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A Millimeter-scale Single Charged Particle Dosimeter for Cancer Radiotherapy

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Abstract

This paper presents a millimeter-scale CMOS 64×64 single charged particle radiation detector system for external beam cancer radiotherapy. A $1\times1 \mu m^2$ diode measures energy deposition by a single charged particle in the depletion region, and the array design provides a large detection area of $512\times512 \mu m^2$. Instead of sensing the voltage drop caused by radiation, the proposed system measures the pulse width, i.e., the time it takes for the voltage to return to its baseline. This obviates the need for using power-hungry and large analog-to-digital converters. A prototype ASIC is fabricated in TSMC 65 nm LP CMOS process and consumes the average static power of 0.535 mW under 1.2 V analog and digital power supply. The functionality of the whole system is successfully verified in a clinical 67.5 MeV proton beam setting. To our' knowledge, this is the first work to demonstrate single charged particle detection for implantable *in-vivo* dosimetry.

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Keywords

In-vivo dosimetry; proton beam therapy; single particle detection; pulse width sensing; CMOS dosimeter

I. INTRODUCTION

MORE than half of cancer patients are treated with ionizing radiation, where the fundamental goal is to deposit sufficient energy (dose) to destroy the tumor cells and stop their proliferation. A key challenge in radiotherapy is to target the tumor while imparting minimal damage to surrounding normal tissues. Commonly-used *external beam radiotherapy* (EBRT) employs x-ray photons to deliver a radiation dose to the tumor. This well-established method encounters several difficulties: 1) X-rays pass through the whole body, leaving unwanted dose in healthy tissues. This can be critical in pediatric cancer, for example, where secondary malignancy results from peripheral dose; 2) The dose from x-rays is highest near the surface, dropping a few percent per centimeter with depth.

Due to these issues, *charged particle radiotherapy* has advantages over x-rays. Unlike photons, charged particles (such as protons and carbon ions) deposit the highest dose in a specific location at the end of their range (the Bragg peak), theoretically allowing dose to be delivered with higher precision and with less peripheral dose than with x-rays (See Fig. 1(a)).

Despite the advantages of charged particle therapy, a current limitation is knowing the exact location of the Bragg peak (range uncertainty) which is caused by a number of factors. First, patient movement such as respiratory motion shifts the Bragg peak. Second, charged particle interactions occurring within the body depend heavily on tissue atomic properties, which are difficult to determine accurately [1]. Lastly, day-to-day anatomical variations may make predictions inaccurate.

The current clinical practice is to mitigate the range uncertainty by using a patient-specific maps of estimated particle stopping power derived from CT image to predict the location of the Bragg peak [2]. However, due to uncertainties in the patient CT image and inaccurate conversion from the CT image to the stopping power, the typical range uncertainty is about 2.5 % of the total range. Given this, it is common in clinics to widen the Bragg peak to cover the full target volume, and then add treatment margins to ensure the target is covered with prescription dose, resulting in increased dose to normal tissue. An example of a spread-out Bragg peak (SOBP) and the additional margins added to account for this range uncertainty is illustrated in Fig. 1(a).

Real-time *in-vivo dosimetry (IVD)* ameliorates uncertainty by measuring the dose delivered in the body, potentially leading to more effective and safer closed-loop treatments (Fig. 1(b)). Clinically viable IVDs have several important constraints. They must be millimeter scale for implantation through a standard core-biopsy needle; consume very small amounts of power; have single-particle sensitivity; be capable of real-time measurement of energy deposition; and be suitable for bio-compatible chronic implantation (usually 1-8 weeks) with

appropriate medical-grade packaging. These requirements strongly drive the need for a CMOS platform capable of compact integration of low-power sensors and readout circuitry.

While existing approaches have made progress towards miniaturized IVD, no previous work has satisfied all requirements [3]–[8]. Single MOSFET dosimeters have been the most widely used, as they can be easily fabricated in a small size [3], [4]. Integrated damage by radiation in the SiO₂ layer of the MOSFET decreases the threshold voltage linearly. However, the lifetime is finite and it lacks single particle sensitivity due to the cumulative nature of the radiation induced damages. Plastic scintillator, thermo-luminescent, or radioluminescent dosimeters detect light intensity when a radiosensitive material is exposed to radiation [5], [8]. However, they measure only cumulative dose, cannot provide real-time data, and require bulky optical equipment to measure light that precludes implantation. Floating gate dosimeters measure the current change when charges are trapped in the floating gate by radiation [6], but they lack single particle sensitivity.

Most importantly, conventional dosimeters measure average dose, and ignore a critical phenomenon: for a given dose, a single high linear-energy-transfer (LET, energy deposition per unit length) particle has a significantly different biological effect on tissue than that of several low LET particles [9], [10]. The key metric to the biological effect is the energy deposition by each particle. Because the biological effect versus energy deposition is non-linear, the cumulative damage does not represent the true biological effect by radiation. For example, the normalized average number of lethal lesions in a HF19 human diploid fibroblasts cell produced by a single 4, 50, and 70 keV/ μ m LET alpha-particle is approximately 1, 34.4, and 65.6, respectively [9]. The biological effect increases more rapidly than the energy deposition. The biological effect plateaus after 100 keV/ μ m. Due to this non-linear relationship between the energy deposition and the biological effect, single particle detection will be a key feature for next-generation IVDs, enabling analysis of the true biological effect by radiation.

In this work, we solve these challenges by introducing an 64×64 pixel implantable millimeter scale single charged particle CMOS dosimeter, compatible with *in-vivo* implantation for EBRT. To the best of our' knowledge, the proposed system is the first work to enable single charged particle detection using only conventional CMOS chip fabrication process.

II. THEORY OF OPERATION

This section describes how protons interact and deposit energy in matter, and how the deposited energy relates to the biological effect. The expected signal measured by a diode is analyzed. Finally, the acquisition of a pulse width (as opposed to a voltage level measurement) is discussed.

A. Proton interaction with matter

With the clinically-relevant energy range, protons deposit energy when passing through matter by three types of interactions: 1) Coulomb interactions with atomic electrons; 2) Coulomb interactions with atomic nuclei; and 3) nuclear reactions accompanied by creation

of secondary particles (proton, neutron, electron, and gamma ray) [1]. The first type is the most dominant type of interaction, where a proton ionizes matter, transferring part of its energy to electrons that deposit their energy in proximity to the point of ionization (~ 1 mm). The second type alters the proton trajectory and contributes to proton scattering. The last type is the rarest. In the first type, LET describes the average amount of proton energy deposited per unit length, and is well-modeled by the Bethe-Bloch equation.

$$\frac{dE_{dep}}{dx} \propto \rho \frac{Z}{A} \frac{1}{\beta^2} \left[\ln \frac{2m_e c^2 \gamma^2 \beta^2}{I} - \beta^2 - \frac{\delta}{2} - \frac{C}{Z} \right],\tag{1}$$

where dE_{dep}/dx is the energy deposition per unit length, ρ is the density of the absorbing material, Z is the atomic number of the absorbing material, A is the atomic weight of the absorbing material, $\beta = v/c$ where v is the velocity of the proton and c is the speed of light, m_e is the electron mass, $\gamma = (1 - \beta^2)^{-1/2}$, I is the average ionization potential of the absorbing material, δ is the density correction term, and C is the shell correction term. Eq. 1 shows why it is challenging to predict the location of the Bragg peak, as the LET value heavily depends on the material property and proton energy [1].

Dose (Gy = J/kg) is widely used in clinical applications to quantify the radiation effect on tissue:

$$Dose = \sum_{i=1}^{N} \frac{E_{dep,i}}{m} = \frac{\mathbb{E}[E_{dep}] \times N}{m},$$
(2)

where N is the number of protons, $E_{dep,i}$ is the energy deposition by each proton in the material, and *m* is the mass of material where the energy deposition occurred [11]. Dose is the sum of individual energy depositions per unit mass. However, the actual biological effect (e.g., the number of double strand breaks in the DNA or cell mortality rate) for particles with higher LET has a highly non-linear relationship with the $E_{dep,i}$ [9], [11]. This means that dose alone is an insufficient measure to evaluate the true effect on tissue. We also need the LET; that is, the single particle detection sensitivity.

B. Proton detection using a diode

When a proton interacts with a semiconductor diode, some of the energy deposited in the depletion region of the diode generates electron-hole pairs (EHPs). The average number of EHPs generated in a silicon diode is

$$EHP = \frac{LET \times t_{dep} \times qu}{\sin \theta_p \times 1.12 \text{ eV}},$$
(3)

where LET is dE_{dep}/dx , t_{dep} is the thickness of the depletion region, θ_p is the incident angle, and *qu* is the quenching effect that describes approximately 1/3 of the deposited energy is used to generate EHPs [12], [13]. The other 2/3 is either dissipated by heat or via fast recombination of EHPs. The value 1.12 eV represents the bandgap energy of the silicon. LET is a highly non-linear function of proton energy. Note that because the proton beam

angle from the source is fixed and we know the sensor orientation, mean θ_p can be easily identified.

Fig. 2 depicts the diode sensing mechanism. When the diode is reversely biased by a current source, the generated electrons move to the parasitic capacitance and create a voltage drop of

$$V_{drop} = \frac{q \times EHP}{C_{par}},\tag{4}$$

where q is the charge of an electron and C_{par} is the parasitic capacitance. Therefore, to achieve single particle sensitivity, a nearly minimum size diode $(1 \ \mu m \times 1 \ \mu m)$ is used to reduce C_{par} because, for a single particle traversing the diode, the average number of EHPs is determined mostly by fabrication parameters and proton energy. In order to have wide detection area, we designed diodes into arrays. When designing an array, we want to maximize the fill factor (defined as the ratio of diode area to the area of the whole circuitry) to capture as many incident particles as possible. Fig. 3(a) depicts the average voltage drop by a single proton assuming C_{par} of 2.5 fF, t_{dep} of 0.1 μ m, and a quenching effect of 1/3. The National Institute of Science and Technology (NIST) pstar table is used to calculate the LET [27]. The voltage signal produced during a collision ranges from 4 mV to 78 mV at 1~67 MeV proton energy range. The voltage drop is a nearly instantaneous event.

Sensing the instantaneous voltage drop generated during a collision requires high speed analog-to-digital converters (ADCs) which are power-hungry and occupy a large area (especially for an array). For example, if the time constant of the diode sensing node is 350 μ s, the sampling rate of per-pixel ADC needs to be greater than 100 kHz to sample the V_{drop} with an error less than 1.5 %. Assuming 64 per-row ADCs, 6 bit resolution, and the figureof-merit of 1.3 fJ/step [14], 64 6.4 MS/s ADCs will consume 34 μ W and the total ADC area will be large. In addition, the system has to output 7.4 Gbps of data, or additional circuitry is required for post-processing, which is impractical in implantable applications. In contrast, measuring the time it takes for the generated voltage to return to its baseline is relatively straightforward. We call this delay the pulse width (PW) (See Fig. 3(b)). The PW can be expressed as

$$PW = \tau \ln\left(\frac{V_{drop}}{V_{th}}\right) = \tau \ln\left(\frac{q \times qu \times E_{dep}}{1.12 \times V_{th} \times C_{par}}\right),$$

where τ is the time constant at the diode sensing node and V_{th} is the threshold voltage of detection. Even though the sensor output has a logarithmic relationship with E_{dep} , this can be pre-calibrated before use.

Including electronic noise at the diode sensing node, v_n , PW can be expressed as

$$PW = \tau \ln\left(\frac{V_{drop}}{V_{th} + v_n}\right).$$
(5)

Given this, we can define pulse-width to noise ratio (PNR) as

$$PNR = \frac{\sqrt{\mathbb{E}[PW^2]}}{\sigma_{PW}} > \frac{\ln(V_{drop} / V_{th})}{\sigma_{v_n} / V_{th}},$$
(6)

where the delta method is used to find the upper bound for the standard deviation of a logarithmic function. Fig. 4 shows the Monte Carlo simulated mean PW versus σ_{PW} and PNR. Because PNR is proportional to the mean PW, V_{drop} versus PNR is logarithmic. We can also define signal to noise ratio (SNR) as $V_{drop}/\sigma_{v_{II}}$. Thus, the ratio of PNR to SNR is

$$\frac{\text{PNR}}{\text{SNR}} > \frac{V_{th} \ln(V_{drop} / V_{th})}{V_{drop}},$$
(7)

which is always less than 1. This means that the PW sensing methodology loses resolution because of the logarithmic transformation of the signal. However, SNR in this analysis assumes perfect sampling of the critical time points of V_{drop} (e.g. the time points corresponding to proton hits) which is impossible in practical situations when using an analog-to-digital converter. The actual PNR loss is subsequently expected to be less than that for the ideal situation.

III. SYSTEM DESIGN

The design consists of a 64×64 pixel array, a main digital block, a SRAM control block, and a frequency locked loop (FLL). The system must feature low power consumption for future wireless applications, millimeter-scale size, enough detection area with sufficient fill-factor, and robustness to process mismatches.

The following subsections discuss the analog pixel design, digital system design, FLL, and calibration steps.

A. Analog Pixel Design

Fig. 5 illustrates the pixel design. To reject common mode noise, a differential sensing scheme is used. Two diodes, diode P and N, are grouped into one pixel unit. A P-type PN diode is used for maximizing the depletion region thickness. A nearly minimum size PMOS current source supplies current to the diode. The bias voltage of the current source (V_{bdio}) can be set to vary the depletion region thickness, time constant of the sensing node, and the DC voltage accordingly based on target beam settings. The trade-off is between the required bandwidth and the measurable proton flux range. In our target beam setting, the time constant at the sensing node is designed to be approximately 350 μ s.

The differential amplifier should feature low input capacitance, high gain, low noise, and low DC output voltage mismatch. Input transistors are critical, as there is a trade-off between the input capacitance and the DC output voltage mismatch. To balance these trade-offs, low V_{th} (LVT) NMOS devices with 600 nm/600 nm are used as the input transistors. The differential amplifier occupies a 4 μ m × 5.6 μ m area.

A high-pass filter with a 30 fF MOMCAP is used to reject the DC output voltage variance of the differential amplifier, and to set the DC voltage to a common voltage uniformly across

all pixels by off-chip V_{DCHPF} . To provide low f_{3dB} , 9 serial pseudo-resistors are used, as the f_{3dB} accuracy is not critical. The f_{3dB} needs to be lower than 10 Hz to ensure accurate measurement of the PW. The high-pass filter is designed to have f_{3dB} of 4.8 Hz.

The level shifters (*LS*) shift the DC voltage downward (*LS_p*) or upward (*LS_p*) to clip signals coming from the other diode. This enables passing signals from the corresponding diode only. The V_{bLS} is an essential variable that controls the trade-off between sensitivity of signal detection (V_{th}) and the pixel failure rate (i.e., the ratio between the number of failed pixels and the total number of pixels). For instance, lowering V_{bLSp} increases the output DC voltage of LS_p , leading to the triggering of the following inverter by a smaller signal. However, it also increases the chance that the noise can trigger the inverter.

Diode transient pulse is converted to a digital pulse through inverters. The output digital pulses, V_{op} and V_{on} , turn on PMOS switches to create the inverted signal on Data Line (DL), which is shared by pixels on the same row.

Due to process, voltage, and temperature (PVT) variations, there is a chance that some pixels are constitutively active and output a false-positive signal even in the absence of radiation events. Because the DL is shared by pixels on the same row, these false positives would hold the DL high and block signals coming from other pixels. Therefore, an in-pixel standard 1-bit 6T SRAM block is implemented to disable any false-positive pixel. Disabling these problematic pixels is called calibration and will be explained in Section III-D.

The overall pixel size is 8 μ m × 8 μ m, leading to a fill-factor of 1/64. This means that there exists a high chance of protons striking the transistors. Assuming the PN junctions of the transistors have a similar depletion depth to that of the diode, this will create a voltage drop at the node with amplitude

$$V_{drop} \le 250 \text{ mV} \times \frac{C_{par, \, diode}}{C_{par, \, circuit}},$$
(8)

where $C_{par,diode}$ and $C_{par,circuit}$ are the parasitic capacitances at the diode node and the node of the proton hit, respectively. To address this issue, we designed the pixel such that either: 1) the time constant of the node is less than the LSB of the PW sampling, which is 6 μ s; or 2) $C_{par,circuit}$ is much greater than $C_{par,diode}$. For instance, the static DC current of the differential amplifier is 120 nA, and thus the worst case scenario will create a signal

$$PW = \frac{V_{drop}}{dV/dt} = \frac{250 \text{ mV} \times C_{diode}}{60 \text{ nA}} \approx 10 \text{ ns}.$$
(9)

Also, the parasitic capacitance at the HPF is more than 10 times larger than that at the diode node so that the proton hit at the HPF cannot trigger the inverter.

Fig. 6 illustrates the timing diagram. A proton hit at the diode creates a voltage pulse at one of the output nodes: V_{op} or V_{on} . Then, the same digital pulse but with opposite polarity is created on the DL. The PW is then quantized by a 10-bit digital counter with LSB of 6 μ s. Sweeping signals (SW_p and SW_n) are 64 non-overlapping periodic 500 ns signals generated from the main digital block. The sweeping signals are then transferred to the Address Lines

(ALs), which are also shared by the pixels on the same row, when the corresponding pixel has a proton hit. Therefore, the main digital block can identify the column address of the proton hit by comparing the sweeping pulse and the AL signal. The sweeping lines are designed so that the overall delay it takes for the signal to travel from the main digital to the pixel and back does not exceed 500 ns.

Note that this design methodology cannot distinguish multiple proton hits at different pixels on the same row. This event creates the DL pulse that is the logical OR operation of two voltage output pulses, making the DL pulse inseparable. However, such an event can be easily identified because more than two sweeping pulses will be transferred onto the AL during a single DL signal (See Violation 1 in Fig. 6). We can simply discard these events because: 1) this is a rare event; and 2) discarding them will not change the overall statistics because this is a purely stochastic event. Also, the DL PW must be greater than 500 ns \times 64 $= 32 \,\mu s$ to guarantee that the column address is accurately identified. If not, there exists a chance that the column address is missing (See Violation 2 in Fig. 6). Two types of events, the multiple hit event and the address missing event, are called violation events, and we discard them. The multiple hit violations can be reduced by decreasing the time constant of the diode sensing node. However, this increases the overall power consumption because the 10-bit counter must count faster. We can also mitigate the address missing violations by sweeping the columns faster. Nevertheless, this might result in addressing the wrong columns, as the overall delay of the sweeping signal can exceed its pulse width. Note that the proton hit count can be retrieved even when violation events occur.

A key advantage of our method is that the pixels consume only static power in the absence of radiation. Unlike traditional imaging applications where every pixel captures the signal periodically, only the struck pixel captures the signal and consumes dynamic power. This is made possible by the PW sensing strategy, and would not be true of a voltage sensing scheme.

B. Digital System Design

Fig. 7 illustrates the overall system. The main digital block features the acquisition of the DL and AL signals, collecting them and buffering, and configuring internal parameters. The SRAM control block manages the enabling and disabling of pixels, as well as the reading of current SRAM values.

The DL and AL lines on each row have pull-down and pull-up transistors, respectively. The 10-bit counter starts counting at the rising edge of the DL signal. The reason why 10-bit resolution is needed is that signals with small PW need to be captured, as it would help more accurately measure the statistics. During counting, the addressing block stores the current SW_{idx} value when the AL is high. The counting is finished at the falling edge; and the 10-bit counter value, 6-bit row address, 6-bit column address, and 2-bit status (00 : valid, 01: multiple proton hit, 10 : column address missing) are transferred to the first-in-first-out (FIFO) block.

When multiple rows have data, the priority encoder selects a row that has data and the highest priority. The rows range from 0 to 63, and a lower number translates to higher

priority. This prevents data congestion at the interface between the 64 row blocks and the FIFO. The FIFO block has a width of 24 bits and depth of 16. Finally, a parallel-in serial-out (PISO) block receives the data from the FIFO and outputs each data to off-chip.

The maximum latency happens when all rows have data ready and the FIFO is full. Therefore, the best and worst case latency can be expressed as

> $t_{latency, min} \approx PW + t_{cnt} + t_{FIFO} + 48t_{PISO}$ $t_{latency, max} \approx PW + t_{cnt} + t_{FIFO} + 48(16 + 64)t_{PISO},$

where PW is the pulse width of the data and t_{cnb} , t_{FIFO} , and t_{PISO} are the clock periods of the counter, FIFO, and PISO, respectively. In default settings, $t_{latency}$ ranges from PW+ 36 μ s to PW+ 1932 μ s. Also, since the PISO block is the bottleneck in transferring data, the maximum proton flux that the digital block can handle is about 41,000 particles per second.

To give more flexibility of operation, internal parameters can be configured through the serial-in parallel-out (SIPO) from off-chip. t_{mst} , t_{addr} and t_{SRAM} , which are the periods of the main clock, the addressing clock, and SRAM clock, respectively, as well as t_{cnt} and t_{PISO} can be configured as shown in Table I.

C. FLL

All internal digital clocks are generated from an on-chip FLL. The FLL obviates the need for external bulky crystal oscillators [19]. A 10kHz beacon signal is sent from off-chip, and the FLL counts the digitally-controlled oscillator (DCO) clock during each period of the beacon signal. DCO frequency is adjusted through negative feedback based on the difference between the desired number of clocks in one period and the actual counter value. This enables the generation of a 1~10 MHz main digital clock with approximately 280 kHz frequency resolution.

D. Calibration

The aforementioned constitutively active pixels are disabled before radiation through calibration steps. Each DL can be monitored off-chip through a 64 to 1 multiplexer. The calibration steps are: 1) disable every pixel through the in-pixel SRAM; 2) enable one pixel and monitor the corresponding DL signal for 50 ms; 3) disable the pixel if the DL signal is noisy or high; and 4) repeat this process for the remaining pixels. This calibration process is carried out by an external FPGA, and takes approximately 5 minutes.

By using this technique, we can indirectly measure the statistics of mismatch among pixels. Fig. 8(a) depicts the function $f_p(V_{bLSp})$ and $f_n(V_{bLSn})$. The percentage of enabled pixels after the calibration, *EN*, will be varied based on $V_{bLSp,n}$ value. EN is essentially the percentage of pixels whose $V_{op,n}$ is VDD, which can be described as

$$EN := \sum_{i=1}^{N} \mathbb{1}\{V_{op, n} = VDD\} / N = \mathbb{E}[\mathbb{1}\{V_{op, n} = VDD\}],$$

where N is the total number of pixels and $V_{op,n}$ means V_{op} or V_{on} . Fig. 8(b) shows the measured EN after the calibration when V_{bLSp} and V_{bLSn} are swept from 900 mV to 1100 mV. The slope from 975 mV to 1025 mV represents the mismatch of the function $V_{op,n} = f_{p,n}(V_{bLSp,n})$ among the pixels. For instance, if the pixels were identical without any mismatch, the slope would be infinite because every pixel becomes enabled at a certain $V_{bLSp,n}$ value; that is, the graph shows the measured cumulative distribution function of $f_{p,n}$. First-order Gaussian fitting of the derivatives of the graphs gives the means of 1000 mV and 995 mV and the standard deviations of 19.33 mV and 21.85 mV for $f_p(V_{bLSp})$ and $f_n(V_{bLSp})$, respectively.

IV. MEASUREMENT RESULTS

A prototype single charged particle dosimeter system was fabricated in TSMC 65 nm Lowpower CMOS technology. The ASIC is 940 μ m×960 μ m and its die photo is shown in Fig. 9. The detection area is 512 μ m×512 μ m with fill factor of 1/64.

This section describes the measurement setups and results. To analyze the electrical noise and pixel-to-pixel variations, a separate 16×16 testing chip was measured. The whole system was verified under a 67.5 MeV proton beam generated by a 76-inch cyclotron. The measurement results were compared to those of the Monte Carlo simulation results.

A. Electrical Measurement Results

Fig. 10 depicts the electrical measurement setup. The diode node does not have a monitoring node in current design, as placing a measurement node on the main chip would add significant parasitic capacitance and reduce the gain. Therefore, a separate 16×16 pixel testing chip with identical pixel design but with an electrical input (M1) to mimic the radiation was used to characterize noise and pixel-to-pixel variations. The M1 is a nearly minimum size transistor, 200 nm/60 nm. The function generator generates 5,000 identical pulses with 1 μ s pulse width. These pulses cause an instantaneous voltage drop at the diode node; the rest of the pixel circuitry outputs digital pulses on the DL. The mean and standard deviation of the PW were then measured. These measurements were repeated for various amplitude values of the input pulses.

Fig. 11(a) shows the single pixel measurement results. The PW variation increases with the mean PW, and the standard deviation of the PW signals is less than 150 μ s throughout the whole operating range (0-6 ms). PNR is 27.7 dB at 3 ms PW.

To measure pixel-to-pixel variation, 5,000 identical pulses were presented to pixels and mean PWs were measured. Fig. 11(b) is the normalized histogram of mean PWs of the 256 pixels. This histogram is essentially the input-to-output PW gain mismatch among the pixels. The variation is mainly due to the mismatch in the differential amplifier and the LS. Note that because the input transistor (M1) mismatch, which is expected to be significant due to small size, is embedded in the measurement result, the actual pixel-to-pixel variation would be smaller. In applications where high-spatial resolution dose map is required, this variation can be pre-calibrated before the treatment by measuring each pixel's responses at different proton energies.

B. Proton Simulation and Measurement Results

The prototype ASIC was tested at the proton beam facility in Crocker Nuclear Laboratory (CNL) at University of California, Davis, which has treated more than 1,700 ocular patients with malignant and benign ocular tumors since 1994 [16]–[18]. To assess sensor performance under clinically relevant conditions, the experiment was conducted in the treating room using similar beam settings that are used for patients.

Fig. 12 depicts a simplified diagram of the proton measurement setup in an eye-treatment room. A 67.5 MeV with 1.3 MeV full width half maximum (FWHM) proton beam is generated by the 76-inch cyclotron. The beam enters the treatment room and passes through: ionization chamber 1 which monitors the dose; a thickness adjustable water chamber that attenuates the proton beam energy; ionization chamber 2; a patient shield; and lastly a collimator. The ASIC was placed at the position of the patient's eye during treatment (the isocenter) and the data was collected via an FPGA. The beam energy at the patient was controlled by the water chamber. Due to the nature of the energy loss mechanism of the charged particle (Eq. 1), the energy deposition by protons has an inverse relationship with the proton energy above ~0.1 MeV, thus EHP increases with increasing water thickness. Also, as the water thickness increases, the beam scatters more and thus fewer protons reach the detector. This leads to a smaller proton flux, which is the number of protons in unit area per second, at the detector. These relationships are summarized in Table II.

Fig. 13 shows measured proton flux and violation rate at different proton beam current settings. The raw beam current is proportional to the actual proton flux. The measured flux increases linearly from 0.1 nA to 3 nA, and starts to saturate after 3 nA. Even though the clinical range at CNL is from 3 nA to 18 nA, the remaining inviolate data provides enough data to extract meaningful statistics of energy deposition. We can also decrease the time constant at the diode sensing node to reduce the chance of having violations.

Normalized PW histograms measured for 80 seconds of the beam time at different water thicknesses are shown in Fig. 14. The 10-bit counter quantized the PW of the DL signals from 0-6138 μ s with 6 μ s resolution. Any DL signal whose PW is more than 6138 μ s is considered to be saturated. The total proton count decreases as the water thickness increases, mainly due to the proton scattering in the water chamber. As expected, the mean PW, which indirectly measures the mean energy deposition in the depletion region, increases as the water becomes thicker.

The histograms are rightward-skewed and become wider as the water thickness increases. This is mainly due to the Landau effect [20], which is the fluctuation in energy loss by ionization of fast charged particles in a thin layer of matter. This is essentially what the sensor measures: energy loss by ionization (generation of EHPs) of a charged particle (proton) in a thin layer of matter (depletion region).

At d = 0 mm, the measured standard deviation is $502 \ \mu s$. This consists of the Landau effect, the energy distribution of the incident proton beam, the electrical noise, the pixel-to-pixel variation, and the quantization noise. From the electrical measurement result shown in Fig. 11(a), the electrical noise contributes less than 9 % to the total uncertainty.

To verify the proton measurement data, the Tool for Particle Simulation (TOPAS) was used [21]–[23]. TOPAS wraps and extends the Geometry and Tracking 4 (GEANT4) Monte Carlo particle simulator. GEANT4 is an industry gold-standard for analyzing the behavior of atomic particles [24]–[26]. Fig. 15 shows the measured total number of protons, mean PW, and summation of PW over a 80-second window. The TOPAS simulated total number of protons, mean energy deposition (average energy deposited by each proton), and total energy deposition for all protons, assuming a depletion region thickness of 0.1 μ m, is also shown for comparison. The trends match well with each other, and we can plot the measured mean PW (black graph in Fig. 15(b)) in the *x*-axis and the TOPAS simulated mean energy deposition (red graph in Fig. 15(b)) in the *y*-axis to show the energy deposition versus PW relationship (See Fig. 16). As expected from Eq. 5, these have a logarithmic relationship. The time constant at the diode sensing node is estimated to be 363 μ s from a curve fit of the data.

The prototype ASIC consumes average static powers of 505 μ W, 28 μ W, and 2 μ W for the analog pixel array, digital system, and FLL, respectively. A comparison table with state-of-the-art dosimeters are summarized in Table 3. This work has the second largest sensing area of 0.512×0.512 mm², the lowest power consumption among active sensors, and the capability of detecting radiation in real time. Most importantly, this work is the first work that can detect energy deposition by single charged particles with a form-factor and the power consumption compatible with wireless *in-vivo* dosimeter for cancer therapy. This work enables not only the detection of the Bragg peak, but an analysis of the radiation dose's true biological effect.

V. CONCLUSION

A new CMOS diode based 64×64 single charged particle radiation detector is proposed and verified using a clinical proton beam. The design incorporates an analog pixel array with nearly minimum sized diodes, a digital system, SRAM control block, and FLL. Theoretical analysis of measuring charged particles using a diode is presented. The prototype is about 1×1 mm² with a detection area of 0.512×0.512 mm². The proton measurement results are compared with detailed simulation results. We envision that the proposed system can be used for various cancer therapies, including targeted radionuclide therapy or hadron beam therapy.

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Biographies



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Eric B. Norman received an A.B. degree in physics from Cornell Univ., Ithaca, NY, USA in 1972. He completed his PhD degree in nuclear astrophysics at the Univ. of Chicago, Chicago, IL, USA in 1978. From 1978 until 1984 he conducted research in nuclear physics at the Univ. of Washington. He then moved to California, where he spent 20 years at Lawrence Berkeley National Lab., 4 years at Lawrence Livermore National Lab., and 6 years at the Univ. of California, Berkeley, CA, USA. He is currently a professor in the Graduate School at UC Berkeley. He is a Fellow of both the American Physical Society and the American Association for the Advancement of Science. He is a winner of the DOE Outstanding Mentor Award and a co-recipient of the 2016 Breakthrough Prize in physics.

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Inder K. Daftari received M.S degree in Physics from Roorkee University, Roorkee, India in 1969 and Ph.D degree (High Energy Physics) from Jadavpur University, Calcutta, India in 1974. He joined the experimental high energy physics (Antiproton group) at Syracuse University, Syracuse, New York in 1981 to work on research projects on antiproton annihilations at Brookhaven National Laboratory, NY. After completing his training in Medical Physics at Thomas Jefferson University, Philadelphia, PA, he joined the Research Medicine at Lawrence Berkeley Laboratory in 1986 to work on heavy charged particle treatments for cancer patients. Since 1994 he is working at UCSF for treating ocular melanoma patients with proton beam therapy. His research interests include both topics in conventional radiation therapy and charged particle therapy.



Kavita K. Mishra is an internationally renowned expert radiation oncologist focused on the treatment of uveal melanomas with proton beam radiotherapy as well as plaque brachytherapy. She earned her undergraduate degree in Biology at Harvard University, followed by her medical degree at the UCSF School of Medicine. She then completed a masters degree at the Harvard School of Public Health. Dr. Mishra finished her residency in radiation oncology at the UCSF Medical Center and thereafter joined the faculty at UCSF.

Dr. Mishra specializes in the use of proton beam radiation and plaque brachytherapy to treat malignant and benign conditions of the eye. Dr. Mishra believes in a multidisciplinary approach to ocular oncology care with the aim to provide the most efficacious and individualized therapy for her patients. She is active in the national and international ocular oncology community, is the Co-Chair of PTCOG Ocular (Particle Therapy Co-Operative Group) - the largest collection of proton beam ocular radiation therapy institutions, and has multiple significant research publications and oral presentations globally in her areas of expertise.

Her current research protocols are focused on the clinical outcomes of uveal melanoma patients, particularly with respect to tumor control, preservation of the eye, and quality of life issues. She hopes to continue using a unified, team-oriented approach to maintain excellent outcomes for patients undergoing modern proton beam, plaque therapy, and external beam radiation techniques for ocular malignancies.



Bruce A. Faddegon has an MSc in physics from University of British Columbia, specializing in radiobiology, and a PhD in physics from Carleton University, Ontario, specializing in radiotherapy. He is certified in clinical medical physics as a Fellow of the Canadian College of Physicists in Medicine. His research objective is to improve the precision and effectiveness of radiotherapy through advancing radiotherapy technology, including development and application of the Monte Carlo method for improved radiation detection, planning, and treatment, with recent emphasis on biologically based planning.



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Mekhail Anwar received the B.A. degree in physics from UC Berkeley, Berkeley, CA, USA, where he graduated as the University Medalist, and the Ph.D. degree in electrical engineering and computer sciences from the Massachusetts Institute of Technology, Cambridge, MA, USA, in 2007, followed by an MD from the University of California, San Francisco, CA, USA, in 2009. After completing a Radiation Oncology residency in 2014 with UCSF, he joined the faculty with the UCSF Department of Radiation Oncology in 2014. He is board certified in Radiation Oncology and a Core Member of the UC Berkeley and UCSF Bioengineering group. He was the recipient of the Department of Defense Prostate Cancer Research Program Physician Research Award and the NIH Trailblazer Award. His research interests include developing sensors to guide cancer care using integrated-circuit based platforms.

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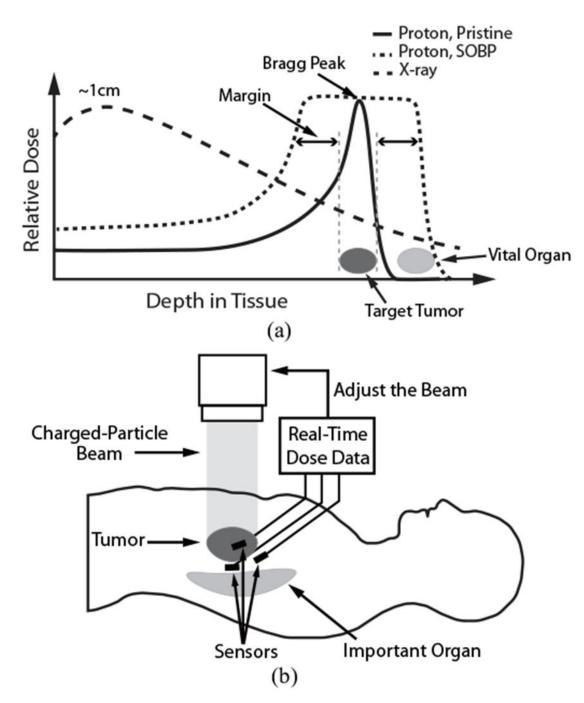


Fig. 1:

Illustrations of (a) depth-dose curve for X-ray, proton (pristine), and proton (SOBP) and (b) cancer treatment with *in-vivo* dosimetry.

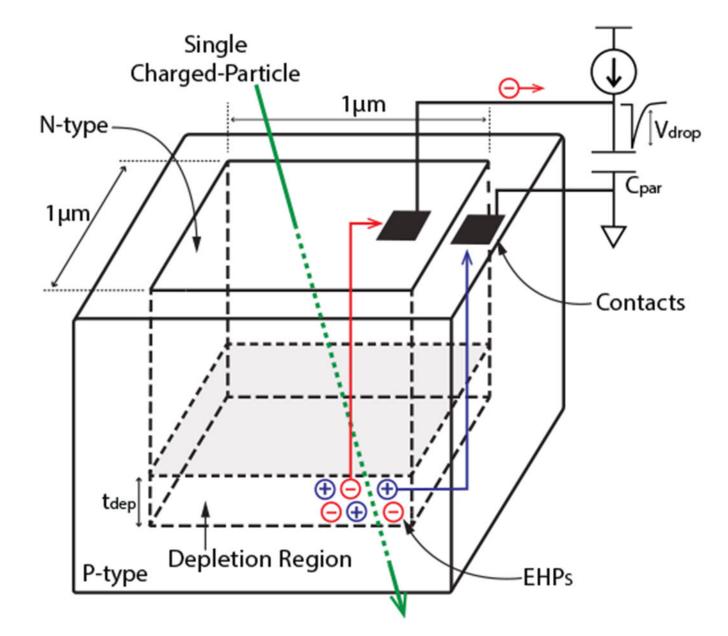


Fig. 2: Illustration of diode sensing mechanism.

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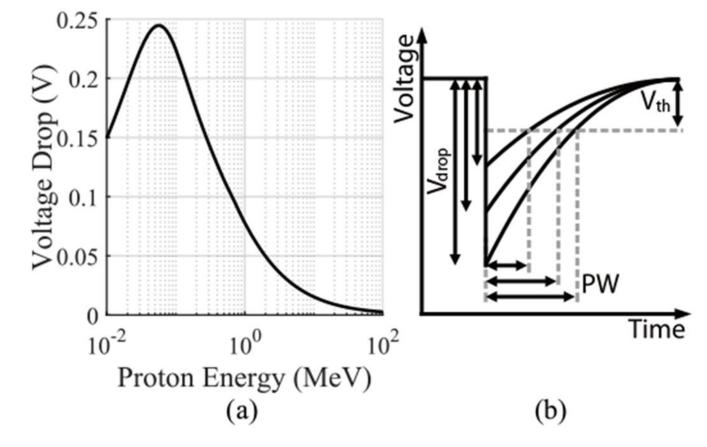
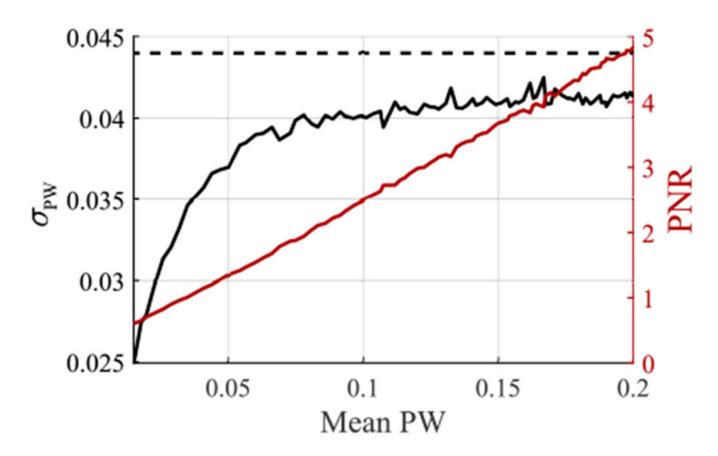
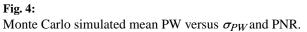
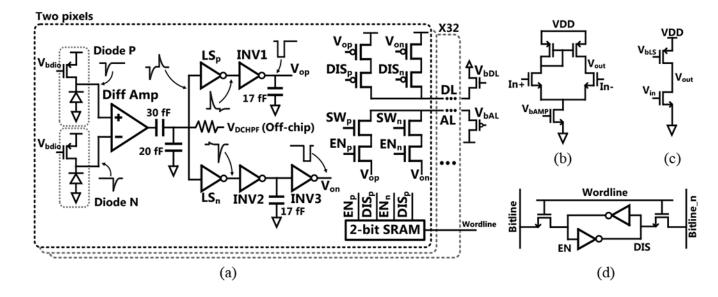


Fig. 3:

(a) Expected average voltage drop at the diode sensing node assuming 0.1 μ m depletion thickness and 2.5 fF C_{par} . The LET data are retrieved from the NIST pstar table [27]. (b) PW sensing mechanism.









Schematic diagram of (a) pixel unit, (b) differential amplifier, (c) level shifter (LS), and (d) in-pixel 1-bit SRAM.

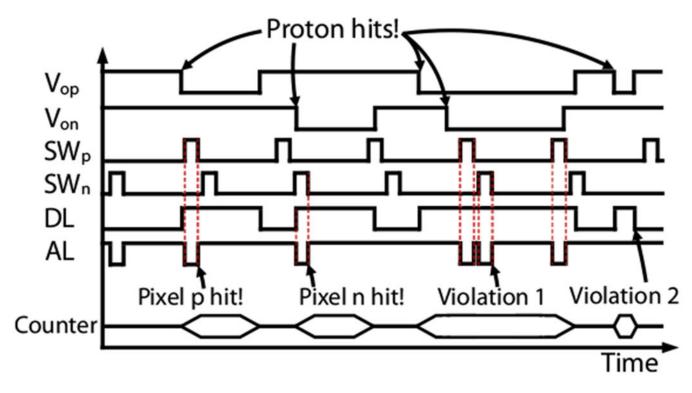


Fig. 6: Timing diagram.

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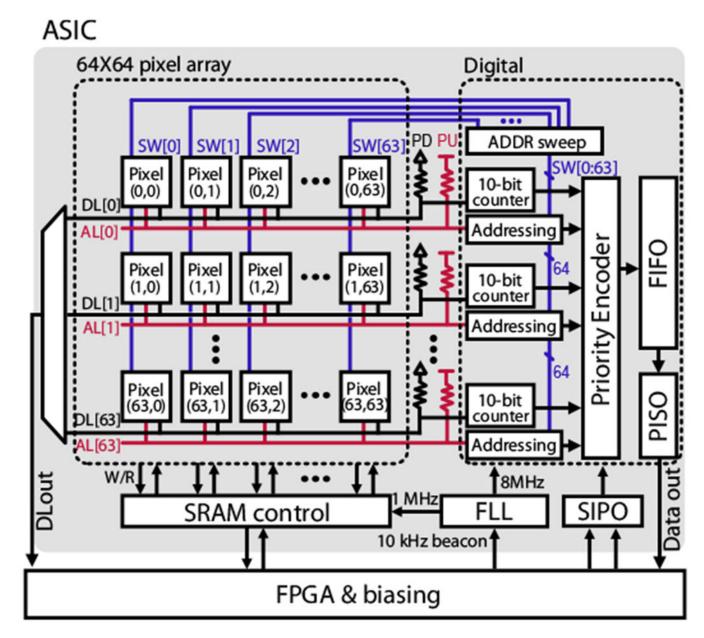
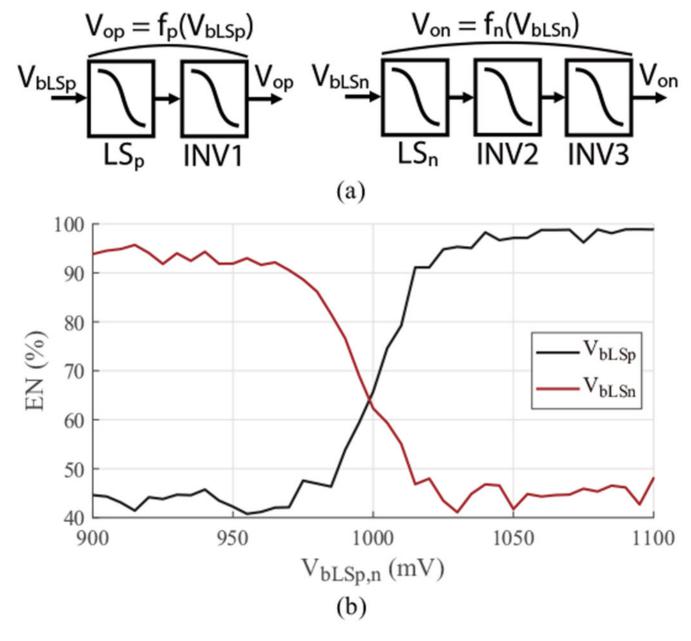


Fig. 7: Overall system diagram.





(a) Illustrations of $f_p(V_{bLSp})$ and $f_n(V_{bLSn})$ and (b) measured percentage of enabled pixels versus V_{bLSp} and V_{bLSn} . $V_{bLSp,n}$ means V_{bLSp} or V_{bLSn} .

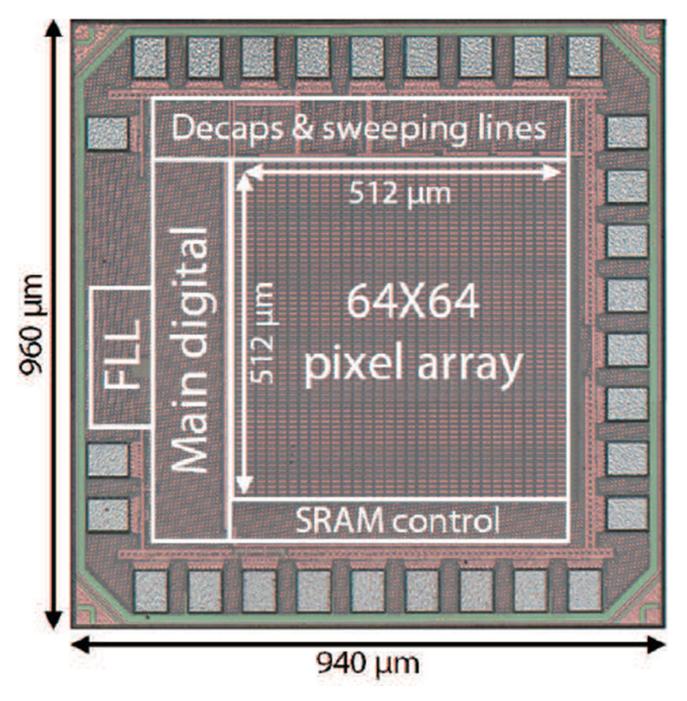
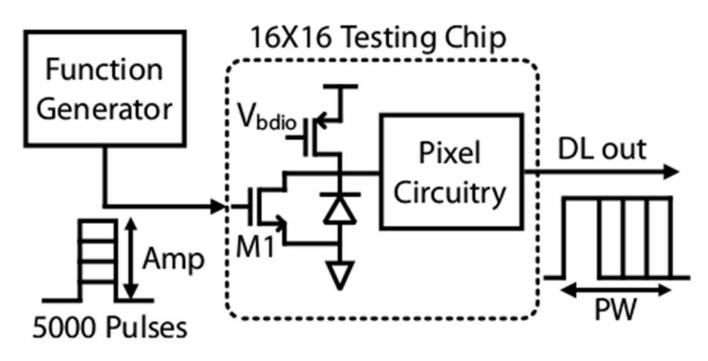
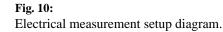
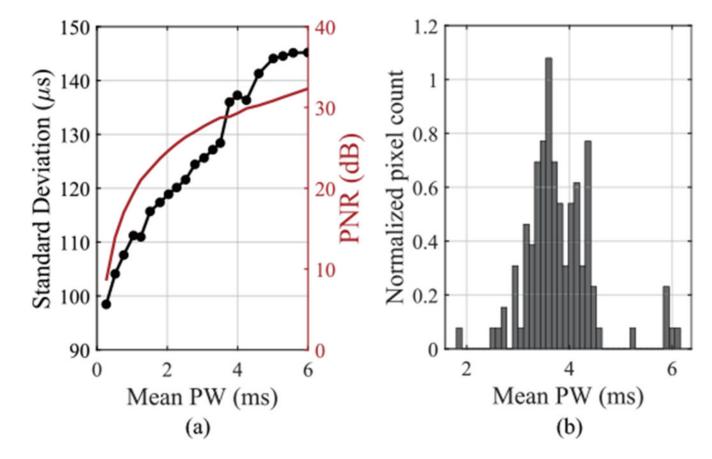


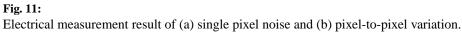
Fig. 9: Chip die photo.





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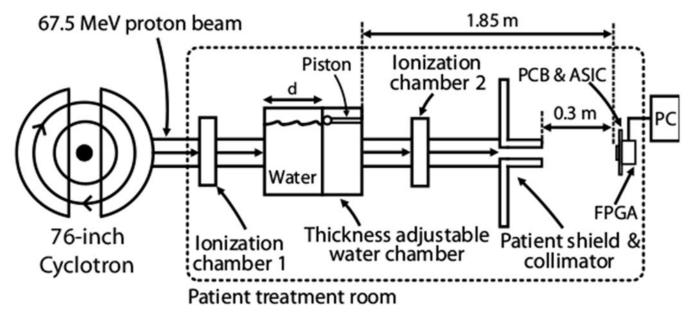


Fig. 12: Proton measurement setup diagram at CNL.

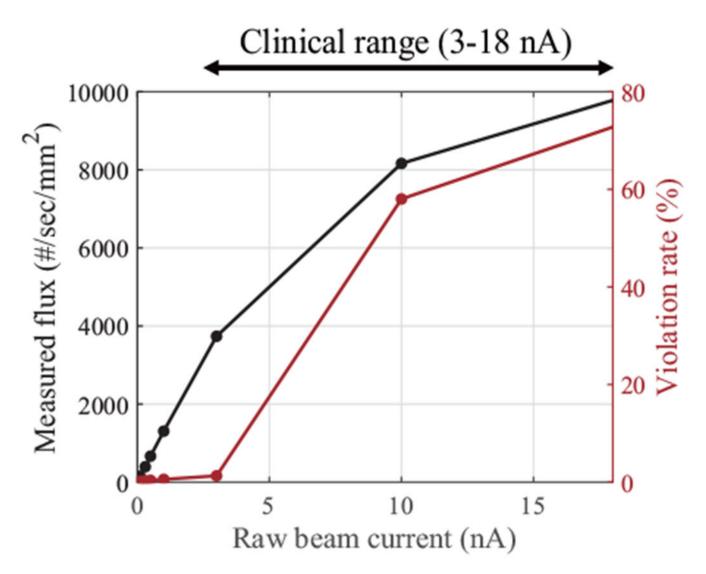
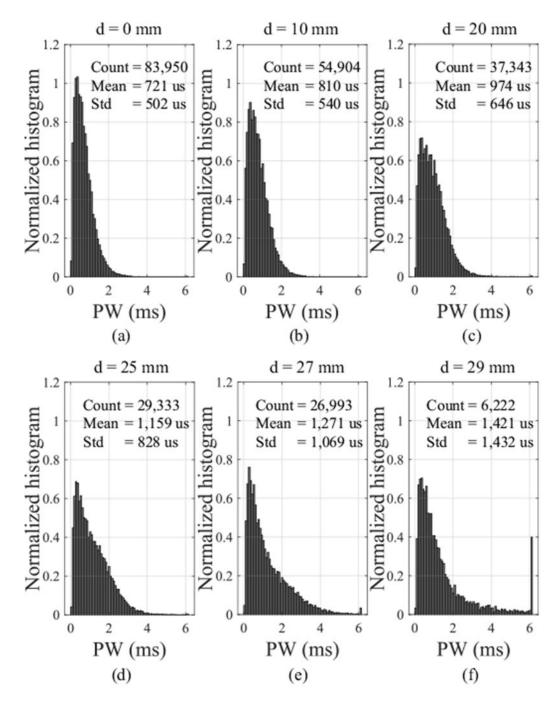


Fig. 13: Proton beam current versus measured flux and violation rate.





Normalized PW histograms measured for 80 seconds at (a) d = 0 mm, (b) d = 10 mm, (c) d = 20 mm, (d) d = 25 mm, (e) d = 27 mm, and (f) d = 29 mm.

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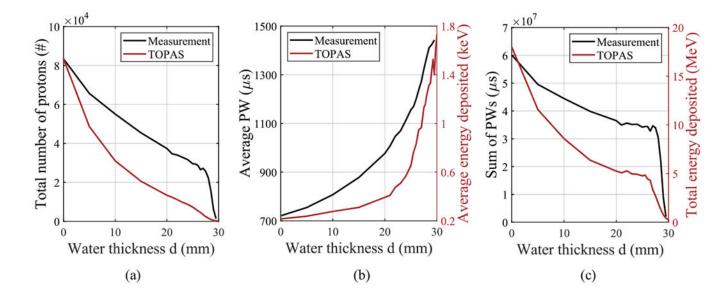


Fig. 15:

Measured and TOPAS simulated (a) total number of protons, (b) average PW (measurement) and energy deposition (simulation), and (c) summation of PW (measurement) and total energy deposited (simulation). Measurements are from 80 seconds of proton beam time. The total number of protons in TOPAS simulation is normalized to match the measured result at d = 0 mm.

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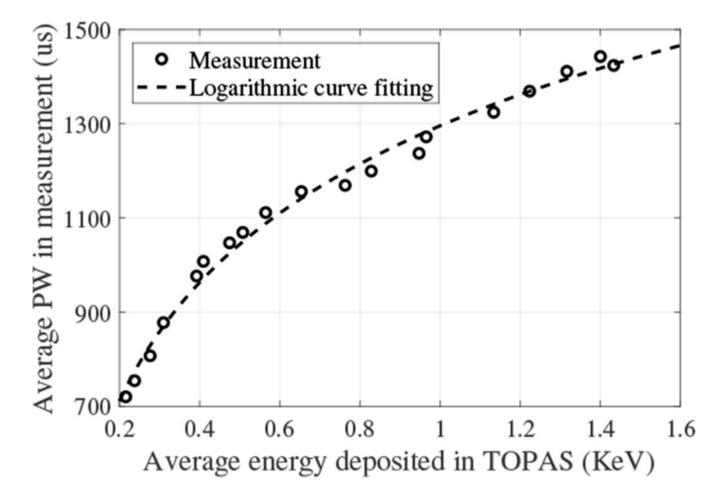


Fig. 16: Topas simulated average energy deposition versus measured average PW.

TABLE I:

Internal Clock Configurations

	Configuration	Default Value	Min	Max
t _{mst}	0.1, 0.125, 0.25, 0.5, 1 μs	0.125 μs	0.1 µs	1 µs
t _{cnt}	<i>t_{mst}</i> ×16, 32, 48, 64, 128	6 µs	1.6 µs	128 µs
t _{addr}	<i>t_{mst}</i> ×2, 4, 8, 32	0.5 µs	0.2 µs	32 µs
t _{PISO}	<i>t_{mst}</i> ×1, 2, 4, 8	0.5 µs	0.1 µs	8 <i>µ</i> s
t _{SRAM}	<i>t_{mst}</i> ×1, 8, 32, 64	1 µs	0.1 µs	64 <i>µ</i> s

TABLE II:

Relationship between the water thickness (d in Fig. 12) and the beam characteristics.

Water Thickness (d)	Increase
Proton energy loss in the water chamber	Increase
Proton energy after the water chamber	Decrease
Proton energy deposition in the detector	Increase
Proton flux at the detector	Decrease

TABLE III:

Comparison table with related state-of-the-art works.

	[3]	[4]	[2]	[9]	This work
Sensing method	Vth shift	Vth shift	RL/OSL	Floating gate Diode	Diode
Sensing area $(mm^2 \text{ or } mm^3)$	0.3×0.05	0.2×0.2	0.5×0.5×2 (single rod) 0.1×0.08	0.1×0.08	0.512×0.512
Power consumption for sensing (mW) N/A (Passive) N/A (Passive) 4 (low), 16 (peak)	N/A (Passive)	N/A (Passive)	4 (low), 16 (peak)	2	0.535
Power supply (V)	N/A	N/A	N/A	1.2	1.2
Real time?	No	Yes	Yes	Yes	Yes
Single particle detection?	No	No	No	No	Yes