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## and

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# **Vapor-Liquid Equilibria for Mixtures of Chain Fluids Near-to and Far-from the Critical Region**

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*. A recently-established crossover equation of state for pure chain fluids is extended to mixtures of chain fluids. Far from the critical region, where density fluctuations are small, it reduces to the classical equation of state. Near or at the critical point, the crossover equation of state incorporates contributions from longwavelength density fluctuations. Using segment-segment parameters for pure components, and one cross parameter*  $k_{12}$  for every binary pair as obtained from *data remote from the critical region, this crossover equation of state gives vaporliquid equilibria in good agreement with experiment for binary asymmetric mixtures of n-alkanes far-from, near-to and at the critical point.* 

*Keywords*: Vapor-liquid equilibrium, Critical point, Equation of state, Renormalizationgroup theory, n-Alkane mixtures

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## **Introduction**

Critical conditions are sometimes encountered in some industrial operations, especially in production and subsequent processing of petroleum and natural gas. Near the critical region, retrograde condensation is often observed. For quantitative process calculations, we require an equation of state (EOS) for mixtures that is valid near-to and far-from critical conditions. An EOS that meets this requirement is called a crossover EOS. This work presents a crossover EOS for mixture of chain fluids.

To illustrate retrograde condensation, Figure 1 shows the pressure-temperature loci for a . mixture at fixed composition. The solid line is the bubble-point curve and the dashed line is the dew-point curve; they join at critical point C (first recognized by Andrews in 1869) where the two phases become identical. Point  $C$  shows the limiting condition where the system can exist in two phases. Near the critical point, the density-dependent properties change dramatically with small changes in temperature or pressure. One century ago, Kuenen (1893, 1897) first observed isothermal retrograde condensation shown in line 1; isobaric retrograde vaporization, shown in line 2, was observed by Duhem (1896, 1901). The maximum pressure at point *A* is called cricondenbar or maxcondenbar, and the maximum temperature at point  $B$  is called cricondentherm or maxcondentherm (Sage et aI., 1934). These points give the upper bounds where phase separation can take place. Quantitative understanding of these phase-equilibrium phenomena is useful for design of production, storage and transportation of fossil-fuel products;

Although extensive experimental studies have been reported (for a review, see Dohrn and Brunner, 1995), it has been difficult to develop a universal model to describe the thermodynamic properties and phase behavior of fluid mixtures at high pressures over a wide range of conditions including the critical region. Most previous studies are concerned with empirical or phenomenological correlations for vapor-liquid equilibria (VLE) (e.g., Chao and Seader, 1961; Dastur and Thodos, 1963; Stevens and Thodos, 1963; Van Hom and Kobayashi, 1968; Reid et aI., 1987 ); these studies use anyone of several popular EOS like RK (Redlich and Kwong, 1949), SRK (Soave, 1972) and PR (peng and Robinson, 1976). These cubic EOS provide improvement over the original van der Waals EOS (van der Waals, 1873) through modifications of the attraction terms as reviewed by Yelash and Kraska (1999). It has long been recognized, however, that although these analytical EOS can describe fluid properties fairly well far away from the critical point, because they are mean-field-based, they fail to reproduce the non-analytical, singular properties at the critical point and therefore give poor results in the critical region (Ma, 1976). Mean-field theories assume that the immediate environment of each particle in a fluid has the same composition and density as those of the bulk fluid. Mean-field theories neglect density fluctuations that become large near the critical point (Greer and Moldover, 1981; Sengers and Levelt-Sengers, 1986; Fisher, 1998). Levelt-Sengers (1999) gives a detailed historical review of the weaknesses and strengths of mean-field theories.

Although the inability of mean-field theories to describe critical behavior has been known for many years, a method for corrections became available only relatively recently. Taking long-range density fluctuations into account, scaling and crossover theory can correct meanfield theory. The crossover theory developed by Sengers and coworkers (Edison et aI., 1998; Anisimov et aI., 1999; Povodyrev et aI., 1999), by Anisimov et ai. (1995) and by Kiselev et al. (1998, 1999a, 1999b) incorporates a crossover from singular thermodynamic behavior at the critical point to regular thermodynamic behavior far away from the critical point. In this way, a common engineering EOS can be modified for use near the critical point and to yield correct critical behavior. However, the necessary modifications are far from trivial; the required calculations are complex and the physical meaning of the many required crossover parameters is not clear in terms of molecular properties.

The optimized random-phase approximation leads to hierarchical reference theory (HRT) (Parola and Reatto, 1984, 1985; Meroni et aI., 1990). HRT can be considered as an exact reformulation of Omstein-Zernike integral theory including density fluctuations at all length scales; it can also be taken as a liquid-state implementation of the renormalization-group (RG) theory. Although HRT has been successfully applied to Lennard-Jones fluids and to binary mixtures (Parola and Reatto, 1991; Pini et aI., 1998c), reduction to practice is tedious. A thermodynamically self-consistent Omstein-Zernike integral theory developed by Stell and coworkers (Pini et aI., 1998a, b) provides thermodynamic properties, critical points and coexistence curves for a lattice gas and for a hard-core Yukawa fluid that compare well with computer simulations. But this integral theory, at present restricted to spherical molecules, has not been reduced to practice.

Finally, White and coworkers (White, 1992; White and Zhang, 1993, 1998) developed a global RG theory based on the Nobel-prize winning RG theory of Wilson (1971a, b, 1983). When extended beyond the range of the original RG theory, it can be successfully applied

beyond the critical region. The major advantage of White's work is that only a few parameters are required and these have a molecular basis.

Lue and Prausnitz (1998a,b) extended the accuracy and range of White's RG transformation through an improved Hamiltonian. Good representations of thermodynamic properties and phase equilibria were obtained for pure fluids and their binary mixtures using an analytical formulae for square-well (SW) model fluids (Tang and Lu, 1993, 1994, 1995). Tang (1998), and White and Zhang (1999) have applied White's theory to Lennard-Jones fluids. However, all of these publications are confined to fluids containing simple spherical molecules. Fornasiero et ai. (1999) reported a limited attempt to apply White's theory to non-spherical molecules using a cubic EOS.

Based on the work of Lue and Prausnitz (1998a, b), Jiang and Prausnitz (1999a) developed a crossover EOS for pure chain fluids (EOSCF+RG) by incorporating contributions from longwavelength density fluctuations using RG theory. Outside the critical region, the crossover EOSCF+RG reduces to a classical EOS for chain molecules (Hu et aI., 1996, 1999; Liu and Hu, 1998; Jiang et aI., 1998) equivalent to the SAFT equation (Chapman et aI., 1990; Huang and Radosz, 1990, 1991); inside the critical region, it gives non-classical universal critical exponents. This crossover EOS has been used to determine the critical properties of mixtures (Jiang and Prausnitz, 1999b).

This work concerns vapor-liquid equilibria for mixtures of chain fluids. To illustrate applicability, we calculate VLE as well as critical properties and cricondertherms for asymmetric binary mixtures of n-alkane; we compare calculated and experimental results.

## **Theoretical Framework**

For a mixture of chain fluids, we represent each molecule as a homosegmented chain with number density  $\rho_i$ , chain length  $m_i$  and segment diameter  $\sigma_i$ . Interaction between nonbonded chain segments is given by a square-well (SW) potential:

$$
u_{ij}(r) = \begin{cases} \infty & r < \sigma_{ij} \\ -\varepsilon_{ij} & \sigma_{ij} < r < \lambda_{ij} \sigma_{ij} \\ 0 & r > \lambda_{ij} \sigma_{ij} \end{cases}
$$

where  $\sigma_{ij}$  is an additive hard-sphere diameter given by

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(1)

$$
\sigma_{ij} = \frac{\sigma_i + \sigma_j}{2} \tag{2}
$$

Parameters  $\varepsilon_{ij}$  and  $\lambda_{ij}$ , denoting depth of the SW interaction potential and the reduced width for pair ij, respectively, are related to corresponding parameters for pure components by

$$
\varepsilon_{ij} = \sqrt{\varepsilon_i \varepsilon_j} (1 - k_{ij})
$$
 (3)

$$
\lambda_{ij} = \frac{\lambda_i \sigma_i + \lambda_j \sigma_j}{\sigma_i + \sigma_j} \tag{4}
$$

where cross parameter  $k_{ij}$  is obtained from binary experimental data remote from critical conditions. When  $k_{ij} = 0$ , equations (2) and (3) are the well-known Lorentz (energy)-Berthelot (size) approximation (Rowlinson, 1982).

Without loss of generality, but with a view towards fitting experimental data for alkanes, we assume that  $\varepsilon_i$  depends on temperature *T* as proposed by Chen and Kreglewski (1977):

$$
\varepsilon_i = \varepsilon_i^0 (1 + e/k_B T) \tag{5}
$$

where  $k_B$  is Boltzmann's constant;  $e/k_B$  is a constant equal to 5K. Following Barker-Henderson (BH) theory (1967a, b), the temperature dependence of the effective diameter  $\sigma_i$  is

$$
\sigma_i = \sigma_i^0 \left[ 1 - C \exp(-3\varepsilon_i^0 / k_B T) \right]
$$
 (6)

where  $\sigma_i^0$  is a temperature-independent diameter. C is an integration constant; following Chen and Kreglewski (1977), we set  $C = 0.12$ .

The Helmholtz energy density  $f$ , i.e., the Helmholtz energy per unit volume, is obtained from the general form of the EOSCF,

$$
f^{\text{EOSCF}} = f^{\text{id}} + f^{\text{hs}} + f^{\text{sw}} + f^{\text{chain}}.
$$
 (7)

Contributions from ideal-gas, hard-sphere, attractive SW and chain formation are given explicitly in the Appendix.

The equations above constitute the EOS for chain fluids (EOSCF) without RG corrections for a mixture. However, EOSCF performs well only far from the critical region where density fluctuations are very small. Following the work of White (White, 1992; White and Zhang, 1993, 1998), and Lue and Prausnitz (1998a, b), incorporation of contributions from density fluctuations with increasingly longer wavelengths leads to  $EOSCF+RG$ . Recursion relations are used to evaluate the Helmholtz energy density:

should be performed until index *n* approaches infinity; however, we find that  $n = 5$  is sufficient. For binary mixtures considered here, we perform the calculations numerically with a density step  $6/(\pi m_i \sigma_i^3 500)$  for each component; we then smooth the step-wise Helmholtz energy density with a two-dimensional cubic spline function (Press et aI., 1992).

After we calculate the Helmholtz energy density of the system, pressure and chemical potential are obtained from

$$
P = -f + \rho \left(\frac{\partial f}{\partial \rho}\right)_{T,N} \tag{18}
$$

$$
\mu_i = \left(\frac{\partial f}{\partial \rho_i}\right)_{T, V, \rho_{J(i)}}
$$
\n(19)

where  $N$  is the total number of molecules and  $V$  is the total volume.

### **Results and Discussion**

Segment-segment parameters for pure  $n$ -alkanes from methane to  $n$ -hexatriacontane have been correlated previously (Jiang and Prausnitz, 1999a). The chain length is estimated from a simple empirical relation with carbon number C<sub>i</sub> by  $m_i = 1 + (C_i-1)/3$ . Interaction potential  $\varepsilon_i^0$ , segment diameter  $\sigma_i^0$  and square-well width  $\lambda_i$  are optimized to fit experimental data outside the critical region. To incorporate contributions from long-wavelength density fluctuations inside the critical region, we set cut-off length  $L = 11.5 \text{ Å}$  and select a suitable parameter  $\Phi_i$  to fit the measured pure-component critical properties.

We fit cross-parameter  $k_{ij}$  to measured vapor-liquid equilibrium data remote from the critical region for binary *n*-alkanes mixtures containing  $CH_4$  or  $C_2H_6$ . Table 1 gives the optimized  $k_{ij}$  and corresponding data sources. Figure 2 shows that parameter  $k_{ij}$  rises linearly with low carbon number of the second component, and then rapidly approaches a constant. Triangles are for binary mixtures containing CH<sub>4</sub>; circles are for those containing C<sub>2</sub>H<sub>6</sub>. The trend shown in Figure 2 was observed more than 20 years ago (Donohue and Prausnitz, 1978). Upon increasing the carbon number of the second component, the rising difference between the two components raises  $k_{ij}$ . However, upon further increase in carbon number (chain length) of

$$
f_n(\rho) = f_{n-1}(\rho) + \delta f_n(\rho) \tag{8}
$$

$$
\delta f_n(\rho) = -K_n \ln \frac{\Omega_n^s(\rho)}{\Omega_n^l(\rho)}, \quad 0 \le \rho < \rho^{\max}/2
$$
 (9.a)

$$
\delta f_n(\rho) = 0, \qquad \rho^{\max}/2 \le \rho < \rho^{\max} \qquad (9.b)
$$

The zero-order solution  $f_0$  is approximated by Eq.(7);  $\Omega_n^l$  and  $\Omega_n^s$  are integrals over the amplitudes of the density fluctuations for long-range attraction and for short-range attraction, respectively;  $\rho$  is total number density,  $\rho^{\max}$  is the maximum possible density, and

$$
K_n = \frac{k_{\rm B}T}{2^{3n}L^3}
$$
 (10)

$$
\Omega_n^{\alpha}(\rho) = \int_0^{\rho_1} dz_1 \cdots \int_0^{\rho_M} dz_M \, \exp[-\overline{E}_n^{\alpha}(\rho, z)/K_n], \quad \alpha = s, l \tag{11}
$$

$$
\overline{E}_n^{\alpha}(\rho, z) = \frac{\overline{f}_n^{\alpha}(\rho + z) + \overline{f}_n^{\alpha}(\rho - z)}{2} - \overline{f}_n^{\alpha}(\rho), \qquad \alpha = s, l \tag{12}
$$

$$
\bar{f}_n^l(\rho) = f_{n-1}(\rho) + \sum_i \sum_j b_{ij} \rho_i \rho_j \tag{13}
$$

$$
\bar{f}_n^s(\rho) = f_{n-1}(\rho) + \sum_i \sum_j b_{ij} \rho_i \rho_j \frac{\Phi_{ij} \xi_{ij}^2}{2^{2n+1} L_{ij}^2}.
$$
 (14)

where  $z_i$  ( $i = 1, 2, \dots M$ ; M is the total number of components) is the integral variable within [0,  $\rho_i$ ];  $b_{ij}$  is the interaction volume and  $\xi_{ij}$  refers to the range of the attractive potential. They are related to the parameters of the SW potential by

$$
b_{ij} = \frac{2\pi}{3} \varepsilon_{ij} (\lambda_{ij} \sigma_{ij})^3
$$
 (15)

$$
\xi_{ij} = \frac{1}{\sqrt{5}} (\lambda_{ij} \sigma_{ij})
$$
 (16)

Parameter  $L_{ij}$  is the cut-off length; we use the same *L* for all components.  $\Phi_{ij}$  is the average gradient of the wavelet function (Battle, 1992, 1994), given by

$$
\Phi_{ij} = \frac{\Phi_i \sigma_i + \Phi_j \sigma_j}{\sigma_i + \sigma_j} \tag{17}
$$

The above recursion procedure can be interpreted in terms of contributions to the Helmholtz energy density; this procedure gives the ratio of non-mean-field contributions to mean-field contributions at gradually increasing long wavelengths. In principle, the recursion

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the second compoent, the first component cannot "see" the increasing difference between itself and the second components; therefore,  $k_{ij}$  becomes constant.

Figure 3(a) shows vapor-liquid equilibria for binary mixtures of  $CH_4$  with  $C_3H_8$ ; Figure 3(b) shows the corresponding equilibrium ratios defined by

$$
K_i = y_i / x_i \tag{20}
$$

where *y* and *x* refer to mole fraction in the vapor phase and liquid phase, respectively. The open points represent experimental data (Knapp et aI., 1982); dashed and solid lines are calculated from EOSCF and EOSCF+RG, respectively. The critical points, indicated by solid triangles, are estimated by extrapolation of a  $K-P$  plot to  $K = 1.0$  as recommended by Sage and others (Sage et aI., 1940, 1942; Reamer, et aI., 1950; Kahre, 1974). At the critical point, we have

$$
\left(\frac{\partial P}{\partial x_1}\right)_T = \left(\frac{\partial P}{\partial y_1}\right)_T = 0 \qquad \text{at } x_1 = y_1 \tag{21}
$$

and

$$
\left(\frac{\partial P}{\partial K_1}\right)_T = \left(\frac{\partial P}{\partial K_2}\right)_T = 0 \quad \text{at } K_1 = K_2 = 1.
$$
 (22)

EOSCF is deficient in its description of phase behavior in the critical region; however, EOSCF+RG repairs this deficiency because density fluctuations are reasonably incorporated. Far from the critical region, EOSCF+RG theory reduces to the original EOSCF where the latter is reliable. In general, EOSCF+RG gives good agreement with experiment in both regions.

Figures 4(a) and (b) show vapor-liquid equilibria and equilibrium ratios for binary mixtures of CH<sub>4</sub> with n-C<sub>4</sub>H<sub>10</sub>. Legends are the same as those in Figure 3(a). The solid circle denotes the cricondentherm where

$$
\left(\frac{\partial P}{\partial y_1}\right)_T = \infty \tag{23}
$$

In a pressure-temperature plot at fixed composition, the cricondentherm condition is

$$
\left(\frac{\partial P}{\partial T}\right)_y = \infty \tag{24}
$$

Figure 4(c) shows critical and cricondentherm properties for binary mixtures of CH<sub>4</sub> with n- $C_4H_{10}$ . Points represent experimental data (Sage et al., 1940) and lines are calculated from

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EOSCF+RG. Triangles and solid lines denote critical properties; circles and dashed lines show cricondenthenn properties. Agreement with experiment is good.

Figure 5, similar to Figure 4, gives results for binary mixtures of  $CH_4$  with *n*-C<sub>5</sub>H<sub>12</sub>. The experimental data for vapor-liquid equilibria are from Knapp et al. (1982); critical and cricondenthenn properties are from Sage (1942), and Berry and Sage (1970).

Figures 6 and 7 show vapor-liquid equilibria for binary mixtures of CH<sub>4</sub> with *n*-C<sub>12</sub>H<sub>26</sub> and *n-C16*H*34,* respectively. The.points show experimental data (Rijkers et aI., 1992; Glaser et aI., 1985); dashed and solid lines are calculated from EOSCF and EOSCF+RG, respectively. EOSCF+RG provides much improvement because it takes into account the contribution from density fluctuations in the critical region.

Figure 8 shows the bubble-point curve for three binary mixtures of  $CH_4$  with  $n-C_{20}H_{42}$ ,  $n-$ C28Hs8, and *n-C36H74.* Points show experimental data (Darwish et aI., 1993; Huang et aI., 1987, 1988a, b); solid lines are calculated from EOSCF+RG. Good agreement is obtained.

Finally, Figure 9 shows vapor-liquid equilibria for binary mixtures of  $C_2H_6$  with n-C<sub>20</sub>H<sub>42</sub>. Experimental data are from Peters et al. (1987, 1988). Similar to binary mixtures containing  $CH<sub>4</sub>$ , remote from the critical region, both EOSCF and EOSCF+RG give almost the same results; however, in the critical region, EOSCF+RG is significantly superior.

# **Conclusion**

A recently developed crossover equation of state for pure chain fluids, EOSCF+RG, has been extended to mixtures of chain fluids. This EOSCF+RG is able to describe the phase equilibria of mixtures both far-from and near-to the critical region. Far from the critical region, where density fluctuations are small and RG corrections are negligible, EOSCF+RG reduces to the classical EOSCF. However, near-to and in the critical region where density fluctuations are large, EOSCF fails due to its mean-field nature. Incorporating the essential contribution from . density fluctuations, EOSCF+RG significantly improves agreement with experiment.

For the binary mixtures of  $n$ -alkanes illustrated here, we use the square-well segmentsegment parameters for pure components from our previous work; in addition, we use crossparameter  $k_{ij}$  optimized by fitting equilibria data remote from the critical region. We find that all parameters vary smoothly with the carbon numbers of the components. Therefore, for those binary  $n$ -alkanes systems where experimental data are not available, we can with confidence

predict phase equilibria for a wide range of conditions, including the critical region. We can also model n-alkanes as Lennard-Jones chains and optimize the Lennard-Jones segmentsegment parameters (BIas and Vega, 1997, 1998a, 1998b).

In general, EOSCF+RG gives good results, much better than those from EOSCF in the critical region. However, we also observe some deviations for EOSCF+RG from experiment. These deviations are not primarily due to RG theory; rather, they result from inadequacies in the classical equation of state remote from critical conditions. Because the classical EOSCF is a first-order perturbation theory, higher-order correlations between the segments in the chain are neglected; also, a crude approximation is used here to subtract contributions from longwavelength density fluctuations in EOSCF; perhaps, some deviation is due to neglect of manybody interactions (Elrod and Saykally, 1994; Adidharma, and Radosz, 1998; Sadus, 1998a, b; Marcelli and Sadus, 1999) that may be important at high densities.

To use the crossover equation of state described here, the first task is to evaluate numerically the Helmholtz energy density through the recursion relations. We perfonn these calculations with a suitable density step  $\rho_i^{max}/N_{step}$  for each component. In our studies for pure components and binary mixtures, we use  $N_{\text{step}} = 500$  to achieve good accuracy with reasonable computational time. However, for ternary mixtures, with  $N_{\text{step}} = 500$ , there is not enough memory in our PC to perform the calculations. To maintain accuracy, we cannot significantly reduce  $N_{\text{step}}$ . The severity of this computational problem increases worse as the number of components in the mixture rises. We are currently making efforts toward solving this computational problem.

While this work discusses the VLE for mixtures of  $n$ -alkanes, it can also be used to describe VLE for fluid mixtures containing a polymer like polyethylene (Folie and Radosz, 1995; Luettmer-Strathmann, et aI., 1998; Orbey, et aI., 1998); for liquid-liquid equilibria of mixtures of small molecules (Greer, 1978; Hölscher, et al., 1986) or polymer with solvent (Hino and Prausnitz, 1997; Liu and Hu, 1998; Vetere, 1998) and for solid-fluid equilibria in natural-gas systems (Won, 1986; Suleiman and Eckert, 1995a, b; Flöter, et al., 1997, 1998; Sun and Teja, 1998; Teja, et aI., 1998; Coutinho, 1998) or for the solubility of a solid polymer in dense fluids (O'Neill, et aI., 1998; Pan and Radosz, 1998, 1999).

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## **Notation**

- $b_{ii}$  = interaction volume for *ij* pair
- $A = Helmholtz$  energy

 $C =$  integration constant in Barker-Henderson theory

 $f =$  Helmholtz energy density

 $g_{ii}(r)$  = pair correlation function for *ij* pair

 $k_B$  = Boltzmann constant

 $k_{ij}$  = cross-parameter for binary mixture *ij* pair

 $K_i$  = equilibrium ratio

 $L = \text{cut-off length}$ 

 $m_i$  = chain length of molecule i

 $M =$  total number of components

 $n_i$  = mole number of component i

 $N =$  total number of molecules

 $N_{\text{step}}$  = step of density

 $P$  = pressure

 $P^c$  = critical pressure of mixture

 $r =$  center-to-center distance

 $SW = square-well potential$ 

 $T^c$  = critical temperature of mixture

 $u =$ interaction potential

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 $V =$ total volume of the system

- $x_i$  = mole fraction of component *i* in the liquid phase
- $y_i$  = mole fraction of component *i* in the vapor phase
- $y_{ii}(r)$  = cavity correlation function for ij pair
	- $z =$  integral variable for density

#### *Greek letters*

- $\rho_i$  = number density of molecule *i*
- $\sigma_i$  = segment diameter of molecule (or segment) i
- $\varepsilon_i$  = SW interaction well-depth of molecule (or segment) i
- $\lambda_i$  = SW interaction range of molecule (or segment) *i*
- $A_i$  = de Broglie thermal wavelength of molecule *i*
- $\mu_i$  = chemical potential of component *i*
- $\Phi_i$  = average gradient of wavelet function for component *i*

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#### Appendix: Helmholtz Energy Density for a Mixture of Square-Well Chain Fluids

The Helmholtz energy density for the mixture of square-well chain fluids has four contributions:

$$
f^{\text{EOSCF}} = f^{\text{id}} + f^{\text{hs}} + f^{\text{sw}} + f^{\text{chain}} \tag{A.1}
$$

The contribution from the ideal gas is

$$
fid = kB T \sum_{i} [\rho_i \ln(\rho_i A_i^3) - \rho_i]
$$
 (A.2)

where  $\rho_i$  is the number density for component *i*;  $A_i$  denotes the de Broglie thermal wavelength of molecule *i.* 

The hard-sphere interaction, given by Boublik (1970) and Mansoori et aI. (1971), is the socalled BMCSL equation

$$
f^{\text{hs}} = k_{\text{B}} T \left[ \left( \zeta_2^3 / \zeta_3^2 - \zeta_0 \right) \ln \Delta + \frac{\pi \zeta_1 \zeta_2 / 2 - \zeta_2^3 / \zeta_3^2}{\Delta} + \frac{\zeta_2^3 / \zeta_3^2}{\Delta^2} \right] \tag{A.3}
$$

where  $\zeta_l = \sum m_i \rho_i \sigma_i^l$  and  $\Delta = 1 - \pi \zeta_3 / 6$ . i

The contribution from the SW attractive potential is estimated by the second-order Baker-Henderson perturbation theory (Barker and Henderson, 1967a, b)

$$
f^{\rm sw} = \frac{1}{\zeta_0} \sum_{i} \sum_{j} m_i m_j \rho_i \rho_j (a_1^{ij} + a_2^{ij} / k_{\rm B} T). \tag{A.4}
$$

The mean-attractive energy  $a_i^{\mu}$  is given by a compact expression from the mean-value theorem (Gil-Villegas et aI., 1997; Galindo et aI., 1998; McCabe et aI., 1998, 1999; McCabe and Jackson, 1999)

$$
a_1^{ij} = -2/3\pi \zeta_0 \sigma_{ij}^3 \varepsilon_{ij} (\lambda_{ij}^3 - 1) g_{ij}^{\text{hs}} (\sigma_{ij}, \zeta_3^{\text{eff}})
$$
 (A.5)

where the pair correlation function of hard-spheres at contact is evaluated at an effective  $\zeta_3^{\text{eff}}$ ,

$$
g_{ij}^{\text{hs}}(\sigma_{ij}) = \frac{1}{\Delta} + \frac{\pi \sigma_i \sigma_j \zeta_2}{4\Delta^2 \sigma_{ij}} + \frac{\pi^2 \sigma_i^2 \sigma_j^2 \zeta_2^2}{72\Delta^3 \sigma_{ij}^2}
$$
(A.6)

with

$$
\zeta_3^{\text{eff}} = c_1 \zeta_3 + c_2 \zeta_3^2 + c_3 \zeta_3^3. \tag{A.7}
$$

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Coefficients  $c_n$  are calculated by the matrix (Gil-Villegas et al., 1997; Galindo et al., 1998; McCabe et aI., 1998, 1999; McCabe and Jackson, 1999)

$$
\begin{pmatrix} c_1 \ c_2 \ c_3 \end{pmatrix} = \begin{pmatrix} 2.25855 & -1.50349 & 0.249434 \ -0.669270 & 1.40049 & -0.827739 \ \ 10.1576 & -15.0427 & 5.30827 \ \end{pmatrix} \begin{pmatrix} 1 \ \lambda_{ij} \ \lambda_{ij}^2 \end{pmatrix}
$$
 (A.8)

The second perturbation term  $a_2^{\hat{y}}$  describing fluctuations of the attractive energy is given by

$$
a_2^{\ddot{y}} = \frac{\varepsilon_{\ddot{y}} \zeta_0^2 \Delta^4}{2(\zeta_0 \Delta^2 + \pi \zeta_1 \zeta_2 \Delta + \pi^2 \zeta_2^3 / 4)} \frac{\partial a_1}{\partial \zeta_0}.
$$
 (A.9)

The contribution from chain formation is

$$
f^{\text{chain}} = k_{\text{B}} T \sum_{i} \rho_i (1 - m_i) \ln y_i^{\text{sw}}(\sigma_i). \tag{A.10}
$$

where cavity correlation function  $y_{ij}^{sw}(\sigma_{ij})$  at contact is defined by

$$
y_{ij}^{\text{sw}}(\sigma_{ij}) = g_{ij}^{\text{sw}}(\sigma_{ij}) \exp(-\varepsilon_{ij}/k_{\text{B}}T)
$$
 (A.11)

with

$$
g_{ij}^{\rm sw}(\sigma_{ij}) = g_{ij}^{\rm hs}(\sigma_{ij}) + \frac{1}{2\pi k_{\rm B}T\sigma_{ij}^3} \left(3\frac{\partial a_i^{ij}}{\partial \zeta_0} - \frac{\lambda_{ij}}{\zeta_0} \frac{\partial a_i^{ij}}{\partial \lambda_{ij}}\right).
$$
 (A.12)

Component $j$	$k_{ii}$ ( $i = CH_4$ )	data source	$k_{ij}$ ( $i = C_2H_6$ )	data source
$C_2H_6$	0.0048	Knapp et al. (1982)		
$C_3H_8$	0.0150	Knapp et al. (1982)	0.0095	Knapp et al. (1982)
$n - C_4H_{10}$	0.0255	Knapp et al. (1982)	0.0163	Knapp et al. (1982)
$n$ -C <sub>5</sub> H <sub>12</sub>	0.0381	Knapp et al. (1982)	0.0220	Knapp et al. (1982)
$n - C_6H_{14}$	0.0490	Knapp et al. (1982)	0.0263	Knapp et al. (1982)
$n - C_7H_{16}$	0.0584	Knapp et al. (1982)	0.0312	Knapp et al. (1982)
$n-C_8H_{18}$	0.0704	Knapp et al. (1982)	0.0375	Knapp et al. (1982)
$n\text{-}C_9H_{20}$	0.0801	Knapp et al. (1982)		
$n - C_{10}H_{22}$	0.0874	Knapp et al. (1982)	0.0455	Knapp et al. (1982)
$n - C_{12}H_{26}$	0.0910	Rijkers et al. (1992)	0.0485	Lee et al. (1969)
$n - C_{16}H_{34}$	0.0920	Glaser et al. (1985)	0.0495	Goede et al. (1989)
$n - C_{20}H_{42}$	0.0932	Darwish et al. (1993)	0.0489	Peters et al. (1987)
		Huang et al. (1988b)		Peters et al. (1988)
$n - C_{28}H_{58}$	0.0930	Darwish et al. (1993)	0.0487	Gasem et al. (1989)
		Huang et al. (1988a)		Huang et al. (1988a)
$n - C_{36}H_{74}$	0.0937	Darwish et al. (1993)	0.0490	Gasem et al. (1989)
		Huang et al. (1987)		Huang et al. (1987)

Table 1. Cross-Parameter  $k_{ij}$  for Binary Mixtures of CH<sub>4</sub> Series and C<sub>2</sub>H<sub>6</sub> Series, Respectively, Evaluated from Experimental Data Remote from Critical Conditions

 $\frac{1}{2}$ 

#### Figure captions:

- Figure 1. Schematic illustration of retrograde-condensation (vaporization) phenomena. (solid curve: bubble point; dashed curve: dew point. point C: critical point; A: cricondenbar; B: cricondentherm. line 1: isothermal retrograde condensation; line 2: isobaric retrograde vaporization.
- Figure 2. Dependence of cross-parameter  $k_{ii}$  on the carbon number of the second component. (triangles: CH<sub>4</sub> series; circles:  $C_2H_6$  series).
- Figure 3(a). Vapor-liquid equilibria for  $\text{CH}_4(1)$ -C<sub>3</sub>H<sub>8</sub>(2) mixtures. (open points: experiment; dashed lines: EOSCF; solid lines: EOSCF+RG; solid triangles: critical points)

Figure 3(b). Equilibrium ratios for CH<sub>4</sub>(1)-C<sub>3</sub>H<sub>8</sub>(2) mixtures. Legend as in Figure 3(a).

Figure 4(a). Vapor-liquid equilibria for  $\text{CH}_4(1)-n-\text{C}_4\text{H}_{10}(2)$  mixtures. (open points: experiment; dashed lines: EOSCF; solid lines: EOSCF+RG; solid triangles: critical points; solid circles: cricondentherms).

Figure 4(b). Equilibrium ratios for  $CH_4(1)-n-C_4H_{10}(2)$  mixtures. Legend as in Figure 3(a).

Figure 4(c). Critical properties and cricondentherm properties for  $CH_4(1)-n-CAH_{10}(2)$  mixtures. (triangles and solid lines: critical properties; circles and dashed lines: cricondentherm properties).

Figure 5(a). Vapor-liquid equilibria for  $CH_4(1)-n-C_5H_{12}(2)$  mixtures. Legend as in Figure 4(a).

Figure 5(b). Equilibrium ratio for CH<sub>4</sub>(1)-n-C<sub>5</sub>H<sub>12</sub>(2) mixtures. Legend as in Figure 4(b).

Figure 5(c). Critical properties and cricondentherm properties for  $CH_4(1)-n-C_5H_{12}(2)$  mixtures. Legend as in Figure  $4(c)$ .

- Figure 6. Vapor-liquid equilibria for CH<sub>4</sub>(1)-n-C<sub>12</sub>H<sub>26</sub>(2) mixtures at 303.15K. Legend as in Figure 3(a).
- Figure 7. Vapor-liquid equilibria for  $CH_4(1)-n-C_{16}H_{34}(2)$  mixtures at 320.0K. Legend as in Figure 3(a).
- Figure 8. Bubble pressures at 373.15K for CH<sub>4</sub>(1)-n-C<sub>20</sub>H<sub>42</sub>(2), CH<sub>4</sub>(1)-n-C<sub>28</sub>H<sub>58</sub>(2) and  $CH<sub>4</sub>(1)-n-C<sub>36</sub>H<sub>74</sub>(2)$ , respectively. (points: experimental data; lines: EOSCF+RG).
- Figure 9. Vapor-liquid equilibria for  $C_2H_6(1)-n-C_{20}H_{42}(2)$  mixtures at 350.0K. Legend as in Figure 3(a).



Pressure

# Temperature



Fig.

Carbon Number of Second Component

 $Fig3(a)$ 



 $x_1, y_1$ 

 $P(MPa)$ 



 $P$  (MPa)

 $Fig 4(a)$ 

 $P(MPa)$ 



 $x_1, y_1$ 



 $F_1$ 

 $0.1$  $\overline{4}$ 6  $10$  $12$  $14$  $\overline{0}$ 8  $\overline{2}$ 

 $P$  (MPa)

 $Fig4C$ 

 $\aleph$ 



 $F(Mb^g)$ 

 $P(MPa)$ 



 $x_1, y_1$ 

Fig

100 10  $K_1$  $\mathbf{1}$  $K_2$  $0.1$ 16 12 8  $\overline{0}$  $\overline{4}$ 

Fig5Cb)

 $P(MPa)$ 



 $F(Mb)$ 

 $F_{\delta}$ 

Fig.G

 $P(MPa)$ 



 $x_1, y_1$ 



 $x_1, y_1$ 

 $F<sub>0</sub>$ 

 $P(MPa)$ 



 $\overline{x}_1$ 

 $\overline{F}$ ig.  $\mathscr G$ 

 $P(MPa)$ 



 $x_1, y_1$ 

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