was thought the fistula may have closed. The time-lapse pictures show patency of the surgically created duct, since rose bengal is shown moving about in the intestine 1 hour after administration. The tracer dose was 50 microcuries, and pictures were taken at the rate of one frame every 2 minutes with the "A" collimator.

CONCLUSION

The sensitivity of the scintillation camera when it is used with multichannel collimators is appreciably higher than focused-collimator mechanical scanners. The resulting greater speed with which pictures can be taken is a decided advantage in clinical situations. A number of different views can be taken if desired, and the examination can still be completed in a relatively short time. Alternatively, the amount of radioactive tracer can be reduced to minimize the radiation dose to the patient.

The scintillation camera has the further advantage that it is continuously sensitive to all parts of the subject within its field of view. Tracer compounds with short effective half-times can be used without the distortion inherent in scanners. Because of this and the high sensitivity, rapid sequences of still pictures or time-lapse movies can be taken to show the function of an organ.

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Table 1.

Parameters of typical parallel-channel collimators with hexagonal array of round holes. Collimator material is lead and scintillator is 1/2-inch-thick sodium iodide. The calculated sensitivity is given for several radionuclides. All dimensions in inches.

Collimator	1	2	3	4	5	6	7	8	"A"	
Resolution	Med.	High	Med.	High	Med.	High	Med.	High	High	
Nominal maximum γ -ray energy	0.20	0.20	0.28	0.28	0.36	0.36	0.41	0.41	0.36	
Resolution-distance (R) at b = 1	0.42	0.28	0.45	0.30	0.49	0.32	0.50	0.34	0.35	
Resolution-distance (R) at b = 2	0.57	0.39	0.60	0.40	0.62	0.41	0.63	0.42	0.43	
Resolution-distance (R) at b = 3	0.75	0.50	0.75	0.50	0.75	0.50	0.75	0.50	0.51	
Resolution-distance (R) at b = 4	0.92	0.61	0.90	0.60	0.88	0.59	0.87	0.58	0.59	
Hole length (a)	1.0	1.0	1.5	1.5	2.2	2.2	2.6	2.6	3.0	
Hole diameter (d)	0.167	0.111	0.225	0.150	0.290	0.193	0.320	0.213	0.237	
Septum thickness (t)	0.045	0.030	0.094	0.063	0.133	0.089	0.160	0.106	0.075	
No. of holes in 11-in. -diam.-area	2480	5600	1090	2450	620	1400	490	1090	1165	
Calculated sensitivity (Dots/min/ μ c of radio-nuclide in air)										
	Ce ¹³⁹	1280	570	410	180	610	270	500	220	270
	Hg ²⁰³	-----	---	860	380	290	130	240	105	130
	I ¹³¹	-----	---	---	---	180	78	145	65	78
	Au ¹⁹⁸	-----	---	---	---	---	---	146	65	---

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FIGURE CAPTIONS

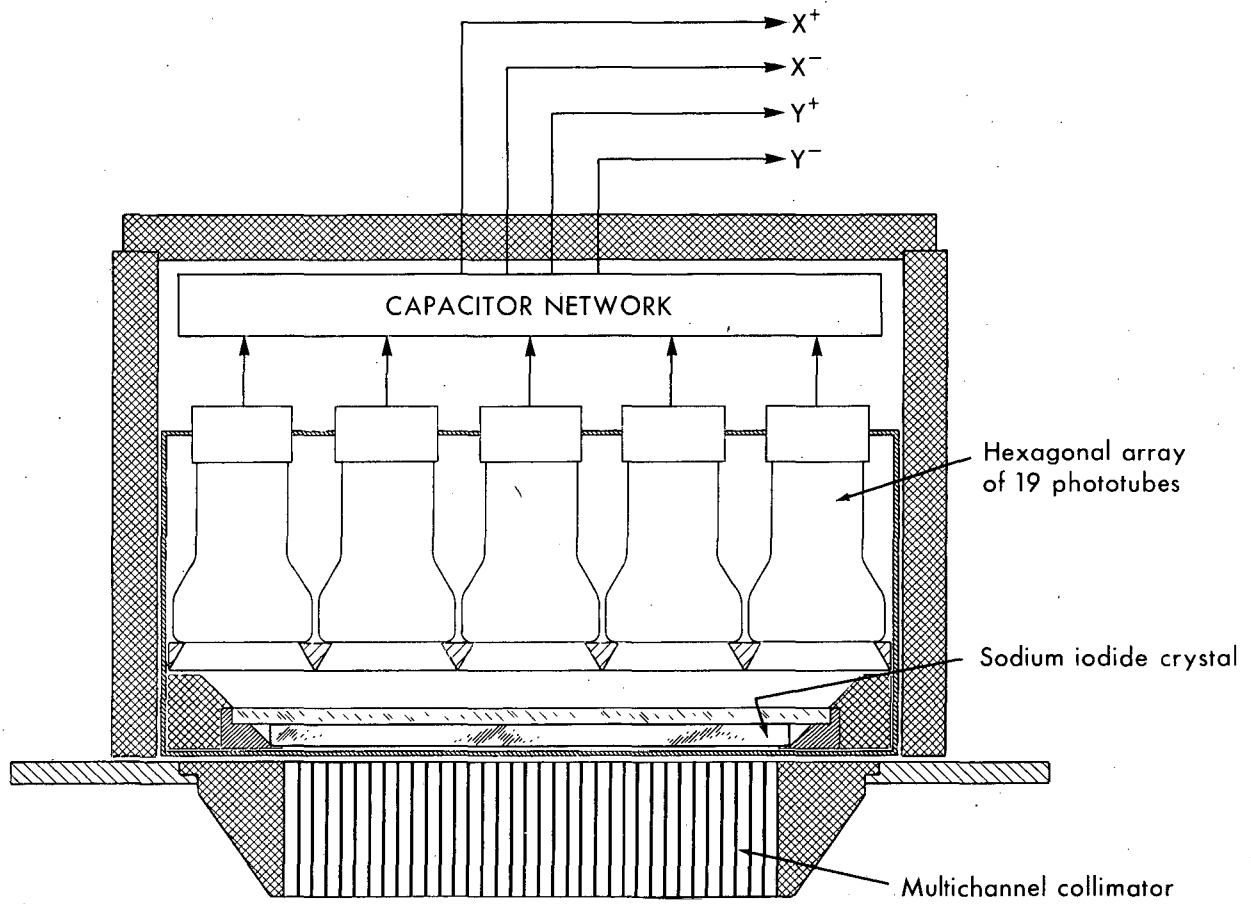
- Fig. 1. Scintillation camera image detector with multichannel collimator.
- Fig. 2. Section view of parallel-channel collimator showing gamma-ray pathways and irradiated areas of scintillator.
- Fig. 3. Path of minimum attenuation for gamma rays penetrating collimator septa.
- Fig. 4. Enlarged section of image showing 5 point sources of Ba^{133} resolved by the "A" multichannel collimator. Sources are 1 inch from collimator and on the axes of holes shown in diagram.
- Fig. 5. Pictures of brain lesion taken with Hg^{203} Neohydrin showing (A) left lateral view, (B) frontal view, and (C) back view. The six images of each view were obtained simultaneously by a 5-minute exposure. A prominent lesion and two marker sources are shown in each view, as well as an outline of the head due to body background.
- Fig. 6. (A) Picture of adult liver taken after administration of 250 microcuries of I^{131} rose bengal. Exposure time was 10 minutes.
- (B) A 5-minute exposure of adult liver after administration of 200 microcuries of rose bengal. A defect is visible at upper left.
- Fig. 7. (A and B) Views of human thyroid and thyroid area. This type of survey shows any abnormal uptake of radioiodine in a 9 - 10 inch diameter area. The three images with graded density were obtained in a single 5-minute exposure.
- (C) Ten-minute exposure of thyroid phantom containing 5.9 microcuries of mock I^{131} .

Fig. 8. (A and B) Pictures of normal human kidneys taken with Hg^{203} Neohydrin. Exposure times were 10 and 2 minutes.

(C) Renal pelvis of diseased kidney shown in a 5-minute exposure 20 minutes after administration of 200 microcuries of I^{131} hippuran.

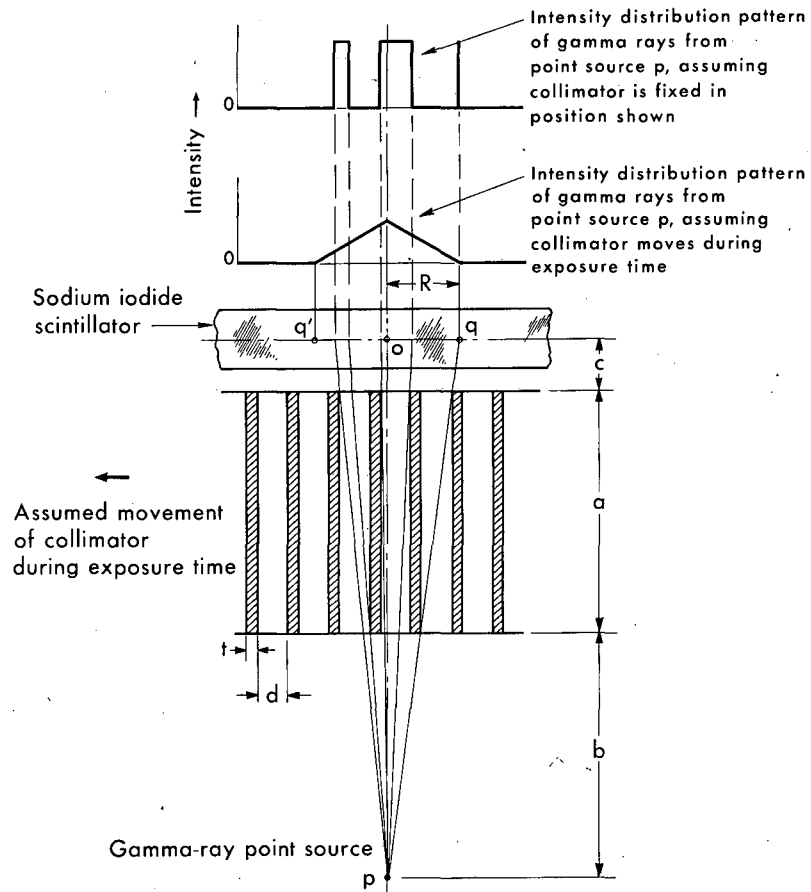
Fig. 9. (A) Time lapse sequence showing I^{131} hippuran going through human kidneys. Exposure time was 30 seconds per picture.

(B) Time lapse sequence showing excretion of I^{131} rose bengal from liver of girl. Exposure time was 2 minutes per picture.



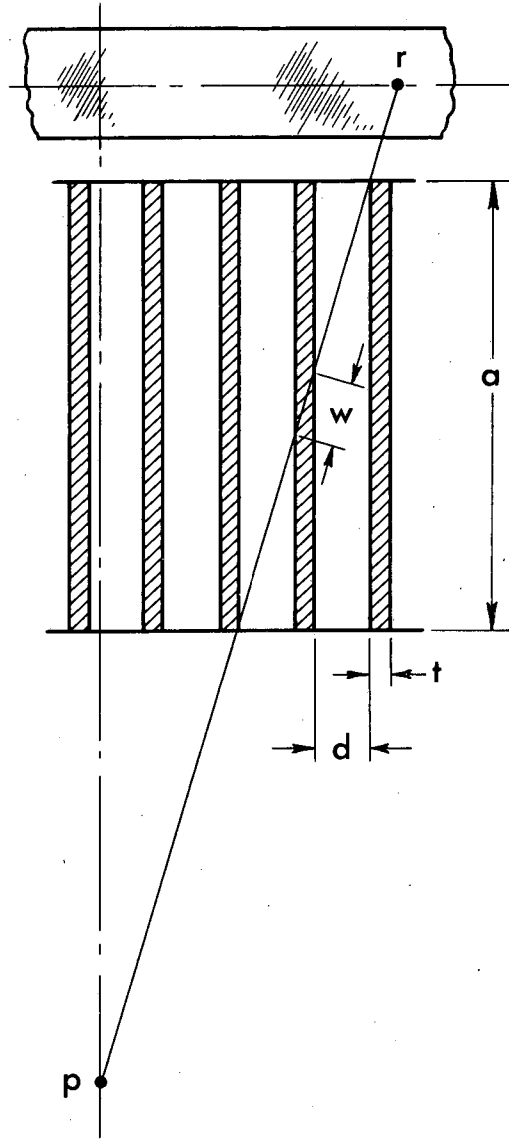
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Fig. 1



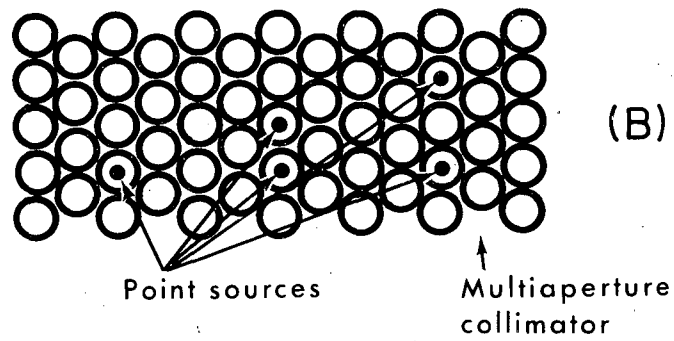
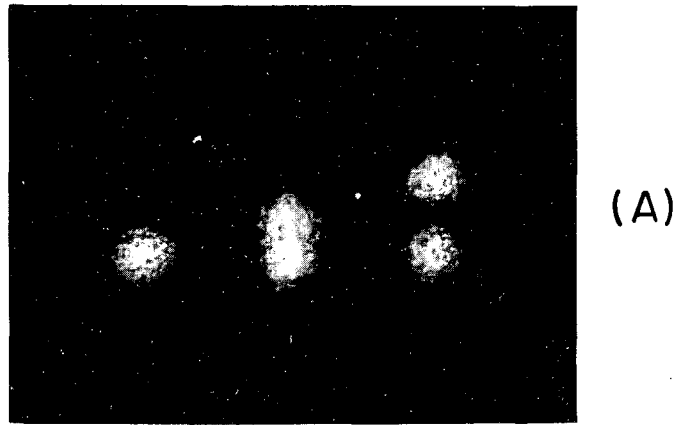
MU-31627

Fig. 2



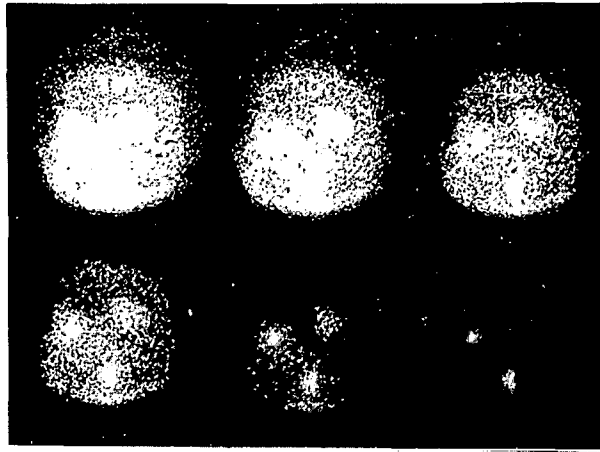
MU-31621

Fig. 3

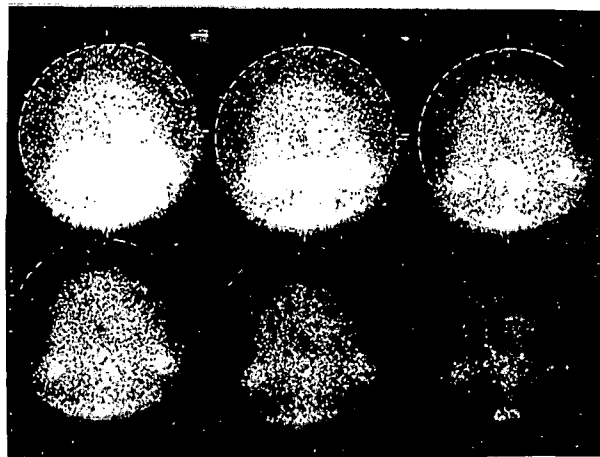


ZN-4217

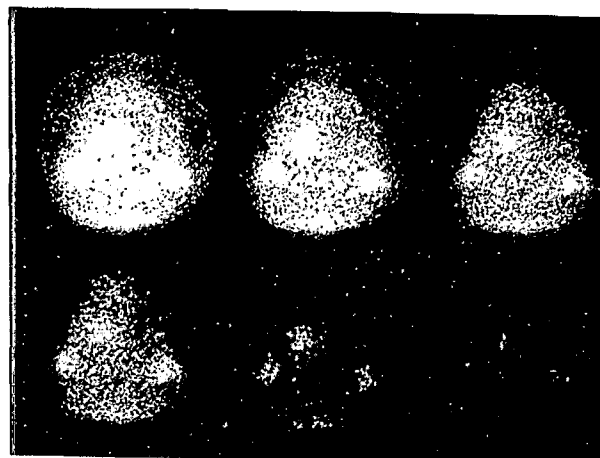
Fig. 4



(A)



(B)



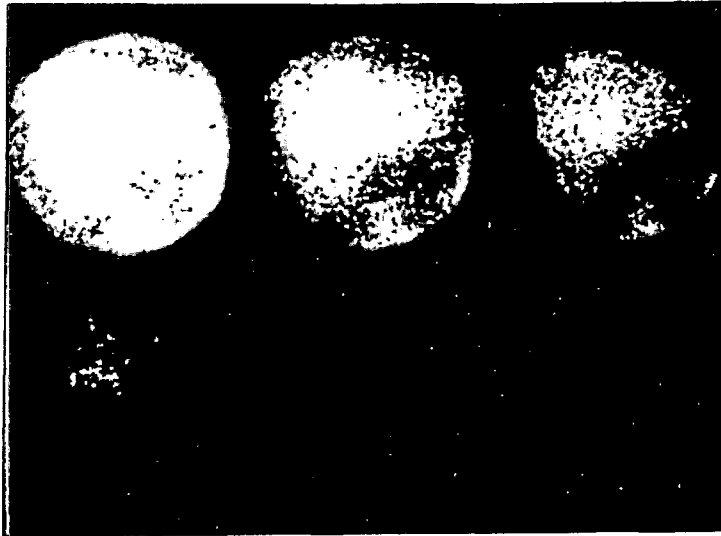
(C)

ZN-4203

Fig. 5



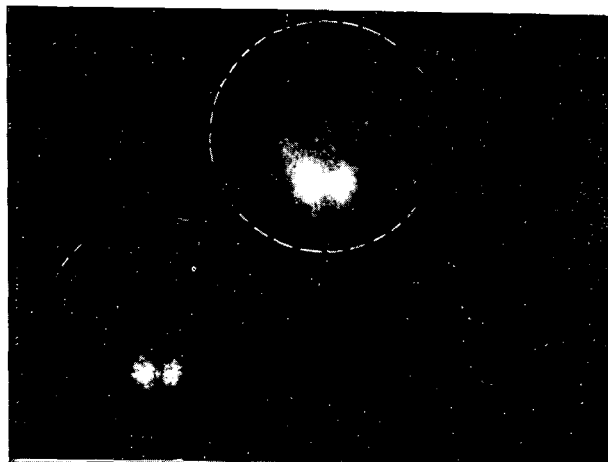
(A)



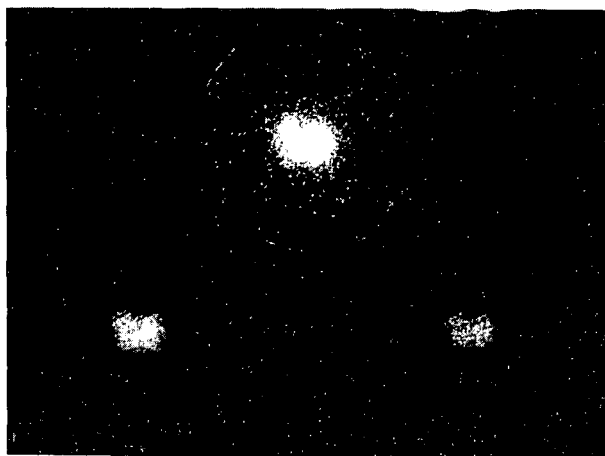
(B)

ZN-4201

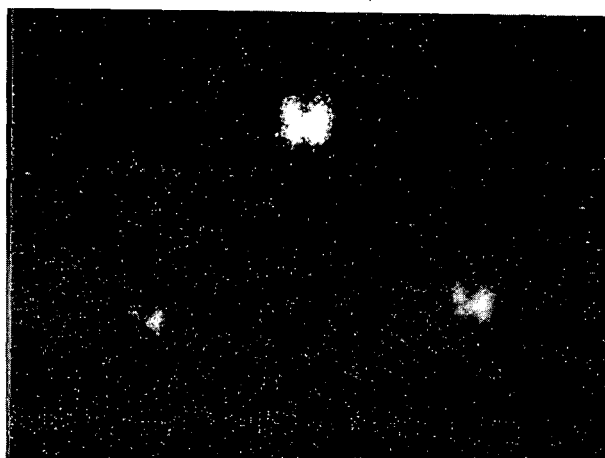
Fig. 6



(A)



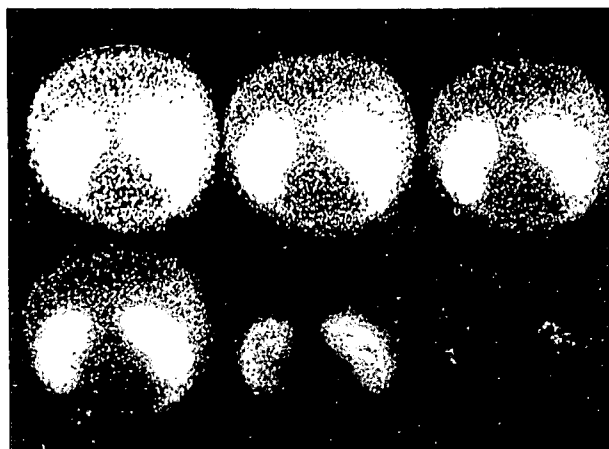
(B)



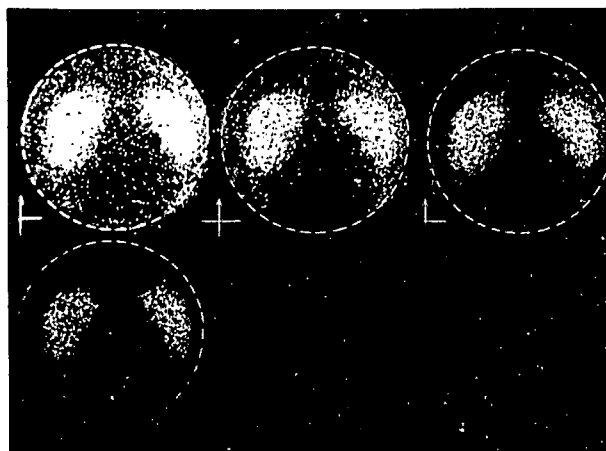
(C)

ZN-4202

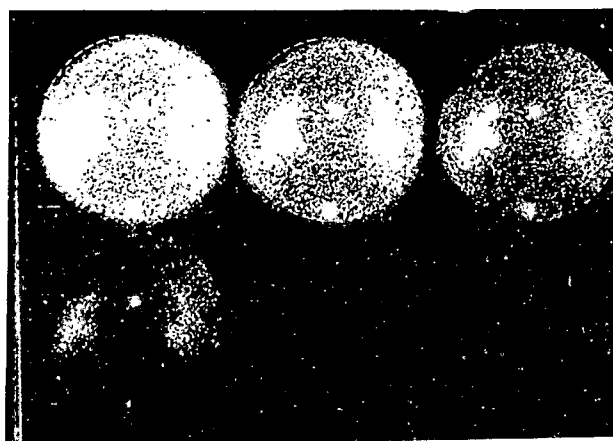
Fig. 7



(A)



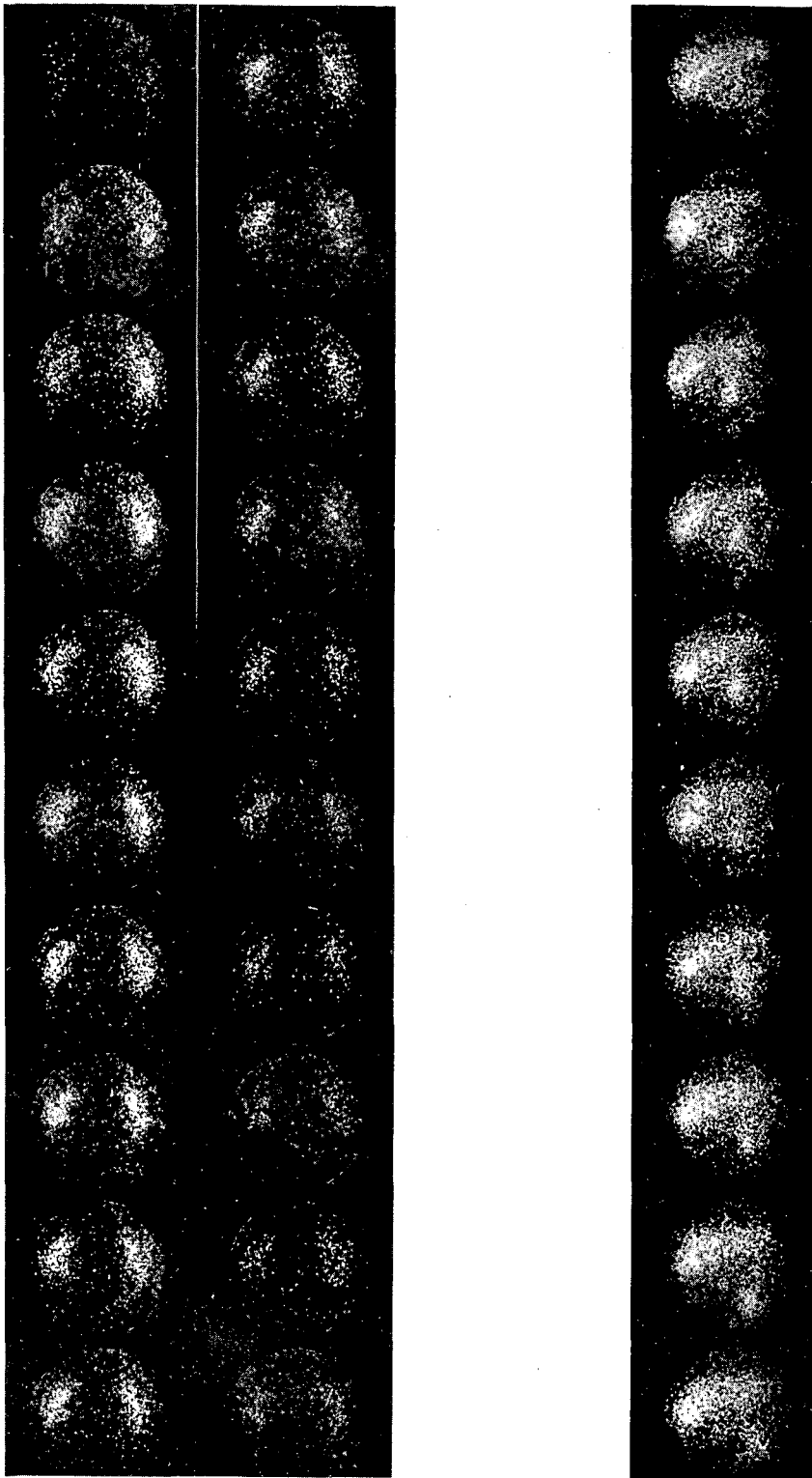
(B)



(C)

ZN-4200

Fig. 8



ZN-4204

Fig. 9

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