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Methodology for optimal in situ alignment and setting of bendable optics for diffraction-limited focusing of soft x-rays

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ABSTRACT

We demonstrate a comprehensive and broadly applicable methodology for the optimal in situ configuration of bendable soft x-ray Kirkpatrick-Baez mirrors. The mirrors used for this application are preset at the ALS Optical Metrology Laboratory prior to beamline installation. The in situ methodology consists of a new technique for simultaneously setting the height and pitch angle of each mirror. The benders of both mirrors were then optimally tuned in order to minimize ray aberrations to a level below the diffraction-limited beam waist size of 200 nm (horizontal) \times 100 nm (vertical). After applying this methodology, we measured a beam waist size of 290 nm (horizontal) \times 130 nm (vertical) with 1 nm light using the Foucault knife-edge test. We also discuss the utility of using a grating-based lateral shearing interferometer with quantitative wavefront feedback for further improvement of bendable optics.

Keywords: metrology of x-ray optics, synchrotron radiation, nano-focusing, shearing interferometry, Hartman test, knife edge measurement.

1. INTRODUCTION

Applications of synchrotron radiation sources are becoming increasingly sophisticated in their ability to probe the smallest scales of interesting natural and man-made materials. This places stringent requirements on the performance of the x-ray optics that are used, especially the mirrors that focus the light onto the sample. Despite highly effective fabrication and ex situ tuning methods, the eventual degradation of these optics due to use, drifts and mechanical instabilities at the beamlines remains a challenge. This has compelled the development of comprehensive methodologies for in situ alignment and tuning of focusing mirrors, in order to realize and maintain the best possible performance.

Much fruitful work has been carried out by groups elsewhere towards the development of adjustable focusing x-ray mirrors. Mimura and coworkers¹⁻⁵ have made significant progress towards developing adaptive optical systems for focusing of hard x-rays as well as metrology techniques for evaluating their characteristics. Similarly, Mercère and coworkers⁶⁻⁸ have developed related methods for tuning active optics to minimize wavefront aberrations. The propagation of focused x-ray beams and their aberrations from precisely figured Kirkpatrick-Baez (KB) mirrors was simulated and studied in great detail by Kewish and coworkers.^{9,10} Achieving diffraction-limited quality from soft x-ray optics requires alignment feedback with sub-100 nrad slope error sensitivity, a challenging goal for any technique.

In this work, we present a systematic and effective methodology for simultaneous alignment and tuning of dual bendable mirrors, arranged in the KB configuration,¹¹ for focusing of soft x-rays at grazing incidence. After applying the described methodology, we demonstrate that the waist size of the resulting focused beam is nearly diffraction-limited. This two dimensional (2D) focusing methodology is based largely on our preceding work,¹²⁻¹⁵ wherein we achieved diffraction-limited one dimensional (1D) focusing with a single bendable mirror. To accommodate two orthogonal KB mirrors, we modified the existing experimental 1D focusing system. The overall system is summarized in Section 2.

Setting of the two bendable mirrors began in the Advanced Light Source (ALS) Optical Metrology Laboratory (OML). In the OML the mirrors' reflective surfaces were bent to most closely fit the desired elliptical slope profile, using the ALS Upgraded Second Generation Long Trace Profiler (LTP-II+).¹⁶⁻²⁰ We discovered (in situ) that maintaining the mutual perpendicularity of the two mirrors to a high accuracy is critical for achieving the best focusing performance. This relative roll alignment was carried out in the OML. After the surface figure of the two mirrors was set close to optimum ex situ, they were brought to the ALS developmental beamline (BL 5.3.1) for in situ tuning and analysis.

The straightforward methodology presented in Section 3 was effectively employed to optimally configure the two mirrors for focusing. The mirror farthest from the desired focus was aligned and tuned first, as described in Section 3.1. The same techniques were then used to align and tune the second mirror, as described in Section 3.2. Following these steps, we obtained nearly diffraction-limited focusing of a coherent monochromatic soft x-ray beam. The size of the beam waist is measured by Foucault knife-edge testing, discussed in Section 4, for verification of the nearly diffraction-limited performance of the KB mirror system. Going further, we implemented a wavefront sensing technique for possible finer tuning of the mirrors, which is described in Section 5.

2. OPTICAL SYSTEM FOR DIFFRACTION-LIMITED FOCUSING OF SOFT X-RAYS

The ALS developmental beamline 5.3.1 and its endstation were configured for development of in situ metrology techniques.^{12,14,15} The endstation chamber was designed to isolate the internal optical elements from the outside environment, in order to reduce the effects of vibrations and thermal drifts. This careful design, already described extensively in Refs. [12,14], was crucial to the success of this work. Most of this apparatus remained unchanged through the transition from 1D to 2D focusing. We therefore limit the scope of this discussion to optics downstream of the monochromator, which emits light of 1 nm wavelength (1.24 keV) into the endstation vacuum chamber. Figure 1 illustrates the arrangement of optics for focusing of the input soft x-ray beam. The beam illuminates an entrance aperture which then produces a divergent cylindrical or spherical wave, when the aperture is a slit or pinhole respectively. Between the entrance aperture and the mirrors is a pair of bidirectional scanning slits of adjustable width. A pair of bendable mirrors in the Kirkpatrick-Baez configuration focuses the beam to a predetermined point. In the vicinity of this expected focal point are a set of downstream metrology tools used to determine the focusing performance of the mirror system. Farther downstream, the beam may be viewed with a wide field CCD camera.

The entrance aperture consists of two components in series. A 20 μm circular pinhole accepts the beam from the monochromator. This is immediately followed (going downstream) by a 2 mm \times 2 mm nano-structure rectangular array of pinholes and slits of varying size and geometry. Fabricated using electron beam lithography at LBNL's Center for X-Ray Optics, this array is embedded on a 2.5 μm thick gold absorber layer deposited on a 100 nm silicon nitride membrane. A thick absorber was required to attenuate the otherwise bright beamline illumination. The slits in this array have widths ranging from 400 nm to 4 μm . The circular, elliptical, triangular and square pinholes in this array vary in diameter from 400 nm to 10 μm . The slits and pinholes are separated from each other by 100 μm . The array is translated transversely to the beam in order to select the appropriate aperture to serve as the optical object for the mirrors.

The bidirectional scanning slits are part of a JJ X-RayTM slit system. They have the dual purpose of acting as a secondary aperture for the input beam and as a pair of scanning slits for the mirror tuning process, described below. The vertical scanning slit translates horizontally, and the horizontal scanning slit translates vertically. They are placed near the upstream end of the horizontally focusing mirror to maximize the angular resolution of the scanning procedure.

Both the vertical and horizontal focusing mirrors were originally created for different optical configurations than their uses here. They were recently delegated to this work, because they have sagittal width profiles compatible to the requirements.^{20,21} The central grazing incidence angle is $\theta = 8$ mrad for both mirrors. For the horizontally focusing mirror, the distance from the entrance aperture to the mirror center is $r_h = 1525.76$ mm, and the predicted distance from the mirror center to focus is $r'_h = 244.59$ mm. For the vertically focusing mirror, these distances are $r_v = 1650.96$ mm and $r'_v = 119.39$ mm, respectively. The lengths of the horizontally and vertically focusing mirror substrates are 102.0 mm and 101.6 mm, respectively. The clear apertures for both mirrors span the middle 80% of the length. From these parameters, the image side numerical apertures (NA) in the vertical and horizontal directions are found to be 2.7 mrad and 1.3 mrad,

respectively. Both mirrors are mounted on a common Thorlabs™ XT95 optical rail. This allows easy transfer of both mirrors to and from the endstation between in situ and ex situ adjustments.

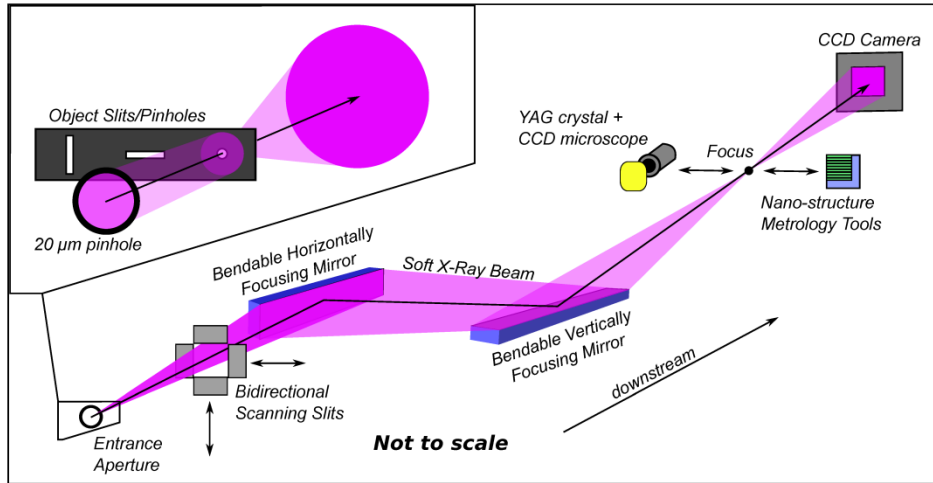


Fig. 1. Layout of Endstation Optics. The input beam is incident on a small entrance aperture which produces a diverging spherical wavefront. Two Kirkpatrick-Baez mirrors focus the beam to the desired location. A comprehensive but straightforward set of metrology tools are employed to quantitatively characterize the performance of the focusing system and provide feedback for in situ optimization.

Prior to in situ alignment and tuning, the expected incidence planes of both mirrors were made orthogonal to within 0.1 mrad in the ALS OML, using a Zygo GPI interferometer. We found that without this relative roll alignment of the mirrors, the best focusing of the two mirrors was far from optimum due to the corresponding optical aberrations. Following this alignment, the benders of both mirrors were adjusted on the OML LTP-II+ such that the surface tangential slope profiles best fit the desired elliptical cylinders, defined by the values of

3. OPTIMAL SETTINGS OF BENDABLE FOCUSING MIRRORS

Using the experimental optics system described here, we have developed a methodology to optimally align and tune a pair of bendable KB mirrors. The mounting of these two mirrors at the BL 5.3.1 endstation permits five degrees of freedom for each mirror: height, pitch, roll, and upstream and downstream bending moments. Each of these is controlled by actively tunable motors. The *height* of either mirror is the position of the mirror in the beam, with respect to motion in the direction perpendicular to the mirror surface. The *pitch* of either mirror is the angle that the x-ray beam makes with the surface in the plane of incidence. The *roll* of the mirrors is as described above. Setting this degree of freedom *ex situ* to a high accuracy simplifies the *in situ* alignment of the mirrors, allowing independent optimization of each mirror. For this reason, we make no further adjustments to the roll of either mirror. The upstream and downstream benders apply a torque to the upstream and downstream ends of the mirror, with the ends as the centers of rotation.²⁰⁻²³ The following procedures optimally configure the available degrees of freedom of both mirrors *in situ*. The first step for both mirrors is to simultaneously set the height and pitch of the mirrors. The second step sets the two benders for each mirror.

Though the desired focal point is known, there are many combinations of mirror height and pitch which may pass the beam through this point. It is difficult to know *a priori* which combination of motor positions sets the correct grazing incidence angle. However, the correct combination of height and pitch of a mirror minimizes the beam width when measured in the desired focal plane. This is easily seen by inspection of the equation for one dimensional grazing incidence tangential imaging,¹¹

$$\frac{1}{r} + \frac{1}{r'} = \frac{2}{R\theta} \quad (1)$$

where, for any small section of the mirror surface, r is the distance from the object to the section, r' is the distance from the section to the image or focal point, while θ and R are the grazing incidence angle and radius of curvature of the section, respectively. Consider varying both the height and pitch of the mirror continuously and in a manner such that the reflected beam always passes through the desired focal point, as illustrated in Fig. 2. A given change in height is compensated by a certain change in pitch, or vice versa. The object distance

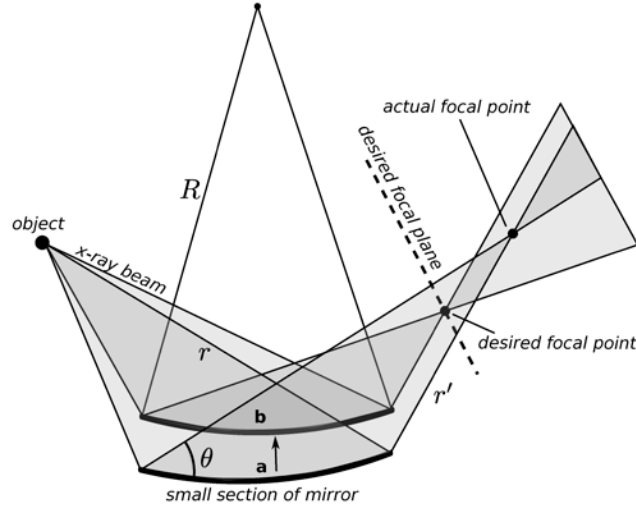


Fig. 2. The height and pitch of either mirror are set simultaneously by seeking the combination that minimizes the beam width in the desired focal plane. The beam width when the mirror is misaligned, as with orientation **a**, will always be larger than the minimum given by the correct orientation **b**. The dimensions of this diagram are not to scale.

3.1. TUNING THE HORIZONTALLY FOCUSING MIRROR

We applied this alignment first to the horizontally focusing mirror. The vertically focusing mirror was completely retracted from the beam path and a 4 μm vertical slit was used as the entrance aperture, serving as the object. In this 1D focusing configuration, the horizontally focusing mirror formed a demagnified image of the slit. The YAG crystal was placed in the desired focal plane in order to observe the beam with the CCD microscope system. From this point forward, we shall simply refer to the desired focal plane as the focal plane. An intensity-inverted image of the beam as viewed on the YAG in the focal plane is shown in Fig. 3.

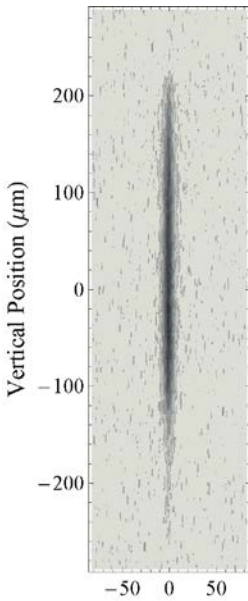


Fig. 3. Image on YAG of horizontally focused beam in the focal plane. Darker pixel values indicate higher intensity.

As the first step we conducted the height-pitch alignment described above. We translated the mirror through various heights, while keeping the position of the beam in the focal plane fixed by adjusting the pitch in compensation. As the mirror height was translated through 500 μm , the mirror angle was adjusted by approximately 0.9 mrad. Here, we define the beam width as the root mean square (RMS) normalized intensity distribution,

$$\sigma \equiv \sqrt{\iint (x - \mu)^2 I(x, y) dx dy} \approx \sqrt{\sum_{m,n} (x_n - \mu)^2 I_{m,n}} \quad (2)$$

where x and y are respectively the horizontal and vertical coordinates on the focal plane, μ is the intensity centroid position and I is the normalized intensity, $\iint I(x, y) dx dy = \sum_{m,n} I_{m,n} = 1$. The summation is taken over pixels within the region of interest, after subtraction of background noise, with x_n and $I_{m,n}$ being the position and normalized intensity of the pixel in the m^{th} row and n^{th} column.

The measured beam width as a function of mirror height for this procedure is shown in Fig. 4. The minimum of this curve indicates the optimal height and corresponding pitch angle of the mirror. After setting the mirror to these values,

the beam width was reduced to $3.7 \mu\text{m}$. The true width of the beam is much less than this value. The beam observed on the YAG is significantly broadened due to the resolution of the CCD microscope system.¹² The effective resolution of a few microns is sufficient for the purposes of this alignment procedure. Moreover, despite this $>1 \mu\text{m}$ image resolution, the beam centroid can in fact be known to within 100 nm because it is a weighted average over all pixels.

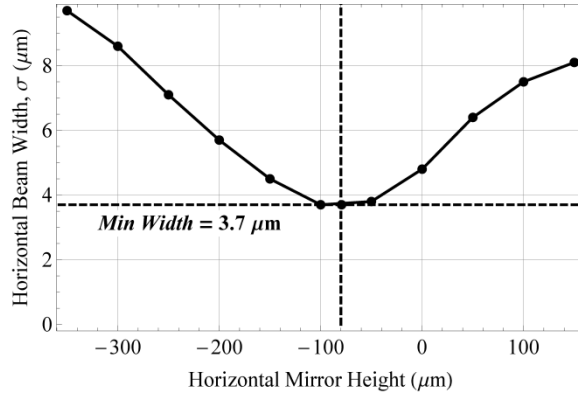


Fig. 4. Horizontal beam width versus horizontal mirror height. There is a one-to-one correspondence between mirror height and pitch. The given values for mirror height are raw motor values.

After setting the height and pitch of the horizontally focusing mirror, we optimized the tangential surface figure by making small adjustments to the benders. The upstream vertical scanning slit was closed to a width of $50 \mu\text{m}$ to illuminate a $\sim 5 \text{ mm}$ longitudinal section of the mirror. We found that the narrower slit sizes do not transmit enough light for reliable measurements. In this configuration, we measured the horizontal centroid of the reflected beam as a function of slit position. In the focal plane, the horizontal distance between the centroid and the focal point is the horizontal ray error. The initially measured horizontal ray error (an average of four sequential measurements) is shown by the dashed curve in the left panel of Fig. 5.

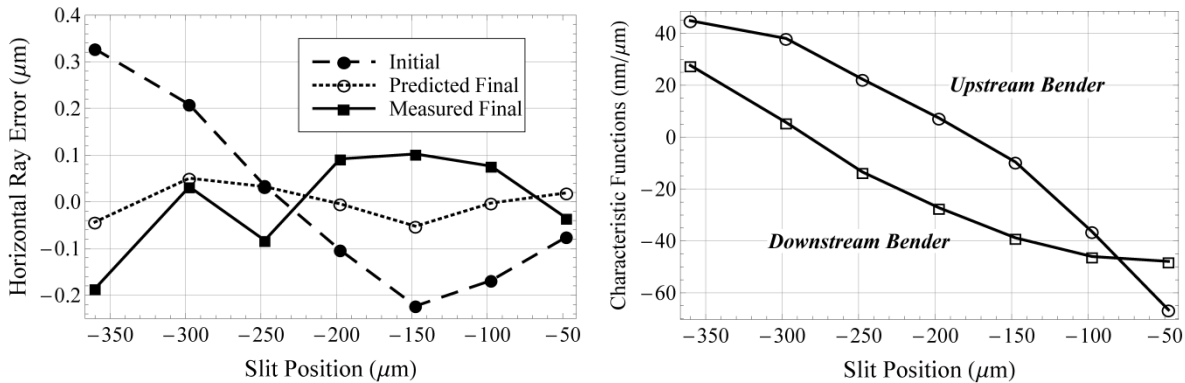


Fig. 5. (Left) Initial and final measurements of horizontal ray error. The optimization was performed using linear regression methods developed for tuning bendable mirrors. (Right) Characteristic functions of the benders for the horizontally focusing mirror, given in nm of ray error change per μm of motor adjustment. Slit position values are relative.

The characteristic functions of the two benders with respect to ray error are shown on the right panel of Fig. 5. They are given by the point-by-point difference in ray error with respect to a unit change of the corresponding bender motor. We assume that the response of the ray error to changes of bender motors is approximately linear for a sufficiently small range of adjustment. Then linear regression^{18,24} predicts a final minimized ray error given by the dotted curve in the left panel on Fig. 5, corresponding to a change of $+3.0 \mu\text{m}$ to the upstream bender motor and $-10.6 \mu\text{m}$ to the downstream bender motor. After applying these changes to the bender motors, we observed the final minimized ray error given by the

solid curve in the left panel of Fig. 5. The RMS variation of ray error in the initial measurement was 202 nm, while the RMS variation in the final measurement was 81 nm. This final value is at the level of the estimated uncertainty of the horizontal centroid, which was 80 nm, indicating that the benders have been set to the maximum precision allowed by this technique.

3.2. TUNING THE VERTICALLY FOCUSING MIRROR

With the horizontally focusing mirror well aligned and tuned for focusing, the vertically focusing mirror was also adjusted independently with the same procedure. This mirror was reinserted into the beam path, and a 4 μm diameter circular pinhole served as the object for 2D focusing. First, the height and pitch alignment was performed for the vertically focusing mirror. Figure 6 shows the measured beam width as a function of mirror height. In the improved configuration the vertically focusing mirror produced a minimum vertical beam width of 4.9 μm .

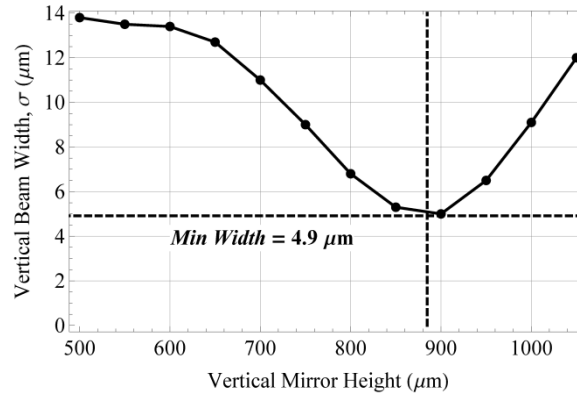


Fig. 6. Vertical beam width versus vertical mirror height. There is a one-to-one correspondence between mirror height and pitch. The given values for mirror height are raw motor values.

The benders of the vertically focusing mirror were optimally tuned in the same way as described for the horizontally focusing mirror. The horizontal upstream scanning slit was closed to a width of 100 μm to illuminate a ~ 10 mm section of the mirror. This was the minimum width that allowed sufficient illumination for clear observation of the reflected beam. To improve the measurement in the presence of low signal intensity, we doubled the density of sample points in the scan. The initially measured vertical ray error is shown as the dashed curve in the left panel of Fig. 7. After measuring the characteristic functions of both benders, plotted in the right panel of Fig. 7, we used linear regression to calculate and apply the optimal bender settings, resulting in the final minimized ray error, shown as the solid curve in the left panel of Fig. 7. This is comparable to the predicted final ray error, shown as the dotted curve. Alignment reduced the RMS vertical ray error from 109 nm to 36 nm. This value is within the 50 nm uncertainty for the vertical beam centroid position, estimated from repeated identical measurements.

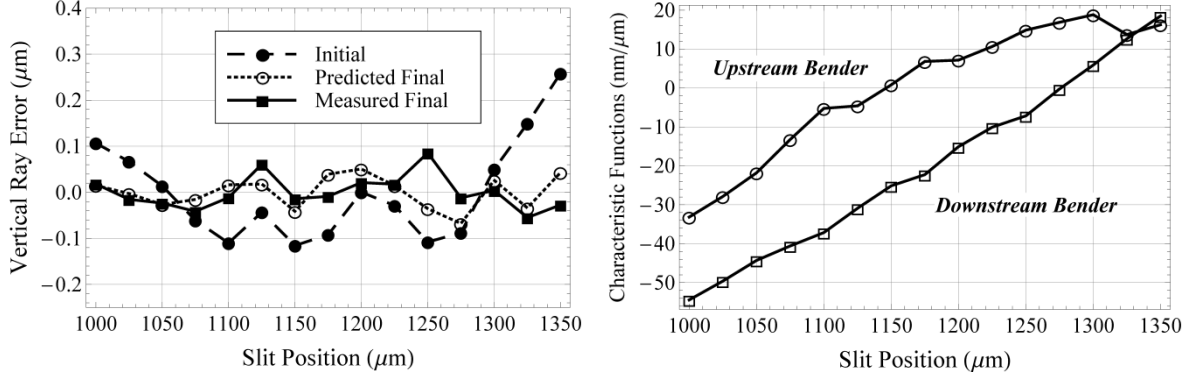


Fig. 7. (Left) Initial and final measurements of vertical ray error. The optimization was performed using linear regression methods developed for tuning bendable mirrors. (Right) Characteristic functions of the benders for the vertically focusing mirror, given in microns of ray error change per micron of motor adjustment.

4. KNIFE-EDGE MEASUREMENT OF BEAM WAIST

We quantitatively verified the focusing performance of this KB mirror system using the scanning Foucault knife-edge test. An opaque half-plane, or knife-edge, was passed transversely through the beam in steps across the focal plane. At each step the total transmitted flux is recorded as a function of the position of the knife-edge. This test yields information about the intensity distribution across the focal plane.

Because the result of this test is essentially the antiderivative of the intensity profile along the scan direction, calculations of beam width are usually made indirectly. Sometimes the 10–90% or 20–80% widths are given, referring to the flux profile directly. This has the drawback that it does not relate to the intensity distribution in a rigorous way. Another evaluation of the intensity distribution is done by fitting the flux data to some assumed functional form, such as an error function (i.e. assuming a Gaussian profile¹⁵), and then taking the derivative, based on the fit. The downside of this approach is that the beam intensity distribution may not match the assumed form.

Here we provide a general method for computing the statistical moments of the intensity profile directly from the flux data. The same approach is used in the horizontal and vertical directions independently. Let $I(x)$ be the normalized intensity, with the flux being its antiderivative $F(x) \equiv \int I(x) dx$, as a function of the horizontal or vertical distance x . In practice, both of these functions are defined only within some measurable interval $x \in [a, b]$, such as the range of knife-edge positions covered by a scan of measurements. Then by definition, we have $\int_a^b I dx = F(b) - F(a) = 1$. The m^{th} order raw moment of the distribution function $I(x)$ is defined as

$$\mu_m \equiv \int_a^b x^m I(x) dx = \int_a^b x^m \frac{dF}{dx}(x) dx.$$

Integration by parts yields

$$\begin{aligned} \mu_m &= b^m F(b) - a^m F(a) - m \int_a^b x^{m-1} F(x) dx \\ &= [b^m - a^m] F(b) + a^m [F(b) - F(a)] - m \int_a^b x^{m-1} F(x) dx. \end{aligned}$$

Using the equalities $F(b) - F(a) = 1$ and $b^m - a^m = m \int_a^b x^{m-1} dx$, this second expression can be reduced to

$$\mu_m = a^m + m \int_a^b x^{m-1} [F(b) - F(x)] dx \quad (3)$$

Then for the intensity profile of the beam, an unambiguous measure of width is the RMS,

$$\sigma = \sqrt{2 \int_a^b [F(b) - F(x)](x - a) dx - \left(\int_a^b [F(b) - F(x)] dx \right)^2} \quad (4)$$

This relation provides a direct way of estimating the width of the beam intensity profile from measurements of the transmitted flux as a function of knife-edge position. It is important that the knife-edge step size be small relative to the beam width, or to spatial fluctuations in the intensity, to ensure that the integrals are accurately estimated by interpolating functions between data points.

We performed horizontal and vertical knife-edge scans using the downstream soft x-ray CCD camera as the detector because of its high sensitivity. To measure the horizontal width of the beam in the focal plane, we scanned the vertical knife-edge horizontally through the beam while measuring the total transmitted flux. The transmitted flux is measured by taking the sum of counts over all pixels in the full-beam footprint on the CCD camera, after suitable background subtraction. The measured flux as a function of the horizontal position of the knife-edge in the focal plane is presented in Fig. 8. The range of knife-edge positions spanned 3 μm , covered in 50 nm steps. Using Eq. (4) and generating the function $F(x)$ from a cubic-spline interpolation between data points, the horizontal RMS width of the beam was 290 nm. The dashed curve in Fig. 8 is the best fit error function, whose derivative has an RMS width of 220 nm. The discrepancy comes from the broader tails of the measured distribution, which are not well represented by the error function's assumed Gaussian intensity profile.

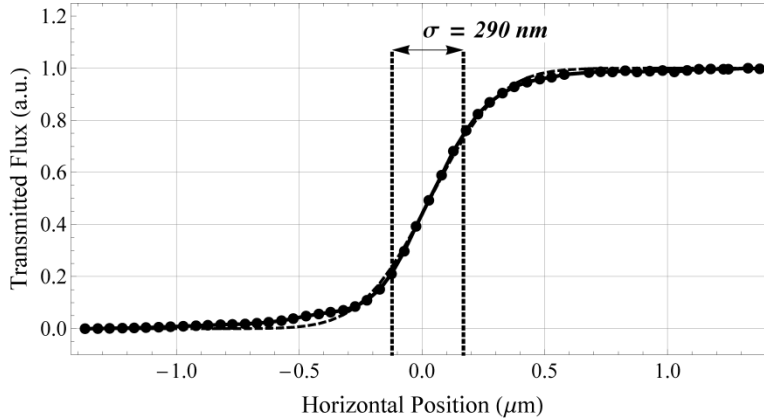


Fig. 8. Transmitted flux as a function of horizontal position of knife-edge. The dashed curve shows the error function which best fits the data.

The vertical width of the beam at the focus was measured in the same way. The horizontal knife-edge was scanned vertically through the beam across the focal plane, in steps of 50 nm through a range of 2 μm . The observed transmitted flux as a function of vertical position of the knife-edge is shown in Fig. 9. Here the RMS vertical width of the beam profile is 130 nm.

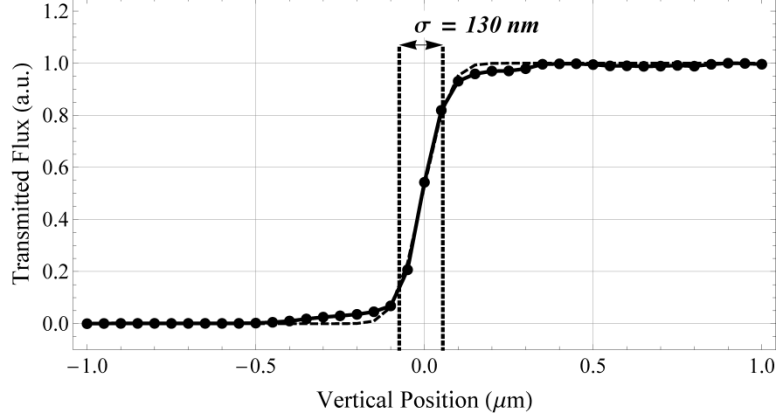


Fig. 9. Transmitted flux as a function of vertical position of knife-edge. The dashed curve shows the error function which best fits the data.

In summary, knife-edge measurements show a focused beam waist size of 290 nm (horizontal) \times 130 nm (vertical). This can be compared to the estimated diffraction-limited beam waist size of 200 nm (horizontal) \times 100 nm (vertical).

5. SHEARING INTERFEROMETER FOR HIGH SENSITY WAVEFRONT FEEDBACK

Lateral shearing interferometry offers a more sensitive measurement of optical aberrations than the techniques described above. It can be much quicker than the scanning slit technique because only a single camera exposure is required, and a sensitive, direct detection soft x-ray CCD can be used. While the scanning slit method for alignment is ultimately one dimensional, the lateral shearing interferometer provides complete two dimensional information about the focusing system. Furthermore, the increased spatial resolution in the wavefront offered by shearing gives clearer insight into quality of the focused beam. The procedure we propose for this purpose is similar to that given above for setting the mirror benders, with the exception that instead of seeking minimal ray error, one seeks minimal wavefront error. This method was previously demonstrated in 1D for the optimization of the same vertically focusing KB mirror.¹⁵

The lateral shearing interferometer is composed of a 2D cross grating, at some distance z_g downstream of the focal point, and a CCD camera placed in the beam some larger distance z_s from the grating. Both the grating and the CCD are inclined to be normal to the central ray. Let m be any integer, d the period of the grating and λ the wavelength of illumination. Then under the condition,

$$\frac{1}{z_s} + \frac{1}{z_g} = \frac{\lambda}{md^2}, \quad (5)$$

the Talbot effect²⁵ is observed: a magnified self-image of the grating forms on the CCD. If the beam is a perfect spherical wave, then the self-image (within the paraxial wave approximation) is perfect. Wavefront aberrations locally deform the self-image in proportion to the slope error. With the CCD camera placed 1.5 m downstream of focus, the first ($m = 1$) Talbot plane (where the grating should be placed) is approximately $z_g \approx d^2 / \lambda$. Using gratings with periods from 4 to 8 μm and soft x-rays of wavelength $\lambda = 1$ nm, we have $16 \text{ mm} \leq z_g \leq 64 \text{ mm}$.

The self-image of the square wave transmission grating is formed on the CCD by the infinite number of overlapping diffracted orders emanating from the grating, rotated in succession by an angle $\sim \lambda/d$. The dominant contributions to the observed intensity pattern I across the CCD as a function of Cartesian coordinates x and y are given by the overlapping zeroth and first order beams,

$$I(x, y) = A + B_1 \cos(k[W(x + s, y) - W(x, y)]) + B_2 \cos(k[W(x, y + s) - W(x, y)]) + \dots ,$$

where W is the wavefront displacement of the zeroth order beam, $s = z_s \lambda / d$ is the shear distance, and A , B_1 , & B_2 are constants (or slowly varying terms in the presence of noise and inhomogeneous illumination). We applied well-known Fourier transform-based phase retrieval methods²⁶⁻⁴⁰ to obtain the directional derivatives of the wavefront,

$$\frac{\partial W}{\partial x} \approx \frac{W(x+s, y) - W(x, y)}{s} \quad \text{and} \quad \frac{\partial W}{\partial y} \approx \frac{W(x, y+s) - W(x, y)}{s}.$$

This approach assumes that the shear distance is much smaller than the characteristic length scales of wavefront aberrations δW across the CCD, $s \ll |\lambda / (\partial \delta W / \partial x)|$ and $s \ll |\lambda / (\partial \delta W / \partial y)|$. It is easy to see that an equivalent restriction is $|\nabla(\delta W)| \ll d / z_g$, using the expression for shear distance provided above and the gradient operator ∇ . That is, the wavefront slope aberrations must be initially small, much less than $\sim 2 \mu\text{rad}$ in our case, in order to assume accurate wavefront reconstruction with the lateral shearing interferometer. Provided that the surface slope of the focusing mirrors is within $1 \mu\text{rad}$ of the desired elliptical figure, this criterion is easily met.

The wavefront is obtained from its measured derivatives in the frequency domain. More detailed approaches^{41,42} can be taken to obtain the wavefront, using more accurate descriptions of the shearing measurement. However, we found the following simplified analysis to be sufficient for this work. Let the Fourier transform of the derivatives $\partial W / \partial x$ and $\partial W / \partial y$ be $\Psi'_x(u, v)$ and $\Psi'_y(u, v)$, respectively, with conjugate variables $(u, v) \leftrightarrow (x, y)$. Then the Fourier transform $\Psi(u, v)$ of the function $W(x, y)$ is (to within an arbitrary additive constant)

$$\Psi(u, v) = \begin{cases} 0 & u = v = 0 \\ \Psi'_v / i2\pi v & u = 0, v \neq 0 \\ \Psi'_u / i2\pi u & u \neq 0, v = 0 \\ \frac{1}{i4\pi} \left[\frac{\Psi'_u}{u} + \frac{\Psi'_v}{v} \right] & u \neq 0, v \neq 0 \end{cases}. \quad (6)$$

If the CCD pixel density is below the Nyquist sampling rate for the wavefront function $W(x, y)$, then its Fourier transform coincides with the discrete Fourier transform of its uniformly spaced samples.⁴³ We can therefore apply this relation along with Eq. (6) to obtain the wavefront from its derivatives, which are recovered from the observed interferogram. Based on a comparison of repeated wavefront measurements, the precision of the overall wavefront retrieval method with 1 nm illumination is on the level of 0.1 nm .

When the KB mirror system was configured nearly optimally (but prior to applying the procedures of Sec. 3), a shearing interferometer measurement was made and is illustrated by Fig. 10. On the left panel of Fig. 10 is the (intensity-inverted) self-image of a grating, as viewed on the downstream CCD camera. This grating, with a period of $6 \mu\text{m}$, was placed a distance of $z_g = 36 \text{ mm}$ downstream of the effective focus of the beam. To find the best position for self-imaging, we varied the grating distance z_g by several mm about this value until the best contrast was observed. We applied the wavefront recovery approach described above to obtain the estimated wavefront, illustrated by the contour plot in the middle panel of Fig. 10. The grating was rotated by a small angle, but this can be accounted for in the wavefront reconstruction by an appropriate transformation of derivatives. The right panel of Fig. 10 shows the residual wavefront error after subtracting the best fitting sphere (radius of curvature = $z_s = 1.524 \text{ m}$) from the recovered wavefront. The peak-to-value magnitude of wavefront error is 2.1 nm , and the RMS value is 0.5 nm . Figure 10 indicates significant $0-90^\circ$ astigmatism of the focused beam, which may be compensated by adjusting the benders of both mirrors.

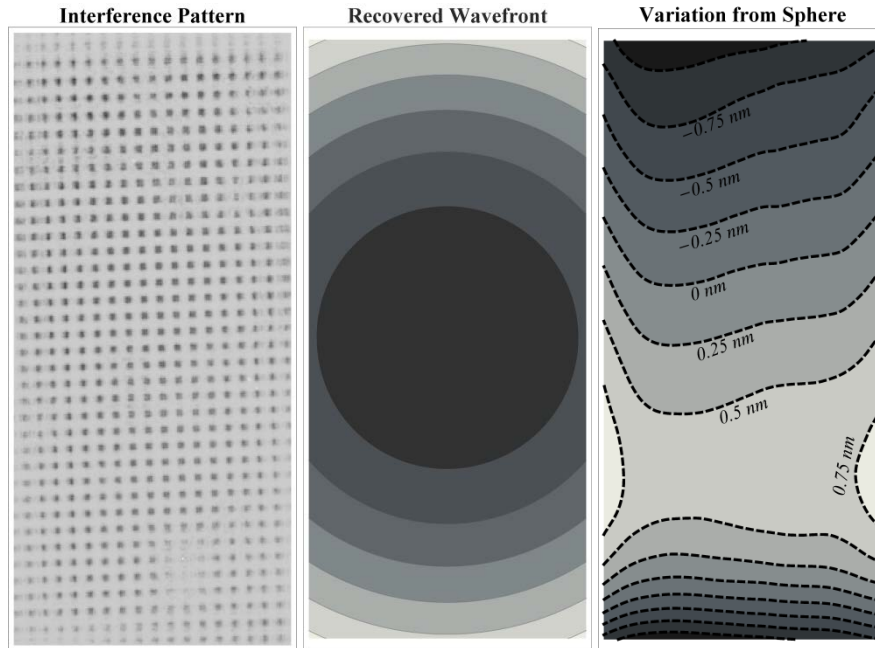


Fig. 10. Wavefront measurements from lateral shearing interferometry. The measured interference pattern is on the left, the recovered wavefront of the zeroth order beam is in the middle, and the difference between this wavefront and a perfect sphere is shown on the right.

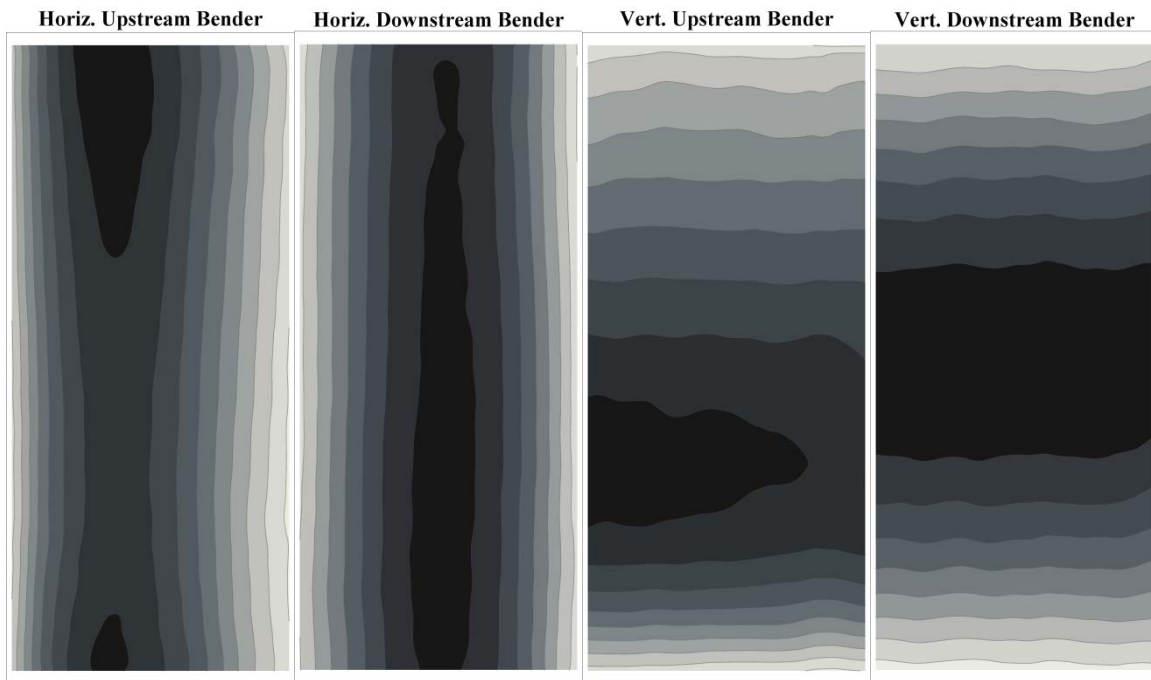


Fig. 11. Wavefront-based characteristic functions of the four mirror benders. From left to right: upstream and downstream benders of the horizontally (Horiz.) focusing mirror, and upstream and downstream benders of the vertically (Vert.) focusing mirror. Characteristic functions shown here are normalized to facilitate comparison.

To perform fine alignment using shearing interferometry, we measured the characteristic functions of all four benders. Each bender is actuated in turn, and the normalized characteristic functions (per unit of actuation) are revealed in the wavefront differences. The contour plots in Figure 11 illustrate the measured characteristic functions. Each bender produces similar results, with cylindrical defocus being the primary change. Yet the relative displacement of these shapes along the mirror surface reveals that third order wavefront shape changes are also controllable.

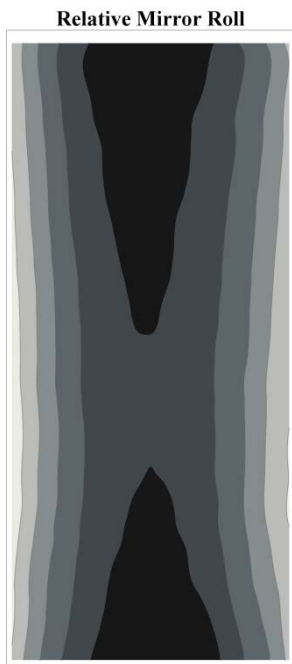


Fig 12. Normalized wavefront-based characteristic functions of the relative roll angle of the KB mirrors.

Taking advantage of the high sensitivity of the shearing interferometer, we also measured the effect of rolling one of the mirrors with respect to the other. The contour plot in Fig. 12 illustrates the observed change of recovered wavefront after a small change of the roll motor of the horizontally focusing mirror. Because of the grazing incidence geometry of the KB mirrors, we expected that rolling the vertically focusing mirror in the opposite direction would have roughly the same effect. The result of this relative roll misalignment is the introduction of 0–90° astigmatism. Based on the mirror bender characteristic functions presented in Fig. 11, this aberration could be compensated, at least in part, by suitable adjustments to the benders. However, if the relative roll of the mirrors is allowed to vary in situ, this establishes a certain degree of indeterminacy in the solutions for the optimal bender settings found by linear regression analysis. It is for this reason that we recommend avoiding this difficulty by presetting the roll alignment of the mirrors to a high precision ex situ, and considering this parameter as fixed during in situ alignment.

The 2D at-wavelength metrology information made available by the lateral shearing interferometer makes it a promising tool for the optimization of bendable focusing optics. Beam-time constraints limited our ability to fully realize the optimization with shearing interferometry, beyond the wavefront shown in Fig. 10. However, this route for further optimization may be beneficial to this and future adaptive optical systems.

6. CONCLUSIONS

At the Advanced Light Source, we are developing and demonstrating a variety of in situ at-wavelength metrology techniques for synchrotron beamlines and short wavelength optical systems. Building upon our previous work with 1D focusing, we have established an effective methodology for ex situ and in situ alignment and tuning of a KB mirror pair, resulting in nearly diffraction-limited focusing of soft x-rays. This methodology incorporates accessible technologies and straightforward analyses and we believe it is broadly applicable to many existing synchrotron beamlines and those of next generation synchrotron light sources.

Central to the success of the interferometric techniques is the creation of a high quality reference wavefront in the object plane. If the beam illuminating the focusing optics is not well conditioned to begin with (a large beam size, or low spatial coherence), then diffraction-limited focusing will never be possible, and the effectiveness of shearing tests will be limited. Such cases may be better served by Hartmann tests. Other essential factors were the incorporation of numerous degrees of freedom in the mirror mounts, with feedback, including the ability to tilt, roll, and bend the mirrors, and to position them into or out of the beam. As we expanded our mirror optimization and testing program from 1D to 2D focusing, the techniques remained similar, except for the challenging requirement that the two mirrors independently focus to the same plane.

The methods we applied have relative strengths and weaknesses. The scanning slit method can be applied to large aberrations present during coarse alignment. It enables fine control of the ray error across the mirror surfaces, yet in practice its accuracy was limited by low-flux and by the visible-light microscope used to image the beam. The knife-edge test provides unambiguous measurement of the beam width in the directions orthogonal to the edges. Finally, shearing interferometry demonstrates high sensitivity and efficient measurement capabilities when the mirrors are close to their final alignment state.

Small-scale demonstrations such as this serve as a model for how the techniques could be applied to existing and future applications where nearly diffraction-limited performance is required. These can include fourth-generation synchrotron, and free-electron laser systems, where brightness and wavefront preservation is critical. Future work will include the exploration of the sensitivity limitations of these techniques, and their application at different beam energies, and NA values, where material selection and nanofabrication may not be as straightforward.

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