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STEEL REAR PLATE

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**Author** 

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**Publication Date** 

1979



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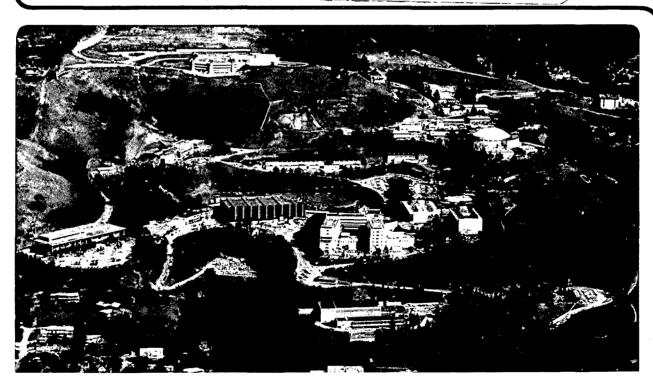
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ENGINEE	RING NOTE	D32221	M5284	1 of 2
AUTHOR	DEPARTMENT	LOCATION	DATE	
MARTIN FONG	MECHANICAL	B29C	1/9/79	
PROGRAM - PROJECT - JOB				
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VACUUM VESSE	<u> </u>			
TITLE				
STEEL . REAR	PLATE			

THE MATERIAL SELECTED IS AISI C1008 PLATE.

IT IS SELECTED FOR ITS MAGNETIC PROPERTY. THE C1008

MATERIAL IS NOW ASME CODE APPROVED, BUT THE CODE

DOES NOT INCLUDE 15 PSIG VESSELS. THE CODE SAFETY

FACTOR OF FOUR IS FOLLOWED IN CALCULATING THE

PLATE THICKNESS. THE TENSILE STRENGTH OF THE C1008

IS TESTED BY ANAMET LABORATORY, INC IN BERKELEY,

CALIFORNIA.

TENSILE STRENGTH OF C1008

LONGITUDINAL DIRECTION = 45,300 PSI

TRANSVERSE DIRECTION = 45,600 PSI

THE ALLOWABLE STRESS, SA, IS

$$S_{R} = \frac{45,300}{4} = 11,325 psi$$

**V** 

THE FLAT PLATE EQUATION FROM UG-39 (d) 2 ON p. 37 (ALSO ON P. 16 OF M.5207) IS

$$t = d \sqrt{2 \left( \frac{CP}{S_AE} + \frac{1.9 \text{ Whg}}{S_AE d^3} \right)}$$

$$d = 90.6 \text{ in}$$

$$C = 0.3$$
FR

Whg = 221,184 in-16

P = 15 psi

E = 1

FROM P. 15 OF M 5207

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	-M. FONG	MECHANICAL	B29C	1/9/7	9

THE MINIMUM THICKNESS IS  $t_{min} = 90.6 \sqrt{2} \left[ \frac{(0.3)(15)}{(1,325)(1)} + \frac{(1.9)(221,184)}{(1,325)(1)(90.6)^{3}} \right]$ 

= 2.710 in

THE PLATE THICKNESS WILL BE 2.875 IN. PLUGGING
THE THICKNESS BACK INTO THE EQUATION AND
CALCULATE SA

 $S_A = 2 \left( \frac{90.6}{2.875} \right)^2 \left[ (0.3)(15) + \frac{(1.9)(221,184)}{(90.6)^3} \right] = 10,060 \text{ psi}$ 

45A= 4(10,060) = 40,240 psi

THIS MEANS THE 2.875 IN CLOOB PLATE CAN HAVE A 5,000 PSI VARIATION IN THE MINIMUM TENSILE STRENGTH

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